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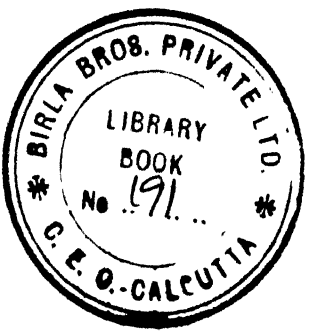

HEATING VENTILATING AIR CONDITIONING GUIDE 1948

INDEX

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HEATING VENTILATING
AIR CONDITIONING
GUIDE 1948

●

TECHNICAL DATA SECTION

CHAPTERS 1-52 and PAGES 1-912

●

Cross Reference to Subjects in Chapters 1-52 Alphabetically Listed

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PREFACE TO THE 26th EDITION

THE 26th edition of The Heating, Ventilating, Air Conditioning Guide continues the tradition of previous Guides in presenting current engineering practice and up-to-date products of manufacturers.

Among the chapters given most extensive revision in the 1948 edition, the following should be noted:

Chapter 10, Air Contaminants, contains revised limits for toxic gases, vapors, fumes, mists and dusts, in conformity with recent conclusions of industrial hygienists.

Chapter 11, Instruments and Measurements, has been enlarged to include a greater number of instruments, as well as more information on test methods and the use of instruments.

Chapter 12, Physiological Principles, incorporates some additional findings based upon recent research.

Chapter 13, Air Conditioning in the Prevention and Treatment of Disease, has been revised to agree with current thought and research.

Chapter 14, Heating Load, includes an enlarged list of approximately 350 localities, including city office and airport stations, for which weather data and design temperatures are given. The list includes data obtained from the U. S. Weather Bureau and Canadian Air Services, Meteorological Division. A new map showing isotherms of outdoor temperature has been provided.

Chapter 15, Cooling Load, has been increased to 45 pages to permit inclusion of an enlarged list of 315 localities for which weather data are listed. The chapter has also been rewritten to assist the user in applying the principles of periodic heat flow, and the data from most recent ASHVE research on solar heat transmission.

Chapter 20, Estimating Fuel Consumption for Space Heating, includes an enlarged list of 211 U. S. cities and 25 Canadian cities showing monthly degree-day values. The information has been obtained from latest statistics of the U. S. Weather Bureau and Canadian Air Services, Meteorological Division.

Chapter 21, Gravity Warm Air Systems, has been rearranged to facilitate use of the design tables.

Chapter 22, Mechanical Warm Air Systems, contains an added section referring to method of designing large systems.

In Chapter 23, Steam Heating Systems and Piping, revised descriptions of various types of systems keep the chapter up to date. Many new diagrams have been added to illustrate current practice.

In Chapter 25, Radiators, Convectors and Coils, there has been added a section on baseboard radiation.

In Chapter 26, Unit Heaters, Unit Ventilators, Unit Humidifiers, piping diagrams and text have been changed to comply with current practice.

In Chapter 27, Pipe, Fittings and Welding, the section on welding has been expanded with reference to proper welding procedure and applicable code requirements.

Chapter 30, Electric Heating, includes an enlarged list of pertinent references.

Chapter 32, Fans, has been improved by addition of typical sound level curves to the fan performance curves. A new diagram illustrating accepted designations of direction of rotation and discharge for fans has been added. The chapter also contains a section on attic fans which has been transferred from Chapter 36.

Chapter 34, Automatic Control, has been rewritten to include more detailed treatment of typical controls and control combinations for all types of systems.

Chapter 36, Unit Air Conditioners, Unit Air Coolers, has been revised and improved in both text and illustrations.

Chapter 37, Spray Apparatus, has been rearranged and includes new information on design and use of air washers, cooling towers and spray ponds.

Chapter 40, Air Distribution, has been completely revised by the ASHVE Technical Advisory Committee on Air Distribution and Air Friction. It contains new definitions and formulas for air distribution. Charts have been included for graphical solution of problems involving flow of air from slots and jets, residual velocity and size of openings. Information on location of outlets has been enlarged, and more information is given on control of air streams in spaces.

Chapter 43, Central Systems for Air Conditioning has been simplified, with improvement in presentation. New diagrams are used to illustrate equipment arrangement and operation.

Chapter 45, Industrial Air Conditioning, has been revised to emphasize growing importance of applications in this field, and the need for safeguarding the health and efficiency of workers as well as the quality of the manufactured product.

Chapter 47, Drying Systems, has been revised and new material has been added.

Chapter 48, Transportation Air Conditioning, has been revised to keep the chapter up to date with recent progress in this phase of air conditioning.

Chapter 50, Water Services, has been enlarged by the addition of a friction and capacity chart applicable to copper tubing. Charts for both standard I. P. S. pipe and for copper tubing have been extended to small capacity and can be used for calculating friction loss for panel heating installations.

Chapter 51, Corrosion and Water Formed Deposits, Causes and Prevention, is a new chapter presenting corrosion theory and also current practice in prevention of corrosion in heating, ventilating and air conditioning systems. The chapter was prepared by the ASHVE Technical Advisory Committee on Corrosion.

Chapter 52, Codes and Standards, contains many new codes which add to the growing usefulness of this convenient list of references to codes applicable to heating, ventilating and air conditioning.

A cross index of the Technical Data Section is included.

The 26th edition of The Guide, like its predecessors, represents an up-to-date collection of practical and useful data and design information provided through the kind cooperation and generosity of many members and friends of the Society. Among those who have been especially helpful in the preparation of this edition, we are pleased to list the following, and to acknowledge the great value of their contributions:

C. M. Ashley	F. W. Hutchinson	S. I. Rottmayer
Merrill Bernard	E. F. Hyde	H. J. Ryan
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G. E. Hulse	L. J. Riconda	G. D. Winans
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In the Catalog Data Section there is an enlarged representation of 230 manufacturers of heating, ventilating and air conditioning equipment whose products are presented in a careful and unexaggerated manner. This section provides a ready reference to products needed in the design and installation of all types of systems. The products are listed in a convenient cross index from which the names of the manufacturers of any desired type of product can readily be found.

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Chapter 1

TERMINOLOGY

Glossary of Physical and Heating, Ventilating, Refrigerating and Air Conditioning Terms Used in the Text

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Absolute Zero: The zero from which absolute temperature is reckoned. Approximately −273.2 C or −459.8 F.

Absorbent: A sorbent which changes physically or chemically, or both, during the sorption process.

Absorption: The action of a material in extracting one or more substances present in an atmosphere or mixture of gases or liquids; accompanied by physical change, chemical change, or both, of the sorbent.

Acceleration: The time rate of change of velocity *i.e.*, the derivative of velocity with respect to time. In the cgs system the unit of acceleration is the centimeter per (second) (second), in the fps system the unit is the foot per (second) (second) $a = \frac{dv}{dt}$.

Acceleration Due to Gravity: The rate of gain in velocity of a freely falling body, the value of which varies with latitude and elevation. The international gravity standard has the value of 980.665 cm per (second) (second) or 32.174 ft per (second) (second) which is the actual value of this acceleration at sea level and about 45 deg latitude.

Adiabatic: An adjective descriptive of a process such that no heat is added to or taken from a substance or system undergoing the process.

Adsorbent: A sorbent which does not change physically or chemically during the sorption process.

Adsorption: The action, associated with surface adherence, of a material in extracting one or more substances present in an atmosphere or mixture of gases and liquids unaccompanied by physical or chemical change. Commercial adsorbent materials have enormous internal surfaces.

Aerosol: An assemblage of small particles, solid or liquid, suspended in air. The diameters of the particles may vary from 100 microns down to 0.01 micron or less, *e.g.* dust, fog, smoke.

Air Cleaner: A device designed for the purpose of removing air-borne impurities such as dusts, gases, vapors, fumes and smokes. (Air cleaners include air washers, air filters, electrostatic precipitators and charcoal filters.)

Air Conditioning: The simultaneous control of all or at least the first three of those factors affecting both the physical and chemical conditions of the atmosphere within any structure. These factors include temperature, humidity, motion, distribution, dust, bacteria, odors and toxic gases, most of which affect in greater or lesser degree human health or comfort. (*See Comfort Air Conditioning.*)

Air, Dry: In psychrometry, air unmixed with, or containing no, water vapor.

Air, Saturated: A mixture of dry air and saturated water vapor, all at the same dry-bulb temperature.

Air, Standard: Air with a density of 0.075 lb per cubic foot and an absolute viscosity of 1.22×10^{-5} lb mass per (foot) (second). This is substantially equivalent to dry air at 70 F and 29.92 in. (Hg) barometer.

Air Washer: An enclosure in which air is drawn or forced through a spray of water in order to cleanse, humidify, or dehumidify the air.

Anemometer: An instrument for measuring the velocity of a fluid.

Aspect Ratio: In air distribution outlets the ratio of the length of the core of a grille, face or register to the width.

In rectangular ducts the ratio of the width to the depth.

Atmospheric Pressure: The pressure due to the weight of the atmosphere. It is the pressure indicated by a barometer. *Standard Atmospheric Pressure* or *Standard Atmosphere* is the pressure of 76 cm of mercury having a density of 13.5951 grams per cubic centimeter, under standard gravity of 980.665 cm per (second) (second). It is equivalent to 14.696 lb per square inch or 29.921 in. of mercury at 32 F.

Baffle: A surface used for deflecting fluids, usually in the form of a plate or wall.

Blast Heater: A set of heat transfer coils or sections used to heat air which is drawn or forced through it by a fan.

Blow (throw): In air distribution, the distance an air stream travels from an outlet to a position at which air motion along the axis reduces to a velocity of 50 fpm.

For unit heaters, the distance an air stream travels from a heater without a perceptible rise due to temperature difference and loss of velocity.

Boiler Heating Surface: That portion of the surface of the heat-transfer apparatus in contact with the fluid being heated on one side and the gas or refractory being cooled on the other, in which the fluid being heated forms part of the circulating system; this surface shall be measured on the side receiving heat. This includes the boiler, water walls, water screens, and water floor. (*A.S.M.E.* Power Test Codes, Series 1929.)

Boiler Horsepower: The equivalent evaporation of 34.5 lb of water per hour from and at 212 F. This is equal to a heat output of 970.3 × 34.5 = 33,475 Btu per hour.

British Thermal Unit: Classically the Btu is defined as the quantity of heat required to raise the temperature of 1 lb of water 1 Fahrenheit degree. By this definition the exact value depends upon the initial temperature of the water. Several values of the Btu are in more or less common use, each differing from the others by a slight amount. One of the more common of these is the *mean Btu* which is defined as 1/180 of the heat required to raise the temperature of 1 lb of water from 32 F to 212 F at a constant atmospheric pressure of 14.696 lb per square inch absolute.

For most accurate work the *International Table* (I.T.) Btu is usually used. This is defined by the relation: 1 (I.T.) Btu per (pound) (Fahrenheit degree) = 1 (I.T.) calorie per (gram) (Centigrade degree). This value corresponds to the amount of heat required to raise the temperature of 1 lb of water 1 Fahrenheit degree at 58 F and also at 149 F. The *mean Btu* corresponds to 1.0008 (I.T.) Btu.

By-Pass: A pipe or duct, usually controlled by valve or damper, for conveying a fluid around an element of a system.

Calorie (Gram Calorie): Classically the calorie is defined as the quantity of heat required to raise the temperature of 1 gram of water 1 Centigrade degree. By this definition the exact value depends upon the initial temperature of the water. Several values of the calorie are in more or less common use, each differing from the others by a slight amount. Among these are the *15 C calorie* and the *17½ C calorie*. The *mean calorie*, *i.e.* 1/100 the quantity of heat required to raise the temperature of 1 gram of water from 0 C to 100 C, is also extensively used.

For the most accurate work the International Table (I.T.) calorie, defined in terms of the international electrical units, is usually used: 1 (I.T.) calorie = 1/860 international watt-hour = 3,600/860 international watt-seconds or international joules.

The kilocalorie = 1,000 cal.

Central Fan System: A mechanical indirect system of heating, ventilating, or air conditioning, in which the air is treated or handled by equipment located outside the rooms served, usually at a central location, and is conveyed to and from the rooms by means of a fan and a system of distributing ducts. (See Chapter 43.)

Chimney Effect: The tendency of air or gas in a duct or other vertical passage to rise when heated due to its lower density compared with that of the surrounding air or gas. In buildings, the tendency toward displacement (caused by the difference in temperature) of internal heated air by unheated outside air due to the difference in density of outside and inside air.

Comfort Air Conditioning: The process by which simultaneously the temperature, moisture content, movement and quality of the air in enclosed spaces intended for human occupancy may be maintained within required limits. (See *Air Conditioning*.)

Comfort Line: The effective temperature at which the largest percentage of adults feels comfortable.

Comfort Zone (*Average*): The range of effective temperatures over which the majority (50 per cent or more) of adults feel comfortable. (See Chapter 12.)

Condensate: The liquid formed by condensation of a vapor. In steam heating, water condensed from steam; in air conditioning, water extracted from air, as by condensation on the cooling coil of a refrigeration machine.

Condensation: The process of changing a vapor into liquid by the extraction of heat. Condensation of steam or water vapor is effected in either steam condensers or in dehumidifying coils and the resulting water is called *condensate*.

Conductance, Surface (*Unit*): The amount of heat transferred by radiation, conduction, and convection from unit area of a surface to the air or other fluid in contact with it, or vice versa, in unit time for a unit difference in temperature between the surface and the fluid. The common unit is: Btu per (hour) (square foot) (Fahrenheit degree). Symbol *f*. The temperature of the fluid should be taken in a plane sufficiently far from the surface that it will not be affected by the temperature of the surface.

Conductance, Thermal: The time rate of heat flow through unit area of a body, of given size and shape, per unit temperature difference. Common unit is: Btu per (hour) (square foot) (Fahrenheit degree). Symbol *C*.

Conduction, Thermal: The process of heat transfer through a material medium in which kinetic energy is transmitted by the particles of the material from particle to particle without gross displacement of the particles.

Conductivity, Thermal: The time rate of heat flow through unit area of a homogeneous substance under the influence of a unit temperature gradient. Common units are: Btu per (hour) (square foot) (Fahrenheit degree per inch). Symbol *k*.

Conductor, Thermal: A material which readily transmits heat by means of conduction.

Convection: The motion resulting in a fluid from the differences in density and the action of gravity. In heat transmission this meaning has been extended to include both *forced* and *natural* motion or circulation.

Convective Heat Transfer: The transmission of heat by either natural or forced motion of a fluid (liquid or gas).

Convector: An agency of convection. In heat transfer, a surface designed to transfer its heat to a surrounding fluid largely or wholly by convection. The heated fluid may be removed mechanically or by gravity (Gravity Convector). Such a surface may or may not be enclosed or concealed. When concealed and enclosed the resulting device is sometimes referred to as a concealed radiator. (See also definition of *Radiator*.) (See also Chapter 25.)

Decibel: A unit used to express the relation between two amounts of power. By definition the difference in decibels between two powers P_1 and P_2, P_2 being the larger, is: db difference $= 10 \log_{10} P_2/P_1$.

In acoustics the threshold of hearing at 1,000 cycles per second has been standardized at 10^{-16} watts per square centimeter. If P_2 is the power in watts per square centimeter of a measured sound, then $10 \log_{10} P_2/10^{-16}$ is the db difference above the threshold and is known as the *intensity level*. This is a definite recognized way of describing the intensity of a sound.

Degree-Day: A unit, based upon temperature difference and time, used in estimating fuel consumption and specifying nominal heating load of a building in winter. For any one day, when the mean temperature is less than 65 F, there exists as many degree-days as there are Fahrenheit degrees difference in temperature between the mean temperature for the day and 65 F.

Dehumidify: To reduce, by any process, the quantity of water vapor within a given space.

Dehydrate: To remove water in all forms from matter. Liquid water, hygroscopic water, and water of crystallization or water of hydration are included.

Density: The ratio of the mass of a specimen of a substance to the volume of the specimen. The mass of a unit volume of a substance. When weight can be used without confusion, as synonymous with mass, density is the weight per unit volume.

Dew-Point: See *Temperature, Dew-Point.*

Direct-Indirect Heating Unit: A heating unit located in the room or space to be heated and partially enclosed, the enclosed portion being used to heat air which enters from outside the room.

Direct-Return System (*Hot Water*): A hot water system in which the water, after it has passed through a heating unit, is returned to the boiler along a direct path so that the total distance traveled by the water is the shortest feasible, and so that there are considerable differences in the lengths of the several circuits composing the system.

Down-Feed One-Pipe Riser (*Steam*): A pipe which carries steam downward to the heating units and into which the condensate from the heating units drains.

Down-Feed System (*Steam*): A steam heating system in which the supply mains are above the level of the heating units which they serve.

Draft: A current of air. Usually refers to the pressure difference which causes a current of air or gases to flow through a flue, chimney, heater or space.

Draft Head (*Side Outlet Enclosure*): The height of a gravity convector between the bottom of the heating unit and the bottom of the air outlet opening. (*Top Outlet Enclosure*): The height of a gravity convector between the bottom of the heating unit and the top of the enclosure.

Drip: A pipe, or a steam trap and a pipe considered as a unit, which conducts condensation from the steam side of a piping system to the water or return side of the system.

Dry: To separate or remove a liquid or vapor from another substance. The liquid may be water but the term is also used for the removal of liquid or vapor forms of other substances.

Dust: An air suspension (aerosol) of solid particles of any material. (See also Chapter 10, p. 166.)

Enthalpy: A term used in lieu of *total heat* or *heat content*. Expressible in Btu per pound. Mathematically defined as $h = u + pv / J$. When a change occurs at constant pressure, as when water is boiled, the change in enthalpy is equal to the heat added, in this case latent heat.

Enthalpy, Free: A thermodynamic property which serves as a measure of the available energy of a system with respect to surroundings at the same temperature and same pressure as that of the system. No process involving an increase in available energy can occur spontaneously.

Enthalpy, Specific: A term sometimes applied to enthalpy per unit weight, the English unit being Btu per pound.

Entropy: The ratio of the heat added to a substance to the absolute temperature at which it is added. Mathematically, for a reversible process, $dS = dQ/T$ or $S = \int dQ/T$.

These formulas are applicable when temperature is not constant. During a reversible adiabatic change entropy is constant. During a reversible isothermal change the heat absorbed by the substance is equal to the product of the absolute temperature of the substance and its change of entropy.

Entropy, Specific: A term sometimes applied to entropy per unit weight, the English unit being Btu per (Fahrenheit degree, absolute) (pound).

Equivalent Evaporation: The amount of water a boiler would evaporate, in pounds per hour, if it received feed water at 212 F and vaporized it at the same temperature and corresponding atmospheric pressure.

Fan Furnace System: See *Warm Air Heating System.*

Fog: Suspended liquid droplets generated by condensation from the gaseous to the liquid state or by breaking up a liquid into a dispersed state, such as by splashing, foaming, and atomizing. (See also Chapter 10, p. 167.)

Force: The action on a body which tends to change its relative condition as to rest or motion.

Fumes: Smoke; aromatic smoke; odor emitted, as of flowers; a smoky or vaporous exhalation, usually odorous, as that from concentrated nitric acid. The word *fumes* is so broad and inclusive that its usefulness as a technical term is very limited. Its principal definitive characteristic is that it implies an odor. The terms vapor, smoke, fog, etc., which can be more strictly defined, should be used whenever possible.

Also defined as solid particles generated by condensation from the gaseous state, generally after volatilization from molten metals, etc., and often accompanied by a chemical reaction such as oxidation. Fumes flocculate and sometimes coalesce. (See also Chapter 10, p. 166.)

Furnace: That part of a boiler or warm air heating plant in which combustion takes place. Also a complete heating unit for transferring heat from fuel being burned to the air supplied to a heating system.

Furnace Volume (*Total*): The total furnace volume for horizontal-return tubular boilers and water-tube boilers is the cubical contents of the furnace between the grate and the first plane of entry into or between tubes. It therefore includes the volume behind the bridge wall as in ordinary horizontal-return tubular boiler settings, unless manifestly ineffective (*i.e.*, no gas flow taking place through it), as in the case of waste-heat boilers with auxiliary coal furnaces, where one part of the furnace is out of action when the other is being used. For Scotch or other internally fired boilers it is the cubical contents of the furnace, flues and combustion chamber, up to the plane of first entry into the tubes. (*A.S.M.E.* Power Test Codes, Series 1929.)

Grate Area: The area of the grate surface, measured in square feet, to be used in estimating the rate of burning fuel. This area is construed to mean the area measured in the plane of the top surface of the grate, except that with special furnaces, such as those having magazine feed, or special shapes, the grate area shall be the mean area of the active part of the fuel bed taken perpendicular to the path of the gases through it. For furnaces having a secondary grate, such as those in double-grate down draft boilers, the effective area shall be taken as the area of the upper grate plus one-eighth of the area of the lower grate, both areas being estimated as previously defined.

Gravity, Specific: The ratio of the mass of a unit volume of a substance to the mass of the same volume of a standard substance at a standard temperature. Water at 39.2 F is the standard substance usually referred to. For gases, dry air, at the same temperature and pressure as the gas, is often taken as the standard substance.

Gravity Warm Air Heating System: See *Warm Air Heating System.*

Head, Dynamic: Same as Total Pressure expressed in height of liquid.

Heat: The form of energy that is transferred by virtue of a temperature difference. constant pressure heat added is equal to enthalpy change.

Heat, Humid: Ratio of increase of enthalpy per pound of dry air to rise of temperature under conditions of constant pressure and constant humidity ratio.

Heat, Latent: A term used to express the energy involved in a change of state.

Heat, Sensible: A term used in heating and cooling to indicate any portion of heat which changes only the temperature of the substances involved.

Heat of the Liquid: The increase in enthalpy per unit weight of a saturated liquid s its temperature increases from a chosen base temperature. For water the base temperature is usually taken as 32 F.

Heat, Specific: The heat absorbed (or given up) by a unit mass of a substance when its temperature is increased (or decreased) by 1 deg. Common Units: Btu per (pound) (Fahrenheit degree), calories per (gram) (Centigrade degree). For gases, both specific heat at constant pressure (C_p) and specific heat at constant volume (C_v) are frequently used. In air-conditioning, C_p is usually used.

Heat, Total: See Enthalpy.

Heat Transmission, Coefficient: Any one of a number of coefficients used in the calculation of heat transmission by conduction, convection, and radiation, through various materials and structures. (See thermal conductance, thermal conductivity, thermal resistance, thermal resistivity, thermal transmittance, etc.).

Hot Water Heating System: A heating system in which water is used as the medium by which heat is carried from the boiler to the heating units.

Humidify: To increase, by any process, the density of water vapor within a given pace.

Humidistat: A regulatory device, actuated by changes in humidity, used for the utomatic control of relative humidity.

Humidity: Water vapor within a given space.

Humidity, Absolute: The weight of water vapor per unit volume, pounds per ubic foot or grams per cubic centimeter.

Humidity, Relative: The ratio of the actual partial pressure of the water vapor n a space to the saturation pressure of pure water at the same temperature. (See discussion in Chapter 3.)

Humidity Ratio: In a mixture of water vapor and air, the weight of water vapor er pound of dry air. Also called *Specific Humidity*.

Humidity, Specific: See Humidity Ratio.

Hygrostat: Same as Humidistat.

Inch of Water: A unit of pressure equal to the pressure exerted by a column of uid water 1 in. high at a standard temperature. The standard temperature is sometmes taken as 0 C and sometimes as 62 F. One inch of water at 62 F = 5.197 lb per uare foot.

Insulation (*Thermal*): A material having a relatively high resistance to heat flow, d used principally to retard the flow of heat.

Isobaric: An adjective used to indicate a change taking place at constant pressure.

Isothermal: An adjective used to indicate a change taking place at constant mperature.

Load, Estimated Design: In a heating or cooling system, the sum of the useful t transfer plus heat transfer from or to the connected piping plus heat transfer urring in any auxiliary apparatus connected to the system. The units are Btu per r or, in heating, equivalent direct radiation (EDR) which is becoming obsolete.

oad, Estimated Maximum: In a heating or cooling system, the calculated maxin heat transfer that the system will be called upon to provide.

anometer: An instrument for measuring pressures; essentially a U-tube partially with a liquid, usually water, mercury, or a light oil, so constructed that the amount splacement of the liquid indicates the pressure being exerted on the instrument.

ss: A measure of the inertia of a body. It also measures the quantity of matter ody. Since the only general property of a given portion of matter that cannot be ed is its inertia, it is this property by which quantities of matter are defined. Two s which have equal inertias are said to have equal masses. Within equal tities of matter. (This definition fails at velocities approaching the velocity of

light.) The mass of a body is numerically equal to the ratio of the force required to give the body a given acceleration to the acceleration. $m = F/a$. The common units of mass are the gram and the pound.

Mechanical Equivalent of Heat: The quantity of mechanical energy equal to one unit of heat. $J = 778.3$ ft-lb per Btu $= 4.187 \times 10^7$ ergs per gram-calorie.

Medium, Heating: A substance such as water, steam, air or furnace gas used to convey heat from the boiler, furnace or other souce of heat or energy to the heating unit from which the heat is dissipated.

Micron: A unit of length, the thousandth part of 1 mm or the millionth of a meter.

Millimeter of Mercury: A unit of pressure equal to the pressure exerted by a column of mercury 1 mm high at a temperature of 0 C. One millimeter of mercury at 0 C $= 1.934 \times 10^{-2}$ lb per square inch.

Mol: A weight of a substance numerically equal to its molecular weight. If the weight is in pounds the unit is a *Pound Mol*, in grams the unit is a *Gram Mol*. For perfect gases the volume of 1 mol is constant for all gases at the same temperature and pressure. For real gases this is approximately true at moderate pressures. At 32 F and zero-pressure the value of the product, pressure times specific volume, is 359.045 ± 0.006 atmosphere cubic feet (atm ft^3), *for 1 mol of any gas*. For dry air at 32 F and standard atmospheric pressure, the specific volume is 358.83 cu ft per mol (ft^3 per mol).

One-Pipe Supply Riser—(*Steam*): A pipe which carries steam vertically to a heating unit and which also carries the condensate from the heating unit. In an upfeed system steam and condensate flow in opposite directions; in an overhead or down-feed system they flow in the same direction.

One-Pipe System—(*Steam*): A steam heating system in which a single main serves the dual purpose of supplying steam to the heating unit and conveying condensate from it. Ordinarily to each heating unit there is but one connection which must serve as both the supply and the return, although separate supply and return connections may be used. (Hot Water)—A hot water system in which the cooled water from the heating units is returned to the supply main. Consequently, the heating units farthest from the boiler are supplied with cooler water than those near the boiler in the same circuit.

Overhead System: Any steam or hot water system in which the supply main is above the heating unit. In a steam system the return must be below the heating units; in a water system the return may be above or below the heating units.

Panel Heating: A heating system in which heat is transmitted by both radiation and convection from panel surfaces to both air and surrounding surfaces.

Panel Radiator: A heating unit placed on or flush with a flat wall surface and intended to function essentially as a radiator.

Plenum Chamber: An air compartment maintained under pressure and connected to one or more distributing ducts.

Potentiometer: An instrument for comparing small electromotive forces or for measuring small electromotive forces by comparison with a known electromotive force. Its principal advantage is that during the measurement no current flows through the source of electromotive force.

Power: The rate of performing work. Common units are horsepower, Btu per hour, and watts.

Pressure: Force per unit area. Common units are pounds per square inch, gram per square centimeter, inch of water, millimeter of mercury.

Pressure, Absolute: The sum of the gage pressure and the barometric pressure.

Pressure, Gage: Pressure measured from atmospheric pressure as a base. Gage pressure may be indicated by a manometer which has one leg connected to the pressure source and the other exposed to atmospheric pressure.

Pressure, Dynamic: Same as Total Pressure.

Pressure, Saturation: The saturation pressure for a pure substance for any given temperature is that pressure at which vapor and liquid or vapor and solid can co-exist in stable equilibrium.

Pressure, Static: The normal force per unit area that would be exerted by a moving fluid on a small body immersed in it if the body were carried along with the fluid. Practically, it is the normal force per unit area at a small hole in a wall of the duct through which the fluid flows (piezometer) or on the surface of a stationary tube at a point where the disturbances created by inserting the tube cancel. It is supposed that the thermodynamic properties of a moving fluid depend on static pressure in exactly the same manner as those of the same fluid at rest depend upon its uniform hydrostatic pressure.

Pressure, Total: [illegible] theory of the flow of fluids; the sum of the static pressure and the velocity pressure at the point

Pressure, Vapor: The pressure exerted by a vapor. If a vapor is kept in confinement over its liquid so that the vapor can accumulate above the liquid, the temperature being held constant, the vapor pressure approaches a fixed limit called the maximum, or saturated, vapor pressure, dependent only on the temperature and the liquid. The term *vapor pressure* is sometimes used as synonymous with *saturated vapor pressure.*

Pressure, Velocity: In a moving fluid, the pressure capable of causing an equivalent velocity if applied to move the same fluid through an orifice such that all pressure energy expended is converted into kinetic energy.

Psychrometer: An instrument for ascertaining the humidity or hygrometric state of the atmosphere.

Psychrometric: Pertaining to psychrometry or the state of the atmosphere with reference to moisture.

Psychrometry: The branch of physics relating to the measurement or determination of atmospheric conditions, particularly regarding the moisture mixed with the air.

Pyrometer: An instrument for measuring high temperatures.

Radiant Heating: A heating system in which only the heat radiated from panels is effective in providing the heating requirements. The term *Radiant Heating* is frequently used to include both *Panel and Radiant Heating.*

Radiation: The transmission of energy by means of electromagnetic waves.

Radiation, Thermal (Heat) Radiation: The transmission of energy by means of electromagnetic waves of very long wave length. Radiant energy of any wave length may, when absorbed, become thermal energy and result in an increase in the temperature of the absorbing body.

Radiation, Equivalent Direct (EDR): A unit of heat delivery of 240 Btu (*Steam*) or 150 Btu (*Water*) per hour. It does not imply 144 sq in. of surface.

Radiator: A heating unit exposed to view within the room or space to be heated. A radiator transfers heat by radiation to objects within visible range and by conduction to the surrounding air which in turn is circulated by natural convection; a so-called radiator is also a convector but the term radiator has been established by long usage.

Radiator, Concealed: A heating device located within, adjacent to, or exterior to the room being heated but so covered or enclosed or concealed that the heat transfer surface of the device, which may be either a radiator or a convector, is not visible from the room. Such a device transfers its heat to the room largely by convection air currents.

Radiator, Direct: Same as Radiator.

Radiator, Recessed: A heating unit set back into a wall recess but not enclosed.

Radiator, Tube or Tubular: A heating unit used as a radiator in which the heat transfer surfaces are principally tubes.

Refrigerant: A substance which produces a refrigerating effect by its absorption of heat while expanding or vaporizing.

Refrigeration, Ton of: The removal of heat at a rate of 200 Btu per minute, 12,000 Btu per hour, or 288,000 Btu per 24 hours.

Resistance, Thermal: The reciprocal of thermal conductance. Symbol *R.*

Resistivity, Thermal: The reciprocal of thermal conductivity. Symbol *r.*

Return, Dry: A return pipe in a steam heating system which carries both water of condensation and air. The dry return is above the level of the water line in the boiler in a gravity system. (See *Return, Wet.*)

Return, Wet: That part of a return main of a steam heating system which is filled with water of condensation. The wet return usually is below the level of the water line in the boiler, although not necessarily so. (See *Return, Dry.*)

Return Mains: Pipes or conduits which return the heating or cooling medium from the heat transfer unit to the source of heat or refrigeration.

Reversed-Return System: A system in which the heating or cooling medium from several heat transfer units is returned along paths arranged so that all circuits composing the system or composing a major sub-division of it are of practically equal length.

Saturation: The condition for co-existence in stable equilibrium of a vapor and liquid or a vapor and solid phase of the same substance. Example: Steam over the water from which it is being generated.

Saturation, Degree of, or Per Cent: The ratio of the weight of a given volume of water vapor to the weight of an equal volume of saturated water vapor at the same temperature.

Smoke: An air suspension (aerosol) of particles, usually but not necessarily solid, often originating in a solid nucleus, formed from combustion or sublimation. Also

defined as carbon or soot particles less than 0.1 micron in size which result from the incomplete combustion of carbonaceous materials such as coal, oil, tar, and tobacco.

Smokeless Arch: An inverted baffle placed in an up-draft furnace toward the rear to aid in mixing the gases of combustion and thereby to reduce the smoke produced.

Solar Constant: The solar intensity incident on a normal surface located outside the earth's atmosphere at a distance from the sun equal to the mean distance between the earth and the sun. Its value is 415, 445, or 430 Btu per (hour) (square foot) as the July, January, or mean value respectively. At sea level in July the solar intensity value is about 300 Btu per (square foot) (hour) since about 28 per cent is absorbed in the earth's atmosphere.

Sorbent: A material which extracts one or more substances present in an atmosphere or mixture of gases or liquids with which it is in contact, due to an affinity for such substances.

Sorption: Adsorption or absorption.

Split System: A system in which the heating is accomplished by means of radiators or convectors supplemented by mechanical circulation of air (heated or unheated) from a central point. Ventilation may be provided by the same system.

Square Foot of Heating Surface (*Equivalent*): This term is synonymous with Equivalent Direct Radiation (EDR).

Stack Height: The height of a gravity convector between the bottom of the heating unit and the top of the outlet opening.

Steam: Water in the vapor phase. *Dry Saturated Steam* is steam at the saturation temperature corresponding to the pressure, and containing no water in suspension. *Wet Saturated Steam* is steam at the saturation temperature corresponding to the pressure, and containing water particles in suspension. *Superheated Steam* is steam at a temperature higher than the saturation temperature corresponding to the pressure.

Steam Heating System: A heating system in which heat is transferred from the boiler or other source of heat to the heating units by means of steam at, above, or below atmospheric pressure.

Steam Trap: A device for allowing the passage of condensate, or of air and condensate and preventing the passage of steam.

Supply Mains: The pipes through which the heating medium flows from the boiler or source of supply to the run-outs and risers leading to the heating units.

Surface, Heating: The exterior surface of a heating unit. *Extended heating surface (or extended surface)*: Heating surface consisting of fins, pins or ribs which receive heat by conduction from the prime surface. *Prime Surface*: Heating surface having the heating medium on one side and air (or extended surface) on the other. (See also Boiler Heating Surface.)

Temperature: The thermal state of matter with reference to its tendency to communicate heat to matter in contact with it. If no heat flows upon contact, there is no difference in temperature.

Temperature, Absolute: Temperature expressed in degrees above absolute zero.

Temperature, Dry-Bulb: The temperature of a gas or mixture of gases indicated by an accurate thermometer after correction for radiation.

Temperature, Dew-Point: The temperature at which the condensation of water vapor in a space begins for a given state of humidity and pressure as the temperature of the vapor is reduced. The temperature corresponding to saturation (100 per cent relative humidity) for a given absolute humidity at constant pressure.

Temperature, Effective: An arbitrary index which combines into a single value the effect of temperature, humidity, and air movement on the sensation of warmth or cold felt by the human body. The numerical value is that of the temperature of still, saturated air which would induce an identical sensation.

Temperature, Wet-Bulb: Thermodynamic wet-bulb temperature is the temperature at which liquid or solid water, by evaporating into air, can bring the air to saturation adiabatically at the same temperature. Wet-bulb temperature (without qualification) is the temperature indicated by a wet-bulb psychrometer constructed and used according to specifications. (*A.S.M.E.* Power Test Codes, Series 1932, Instruments and Apparatus, Part 18.)

Thermodynamics, Laws of: Two laws upon which rest the classical theory of thermodynamics. These laws have been stated in many different, but equivalent ways. *The First Law*: (1) When work is expended in generating heat, the quantity of heat produced is proportional to the work expended; and conversely, when heat is employed in the performance of work, the quantity of heat which disappears is proportional to

the work done. (Joule)[a] (G.P.)[b]; (2) If a system is caused to change from an initial state to a final state by adiabatic means only, the work done is the same for all adiabatic paths connecting the two states. (Zemansky); (3) In any power cycle or refrigeration cycle the net heat absorbed by the working substance is exactly equal to the net work done. *The Second Law*: (1) It is impossible for a self acting machine, unaided by any external agency, to convey heat from a body of lower to one of higher temperature. (Clausius) (G.P.); (2) It is impossible to derive mechanical work from heat taken from a body unless there is available a body of lower temperature into which the residue not so used may be discharged (Kelvin) (G.P.); (3) It is impossible to construct an engine that, operating in a cycle, will produce no effect other than the extraction of heat from a reservoir and the performance of an equivalent amount of work (Zemansky).

Thermostat: An instrument which responds to changes in temperature and which directly or indirectly controls temperature.

Transmittance, Thermal: The time rate of heat flow, from the fluid on the warm side to the fluid on the cold side, per (square foot) (degree temperature difference between the two fluids). Sometimes called *Over-all Coefficient of Heat Transfer.*

Common unit is Btu per (hour) (square foot) (Fahrenheit degree). Symbol *U.*

Two-Pipe System (*Steam or Water*): A heating system in which one pipe is used for the supply of the heating medium to the heating unit and another for the return of the heating medium to the source of heat supply. The essential feature of a two-pipe system is that each heating unit receives a direct supply of the heating medium which medium cannot have served a preceding heating unit.

Up-Feed System: A heating system in which the supply mains are below the level of the heating units which they serve.

Vacuum Heating System: A two-pipe steam heating system equipped with the necessary accessory apparatus which will permit operating the system below atmospheric pressure when desired

Vane Ratio: In air distributing devices the ratio of depth of vane to shortest opening width between two adjacent grille bars.

Vapor: The gaseous form of substances which are normally in the solid or liquid state and which can be changed to these states either by increasing the pressure or decreasing the temperature. Vapors diffuse. (*A.S.A.* definition.)

Vapor Heating System: A steam heating system which operates under pressures at or near atmospheric and which returns the condensate to the boiler or receiver by gravity. Vapor systems have thermostatic traps or other means of resistance on the return ends of the heating units for preventing steam from entering the return mains; they also have a pressure-equalizing and air-eliminating device at the end of the dry return.

Velocity: A vector quantity which denotes at once the time rate and the direction of a linear motion. $V = \frac{ds}{dt}$. For uniform linear motion $V = \frac{s}{t}$. Common units are: feet per second.

Ventilation: The process of supplying or removing air, by natural or mechanical means, to or from any space. Such air may or may not have been conditioned. (See Air Conditioning.)

Volume, Specific: The volume of a substance per unit mass; the reciprocal of density. Units: cubic feet per pound, cubic centimeters per gram, etc.

Warm Air Heating System: A warm air heating plant consists of a heating unit (fuel-burning furnace) enclosed in a casing, from which the heated air is distributed to the various rooms of the building through ducts.

Warm Air Heating System, Gravity: A warm air heating system in which the motive head producing flow depends on the difference in weight between the heated air leaving the casing and the cooler air entering the bottom of the casing.

Warm Air Heating System, Mechanical: A warm air heating system in which circulation of air is effected by a fan. Such a system may include air cleaning devices.

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[a]Names of authors who first stated law are given in parentheses.

[b]From Glossary of Physics, by LeRoy Dougherty Weld, (McGraw-Hill, 1937).

Chapter 2

ABBREVIATIONS AND SYMBOLS

Standard Abbreviations; Standard Symbols; Greek Alphabet; Conversion Equations; Graphical Symbols for Piping, Ductwork, Heating and Ventilating, Refrigerating; Identification of Piping by Color; Specific Heat Table

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THIS chapter contains information regarding abbreviations, symbols, and conversion equations, which are of particular interest to the engineer engaged in heating, ventilating, and air conditioning.

ABBREVIATIONS

Abbreviations are shortened forms of names and expressions employed in texts and tabulations and should not generally be used as symbols in equations. Most of the following abbreviations have been compiled from a list of approved standards [1]. In general the period has been omitted in all abbreviations except where the omission results in the formation of an English word. Additional abbreviations applying to individual chapters will be found at the end of Chapters 3, 4, 5, 7, 15, 16, 39, and 41.

Absolute	abs
Air horsepower	air hp
Alternating-current (as adjective)	a-c
Ampere	amp
Ampere-hour	amp-hr
Atmosphere	atm
Average	avg
Avoirdupois	avdp
Barometer	bar.
Boiling point	bp
Brake horsepower	bhp
Brake horsepower-hour	bhp-hr
British thermal unit	Btu
British thermal units per hour	Btuh
Calorie	cal
Centigram	cg
Centimeter	cm
Centimeter-gram-second (system)	cgs
Cubic	cu
Cubic centimeter	cu cm or cc
Cubic foot	cu ft
Cubic feet per minute	cfm
Cubic feet per second	cfs
Decibel	db
Degree[2]	deg or °
Degree, Centigrade	C
Degree, Fahrenheit	F
Degree, Kelvin	K
Degree, Réaumur	R
Diameter	diam

[1] Abbreviations for Scientific and Engineering Terms, Z10.1-1941 (*American Standards Association*).

[2] It is recommended that the abbreviation for the temperature scale, F, C, K, R, be included in expressions for numerical temperatures but, wherever feasible, the abbreviation for *degree* be omitted; as 68 F.

Direct-current (as adjective)	d-c
Electromotive Force	emf
Feet per minute	fpm
Feet per second	fps
Foot	ft
Foot-pound	ft-lb
Foot-pound-second (system)	fps
Freezing point	fp
Gallon	gal
Gallons per minute	gpm
Gallons per second	gps
Gram	g
Gram-calorie	g-cal
Horsepower	hp
Horsepower-hour	hp-hr
Hour	hr
Inch	in.
Inch-pound	in.-lb
Indicated horsepower	ihp
Indicated horsepower-hour	ihp-hr
Kilogram	kg
Kilowatt	kw
Kilowatthour	kwhr
Mass	mass
Melting point	mp
Meter	m
Micron	μ (mu)
Miles per hour	mph
Millimeter	mm
Minute	min
Molecular weight	mol. wt
Mol	mol
Ounce	oz
Pound	lb
Pounds per square inch	psi
Pounds per square inch, gage	psig
Pounds per square inch, absolute	psia
Revolutions per minute	rpm
Revolutions per second	rps
Second	sec
Specific gravity	sp gr
Specific heat	sp ht
Square foot	sq ft
Square inch	sq in.
Watt	w
Watthour	whr

SYMBOLS

A letter symbol is a single character, with subscript or superscript if required, used to designate a physical magnitude in mathematical equations and expressions. Two or more symbols together always represent a product. The following have been compiled from a selected list of approved standards [3]. Additional symbols and variations in the standard

[3] Letter Symbols for Mechanics of Solid Bodies, Z10.3-1942, and Letter Symbols for Heat and Thermodynamics, Z10.4-1943 (*American Standards Association*).

symbols found necessary in the individual chapters will be found in a list at the end of Chapters 3, 4, 5, 7, 15, 16, 39, and 41.

Acceleration, due to gravity ..... g
Acceleration, linear ..... a
Area ..... A
Change in specific volume during vaporization ..... v_{fg}
Density, Weight per unit volume, Specific weight ..... d or ρ (rho)

$$d = \frac{1}{v}$$

Distance, linear ..... s
Dry saturated vapor, Dry saturated gas at saturation pressure and temperature, vapor in contact with liquid ..... *Subscript* g

Efficiency ..... η
Elevation above some datum ..... z, Z
Emissivity ..... ϵ
Energy in general; work, total; work, molal ..... E
Entropy. (The capital should be used for any weight, and the small letter for unit weight) ..... S or s

Force, total load ..... F
Gas Constant, in equation $pV = nRT$ ..... R
Head ..... H or h
Heat content, Total heat, Enthalpy. (The capital should be used for any weight and the small letter for unit weight) ..... H or h
Heat content of saturated liquid, Total heat of saturated liquid, Enthalpy of saturated liquid, sometimes called heat of the liquid ..... h_f

Heat content of dry saturated vapor, Total heat of dry saturated vapor, Enthalpy of dry saturated vapor ..... h_g
Heat of vaporization at constant pressure ..... L or h_{fg}
Hydraulic radius ..... R_H
Internal energy, Intrinsic energy. (The capital should be used for any weight and the small letter for unit weight) ..... U or u
Length of path of heat flow, thickness L

Load, total ..... W
Mechanical efficiency ..... e_m
Mechanical equivalent of heat ..... J
Power, Horsepower, Work per unit time ..... P
Pressure, Absolute pressure, Gage pressure, Force per unit area ..... p

Quantity (total) of fluid, water, gas, heat; Quantity by volume; Total quantity of heat transferred ..... Q
Quality of steam, Pounds of dry steam per pound of mixture x
Reynolds Number ..... N_{Re}
Saturated liquid at saturation pressure and temperature, Liquid in contact with vapor ..... *Subscript* f
Specific heat c

Specific heat at constant pressure ..... c_p
Specific heat at constant volume ..... c_v
Specific volume, Volume per unit weight, Volume per unit mass v
Temperature (ordinary) F or C. (*Theta* is used preferably only when t is used for Time in the same discussion) ..... t or θ (*theta*)
Temperature (absolute) F abs or K. (Capital *theta* is used preferably only when small *theta* is used for ordinary temperature) ..... T or Θ (*capital theta*)

Thermal conductance[4]: heat transferred per (unit time) (degree)..... C

$$C = \frac{1}{R} = \frac{kA}{L} = \frac{q}{t_1 - t_2}$$

Thermal conductance per unit area, Unit conductance: heat transferred per (unit time) (unit area) (degree)..... C_a

$$C_a = \frac{C}{A} = \frac{1}{RA} = \frac{q}{A(t_1 - t_2)} = \frac{k}{L}$$

Thermal conductivity: heat transferred per (unit time) (unit area) (degree per unit length)..... k

$$k = \frac{\frac{q}{A}}{\frac{(t_1 - t_2)}{L}}$$

Surface coefficient of heat transfer, Film coefficient of heat transfer, Individual coefficient of heat transfer: heat transferred per (unit time) (unit area) (degree)..... f

$$= \frac{\frac{q}{A}}{t_1 - t_2}$$

(In general f is not equal to k/L, where L is the actual thickness of the fluid film.)

Over-all coefficient of heat transfer, Thermal transmittance per unit area: heat transferred per (unit time) (unit area) (degree over-all)..... U

$$U = \frac{\frac{q}{A}}{t_1 - t_2}$$

Thermal transmission (heat transferred per unit time)..... q

$$q = \frac{Q}{t}$$

Thermal resistance (degree per unit of heat transferred per unit time)..... R

$$R = \frac{t_1 - t_2}{q} = \frac{L}{kA}$$

Thermal resistivity..... $1/k$

Vaporization values at constant pressure, Differences between values for saturated vapor and saturated liquid at the same pressure..... *Subscript* $_{fg}$

Velocity..... V

Viscosity, absolute..... μ

Viscosity, kinematic..... μ/ρ

Volume (total)..... V

Volume per unit time, Rate at which quantity of material passes through a machine, Quantity of heat per unit time, Quantity of heat per unit weight..... q

Weight of a major item, Total weight..... W

Weight rate, Weight per unit of power, Weight per unit of time..... w

Work (total)..... W

---

[4]Terms ending *ivity* designate properties independent of size or shape, sometimes called *specific properties*. Examples: conductivity, resistivity. Terms ending *ance* designate quantities depending not only on the material, but also upon size and shape, sometimes called *total quantities*. Examples: conductance, transmittance. Terms ending *ion* designate rate of heat transfer. Examples: conduction, transmission.

THE GREEK ALPHABET

A α Alpha	I ι Iota	P ρ Rho
B β Beta	K κ Kappa	Σ σ s Sigma
Γ γ Gamma	Λ λ Lambda	T τ Tau
Δ δ Delta	M μ Mu	Υ υ Upsilon
E ε Epsilon	N ν Nu	Φ φ Phi
Z ζ Zeta	Ξ ξ Xi	X χ Chi
H η Eta	O o Omicron	Ψ ψ Psi
Θ ϑ θ Theta	Π π Pi	Ω ω Omega

CONVERSION EQUATIONS[5]

Heat, Power and Work

1 ton refrigeration	= 12,000 Btu per hour = 200 Btu per minute
Latent heat of ice	= 143.4 Btu per pound
1 Btu	= 778.3 ft-lb = 0.2930 Int. whr = 252.0 I.T. calorie
1 Int. watthour	= 2656 ft-lb = 3.413 Btu = 3600 Int. joules = 860 I.T. calories
1 Int. kilowatthour	= 3,413 Btu = 3.517 lb water evaporated from and at 212 F
1 Int. kilowatt (1000 watts)	= 1.341 hp = 56.88 Btu per minute = 44,267 ft-lb per minute
1000 I.T. calories 1 I.T. Kilocalorie	= 3.968 Btu = 3088 ft-lb = 1.1628 Int. whr
1 horsepower	= 0.7455 Int. kw = 42.40 Btu per minute = 33,000 ft-lb per minute = 550 ft-lb per second
1 boiler horsepower	= 33,475 Btu per hour = 9.809 Int. kw

Weight and Volume

1 gal (U. S.)	= 231 cu in. = 0.1337 cu ft
1 British or Imperial gallon	= 277.42 cu in.
1 cu ft	= 7.481 gal = 1728 cu in.
1 cu ft water at 60 F (in vacuo)	= 62.37 lb
1 cu ft water at 212 F (" ")	= 59.83 lb
1 gal water at 60 F (" ")	= 8.338 lb
1 gal water at 212 F (" ")	= 7.998 lb
1 lb (avdp)	= 16 oz = 7000 grains
1 bushel	= 1.244 cu ft
1 short ton	= 2000 lb

[5]Checked in 1944 by *National Bureau of Standards*. Abbreviations *Int.* and *I.T.* refer to *International* and *International (Steam) Table* respectively.

Pressure

1 lb per square inch	= 144 lb per square foot = 2.0360 in. mercury at 32 F = 2.0422 in. mercury at 62 F = 2.309 ft water at 62 F = 27.71 in. water at 62 F
1 oz per square inch	= 0.1276 in. mercury at 62 F = 1.732 in. water at 62 F
1 atmosphere	= 14.696 lb per square inch = 2116 lb per square foot = 33.94 ft water at 62 F = 30.01 in. mercury at 62 F = 29.921 in. mercury at 32 F
1 in. water at 62 F (in vacuo)	= 0.03609 lb per square inch = 0.5774 oz per square inch = 5.197 lb per square foot
1 ft water at 62 F (in vacuo)	= 0.4330 lb per square inch = 62.37 lb per square foot
1 in. mercury at 62 F (in vacuo)	= 0.4897 lb per square inch = 7.835 oz per square inch = 1.131 ft water at 62 F = 13.57 in. water at 62 F
1 in. mercury at 32 F (in vacuo)	= 0.49115 lb per square inch

Metric Units

1 cm	= 0.3937 in. = 0.0328 ft
1 in.	= 2.540 cm
1 m	= 3.281 ft
1 ft	= 0.3048 m
1 sq cm	= 0.1550 sq in.
1 sq in.	= 6.452 sq cm
1 sq m	= 10.76 sq ft
1 sq ft	= 0.09290 sq m
1 cu cm	= 0.06102 cu in.
1 cu in.	= 16.39 cu cm
1 cu m	= 35.31 cu ft
1 cu ft	= 0.02832 cu m
1 liter	= 1000 cu cm = 0.2642 gal
1 kg	= 2.205 lb (avdp)
1 lb	= 0.4536 kg
1 metric ton	= 2205 lb (avdp)
1 gram	= 0.002205 lb (avdp)
1 kilometer per hour	= 0.6214 mph
1 gram per square centimeter	= 0.02905 in. mercury at 62 F = 0.3942 in. water at 62 F
1 kg per sq cm (metric atmosphere)	= 14.22 lb per square inch
1 gram per cubic centimeter	= 0.03613 lb per cubic inch = 62.43 lb per cubic foot
1 dyne	= 0.00007233 poundals
1 absolute joule	= 10,000,000 ergs = 0.7376 ft-lb
1 Int. joule	= 0.7378 ft-lb
1 metric horsepower	= 75 kg-m per second = 0.986 hp (U. S.)
1 I. T. kilocalorie per kilogram	= 1.8 Btu per pound
1 I.T. calorie per square centimeter	= 3.687 Btu per square foot
1 I.T. calorie per (second) (square centimeter) for a temperature gradient of 1 C deg per centimeter	= 2903 Btu per (hour) (square foot) for a temperature gradient of 1 F deg per inch of thickness.

GRAPHICAL SYMBOLS FOR DRAWINGS[6]

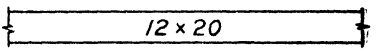
GRAPHICAL SYMBOLS FOR DRAWINGS	*Piping*
HEATING	
1. High Pressure Steam	
2. Medium Pressure Steam	
3. Low Pressure Steam	
4. High Pressure Return	
5. Medium Pressure Return	
6. Low Pressure Return	
7. Boiler Blow Off	
8. Condensate or Vacuum Pump Discharge	
9. Feedwater Pump Discharge	
10. Make Up Water	
11. Air Relief Line	
12. Fuel Oil Flow	FOF
13. Fuel Oil Return	FOR
14. Fuel Oil Tank Vent	FOV
15. Compressed Air	A
16. Hot Water Heating Supply	
17. Hot Water Heating Return	
AIR CONDITIONING	
18. Refrigerant Discharge	RD
19. Refrigerant Suction	RS
20. Condenser Water Flow	C
21. Condenser Water Return	CR
22. Circulating Chilled or Hot Water Flow	CH
23. Circulating Chilled or Hot Water Return	CHR
24. Make Up Water	
25. Humidification Line	H
26. Drain	D
27. Brine Supply	B
28. Brine Return	BR
PLUMBING	
29. Soil, Waste or Leader (Above Grade)	
30. Soil, Waste or Leader (Below Grade)	
31. Vent	
32. Cold Water	
33. Hot Water	
34. Hot Water Return	
35. Fire Line	F F
36. Gas	G G
37. Acid Waste	ACID
38. Drinking Water Flow	
39. Drinking Water Return	
40. Vacuum Cleaning	V V
41. Compressed Air	A
SPRINKLERS	
42. Main Supplies	S
43. Branch and Head	
44. Drain	S S

[6]Graphical Symbols for Use on Drawings in Mechanical Engineering, Z32.2-1941 (*American Standards Association*).

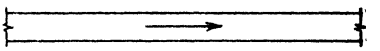
GRAPHICAL SYMBOLS FOR DRAWINGS

Ductwork

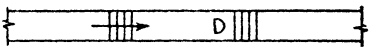
45. Duct (1st Figure, Width; 2nd, Depth)



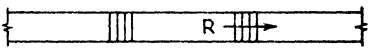
46. Direction of Flow



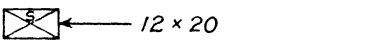
47. Inclined Drop in Respect to Air Flow



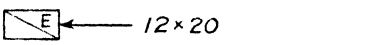
48. Inclined Rise in Respect to Air Flow



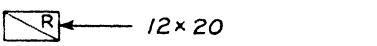
49. Supply Duct Section



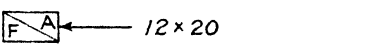
50. Exhaust Duct Section



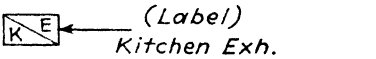
51. Recirculation Duct Section



52. Fresh Air Duct Section



53. Other Duct Sections



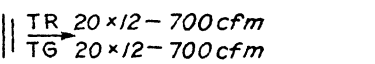
54. Register

55. Grille

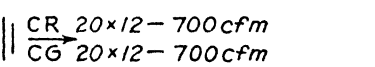
56. Supply Outlet

57. Exhaust Inlet

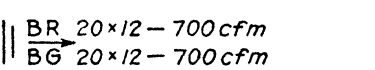
58. Top Register or Grille



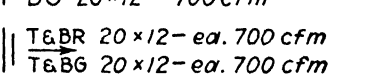
59. Center Register or Grille



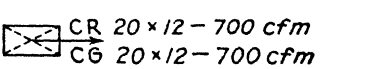
60. Bottom Register or Grille



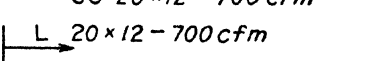
61. Top and Bottom Register or Grille



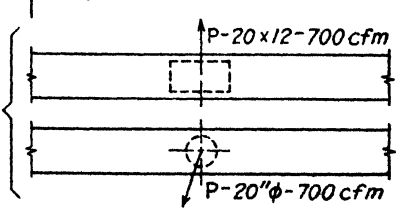
62. Ceiling Register or Grille



63. Louver Opening

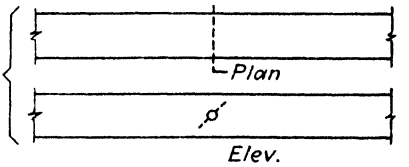


64. Adjustable Plaque

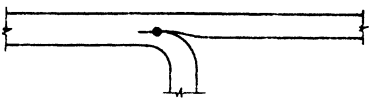


GRAPHICAL SYMBOLS FOR DRAWINGS *Ductwork*

65. Volume Damper



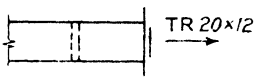
66. Deflecting Damper



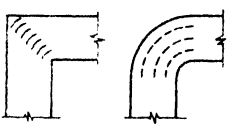
67. Deflecting Damper, Up

68. Deflecting Damper, Down

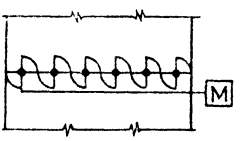
69. Adjustable Blank Off



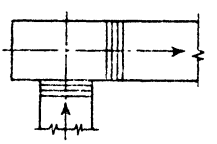
70. Turning Vanes



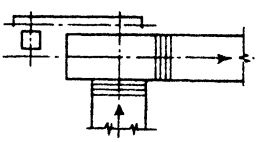
71. Automatic Dampers



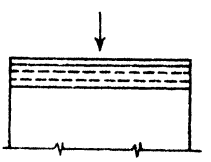
72. Canvas Connections



73. Fan and Motor With Guard

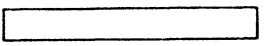


74. Intake Louvers and Screen

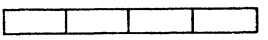


GRAPHICAL SYMBOLS FOR DRAWINGS — *Heating and Ventilating*

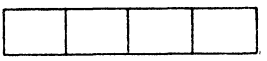
75. Heat Transfer Surface, Plan



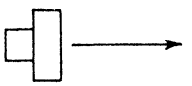
76. Wall Radiator, Plan



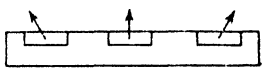
77. Wall Radiator on Ceiling, Plan



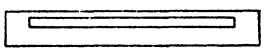
78. Unit Heater (Propeller), Plan



79. Unit Heater (Centrifugal Fan), Plan

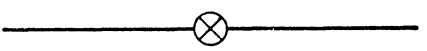


80. Unit Ventilator, Plan

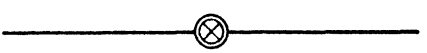


TRAPS

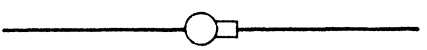
81. Thermostatic



82. Blast Thermostatic

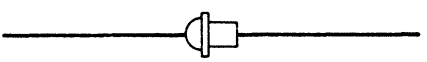


83. Float and Thermostatic



84. Float

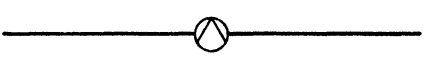
85. Boiler Return



VALVES

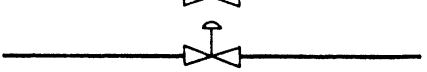
86. Reducing Pressure

87. Air Line

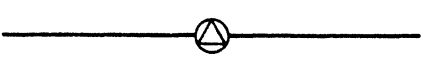


88. Lock and Shield

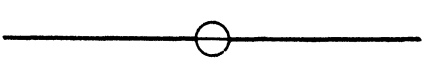
89. Diaphragm



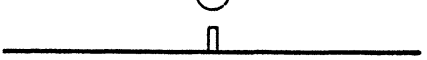
90. Air Eliminator



91. Strainer



92. Thermometer



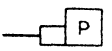
93. Thermostat

GRAPHICAL SYMBOLS FOR DRAWINGS

Refrigerating

94. Thermostat (Self Contained)

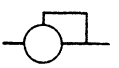
95. Thermostat (Remote Bulb)

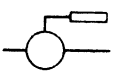
96. Pressurestat 

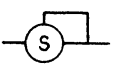
97. Hand Expansion Valve

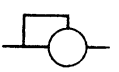
98. Automatic Expansion Valve

99. Thermostatic Expansion Valve

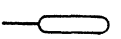
100. Evaporator Press. Regulating Valve, Throttling Type 

101. Evaporator Press. Regulating Valve, Thermostatic Throttling Type 

102. Evaporator Press. Regulating Valve, Snap-Action Valve 

103. Compressor Suction Pressure Limiting Valve, Throttling Type 

104. Hand Shut Off Valve

105. Thermal Bulb 

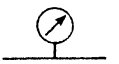
106. Scale Trap

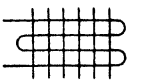
107. Dryer

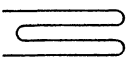
108. Strainer

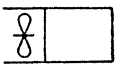
109. High Side Float

110. Low Side Float

111. Gage 

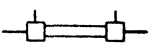
112. Finned Type Cooling Unit, Natural Convection 

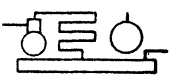
113. Pipe Coil 

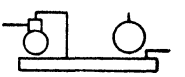
114. Forced Convection Cooling Unit 

115. Immersion Cooling Unit

116. Ice Making Unit

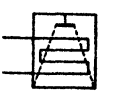
117. Heat Interchanger 

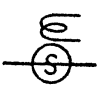
118. Condensing Unit, Air Cooled 

119. Condensing Unit, Water Cooled 

120. Compressor

121. Cooling Tower

122. Evaporative Condenser 

123. Solenoid Valve 

124. Pressurestat With High Pressure Cut-Out

IDENTIFICATION OF PIPING SYSTEMS BY COLOR

The color scheme for identification of piping systems listed in the following table and shown in Fig. 1 is reprinted from Part V, Fourth Edition, of the Engineering Standards of the *Heating, Piping and Air Conditioning Contractors National Association*[7].

All piping systems are classified according to the material carried in the pipes and colors are assigned as follows:

Class	Color
F—Fire-protection	Red
D—Dangerous materials	Yellow or Orange
S—Safe Materials	Green (or the achromatic colors, white, black, gray or aluminum)
and, when required	
P—Protective materials	Bright blue
V—Extra valuable materials	Deep purple

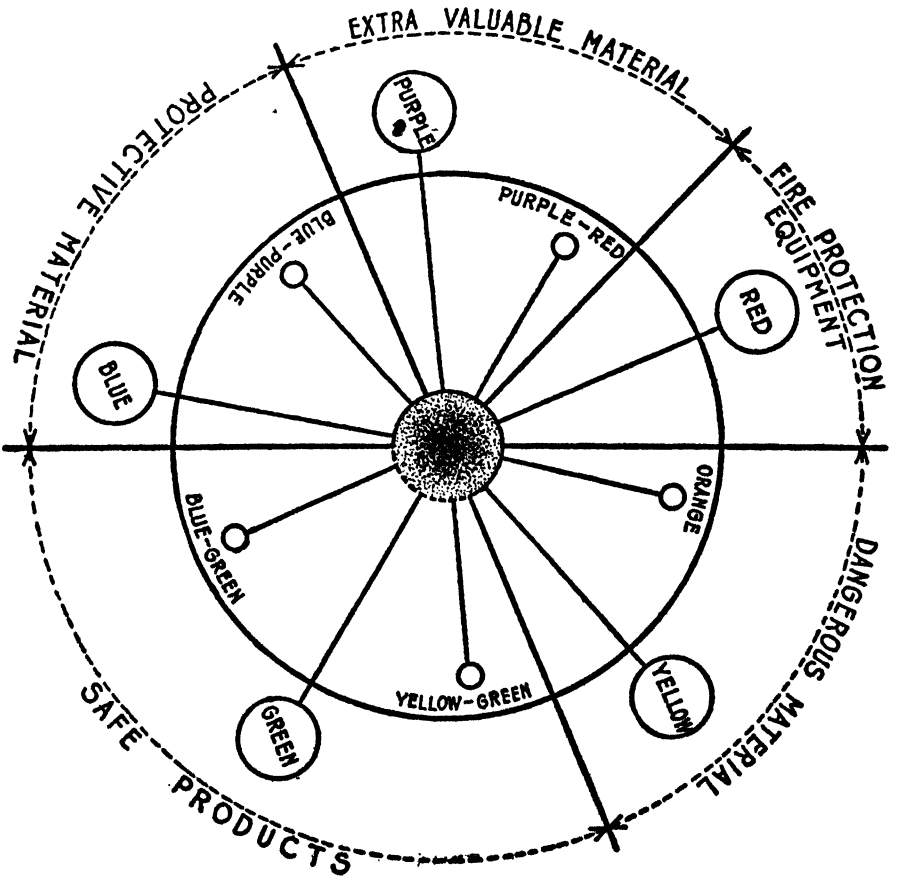


FIG. 1. MAIN CLASSIFICATION BY COLOR[8]

[8]From Scheme for Identification of Piping Systems, *Heating, Piping and Air Conditioning Contractors National Association*, Part V, Fourth Edition, p. 17. Used by permission.

[7]See Scheme for Identification of Piping Systems, A13-1928, *American Standards Association*.

Chapter 3

THERMODYNAMICS

Degree of Saturation; Mollier Diagram; Derived Properties; Typical Air Conditioning Processes, Heating, Cooling, Adiabatic Mixing; Wet-Bulb Temperatures Below 32F; Dalton's Rule; Steady Flow Energy Equation, U. S. Standard Atmosphere

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THE working substance of the air conditioning engineer is called *moist air.* In order to be able to apply the laws of conservation of energy and mass to the analysis of typical air conditioning processes, it is necessary to know the thermodynamic properties of moist air, particularly its enthalpy and volume. When the limitations imposed by the Second Law of Thermodynamics have to be considered, it is also necessary to know its entropy.

For the purpose of analysis, moist air may be regarded as a mixture of only two constituents, namely, dry air and water vapor. It has long been customary to predict the thermodynamic properties of the mixture from a knowledge of those of dry air and water vapor separately by means of Dalton's Rule. According to this rule: each constituent of a gas mixture occupies the whole volume of the mixture just as if no other constituent were present; it therefore exerts a *partial pressure* equal to the pressure it would exert if alone in the whole volume at the temperature of the mixture: the observed pressure of the mixture is the sum of these so-called partial pressures; the enthalpy of the mixture is the sum of separate contributions from the individual constituents as determined by their partial pressures, their weights, and the temperature of the mixture; and the entropy of the mixture is obtained in a similar manner.

Dalton's Rule has long been regarded erroneously as a fundamental law of nature. Actually it is not, and in many cases its predictions are quite unreliable. In the case of moist air at atmospheric pressure, it happens to give a close approximation to the truth; but as progress is made the need for greater accuracy than the rule can afford is felt even in this case. Fortunately most of the complications involved in following a correct procedure based on the predictions of statistical mechanics are met in preparing suitable tables of thermodynamic properties; and, once these tables have been prepared, their use in the analysis of typical air conditioning processes is actually simplified by abandonment of the rule together with its fictitious concepts of partial pressure, relative humidity, etc.

Thermodynamic Properties of Moist Air

Table 1, Thermodynamic Properties of Moist Air (Standard Atmospheric Pressure, 29.921 In. Hg), contains results of a cooperative investigation between the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS and the Towne Scientific School, University of Pennsylvania. These results are to be considered by an International Joint Committee on Psychrometric Data as a possible starting point from which to reach agreement on standard properties of moist air. A detailed explanation of the data and methods used in constructing Table 1 is given in a paper [1] presented before the ASHVE upon the recommendation of its Technical

Advisory Committee on Psychrometry as a final report of the cooperative investigation.

In Table 1 there are 15 columns of figures, each column being headed by a suitable symbol. In the following sub-paragraphs are given brief explanations of the data in Table 1 under the appropriate column headings.

t(F) = Fahrenheit temperature defined in terms of absolute temperature T by the relation,

$$T = t + 459.69 \tag{1}$$

This particular Fahrenheit scale differs slightly from that derived from the International Centigrade Scale t(C) by the definition,

$$t(\text{F}) = 1.8t(\text{C}) + 32 \tag{2}$$

However, the maximum difference between the two Fahrenheit scales appears not to exceed 0.01 Fahrenheit deg in the range 32 to 212 F.

W_s = humidity ratio *at saturation*. By humidity ratio is meant the ratio, by weight, of water vapor to dry air, pounds of water vapor per pound of dry air. By saturation is meant the point where coexistence of the vapor phase (moist air) with a condensed phase (liquid or solid) is possible at the given temperature and pressure (standard atmospheric pressure in the case of Table 1). At given values of temperature and pressure the humidity ratio W can have any value from zero to W_s.

v_a = specific volume of dry air, cubic feet per pound.

$v_{as} = v_s - v_a$, the difference between the volume of moist air *at saturation*, per pound of dry air, and the specific volume of the dry air itself, cubic feet per pound of dry air.

v_s = volume of moist air *at saturation* per pound of dry air, cubic feet per pound of dry air.

h_a = specific enthalpy of dry air, Btu per pound. It will be noticed that the specific enthalpy of dry air has been assigned the value zero at 0 F, standard atmospheric pressure. The energy unit Btu is related to the foot-pound, though not exactly, by definition, as follows: 1 Btu = 778.18 ft-lb.

$h_{as} = h_s - h_a$, the difference between the enthalpy of moist air *at saturation*, per pound of dry air, and the specific enthalpy of the dry air itself, Btu per pound of dry air.

h_s = enthalpy of moist air *at saturation* per pound of dry air, Btu per pound of dry air.

s_a = specific entropy of dry air, Btu per (pound) (F). It will be noticed that the specific entropy of dry air has been assigned the value zero at 0 F and standard atmospheric pressure.

$s_{as} = s_s - s_a$, the difference between the entropy of moist air *at saturation*, per pound of dry air, and the specific entropy of the dry air itself, Btu per (pound of dry air) (F).

s_s = entropy of moist air *at saturation* per pound of dry air, Btu per (pound of dry air) (F).

h_w = specific enthalpy of condensed water (liquid or solid) at standard atmospheric pressure, Btu per pound of water. The specific enthalpy of liquid water has been assigned the value zero at 32 F, saturation pressure. It will be noticed that, under this assignment, the specific enthalpy of liquid water at 32 F, standard atmospheric pressure, assumes the value 0.04 Btu/lb_w.

s_w = specific entropy of condensed water (liquid or solid) at standard atmospheric pressure, Btu per (pound of water) (F). The specific entropy of liquid water has been assigned the value zero at 32 F, saturation pressure. It will be noticed that, under this assignment, the specific entropy of liquid water at 32 F, standard atmospheric pressure, is also zero, though not exactly.

p_s = saturation pressure of pure water vapor, pounds per square inch or inches of Hg. Moist air can be saturated at any given values of temperature and pressure, though this requires that it have a definite humidity ratio W_s and that the coexisting condensed phase contain a definite, but very small quantity of dissolved air. On the other hand, pure water vapor (steam) cannot be saturated at any given values of temperature and pressure because its composition is invariable. It can, however, be saturated at any

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^3$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg $p_s \times 10^3$	
−160	0.2120	7.520	0.000	7.520	−38.504	0 000	−38.504	−0.10300	0.00000	−0.10300	−222.00	−0.4907	0.1009	−160
−159	0 2394	7.545	0.000	7.545	−38.262	0.000	−38 262	−0 10219	0.00000	−0.10219	−221.68	−0.4896	0.1139	−159
−158	0.2703	7.571	0.000	7.571	−38.021	0.000	−38.021	−0.10139	0.00000	−0.10139	−221.36	−0.4885	0.1286	−158
−157	0.3049	7.596	0.000	7.596	−37.779	0.000	−37.779	−0.10059	0.00000	−0.10059	−221.04	−0 4874	0.1450	−157
−156	0.3435	7.622	0.000	7.622	−37.538	0.000	−37.538	−0.09980	0.00000	−0.09980	−220.72	−0.4864	0.1635	−156
−155	0.3869	7.647	0.000	7.647	−37.296	0.000	−37.296	−0.09901	0.00000	−0.09901	−220.40	−0.4853	0.1842	−155
−154	0.4354	7.673	0.000	7.673	−37.055	0.000	−37.055	−0.09822	0.00000	−0.09822	−220.07	−0.4843	0.2073	−154
−153	0.4897	7.699	0.000	7.699	−36 813	0.000	−36.813	−0.09743	0.00000	−0.09743	−219.75	−0.4832	0.2331	−153
−152	0.5502	7.724	0.000	7.724	−36.572	0.000	−36.572	−0.09664	0.00000	−0.09664	−219.42	−0.4822	0.2620	−152
−151	0.6178	7.750	0.000	7.750	−36.330	0.000	−36.330	−0.09586	0.00000	−0.09586	−219.10	−0.4811	0.2942	−151
−150	0.6932	7.775	0.000	7.775	−36.088	0.000	−36.088	−0.09508	0.00000	−0.09508	−218.77	−0.4800	0.3301	−150
−149	0.7772	7.801	0.000	7.801	−35.847	0.000	−35.847	−0.09430	0.00000	−0.09430	−218.44	−0.4789	0.3701	−149
−148	0.8709	7.826	0.000	7.826	−35.606	0.000	−35.606	−0.09352	0.00000	−0.09352	−218.11	−0.4779	0.4146	−148
−147	0.9750	7.851	0 000	7.851	−35.364	0.000	−35.364	−0.09274	0.00000	−0.09274	−217.78	−0.4768	0.4641	−147
−146	1.091	7.876	0 000	7.876	−35.123	0.000	−35.123	−0.09198	0.00000	−0.09198	−217 45	−0.4758	0.5194	−146
−145	1.219	7.902	0.000	7.902	−34.881	0.000	−34.881	−0.09121	0.00000	−0.09121	−217.12	−0.4747	0.5807	−145
−144	1.362	7.927	0.000	7.927	−34 640	0.000	−34.640	−0.09044	0 00000	−0.09044	−216.78	−0.4737	0.6488	−144
−143	1.521	7.953	0 000	7.953	−34.399	0.000	−34.399	−0.08967	0.00000	−0 08967	−216 45	−0.4726	0.7243	−143
−142	1.698	7.978	0.000	7.978	−34.157	0.000	−34.157	−0.08892	0.00000	−0.08892	−216.11	−0.4716	0.8082	−142
−141	1.893	8.004	0.000	8 004	−33.916	0.000	−33.916	−0.08816	0.00000	−0.08816	−215.78	−0.4705	0.9011	−141
−140	2.109	8.029	0.000	8.029	−33.674	0.000	−33.674	−0.08740	0.00000	−0.08740	−215.44	−0.4695	1.004	−140
−139	2.348	8.054	0.000	8.054	−33.433	0.000	−33.433	−0.08664	0.00000	−0.08664	−215.11	−0.4684	1.118	−139
−138	2.613	8.079	0.000	8.079	−33.192	0.000	−33.192	−0.08589	0.00000	−0.08589	−214.77	−0.4674	1.244	−138
−137	2.906	8.105	0.000	8.105	−32.951	0.000	−32.951	−0.08514	0.00000	−0.08514	−214.43	−0.4663	1.383	−137
−136	3.229	8.130	0.000	8.130	−32.709	0.000	−32.709	−0.08440	0.00000	−0.08440	−214.09	−0.4653	1.537	−136
−135	3.586	8.156	0.000	8.156	−32.468	0.000	−32.468	−0.08365	0.00000	−0.08365	−213.75	−0.4642	1 707	−135
−134	3.980	8.181	0.000	8.181	−32.226	0.000	−32.226	−0.08291	0.00000	−0.08291	−213.41	−0.4632	1 895	−134
−133	4.414	8.207	0.000	8.207	−31.985	0 000	−31.985	−0.08217	0.00000	−0.08217	−213.07	−0.4621	2.102	−133
−132	4.893	8.232	0.000	8.232	−31.744	0.000	−31.744	−0.08144	0.00000	−0.08144	−212.72	−0.4611	2.330	−132
−131	5 419	8.258	0 000	8.258	−31.503	0.000	−31.503	−0.08070	0.00000	−0.08070	−212.38	−0.4600	2.581	−131
−130	6.000	8 283	0 000	8.283	−31.262	0.000	−31.262	−0.07997	0.00000	−0.07997	−212.03	−0.4590	2.858	−130
−129	6.637	8.309	0.000	8.309	−31.021	0.000	−31.021	−0.07924	0.00000	−0.07924	−211.68	−0.4579	3.182	−129

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^7$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg $p_s \times 10^3$	
−128	0.7339	8.334	0.000	8.334	−30.780	0.000	−30.780	−0.07851	0.00000	−0.07851	−211.33	−0.4569	0.3492	−128
−127	0.8111	8.360	0.000	8.360	−30.539	0.000	−30.539	−0.07778	0.00000	−0.07778	−210.98	−0.4559	0.3863	−127
−126	0.8958	8.385	0.000	8.385	−30.298	0.000	−30.298	−0.07707	0.00000	−0.07707	−210.63	−0.4548	0.4267	−126
−125	0.9887	8.411	0.000	8.411	−30.057	0.000	−30.057	−0.07634	0.00000	−0.07634	−210.28	−0.4538	0.4710	−125
−124	1.091	8.436	0.000	8.436	−29.816	0.000	−29.816	−0.07562	0.00000	−0.07562	−209.93	−0.4527	0.5197	−124
−123	1.202	8.461	0.000	8.461	−29.575	0.000	−29.575	−0.07490	0.00000	−0.07490	−209.58	−0.4517	0.5730	−123
−122	1.325	8.486	0.000	8.486	−29.334	0.000	−29.334	−0.07419	0.00000	−0.07419	−209.23	−0.4506	0.6314	−122
−121	1.459	8.512	0.000	8.512	−29.093	0.000	−29.093	−0.07348	0.00000	−0.07348	−208.88	−0.4496	0.6953	−121
−120	1.606	8.537	0.000	8.537	−28.852	0.000	−28.852	−0.07277	0.00000	−0.07277	−208.52	−0.4485	0.7653	−120
−119	1.767	8.563	0.000	8.563	−28.611	0.000	−28.611	−0.07206	0.00000	−0.07206	−208.17	−0.4475	0.8419	−119
−118	1.942	8.588	0.000	8.588	−28.370	0.000	−28.370	−0.07135	0.00000	−0.07135	−207.81	−0.4464	0.9256	−118
−117	2.134	8.613	0.000	8.613	−28.129	0.000	−28.129	−0.07064	0.00000	−0.07064	−207.45	−0.4454	1.017	−117
−116	2.343	8.639	0.000	8.639	−27.889	0.000	−27.889	−0.06994	0.00000	−0.06994	−207.09	−0.4444	1.117	−116
−115	2.571	8.664	0.000	8.664	−27.648	0.000	−27.648	−0.06924	0.00000	−0.06924	−206.73	−0.4433	1.226	−115
−114	2.820	8.690	0.000	8.690	−27.407	0.000	−27.407	−0.06854	0.00000	−0.06854	−206.37	−0.4423	1.345	−114
−113	3.092	8.715	0.000	8.715	−27.166	0.000	−27.166	−0.06784	0.00000	−0.06784	−206.01	−0.4412	1.475	−113
−112	3.388	8.741	0.000	8.741	−26.926	0.000	−26.926	−0.06715	0.00000	−0.06715	−205.65	−0.4402	1.617	−112
−111	3.711	8.766	0.000	8.766	−26.685	0.000	−26.685	−0.06646	0.00000	−0.06646	−205.29	−0.4392	1.771	−111
−110	4.063	8.792	0.000	8.792	−26.444	0.000	−26.444	−0.06577	0.00000	−0.06577	−204.92	−0.4381	1.939	−110
−109	4.445	8.817	0.000	8.817	−26.204	0.000	−26.204	−0.06508	0.00000	−0.06508	−204.46	−0.4371	2.121	−109
−108	4.861	8.842	0.000	8.842	−25.963	0.001	−25.962	−0.06439	0.00000	−0.06439	−204.19	−0.4360	2.320	−108
−107	5.314	8.868	0.000	8.868	−25.772	0.001	−25.721	−0.06370	0.00000	−0.06370	−203.83	−0.4350	2.536	−107
−106	5.806	8.893	0.000	8.893	−25.481	0.001	−25.480	−0.06302	0.00000	−0.06302	−203.46	−0.4339	2.771	−106
−105	6.340	8.919	0.000	8.919	−25.240	0.001	−25.239	−0.06234	0.00000	−0.06234	−203.09	−0.4329	3.026	−105
−104	6.920	8.944	0.000	8.944	−25.000	0.001	−24.999	−0.06167	0.00000	−0.06167	−202.72	−0.4318	3.303	−104
−103	7.549	8.970	0.000	8.970	−24.759	0.001	−24.758	−0.06099	0.00000	−0.06099	−202.35	−0.4308	3.603	−103
−102	8.232	8.995	0.000	8.995	−24.518	0.001	−24.517	−0.06032	0.00000	−0.06032	−201.98	−0.4298	3.929	−102
−101	8.972	9.020	0.000	9.020	−24.278	0.001	−24.277	−0.05964	0.00000	−0.05964	−201.61	−0.4287	4.283	−101
−100	9.772	9.046	0.000	9.046	−24.037	0.001	−24.036	−0.05897	0.00000	−0.05897	−201.23	−0.4277	4.666	−100
−99	10.63	9.071	0.000	9.071	−23.797	0.001	−23.796	−0.05830	0.00000	−0.05830	−200.86	−0.4266	5.081	−99
−98	11.57	9.097	0.000	9.097	−23.556	0.001	−23.555	−0.05764	0.00000	−0.05764	−200.48	−0.4256	5.530	−98
−97	12.59	9.122	0.000	9.122	−23.316	0.001	−23.315	−0.05697	0.00000	−0.05697	−200.11	−0.4245	6.016	−97

[a]Compiled by John A. Goff and S Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^6$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg $p_s \times 10^4$	
−96	1.369	9.147	0.000	9.147	−23.075	0.001	−23.074	−0.05631	0.00000	−0.05631	−199.73	−0.4235	0.6542	−96
−95	1.489	9.173	0.000	9.173	−22.835	0.002	−22.833	−0.05565	0.00000	−0.05565	−199.35	−0.4225	0.7111	−95
−94	1.617	9.198	0.000	9.198	−22.594	0.002	−22.592	−0.05500	0.00000	−0.05500	−198.97	−0.4214	0.7725	−94
−93	1.756	9.224	0.000	9.224	−22.353	0.002	−22.341	−0.05434	0.00000	−0.05434	−198.59	−0.4204	0.8388	−93
−92	1.906	9.249	0.000	9.249	−22.113	0.002	−22.111	−0.05369	0.00001	−0.05368	−198.21	−0.4193	0.9105	−92
−91	2.068	9.275	0.000	9.275	−21.872	0.002	−21.870	−0.05303	0.00001	−0.05302	−197.83	−0.4183	0.9879	−91
−90	2.242	9.300	0.000	9.300	−21.631	0.002	−21.629	−0.05237	0.00001	−0.05236	−197.44	−0.4173	1.071	−90
−89	2.430	9.325	0.000	9.325	−21.391	0.003	−21.388	−0.05172	0.00001	−0.05171	−197.06	−0.4162	1.161	−89
−88	2.634	9.351	0.000	9.351	−21.150	0.003	−21.147	−0.05107	0.00001	−0.05106	−196.67	−0.4152	1.259	−88
−87	2.852	9.376	0.000	9.376	−20.909	0.003	−20.906	−0.05042	0.00001	−0.05041	−196.29	−0.4142	1.363	−87
−86	3.089	9.401	0.000	9.401	−20.669	0.003	−20.666	−0.04978	0.00001	−0.04977	−195.90	−0.4131	1.476	−86
−85	3.342	9.426	0.000	9.426	−20.428	0.003	−20.425	−0.04913	0.00001	−0.04912	−195.51	−0.4121	1.597	−85
−84	3.615	9.451	0.000	9.451	−20.188	0.004	−20.184	−0.04849	0.00001	−0.04848	−195.12	−0.4110	1.728	−84
−83	3.909	9.477	0.000	9.477	−19.947	0.004	−19.943	−0.04785	0.00001	−0.04784	−194.73	−0.4100	1.868	−83
−82	4.225	9.502	0.000	9.502	−19.706	0.004	−19.702	−0.04721	0.00001	−0.04720	−194.34	−0.4090	2.019	−82
−81	4.564	9.527	0.000	9.527	−19.466	0.005	−19.461	−0.04658	0.00001	−0.04657	−193.95	−0.4079	2.181	−81
−80	4.930	9.553	0.000	9.553	−19.225	0.005	−19.220	−0.04595	0.00001	−0.04594	−193.55	−0.4069	2.356	−80
−79	5.322	9.578	0.000	9.578	−18.984	0.005	−18.979	−0.04532	0.00002	−0.04530	−193.16	−0.4059	2.543	−79
−78	5.742	9.604	0.000	9.604	−18.744	0.006	−18.738	−0.04469	0.00002	−0.04467	−192.76	−0.4048	2.744	−78
−77	6.193	9.629	0.000	9.629	−18.503	0.006	−18.497	−0.04406	0.00002	−0.04404	−192.37	−0.4038	2.960	−77
−76	6.677	9.654	0.000	9.654	−18.263	0.007	−18.256	−0.04343	0.00002	−0.04341	−191.97	−0.4027	3.192	−76
−75	7.196	9.680	0.000	9.680	−18.022	0.007	−18.015	−0.04280	0.00002	−0.04278	−191.57	−0.4017	3.441	−75
−74	7.753	9.705	0.000	9.705	−17.782	0.008	−17.774	−0.04218	0.00003	−0.04215	−191.17	−0.4007	3.707	−74
−73	8.349	9.730	0.000	9.730	−17.541	0.008	−17.533	−0.04155	0.00003	−0.04152	−190.77	−0.3996	3.992	−73
−72	8.990	9.756	0.000	9.756	−17.301	0.009	−17.292	−0.04093	0.00003	−0.04090	−190.37	−0.3986	4.298	−72
−71	9.675	9.781	0.000	9.781	−17.060	0.010	−17.050	−0.04031	0.00003	−0.04028	−189.97	−0.3975	4.625	−71
−70	10.40	9.806	0.000	9.806	−16.820	0.011	−16.809	−0.03969	0.00003	−0.03966	−189.56	−0.3965	4.976	−70
−69	11.19	9.831	0.000	9.831	−16.579	0.011	−16.568	−0.03908	0.00004	−0.03904	−189.16	−0.3954	5.351	−69
−68	12.03	9.856	0.000	9.856	−16.339	0.012	−16.327	−0.03846	0.00004	−0.03842	−188.75	−0.3944	5.752	−68
−67	12.92	9.882	0.000	9.882	−16.098	0.013	−16.085	−0.03785	0.00004	−0.03781	−188.35	−0.3934	6.181	−67
−66	13.88	9.907	0.000	9.907	−15.858	0.014	−15.844	−0.03724	0.00004	−0.03720	−187.94	−0.3924	6.640	−66
−65	14.91	9.932	0.000	9.932	−15.617	0.015	−15.602	−0.03663	0.00005	−0.03658	−187.53	−0.3913	7.130	−65

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^5$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg $p_s \times 10^3$	
−64	1.601	9.958	0.000	9.958	−15.377	0 016	−15.361	−0 03602	0.00005	−0.03597	−187.12	−0.3903	0.7654	−64
−63	1.718	9.983	0.000	9.983	−15.137	0.018	−15.119	−0.03541	0 00005	−0.03536	−186.71	−0.3893	0 8213	−63
−62	1.843	10.009	0.000	10.009	−14.896	0.019	−14.877	−0.03481	0 00006	−0.03475	−186.30	−0.3882	0.8810	−62
−61	1.976	10.034	0.000	10.034	−14.656	0.020	−14.636	−0 03420	0.00006	−0.03414	−185.89	−0.3872	0.9447	−61
−60	2.118	10.059	0.000	10.059	−14.416	0.022	−14.394	−0.03360	0 00006	−0 03354	−185.47	−0.3861	1.0127	−60
−59	2.269	10.085	0.000	10 085	−14.175	0.023	−14.152	−0.03300	0.00007	−0 03293	−185.06	−0.3851	1 0852	−59
−58	2.431	10.110	0.000	10.110	−13.935	0.025	−13.910	−0 03240	0 00007	−0.03233	−184.64	−0.3841	1.1624	−58
−57	2.603	10.135	0.000	10.135	−13.695	0.027	−13.668	−0.03180	0.00008	−0.03172	−184.23	−0.3830	1.2447	−57
−56	2.786	10.161	0.000	10.161	−13.454	0 029	−13.425	−0.03120	0.00008	−0 03112	−183.81	−0.3820	1.3324	−56
−55	2.982	10.186	0.000	10.186	−13.214	0 031	−13.183	−0 03061	0 00009	−0.03052	−183.39	−0.3810	1.4258	−55
−54	3.190	10.211	0 000	10.211	−12.974	0.033	−12.941	−0 03002	0.00009	−0.02993	−182.97	−0.3799	1.5253	−54
−53	3.411	10.237	0.000	10 237	−12.733	0.035	−12.698	−0.02943	0.0010	−0 02933	−182.55	−0.3789	1.6312	−53
−52	3.646	10.262	0.001	10.263	−12.493	0.038	−12.455	−0.02884	0.00011	−0.02873	−182.13	−0.3779	1.7438	−52
−51	3.897	10.288	0.001	10.289	−12.253	0.041	−12.212	−0.02825	0.00011	−0.02814	−181.71	−0.3769	1.8635	−51
−50	4.163	10.313	0.001	10.314	−12.012	0.043	−11.969	−0.02766	0.00012	−0.02754	−181.29	−0.3758	1.9910	−50
−49	4.446	10.338	0.001	10.339	−11.772	0.046	−11.726	−0.02707	0.00012	−0.02695	−180.87	−0.3748	2.1264	−49
−48	4.747	10.364	0.001	10.365	−11.532	0.049	−11.483	−0 02649	0 00013	−0.02636	−180.44	−0.3738	2.2702	−48
−47	5 066	10.389	0.001	10.390	−11.292	0.053	−11.239	−0.02590	0.00013	−0.02577	−180.02	−0.3728	2.4230	−47
−46	5.406	10.414	0.001	10 415	−11.051	0.056	−10.995	−0.02532	0.00014	−0.02518	−179.59	−0.3717	2.5854	−46
−45	5.766	10.440	0.001	10.441	−10.811	0.060	−10.751	−0.02474	0.00015	−0.02459	−179.16	−0.3707	2.7578	−45
−44	6.149	10.465	0.001	10.466	−10.571	0.064	−10.507	−0.02416	0.00016	−0.02400	−178.73	−0.3696	2.9408	−44
−43	6.555	10.490	0.001	10.491	−10.330	0.068	−10.262	−0.02358	0.00017	−0.02341	−178.30	−0.3686	3.1349	−43
−42	6.985	10.516	0.001	10.517	−10.090	0.073	−10.017	−0.02301	0.00019	−0.02282	−177.87	−0.3676	3.3408	−42
−41	7.441	10.541	0.001	10.542	−9.850	0.078	−9.772	−0.02243	0.00020	−0.02223	−177.44	−0.3665	3.5591	−41
−40	7.925	10.566	0.001	10.567	−9.609	0.083	−9.526	−0.02186	0.00021	−0.02165	−177.01	−0.3655	3.7906	−40
−39	8.437	10.592	0.001	10.593	−9.369	0.089	−9.280	−0.02129	0.00022	−0.02107	−176.58	−0.3645	4.0359	−39
−38	8.980	10.617	0.002	10.619	−9.129	0.094	−9.035	−0.02072	0.00024	−0.02048	−176.14	−0.3634	4 2958	−38
−37	9.556	10.642	0.002	10.644	−8.889	0.100	−8.789	−0.02015	0.00025	−0.01990	−175.71	−0.3624	4.5711	−37
−36	10.16	10.668	0.002	10.670	−8.648	0.106	−8.542	−0.01958	0.00026	−0.01932	−175.27	−0.3614	4.8626	−36
−35	10.81	10.693	0.002	10.695	−8.408	0.113	−8.295	−0.01902	0.00028	−0.01874	−174.84	−0.3604	5.1713	−35
−34	11.49	10.718	0.002	10.720	−8.168	0.121	−8.047	−0.01845	0.00030	−0.01815	−174.40	−0.3593	5.4980	−34
−33	12.21	10.744	0 002	10.746	−7.927	0.128	−7.799	−0.01789	0.00032	−0.01757	−173.96	−0.3583	5.8437	−33

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^4$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg $p_s \times 10^3$	
−32	1.298	10.769	0.002	10.771	−7.687	0.136	−7.551	−0.01733	0.00034	−0.01699	−173.52	−0.3573	0.62093	−32
−31	1.378	10.794	0.002	10.796	−7.447	0.145	−7.302	−0.01677	0 00036	−0.01641	−173.08	−0.3563	0.65979	−31
−30	1.464	10.820	0.002	10.822	−7.207	0.154	−7.053	−0.01621	0.00038	−0.01583	−172.64	−0.3552	0.70046	−30
−29	1.554	10.845	0.003	10.848	−6.966	0.163	−6.803	−0.01565	0.00040	−0.01525	−172.20	−0.3542	0.74365	−29
−28	1.649	10.870	0.003	10.873	−6.726	0.173	−6.553	−0.01509	0.00043	−0.01466	−171.75	−0.3531	0.78928	−28
−27	1.750	10.896	0.003	10.899	−6.486	0.184	−6.302	−0.01453	0.00045	−0.01408	−171 31	−0.3521	0.83748	−27
−26	1.856	10.921	0.003	10.924	−6.246	0.196	−6.050	−0.01398	0.00048	−0.01350	−170.86	−0.3511	0.88838	−26
−25	1.969	10.946	0.004	10.950	−6.005	0.207	−5.798	−0.01342	0.00051	−0.01291	−170.42	−0.3500	0.94212	−25
−24	2.087	10.972	0.004	10.976	−5.765	0.219	−5.546	−0.01287	0.00054	−0.01233	−169.97	−0.3490	0.99885	−24
−23	2.212	10.997	0 004	11.001	−5.525	0.232	−5.293	−0.01232	0.00057	−0.01175	−169.52	−0.3480	1.0587	−23
−22	2.344	11 022	0.004	11.026	−5.285	0.246	−5.039	−0.01177	0.00061	−0 01116	−169.07	−0.3469	1.1219	−22
−21	2.483	11.048	0.004	11.052	−5.044	0.261	−4.783	−0.01122	0.00064	−0.01058	−168.62	−0.3459	1.1885	−21
−20	2.630	11.073	0.005	11.078	−4.804	0.277	−4.527	−0.01067	0.00068	−0.00999	−168.17	−0.3449	1.2587	−20
−19	2.785	11.098	0.005	11.103	−4.564	0.293	−4.271	−0.01012	0.00072	−0.00940	−167.72	−0.3439	1.3327	−19
−18	2.948	11.124	0.005	11.129	−4.324	0.310	−4.014	−0.00958	0.00076	−0.00882	−167.26	−0.3428	1.4107	−18
−17	3.120	11.149	0.006	11.155	−4.083	0.328	−3.755	−0.00904	0.00080	−0.00824	−166.81	−0.3418	1.4929	−17
−16	3.301	11.174	0.0006	11.180	−3.843	0.348	−3.495	−0.00850	0.00084	−0.00766	−166.35	−0.3408	1.5795	−16
−15	3.491	11.200	0.006	11.206	−3.603	0.368	−3.235	−0.00796	0.00089	−0.00707	−165.90	−0.3398	1.6706	−15
−14	3.692	11.225	0.007	11.232	−3.363	0.389	−2.974	−0.00743	0.00094	−0.00649	−165.44	−0.3387	1.7666	−14
−13	3.903	11.250	0.007	11.257	−3.123	0.412	−2.711	−0.00689	0.00099	−0.00590	−164.98	−0.3377	1.8677	−13
−12	4.125	11.275	0.008	11.283	−2.882	0.436	−2.446	−0.00636	0.00104	−0.00532	−164.52	−0.3367	1.9740	−12
−11	4.359	11.301	0.008	11.309	−2.642	0.461	−2.181	−0.00582	0.00109	−0.00473	−164.06	−0.3357	2.0859	−11
−10	4.606	11.326	0.008	11.334	−2.402	0.487	−1.915	−0.00529	0.00115	−0.00414	−163.60	−0.3346	2.2035	−10
−9	4.865	11.351	0.008	11.359	−2.162	0.514	−1.648	−0.00475	0.00121	−0.00354	−163.14	−0.3336	2.3272	−9
−8	5.137	11.376	0.009	11.385	−1.922	0.543	−1.379	−0.00422	0.00128	−0.00294	−162.67	−0.3326	2.4573	−8
−7	5.423	11.401	0.010	11.411	−1.681	0.574	−1.107	−0.00369	0.00135	−0.00234	−162.21	−0.3316	2.5940	−7
−6	5.724	11.427	0.010	11.437	−1.441	0.606	−0.835	−0.00316	0.00142	−0.00174	−161.74	−0.3305	2.7377	−6
−5	6.040	11.452	0.011	11.463	−1.201	0.639	−0.562	−0.00263	0.00149	−0.00114	−161.28	−0.3295	2.8886	−5
−4	6.371	11.477	0.012	11.489	−0.961	0.675	−0.286	−0.00210	0.00157	−0.00053	−160.81	−0.3285	3.0472	−4
−3	6.720	11 502	0.013	11.515	−0.721	0.712	−0.009	−0.00157	0.00165	0.00008	−160.34	−0.3275	3.2137	−3
−2	7.085	11.528	0.013	11.541	−0.480	0.751	0.271	−0.00105	0.00174	0.00069	−159.87	−0.3264	3.3885	−2
−1	7.469	11.553	0.014	11.567	−0.240	0.792	0.552	−0.00052	0.00183	0.00131	−159.40	−0.3254	3.5720	−1

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^3$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg $p_s \times 10^3$	
0	0.7872	11.578	0.015	11.593	0.000	0.835	0.835	0.00000	0.00192	0.00192	−158.93	−0.3244	3.7645	0
1	0.8295	11.604	0.015	11.619	0.240	0.880	1.120	0.00052	0.00202	0.00254	−158.46	−0.3234	3.9666	1
2	0.8739	11.629	0.016	11.645	0.480	0.928	1.408	0.00104	0.00212	0.00316	−157.99	−0.3223	4.1785	2
3	0.9204	11.654	0.017	11.671	0.721	0.977	1.698	0.00156	0.00223	0 00379	−157.52	−0.3213	4.4007	3
4	0.9692	11.679	0.018	11.697	0.961	1.030	1.991	0.00208	0.00234	0.00442	−157.04	−0.3203	4.6337	4
5	1.020	11.705	0.019	11.724	1.201	1.085	2.286	0.00260	0.00246	0.00506	−156.57	−0.3193	4.8779	5
6	1.074	11.730	0.020	11.750	1.441	1.142	2.583	0.00312	0.00258	0.00570	−156.09	−0.3182	5.1339	6
7	1.130	11.756	0.021	11.777	1.681	1.202	2.883	0.00364	0.00271	0.00635	−155.61	−0.3172	5.4022	7
8	1 189	11.781	0.022	11.803	1.922	1.266	3.188	0.00415	0.00285	0.00700	−155.13	−0.3162	5.6832	8
9	1.251	11.806	0.024	11.830	2.162	1.332	3.494	0.00467	0.00299	0.00766	−154.65	−0.3152	5.9776	9
10	1.315	11.831	0.025	11.856	2.402	1.401	3.803	0.00518	0.00314	0.00832	−154.17	−0.3141	6.2858	10
11	1.383	11.857	0.026	11.883	2.642	1.474	4.116	0.00569	0.00330	0.00899	−153.69	−0.3131	6.6085	11
12	1.454	11.882	0.028	11.910	2.882	1.550	4.432	0.00620	0.00346	0.00966	−153.21	−0.3121	6.9462	12
13	1.528	11.907	0.029	11.936	3.123	1.630	4.753	0.00671	0.00363	0 01034	−152.73	−0.3111	7.2997	13
14	1.606	11.933	0.030	11.963	3.363	1.713	5.076	0.00721	0.00380	0.01101	−152.24	−0.3100	7.6696	14
15	1.687	11.958	0.032	11.990	3.603	1.800	5.403	0.00772	0.00399	0.01171	−151.76	−0.3090	8.0565	15
16	1.772	11 983	0.034	12.017	3.843	1.892	5.735	0.00822	0.00418	0.01210	−151.27	−0.3080	8.4612	16
17	1.861	12.009	0.035	12.044	4.083	1.988	6.071	0.00873	0.00438	0.01311	−150.78	−0.3070	8.8843	17
18	1.953	12.034	0 038	12.072	4.324	2.088	6.412	0.00923	0.00459	0.01382	−150.29	−0.3059	9.3267	18
19	2.051	12.059	0.040	12.099	4.564	2.192	6.756	0.00973	0.00481	0.01154	−149.80	−0.3049	9.7889	19
20	2.152	12.084	0.042	12.126	4.804	2.302	7.106	0.01023	0.00504	0.01527	−149.31	−0.3039	10 272	20
21	2.258	12.110	0.044	12.154	5.044	2.416	7.460	0.01073	0.00528	0.01601	−148.82	−0.3029	10.777	21
22	2.369	12.135	0 046	12.181	5.284	2.536	7.820	0.01123	0.00553	0.01676	−148.33	−0.3018	11.305	22
23	2.485	12.160	0.049	12.209	5.525	2.661	8.186	0 01173	0 00579	0.01752	−147 84	−0.3008	11.856	23
24	2.606	12.186	0.051	12.237	5.765	2.792	8.557	0.01223	0.00607	0.01830	−147 34	−0.2998	12.431	24
25	2.733	12.211	0.054	12.265	6.005	2.929	8.934	0.01273	0.00635	0.01908	−146.85	−0.2988	13.032	25
26	2.865	12.236	0.057	12.293	6.245	3.072	9.317	0.01322	0.00665	0.01987	−146.35	−0.2977	13.659	26
27	3.003	12.262	0.059	12.321	6 485	3.221	9.706	0.01372	0.00696	0.02068	−145.85	−0.2967	14.313	27
28	3.147	12.287	0.062	12.349	6.726	3 377	10.103	0.01421	0.00728	0.02149	−145.36	−0.2957	14.996	28
29	3.297	12.312	0.065	12.377	6.966	3.540	10.506	0.01470	0.00761	0.02231	−144.86	−0.2947	15.709	29
30	3.454	12.338	0 068	12.406	7 206	3.709	10 915	0.01519	0.00796	0.02315	−144.36	−0.2936	16.452	30
31	3.617	12.363	0 071	12.434	7.446	3.887	11.333	0.01568	0.00832	0.02400	−143.86	−0.2926	17.227	31
32	3.788	12.388	0.075	12.463	7.686	4.072	11.758	0.01617	0.00870	0.02487	−143.36	−0.2916	18.035	32
*32	3.788	12.388	0.075	12.463	7.686	4.072	11.758	0.01617	0.00870	0 02487	0.04	0.0000	18.037	32*
33	3.944	12 413	0.079	12 492	7.927	4.242	12.169	0.01666	0.00904	0.02570	1.05	0 0020	18.778	33
34	4.107	12.438	0.082	12.520	8.167	4.418	12.585	0.01715	0.00940	0.02655	2.06	0.0041	19.546	34

[a]Compiled by John A. Goff and S. Gratch.
*Extrapolated to represent metastable equilibrium with undercooled liquid.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^3$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg p_s	
35	4.275	12.464	0.085	12.549	8.407	4.601	13.008	0.01764	0.00977	0.02741	3.06	0.00061	0 20342	35
36	4.450	12.489	0.089	12.578	8.647	4.791	13.438	0.01812	0.01016	0.02828	4.07	0.0081	0.21166	36
37	4.631	12.514	0.093	12.607	8.887	4.987	13.874	0.01861	0.01056	0.02917	5.07	0.0102	0.22020	37
38	4.818	12.540	0.097	12.637	9.128	5.191	14 319	0.01909	0.01097	0.03006	6.08	0 0122	0.22904	38
39	5.012	12.565	0.101	12.666	9.368	5.403	14.771	0.01957	0.01139	0.03096	7.08	0.0142	0.23819	39
40	5.213	12.590	0.105	12.695	9.608	5 622	15.230	0.02005	0.01183	0.03188	8.09	0.0162	0.24767	40
41	5.421	12.616	0.109	12.725	9.848	5.849	15.697	0.02053	0.01228	0.03281	9.09	0.0182	0.25748	41
42	5.638	12.641	0.114	12.755	10.088	6.084	16.172	0.02101	0.01275	0.03376	10.09	0.0202	0.26763	42
43	5.860	12.666	0.119	12.785	10.329	6.328	16.657	0.02149	0.01323	0.03472	11.10	0.0222	0.27813	43
44	6.091	12.691	0.124	12.815	10.569	6.580	17.149	0.02197	0.01373	0.03570	12.10	0.0242	0.28899	44
45	6.331	12.717	0.129	12.846	10.809	6.841	17.650	0.02245	0.01425	0.03670	13.10	0.0262	0.30023	45
46	6.578	12.742	0.134	12.876	11.049	7.112	18.161	0.02293	0.01478	0.03771	14.10	0.0282	0.31185	46
47	6.835	12.767	0.140	12.907	11.289	7.391	18.680	0.02340	0.01534	0.03874	15.11	0.0302	0.32386	47
48	7.100	12.792	0.146	12.938	11.530	7.681	19.211	0.02387	0.01591	0.03978	16.11	0.0321	0.33629	48
49	7.374	12.818	0.151	12.969	11.770	7.981	19.751	0.02434	0.01650	0.04084	17.11	0.0341	0.34913	49
50	7.658	12.843	0.158	13.001	12.010	8.291	20.301	0.02481	0.01711	0.04192	18.11	0.0361	0.36240	50
51	7.952	12.868	0.164	13.032	12.250	8.612	20.862	0.02528	0.01774	0.04302	19.11	0.0381	0.37611	51
52	8.256	12.894	0.170	13.064	12.491	8.945	21.436	0.02575	0.01839	0.04414	20.11	0.0400	0.39028	52
53	8.569	12.919	0.178	13.097	12.731	9.289	22.020	0.02622	0.01906	0.04528	21.12	0.0420	0.40192	53
54	8.894	12.944	0.185	13.129	12.971	9.644	22.615	0.02669	0.01976	0.04645	22.12	0.0439	0.42004	54
55	9.229	12.970	0.192	13.162	13.211	10.01	23.22	0.02716	0.02047	0.04763	23.12	0.0459	0.43565	55
56	9.575	12.995	0.200	13.195	13.452	10.39	23.84	0.02762	0.02121	0.04883	24.12	0.0478	0.45176	56
57	9.934	13.020	0.208	13.228	13.692	10.79	24.48	0.02809	0.02197	0.05006	25.12	0.0497	0.46840	57
58	10.30	13.045	0.216	13.261	13.932	11.19	25.12	0.02855	0.02276	0.05131	26.12	0.0517	0.48558	58
59	10.69	13.071	0.224	13.295	14.172	11.61	25.78	0.02902	0.02357	0.05259	27.12	0.0536	0.50330	59
60	11.08	13.096	0.233	13.329	14.413	12.05	26.46	0.02948	0.02441	0.05389	28.12	0.0555	0.52159	60
61	11.49	13.121	0.242	13.363	14.653	12.50	27.15	0.02994	0.02527	0.05521	29.12	0.0574	0.54047	61
62	11.91	13.147	0.251	13.398	14.893	12.96	27.85	0.03040	0.02616	0.05656	30.12	0.0594	0.55994	62
63	12.35	13.172	0.261	13.433	15.134	13.44	28.57	0.03086	0.02708	0.05794	31.12	0.0613	0.58002	63
64	12.80	13.197	0.271	13.468	15.374	13.94	29.31	0.03132	0.02803	0.05935	32.12	0.0632	0.60073	64
65	13.26	13.222	0.282	13.504	15.614	14.45	30.06	0.03177	0.02901	0.06078	33.11	0.0651	0.62209	65
66	13.74	13.247	0.292	13.539	15.855	14.98	30.83	0.03223	0.03002	0.06225	34.11	0.0670	0.64411	66
67	14.24	13.273	0.303	13.576	16.095	15.53	31.62	0.03269	0.03106	0.06375	35.11	0.0689	0.66681	67
68	14.75	13.298	0.315	13.613	16.335	16.09	32.42	0.03314	0.03213	0.06527	36.11	0.0708	0.69019	68
69	15.28	13.323	0.327	13.650	16.576	16.67	33.25	0.03360	0.03323	0.06683	37.11	0.0727	0.71430	69

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO $W_s \times 10^2$	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap Press In. Hg p_s	
70	1.582	13.348	0.339	13.687	16.816	17.27	34.09	0.03405	0.03137	0.06842	38.11	0.0746	0.73915	70
71	1.639	13.373	0.351	13.724	17.056	17.89	34.95	0.03450	0.03554	0.07004	39.11	0.0765	0.76475	71
72	1.697	13.398	0.364	13.762	17.297	18.53	35.83	0.03495	0.03675	0.07170	40.11	0.0784	0.79112	72
73	1.757	13.424	0.377	13.801	17.537	19.20	36.74	0.03540	0.03800	0.07340	41.11	0.0803	0.81828	73
74	1.819	13.449	0.392	13.841	17.778	19.88	37.66	0.03585	0.03928	0.07513	42.10	0.0821	0.84624	74
75	1.882	13.474	0.407	13.881	18.018	20.59	38.61	0.03630	0.04060	0.07690	43.10	0 0840	0.87504	75
76	1.948	13.499	0.422	13.921	18.259	21.31	39.57	0.03675	0 04197	0.07872	44.10	0.0859	0.90470	76
77	2.016	13.525	0.437	13.962	18.499	22.07	40.57	0.03720	0.04337	0.08057	45.10	0.0877	0.93523	77
78	2.086	13.550	0.453	14.003	18.740	22.84	41.58	0.03765	0.04482	0.08247	46.10	0.0896	0.96665	78
79	2.158	13.575	0.470	14.045	18.980	23.64	42.62	0.03810	0.04631	0.08441	47.10	0.0914	0.99899	79
80	2.233	13.601	0.486	14.087	19.221	24.47	43.69	0.03854	0.04784	0.08638	48.10	0.0933	1.0323	80
81	2.310	13.626	0.504	14.130	19.461	25.32	44.78	0.03899	0.04942	0.08841	49.09	0.0952	1.0665	81
82	2.389	13.651	0.523	14.174	19.702	26.20	45.90	0.03943	0.05105	0.09048	50.09	0.0970	1.1017	82
83	2.471	13.676	0.542	14.218	19.942	27.10	47.04	0.03987	0.05273	0.09260	51.09	0.0989	1.1379	83
84	2.555	13.702	0.560	14.262	20.183	28.04	48.22	0.04031	0.05446	0.09477	52.09	0.1007	1.1752	84
85	2.642	13.727	0.581	14.308	20.423	29.01	49.43	0.04075	0.05624	0.09699	53.09	0.1025	1.2135	85
86	2.731	13.752	0.602	14.354	20.663	30.00	50.66	0.04119	0.05807	0.09926	54.08	0.1043	1.2529	86
87	2.824	13.777	0.624	14.401	20.904	31.03	51.93	0.04163	0.05995	0.10158	55.08	0.1062	1.2934	87
88	2.919	13.803	0.645	14.448	21.144	32.09	53.23	0.04207	0.06189	0.10396	56.08	0.1080	1.3351	88
89	3.017	13.828	0.668	14.496	21.385	33.18	54.56	0.01251	0.06389	0.10640	57.08	0.1098	1.3779	89
90	3.118	13.853	0.692	14.545	21.625	34.31	55.93	0.04295	0.06596	0.10890	58.08	0.1116	1.4219	90
91	3.223	13.879	0.716	14.595	21.865	35.47	57.33	0.04339	0.06807	0.11146	59.07	0.1135	1.4671	91
92	3.330	13.904	0.741	14.645	22.106	36.67	58.78	0.04382	0.07025	0.11407	60.07	0.1153	1.5135	92
93	3.441	13.929	0.768	14.697	22.346	37.90	60.25	0.04426	0.07249	0.11675	61.07	0.1171	1.5612	93
94	3.556	13.954	0.795	14.749	22.587	39.18	61.77	0.01469	0.07480	0.11949	62.07	0.1188	1.6102	94
95	3.673	13.980	0.822	14.802	22.827	40.49	63.32	0.04513	0.07718	0.12231	63.07	0.1206	1.6606	95
96	3.795	14.005	0.851	14.856	23.068	41.85	64.92	0.04556	0.07963	0.12519	64.06	0.1224	1.7123	96
97	3.920	14.030	0.881	14.911	23.308	43.24	66.55	0.04600	0.08215	0.12815	65.06	0.1242	1.7654	97
98	4.049	14.056	0.911	14.967	23.548	44.68	68.23	0.04643	0.08474	0.13117	66.06	0.1260	1.8199	98
99	4.182	14.081	0.942	15.023	23.789	46.17	69.96	0.04686	0.08741	0.13427	67.06	0.1278	1.8759	99
100	4.319	14.106	0.975	15.081	24.029	47.70	71.73	0.04729	0.09016	0.13745	68.06	0.1296	1.9333	100
101	4.460	14.131	1.009	15.140	24.270	49.28	73.55	0.04772	0.09299	0.14071	69.05	0.1314	1.9923	101
102	4.606	14.157	1.043	15.200	24.510	50.91	75.42	0.04815	0.09591	0.14406	70.05	0.1332	2.0528	102
103	4.756	14.182	1.079	15.261	24.751	52.59	77.34	0.04858	0.09891	0.14749	71.05	0.1350	2.1149	103
104	4.911	14.207	1.117	15.324	24.991	54.32	79.31	0.04900	0.1020	0.1510	72.05	0.1367	2.1786	104

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO W_s x 10	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap Press In. Hg p_s	
105	0.5070	14.232	1.155	15.387	25.232	56.11	81.34	0.04943	0.1052	0.1546	73.04	0.1385	2.2439	105
106	0.5234	14.258	1.194	15.452	25.472	57.95	83.42	0.04985	0.1085	0.1584	74.04	0.1403	2.3109	106
107	0.5404	14.283	1.235	15.518	25.713	59.85	85.56	0 05028	0.1118	0.1621	75.04	0.1421	2.3797	107
108	0.5578	14.308	1.278	15.586	25.953	61.80	87.76	0.05070	0.1153	0.1660	76.04	0.1438	2.4502	108
109	0.5758	14.333	1.321	15.654	26.194	63.82	90.03	0.05113	0.1189	0.1700	77.04	0.1456	2.5225	109
110	0.5944	14.359	1.365	15.724	26.434	65.91	92.34	0.05155	0.1226	0.1742	78.03	0.1472	2.5966	110
111	0.6135	14.384	1.412	15.796	26.675	68.05	94.72	0.05197	0 1264	0.1784	79.03	0.1491	2.6726	111
112	0.6333	14.409	1.460	15.869	26.915	70.27	97 18	0.05239	0.1302	0.1826	80.03	0.1508	2.7505	112
113	0.6536	14.435	1.509	15.944	27.156	72.55	99.71	0.05281	0.1342	0.1870	81.03	0.1525	2.8304	113
114	0.6746	14.460	1.560	16.020	27.397	74.91	102.31	0.05323	0.1384	0.1916	82.03	0.1543	2.9123	114
115	0.6962	14.485	1.613	16.098	27.637	77.34	104.98	0.05365	0.1426	0.1963	83.02	0.1560	2.9962	115
116	0.7185	14.510	1.668	16.178	27.878	79.85	107.73	0.05407	0.1470	0.2011	84.02	0.1577	3.0821	116
117	0.7415	14.536	1.723	16.259	28.119	82.43	110.55	0.05449	0.1515	0.2060	85.02	0.1595	3.1701	117
118	0.7652	14.561	1.782	16.343	28.359	85.10	113.46	0.05490	0.1562	0.2111	86.02	0.1612	3.2603	118
119	0.7897	14.586	1.842	16.428	28.600	87.86	116.46	0.05532	0.1610	0.2163	87.02	0.1629	3.3527	119
120	0.8149	14.611	1.905	16.516	28.841	90.70	119.54	0.05573	0.1659	0.2216	88.01	0.1646	3.4474	120
121	0.8410	14.637	1.968	16.605	29.082	93.64	122.72	0.05615	0.1710	0.2272	89.01	0.1664	3.5443	121
122	0.8678	14.662	2.034	16.696	29.322	96.66	125.98	0.05656	0.1763	0.2329	90.01	0.1681	3.6436	122
123	0.8955	14.687	2.103	16.790	29.563	99.79	129.35	0.05698	0.1817	0.2387	91.01	0.1698	3.7452	123
124	0.9242	14.712	2.174	16.886	29.804	103.0	132.8	0.05739	0.1872	0.2446	92.01	0.1715	3.8493	124
125	0.9537	14.738	2.247	16.985	30.044	106.4	136.4	0 05780	0.1930	0.2508	93.01	0.1732	3.9558	125
126	0.9841	14.763	2.323	17.086	30.285	109.8	140.1	0.05821	0.1989	0.2571	94.01	0.1749	4.0649	126
127	1.016	14.788	2.401	17.189	30.526	113.4	143.9	0.05862	0.2050	0 2636	95.00	0.1766	4.1765	127
128	1.048	14.813	2.482	17.295	30.766	117.0	147.8	0.05903	0.2113	0 2703	96.00	0.1783	4.2907	128
129	1.082	14.839	2.565	17.404	31.007	120.8	151.8	0.05944	0.2178	0.2772	97.00	0.1800	4.4076	129
130	1 116	14.864	2.652	17.516	31.248	124.7	155.9	0.05985	0.2245	0 2844	98.00	0.1817	4.5272	130
131	1.152	14.889	2.742	17.631	31.489	128.8	160.3	0.06026	0.2314	0.2917	99.00	0.1834	4.6495	131
132	1.189	14.915	2.834	17.749	31.729	133.0	164.7	0.06067	0.2386	0.2993	100.00	0 1851	4.7747	132
133	1.227	14.940	2.930	17.870	31.970	137.3	169.3	0.06108	0.2459	0.3070	101.00	0.1868	4.9028	133
134	1.267	14.965	3.029	17.994	32.211	141.8	174.0	0.06148	0.2536	0.3151	102.00	0.1885	5.0337	134
135	1.308	14 990	3.132	18.122	32.452	146.4	178 9	0 06189	0.2614	0.3233	103.00	0.1902	5.1676	135
136	1.350	15 016	3.237	18.253	32.692	151.2	183.9	0 06229	0.2695	0.3318	104.00	0.1918	5.3046	136
137	1.393	15.041	3.348	18.389	32.933	156.1	189.0	0 06270	0 2778	0.3405	105.00	0.1935	5.4446	137
138	1.439	15.066	3.462	18.528	33.174	161.2	194.4	0 06310	0.2865	0.3496	106 00	0.1952	5.5878	138
139	1.485	15.091	3.580	18.671	33.414	166.5	199.9	0.06350	0.2954	0.3589	107.00	0.1969	5.7342	139

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Continued)

FAHR. TEMP. t(F)	HUMIDITY RATIO W_s	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg p_s	
140	0.1534	15.117	3.702	18 819	33.655	172 0	205.7	0 06390	0 3047	0.3686	107 99	0.1985	5.8838	140
141	0.1584	15.142	3.829	18.971	33.896	177.7	211.6	0.06430	0.3142	0.3785	108.99	0.2002	6.0367	141
142	0.1636	15.167	3.961	19 128	34.136	183.6	217 7	0 06470	0.3241	0.3888	109.99	0.2018	6.1930	142
143	0.1689	15.192	4.098	19.290	34.377	189.7	224.1	0.06510	0.3343	0.3994	110.99	0.2035	6 3527	143
144	0.1745	15.218	4.239	19.457	34.618	196.0	230.6	0.06549	0.3449	0.4104	111.99	0.2051	6.5160	144
145	0.1803	15.243	4.386	19.629	34.859	202.5	237 4	0 06589	0.3559	0 4218	112.99	0.2068	6.6828	145
146	0.1862	15.268	4.539	19.807	35.099	209.3	244.4	0.06629	0.3672	0.4335	113.99	0.2084	6.8532	146
147	0.1924	15.293	4.698	19.991	35.340	216.4	251.7	0.06669	0.3790	0.4457	114 99	0.2101	7.0273	147
148	0.1989	15.319	4 862	20.181	35.581	223.7	259.3	0.06708	0.3912	0.4583	115.99	0.2117	7.2051	148
149	0.2055	15.344	5.033	20.377	35.822	231.3	267.1	0.06748	0.4038	0.4713	116.99	0.2134	7.3867	149
150	0.2125	15.369	5.211	20.580	36.063	239.2	275.3	0.06787	0.4169	0.4848	117 99	0.2150	7.5722	150
151	0 2197	15.394	5.396	20.790	36.304	247.3	283.6	0.06827	0.4304	0.1987	118.99	0.2167	7.7616	151
152	0.2271	15.420	5.587	21.007	36.545	255.9	292.4	0 06866	0.4445	0.5132	119.99	0.2183	7.9550	152
153	0.2349	15.445	5.788	21.233	36 785	264.7	301.5	0 06906	0.4591	0.5282	120.99	0.2200	8.1525	153
154	0.2430	15.470	5.996	21.466	37.026	273.9	310.9	0.06945	0.4743	0.5438	121.99	0.2216	8.3541	154
155	0 2514	15.496	6.213	21.709	37.267	283.5	320.8	0.06984	0.4901	0.5599	122.99	0.2232	8.5599	155
156	0.2602	15.521	6.439	21.960	37.508	293.5	331.0	0.07023	0.5066	0.5768	123.99	0.2248	8.7701	156
157	0.2693	15.546	6.675	22.221	37.749	303.9	341.7	0.07062	0.5237	0.5943	124.99	0 2265	8.9846	157
158	0.2788	15.571	6.922	22.493	37.990	314.7	352.7	0.07101	0 5415	0 6125	125.99	0 2281	9 2036	158
159	0.2887	15.597	7.178	22.775	38.231	326.0	364.2	0.07140	0.5600	0.6314	127.00	0.2297	9.4271	159
160	0.2990	15.622	7.446	23.068	38.472	337.8	376.3	0.07179	0.5793	0.6511	128.00	0.2313	9.6556	160
161	0 3098	15.647	7.727	23.374	38.713	350.1	388.8	0.07218	0.5994	0.6716	129.00	0.2329	9.8876	161
162	0.3211	15 672	8.020	23.692	38.954	363.0	402.0	0.07257	0.6204	0.6930	130.00	0.2345	10.125	162
163	0.3329	15.698	8.326	24.024	39.195	376.5	415.7	0.07296	0.6423	0.7153	131 00	0.2361	10.367	163
164	0.3452	15.723	8.648	24.371	39.436	390.5	429.9	0 07334	0.6652	0.7385	132.00	0.2377	10.614	164
165	0.3581	15.748	8.985	24.733	39.677	405.3	445.0	0.07373	0.6892	0.7629	133 00	0.2393	10.866	165
166	0.3716	15.773	9.339	25.112	39.918	420.8	460.7	0.07411	0.7142	0.7883	134.00	0.2409	11.123	166
167	0.3858	15.799	9 708	25.507	40 159	437.0	447 2	0.07450	0 7405	0.8150	135.01	0.2426	11.385	167
168	0.4007	15.824	10.098	25 922	40.400	454.0	494.4	0.07488	0.7680	0 8429	136.01	0.2441	11.652	168
169	0.4163	15.849	10.508	26.357	40.641	471.8	512.4	0.07527	0.7969	0.8722	137.01	0.2457	11.925	169
170	0.4327	15.874	10.938	26.812	40.882	490.6	531.5	0.07565	0.8273	0.9030	138.01	0.2473	12.203	170
171	0.4500	15.900	11.391	27.291	41.123	510.4	551.5	0.07603	0.8592	0.9352	139.01	0 2489	12.486	171
172	0.4682	15.925	11.870	27.795	41.364	531.3	572.7	0.07641	0 8927	0.9691	140.01	0.2505	12.775	172
173	0.4875	15.950	12.376	28.326	41.605	553.3	594 9	0.07680	0.9281	1.0049	141.01	0.2521	13.069	173
174	0.5078	15.975	12.911	28.886	41.846	576.5	618.3	0.07718	0.9654	1.0426	142.02	0.2537	13.369	174

[a]Compiled by John A. Goff and S. Gratch.

TABLE 1. THERMODYNAMIC PROPERTIES OF MOIST AIR[a] (STANDARD ATMOSPHERIC PRESSURE, 29.921 IN. HG) (Concluded)

FAHR. TEMP. t(F)	HUMIDITY RATIO W_s	VOLUME CU FT/LB DRY AIR			ENTHALPY BTU/LB DRY AIR			ENTROPY BTU PER (°F) (LB DRY AIR)			CONDENSED WATER			FAHR. TEMP. t(F)
		v_a	v_{as}	v_s	h_a	h_{as}	h_s	s_a	s_{as}	s_s	Enthalpy Btu/Lb h_w	Entropy Btu/(Lb) (°F) s_w	Vap. Press In. Hg p_s	
175	0.5292	16.001	13.475	29.476	42.087	601.1	643.2	0.07756	1.005	1.083	113.02	0.2553	13.675	175
176	0.5519	16.026	14.074	30.100	42.328	627.1	66.94	0.07794	1.047	1.125	144.02	0.2568	13.987	176
177	0.5760	16.051	14.710	30.761	42.569	654.7	697.3	0.07832	1.091	1.169	145.02	0.2584	14.304	177
178	0.6016	16.076	15.386	31.462	42.810	684.1	726.9	0.07870	1.137	1.216	146.03	0.2600	14.628	178
179	0.6288	16.102	16.104	32.206	43.051	715.2	758.3	0.07908	1.187	1.266	147.03	0.2616	14.958	179
180	0.6578	16.127	16.870	32.997	43.292	748.5	791.8	0.07946	1.240	1.319	148.03	0.2631	15.294	180
181	0.6887	16.152	17.689	33.841	43.534	783.9	827.4	0.07984	1.296	1.376	149.03	0.2647	15.636	181
182	0.7218	16.177	18.565	34.742	43 775	821.9	865.7	0.08021	1.357	1.437	150.04	0.2662	15.985	182
183	0.7572	16.203	19.504	35.707	44.016	862.5	906.5	0.08059	1.421	1 502	151.04	0.2678	16.340	183
184	0.7953	16.228	20.513	36.741	44.257	906.2	950.5	0.08096	1.490	1.571	152.04	0.2693	16.702	184
185	0.8363	16.253	21.601	37.854	44.498	953.2	997.7	0.08134	1.565	1.646	153.05	0.2709	17.071	185
186	0.8805	16.278	22.775	39.053	44.740	1004	1049	0.08171	1.645	1.727	154.05	0.2724	17.446	186
187	0.9283	16.304	24.047	40.351	44.981	1059	1104	0.08208	1.731	1.813	155.05	0.2740	17.828	187
188	0.9802	16.329	25.427	41.756	45.222	1119	1164	0.08245	1.825	1.907	156 06	0.2755	18.217	188
189	1.037	16.354	26.934	43.288	45.463	1184	1229	0.08283	1.928	2.011	157.06	0.2771	18.614	189
190	1.099	16.379	28.580	44.959	45.704	1255	1301	0.08320	2.039	2.122	158.07	0.2786	19.017	190
191	1.166	16.405	30.385	46.790	45.946	1332	1378	0.08357	2.161	2.215	159 07	0.2802	19.427	191
192	1.241	16.430	32.375	48.805	46.187	1418	1464	0.08394	2.296	2.380	160.07	0.2817	19.845	192
193	1.324	16.455	34.581	51.036	46.428	1513	1559	0.08431	2.444	2.528	161.08	0.2833	20.271	193
194	1.416	16.480	37.036	53.516	46.670	1619	1666	0.08468	2.609	2 694	162.08	0.2848	20.704	194
195	1.519	16.506	39.785	56.291	46.911	1737	1784	0.08505	2.794	2.879	163 09	0 2864	21.145	195
196	1.635	16.531	42.885	59.416	47.153	1871	1918	0.08542	3.002	3.087	164 09	0 2879	21.594	196
197	1.767	16.556	46.402	62.958	47.394	2022	2069	0.08579	3.238	3.324	165 10	0.2895	22.050	197
198	1.917	16.581	50.426	67 007	47.636	2195	2243	0.08616	3.507	3.593	166.10	0.2910	22.514	198
199	2.091	16.607	55.074	71.681	47.877	2395	2443	0.08653	3.817	3.904	167 11	0.2925	22.987	199
200	2.295	16.632	60.510	77 142	48.119	2629	2677	0 08689	4.179	4.266	168 11	0 2940	23.468	200

[a]Compiled by John A. Goff and S. Gratch.

given temperature (below the critical temperature), though this requires that it have a definite pressure p_s and that the coexisting condensed phase have the same temperature and pressure. The values of saturation pressure listed in Table 1 have been computed from the formulae of Goff and Gratch [2].

Thermodynamic Properties of Water at Saturation

Table 2 offers revisions to existing steam table data [3] with extension downward to −160 F. These revisions and extension were a necessary preliminary to the construction of Table 1. A detailed explanation of the methods employed in constructing Table 2 is given in a paper [2] by John A. Goff and S. Gratch. As in Table 1 the temperature scale used as argument in Table 2 is the Fahrenheit scale defined in terms of absolute temperature T by Equation 1, whereas the Fahrenheit scale used as argument in existing steam tables is that derived from the International Centigrade scale by means of Equation 2. The symbols used as column headings in Table 2 are the same as those used in the steam tables and have the same meanings; therefore, a detailed explanation seems unnecessary.

Properties of water above 212 F from Keenan and Keyes [3] are given in Table 3.

DEGREE OF SATURATION

At given values of temperature and pressure the humidity ratio W of moist air can have any value between zero (dry air) and W_s (moist air at saturation). For convenience a parameter μ called alternatively *degree of saturation* or *per cent saturation* is introduced through the definition,

$$W = \mu W_s \tag{3}$$

Obviously the degree of saturation μ can have any value from zero (dry air) to unity (moist air at saturation).

To a degree of approximation within the estimated uncertainty of the data in Table 1 at temperatures below about 150 F, the volume v of moist air per pound of dry air at any degree of saturation μ may be computed from the simple relation,

$$v = v_a + \mu v_{as} \tag{4}$$

To obtain comparable accuracy at temperatures above about 150 F it is necessary to add a correction term $\bar{v}$ as follows,

$$\bar{v} = \frac{\mu(1 - \mu)A}{1 + aW_s\mu} \tag{4a}$$

where a denotes the ratio of the apparent molecular weight of dry air (28.966) to the molecular weight of water (18.016), namely, 1.6078. In Table 4 are given, for each of several higher temperatures, the corresponding value of the coefficient A, the value of μ at which the correction term $\bar{v}$ attains its maximum value, and the maximum value of the correction term there attained.

At temperatures below about 150 F the enthalpy h of moist air per pound of dry air at any degree of saturation μ may be computed from the simple relation,

$$h = h_a + \mu h_{as} \tag{5}$$

To obtain comparable accuracy at temperatures above about 150 F it is

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a]

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE $p_s \times 10^3$		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Solid v_i	Evap. $v_{ig} \times 10^{-3}$	Sat. Vapor $v_g \times 10^{-3}$	Sat. Solid h_i	Evap. h_{ig}	Sat. Vapor h_g	Sat. Solid s_i	Evap. s_{ig}	Sat. Vapor s_g	
−160	0.4949	1.008	0.01722	36.07	36.07	−222.05	1212.43	990.38	−0.4907	4.0456	3.5549	−160
−159	0.5592	1.138	0 01722	32.03	32.03	−221.73	1212.55	990.82	−0.4896	4.0325	3.5429	−159
−158	0.6312	1.285	0.01723	28.47	28.47	−221.41	1212.67	991.26	−0.4886	4.0196	3.5310	−158
−157	0.7121	1.450	0 01723	25.32	25.32	−221.09	1212.79	991.70	−0.4875	4.0067	3.5192	−157
−156	0.8026	1.634	0.01723	22.54	22.54	−220.76	1212.90	992.14	−0.4864	3.9939	3.5075	−156
−155	0.9040	1.840	0.01723	20 08	20.08	−220.44	1213.02	992.58	−0.4854	3.9812	3.4958	−155
−154	1.017	2.072	0 01723	17 90	17.90	−220.12	1213.15	993 03	−0.4843	3.9685	3.4842	−154
−153	1.144	2.329	0.01723	15.97	15.97	−219.79	1213.26	993.47	−0.4832	3.9559	3.4727	−153
−152	1.286	2.618	0.01723	14.26	14.26	−219.47	1213.38	993.91	−0.4822	3.9435	3.4613	−152
−151	1.444	2.939	0.01723	12.74	12.74	−219.14	1213.49	994.35	−0.4811	3.9311	3.4500	−151
−150	1.620	3.298	0.01723	11.39	11.39	−218.82	1213.62	994.80	−0.4801	3.9188	3.4387	−150
−149	1.816	3.698	0.01723	10.19	10.19	−218.49	1213.73	995.24	−0.4790	3.9065	3.4275	−149
−148	2.035	4.143	0.01724	9.123	9.123	−218.16	1213 84	995 68	−0.4780	3.8944	3.4164	−148
−147	2.278	4.639	0.01724	8.174	8.174	−217.83	1213.95	996.12	−0.4769	3.8823	3.4054	−147
−146	2.549	5.190	0.01724	7.330	7.330	−217.50	1214.06	996.56	−0.4758	3.8702	3.3944	−146
−145	2.850	5.803	0 01724	6.577	6.577	−217.17	1214.17	997.00	−0.4748	3.8583	3.3835	−145
−144	3.184	6.483	0.01724	5.905	5.905	−216.83	1214.28	997.45	−0.4737	3.8464	3.3727	−144
−143	3.556	7.240	0 01724	5.305	5.305	−216.50	1214.39	997 89	−0.4727	3.8346	3.3619	−143
−142	3.967	8.076	0.01724	4.770	4.770	−216.16	1214.49	998 33	−0.4716	3.8229	3.3513	−142
−141	4.423	9.005	0.01724	4.292	4.292	−215.83	1214.60	998.77	−0.4706	3.8112	3.3406	−141
−140	4.928	10 03	0.01724	3.864	3.864	−215.49	1214 70	999.21	−0.4695	3.7996	3.3301	−140
−139	5.487	11.17	0.01724	3.481	3.481	−215.16	1214 82	999.66	−0.4685	3.7881	3.3196	−139
−138	6.106	12.43	0.01724	3 138	3.138	−214.82	1214.92	1000.10	−0.4674	3.7766	3.3092	−138
−137	6.790	13.82	0.01724	2.831	2.831	−214.48	1215.02	1000.54	−0.4664	3.7653	3.2989	−137
−136	7.546	15.36	0.01725	2.555	2.555	−214.14	1215 12	1000 98	−0.4653	3 7540	3.2887	−136
−135	8.380	17.06	0.01725	2.308	2.308	−213 80	1215.22	1001 42	−0.4643	3 7428	3.2785	−135
−134	9.301	18 94	0 01725	2.086	2.086	−213.46	1215.32	1001.86	−0.4632	3.7315	3.2683	−134
−133	10.32	21.01	0.01725	1.886	1.886	−213.11	1215.42	1002.31	−0.4622	3.7205	3.2583	−133
−132	11.44	23.28	0.01725	1.707	1.707	−212.77	1215.52	1002.75	−0.4611	3.7093	3.2482	−132
−131	12.67	25.79	0.01725	1 545	1.545	−212.43	1215.62	1003.19	−0.4601	3.6984	3.2383	−131
−130	14.03	28.56	0.01725	1.400	1.400	−212 08	1215.71	1003 63	−0.4590	3.6874	3.2284	−130
−129	15.52	31.60	0.01725	1.269	1.269	−211.73	1215 80	1004.07	−0.4580	3.6766	3.2186	−129

[a]Compiled by John A. Goff and S. Gratch.

Table 2. Thermodynamic Properties of Water at Saturation[a] (Continued)

Fahr. Temp. t(F)	Absolute Pressure $p_s \times 10^6$		Specific Volume, cu ft per lb			Enthalpy, Btu per lb			Entropy, Btu per (Lb) (°F)			Fahr. Temp. t(F)
	Lb/Sq In.	In. Hg	Sat. Solid v_i	Evap. $v_{ig} \times 10^{-7}$	Sat. Vapor $v_g \times 10^{-7}$	Sat. Solid h_i	Evap. h_{ig}	Sat. Vapor h_g	Sat. Solid s_i	Evap. s_{ig}	Sat. Vapor s_g	
−128	1.716	3.494	0.01726	11.51	11.51	−211.39	1215 91	1004.52	−0.4569	3.6658	3.2089	−128
−127	1.897	3.862	0.01726	10.45	10.45	−211.04	1216.00	1004.96	−0.4559	3.6551	3.1992	−127
−126	2.095	4.265	0.01726	9.489	9.489	−210.69	1216 09	1005.40	−0.4548	3.6444	3.1896	−126
−125	2.312	4.708	0.01726	8.622	8.622	−210.34	1216.18	1005.84	−0.4538	3.6338	3.1800	−125
−124	2.551	5.194	0.01726	7.839	7.839	−209 99	1216.27	1006.28	−0.4527	3.6232	3.1705	−124
−123	2.812	5.726	0.01726	7.131	7.131	−209.64	1216.37	1006 73	−0.4517	3.6127	3.1610	−123
−122	3.099	6.310	0.01726	6.491	6.491	−209.28	1216 45	1007 17	−0.4506	3.6022	3.1516	−122
−121	3.413	6.949	0.01726	5.911	5.911	−208.93	1216.54	1007.61	−0.4496	3.5919	3.1423	−121
−120	3.757	7.649	0.01726	5.386	5.386	−208.58	1216.63	1008 05	−0.4485	3.5815	3 1330	−120
−119	4.133	8.414	0.01726	4.911	4.911	−208.22	1216 71	1008.49	−0.4475	3.5713	3.1238	−119
−118	4.544	9.251	0.01727	4.480	4.480	−207.86	1216 80	1008 94	−0.4464	3.5611	3.1147	−118
−117	4.993	10.17	0.01727	4.088	4.088	−207.51	1216.89	1009.38	−0.4454	3.5510	3.1056	−117
−116	5.484	11.16	0.01727	3.733	3.733	−207.15	1216.97	1009.82	−0.4444	3.5409	3.0965	−116
−115	6.019	12.26	0.01727	3.411	3.411	−206.79	1217.05	1010.26	−0.4433	3.5308	3.0875	−115
−114	6.604	13.44	0.01727	3.118	3.118	−206.43	1217.13	1010.70	−0.4423	3.5209	3.0786	−114
−113	7.241	14.74	0.01727	2.852	2.852	−206.07	1217.21	1011.14	−0.4412	3.5109	3.0697	−113
−112	7.936	16.16	0 01727	2.610	2 610	−205 70	1217.29	1011.59	−0.4402	3.5011	3.0609	−112
−111	8 693	17.70	0 01727	2.389	2.389	−205.34	1217.37	1012.03	−0.4391	3.4912	3.0521	−111
−110	9.517	19.38	0.01728	2.189	2.189	−204.98	1217.45	1012.47	−0.4381	3.4815	3.0434	−110
−109	10.41	21.20	0.01728	2.006	2.006	−204 61	1217.52	1012.91	−0.4370	3.4718	3.0348	−109
−108	11.39	23.19	0 01728	1.839	1 839	−204.24	1217.60	1013.36	−0.4360	3.4621	3.0261	−108
−107	12.45	25.35	0.01728	1.687	1.687	−203.88	1217.68	1013.80	−0.4350	3.4526	3.0176	−107
−106	13.60	27.70	0.01728	1.549	1.549	−203.51	1217.75	1014.24	−0.4339	3.4430	3.0091	−106
−105	14.86	30.25	0.01728	1.422	1.422	−203.14	1217.82	1014.68	−0.4329	3.4335	3.0006	−105
−104	16.22	33.01	0 01728	1.307	1.307	−202.77	1217.89	1015.12	−0.4318	3.4240	2.9922	−104
−103	17.69	36.02	0.01728	1.201	1.201	−202.40	1217.96	1015.56	−0.4308	3.4146	2.9838	−103
−102	19.29	39.28	0.01728	1.104	1.104	−202.03	1218.04	1016.01	−0.4298	3.4053	2.9755	−102
−101	21.03	42.81	0.01729	1.016	1.016	−201.65	1218.10	1016.45	−0.4287	3.3960	2.9673	−101
−100	22.91	46.64	0.01729	0.9352	0.9352	−201.28	1218.17	1016.89	−0.4277	3.3868	2.9591	−100
−99	24.94	50 79	0.01729	0.8613	0 8613	−200.90	1218.23	1017 33	−0.4266	3.3775	2.9509	−99
−98	27.15	55.28	0.01729	0.7936	0.7936	−200.53	1218.30	1017.77	−0 4256	3.3684	2.9428	−98
−97	29.54	60.14	0.01729	0.7314	0.7314	−200.15	1218.37	1018.22	−0.4246	3.3593	2.9347	−97

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE $p_s \times 10^5$		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Solid v_i	Evap. $v_{ig} \times 10^{-6}$	Sat. Vapor $v_g \times 10^{-6}$	Sat. Solid h_i	Evap. h_{ig}	Sat. Vapor h_g	Sat. Solid s_i	Evap. s_{ig}	Sat. Vapor s_g	
−96	3.212	6.539	0.01729	6.745	6.745	−199.78	1218 44	1018.66	−0.4235	3.3502	2 9267	−96
−95	3.491	7.108	0.01729	6.223	6.223	−199.40	1218.50	1019 10	−0.4225	3.3412	2.9187	−95
−94	3.793	7.722	0.01729	5.743	5.743	−199.02	1218.56	1019.54	−0.4214	3.3322	2.9108	−94
−93	4.118	8.385	0.01730	5.303	5.303	−198.64	1218.62	1019.98	−0.4204	3.3233	2.9029	−93
−92	4.470	9.102	0 01730	4.899	4.899	−198.25	1218.68	1020 43	−0.4194	3.3145	2.8951	−92
−91	4.850	9.876	0.01730	4.528	4.528	−197.87	1218 74	1020 87	−0.4183	3.3056	2.8873	−91
−90	5.260	10.71	0.01730	4.186	4.186	−197 49	1218.80	1021.31	−0 4173	3.2969	2.8796	−90
−89	5.702	11 61	0.01730	3.872	3.872	−197.10	1218.85	1021.75	−0 4162	3.2880	2.8718	−89
−88	6.179	12.58	0.01730	3.583	3.583	−196.72	1218.92	1022.20	−0.4152	3.2794	2.8642	−88
−87	6.692	13.63	0.01730	3.317	3 317	−196.33	1218 97	1022.64	−0.4142	3.2708	2.8566	−87
−86	7.245	14.75	0.01730	3.072	3.072	−195.94	1219 02	1023 08	−0.4131	3.2621	2.8490	−86
−85	7.841	15.96	0.01730	2.846	2.846	−195.56	1219.08	1023.52	−0.4121	3.2536	2 8415	−85
−84	8.482	17.27	0 01731	2.638	2.638	−195.16	1219.12	1023.96	−0.4110	3.2450	2.8340	−84
−83	9.171	18.67	0.01731	2.446	2 446	−194.78	1219.18	1024 40	−0.4100	3.2366	2.8266	−83
−82	9 913	20.18	0.01731	2.270	2.270	−194.38	1219.23	1024.85	−0 4090	3 2282	2.8192	−82
−81	10.71	21.81	0.01731	2.106	2.106	−193.99	1219.28	1025.29	−0.4079	3 2197	2.8118	−81
−80	11.57	23.55	0.01731	1.955	1 955	−193.60	1219.33	1025.73	−0.4069	3.2114	2.8045	−80
−79	12.49	25.42	0.01731	1 816	1.816	−193 20	1219.37	1026.17	−0.4058	3.2030	2.7972	−79
−78	13.47	27.43	0 01731	1.687	1.687	−192.81	1219.43	1026.62	−0.4048	3.1948	2.7900	−78
−77	14.53	29.59	0.01732	1 568	1.568	−192.41	1219.47	1027.06	−0.4038	3.1866	2.7828	−77
−76	15.67	31.91	0.01732	1.458	1.458	−192.01	1219.51	1027.50	−0.4028	3.1784	2.7756	−76
−75	16.89	34.39	0.01732	1.356	1.356	−191.62	1219.56	1027.94	−0.4017	3.1702	2.7685	−75
−74	18.20	37 05	0.01732	1.262	1.262	−191 22	1219.60	1028.38	−0.4007	3.1622	2.7615	−74
−73	19.60	39.91	0.01732	1.175	1 175	−190.82	1219.65	1028 83	−0.3996	3.1540	2.7544	−73
−72	21.10	42.96	0.01732	1.094	1.094	−190 41	1219.68	1029.27	−0 3986	3.1460	2 7474	−72
−71	22.71	46.24	0.01732	1.020	1.020	−190.01	1219.72	1029.71	−0.3976	3 1381	2.7405	−71
−70	24.43	49.74	0.01732	0.9501	0.9501	−189.61	1219.76	1030.15	−0.3965	3.1301	2.7336	−70
−69	26.27	53.49	0.01732	0.8858	0.8858	−189.20	1219.80	1030.60	−0.3955	3.1222	2.7267	−69
−68	28 24	57.51	0.01733	0.8261	0.8261	−188.80	1219.84	1031.04	−0.3945	3 1143	2.7198	−68
−67	30.35	61.80	0.01733	0.7707	0.7707	−188.39	1219.87	1031.48	−0.3934	3.1064	2.7130	−67
−66	32.60	66.38	0.01733	0.7193	0.7193	−187 98	1219 90	1031.92	−0 3924	3.0987	2.7063	−66
−65	35.01	71.28	0.01733	0.6715	0.6715	−187 58	1219.94	1032.36	−0.3914	3.0910	2.6996	−65

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE $p_s \times 10^3$		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Solid v_i	Evap. $v_{ig} \times 10^{-5}$	Sat. Vapor $v_g \times 10^{-5}$	Sat. Solid h_i	Evap. h_{ig}	Sat. Vapor h_g	Sat. Solid s_i	Evap. s_{ig}	Sat. Vapor s_g	
−64	0.3758	0.7652	0.01733	6.272	6.272	−187.17	1219.98	1032.81	−0.3903	3.0832	2.6929	−64
−63	0.4033	0.8211	0.01733	5.859	5.859	−186.76	1220.01	1033.25	−0.3893	3.0755	2.6862	−63
−62	0.4326	0.8808	0.01734	5.476	5.476	−186.35	1220.04	1033.69	−0.3882	3.0678	2.6796	−62
−61	0.4639	0.9444	0.01734	5.120	5.120	−185.93	1220.06	1034.13	−0.3872	3.0602	2.6730	−61
−60	0.4972	1.012	0.01734	4.788	4.788	−185.52	1220.10	1034.58	−0.3862	3.0526	2.6664	−60
−59	0.5328	1.085	0.01734	4.479	4.479	−185.11	1220.13	1035.02	−0.3851	3.0450	2.6599	−59
−58	0.5708	1.162	0.01734	4.192	4.192	−184.69	1220.15	1035.46	−0.3841	3.0376	2.6535	−58
−57	0.6112	1.244	0.01734	3.925	3.925	−184.28	1220.18	1035.90	−0.3831	3.0301	2.6470	−57
−56	0.6543	1.332	0.01734	3.675	3.675	−183.86	1220.20	1036.34	−0.3820	3.0226	2.6406	−56
−55	0.7001	1.426	0.01734	3.443	3.443	−183.44	1220.23	1036.79	−0.3810	3.0152	2.6342	−55
−54	0.7489	1.525	0.01735	3.226	3.226	−183.02	1220.25	1037.23	−0.3800	3.0079	2.6279	−54
−53	0.8009	1.631	0.01735	3.024	3.024	−182.60	1220.27	1037.67	−0.3789	3.0005	2.6216	−53
−52	0.8562	1.743	0.01735	2.836	2.836	−182.18	1220.29	1038.11	−0.3779	2.9932	2.6153	−52
−51	0.9151	1.863	0.01735	2.660	2.660	−181.76	1220.31	1038.55	−0.3769	2.9860	2.6091	−51
−50	0.9776	1.990	0.01735	2.496	2.496	−181.34	1220.34	1039.00	−0.3758	2.9786	2.6028	−50
−49	1.044	2.126	0.01735	2.343	2.343	−180.92	1220.36	1039.44	−0.3748	2.9715	2.5967	−49
−48	1.115	2.270	0.01736	2.200	2.200	−180.49	1220.37	1039.88	−0.3738	2.9643	2.5905	−48
−47	1.190	2.422	0.01736	2.066	2.066	−180.06	1220.38	1040.32	−0.3727	2.9571	2.5844	−47
−46	1.270	2.585	0.01736	1.941	1.941	−179.64	1220.40	1040.76	−0.3717	2.9501	2.5784	−46
−45	1.354	2.757	0.01736	1.824	1.824	−179.21	1220.42	1041.21	−0.3707	2.9430	2.5723	−45
−44	1.444	2.940	0.01736	1.715	1.715	−178.78	1220.43	1041.65	−0.3696	2.9359	2.5663	−44
−43	1.539	3.134	0.01736	1.612	1.612	−178.35	1220.44	1042.09	−0.3686	2.9289	2.5603	−43
−42	1.641	3.340	0.01736	1.516	1.516	−177.92	1220.45	1042.53	−0.3676	2.9219	2.5543	−42
−41	1.748	3.559	0.01736	1.427	1.427	−177.49	1220.47	1042.98	−0.3665	2.9149	2.5484	−41
−40	1.861	3.790	0.01737	1.343	1.343	−177.06	1220.48	1043.42	−0.3655	2.9080	2.5425	−40
−39	1.982	4.035	0.01737	1.264	1.264	−176.63	1220.49	1043.86	−0.3645	2.9012	2.5367	−39
−38	2.110	4.295	0.01737	1.191	1.191	−176.19	1220.49	1044.30	−0.3634	2.8942	2.5308	−38
−37	2.245	4.570	0.01737	1.122	1.122	−175.76	1220.50	1044.74	−0.3624	2.8874	2.5250	−37
−36	2.388	4.862	0.01737	1.057	1.057	−175.32	1220.51	1045.19	−0.3614	2.8807	2.5193	−36
−35	2.540	5.170	0.01737	0.9961	0.9961	−174.88	1220.51	1045.63	−0.3604	2.8739	2.5135	−35
−34	2.700	5.497	0.01737	0.9391	0.9391	−174.45	1220.52	1046.07	−0.3593	2.8671	2.5078	−34
−33	2.870	5.843	0.01738	0.8857	0.8857	−174.01	1220.52	1046.51	−0.3583	2.8604	2.5021	−33

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE $p_s \times 10^3$		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Solid v_i	Evap. $v_{ig} \times 10^{-4}$	Sat. Vapor $v_g \times 10^{-4}$	Sat. Solid h_i	Evap. h_{ig}	Sat. Vapor h_g	Sat. Solid s_i	Evap. s_{ig}	Sat. Vapor s_g	
−32	0.3049	0.6208	0.01738	8.355	8.355	−173.57	1220.52	1046.95	−0.3573	2.8538	2.4965	−32
−31	0.3239	0.6595	0.01738	7.883	7.883	−173.13	1220 53	1047.40	−0.3562	2.8470	2.4908	−31
−30	0.3440	0.7003	0.01738	7.441	7.441	−172.68	1220.52	1047.84	−0.3552	2.8405	2.4853	−30
−29	0.3652	0.7435	0.01738	7.025	7.025	−172.24	1220.52	1048.28	−0.3542	2.8339	2.4797	−29
−28	0.3876	0.7891	0.01738	6.634	6.634	−171.80	1220.52	1048.72	−0.3532	2.8274	2.4742	−28
−27	0.4113	0.8373	0.01738	6.267	6.267	−171 35	1220.51	1049.16	−0.3521	2.8207	2.4686	−27
−26	0.4363	0.8882	0.01738	5.921	5.921	−170.91	1220.51	1049.60	−0.3511	2.8143	2.4632	−26
−25	0.4627	0.9420	0.01739	5.596	5.596	−170.46	1220.51	1050.05	−0.3501	2.8078	2.4577	−25
−24	0 4905	0.9987	0.01739	5.290	5.290	−170.01	1220.50	1050.49	−0.3490	2.8013	2.4523	−24
−23	0.5199	1.059	0.01739	5.003	5.003	−169.56	1220.49	1050.93	−0.3480	2.7949	2.4469	−23
−22	0.5509	1.122	0.01739	4.732	4.732	−169.12	1220 49	1051.37	−0.3470	2.7885	2.4415	−22
−21	0.5836	1.188	0.01739	4.477	4.477	−168.66	1220.48	1051.82	−0.3460	2.7822	2.4362	−21
−20	0.6181	1.259	0.01739	4.237	4.237	−168.21	1220.47	1052.26	−0.3449	2.7757	2.4308	−20
−19	0.6545	1.333	0.01739	4.011	4.011	−167.76	1220 46	1052.70	−0.3439	2.7695	2.4256	−19
−18	0.6928	1.410	0.01740	3.797	3.797	−167.31	1220.45	1053.14	−0.3429	2.7632	2.4203	−18
−17	0.7332	1.493	0.01740	3.596	3.596	−166.85	1220.43	1053.58	−0.3418	2.7568	2.4150	−17
−16	0.7757	1.579	0.01740	3.407	3.407	−166.40	1220.42	1054.02	−0.3408	2.7506	2.4098	−16
−15	0.8204	1.670	0.01740	3.228	3.228	−165.94	1220.41	1054.47	−0.3398	2.7444	2.4046	−15
−14	0.8676	1.766	0.01740	3.060	3.060	−165.48	1220.39	1054.91	−0.3388	2.7383	2.3995	−14
−13	0.9172	1.867	0.01740	2.901	2.901	−165.03	1220.38	1055.35	−0.3377	2.7320	2.3943	−13
−12	0.9694	1.974	0.01740	2.750	2.750	−164.57	1220 36	1055.79	−0.3367	2.7259	2.3892	−12
−11	1.024	2.086	0.01740	2.609	2.609	−164.11	1220.34	1056 23	−0.3357	2.7198	2.3841	−11
−10	1.082	2.203	0.01741	2.475	2.475	−163.65	1220.32	1056.67	−0.3347	2.7138	2.3791	−10
−9	1.143	2.327	0.01741	2.349	2.349	−163.18	1220.30	1057.12	−0.3336	2.7076	2.3740	−9
−8	1.207	2.457	0.01741	2.229	2.229	−162.72	1220.28	1057.56	−0.3326	2.7016	2.3690	−8
−7	1.274	2.594	0.01741	2.116	2.116	−162.26	1220.26	1058.00	−0.3316	2.6956	2.3640	−7
−6	1.344	2.737	0.01741	2.010	2.010	−161 79	1220.23	1058.44	−0.3306	2.6896	2.3590	−6
−5	1.419	2.888	0.01741	1.909	1.909	−161.33	1220.21	1058.88	−0.3295	2.6836	2.3541	−5
−4	1.496	3.047	0.01742	1.814	1.814	−160.86	1220.18	1059.32	−0.3285	2.6777	2.3492	−4
−3	1.578	3.213	0.01742	1.723	1.723	−160.39	1220.15	1059.76	−0.3275	2.6718	2.3443	−3
−2	1.664	3.388	0.01742	1.638	1.638	−159.92	1220.13	1060.21	−0.3264	2.6658	2.3394	−2
−1	1.754	3.572	0.01742	1.557	1.557	−159.45	1220.10	1060.65	−0.3254	2.6600	2.3346	−1

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE p_s		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Solid v_i	Evap. $v_{ig} \times 10^{-3}$	Sat. Vapor $v_g \times 10^{-3}$	Sat. Solid h_i	Evap. h_{ig}	Sat. Vapor h_g	Sat. Solid s_i	Evap. s_{ig}	Sat. Vapor s_g	
0	0.01849	0.03764	0.01742	14.81	14.81	−158.98	1220.07	1061.09	−0.3244	2.6541	2.3297	0
1	0.01948	0.03966	0.01742	14.08	14.08	−158.51	1220.04	1061.53	−0.3234	2.6483	2.3249	1
2	0.02052	0.04178	0.01742	13.40	13.40	−158.04	1220.01	1061.97	−0.3224	2.6425	2.3201	2
3	0.02616	0.04400	0.01743	12.75	12.75	−157.56	1219.97	1062.41	−0.3213	2.6367	2.3154	3
4	0.02276	0.04633	0.01743	12.14	12.14	−157.09	1219.94	1062.85	−0.3203	2.6309	2.3106	4
5	0.02396	0.04878	0 01743	11.55	11.55	−156.61	1219.90	1063.29	−0.3193	2.6252	2.3059	5
6	0.02521	0.05134	0.01743	11.00	11.00	−156.14	1219.88	1063.74	−0.3182	2.6194	2.3012	6
7	0.02653	0.05402	0.01743	10.48	10.48	−155.66	1219.84	1064.18	−0.3172	2.6138	2.2966	7
8	0.02791	0.05683	0.01743	9.979	9.979	−155.18	1219.80	1064.62	−0.3162	2.6081	2.2919	8
9	0.02936	0.05977	0.01744	9.507	9.507	−154.70	1219.76	1065.06	−0.3152	2.6025	2.2873	9
10	0.03087	0.06286	0.01744	9.060	9 060	−154.22	1219.72	1065.50	−0.3142	2.5969	2.2827	10
11	0.03246	0.06608	0.01744	8 636	8.636	−153.74	1219.68	1065.94	−0.3131	2.5912	2.2781	11
12	0.03412	0.06946	0.01744	8.234	8.234	−153.26	1219.64	1066.38	−0.3121	2.5857	2.2736	12
13	0.03585	0.07300	0.01744	7.851	7.851	−152.77	1219.59	1066.82	−0.3111	2.5801	2.2690	13
14	0.03767	0.07669	0.01744	7.489	7.489	−152.29	1219.55	1067.26	−0.3101	2.5746	2.2645	14
15	0.03957	0,08056	0.01744	7.144	7.144	−151.80	1219.50	1067.70	−0.3090	2.5690	2.2600	15
16	0.04156	0.08461	0.01745	6.817	6.817	−151.32	1219.46	1068.14	−0.3080	2.5635	2.2555	16
17	0.04363	0.08884	0.01745	6.505	6.505	−150.83	1219.41	1068.58	−0.3070	2.5581	2.2511	17
18	0.04581	0.09326	0.01745	6.210	6.210	−150.34	1219.36	1069.02	−0.3060	2.5526	2.2466	18
19	0.04808	0.09789	0.01745	5.929	5.929	−149.85	1219.31	1069.46	−0.3049	2.5471	2.2422	19
20	0.05045	0.1027	0.01745	5.662	5.662	−149.36	1219.26	1069.90	−0.3039	2.5417	2.2378	20
21	0.05293	0.1078	0.01745	5.408	5.408	−148.87	1219.21	1070.34	−0.3029	2.5364	2.2335	21
22	0.05552	0.1130	0.01746	5.166	5.166	−148.38	1219.16	1070.78	−0.3019	2.5310	2.2291	22
23	0.05823	0.1186	0.01746	4.936	4.936	−147.88	1219.10	1071.22	−0.3008	2.5256	2.2248	23
24	0.06105	0.1243	0.01746	4.717	4.717	−147.39	1219.05	1071.66	−0.2998	2.5203	2.2205	24
25	0.06400	0.1303	0.01746	4.509	4 509	−146.89	1218.98	1072.09	−0.2988	2.5150	2.2162	25
26	0.06708	0.1366	0.01746	4.311	4.311	−146.40	1218.93	1072.53	−0.2978	2.5097	2.2119	26
27	0.07030	0.1431	0.01746	4.122	4.122	−145.90	1218.87	1072.97	−0.2968	2.5045	2.2077	27
28	0.07365	0.1500	0.01746	3.943	3.943	−145.40	1218.81	1073.41	−0.2957	2.4991	2.2034	28
29	0.07715	0.1571	0.01747	3.771	3.771	−144.90	1218.75	1073.85	−0.2947	2.4939	2.1992	29
30	0.08080	0.1645	0.01747	3.608	3.608	−144.40	1218.69	1074.29	−0.2937	2.4887	2.1950	30
31	0.08461	0.1723	0.01747	3.453	3.453	−143.90	1218.63	1074.73	−0.2927	2.4835	2.1908	31
32	0.08858	0.1803	0.01747	3.305	3.305	−143.40	1218.56	1075.16	−0.2916	2.4783	2.1867	32

[a]Compiled by John A. Goff and S. Gratch.

Table 2. Thermodynamic Properties of Water at Saturation[a] (Continued)

Fahr. Temp. t(F)	Absolute Pressure p_s		Specific Volume, cu ft per lb			Enthalpy, Btu per lb			Entropy, Btu per (lb) (°F)			Fahr. Temp. t(F)
	Lb/Sq In.	In. Hg	Sat. Liquid v_f	Evap. v_{fg}	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g	
*32	0.088586	0.18036	0.01602	3304.6	3304.6	0.00	1075.16	1075.16	0.00000	2.1867	2.1867	32*
33	0.092227	0.18778	0.01602	3180.5	3180.5	1.01	1074.59	1075.60	0.00205	2.1811	2.1831	33
34	0.095999	0.19546	0.01602	3061.7	3061.7	2.01	1074.03	1076.04	0.00409	2.1755	2.1796	34
35	0.099908	0.20342	0.01602	2947.8	2947.8	3.02	1073.46	1076.48	0.00612	2.1700	2.1761	35
36	0.10396	0.21166	0.01602	2838.7	2838.7	4.02	1072.90	1076.92	0.00815	2.1644	2.1726	36
37	0.10815	0.22020	0.01602	2734.1	2734.1	5.03	1072.33	1077.36	0.01018	2.1589	2.1691	37
38	0.11249	0.22904	0.01602	2633.8	2633.8	6.03	1071.77	1077.80	0.01220	2.1535	2.1657	38
39	0.11699	0.23819	0.01602	2537.6	2537.6	7.04	1071.20	1078.24	0.01422	2.1480	2.1622	39
40	0.12164	0.24767	0.01602	2445.4	2445.4	8.04	1070.64	1078.68	0.01623	2.1426	2.1588	40
41	0.12646	0.25748	0.01602	2356.9	2356.9	9.05	1070.06	1079.11	0.01824	2.1372	2.1554	41
42	0.13145	0.26763	0.01602	2272.0	2272.0	10.05	1069.50	1079.55	0.02024	2.1318	2.1520	42
43	0.13660	0.27813	0.01602	2190.5	2190.5	11.05	1068.94	1079.99	0.02224	2.1265	2.1487	43
44	0.14194	0.28899	0.01602	2112.3	2112.3	12.06	1068.37	1080.43	0.02423	2.1211	2.1453	44
45	0.14746	0.30023	0.01602	2037.3	2037.3	13.06	1067.81	1080.87	0.02622	2.1158	2.1420	45
46	0.15317	0.31185	0.01602	1965.2	1965.2	14.06	1067.24	1081.30	0.02820	2.1105	2.1387	46
47	0.15907	0.32387	0.01602	1896.0	1896.0	15.06	1066.68	1081.74	0.03018	2.1052	2.1354	47
48	0.16517	0.33629	0.01602	1829.5	1829.5	16.07	1066.11	1082.18	0.03216	2.0999	2.1321	48
49	0.17148	0.34913	0.01602	1765.7	1765.7	17.07	1065.55	1082.62	0.03413	2.0947	2.1288	49
50	0.17799	0.36240	0.01602	1704.3	1704.3	18.07	1064.99	1083.06	0.03610	2.0895	2.1256	50
51	0.18473	0.37611	0.01602	1645.4	1645.4	19.07	1064.42	1083.49	0.03806	2.0842	2.1223	51
52	0.19169	0.39028	0.01602	1588.7	1588.7	20.07	1063.86	1083.93	0.04002	2.0791	2.1191	52
53	0.19888	0.40492	0.01603	1534.3	1534.3	21.07	1063.30	1084.37	0.04197	2.0739	2.1159	53
54	0.20630	0.42003	0.01603	1481.9	1481.9	22.08	1062.72	1084.80	0.04392	2.0688	2.1127	54
55	0.21397	0.43564	0.01603	1431.5	1431.5	23.08	1062.16	1085.24	0.04587	2.0637	2.1096	55
56	0.22188	0.45176	0.01603	1383.1	1383.1	24.08	1061.60	1085.68	0.04781	2.0586	2.1064	56
57	0.23006	0.46840	0.01603	1336.5	1336.5	25.08	1061.04	1086.12	0.04975	2.0535	2.1033	57
58	0.23849	0.48558	0.01603	1291.7	1291.7	26.08	1060.47	1086.55	0.05168	2.0485	2.1002	58
59	0.24720	0.50330	0.01603	1248.6	1248.6	27.08	1059.91	1086.99	0.05361	2.0434	2.0970	59
60	0.25618	0.52160	0.01603	1207.1	1207.1	28.08	1059.34	1087.42	0.05553	2.0385	2.0940	60
61	0.26545	0.54047	0.01604	1167.2	1167.2	29.08	1058.78	1087.86	0.05746	2.0334	2.0909	61

[a]Compiled by John A. Goff and S. Gratch.

*Extrapolated to represent metastable equilibrium with undercooled liquid.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE p_s		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Liquid v_f	Evap. v_{fg}	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g	
62	0.27502	0.55994	0.01604	1128.7	1128.7	30.08	1058.22	1088.30	0.05937	2.0284	2.0878	62
63	0.28488	0.58002	0.01604	1091.7	1091.7	31.08	1057.65	1088.73	0.06129	2.0235	2.0848	63
64	0.29505	0.60073	0.01604	1056.1	1056.1	32.08	1057.09	1089.17	0.06320	2.0186	2.0818	64
65	0.30554	0.62209	0.01604	1021.7	1021.7	33.08	1056.52	1089.60	0.06510	2.0136	2.0787	65
66	0.31636	0.64411	0.01604	988.63	988.65	34.07	1055.97	1090.04	0.06700	2.0087	2.0757	66
67	0.32750	0.66681	0.01605	956.76	956.78	35.07	1055.40	1090.47	0.06890	2.0039	2.0728	67
68	0.33900	0.69021	0.01605	926.06	926.08	36.07	1054.84	1090.91	0.07080	1.9990	2.0698	68
69	0.35084	0.71432	0.01605	896.47	896.49	37.07	1054.27	1091.34	0.07269	1.9941	2.0668	69
70	0.36304	0.73916	0.01605	867.95	867.97	38.07	1053.71	1091.78	0.07458	1.9893	2.0639	70
71	0.37561	0.76476	0.01605	840.45	840.47	39.07	1053.14	1092.21	0.07646	1.9845	2 0610	71
72	0.38856	0.79113	0.01606	813.95	813.97	40.07	1052.58	1092.65	0 07834	1 9797	2.0580	72
73	0.40190	0.81829	0.01606	788.38	788.40	41.07	1052.01	1093.08	0.08022	1.9749	2.0551	73
74	0.41564	0.84626	0.01606	763.73	763.75	42.06	1051.46	1093.52	0.08209	1.9701	2.0522	74
75	0.42979	0.87506	0.01606	739.95	739.97	43.06	1050.89	1093.95	0.08396	1.9654	2.0494	75
76	0.44435	0.90472	0.01606	717.01	717.03	44.06	1050.32	1094.38	0.08582	1.9607	2.0465	76
77	0.45935	0.93524	0.01607	694.88	694.90	45.06	1049.76	1094.82	0.08769	1.9560	2.0437	77
78	0.47478	0.96666	0.01607	673.52	673.54	46.06	1049.19	1095.25	0.08954	1.9513	2.0408	78
79	0.49066	0.99900	0.01607	652.91	652.93	47.06	1048.62	1095.68	0.09140	1.9466	2.0380	79
80	0.50701	1.0323	0.01607	633.01	633.03	48.05	1048.07	1096.12	0.09325	1.9419	2.0352	80
81	0.52382	1.0665	0.01608	613.80	613.82	49.05	1047.50	1096.55	0.09510	1.9373	2.0324	81
82	0.54112	1.1017	0.01608	595.25	595.27	50.05	1046.93	1096.98	0.09694	1.9328	2.0297	82
83	0.55892	1.1380	0.01608	577.34	577.36	51.05	1046 37	1097.42	0.09878	1.9281	2.0269	83
84	0.57722	1.1752	0.01608	560.04	560.06	52.05	1045.80	1097.85	0.10062	1.9236	2 0242	84
85	0.59604	1.2136	0.01609	543.33	543.35	53.05	1045.23	1098.28	0.10246	1.9189	2.0214	85
86	0.61540	1.2530	0.01609	527.19	527.21	54.04	1044.67	1098.71	0.10429	1.9144	2.0187	86
87	0.63530	1.2935	0.01609	511.60	511.62	55.04	1044.10	1099.14	0.10611	1.9099	2.0160	87
88	0.65575	1.3351	0.01610	496.52	496.54	56.04	1043.54	1099.58	0.10794	1.9054	2.0133	88
89	0.67678	1.3779	0.01610	481.96	481.98	57.04	1042.97	1100.01	0.10976	1.9008	2.0106	89
90	0.69838	1.4219	0.01610	467.88	467.90	58.04	1042.40	1100.44	0.11158	1.8963	2.0079	90
91	0.72059	1.4671	0.01610	454.26	454.28	59.03	1041.84	1100.87	0.11339	1.8919	2.0053	91

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE p_s		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Liquid v_f	Evap. v_{fg}	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g	
92	0.74340	1.5136	0.01611	441.10	441.12	60.03	1041.27	1101.30	0.11520	1.8874	2.0026	92
93	0.76684	1.5613	0.01611	428.38	428.40	61.03	1040.70	1101.73	0.11701	1.8830	2.0000	93
94	0.79091	1.6103	0.01611	416.07	416.09	62.03	1040.13	1102.16	0.11881	1.8786	1.9974	94
95	0.81564	1.6607	0.01612	404.17	404.19	63.03	1039.56	1102.59	0.12061	1.8741	1.9947	95
96	0.84103	1.7124	0.01612	392.65	392.67	64.02	1039.00	1103.02	0.12241	1.8698	1.9922	96
97	0.86711	1.7655	0.01612	381.51	381.53	65.02	1038.43	1103.45	0.12420	1.8654	1.9896	97
98	0.89388	1.8200	0.01612	370.73	370.75	66.02	1037.86	1103.88	0.12600	1.8610	1.9870	98
99	0.92137	1.8759	0.01613	360.30	360.32	67.02	1037.29	1104.31	0.12778	1.8566	1.9844	99
100	0.94959	1.9334	0.01613	350.20	350.22	68.02	1036.72	1104.74	0.12957	1.8523	1.9819	100
101	0.97854	1.9923	0.01614	340.42	340.44	69.01	1036.16	1105.17	0.13135	1.8480	1.9793	101
102	1.0083	2.0529	0.01614	330.96	330 98	70.01	1035.58	1105.59	0.13313	1.8437	1.9768	102
103	1.0388	2.1149	0.01614	321.80	321.82	71.01	1035.01	1106.02	0.13490	1.8394	1.9743	103
104	1.0700	2.1786	0.01614	312.93	312.95	72.01	1034.44	1106.45	0.13667	1.8351	1.9718	104
105	1.1021	2.2440	0.01615	304.34	304.36	73.01	1033.87	1106.88	0.13844	1.8309	1.9693	105
106	1.1351	2.3110	0.01615	296.02	296.04	74.01	1033.29	1107.30	0.14021	1.8266	1.9668	106
107	1.1688	2.3798	0.01616	287.96	287.98	75.00	1032.73	1107.73	0.14197	1.8224	1.9644	107
108	1.2035	2.4503	0.01616	280.14	280.16	76.00	1032.16	1108.16	0.14373	1.8182	1.9619	108
109	1.2390	2.5226	0.01616	272.58	272.60	77.00	1031.58	1108.58	0.14549	1.8140	1.9595	109
110	1.2754	2.5968	0.01617	265.24	265.26	78.00	1031.01	1109.01	0.14724	1.8098	1.9570	110
111	1.3128	2.6728	0.01617	258.14	258.16	79.00	1030.44	1109.44	0.14899	1.8056	1.9546	111
112	1.3510	2.7507	0.01617	251.25	251.27	80.00	1029.86	1109.86	0.15074	1.8015	1.9522	112
113	1.3902	2.8306	0.01618	244.57	244.59	80.99	1029.30	1110.29	0.15248	1.7973	1.9498	113
114	1.4305	2.9125	0.01618	238.10	238.12	81.99	1028.72	1110.71	0 15423	1.7932	1.9474	114
115	1.4717	2.9963	0.01618	231.82	231.84	82.99	1028.15	1111.14	0.15596	1.7890	1.9450	115
116	1.5139	3.0823	0.01619	225.73	225.75	83.99	1027.57	1111.56	0.15770	1.7849	1.9426	116
117	1.5571	3.1703	0.01619	219.83	219.85	84.99	1026.99	1111.98	0.15943	1.7809	1.9403	117
118	1.6014	3.2606	0.01620	214.10	214.12	85.99	1026.42	1112.41	0.16116	1.7767	1.9379	118
119	1.6468	3.3530	0.01620	208.54	208 56	86.98	1025.85	1112.83	0.16289	1.7727	1.9356	119
120	1.6933	3.4477	0.01620	203.16	203.18	87.98	1025.28	1113.26	0.16461	1.7687	1.9333	120
121	1.7409	3.5446	0.01621	197 93	197.95	88.98	1024.70	1113.68	0.16634	1.7647	1.9310	121

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE p_s		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Liquid v_f	Evap. v_{fg}	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g	
122	1.7897	3.6439	0.01621	192.85	192.87	89.98	1024.12	1114.10	0.16805	1.7606	1.9286	122
123	1.8396	3.7455	0.01622	187.93	187.95	90.98	1023.54	1114.52	0.16977	1.7566	1.9264	123
124	1.8907	3.8496	0.01622	183.15	183.17	91.98	1022.96	1114.94	0.17148	1.7526	1.9241	124
125	1.9430	3.9561	0.01622	178.51	178.53	92.98	1022.39	1115.37	0.17319	1.7486	1.9218	125
126	1.9966	4.0651	0.01623	174.00	174.02	93.98	1021.81	1115.79	0.17490	1.7446	1.9195	126
127	2.0514	4.1768	0.01623	169.63	169.65	94.97	1021.24	1116.21	0.17660	1.7407	1.9173	127
128	2.1075	4.2910	0.01624	165.38	165.40	95.97	1020.66	1116.63	0.17830	1.7367	1.9150	128
129	2.1649	4.4078	0.01624	161.26	161.28	96.97	1020.08	1117.05	0.18000	1.7328	1.9128	129
130	2.2237	4.5274	0.01625	157.25	157.27	97.97	1019.50	1117.47	0.18170	1.7289	1.9106	130
131	2.2838	4.6498	0.01625	153.36	153.38	98.97	1018.92	1117.89	0.18339	1.7250	1.9084	131
132	2.3452	4.7750	0.01626	149.58	149.60	99.97	1018.34	1118.31	0.18508	1.7211	1.9062	132
133	2.4081	4.9030	0.01626	145.91	145.93	100.97	1017.76	1118.73	0.18676	1.7172	1.9040	133
134	2.4725	5.0340	0.01626	142.34	142.36	101.97	1017.18	1119.15	0.18845	1.7134	1.9018	134
135	2.5382	5.1679	0.01627	138.87	138.89	102.97	1016.59	1119.56	0.19013	1.7095	1.8996	135
136	2.6055	5.3049	0.01627	135.50	135.52	103.97	1016.01	1119.98	0.19181	1.7056	1.8974	136
137	2.6743	5.4450	0.01628	132.22	132.24	104.97	1015.43	1120.40	0.19348	1.7018	1.8953	137
138	2.7446	5.5881	0.01628	129.04	129.06	105.97	1014.85	1120.82	0.19516	1.6979	1.8931	138
139	2.8165	5.7345	0.01629	125.94	125.96	106.97	1014.26	1121.23	0.19683	1.6942	1.8910	139
140	2.8900	5.8842	0.01629	122.94	122.96	107.96	1013.69	1121.65	0.19850	1.6903	1.8888	140
141	2.9651	6.0371	0.01630	120.01	120.03	108.96	1013.11	1122.07	0.20016	1.6865	1.8867	141
142	3.0419	6.1934	0.01630	117.16	117.18	109.96	1012.52	1122.48	0.20182	1.6828	1.8846	142
143	3.1204	6.3532	0.01631	114.40	114.42	110.96	1011.94	1122.90	0.20348	1.6790	1.8825	143
144	3.2006	6.5164	0.01631	111.70	111.72	111.96	1011.35	1123.31	0.20514	1.6753	1.8804	144
145	3.2825	6.6832	0.01632	109.09	109.11	112.96	1010.77	1123.73	0.20679	1.6715	1.8783	145
146	3.3662	6.8536	0.01632	106.54	106.56	113.96	1010.18	1124.14	0.20845	1.6678	1.8763	146
147	3.4517	7.0277	0.01633	104.06	104.08	114.96	1009.59	1124.55	0.21010	1.6641	1.8742	147
148	3.5390	7.2056	0.01633	101.65	101.67	115.96	1009.01	1124.97	0.21174	1.6604	1.8721	148
149	3.6282	7.3872	0.01634	99.306	99.322	116.96	1008.42	1125.38	0.21339	1.6567	1.8701	149
150	3.7194	7.5727	0.01634	97.022	97.038	117.96	1007.83	1125.79	0.21503	1.6530	1.8680	150
151	3.8124	7.7622	0.01635	94.799	94.815	118.96	1007.24	1126.20	0.21667	1.6493	1.8660	151

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Continued)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE p_s		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Liquid v_f	Evap. v_{fg}	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g	
152	3.9074	7.9556	0.01635	92.635	92.651	119.96	1006.66	1126.62	0.21830	1.6457	1.8640	152
153	4.0044	8.1532	0.01636	90.528	90.544	120.97	1006.06	1127.03	0.21994	1.6421	1.8620	153
154	4.1035	8.3548	0.01636	88.477	88.493	121.97	1005.47	1127.44	0.22157	1.6384	1.8600	154
155	4.2046	8.5607	0.01637	86.480	86.496	122.97	1004 88	1127.85	0 22320	1.6348	1.8580	155
156	4.3078	8.7708	0.01637	84.536	84.552	123.97	1004.29	1128.26	0.22482	1.6312	1.8560	156
157	4.4132	8.9853	0.01638	82.642	82.658	124.97	1003.70	1128.67	0.22645	1.6276	1.8540	157
158	4.5207	9.2042	0.01638	80.798	80.814	125.97	1003.11	1129.08	0.22807	1.6239	1.8520	158
159	4.6304	9.4276	0.01639	79.001	79.017	126 97	1002.51	1129.48	0.22969	1.6204	1.8501	159
160	4.7424	9.6556	0.01639	77.251	77.267	127.97	1001.92	1129.89	0.23130	1.6168	1.8481	160
161	4.8566	9.8882	0.01640	75.546	75.562	128.97	1001.33	1130.30	0.23292	1.6133	1.8462	161
162	4.9732	10.126	0.01640	73.885	73.901	129.97	1000.74	1130.71	0.23453	1.6097	1.8442	162
163	5.0921	10.368	0.01641	72.267	72.283	130.98	1000.13	1131.11	0.23614	1.6062	1.8423	163
164	5.2134	10.615	0.01642	70.690	70.706	131.98	999.54	1131.52	0.23774	1.6027	1.8404	164
165	5.3372	10.867	0.01642	69.153	69.169	132.98	998.94	1131.92	0.23935	1.5990	1.8384	165
166	5.4634	11.124	0.01643	67.654	67.670	133.98	998.35	1132.33	0.24095	1.5956	1.8365	166
167	5.5921	11.386	0.01643	66.194	66.210	134.98	997.75	1132.73	0.24255	1.5920	1.8346	167
168	5.7233	11.653	0.01644	64.770	64.786	135.98	997.16	1133.14	0.24414	1.5887	1.8328	168
169	5.8572	11.925	0.01644	63.382	63.398	136.99	996.55	1133.54	0.24574	1.5852	1.8309	169
170	5.9936	12.203	0.01645	62.029	62.045	137.99	995.95	1133.94	0.24733	1.5817	1.8290	170
171	6.1328	12.487	0.01645	60.710	60.726	138.99	995.36	1134.35	0.24892	1.5782	1.8271	171
172	6.2746	12.775	0.01646	59.423	59.439	139.99	994.76	1134.75	0.25051	1.5748	1.8253	172
173	6.4192	13.070	0.01647	58.168	58.184	141.00	994.15	1135.15	0.25209	1.5713	1.8234	173
174	6.5666	13.370	0.01647	56.944	56.960	142.00	993.55	1135.55	0.25367	1.5679	1.8216	174
175	6.7168	13.676	0.01648	55.750	55.766	143.00	992.95	1135.95	0.25525	1.5644	1.8197	175
176	6.8699	13.987	0.01648	54.586	54.602	144.00	992.35	1136.35	0.25683	1.5611	1.8179	176
177	7.0259	14.305	0 01649	53.450	53.466	145.00	991.75	1136.75	0.25841	1.5577	1.8161	177
178	7.1849	14.629	0.01650	52.341	52.357	146.01	991.14	1137.15	0.25998	1.5543	1.8143	178
179	7.3469	14.959	0.01650	51.260	51.276	147.01	990.54	1137.55	0.26155	1.5508	1.8124	179
180	7.5119	15.295	0.01651	50.203	50.220	148.01	989.93	1137.94	0.26312	1.5475	1.8106	180
181	7.6801	15.637	0.01651	49.173	49.190	149.02	989.32	1138.34	0.26468	1.5442	1.8089	181

[a]Compiled by John A. Goff and S. Gratch.

TABLE 2. THERMODYNAMIC PROPERTIES OF WATER AT SATURATION[a] (Concluded)

FAHR. TEMP. t(F)	ABSOLUTE PRESSURE p_s		SPECIFIC VOLUME, CU FT PER LB			ENTHALPY, BTU PER LB			ENTROPY, BTU PER (LB) (°F)			FAHR. TEMP. t(F)
	Lb/Sq In.	In. Hg	Sat. Liquid v_f	Evap. v_{fg}	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g	
182	7.8514	15.986	0 01652	48.168	48.185	150.02	988.72	1138.74	0.26625	1.5408	1.8071	182
183	8.0258	16.341	0.01652	47.187	47.204	151.02	988.12	1139.14	0.26781	1.5375	1.8053	183
184	8.2035	16.703	0.01653	46.229	46.246	152.03	987.50	1139.53	0.26937	1.5341	1.8035	184
185	8.3845	17 071	0.01654	45.294	45.311	153 03	986.89	1139.92	0.27093	1.5308	1.8017	185
186	8.5688	17.446	0.01654	44.381	44.398	154.04	986.28	1140.32	0 27248	1.5275	1.8000	186
187	8.7565	17.829	0.01655	43.489	43.506	155.04	985.67	1140.71	0.27404	1.5242	1.7982	187
188	8.9476	18.218	0.01656	42.619	42.636	156.04	985.07	1141.11	0.27559	1.5209	1.7965	188
189	9.1422	18.614	0.01656	41.769	41.786	157.05	984.45	1141.50	0.27713	1.5176	1.7947	189
190	9.3403	19.017	0.01657	40.939	40.956	158.05	983.84	1141.89	0.27868	1.5143	1.7930	190
191	9.5420	19.428	0.01658	40.128	40.145	159.06	983.22	1142.28	0.28022	1.5111	1.7913	191
192	9.7473	19.846	0.01658	39.337	39.354	160.06	982.61	1142.67	0.28176	1.5078	1.7896	192
193	9.9563	20.271	0.01659	38.563	38.580	161.06	982.00	1143.06	0.28330	1.5045	1.7878	193
194	10.169	20.704	0.01659	37.807	37.824	162.07	981.38	1143.45	0.28484	1.5013	1.7861	194
195	10.386	21.145	0.01660	37.069	37.086	163.08	980.76	1143.84	0.28638	1.4980	1.7844	195
196	10.606	21.594	0.01661	36.348	36.365	164.08	980.15	1144.23	0.28791	1.4949	1.7828	196
197	10.830	22.050	0.01661	35.643	35.660	165.08	979.54	1144.62	0.28944	1.4917	1.7811	197
198	11.058	22.515	0.01662	34.954	34.971	166.09	978.91	1145.00	0.29097	1.4884	1.7794	198
199	11.290	22.987	0.01663	34.281	34.298	167.10	978.29	1145.39	0.29250	1.4852	1.7777	199
200	11.526	23.468	0.01663	33.623	33.640	168.10	977.68	1145.78	0.29402	1 4820	1.7760	200
201	11.767	23.957	0.01664	32.980	32.997	169.11	977.05	1146.16	0.29554	1.4789	1.7744	201
202	12.011	24.455	0.01665	32.351	32.368	170.11	976.43	1146.54	0.29706	1.4756	1.7727	202
203	12.260	24.961	0.01665	31.737	31.754	171.12	975.81	1146.93	0.29858	1.4725	1.7711	203
204	12.513	25.476	0.01666	31.136	31.153	172.12	975.19	1147.31	0.30010	1.4693	1.7694	204
205	12.770	26.000	0.01667	30 549	30.566	173.13	974.56	1147.69	0.30161	1.4662	1.7678	205
206	13.031	26.532	0.01667	29.974	29.991	174.14	973.94	1148.08	0.30312	1.4631	1.7662	206
207	13.297	27.074	0.01668	29.413	29.430	175.14	973.32	1118.46	0.30463	1.4600	1.7646	207
208	13.568	27.625	0.01669	28.863	28.880	176.15	972.69	1148.84	0.30614	1.4568	1.7629	208
209	13.843	28.185	0.01669	28.326	28.343	177.16	972.06	1149.22	0.30765	1.4536	1.7613	209
210	14.123	28.754	0.01670	27.801	27.818	178.17	971 43	1149.60	0.30915	1.4506	1.7597	210
211	14.407	29.333	0.01671	27.287	27.304	179.17	970.81	1149.98	0.31065	1.4474	1.7581	211
212	14.696	29 921	0.01671	26.784	26.801	180.18	970.17	1150.35	0.31215	1.4444	1.7565	212

[a]Compiled by John A. Goff and S. Gratch.

TABLE 3. PROPERTIES OF SATURATED STEAM: PRESSURE TABLE[a]

Abs. Press. In. Hg p	Temp F t	Specific Volume		Enthalpy			Entropy			Abs Press. In. Hg p
		Sat. Liquid v_f	Sat. Vapor v_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid S_f	Evap. S_{fg}	Sat. Vapor S_g	
0.25	40.23	0.01602	2423.7	8.28	1071.1	1079.4	0.0166	2.1423	2.1589	0.25
0.50	58.80	0.01604	1256.4	26.86	1060.6	1087.5	0.0532	2.0453	2.0985	0.50
0.75	70.43	0.01606	856.1	38.47	1054.0	1092.5	0.0754	1.9881	2.0635	0.75
1.00	79.03	0.01608	652.3	47.05	1049.2	1096.3	0.0914	1.9473	2.0387	1.00
1.5	91.72	0.01611	444.9	59.71	1042.0	1101.7	0.1147	1.8894	2.0041	1.5
2	101.14	0.01614	339.2	69.10	1036.6	1105.7	0.1316	1.8481	1.9797	2
4	125.43	0.01622	176.7	93.34	1022.7	1116.0	0.1738	1.7476	1.9214	4
6	140.78	0.01630	120.72	108.67	1013.6	1122.3	0.1996	1.6881	1.8877	6
8	152.24	0.01635	92.16	120.13	1006.9	1127.0	0.2186	1.6454	1.8640	8
10	161.49	0.01640	74.76	129.38	1001.4	1130.8	0.2335	1.6121	1.8456	10
12	169.28	0.01644	63.03	137.18	996.7	1133.9	0.2460	1.5847	1.8307	12
14	176.05	0.01648	54.55	143.96	992.6	1136.6	0.2568	1.5613	1.8181	14
16	182.05	0.01652	48.14	149.98	988.9	1138.9	0.2662	1.5410	1.8072	16
18	187.45	0.01655	43.11	155.39	985.7	1141.1	0.2746	1.5231	1.7977	18
20	192.37	0.01658	39.07	160.33	982.7	1143.0	0.2822	1.5069	1.7891	20
22	196.90	0.01661	35.73	164.87	979.8	1144.7	0.2891	1.4923	1.7814	22
24	201.09	0.01664	32.94	169.09	977.2	1146.3	0.2955	1.4789	1.7744	24
26	205.00	0.01667	30.56	173.02	974.8	1147.8	0.3014	1.4665	1.7679	26
28	208.67	0.01669	28.52	176.72	972.5	1149.2	0.3069	1.4550	1.7619	28
30	212.13	0.01672	26.74	180.19	970.3	1150.5	0.3122	1.4442	1.7564	30
Lb/Sq In.										Lb/Sq In.
14.696	212.00	0.01672	26.80	180.07	970.3	1150.4	0.3120	1.4446	1.7566	14.696
16	216.32	0.01674	24.75	184.42	967.6	1152.0	0.3184	1.4313	1.7497	16
18	222.41	0.01679	22.17	190.56	963.6	1154.2	0.3275	1.4128	1.7403	18
20	227.96	0.01683	20.089	196.16	960.1	1156.3	0.3356	1.3962	1.7319	20
22	233.07	0.01687	18.375	201.33	956.8	1158.1	0.3431	1.3811	1.7242	22
24	237.82	0.01691	16.938	206.14	953.7	1159.8	0.3500	1.3672	1.7172	24
26	242.25	0.01694	15.715	210.62	950.7	1161.3	0.3564	1.3544	1.7108	26
28	246.41	0.01698	14.663	214.83	947.9	1162.7	0.3623	1.3425	1.7048	28
30	250.33	0.01701	13.746	218.82	945.3	1164.1	0.3680	1.3313	1.6993	30
32	254.05	0.01704	12.940	222.59	942.8	1165.4	0.3733	1.3209	1.6941	32
34	257.58	0.01707	12.226	226.18	940.3	1166.5	0.3783	1.3110	1.6893	34
36	260.95	0.01709	11.588	229.60	938.0	1167.6	0.3831	1.3017	1.6848	36
38	264.16	0.01712	11.015	232.89	935.8	1168.7	0.3876	1.2929	1.6805	38
40	267.25	0.01715	10.498	236.03	933.7	1169.7	0.3919	1.2844	1.6763	40
42	270.21	0.01717	10.029	239.04	931.6	1170.7	0.3960	1.2764	1.6724	42
44	273.05	0.01720	9.601	241.95	929.6	1171.6	0.4000	1.2687	1.6687	44
46	275.80	0.01722	9.209	244.75	927.7	1172.4	0.4038	1.2613	1.6652	46
48	278.45	0.01725	8.848	247.47	925.8	1173.3	0.4075	1.2542	1.6617	48
50	281.01	0.01727	8.515	250.09	924.0	1174.1	0.4110	1.2474	1.6585	50
52	283.49	0.01729	8.208	252.63	922.2	1174.8	0.4144	1.2409	1.6553	52
54	285.90	0.01731	7.922	255.09	920.5	1175.6	0.4177	1.2346	1.6523	54
56	288.23	0.01733	7.656	257.50	918.8	1176.3	0.4209	1.2285	1.6494	56
58	290.50	0.01736	7.407	259.82	917.1	1176.9	0.4240	1.2226	1.6466	58
60	292.71	0.01738	7.175	262.09	915.5	1177.6	0.4270	1.2168	1.6438	60
62	294.85	0.01740	6.957	264.30	913.9	1178.2	0.4300	1.2112	1.6412	62
64	296.94	0.01742	6.752	266.45	912.3	1178.8	0.4328	1.2059	1.6387	64
66	298.99	0.01744	6.560	268.55	910.8	1179.4	0.4356	1.2006	1.6362	66
68	300.98	0.01746	6.378	270.60	909.4	1180.0	0.4383	1.1955	1.6338	68
70	302.92	0.01748	6.206	272.61	907.9	1180.6	0.4409	1.1906	1.6315	70
72	304.83	0.01750	6.044	274.57	906.5	1181.1	0.4435	1.1857	1.6292	72
74	306.68	0.01752	5.890	276.49	905.1	1181.6	0.4460	1.1810	1.6270	74
76	308.50	0.01754	5.743	278.37	903.7	1182.1	0.4484	1.1764	1.6248	76
78	310.29	0.01755	5.604	280.21	902.4	1182.6	0.4508	1.1720	1.6228	78
80	312.03	0.01757	5.472	282.02	901.1	1183.1	0.4531	1.1676	1.6207	80
82	313.74	0.01759	5.346	283.79	899.7	1183.5	0.4554	1.1633	1.6187	82
84	315.42	0.01761	5.226	285.53	898.5	1184.0	0.4576	1.1592	1.6168	84
86	317.07	0.01762	5.111	287.24	897.2	1184.4	0.4598	1.1551	1.6149	86
88	318.68	0.01764	5.001	288.91	895.9	1184.8	0.4620	1.1510	1.6130	88
90	320.27	0.01766	4.896	290.56	894.7	1185.3	0.4641	1.1471	1.6112	90
92	321.83	0.01768	4.796	292.18	893.5	1185.7	0.4661	1.1433	1.6094	92
94	323.36	0.01769	4.699	293.78	892.3	1186.1	0.4682	1.1394	1.6076	94
96	324.87	0.01771	4.606	295.34	891.1	1186.4	0.4702	1.1358	1.6060	96
98	326.35	0.01772	4.517	296.89	889.9	1186.8	0.4721	1.1322	1.6043	98
100	327.81	0.01774	4.432	298.40	888.8	1187.2	0.4740	1.1286	1.6026	100
150	358.42	0.01809	3.015	330.51	863.6	1194.1	0.5138	1.0556	1.5694	150
200	381.79	0.01839	2.288	355.36	843.0	1198.4	0.5435	1.0018	1.5453	200
300	417.33	0.01890	1.5433	393.84	809.0	1202.8	0.5879	0.9225	1.5104	300
400	444.59	0.0193	1.1613	424.0	780.5	1204.5	0.6214	0.8630	1.4844	400
500	467.01	0.0197	0.9278	449.4	755.0	1204.4	0.6487	0.8147	1.4634	500

[a]Reprinted by permission from *Thermodynamic Properties of Steam*, by J. H. Keenan and F. G. Keyes published by John Wiley and Sons, Inc., 1936 edition.

necessary to add a correction term $\bar{h}$ as follows,

$$\bar{h} = \frac{\mu(1 - \mu)B}{1 + aW_s\,\mu} \tag{5a}$$

In Table 4 are listed values of the coefficient B and maximum values of the correction term $\bar{h}$, the latter occurring at the same values of μ as do those of the correction term $\bar{v}$.

Unfortunately, values of the entropy s of moist air per pound of dry air computed from the simple relation,

$$s = s_a + \mu s_{as} \tag{6}$$

do not approximate the true values as closely as might be desired except at temperatures considerably lower than 150 F. Only a relatively small portion of the error is contributed by the correction term

$$\bar{s} = \frac{\mu(1 - \mu)C}{1 + aW_s\,\mu} \tag{6a}$$

Table 4 lists values of the coefficient C and maximum values of the correction term $\bar{s}$, the latter occurring at the same values of μ as do those of the correction terms $\bar{v}$ and $\bar{h}$. The larger portion of the error is contributed by the so-called *mixing entropy*. It can be expressed as an additional correction term $\bar{\bar{s}}$ as follows,

$$\bar{\bar{s}} = 0.1579\,[(1 + \mu aW_s)\log_{10}(1 + \mu aW_s) - \mu aW_s \log_{10}(\mu) - \mu(1 + aW_s)\log_{10}(1 + aW_s)] \tag{6b}$$

Maximum values of $\bar{\bar{s}}$ and the values of μ at which they occur are given in Table 4. In Equation 6b $\log_{10}$ denotes logarithm to the base 10.

MOLLIER DIAGRAM

It is a fundamental proposition of thermodynamics that *when a fluid flows across a section fixed in space it convects with it an amount of energy equal to its enthalpy as determined by the pressure, temperature, and composition of the fluid at that section.* This fundamental proposition provides the correct procedure for applying the law of conservation of energy to

TABLE 4. COEFFICIENTS A, B, C APPEARING IN EQUATIONS 4a, 5a, 6a, MAXIMUM VALUES OF CORRECTIONS DEFINED BY EQUATIONS 4a, 5a, 6a. DEGREE OF SATURATION AT WHICH THESE MAXIMA OCCUR, $\bar{\mu}_m$. MAXIMUM VALUE OF CORRECTION DEFINED BY EQUATION 6b. DEGREE OF SATURATION AT WHICH THIS MAXIMUM OCCURS, $\bar{\bar{\mu}}_m$.

(*Standard Atmospheric Pressure*)

t (F)	A (ft³/lb$_a$)	B (Btu/lb$_a$)	C (Btu/F/lb$_a$)	$\bar{v}_{max}$ (ft³/lb$_a$)	$\bar{h}_{max}$ (Btu/lb$_a$)	$\bar{s}_{max}$ (Btu/F/lb$_a$)	$\bar{\mu}_m$	$\bar{\bar{s}}_{max}$ (Btu/F/lb$_a$)	$\bar{\bar{\mu}}_m$
96	0.0018	0.0286	0.00004	0.0004	0.0069	0.00001	0.4925	0.0015	0.3650
112	0.0042	0.0650	0.00009	0.0010	0.0155	0.00002	0.4878	0.0025	0.3632
128	0.0096	0.1439	0.00020	0.0022	0.0332	0.00005	0.4805	0.0040	0.3602
144	0.0215	0.3149	0.00042	0.0047	0.0693	0.00009	0.4691	0.0065	0.3557
160	0.0487	0.6969	0.00091	0.0099	0.1418	0.00019	0.4511	0.0106	0.3485
176	0.1169	1.636	0.00207	0.0207	0.2903	0.00037	0.4213	0.0179	0.3363
192	0.3363	4.608	0.00567	0.0451	0.6180	0.00076	0.3662	0.0333	0.3129

the processes occurring most frequently in air conditioning practice. Thus if moist air is flowing through a duct it carries across any section of the duct energy of amount mh Btu per minute and water of amount mW pounds per minute, if m denotes the weight of dry air crossing the section per minute.

The foregoing considerations suggest the importance of having accurate knowledge regarding the enthalpy of the fluid in question and the desirability of using enthalpy as one of the coordinates in graphical representation. The use of enthalpy h and humidity ratio W as coordinates in the case of moist air is due to Mollier [4]. A convenient modification of the Mollier diagram introduced by Goff is obtained by taking humidity ratio W as ordinate and reduced enthalpy (h-1000W) as abscissa. A Mollier Diagram modified in this way is enclosed in the envelope attached to the inside back cover and an abridgement of the Diagram is shown in Fig. 1.

The Mollier Diagram is a constant-pressure chart, the one provided with this book being drawn for standard atmospheric pressure from the data in Table 1. Along the axis of abscissae ($W = 0$, $\mu = 0$) are plotted values of the specific enthalpy of dry air h_a at one-degree intervals of temperature. Values of humidity ratio at saturation W_s plotted against values of reduced enthalpy at saturation (h_s-1000W_s) determine the saturation curve ($\mu = 100$ per cent). Lines of constant temperature connect points on the saturation curve with corresponding points on the dry-air axis and are inclined upward to the right. They are drawn straight in accordance with Equations 3 and 5 because the curvature contributed by the correction term 5a is inappreciable at all temperatures within the range of the chart. The portion of each isotherm lying between the dry-air axis and the saturation curve is divided into 10 equal parts by curves of constant per cent saturation. The per cent saturation of any point below the saturation curve is readily determined by linear interpolation along the isotherm through that point.

Each isotherm breaks at the saturation curve to incline upward to the left into the two-phase region above the saturation curve. The ordinate of a point in this region is the total weight of water in both the vapor phase (moist air) and the condensed phase (liquid or solid) per pound of dry air in both phases. Neglecting the very small amount of dissolved air in the condensed phase, it is the weight of water in both phases per pound of dry air in the vapor phase. The ordinate at the break in the isotherm through the point in question is the weight of water per pound of dry air in the vapor phase. Consequently, the difference between the two ordinates is the weight of condensed phase per pound of dry air in the vapor phase.

It has been stated that the region above the saturation curve is the two-phase region. This is so except in the wedge with apex on the saturation curve at 32 F where three distinct phases, namely, solid, liquid, and vapor coexist. In fact, this wedge separates the liquid-vapor region above the wedge from the solid-vapor region below it. A point inside the wedge divides the horizontal line extending through it from one boundary to the other into two segments which are in the same ratio as are the weights of solid and liquid. The temperature is 32 F throughout the wedge.

The isotherms in the two-phase regions above the saturation curve have been extended downward to the right into the vapor-phase region

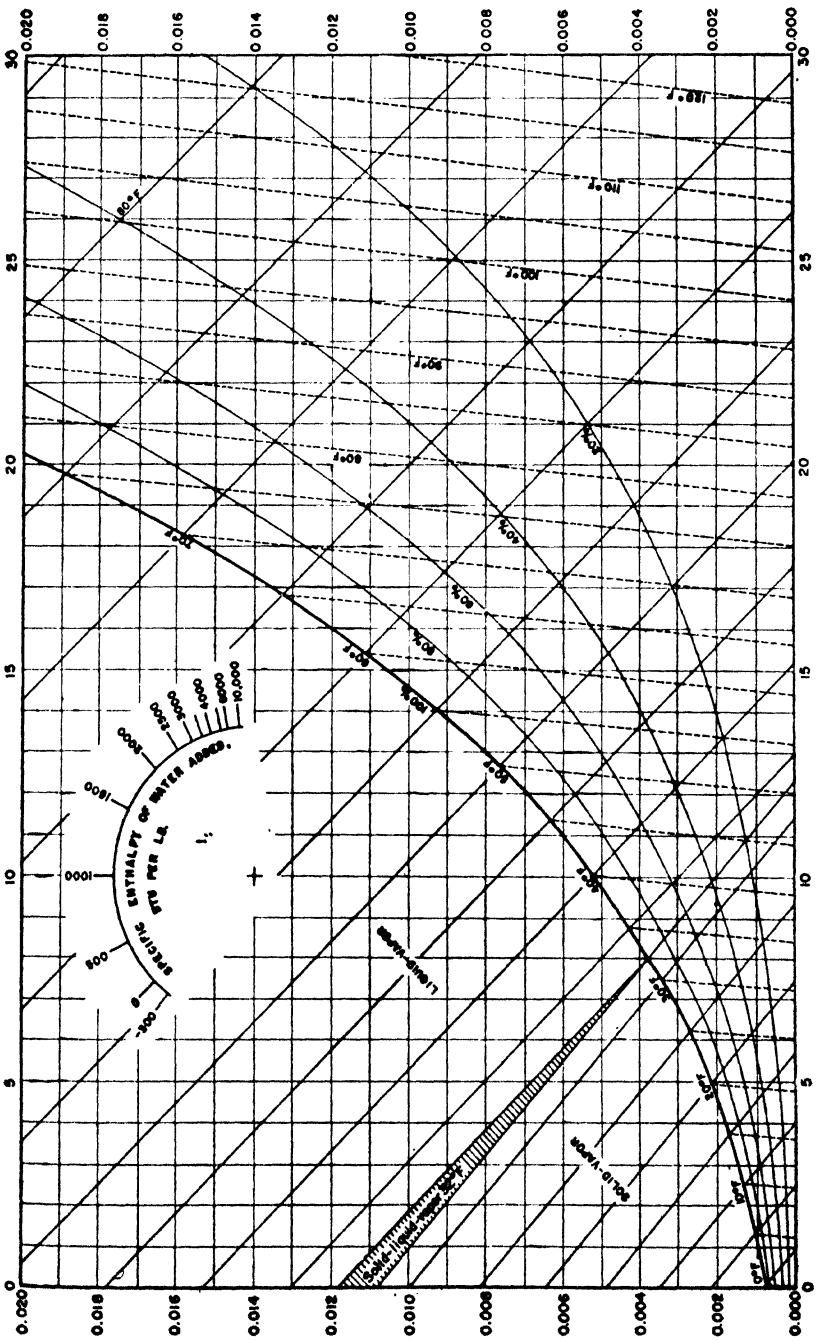

FIG. 1. ABRIDGEMENT OF MOLLIER DIAGRAM FOR MOIST AIR

below the saturation curve as lines of constant *thermodynamic wet-bulb temperature.* The definition of thermodynamic wet-bulb temperature will be given later.

On the Mollier Diagram provided with THE 1948 GUIDE there has been drawn a *protractor* from which can be determined the direction in which the state point of a mixture of water and dry air will be moved *by simultaneous addition of energy and water without addition of dry air.* A particular direction is specified by the numerical value of the *ratio of energy to water added* which ratio is designated as q and called the *specific enthalpy of water added, Btu per pound.* The protractor is useful in locating the *condition line* of a cooling load or heating load problem.

DERIVED PROPERTIES

Thermodynamic Wet-bulb Temperature. For any state of moist air there exists a temperature t^* at which liquid (or solid) water may be evaporated into the air to bring it to saturation at exactly this same temperature. The humidity ratio of the air is increased from a given initial value W to the value W_s^* corresponding to saturation at the temperature t^*; the enthalpy of the air is increased from a given initial value h to the value h_s^* corresponding to saturation at the temperature t^*; the weight of water added per pound of dry air is $W_s^* - W$ and this adds energy of amount $(W_s^* - W)\, h_w^*$, where h_w^* denotes the specific enthalpy of the water as added at the temperature t^*; therefore, if the process is strictly adiabatic,

$$h + (W_s^* - W)h_w^* = h_s^* \qquad (7)$$

The solution of Equation 7 for given values of h and W is called *thermodynamic wet-bulb temperature.*

Example 1. Find the thermodynamic wet-bulb temperature of moist air at 80 F, 50 per cent saturation, atmospheric pressure.

Solution. From the data of Table 1, the enthalpy of the air is $h = 19.221 + 0.50 \times 24.47 = 31.46$ Btu/lb$_a$ (Equation 5). To a first approximation this is the enthalpy at saturation at the thermodynamic wet-bulb temperature which is therefore approximately 67 F.

At 67 F the humidity ratio at saturation is 0.01424 lb$_w$/lb$_a$ and the specific enthalpy of liquid water is 35.11 Btu/lb$_w$. The humidity ratio of the air is $W = 0.50 \times 0.02233 = 0.01117$ lb$_w$/lb$_a$ (Equation 3). Therefore, to a second approximation, the enthalpy at saturation at the thermodynamic wet-bulb temperature is $h_s^* = 31.46 + (0.01424 - 0.01117) \times 35.11 = 31.57$ Btu/lb$_a$, Equation 7. Interpolation in Table 1 gives as final answer,

$$t^* = 66.94 \text{ F}$$

The answer can also be read directly on the Mollier Diagram at the intersection of the 80 F dry-bulb and 50 per cent saturation lines.

The psychrometer is an instrument consisting of two thermometers one of which has the bulb covered with a suitable wick that has been dipped in liquid water and thoroughly wetted by it. On placing the wet-bulb of the instrument in an air stream, the liquid begins to evaporate from the wick and it is usually assumed that such evaporation brings the air immediately adjacent to the wick to saturation. At first this air may reach saturation at a higher or lower temperature than that of the liquid on the wick; but in a relatively short time the temperature of the liquid will have changed to approach equality with that of the air touching the wick, even if this requires the liquid to freeze on the wick. Then the liquid (or solid) will continue for a time to evaporate into the air stream at such temperature as will bring a portion of the air stream to saturation

at this same temperature. This equilibrium temperature is called *wet-bulb temperature.*

It is clear that the readings of an actual wet-bulb thermometer cannot be regarded as values of a thermodynamic property of moist air; for these readings are importantly affected by a number of non-thermodynamic factors including design, construction, installation, and technique of using the instrument. Thus, unless the wet-bulb is effectively shielded against radiation from relatively warm surfaces the process will not be strictly adiabatic as tacitly assumed in writing Equation 7. Also, partial drying of the wick will prevent the air immediately adjacent to it from reaching complete saturation as assumed in Equation 7. A working theory developed by Arnold [5] enables the calculation of corrections to be applied to the readings of the actual instrument in order to make them agree with the values of temperature calculated from Equation 7. Fortunately, and indeed fortuitously, these corrections can be made small, but to emphasize the necessity of making them in accurate experimentation, the temperature defined by Equation 7 is called *thermodynamic wet-bulb temperature.*

Example 2. Find the degree of saturation of moist air at 90 F dry-bulb, 63 F thermodynamic wet-bulb, atmospheric pressure.

Solution. Inserting numerical data from Table 1 into Equation 7 gives

$$(21.625 + 34.31\mu) + (0.01235 - 0.03118\mu) \times 31.12 = 28.57$$

The solution of this equation is direct and the final answer is

$$\mu = 19.67 \text{ per cent}$$

The per cent saturation may also be read directly at intersection of 90 F dry-bulb and 63 F thermodynamic wet-bulb lines on the Mollier Diagram.

Example 3. Find the temperature to which moist air initially saturated at 40 F and at standard atmospheric pressure must be heated in order to have a thermodynamic wet-bulb temperature of 60 F.

Solution. On the Mollier Diagram follow a horizontal line from the saturation curve at 40 F to its intersection with the 60 F thermodynamic wet-bulb line and read the corresponding temperature directly.

Inserting numerical data from Table 1 into Equation 7, this becomes

$$h_a + 0.005213 h_{as}/W_s = 26.46 - (0.01108 - 0.005213) \times 28.12 = 26.295$$

At 85 F the lefthand member of this equation has the value 26.147; at 86 F its value is 26.389; by linear interpolation the answer is: $t = 85.61$ F.

Dew-Point Temperature. Corresponding to any given state of moist air there exists another state on the saturation curve having the same humidity ratio W and same pressure p as the given state. The temperature at this other state on the saturation curve is called the *dew-point temperature* of the given state. Obviously, if moist air is cooled at constant pressure and constant humidity ratio it will reach saturation when its temperature falls to a value equal to its dew-point temperature. This will usually be marked by the first appearance of a coexisting condensed phase. In one type of dew-point apparatus a continuous sample of air is passed over a mirror which can be cooled by external refrigeration and whose temperature can be accurately measured. The measured temperature at which the intensity of light reflected from the mirror is abruptly diminished by condensation is taken to be the dew-point temperature of the air sample. Examples 4 and 5 illustrate the relation between the dew-point, degree of saturation and dry-bulb temperature.

Example 4. Find the dew-point temperature of moist air at 80 F, 50 per cent saturation, atmospheric pressure.

Solution. On the Mollier Diagram follow a horizontal line from a given state point (80 F, 50 per cent) to the saturation curve and read the temperature at the intersection.

To solve from Table 1:

From the data in Table 1, the humidity ratio of the air is $W = 0.50 \times 0.02233 = 0.01117$ lb_w/lb_a. By interpolation this is found to be the humidity ratio at saturation at 60.22 F which is therefore the required answer.

Example 5. Find the degree of saturation of moist air at 90 F dry-bulb, 40 F (dew-point), atmospheric pressure.

Solution. On the Mollier Diagram follow a horizontal line from 40 F on the saturation curve to the 90 F isotherm (dry-bulb) and read the degree of saturation directly.

To solve from Table 1:

From the data in Table 1, the humidity ratio of the air must be $W = 0.005213$. But the humidity ratio at saturation at 90 F is 0.03118; hence the degree of saturation is

$$\mu = 0.005213/0.03118 = 16.72 \text{ per cent}$$

TYPICAL AIR CONDITIONING PROCESSES

The use of Table 1 and the Mollier Diagram in analyzing typical air conditioning processes is best explained by means of illustrative examples. In each of the following, it is to be understood that the process in question takes place at a constant pressure of 29.921 in. Hg, or standard atmospheric pressure.

Heating

The process of adding heat to moist air is represented by a horizontal line on the Mollier Diagram. The length of the line between the initial and final state points is the increase of reduced enthalpy; but, since the humidity ratio is constant, it is also the increase of enthalpy itself and therefore the quantity of heat added per pound of dry air.

Example 6. Air initially at 20 F, 80 per cent saturation is heated to 120 F. Find the quantity of heat required to process 20,000 cfm of heated air.

Solution. From the data in Table 1: the initial humidity ratio is $0.80 \times 0.002152 = 0.001722$ lb_w/lb_a; the initial enthalpy is $4.804 + 0.80 \times 2.302 = 6.646$ Btu/lb_a; the final degree of saturation is $0.001722/0.08149 = 2.113$ per cent; the final enthalpy is $28.841 + 0.02113 \times 90.70 = 30.757$ Btu/lb_a.

It may be supposed that the air is heated between two sections of a duct. The quantities of energy convected across the two sections per pound of dry air crossing them are the two enthalpies calculated. Conservation of energy requires that the difference between these two enthalpies be the quantity of heat added; thus,

$$_AQ_B = 30.757 - 6.646 = 24.111 \text{ Btu/lb}_a.$$

The final volume is $14.611 + 0.02113 \times 1.905 = 14.651$ cu ft/lb_a. Since 20,000 cfm of heated air is to be processed, the total quantity of heat required is

$$_AQ_B = 24.111 \times 20{,}000/14.651 = 32{,}914 \text{ Btu per minute.}$$

On the Mollier Diagram the process is represented by the horizontal line AB, Fig. 2, whose length is the quantity of heat added per pound of dry air. The reduced enthalpy at A is 4.92 while that at B is 29.03, both being read directly from the chart. Since humidity ratio is constant the difference between these reduced enthalpies is also the difference between the enthalpies themselves, namely, 24.11 Btu/lb_a.

Cooling

The process of cooling moist air is also represented by a horizontal line on the Mollier Diagram. The line may extend across the saturation curve into the two-phase region, nevertheless, the length of the line between

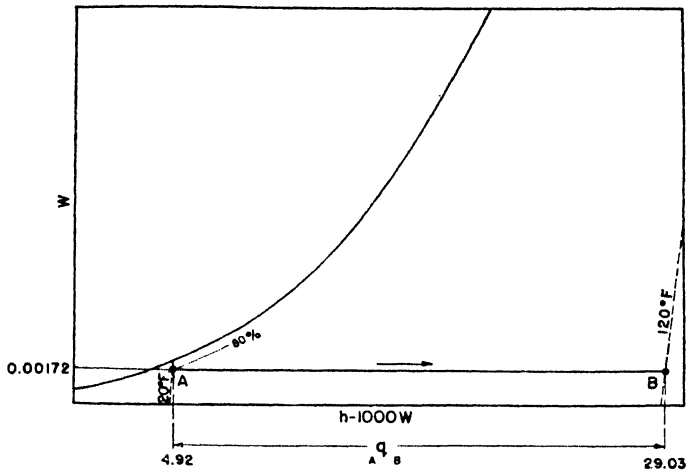

FIG. 2. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 6

the initial and final states is the quantity of heat removed, or refrigeration supplied, per pound of dry air. By following the final isotherm downward to the right to the saturation curve and reading the ordinate there, the weight of water vapor per pound of dry air in the vapor phase is determined. The difference between the initial humidity ratio and this ordinate is the weight of condensed phase per pound of dry air in the final state.

Example 7. Air at 95 F and 50 per cent saturation is cooled to 70 F. Find the refrigeration required to process 20,000 cfm of uncooled air.

Solution. From the data in Table 1: the initial humidity ratio is $0.50 \times 0.03673 = 0.01837$ lb_w/lb_a; the initial enthalpy is $22.827 + 0.50 \times 40.49 = 43.072$ Btu/lb_a; the humidity ratio at saturation at the final temperature is 0.01582 lb_w/lb_a; the quantity of liquid formed is $0.01837 - 0.01582 = 0.00255$ lb_w/lb_a; the enthalpy of the final two-phase mixture is $34.09 + 0.00255 \times 38.11 = 34.187$ Btu/lb_a.

It may be supposed that the air is cooled between two sections of a duct. The quantities of energy convected across the two sections per pound of dry air crossing them

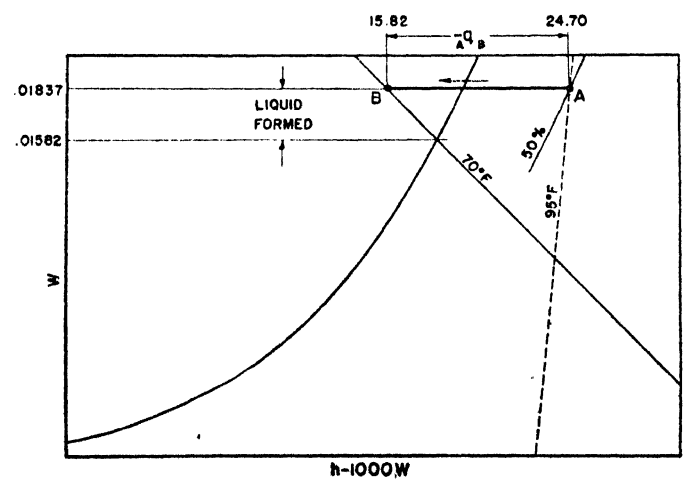

FIG. 3. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 7

are the two enthalpies calculated. Conservation of energy requires that the difference between these two enthalpies be the quantity of heat removed, or refrigeration supplied, between the two sections. Therefore,

$$-{}_AQ_B = 43{,}072 - 34.187 = 8.885 \text{ Btu/lb}_a$$

The initial volume is $13.980 + 0.50 \times 0.822 = 14.391$ cu ft/lb$_a$. Since 20,000 cfm of air is to be processed, the total refrigeration required is

$$-{}_AQ_B = 8.885 \times 20{,}000 \div 14.391 = 12{,}348 \text{ Btu per minute.}$$

On the Mollier Diagram the process is represented by the horizontal line AB, Fig. 3, whose length is the quantity of refrigeration required per pound of dry air.

Adiabatic Mixing of Two Air Streams

A typical air conditioning process requiring special analysis is the adiabatic mixing of two air streams. Referring to Fig. 4, let m_1, m_2, m_3 denote the weights of dry air convected across sections F_1, F_2, F_3, respectively, per minute. Then m_1W_1, m_2W_2, m_3W_3 and m_1h_1, m_2h_2, m_3h_3 will

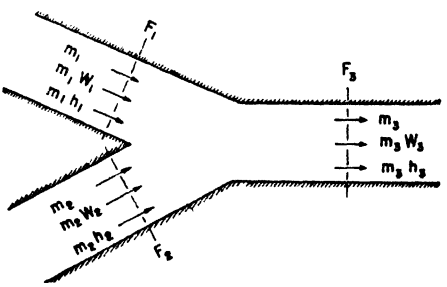

FIG. 4. ADIABATIC MIXING OF 2 AIR STREAMS

denote the weights of water and the quantities of energy similarly convected. If the mixing is adiabatic, it must be governed by the three equations,

$$\begin{aligned} m_1 + m_2 &= m_3 \\ m_1W_1 + m_2W_2 &= m_3W_3 \\ m_1h_1 + m_2h_2 &= m_3h_3 \end{aligned} \tag{8}$$

Elimination of m_3 gives,

$$\frac{h_2 - h_3}{h_3 - h_1} = \frac{W_2 - W_3}{W_3 - W_1} = \frac{m_1}{m_2} \tag{9}$$

according to which: *on the Mollier Diagram the state point of the resulting mixture lies on the straight line connecting the state points of the two streams being mixed and divides the line into two segments which are in the same ratio as are the weights of dry air in the two streams.*

Example 8. Outside Air at 0 F and 80 per cent saturation is to be mixed adiabatically with recirculated Inside Air at 70 F and 20 per cent saturation in the ratio of one pound of dry air in the former to seven in the latter. Find the temperature and degree of saturation of the resulting mixture.

Solution. The humidity ratio W_3 and the enthalpy h_3 of the resulting mixture must satisfy Equations 9, namely,

$$\frac{0.003164 - W_3}{W_3 - 0.000630} = \frac{20.270 - h_3}{h_3 - 0.668} = \frac{1}{7}$$

from which: $W_3 = 0.002847$, $h_3 = 17.820$. At the temperature of the resulting mixture, therefore,

$$h_a + 0.002847\, h_{as}/W_s = 17.820$$

At 61 F the lefthand member of this equation has the value 17.750; at 62 F its value is 17.991; by interpolation the temperature of the resulting mixture is 61.29 F where the humidity ratio at saturation, also by interpolation, is 0.01161; hence the degree of saturation of the resulting mixture is

$$\mu = 0.002847 \div 0.01161 = 24.52 \text{ per cent}$$

On the Mollier Diagram, Fig. 5, a straight line is drawn between point 1 (0 F, 80 per cent) and point 2 (70 F, 20 per cent); then point 3 is located on the line one-eighth of the distance from point 2 to point 1. The temperature and degree of saturation at point 3 are read directly.

Adiabatic Mixing with Injected Water

Another typical air conditioning process is that of injecting water into an air stream to mix with it adiabatically. Let $W_2 - W_1$, denote the increase in humidity ratio of the air; this is obviously the quantity of water injected per pound of dry air; it follows that the quantity of energy injected per pound of dry air is $(W_2 - W_1)h_w$, where h_w denotes the specific enthalpy of the water as injected; if the process is adiabatic this produces an equal increase in the enthalpy of the air, namely, $h_2 - h_1$; therefore,

$$h_2 - h_1 = h_w(W_2 - W_1) \tag{10}$$

according to which: *the process of injecting water into an air stream to mix adiabatically with it is represented by a straight line on the Mollier Diagram whose direction is fixed by the specific enthalpy of the water as injected.* The protractor drawn on the Mollier Diagram provided with this book provides a convenient means for determining this direction.

Example 9. It is desired to increase the humidity ratio of air at 70 F dry-bulb, without changing its temperature. Under what conditions may water be injected in order to accomplish the desired result?

Solution. At 70 F the increase of enthalpy per unit increase of humidity ratio is $h_{as}/W_s = 17.27 \div 0.01582 = 1092$ Btu per pound of water. This must be the specific enthalpy of the water added if the state point of the air is to be moved along the 70 F isotherm. Saturated steam at 668 F has this specific enthalpy[3].

On the Mollier Diagram, Fig. 6, it is seen that the 70 F isotherm is parallel to the line on the protractor for a specific enthalpy of 1092 Btu per pound.

Adiabatic Saturation

Any process by which the state point of moist air is moved to the saturation curve adiabatically may properly be called adiabatic saturation.

Example 10. Liquid water chilled to 35 F is evaporated into an air stream initially at 90 F and 50 per cent saturation. How much water must be evaporated to bring the air to saturation at what temperature?

Solution. The initial enthalpy of the air is $21.625 + 0.50 \times 34.31 = 38.780$ Btu/lb$_a$; the initial humidity ratio is $0.50 \times 0.03118 = 0.01559$ lb$_w$/lb$_a$; the specific enthalpy of the chilled water is 3.06 Btu/lb$_w$; therefore, the temperature at which the air reaches the saturation curve must be such that the enthalpy h_s and humidity ratio W_s at saturation satisfy the equation,

$$h_s - (W_s - 0.01559) \times 3.06 = 38.780$$

The solution is 75.19 F where the humidity ratio at saturation is 0.01894; consequently,

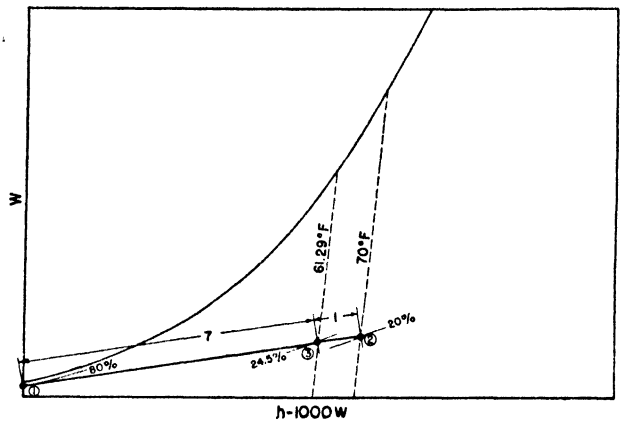

FIG. 5. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 8

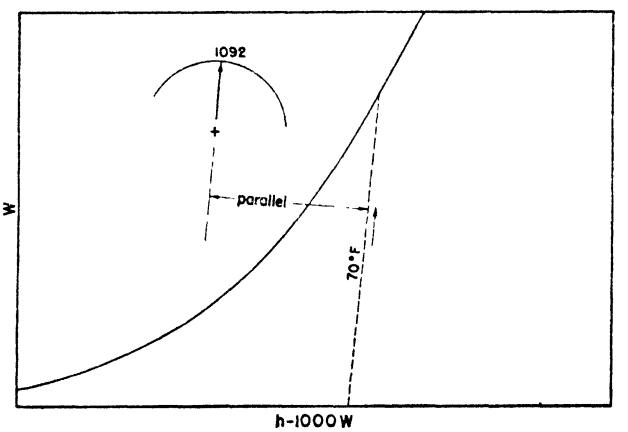

FIG. 6. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 9

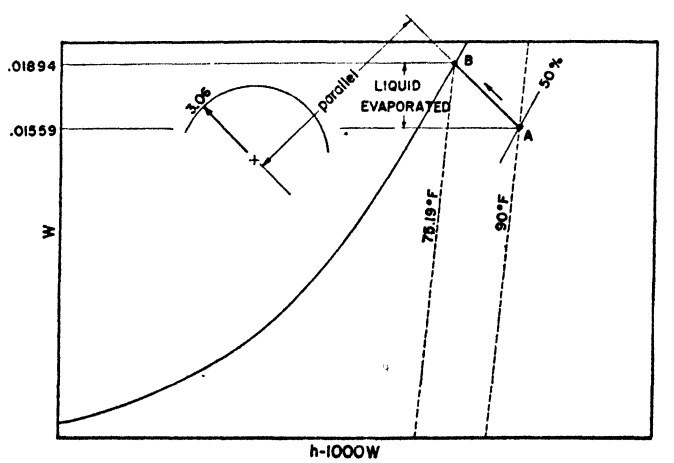

FIG. 7. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 10

the weight of water evaporated is 0.01894 − 0.01559 = 0.00335 lb per pound of dry air.

On the Mollier Diagram, Fig. 7, a line is drawn through the initial state point (90 F, 50 per cent saturation) in the direction given by the protractor for a specific enthalpy of 3.06 Btu/lb_w.

If air is saturated adiabatically with spray water which is recirculated, the water will ultimately assume a temperature such that the air is brought to saturation at exactly the same temperature; that is, the water will assume the thermodynamic wet-bulb temperature of the air.

Example 11. Air at 75 F and 60 per cent saturation is saturated adiabatically with recirculated spray water. Find the resulting temperature and the weight of water added per pound of dry air.

Solution. In view of the foregoing remarks the solution of this example reduces to the determination of the thermodynamic wet-bulb temperature of the air. Its humidity

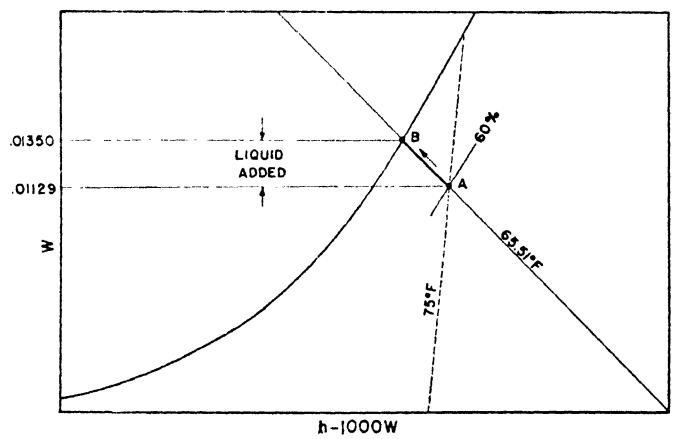

FIG. 8. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 11

ratio is 0.60 × 0.01882 = 0.01129; its enthalpy is 18.018 + 0.60 × 20.59 = 30.372; Equation 7 defining thermodynamic wet-bulb temperature becomes

$$h_s^* - (W_s^* - 0.01129)h_w^* = 30.372$$

At 65 F the value of the lefthand member is 29.995; at 66 F its value is 30.746; by interpolation the thermodynamic wet-bulb temperature is 65.51 F where the humidity ratio at saturation is 0.01350; consequently the weight of water added is 0.01350 − 0.01129 = 0.00221 lb per pound of dry air.

On the Mollier Diagram, Fig. 8, the process is represented by the line AB which is a segment of the 65.51 F thermodynamic wet-bulb line. The difference between the ordinates at B and at A is the weight of water added per pound of dry air.

Cooling Load

The problem of calculating the cooling load for an air conditioned space usually reduces to the determination of the quantity of *inside air* that must be withdrawn and the condition to which it must be brought by suitable processing so that its return to the conditioned space will have the net effect of removing given amounts of energy and water from the space.

Let M denote the weight of dry air withdrawn with *inside air* per hour. With it will be withdrawn energy of amount Mh_1 and water of amount

MW_1 per hour, where h_1 and W_1 denote the enthalpy and humidity ratio of the *inside air*, respectively. The weight of dry air returned with the *conditioned air* will necessarily be the same as that withdrawn with the *inside air*, but with it must be returned a smaller quantity of energy Mh and a smaller quantity of water MW. Let ΔQ and ΔW denote the given amounts of energy and water to be removed from the conditioned space per hour; then

$$Mh = Mh_1 - \Delta Q$$
$$MW = MW_1 - \Delta W$$

Eliminating M and letting q denote the ratio of energy removed to water removed, that is, $q = \Delta Q/\Delta W$,

$$\frac{h - h_1}{W - W_1} = q \tag{11}$$

according to which: *all possible states for the conditioned air lie on a straight line on the Mollier Diagram passing through the state point of the inside air in the direction specified by the numerical value of the ratio q.* This line is called the *condition line* for the given problem. If the condition line crosses the saturation curve, the point of intersection is called the *apparatus dew-point* for the given problem.

The protractor on the Mollier Diagram facilitates the drawing of the condition line and the locating of the apparatus dew-point. For this purpose the numerical value of the ratio q is to be regarded as a value of the *specific enthalpy of water added, Btu per pound.*

Example 12. A condition of 80 F dry-bulb, and 67 F thermodynamic wet-bulb, is to be maintained in a clothing store, outside conditions being 95 F dry-bulb, and 75 F thermodynamic wet-bulb. The energy gain from normal heat transmission is estimated at 16,000 Btu per hour, that from solar radiation at 48,000 Btu per hour. The energy generated by lights, fans, etc. is estimated at 13,900 Btu per hour. The ventilation requirement is 30,000 cu ft per hour. The number of occupants is 50. Find the apparatus dew-point.

Solution. The properties of *inside air* and *outside air* are readily calculated from the data in Table 1, see especially Example 2.

		Inside Air	Outside Air
μ	=	0.5024	0.3848
h	=	31.514	38.408
W	=	0.01122	0.01413
v	=	.....	14.296

The weight of dry air entering with the *ventilating air* is 30,000/14.296 = 2098.5 lb per hour which brings with it energy of amount 2098.5 × 38.408 = 80.595 Btu per hour and water of amount 2098.5 × 0.01413 = 29.659 lb per hour.

The weight of dry air displaced from the store by the *ventilating air* is 2098.5 lb per hour which takes with it energy of amount 2098.5 × 31.514 = 66,132 Btu per hour and water of amount 2098.5 × 0.01122 = 23.541 lb per hour.

Each occupant may be regarded as a normal person standing at rest and evaporating (1386 grains) 0.198 lb of water per hour (value obtained by interpolation between Curves D and C Fig. 7, Chapter 12) at about 79 F. From this source there is water of amount 50 × 0.198 = 9.90 lb per hour and energy of amount 9.90 × 1095.7 = 10,847 Btu per hour added to the conditioned space. In addition each occupant loses 225 Btu per hour by conduction, convection, and radiation, making a total for 50 persons of 11,300 Btu per hour.

The net energy gain is 16,000 + 48,000 + 13,900 + 80,595 − 66,132 + 10,847 + 11,300 = 114,510 Btu per hour. The net water gain is 29.659 − 23.541 + 9.90 = 16.018 lb per hour. Accordingly the direction of the condition line is fixed by the ratio, q = 114,510 ÷ 16.018 = 7148.8 Btu per pound of water.

On the Mollier Diagram, Fig. 9, the direction of the condition line is given by the protractor for a *specific enthalpy of water added* of 7148.8 Btu per pound. The line itself

passes through the state point of the inside air and intersects the saturation curve at the apparatus dew-point.

According to Equation 11 the enthalpy h_s and humidity ratio W_s at the apparatus dew-point must satisfy the equation

$$7148.8W_s - h_s = 7148.8 \times 0.01122 - 31.514 = 48.681$$

At 58 F the left-hand member has the value 48.513; at 59 F its value is 50.641; by interpolation the apparatus dew-point is 58.08 F.

It would be a mistake to assume that the refrigeration to be supplied is equal to the net energy to be removed; for in general water is to be removed simultaneously and unless this is removed as liquid at 32 F it will automatically take some energy with it. Thus, unless the water is removed as solid (ice) the refrigeration to be supplied will be somewhat less than the net energy to be removed.

Example 13. Referring to the cooling load problem of Example 12, suppose that the conditioning process consists of cooling a portion of the *inside air* to the apparatus dew-point temperature, separating out the liquid thus formed, and returning the resulting saturated mixture to the conditioned space. Find the quantity of *inside air* that must be processed in this manner and the corresponding quantity of refrigeration required.

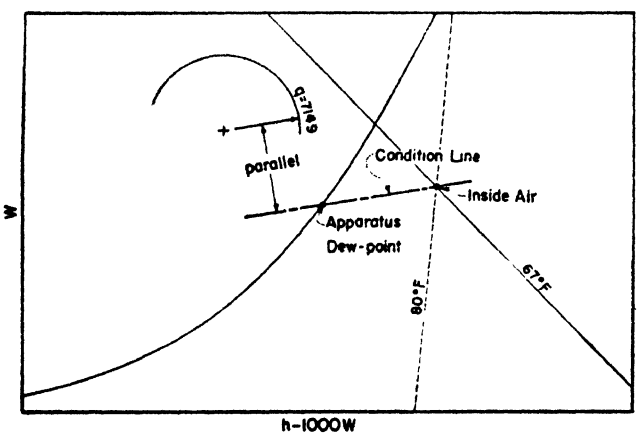

FIG. 9. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 12

Solution. During the cooling operation the enthalpy of the inside air is reduced to the value,

$$h = 25.17 + (0.01122 - 0.01033) \times 26.20 = 25.193$$

where 25.17 and 0.01033 are the values of enthalpy and humidity ratio at saturation at the apparatus dew-point temperature and 26.20 is the specific enthalpy of liquid water at that temperature. It follows that the quantity of refrigeration required is 31.514 − 25.193 = 6.321 Btu per pound of dry air.

The *inside air* being processed leaves the store with an enthalpy of 31.514 and is returned with an enthalpy of 25.17; it therefore removes energy of amount 6.344 Btu per pound of dry air. This means that the weight of dry air involved in the process is 114,510/6.344 = 18,050 lb per hour and that the total refrigeration to be supplied is 18,050 × 6.321 = 114,090 Btu per hour, or 9.508 tons.

The quantity of liquid separated out during the conditioning process is 18,050 × (0.01122 − 0.01033) = 16.018 lb per hour as required. In leaving the apparatus it takes with it energy of amount 16.018 × 26.20 = 420 Btu per hour. This plus the refrigeration accounts for the total energy removal of 114,510 Btu per hour as required.

On the Mollier Diagram, Fig. 10, the cooling operation is represented by line AB whose length is the quantity of refrigeration per pound of dry air; the separation of the liquid

formed in the cooling operation is represented by line BC whose projection on the ordinate axis is the quantity of liquid so separated per pound of dry air. Point C is the apparatus dew-point and lies on the condition line as required.

In practice it may not be feasible to choose the apparatus dew-point as the point on the condition line to which to condition the *inside air* because to do so would require an excessive number of air changes in the given space. Or it may be that the condition line does not cross the saturation curve at all so that the apparatus dew-point as defined does not exist. Finally, it is rarely possible to obtain complete saturation in conventional air conditioning apparatus. Nevertheless the requirements of the cooling load problem can be exactly met if the conditioned air is brought to *any* point on the condition line of the problem.

Heating Load

The condition line is also useful in the analysis of heating load problems as may best be illustrated by means of an illustrative example.

Example 14. A certain space is to be maintained at 70 F and 50 per cent saturation with outside conditions at 0 F and 80 per cent saturation. The normal heat transmission through walls, partitions, floor, roof, glass and doors is estimated at 75,000 Btu per hour. Energy gained from lights and appliances is estimated at 15,000 Btu per hour.

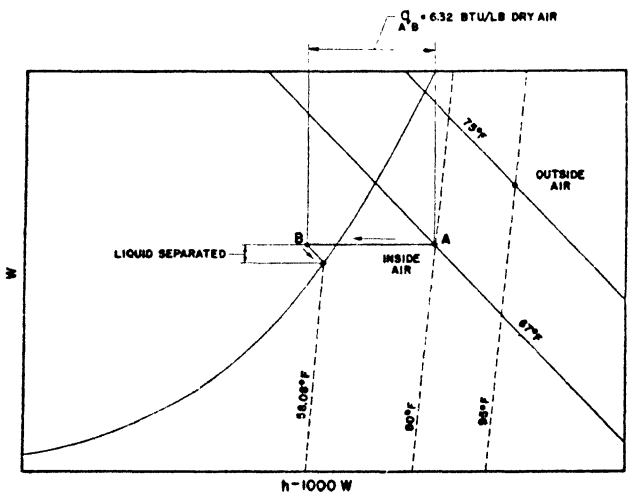

FIG. 10. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 13

Energy and water gains from occupants are to be disregarded in the calculations. Double doors and windows are used so that infiltration is negligible. The ventilation requirement is 30,000 cu ft per hour of *outside air*.

The requirements of the problem are to be met in the following manner; preheat the *ventilating air*; mix it adiabatically with recirculated *inside air*; saturate the mixture adiabatically with recirculated spray water; heat the resulting mixture to 105 F and return it to the conditioned space as *supply air*.

Analysis. Every pound of dry air admitted to the system (air conditioned space plus air conditioning apparatus) with the *ventilating air* displaces a pound of dry air from the system with *inside air*. Since the *ventilating air* is not admitted directly to the space, then for every pound of dry air withdrawn with *inside air* there is a pound of dry air returned with *supply air*. This has to have the net effect of adding energy of amount 60,000 Btu per hour and water of amount *zero* pounds per hour. Thus the ratio q determining the direction of the condition line is infinite, which means that the condition line is horizontal as indicated by the protractor on the Mollier Diagram.

The properties of *inside air* are: $h = 25.451$, $W = 0.007910$. Since the state point of the *supply air* must be on the condition line at 105 F, its properties are: $h = 33.986$,

$W = 0.007910$. Therefore the weight of dry air withdrawn with *inside air* and returned with *supply air* is 60,000 ÷ (33.986 − 25.451) = 7029.9 lb per hour.

The properties of *outside air* are: $h = 0.668$, $W = 0.0006298$, $v = 11.590$. Therefore the weight of dry air introduced into the system with the *ventilating air* is 30,000 ÷ 11.590 = 2588.4 lb per hour. This *ventilating air* is to be mixed adiabatically with *inside air* containing 7029.9 − 2588.4 = 4441.5 lb of dry air per hour; therefore, the humidity ratio of the mixture must be (2588.4 × 0.0006298 + 4441.5 × 0.007910) ÷ 7029.9 = 0.005229.

The condition line crosses the saturation curve at 50.86 F where the enthalpy is 20.782 and the humidity ratio is 0.007910. This is the state point to be reached by adiabatic saturation of the mixture of *ventilating air* and *inside air* with recirculated spray water. Accordingly, the state point of the mixture must lie on the 50.86 F thermodynamic wet-bulb line so that its enthalpy must have the value,

$$h = 20.782 - (0.007910 - 0.005229) \times 18.97 = 20.731$$

This requires that the enthalpy of the preheated *ventilating air* have the value,

$$h = (7029.9 \times 20.731 - 4441.5 \times 25.451) \div 2588.4 = 12.632$$

Since the humidity ratio of the preheated *ventilating air* is known to be 0.0006298, its temperature is readily found to be 49.75 F.

The quantity of heat required for preheating the *ventilating air* is 2588.4 × (12.632 − 0.668) = 30,968 Btu per hour; that to be added to the *supply air* is 7029.9 × (33.986 −

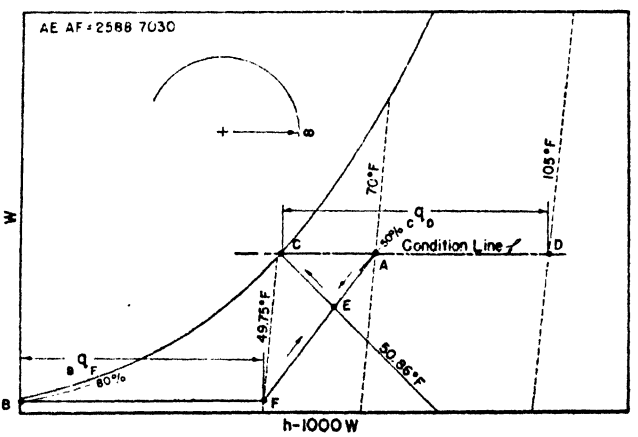

FIG. 11. ILLUSTRATION OF USE OF MOLLIER DIAGRAM IN SOLUTION OF EXAMPLE 14

20.782) = 92,823 Btu per hour; the energy added with the spray water is 7029.9 × 18.97 × (0.007910 − 0.005229) = 357 Btu per hour; that introduced into the system with the *ventilating air* is 2588.4 × 0.668 = 1729 Btu per hour; that carried out of the system with the *inside air* displaced by the *ventilating air* is 2588.4 × 25.451 = 65,877 Btu per hour; therefore, the net energy added to the system is 30,968 + 92,823 + 357 + 1729 − 65,877 = 60,000 Btu per hour as required.

On the Mollier Diagram, Fig. 11, point A is the state point of the *inside air*. The condition line is horizontal so that point D is the state point of the *supply air*. The condition line crosses the saturation curve at point C so that the state point of the mixture of preheated *ventilating air* and *inside air* before adiabatic saturation with recirculated spray water must lie somewhere on the thermodynamic wet-bulb line through C. The state point of the *ventilating air* is point B, hence that of the preheated *ventilating air* must lie somewhere on the horizontal line through B. Its exact location is determined graphically by finding the straight line AF which is cut by the thermodynamic wet-bulb line through C into two segments such that AE : AF = 2588.4 : 7029.9. The length of the line BF is the quantity of heat required for preheating the *ventilating air* per pound of dry air; the length of the line CD is the quantity of heat to be added to the *supply air*, per pound of dry air.

WET-BULB TEMPERATURES BELOW 32F

A condition in which the water evaporating from the wick of a wet-bulb thermometer remains liquid at 32 F or lower is one of metastable equilibrium and should therefore not be expected to occur in practice. The evidence that it does sometimes occur appears to be indirect and inconclusive. Stable equilibrium requires that the water freeze at 32 F or lower and is the condition to be expected in practice. On the Mollier Diagram the lines of constant thermodynamic wet-bulb temperature have been drawn for stable equilibrium only. In other words it has been assumed that the water evaporating from the wick of the wet-bulb thermometer freezes when its temperature falls to 32 F or lower.

Example 15. Find the temperature at which dry air has a thermodynamic wet-bulb temperature of 32 F.

Solution. If it is assumed that the water evaporating from the wick of the wet-bulb thermometer remains liquid, the specific enthalpy of the dry air must have the value

$$h_a = 11.758 - 0.04 \times 0.003788 = 11.758$$

corresponding to which the temperature is 48.95 F. On the other hand if it is assumed that the water freezes, the specific enthalpy of the dry air must have the value,

$$h_a = 11.758 + 143.36 \times 0.003788 = 12.301$$

corresponding to which the temperature is 51.21 F. The second assumption is the assumption of stable equilibrium and should be expected to represent the actual situation.

The corresponding answer, namely 51.21 F, is the one given by the Mollier Diagram at intersection of 32 F thermodynamic wet-bulb and 0 per cent saturation.

DALTON'S RULE

As stated in the introduction the thermodynamic properties of moist air have hitherto been obtained from those of dry air and water vapor separately by application of Dalton's Rule. Actual departures from the rule are due principally, but not entirely, to intermolecular forces; therefore, in order to apply the rule with any measure of consistency it is necessary to idealize the situation by assuming that the effects of such intermolecular forces are negligible and that both the dry air and the water vapor behave like perfect gases. Making this assumption, the volume v_T occupied by n_a mols of dry air at temperature T and pressure p_a is $v_T = n_a RT/p_a$ while that occupied by n_w mols of water vapor at the same temperature but at pressure p_w is $v_T = n_w RT/p_w$. According to Dalton's Rule, if the dry air and water vapor are mixed, each occupies the whole volume of the mixture at the temperature of the mixture and the pressure of the mixture is the sum of the individual pressures. Mathematically,

$$v_T = \frac{n_a RT}{p_a} = \frac{n_w RT}{p_w} = \frac{(n_a + n_w)RT}{p} \tag{12}$$

It follows from these equations that the so-called *partial* pressure of each constituent is its mol-fraction times the observed pressure of the mixture; thus, for water vapor,

$$p_w = \frac{n_w}{n_a + n_w} p \tag{13}$$

and similarly for dry air. Equation 13 may be regarded as the Dalton Rule definition of partial pressure in terms of the observable terms n_a, n_w, p.

The humidity ratio W is the mol ratio n_w/n_a times the ratio of molecular weights, namely, 18.016/28.966 = 0.6220; hence Equation 13 can be written

$$W = 0.6220 \frac{p_w}{p - p_w} \tag{14}$$

Now, even if it is assumed that both the dry air and the water vapor behave like perfect gases, it does not follow that at saturation the *partial* pressure of the water vapor can be put equal to the saturation pressure of pure water at the temperature of the mixture because: (1) the coexisting liquid (or solid) phase is not pure water but contains a small amount of dissolved air, and (2) the coexisting liquid (or solid) phase has to support the observed pressure p and not just the saturation pressure p_s of pure water. These effects are calculable but are in general smaller than the effects of intermolecular forces which have already been ignored. Besides, the only legitimate reason for retaining Dalton's Rule is to gain simplicity; hence these effects should be disregarded also, and the humidity ratio at saturation estimated as follows,

$$W_s = 0.6220 \frac{p_s}{p - p_s} \tag{15}$$

In this chapter the ratio W/W_s has been called degree of saturation and denoted by the greek letter μ. The ratio p_w/p_s has long been called *relative humidity* and will be denoted by the Greek letter φ. Equations 14 and 15 can be combined to give

$$\mu = \varphi \frac{1 - p_s/p}{1 - \varphi p_s/p} \tag{16}$$

which can be inverted to give

$$\varphi = \frac{\mu}{1 - (1 - \mu)p_s/p} \tag{17}$$

Example 16. Find the relative humidity of moist air at 180 F, 20 per cent saturation.

Solution. Inserting numerical data from Table 1 into Equation 17, the answer is

$$\varphi = \frac{0.20}{1 - 0.80 \times 15.294/29.921} = 0.3384$$

Example 17. Find the degree of saturation of moist air at 70 F, 50 per cent relative humidity.

Solution. Inserting numerical data from Table 1 into Equation 16, the answer is

$$\mu = 0.50 \frac{1 - 0.73915/29.921}{1 - 0.50 \times 0.73915/29.921} = 0.4937$$

The foregoing examples show that there is a substantial difference between degree of saturation and relative humidity, particularly at higher temperatures. Of course, they both have the value zero for dry air and the value unity for saturated moist air regardless of the temperature.

A Dalton Rule expression for the volume of moist air per pound of dry air obtainable directly from Equation 12 is

$$v = \left(\frac{R_a T}{p}\right) + \mu \left(\frac{W_s R_w T}{p}\right) \tag{18}$$

where

R_a = gas constant for dry air = 1545.31 ÷ 28.966 = 53.349 (ft/F).

R_w = gas constant for water vapor = 1545.31 ÷ 18.016 = 85.774 (ft/F).

This expression is of the form of Equation 4.

According to Dalton's Rule the enthalpy of moist air is the sum of separate contributions from the dry air and the water vapor; thus,

$$h = h_a + \mu(W_s h_w) \tag{19}$$

where, to be consistent, the specific enthalpies h_a and h_w should be allowed to vary with temperature only, not with pressure or composition. This expression is of the form of Equation 5.

Within the accuracy of Dalton's Rule the following empirical equations give suitable values of h_a and h_w:

$$\begin{aligned} h_a &= 0.240t \\ h_w &= 0.444t + 1061 \end{aligned} \tag{20}$$

Equation 7 defining thermodynamic wet-bulb temperature may be written in the form,

$$h - h' + (W_s^* - W)h_w^* = h_s^* - h'$$

If the quantity h' that has been subtracted from both sides is understood to be the enthalpy at the thermodynamic wet-bulb temperature t^* but at the humidity ratio W, then within the accuracy of Dalton's Rule

$$\begin{aligned} h - h' &= (0.240 + 0.444W)(t - t^*) \\ h_s^* - h' &= (1061 + 0.444t^*)(W_s^* - W) \\ h_w^* &= t^* - 32 \end{aligned}$$

With these approximations Equation 7 becomes

$$W_s^* - W = \frac{0.240 + 0.444W}{1093 - 0.556t^*}(t - t^*) \tag{21}$$

Carrier[6] has modified Equation 21 by introducing further approximations as follows,

$$\begin{aligned} W_s^* &= 0.6220p_s^*/(p - p_s^*) \\ W &= 0.6220p_w/(p - p_s^*) \\ 0.444\,W &= 0 \end{aligned}$$

the first of which is part of Dalton's Rule. The result is

$$p_w = p_s^* - \frac{p - p_s^*}{2830 - 1.44t^*}(t - t^*) \tag{22}$$

except that the numerical values of the constants in the denominator of the rightmost term are somewhat different than Carrier's.

Equation 22 permits direct calculation of the partial pressure p_w from observed values of pressure p, temperature t, and wet-bulb temperature t^*, assuming that information is available regarding the saturation pressure p_s. The ratio p_w/p_s is the so-called relative humidity.

Example 18. Find the relative humidity of moist air at 90 F dry-bulb, and 63 F (thermodynamic wet-bulb).

Solution. At 63 F the value of the saturation pressure is 0.58002 in. Hg. Therefore, at atmospheric pressure (29.921 in. Hg),

$$p_w = 0.58002 - 29.341 \times 27/2739 = 0.2908 \text{ in. Hg}$$

The relative humidity is

$$\varphi = 0.2908/1.4219 = 0.2045$$

the denominator being the value of saturation pressure at 90 F.

From Equation 16 may be computed the corresponding degree of saturation, the result being

$$\mu = 19.67 \text{ per cent}$$

in remarkably close agreement with the answer to Example 2.

STEADY FLOW ENERGY EQUATION

In steady flow, the energy convected by the fluid at any section is the sum of (*a*) kinetic energy due to velocity; (*b*) gravitational energy due to elevation; (*c*) enthalpy due to the condition of pressure, temperature and composition of the fluid.

Kinetic Energy

There are reasons to believe that the so-called *velocity pressure* h_v read by a Pitot tube is simply the kinetic energy per unit volume of the fluid immediately upstream from the tube, as application of Bernoulli's Equation suggests. Thus

$$V = 1097.3 \sqrt{\frac{h_v}{\rho}} \tag{23}$$

where

V = velocity, feet per minute.

h_v = velocity pressure, inches of water at 60 F.

ρ = density of fluid, pounds per cubic foot.

In the case of flow through a duct, the velocity pressure is found to vary considerably over the section and a traverse has to be made. The cross-sectional area of the duct is divided into a number of equal concentric areas, and measuring stations are located at centroidal points in each area along two perpendicular diameters. Usually the ultimate object is to determine an *average* velocity $\overline{V}$ from which the weight of fluid crossing the section per unit time can be obtained on multiplying by the cross-sectional area of the duct and by the density of the fluid. This is obtained by simply averaging the square roots of all measured velocity pressures as follows:

$$\overline{V} = \frac{1097.3}{\sqrt{\rho}} \left(h_v^{1/2} \right)_{av} \tag{24}$$

where

$\overline{V}$ = average velocity, feet per minute.

$(h_v^{1/2})_{av}$ = arithmetic average of the square roots of all measured velocity pressures, inches of water at 60 F.

But the item of present importance is the *average kinetic energy* convected with each pound of fluid. Consistently with the previous discussion, this can be shown to be

$$\overline{KE} = 0.006678\, v \frac{(h_v^{3/2})_{av}}{(h_v^{1/2})_{av}} \tag{25}$$

where

$\overline{KE}$ = average kinetic energy, Btu per pound.
v = specific volume, cubic feet per pound.
$(h_v^{3/2})_{av}$ = arithmetic average of the 3/2-powers of all measured velocity pressures, inches of water at 60 F.

If the velocity pressure were uniform over the section, Equations 24 and 25 could be combined to give

$$\overline{KE} = \left(\frac{\overline{V}}{13{,}430}\right)^2 \tag{26}$$

But, it is interesting to note that if the velocity varies *parabolically* from zero at the walls to maximum at the center as it does in the case of purely viscous flow in a circular duct, *then the average kinetic energy is twice that given by* Equation 26.

Example 19. If 2000 cfm of air flow through an 8 in. diameter circular duct, find the average kinetic energy per pound of air.

Solution. The cross-sectional area of the duct is 0.349 sq ft; hence the average flow velocity is 5730 fpm. If the velocity were uniform over the section, the average kinetic energy would be $(5730 \div 13{,}430)^2 = 0.182$ Btu per pound. But it is more likely that the actual distribution of velocity would approximate that characteristic of viscous flow; hence the average kinetic energy would be more nearly $2 \times 0.182 = 0.364$ Btu per pound.

Gravitational Energy

The potential energy due to elevation Z (feet) above any convenient datum is simply $Z \div 778.3$ Btu per pound of fluid. In the case of moist air,

$$\overline{PE} = \frac{\overline{Z}\,(1 + W)}{778.3} \tag{27}$$

where

$\overline{PE}$ = average potential energy, Btu per pound dry air.
$\overline{Z}$ = average elevation, feet.
W = humidity ratio, pound water per pound dry air.

Enthalpy

No further discussion of enthalpy is required. It may be well to emphasize, however, that enthalpies have been figured on the basis of one pound of dry air.

Heat and Shaft Work

Between any two sections 1 and 2 in an apparatus through which steady flow occurs, there may be heat *absorbed* from outside, ${}_1q_2$, Btu per pound of dry air, and shaft work *removed* to outside, ${}_1l_2$, Btu per pound of dry air. If heat is actually rejected to outside, ${}_1q_2$ is intrinsically negative; and if shaft work is actually put in from outside, ${}_1l_2$ is intrinsically negative.

Steady-flow Energy Equation

A complete energy accounting takes the form of Equation 28 which is usually referred to as the steady-flow energy equation.

$${}_1q_2 = (h_2 + \overline{KE}_2 + \overline{PE}_2) - (h_1 + \overline{KE}_1 + \overline{PE}_1) + {}_1l_2 \tag{28}$$

where

$_1Q_2$ = heat *added* from outside *between* sections 1 and 2, Btu per pound dry air.
h_2 = enthalpy of the mixture *at* section 2, Btu per pound dry air.
$\overline{KE}_2$ = average kinetic energy *at* section 2, Btu per pound dry air.
$\overline{PE}_2$ = average potential energy *at* section 2, Btu per pound dry air.
h_1 = enthalpy *at* section 1, Btu per pound dry air.
$\overline{KE}_1$ = average kinetic energy *at* section 1, Btu per pound dry air.
$\overline{PE}_1$ = average potential energy *at* section 1, Btu per pound dry air.
$_1l_2$ = shaft work withdrawn *between* sections 1 and 2, Btu per pound dry air.

In Equation 28 all quantities are *per pound of dry air*. If Equation 25 is used in computing average kinetic energy, the result will be in Btu per pound of dry air if v is taken as volume per pound of dry air. If Equation 26 is used, multiplication by $(1 + W)$ as in Equation 27 is required though this is a refinement seldom justified.

Thermodynamic properties of water at saturation are given in Table 2 for the range -160 to $+212$ F.

U. S. STANDARD ATMOSPHERE

The so-called U. S. Standard Atmosphere is an essential standard of reference in aeronautics and as such has become important to the air conditioning engineer who frequently has to simulate atmospheric conditions at high altitudes in connection with aeronautical research. In defining this standard it is first assumed that temperature T varies linearly with altitude Z above sea level, at any rate up to the lower limit of the isothermal layer at 35,332 ft. Thus,

$$T = T_0 - 0.0019812\,Z \tag{29}$$

or

$$\frac{dT}{dZ} = -0.0019812 \text{ (degree Centigrade per foot)} \tag{30}$$

The second assumption is the validity of the perfect gas laws, namely,

$$Pv = RT \tag{31}$$

A horizontal disc of air having unit cross-sectional area (1 sq ft) and vertical thickness dZ (ft) weighs dZ/v (lb). This accounts for the difference of pressure dP (lb per sq ft) between the upper and lower faces of the disc; hence, using Equation 31

$$dZ = \frac{RT\,dP}{P} \tag{32}$$

Equations 30 and 32 can be combined to eliminate Z and then integrated to obtain the relation between pressure and temperature, namely,

$$\frac{T}{T_0} = \left(\frac{P}{P_0}\right)^{0.1903} \tag{33}$$

The values $T_0 = 288\ K$ and $P_0 = 29.921$ in. Hg are parts of the definition of the standard atmosphere.

Values of pressure and temperature are listed in Table 5 for altitudes in the standard atmosphere from $-1{,}000$ to 50,000 ft above sea level. Values for altitudes below the lower limit of the isothermal layer conform

to Equations 29 and 33. For further explanation, reference (7) should be consulted.

TABLE 5. PRESSURE AND TEMPERATURE FOR ALTITUDES IN U. S. STANDARD ATMOSPHERE

ALTITUDE FEET Z	PRESSURE IN. OF HG P	TEMP F t
− 1,000	31.02	+62.6
− 500	30.47	+60.8
0	29.921	+59.0
+ 500	29.38	+57.2
+ 1,000	28.86	+55.4
+ 5,000	24.89	+41.2
10,000	20.58	+23.4
15,000	16.88	+ 5.5
20,000	13.75	−12.3
25,000	11.10	−30.1
30,000	8.88	−47.9
35,000	7.04	−65.8
40,000	5.54	−67.0
45,000	4.36	−67.0
50,000	3.436	−67.0

LETTER SYMBOLS USED IN CHAPTER 3

μ = degree of saturation or per cent saturation.

ρ = density of fluid, pounds per cubic foot.

φ = relative humidity (decimal).

a = ratio of apparent molecular weight of dry air (28.966) to the molecular weight of water (18.016) = 1.6078.

A = coefficient from Table 4 for use in Equation 4a (obtained from Table 4).

B = coefficient to be used in Equation 5a (obtained from Table 4).

C = coefficient for use in Equation 6a (obtained from Table 4).

h = enthalpy of moist air, Btu per pound of dry air.

$\bar{h}$ = enthalpy correction term to be added above 150 F, to enthalpy.

h_a = specific enthalpy of dry air, Btu per pound.

$h_{as} = h_s - h_a$ = the difference between the enthalpy of moist air *at saturation* per pound of dry air, and the specific enthalpy of the dry air itself, Btu per pound of dry air.

h_s^* = enthalpy of moist air at saturation at *thermodynamic wet-bulb temperature*, Btu per pound of dry air.

h_s = enthalpy of moist air at saturation per pound of dry air, Btu per pound of dry air.

h_v = velocity pressure, inches of water at 60 F.

h_w = specific enthalpy of condensed water (liquid or solid) at standard pressure, Btu per pound water.

h_w^* = specific enthalpy of water as added at the *thermodynamic wet-bulb* temperature t^*, Btu per pound of dry air.

K = Kelvin degrees.

KE = kinetic energy, Btu per pound.

$\overline{KE}$ = average kinetic energy, Btu per pound.

l = shaft work withdrawn, Btu per pound of air.

$_1l_2$ = shaft work withdrawn between sections 1 and 2, Btu per pound of air.

LETTER SYMBOLS (Continued)

m = weight of dry air crossing any duct section, pounds per minute.

m_1, m_2, m_3 = weights of dry air convected across sections F_1, F_2, F_3 respectively, pounds per minute.

M = weight of dry air withdrawn with inside air, pounds per hour.

n_a = mols of dry air.

n_w = mols of water vapor.

p = total pressure of a mixture of air and water vapor, pounds per square inch or inches Hg.

p_a = partial pressure of air, pounds per square inch or inches Hg.

p_s = *saturation* pressure of pure water vapor, pounds per square inch or inches Hg.

p_w = partial pressure of water vapor in mixture of air and water vapor, pounds per square inch or inches Hg.

P = atmospheric pressure, inches Hg.

P_o = standard atmospheric pressure by definition 29.921 in. Hg.

PE = potential energy, Btu per pound dry air.

$\overline{\text{PE}}$ = average potential energy, Btu per pound dry air.

q = ratio of energy added (or removed) to water added (or removed), Btu per pound. Also called specific enthalpy of *water added.*

$_1q_2$ = heat added between sections 1 and 2, Btu per pound dry air.

$_Aq_B$ = heat added between sections A and B per pound of dry air, Btu per pound.

$_AQ_B$ = total heat added between sections A and B, Btu per minute.

ΔQ = energy to be removed from or added to conditioned space, Btu per hour.

R = universal gas constant.

R_a = gas constant for dry air.

R_w = gas constant for water vapor.

s = entropy of moist air per pound of dry air, Btu per (pound) (Fahrenheit degree).

$\bar{s}$ = correction to be added to entropy of moist air obtained from Equation 6.

$\bar{\bar{s}}$ = additional correction to be added to entropy because of "mixing entropy" (obtained from Table 4). Correction to be added to value of s obtained from Equation 6.

s_a = specific entropy of dry air, Btu per (pound) (Fahrenheit degree, absolute).

s_{as} = the difference between the entropy of moist air *at saturation* per pound of dry air, and the specific entropy of the dry air itself, Btu per (pound of dry air) (Fahrenheit degree, absolute).

s_s = entropy of moist air at saturation per pound of dry air, Btu per (pound of dry air) (Fahrenheit degree, absolute).

s_w = specific entropy of condensed water (liquid or solid) at standard atmospheric pressure, Btu per (pound of water) (Fahrenheit degree, absolute).

t^* = thermodynamic wet-bulb temperature, Fahrenheit degrees.

t(F) = temperature, Fahrenheit degrees.

T = absolute temperature, Fahrenheit degrees.

T_o = standard atmospheric temperature, by definition 288 Kelvin degrees.

v = volume of moist air per pound of dry air, cubic feet per pound.

$\bar{v}$ = correction to be added to volume of moist air per pound of dry air, above 150 F.

v_a = specific volume of dry air, cubic feet per pound.

LETTER SYMBOLS (Continued)

v_{as} = $v_s - v_a$, the difference between volume of moist air *at saturation*, per pound of dry air, and the volume of the dry air itself, cubic feet per pound of dry air.

v_s = volume of moist air at saturation per pound of dry air, cubic feet per pound of dry air.

v_T = total volume, cubic feet.

V = velocity, feet per minute.

$\overline{V}$ = average velocity, feet per minute.

W = humidity ratio, of moist air, pounds of water per pound of dry air.

ΔW = water to be removed from (or added to) conditioned space, pounds per hour.

W_s = humidity ratio, *at saturation*, weight of water vapor per pound of dry air, pound per pound.

W_s^* = humidity ratio corresponding to thermodynamic wet-bulb temperature t^*, pounds of water per pound of dry air.

Z = elevation above any datum, feet.

$\overline{Z}$ = average elevation, feet.

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Chapter 4

FLUID FLOW

Theory; Pressure Loss in Circular and Non-Circular Pipes; Compressible Fluids; Nozzles and Orifices; Steam Flow Measurement; Metering Liquids; Nozzle Coefficients and Expansion Factors; Pitot Tube; Installation of Nozzles and Orifices

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THE flow of fluids is part of the branch of engineering science known as fluid mechanics, which will be discussed here insofar as it applies to the work of engineers in the fields of heating, ventilating, and air conditioning. Probably air is the most frequently handled fluid, but other gases and liquids are often involved. Compressible fluids (gases) and incompressible fluids (liquids) vary somewhat in behavior, though in cases where pressure and density changes are small, the gases may be treated as incompressible fluids.

THEORY OF FLUID FLOW

The following head equation based on energy considerations for steady flow processes will serve as a basis for the theory of the flow of fluids. This equation is presented in several ways in various texts, but a suitable form is:

$$\frac{V_1^2}{2g} + Ju_1 + p_1v_1 + E + Jq + z_1 = \frac{V_2^2}{2g} + Ju_2 + p_2v_2 + z_2 \qquad (1)$$

where

V = velocity in feet per second.
g = acceleration due to gravity = 32.17 ft per (second) (second).
J = mechanical equivalent of heat = 778 foot pounds per Btu.
u = internal energy, in Btu per pound of fluid.
p = pressure in pounds per square foot.
v = specific volume, in cubic feet per pound.
E = mechanical work, in foot pounds per pound of fluid flowing.
q = heat transferred to the fluid, in Btu per pound of fluid flowing.
z = elevation above some arbitraty datum, in feet.
Subscript 1 refers to the entrance, subscript 2 to the exit.

Introducing the enthalpy h, which by definition is $u + \frac{pv}{J}$, expressed in Btu per pound of fluid, Equation 1 becomes

$$\frac{V_1^2}{2g} + Jh_1 + E + Jq + z_1 = \frac{V_2^2}{2g} + Jh_2 + z_2 \qquad (2)$$

The steady flow energy equation is applicable to a wide range of problems in the flow of fluids. Obviously it applies to flow through pipes, orifices, and nozzles, and to the flow through turbines and centrifugal pumps. Reciprocating engines and pumps are essentially intermittent, but the flow tends to become steady as the number of cylinders increases, and becomes practically uniform at the entrance and exit if the system includes receivers and pipes of sufficient size.

By substituting $\frac{p}{\rho}$ (where ρ is density in pounds per cubic foot) for

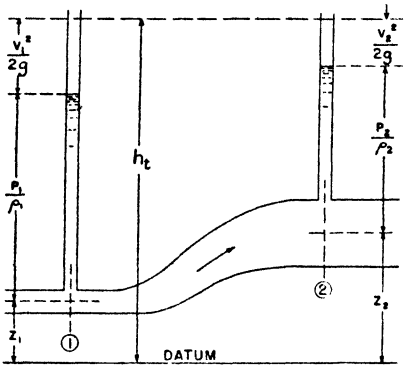

FIG. 1. RELATION OF VARIOUS FACTORS IN BERNOULLI EQUATION

its equivalent pv in Equation 1, the result, after rearranging, will be:

$$\frac{V_1^2}{2g} + \frac{p_1}{\rho_1} + z_1 = \frac{V_2^2}{2g} + \frac{p_2}{\rho_2} + z_2 + \left[J(u_2 - u_1) - E - Jq \right] \qquad (3)$$

In the case of flow through a pipe, no outside work is performed and, if the process is considered adiabatic, and if the change due to turbulence and friction is considered to be negligible, the bracketed expression in Equation 3 will disappear, leaving:

$$\frac{V_1^2}{2g} + \frac{p_1}{\rho_1} + z_1 = \frac{V_2^2}{2g} + \frac{p_2}{\rho_2} + z_2 \qquad (4)$$

which is commonly called the Bernoulli equation, named after the Swiss mathematician and physician who first propounded the theory. $\frac{V^2}{2g}$ is

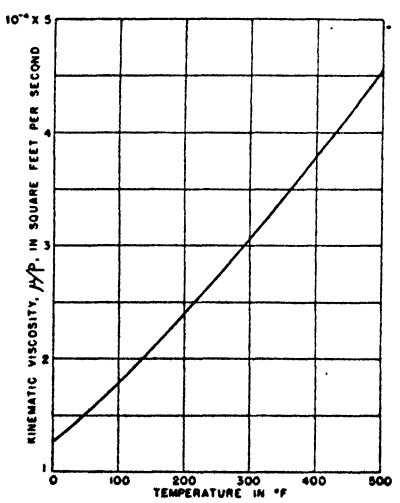

FIG. 2. RELATION OF KINEMATIC VISCOSITY TO TEMPERATURE OF AIR

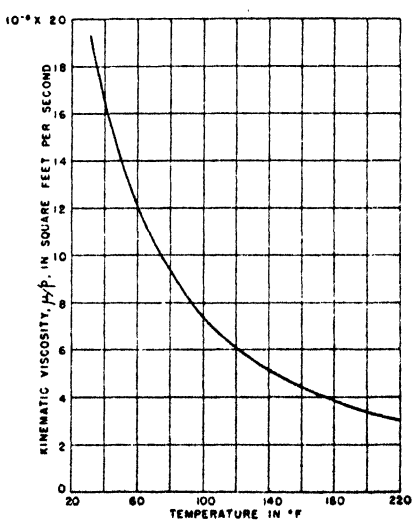

FIG. 3. RELATION OF KINEMATIC VISCOSITY TO TEMPERATURE OF WATER

known as the velocity head, $\frac{p}{\rho}$ is the pressure head, and z is the elevation head, all in feet of the fluid; the total head, h_t is the sum of the other three heads. Fig. 1 shows diagrammatically the relation of the various factors. The pressure at point 2 is lower than at point 1 because of the elevation of point 2 over point 1, and the velocity at point 2 is lower than at point 1 because of the larger pipe diameter at point 2. If the pipe diameter were the same throughout, the velocity, and consequently the velocity head, would be the same at both points, but the higher elevation at point 2 would still be responsible for a loss in pressure. The utility of the equation is evident, though it should be remembered that in it the *effects of friction and turbulence are neglected*, and that Fig. 1 represents ideal conditions. It should also be noted that the *Bernoulli equation applies only to incompressible fluids.*

Pressure Loss in Circular Pipes

The pressure loss in circular pipes is customarily expressed by the formula:

$$h_f = \frac{f l V^2}{2g d} \tag{5}$$

where

h_f = the loss in head of the fluid under conditions of flow, in feet.
l = the length of the pipe, in feet.
V = the velocity, in feet per second.
g = the acceleration due to gravity = 32.17 ft per (second) (second).
d = the internal diameter of the pipe, in feet.
f = a dimensionless friction coefficient.

The formula is generally known by the name of Darcy or Fanning, though it seems to have been originated by d'Aubisson de Voisins in 1834.

The factor f is a function of the Reynolds number

$$N_{Re} = \frac{d V \rho}{\mu} \tag{6}$$

where

N_{Re} = Reynolds number.
ρ = the density in pounds per cubic foot.
μ = the absolute viscosity in pounds per foot-second.

Both f and the Reynolds number are dimensionless. To aid in computing the Reynolds number, values of $\frac{\mu}{\rho}$, the kinematic viscosity, are shown as a function of temperature for air in Fig. 2 and for water in Fig. 3.

Fig. 4 shows the relation between f and the Reynolds number, adapted from a review by Moody[1]. The straight line sloping downward at the left of the chart supplies the values of f for laminar flow; it represents the formula

$$f = \frac{64}{N_{Re}} \tag{7}$$

With laminar flow, the velocity profile is a parabola, having the formula

[1]Superior numbers refer to the references at the end of the chapter.

$$V = \frac{\rho h_f}{4\mu l}(r^2 - L^2) \tag{8}$$

where

r = the radius of the pipe in feet.
L = distance perpendicularly from the axis of the pipe, in feet.

Accordingly, the maximum velocity occurs at the center of the pipe and is twice the average velocity; the average velocity is found when $L = 0.707\ r$. It is worth noting that roughness of the pipe wall has no effect on the loss in head for laminar flow.

Between values of the Reynolds number of 2000 and 4000, there is an

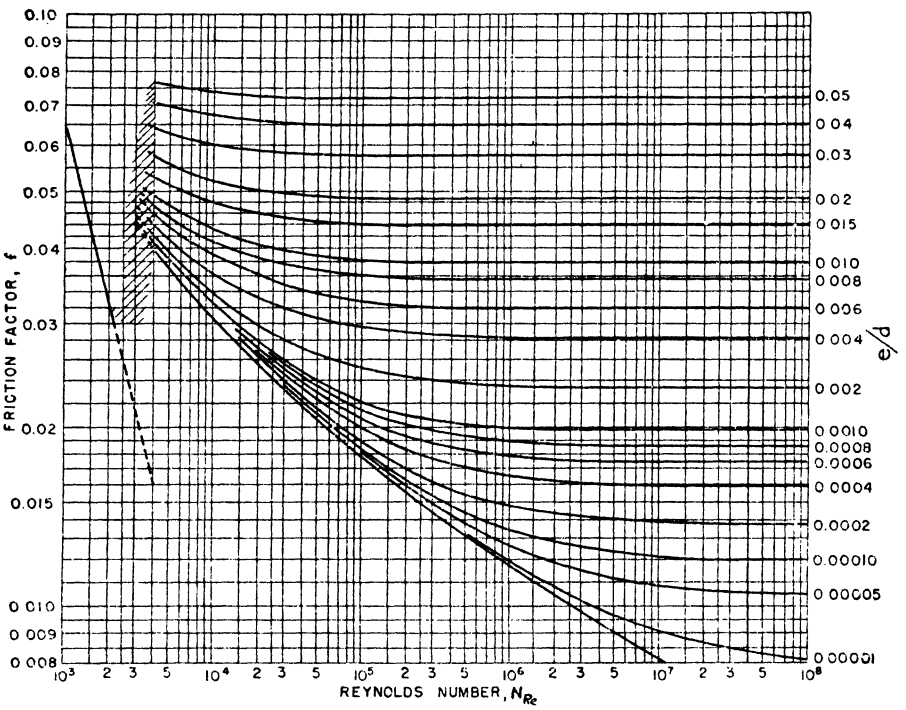

FIG. 4. RELATION BETWEEN FRICTION FACTOR AND REYNOLDS NUMBER
NOTE: The straight line at left shows values of Friction Factor for laminar flow.
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unstable region where the flow changes from laminar to turbulent, or vice versa. The actual value is impossible of prediction for any conditions of flow, though in general it may be said that the prevailing type of flow persists into the unstable region; however, once the change starts, it proceeds very rapidly.

When the flow is turbulent, the velocity profile is essentially parabolic over four fifths of the pipe diameter, but near the pipe walls, the effect of friction becomes evident, and in the boundary layer at the pipe wall the flow is laminar. Fig. 5 compares the velocity profiles for three different Reynolds numbers, but for the same average velocity.

The lower curve in the turbulent region in Fig. 4 represents the relation of f to the Reynolds number for smooth pipe, such as drawn brass tubing or glass tubing. The effect of roughness on f, which is a considerable

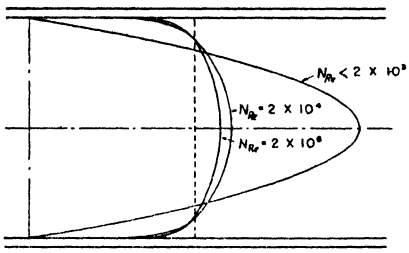

FIG. 5. COMPARISON OF VELOCITY PROFILES FOR 3 DIFFERENT REYNOLDS NUMBERS BUT FOR SAME AVERAGE VELOCITY

factor in turbulent flow, is open to some conjecture; artificially roughened pipes, for instance, give results at variance with actual tests. The curves above the smooth pipe curve of Fig. 4 represent a summary of tests on rough pipe, each of them identified by a value of e/d, with e signifying the absolute roughness in feet. Values of e/d for different pipes are given in Table 1.

To find the friction loss for any pipe, follow the curve with the proper value of e/d, to the pertinent value of N_{Re}; and from this point proceed horizontally to left margin to find the value of f to use in Equation 5.

Equation 5 is applicable to all liquids, and to gases when the pressure loss is less than 10 per cent of the initial pressure. When the loss in head is high, the formula to be used for gases is

$$\frac{p_1^2 - p_2^2}{p_1^2} = \frac{flV_1^2}{gd\ p_1 v_1} \tag{9}$$

which may be rearranged to give the loss in pressure

$$p_1 - p_2 = p_1 \left[1 - \sqrt{1 - \frac{flV_1^2}{gd\ p_1 v_1}} \right] \tag{10}$$

Pressure Loss in Non-Circular Pipes

The formulas for flow in pipes are based upon the use of pipes of circular cross-section. The formulas may be used with conduits of other shapes, and in conduits not flowing full, when the flow is turbulent, by using the hydraulic radius, R_H, which is really a ratio:

$$R_H = \frac{\text{area of cross-section}}{\text{wetted perimeter of cross-section}} \tag{11}$$

TABLE 1. VALUES OF e/d FOR DIFFERENT KINDS OF PIPE

TYPE OF PIPE	e/d
Smooth drawn tubing	0.000005
Commercial steel or wrought iron	0.00015
Asphalted cast-iron	0.0004
Galvanized iron	0.0005
Cast-iron	0.00085
Wood stave	0.0006 to 0.003
Concrete	0.001 to 0.01
Riveted steel	0.003 to 0.03

For instance, in a square duct, 1 ft on a side, handling air, the hydraulic radius is ¼ or 0.25. If the same duct is handling water, flowing 9 in. deep, the hydraulic radius is 0.75/2.5 or 0.30. Note in this latter case that the wetted perimeter does not include the distance across the free surface.

In the case of a round pipe

$$R_H = \frac{\pi d^2/4}{\pi d} = \frac{d}{4} \text{ or } d = 4R_H \tag{12}$$

Substituting Equation 12 in Equation 6,

$$N_{Re} = \frac{4R_H V\rho}{\mu} \tag{13}$$

and in the flow Equation 5,

$$h_f = \frac{fl V^2}{8gR_H} \tag{14}$$

and finally in the compressible fluid flow Equation 10,

$$p_1 - p_2 = p_1 \left[1 - \sqrt{1 - \frac{fl V_1^2}{4g R_H p_1 v_1}} \right] \tag{15}$$

Equations 13, 14, and 15 may be used to compute the flow in pipes and ducts of non-circular section and in any type of conduit not flowing full. *They should not be used when the flow is laminar.*

FLOW OF COMPRESSIBLE FLUIDS

The energy equation for the flow of compressible fluids, as represented by the gases, is derived from Equation 1. Assuming that no heat is transferred to the fluid, that no work is done, and that there is no difference in elevation, Equation 1 becomes

$$\frac{V_1^2}{2g} + Ju_1 + p_1 v_1 = \frac{V_2^2}{2g} + Ju_2 + p_2 v_2 \tag{16}$$

or, after rearrangement,

$$\frac{V_2^2 - V_1^2}{2g} = p_1 v_1 - p_2 v_2 + J(u_1 - u_2) \tag{17}$$

Since internal energy is dependent only on temperature,

$$u_1 - u_2 = c_v(T_1 - T_2) \tag{18}$$

where

c_v = the specific heat of the gas at constant volume.
T_1 and T_2 = the absolute temperatures in Fahrenheit degrees at points 1 and 2, respectively.

Substituting Equation 18 in Equation 17,

$$\frac{V_2^2 - V_1^2}{2g} = p_1 v_1 - p_2 v_2 + Jc_v(T_1 - T_2) \tag{19}$$

Now

$$c_v = \frac{R}{J(k-1)} \tag{20}$$

where

R = the gas constant in the expression.

$$pv = RT \tag{21}$$

k = the ratio of the specific heat at constant pressure to the specific heat at constant volume.

This ratio, k, is used extensively in fluid dynamics; values of k for various gases are given in Table 2.

TABLE 2. RATIO OF SPECIFIC HEAT AT CONSTANT PRESSURE TO SPECIFIC HEAT AT CONSTANT VOLUME FOR COMPRESSIBLE FLUIDS

COMPRESSIBLE FLUID	RATIO $k = c_p/c_v$
Helium and other monatomic gases	1.66
Air and other diatomic gases	1.40
Ammonia and hydrogen sulfide	1.34
Carbon dioxide, methane, natural gas, superheated steam, moist steam down to a quality of 97 per cent	1.28 to 1.32
Sulfur dioxide, ethylene, acetylene	1.24 to 1.26

Substituting Equations 20 and 21 in Equation 19, the energy equation becomes

$$\frac{V_2^2 - V_1^2}{2g} = \frac{k}{k-1}(p_1v_1 - p_2v_2) \tag{22}$$

While this is a convenient form of equation, it does not include all the necessary specifications. If the steady flow process is frictionless and reversible,

$$\frac{p_2}{p_1} = \left(\frac{v_1}{v_2}\right)^k = \left(\frac{\rho_2}{\rho_1}\right)^k \tag{23}$$

By introducing this relation in Equation 22 it is possible to reduce that equation to:

$$\frac{V_2^2 - V_1^2}{2g} = \frac{k}{k-1}\frac{p_1}{\rho_1}\left[1 - \left(\frac{p_2}{p_1}\right)^{\frac{k-1}{k}}\right] \tag{24}$$

This form of the equation is applicable not only to flow in pipes, but also to flow through orifices and nozzles.

A significant factor in the flow of compressible fluids is the velocity of sound, V_{so}, which for present purposes will be considered as the velocity at which sound will travel in the fluid at its density at the first or inlet section of the flow system being considered.

The velocity of sound is expressed as

$$V_{so} = \sqrt{\frac{gkp_1}{\rho_1}} \tag{25}$$

This formula may be developed rationally and agrees perfectly with experimental results. Substituting Equation 25 in Equation 24:

$$\frac{V_2^2 - V_1^2}{2} = \frac{V_{so}^2}{k-1}\left[1 - \left(\frac{p_2}{p_1}\right)^{\frac{k-1}{k}}\right] \tag{26}$$

or, by rearrangement,

$$\frac{p_2}{p_1} = \left[1 - \frac{k-1}{V_{so}^2}\left(\frac{V_2^2 - V_1^2}{2}\right)\right]^{\frac{k}{k-1}} \tag{27}$$

which permits the calculation of the ratio of pressures at entrance and exit of the steady flow device,—pipe, orifice, or nozzle.

FLOW THROUGH NOZZLE OR ORIFICE

Another useful expression, covering the energy change in an orifice or nozzle, may be derived from Equation 2. As with the flow through pipes, no outside work is done. Then, assuming that there is no difference in elevation, and since practically no heat is evolved or absorbed, *i.e.*, the process is adiabatic, E, z, and q of Equation 2 may be eliminated, and, by rearranging, the equation becomes

$$\frac{V_2^2}{2g} - \frac{V_1^2}{2g} = J(h_1 - h_2) \text{ foot pounds per second} \tag{28}$$

In any flow device,

$$\frac{V_1 A_1}{v_1} = \frac{V_2 A_2}{v_2} \text{ or, } V_1 = V_2 \frac{A_2 v_1}{A_1 v_2} \tag{29}$$

in which A_1 or A_2 is the cross-sectional area of the flow at a particular point, expressed in square feet. With this substituted in Equation 28, and solving for V_2:

$$V_2 = \sqrt{\frac{2gJ(h_1 - h_2)}{1 - (A_2/A_1)^2 (v_1/v_2)^2}} \tag{30}$$

Using this expression, it is possible to determine the velocity at any point in the flow through an orifice or nozzle. If the area at the point of entry is very large with respect to that at point 2, the denominator on the right side of Equation 30 will approach unity, and the equation will reduce to

$$V_2 = \sqrt{2gJ(h_1 - h_2)} \tag{31}$$

For this reason, the expression $\sqrt{\frac{1}{1 - (A_2/A_1)^2 (v_1^2/v_2^2)}}$ is called the correction factor for the velocity of approach.

The velocity of approach factor may be further simplified if the difference in volume between points 1 and 2 is negligible. Under this condition, the velocity of approach factor becomes $\sqrt{\frac{1}{1 - (A_2/A_1)^2}}$. If

$$\frac{A_2}{A_1} = \frac{D_2^2}{D_1^2} = \beta^2 \tag{32}$$

the velocity of approach factor is $\sqrt{\frac{1}{1 - \beta^4}}$, in which form it is generally used in flow formulas. The quantity β is the ratio of the throat or orifice diameter to the pipe diameter.

The connection of the velocity of sound with the flow of fluids has already been noted. Its most important application is to the flow of gases through a converging tube or nozzle. If it is assumed that the inlet velocity of the fluid, V_1, is negligible, Equation 24 will reduce to

$$V_2 = \sqrt{\left(\frac{2gk}{k-1}\right)\frac{p_1}{\rho_1}\left[1 - \left(\frac{p_2}{p_1}\right)^{\frac{k-1}{k}}\right]} \tag{33}$$

Let W represent the weight of gas flowing through the converging tube in a unit of time, and A_2 the area at the throat; then,

$$W = A_2V_2/v_2 \text{ or } V_2 = Wv_2/A_2 \tag{34}$$

Substituting this, as well as the relation $p_1v_1^k = p_2v_2^k$, in Equation 33 gives,

$$W = A_2\sqrt{\left(\frac{2gk}{k-1}\right)\frac{p_1}{v_1}\left[\left(\frac{p_2}{p_1}\right)^{\frac{2}{k}} - \left(\frac{p_2}{p_1}\right)^{\frac{k+1}{k}}\right]} \tag{35}$$

If this is computed and the figures are plotted, the curved line (partly solid and partly broken) of Fig. 6 is found. The maximum value of $\frac{p_2}{p_1}$ may be computed by differentiating W with respect to p_2 and equating the result to zero. This operation produces the formula:

$$\frac{p_2}{p_1} = \left(\frac{2}{k+1}\right)^{\frac{k}{k-1}} \tag{36}$$

For air, with $k = 1.40$, $\frac{p_2}{p_1} = 0.53$.

Critical Pressure and Critical Flow

Actually, the broken part of the curve is not attained for the flow in the nozzle. If the ratio of p_2 to p_1 is decreased from unity, the weight

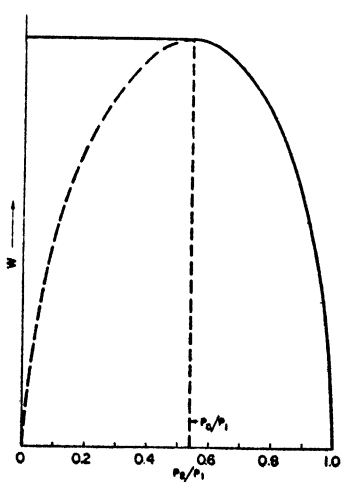

FIG. 6. RELATION OF FLOW OF GAS TO PRESSURE DROP IN A CONVERGING TUBE

rate of discharge, as well as the volume, increases from zero to a maximum, as shown by the solid section of the curve in Fig. 6; thereafter, as p_2/p_1 is decreased further, the discharge is constant, as indicated by the horizontal line. The value of p_2 at the maximum point is called the critical pressure, or p_c, and from Equation 27 it is seen that p_c is approximately 53 per cent of p_1 when air is flowing.

To find the velocity at the critical pressure, it is assumed that the upstream velocity V_1 in Equation 22 is so small as to be negligible. Using the subscript c to indicate conditions at the critical point,

$$\frac{V_c^2}{2g} = \left(\frac{k}{k-1}\right)(p_1v_1 - p_cv_c) \quad or,$$

$$V_c = \sqrt{\left(\frac{2gk}{k-1}\right)(p_1v_1 - p_cv_c)} \tag{37}$$

Substituting Equations 23 and 36. and rearranging, Equation 37 becomes

$$V_c = \sqrt{\left(\frac{2gk}{k+1}\right)p_1v_1} \tag{38}$$

and

$$V_c = \sqrt{\frac{gkp_c}{\rho_c}} \tag{39}$$

Comparing Equation 39 with Equation 25, it will be seen that the velocity at the throat is equal to the velocity of sound at the critical pressure.

Critical flow is attained only in converging tubes, in nozzles, and in orifices with a well-rounded approach. It does not occur in sharp-edged orifices or in nozzles having an expanding outlet section. The so-called critical flow prover uses this property of constant rate of flow above the critical pressure, and finds application as a flow regulator and a quantity-rate meter; in either case, the theoretical rate of flow may be computed from Equation 38, multiplying V_c by the area of the constriction to obtain the volume rate of flow.

In developing the working equations for orifices and nozzles, it is customary to start with

$$V_2^2 - V_1^2 = 2gh_f \tag{40}$$

This may be derived from the Bernoulli equation or from the relations of falling bodies. Now, since

$$A_1V_1 = A_2V_2 = Q_s \tag{41}$$

in which Q_s is the discharge rate in cubic feet per second,

$$\frac{Q_s^2}{A_2^2} - \frac{Q_s^2}{A_1^2} = 2gh_f \tag{42}$$

Transposing,

$$Q_s = \frac{A_1A_2}{\sqrt{A_1^2 - A_2^2}}\sqrt{2gh_f} \tag{43}$$

or

$$Q_s = A_2 \frac{1}{\sqrt{1 - \left(\frac{A_2}{A_1}\right)^2}} \sqrt{2gh_f} \tag{44}$$

The central term on the right hand side of Equation 44 will be recognized as the *velocity of approach factor*, so that

$$Q_s = A_2 \frac{1}{\sqrt{1 - \beta^4}} \sqrt{2gh_f} \tag{45}$$

Actual Flow Through Orifices and Nozzles

The actual rate of flow through an orifice, nozzle, or Venturi tube is rarely equal to the theoretical, and generally the actual rate is less than the theoretical. In the case of the nozzle and Venturi tube, this is due to losses from wall roughness, fluid friction, and turbulence during the expansion in the section following the throat. While wall roughness is not a factor in a sharp-edged orifice, fluid friction and turbulence are important, as is the fact that the discharge contracts to a degree variable with the ratio of outlet to inlet pressure after leaving the orifice, so that the limiting area is somewhat less than the opening in the orifice plate. Accordingly, Equation 45 must be modified by a correction factor, C. Usually, the velocity of approach factor is included with this correction factor, and, if

$$K = C \frac{1}{\sqrt{1 - \beta^4}}, \tag{46}$$

$$Q_s = KA_2 \sqrt{2gh_f}. \tag{47}$$

Multiplying by 3600 to convert from cubic feet per second to cubic feet per hour and converting area in square feet to diameter in inches, gives

$$Q_f = 3600\, K \frac{\pi D_2^2}{4 \times 144} \sqrt{2gh_f}$$

or

$$Q_f = 19.635\, KD_2^2 \sqrt{2gh_f} \tag{48}$$

where

Q_f = rate of flow in cubic feet per hour.
D_2 = the diameter of the orifice or nozzle throat in inches.
K = flow coefficient including correction for velocity of approach.

Equation 48 is a general equation, expressing the flow of any fluid through an orifice or nozzle. Further use of it will be made as other types of flow are discussed.

The differential loss, h_f, is in terms of feet of the fluid flowing through the orifice or nozzle. In the case of a gas flowing, where it is customary to read the differential pressure in inches of water, feet of gas must be converted to inches of water. Since dry air at 32 F and 14.7 psi absolute pressure weighs 0.0807 lb per cubic foot, the weight of a cubic foot of any other kind of gas under the same conditions is 0.0807 G, where G is the specific gravity of the gas referred to air. Water weighs 62.37 lb per cubic foot at 60 F. Using also the relation of 12 in. in 1 ft,

$$h_f = \frac{h_w}{12} \times \frac{62.37}{0.0807G} \tag{49}$$

in which h_w is the differential pressure in inches of water.

Also, since the gas flowing is not necessarily at 32 F and 14.7 psi, it is necessary to apply Charles' and Boyle's laws to the density of the gas and therefore:

$$h_f = \frac{h_w}{12} \times \frac{62.37}{0.0807G} \times \frac{14.7}{P_f} \times \frac{T_f}{492} \tag{50}$$

in which P_f and T_f are the absolute pressure and temperature of the flowing gas. Substituting this in Equation 48, and combining the constants,

$$Q_f = 218.44KD_2^2 \sqrt{\frac{h_w T_f}{P_f G}} \tag{51}$$

Then, to correct the value of Q_f to any other standard conditions of pressure P_b and temperature T_b, using the gas laws,

$$Q_b = Q_f \times \frac{P_f}{P_b} \times \frac{T_b}{T_f} \tag{52}$$

Equation 51 becomes

$$Q_b = 218.44KD_2^2 \frac{T_b}{P_b} \sqrt{\frac{P_f h_w}{T_f G}} \tag{53}$$

Finally, since gases expand under the conditions of reduced pressure downstream from the orifice or nozzle, an expansion factor, Y, must be added. The final formula, then, is

$$Q_b = 218.44KYD_2^2 \frac{T_b}{P_b} \sqrt{\frac{P_f h_w}{T_f G}} \tag{54}$$

In Equation 54, all the data must be observed at the time of measurement except K and Y. These must be obtained from charts, tables, or formulas, derived from or based on the results of a great many experiments, the results of which have been collected by a joint committee of the *American Gas Association* and the *American Society of Mechanical Engineers*[2,3]. The report of the two associations gives orifice coefficients as a function of the Reynolds number and of the ratio of orifice to pipe diameter, for pipes 2 to 12 in. and 14 in. in diameter, and for four different types of pressure taps in use in the United States. The coefficients are higher for the smaller pipe sizes. This is an effect of the turbulence produced by the roughness of the pipe surface, a given roughness being relatively greater with a small pipe than with a large one.

Space does not permit presenting all the coefficient data that are available. However, if the pipe is smooth drawn tubing, the effect of roughness is negligible, and the coefficients for the largest size of pipe apply also to smaller pipes. Figs. 7, 8, and 9 show these coefficients, N_{Re}, being the Reynolds number referred to the diameter of the orifice or throat of the nozzle, in feet.

Pressure Taps—Location and Types

The different sets of pressure taps are called flange taps, radius taps, vena contracta taps, and pipe or full-flow taps. The relative locations of the first three of these are shown in Fig. 10, and the need for different coefficients for the different taps is indicated by the course of the change in pressure of the flowing fluid shown in the lower part of the figure. Pipe taps are located 2½ pipe diameters upstream and 8 pipe diameters downstream, both measured from the upstream face of the orifice plate,

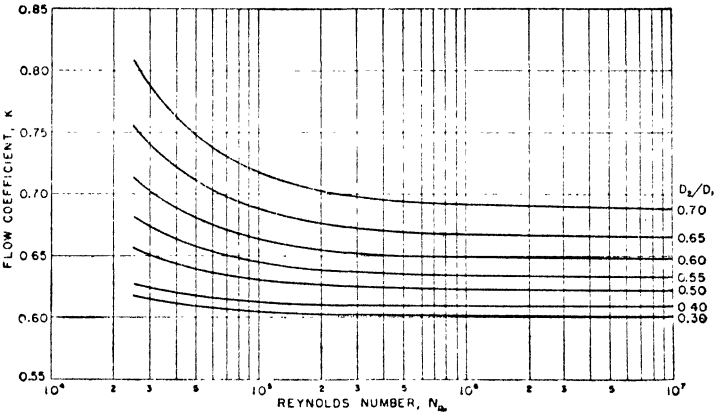

FIG. 7. FLOW COEFFICIENTS, K, FOR SQUARE-EDGED ORIFICE PLATES AND FLANGE TAPS IN SMOOTH PIPE

NOTE: From Table 6, Bibliography [H].

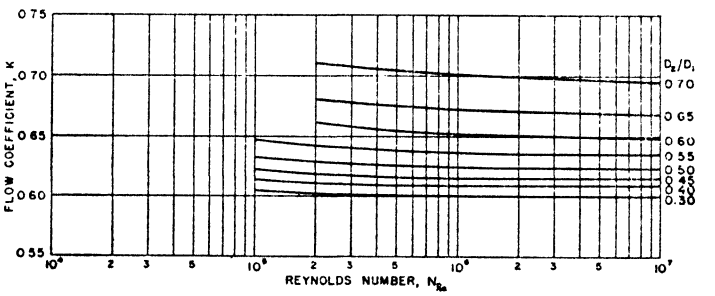

FIG. 8. FLOW COEFFICIENTS, K, FOR SQUARE-EDGED ORIFICE PLATES AND RADIUS TAPS IN SMOOTH PIPE

NOTE: From Fig. 36d, Bibliography [K].

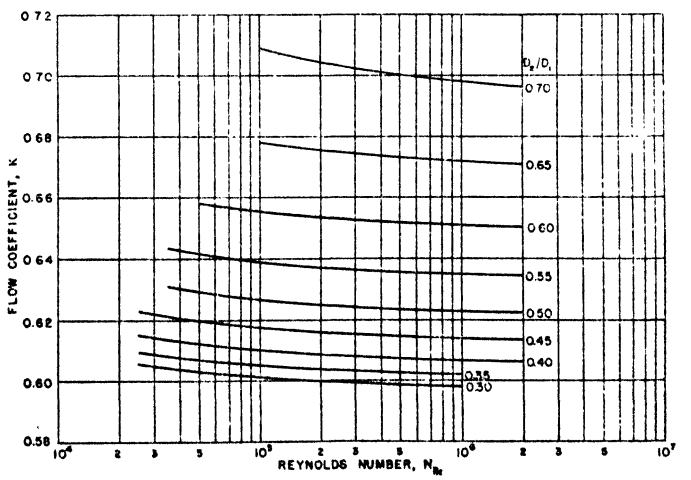

FIG. 9. FLOW COEFFICIENTS, K, FOR SQUARE-EDGED ORIFICE PLATES AND VENA CONTRACTA TAPS, IN SMOOTH PIPE

NOTE: From Table 7, Bibliography [H].

or in other words, before the orifice plate has had any effect on the flow and after the recovery in pressure has been completed. The use of pipe or full-flow taps has been limited to the metering of natural fuel gas in certain areas. As they are not suited to use in heating and ventilating work no data for them are given in this chapter.

Still another type of pressure tap is used in European practice,—corner taps. Pressures are taken from recesses in the flange connected to annular slits in the corners formed by the pipe wall and the orifice plate. Coefficients for these taps have been adopted by the *International Standards Association*, but are not used commercially in America.

It will be noted that the location of the downstream pressure tap of the vena contracta arrangement is variable. Vena contracta is the term

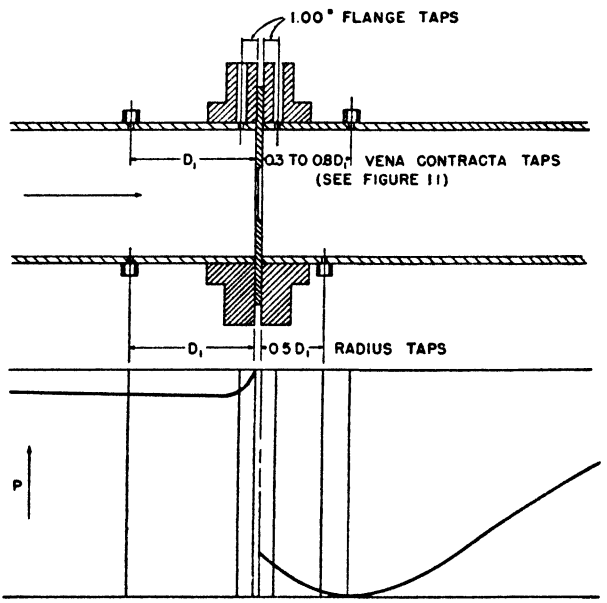

FIG. 10. RELATIVE LOCATION OF FLANGE, RADIUS AND VENA CONTRACTA TAPS

applied to the minimum cross-section of the jet from the orifice, where the static pressure is at a minimum. Its location, and the location of the downstream vena contracta tap, vary with the ratio of orifice to pipe diameter, and with rate of flow, as shown in Fig. 11; the tap is generally located in accordance with the mean curve in the figure.

Expansion Factor for Gases

The expansion factor, Y, for gases (for liquids, $Y = 1$) is found from the empirical formula

$$Y = 1 - (0.41 + 0.35\beta^4)\left(\frac{p_1 - p_2}{p_1}/k\right) \qquad (55)$$

This is applicable to flange, radius, and vena contracta taps.

Values of Y for air, computed from these equations, are given in Fig. 12.

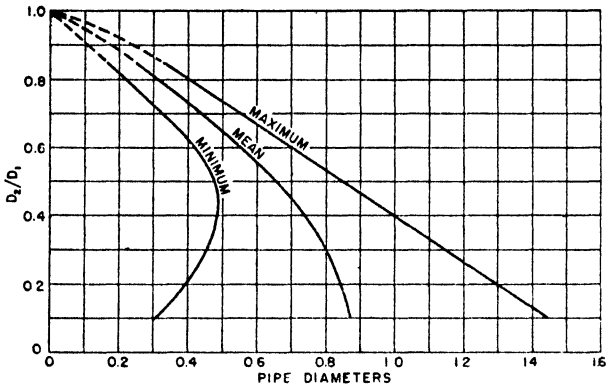

FIG. 11. LOCATION OF VENA CONTRACTA IN RELATION TO RATIO OF ORIFICE TO PIPE DIAMETER AND TO RATE OF FLOW

Computing Orifice Discharge

With this information it is possible to compute the discharge from an orifice if the Reynolds number is known. Here an odd complication is encountered—when the value of N_{Re} is computed, the rate of flow, which is the unknown quantity, must be used in the computation. However, it will be noted in Figs. 7, 8, and 9 that the orifice coefficient does not change greatly as N_{Re} changes. If, then, an estimate is made of the velocity, using this in computing N_{Re}, and if the corresponding coefficient is used in Equation 54, a value for the rate of flow will be found. Using this velocity to compute a corrected value of N_{Re} and repeating the process, a more nearly correct value of Q_f is found. This cut-and-try method may be continued for several more cycles, but generally the first or second correction will be found sufficient.

Another method would be to use the value of K corresponding to $N_{Re} = \infty$, modifying this with a factor involving the rate of flow, determined from the temperature, and the differential and static pressures. This method is used by the *American Gas Association*[3].

STEAM FLOW MEASUREMENT

While steam may be considered as a gas, its measurement differs from that of the usual gases because of a number of factors. Equation 48 serves as the starting point. Since it is usual to measure the differential pressure in inches of water, it is necessary to convert h_f, the head in feet

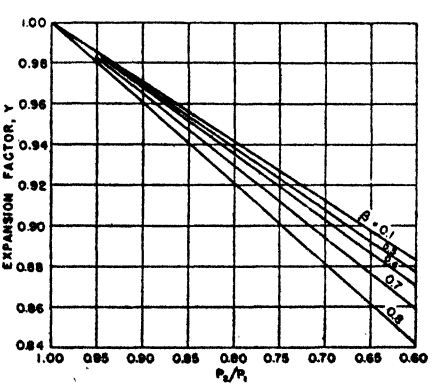

FIG. 12. EXPANSION FACTOR FOR AIR AND OTHER DIATOMIC GASES APPLICABLE TO FLANGE, RADIUS AND VENA CONTRACTA TAPS

in terms of the flowing fluid, to h_{aw}, the actual head in inches of water, using the equation

$$h_f = \frac{h_{aw}}{12} \frac{\rho_w}{\rho} \tag{56}$$

where

ρ_w = the density of water at 60 F (62.37 lb per cubic foot).
ρ = the density of the flowing fluid.

Substituting Equation 56 in Equation 48 gives

$$Q_f = 359.15\, KD_2^2 \sqrt{\frac{h_{aw}}{\rho}} \tag{57}$$

In steam measurement, a constant head of water is maintained over each leg of the manometer by means of condensing chambers, in order to keep the heat of the steam away from the meter. As the mercury

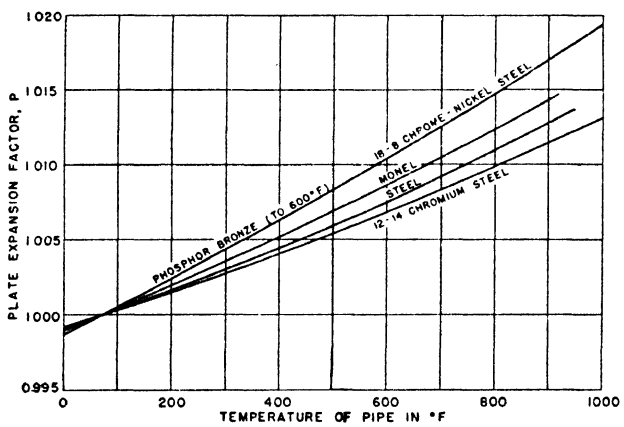

FIG. 13. VARIATION OF ORIFICE PLATE EXPANSION FACTOR, P, WITH TEMPERATURE AND MATERIAL

level fluctuates, the difference in head as recorded on the chart, therefore, is not that due to mercury alone, but to mercury minus an equivalent head of water. To correct for this, the equation

$$h_{aw} = h_w \frac{12.557}{13.557} \tag{58}$$

is applied to Equation 57. The denominator in Equation 58 is the specific gravity of mercury; and the numerator is the difference in specific gravity between mercury and water. Equation 57, hence, becomes

$$Q_f = 345.65\, KD_2^2 \sqrt{\frac{h_w}{\rho}} \tag{59}$$

Steam is commonly measured in terms of weight, and since

$$W = \rho Q_f \tag{60}$$

where

W = the rate of flow in pounds per hour.

$$W = 345.65\, KD_2^2 \sqrt{h_w \rho} \tag{61}$$

The expansion factor Y, and the factor P, correcting for the expansion of the orifice plate with the temperature must then be applied, so that

$$W = 345.65\, KYPD_2^2 \sqrt{h_w \rho} \tag{62}$$

which is the *final form of the equation for the flow of steam through orifices.* Values of K may be obtained from Figs. 7, 8, and 9, according to the pressure taps used. Y may be computed from Equation 55. Fig. 13 gives values of the correction factor P, according to the temperature and the material of the orifice plate. Values of the density, ρ, may be obtained from steam tables, such as Keenan and Keyes[4], which are widely used.

METERING LIQUIDS

Orifices are also used for metering liquids, and Equation 48 serves again as a starting point for developing the working formula. Again,

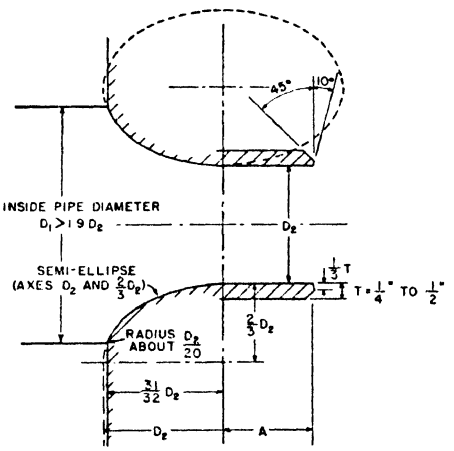

FIG. 14. SHAPE OF *ASME* LONG RADIUS NOZZLE WHEN RATIO OF THROAT TO PIPE DIAMETER IS 0.53 OR LESS

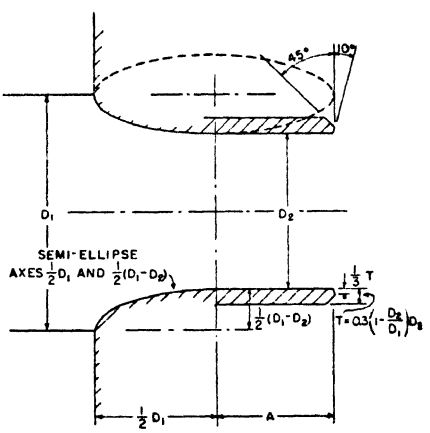

FIG. 15. SHAPE OF *ASME* LONG RADIUS NOZZLE WHEN RATIO OF THROAT TO PIPE DIAMETER IS 0.4 TO 0.7

too, it is necessary to convert h_f to h_{aw}, the actual head in inches of water, by substituting Equation 56. It is also necessary to correct for the weight of the fluid above the manometer, and since this may be other than water, it is better to use an equation of more general form than Equation 58:

$$h_{aw} = h_w \frac{13.557 - \frac{\rho_f}{\rho_w}}{13.557} \tag{63}$$

where

ρ_f = the density of the fluid over the mercury in the manometer.

ρ_w = the density of water at 60 F.

Substituting Equations 56 and 63 in Equation 48 gives

$$Q_f = 44.764\, KD_2^2 \sqrt{h_w \left(\frac{1}{\rho_f} - 0.00118\right)} \tag{64}$$

Then, since liquids are generally measured in gallons instead of cubic feet, and since there are 7.4805 gal in 1 cu ft,

$$Q_w = 334.86\, K D_2^2 \sqrt{h_w \left(\frac{1}{\rho_f} - 0.00118\right)} \qquad (65)$$

in which Q_w is the discharge or rate of flow, in gallons per hour.

Since liquids, for practical purposes, are incompressible, no expansion factor is necessary. If circumstances demand, the factor P for the expansion of the orifice may be applied. Also, if it is necessary to correct the volumetric discharge to a base temperature, application of the known expansion characteristics of the liquid will enable the conversion to be made. Values of K again are obtainable from Figs. 7, 8, and 9, according to the type of pressure tap.

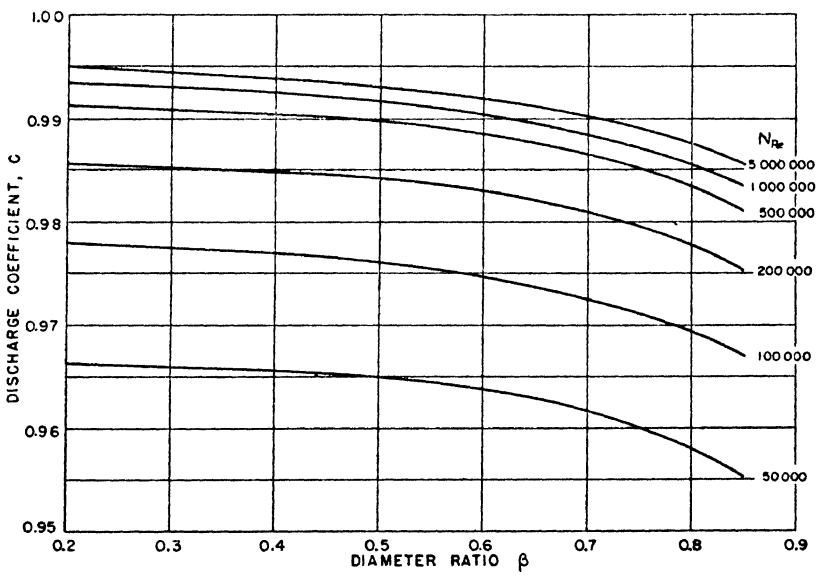

FIG. 16. RELATION OF NOZZLE DISCHARGE COEFFICIENT, C, FOR 2-INCH PIPE, TO DIAMETER RATIO AND REYNOLDS NUMBER

NOZZLE COEFFICIENTS AND EXPANSION FACTORS

Nozzles differ from orifices in that the flow is guided to the throat in such a way that contraction of the jet is suppressed, or, in other words, there is no vena contracta. Because of this fact, the coefficients are different from those of orifices, and are very close to unity before the velocity of approach factor is added. Also, the expansion factor may be deduced rationally, rather than empirically, as with orifices.

Two shapes of nozzles that have been under investigation by the *A.S.M.E.* for some time are shown in Figs. 14 and 15. They are referred to as long-radius nozzles. Their contour is that of a semi-ellipse, and the contracting portion is followed by a cylindrical section of the same area as the throat. The shape shown in Fig. 14 is designed for use with ratios of throat to pipe diameter of 0.53 or less, that of Fig. 15 for ratios of 0.4 to 0.7. The most usual location of pressure taps is 1 pipe diameter up-

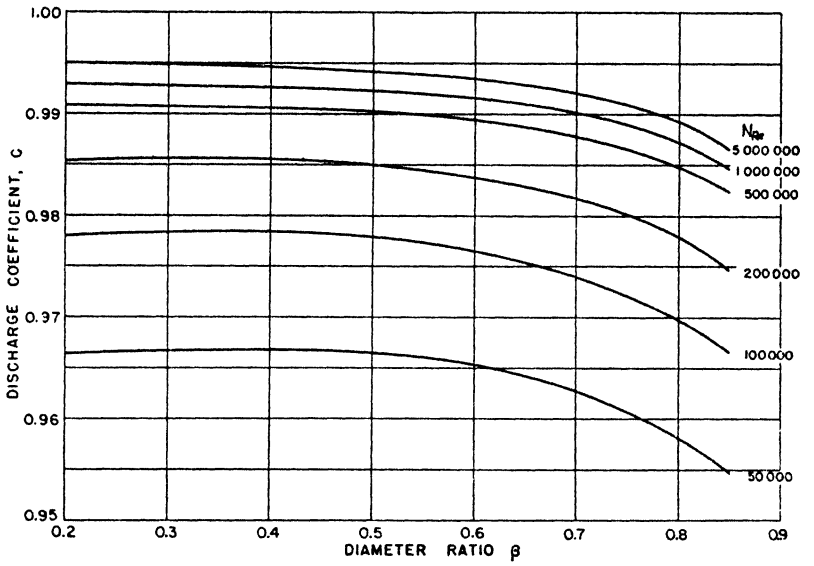

FIG. 17. RELATION OF NOZZLE DISCHARGE COEFFICIENT, *C*, FOR 6-INCH PIPE, TO DIAMETER RATIO AND REYNOLDS NUMBER

stream and ½ diameter downstream, both measured from the plane of the nozzle inlet. In addition, the *International Standards Association* has adopted still another shape of nozzle, which has a somewhat sharper approach than the *A.S.M.E.* nozzles, and which uses corner taps. Very little use of this nozzle has been made in this country.

The formulas already given for orifices apply equally to nozzles except for discharge coefficients, and for the expansion factor, when it is applied.

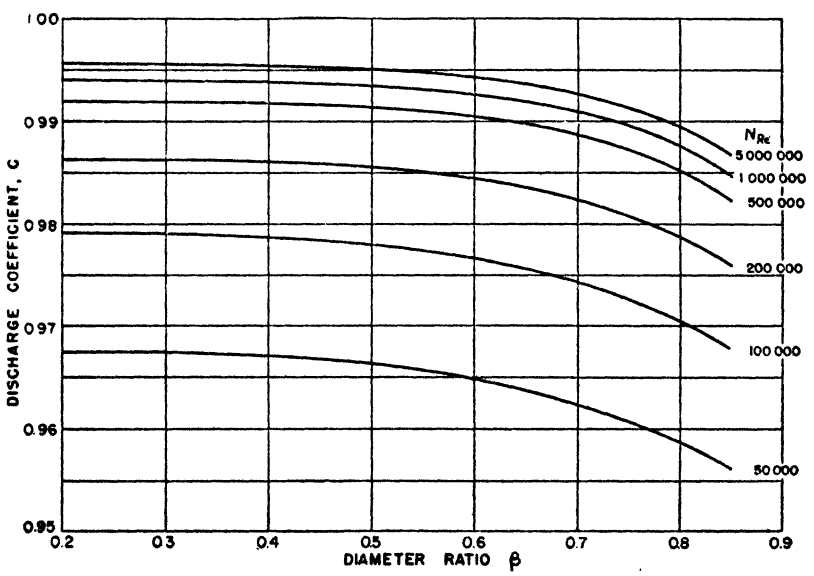

FIG. 18. RELATION OF NOZZLE DISCHARGE COEFFICIENT, *C*, FOR 10-INCH PIPE, TO DIAMETER RATIO AND REYNOLDS NUMBER

Discharge coefficients for nozzles, as for orifices, vary with pipe size; they may either increase or decrease with decreasing size of pipes depending on the sharpness of the approach curvature of the nozzle. For the *A.S.M.E.* nozzles, they tend to decrease. Generally speaking, too, the coefficient for a given nozzle shape is higher if the finish of the surface is smoother.

Discharge coefficients, C, for pipes 2, 6, and 10 in. in diameter are given in Figs. 16, 17, and 18, as correlated by Bean, Beitler and Sprenkle[5], as functions of the diameter ratio β and the Reynolds number N_{Re} (Equation 66) referred to the diameter of the throat in feet.

$$N_{Re} = \frac{D_2 V_2 \rho_1}{\mu_1} \tag{66}$$

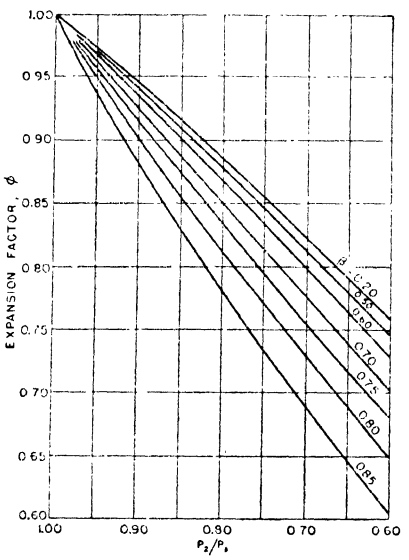

FIG. 19. RELATION OF EXPANSION FACTOR, φ, FOR NOZZLES TO DIAMETER RATIO AND PRESSURE LOSS FOR AIR AND OTHER DIATOMIC GASES

Coefficients from these curves must be multiplied by $\frac{1}{\sqrt{1-\beta^4}}$, the velocity of approach factor, in accordance with Equation 46, to obtain the value of K to use in the various equations.

The expansion factor for nozzles, designated by φ, is obtained from a rational formula, as already noted.

$$\varphi = \sqrt{\left(\frac{p_2}{p_1}\right)^{2/k} \left(\frac{k}{k-1}\right)\left(\frac{1-(p_2/p_1)^{k-1/k}}{1-p_2/p_1}\right)\left(\frac{1-\beta^4}{1-\beta^4 (p_2/p_1)^{2/k}}\right)} \tag{67}$$

This formula is plotted for $k = 1.40$ (air and other diatomic gases) and 1.30 (steam, carbon dioxide, natural gas) in Figs. 19 and 20, respectively.

FLOW MEASUREMENT BY PITOT TUBE

There remains one other head type meter useful in ventilating work, the Pitot tube, named for the Frenchman who discovered the principle. The Pitot tube is essentially a bent tube with its open end pointed upstream, combined with another tube with its end pointed crosswise to the flow or downstream, or connected to openings crosswise to the flow. Used with flowing liquid, the liquid will rise in each tube, but higher in the one pointed upstream. Used with a flowing gas, and the two tubes connected by a U-tube containing water, the liquid level in the U-tube will be displaced, with the lower level on the side connected to the tube pointed upstream. The tube directed upstream receives the impact pressure, which is the sum of the static and kinetic pressures, while the tube directed crosswise receives only the static pressure; the difference

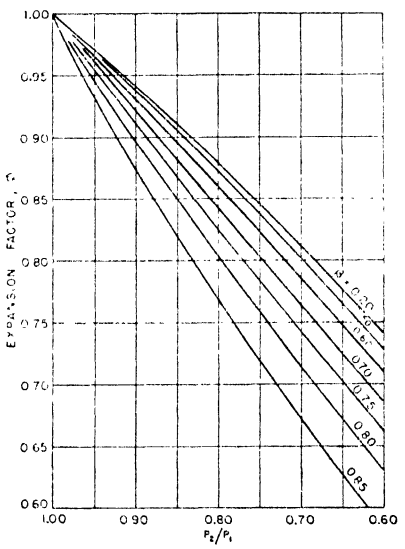

FIG. 20. RELATION OF EXPANSION FACTOR, φ, FOR NOZZLES TO DIAMETER RATIO AND PRESSURE LOSS FOR STEAM, CARBON DIOXIDE AND NATURAL GAS

between the two, as read on the separate tubes or on the U-tube is, of course, the kinetic pressure. The velocity is expressed as

$$V = \sqrt{2gh_f} \tag{68}$$

Application of Equation 56 serves to make the formula general, assuming that water is used in the manometer connecting the two tubes. Using this equation, and mutiplying by 60 to convert feet per second to feet per minute,

$$V_m = 1096.5 \sqrt{\frac{h_{aw}}{\rho}} \tag{69}$$

in which V_m is the rate of flow in feet per minute.

It is often difficult to obtain the exact static pressure. In the usual construction of Pitot tubes, the static pressure openings are downstream from the impact pressure opening, and turbulence induced by the nose

may affect the static pressure reading. If the static pressure openings point downstream in any degree, a suction effect is produced to falsify the reading. In instruments having the static pressure opening pointed downstream, the coefficient may be as low as 0.86. Consequently, for accurate work, Pitot tubes should be calibrated, and the pertinent coefficient should be applied to Equation 68. In a sense, this coefficient is advantageous, since it results in a higher differential reading, which, in turn, enables more accurate readings at low flows.

In using Pitot tubes, it is generally necessary to make a traverse of the pipe or duct to determine the course of the velocity pattern. In a pipe, for instance, one of the profiles shown in Fig. 5 would be obtained. Near a valve or fitting, however, the profile might be quite distorted, a fact which would be revealed by the traverse. If the pipe or duct is

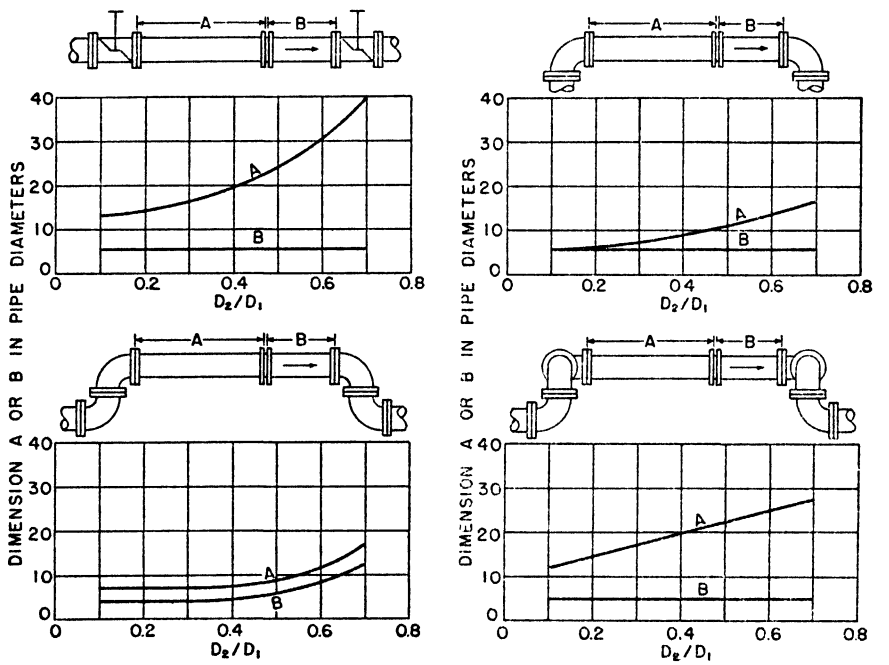

FIG. 21. MINIMUM CONDITIONS TO BE OBSERVED WHEN INSTALLING ORIFICES AND NOZZLES BETWEEN FITTINGS AND VALVES

divided into equal areas, and a determination of h_{aw} is made for each, the average velocity would be obtained by using the average of the square roots of h_{aw} in Equation 69.

INSTALLATION OF NOZZLES AND ORIFICES

A final note should be made of the installation of orifices and nozzles. Generally speaking, the orifice or nozzle, together with a holding arrangement, including pressure taps, is available from the manufacturer. In making the installation, the user should make certain that the flow approaching the nozzle or orifice is steady and evenly distributed, *i.e.*, with velocity profiles similar to those shown in Fig. 5. Fittings and valves,

which tend to direct the flow to one side and which in some cases cause it to rotate as it advances, must be far enough upstream from the orifice or nozzle to permit the disturbed stream to straighten out to the even form before reaching the meter. Minimum conditions in the installation for avoiding trouble from fittings and valves are shown in Fig. 21. If necessary, straightening vanes may be used upstream from the orifice or nozzle at a distance of not less than 8 pipe diameters.

LETTER SYMBOLS USED IN CHAPTER 4

β = ratio, throat or orifice diameter to pipe diameter.
μ = absolute viscosity in pounds per foot second.
μ/ρ = kinematic viscosity in square feet per second.
ρ = density of flowing fluid in pounds per cubic foot.
ρ_w = density of water at 60 F, (62.37 lb per cubic foot).
ρ_f = density of fluid over mercury in a manometer.
φ = expansion factor for nozzles.
A = cross-sectional area of flow, in square feet.
C = correction factor (coefficient of discharge) for flow through orifice, nozzle or Venturi.
c_p = specific heat of gas at constant pressure.
c_v = specific heat of gas at constant volume.
D = diameter of fluid stream in feet.
d = internal diameter of pipe in feet.
E = mechanical work in foot pounds per pound of fluid flowing.
e = absolute roughness of pipe surface, in feet.
f = dimensionless friction coefficient.
g = acceleration due to gravity = 32.17 ft per (second) (second).
G = specific gravity of gas referred to air.
h = enthalpy, Btu per pound of fluid.
h_{aw} = loss of head in inches of water.
h_f = loss of head in feet of fluid.
h_t = total head in feet of fluid.
h_w = differential pressure in inches of water.
J = mechanical equivalent of heat = 778 foot pounds per Btu.
K = flow coefficient (correction factor), including velocity of approach correction factor, for flow through orifice, nozzle or Venturi.
k = ratio of specific heat at constant pressure to specific heat at constant volume.
L = perpendicular distance from axis of pipe in feet.
l = length of pipe in feet.
N_{Re} = Reynolds number.
P = correction factor for expansion of orifice plate with temperature.
p = pressure in pounds per square foot.
p_c = critical pressure.
P_b = standard pressure to which correction is to be made, pounds per square inch, absolute.
P_f = pressure of gas flowing, pounds per square inch, absolute.
Q_b = rate of flow in cubic feet per hour under standard conditions of pressure and temperature.
Q_f = rate of flow in cubic feet per hour.
Q_s = discharge rate in cubic feet per second.
Q_w = rate of flow in gallons per hour.
q = heat transferred to the fluid per pound of fluid flowing.
R = gas constant.
R_H = hydraulic radius = ratio of area of cross-section to wetted perimeter of cross-section.
r = radius of pipe in feet.

T = temperature, Fahrenheit degrees, absolute.
T_b = standard temperature to which correction is to be made, Fahrenheit degrees absolute.
T_f = temperature of gas flowing, Fahrenheit degrees, absolute.
u = internal energy, Btu per pound of fluid.
V = velocity in feet per second.
V_c = critical velocity, feet per second.
V_{so} = velocity of sound, feet per second.
V_m = velocity in feet per minute.
v = specific volume, cubic feet per pound.
W = weight of gas flowing, pounds per hour.
Y = expansion factor—correcting for expansion of gas under reduced downstream pressure.
z = elevation above some arbitrary datum, in feet.

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Chapter 5

FUNDAMENTALS OF HEAT TRANSFER

Conduction, Convection, Radiation, Combined Convection and Radiation, Heat-Flow Resistance, Practical Heat Transfer Problems, Unit Conductances for Convection Flow Systems, Radiation Factors or Emissivities, Solutions for Steady-State Conduction Problems

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HEAT is that form of energy that is transferred by virtue of an existing temperature difference. The temperature difference is the potential which causes the transfer, the latter in turn being resisted by the thermal properties of the material combined in a single term known as the resistance. Energy exchange associated with evaporation, condensation, etc. is treated elsewhere such as in the section on *cooling tower design* in Chapter 37. The objectives of this chapter are to:

1. Describe the mechanisms and present the rate equations for the different modes of heat transfer.

2. Illustrate the application of the basic concepts to steady-state problems (temperature independent of time or a cyclic variable thereof) by means of several typical solutions of heat transfer systems.

Further applications to specific systems will be found throughout THE GUIDE.

CONDUCTION, CONVECTION AND RADIATION

Thermal conduction is the term applied to the mechanism of heat transfer whereby the molecules of higher kinetic energy transmit part of their energy to adjacent molecules of lower kinetic energy by direct molecular action. Since the temperature is proportional to the average kinetic energy of the molecules, thermal transfer will occur in the direction of decreasing temperature. The motion of the molecules is random; there is no net material flow associated with the conduction mechanism. In the case of flowing fluids, thermal conduction is significant in the region very close to a solid boundary or wall, for in this region the flow is laminar, parallel with the wall surface, and there are practically no cross currents in the direction of the heat transfer across the solid fluid boundary. In solid bodies the significant mechanism of heat transfer is always thermal conduction.

Contrasted to the thermal conduction mechanism, *thermal convection* involves energy transfer by eddy mixing and diffusion [1] in addition to conduction. This is shown schematically in Fig. 1 which exhibits transfer from a pipe wall at surface temperature t_s to a colder fluid at a bulk temperature t_f. (Bulk temperature is that which would be attained if the fluid stream were drawn off at a certain section and mixed. It is therefore slightly higher than the lowest temperature in the stream). In the *laminar* sublayer, immediately adjacent to the wall, the heat transfer occurs by thermal conduction; in the *transition* region, which is called the buffer layer, eddy mixing as well as conduction effects are significant; in the *eddy* or *turbulent* region the major fraction of the transfer occurs by eddy mixing.

In most commercial equipment the main body of the fluid is in turbulent flow, and the laminar film exists at the solid walls only, as shown in

Fig. 1. But in cases of low-velocity flow in small tubes, or with viscous liquids such as heavy oil (low Reynolds numbers), the entire flow may be laminar. In these latter cases there is no transition or eddy region.

When the fluid currents are produced by sources external to the heat transfer region, as for example by a pump, the described solid to fluid heat transfer is termed *forced convection.* In contrast, if the fluid currents are generated internally, as a result of non-homogeneous densities arising from the temperature variations, the heat transfer is termed *free convection.*

In the conduction and convection mechanisms heat is transferred as internal energy, *i.e.*, the random molecular kinetic energy associated with the material temperature. For *radiant heat transfer*, however, a change in energy form takes place from internal energy at the source to electromagnetic energy for transmission, then back to internal energy at the receiver.

The rate of heat transfer, corresponding to the three transfer mechanisms previously described, may be expressed by three rate equations.

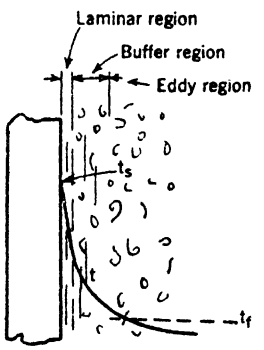


FIG. 1. THERMAL CONVECTION CONDITIONS

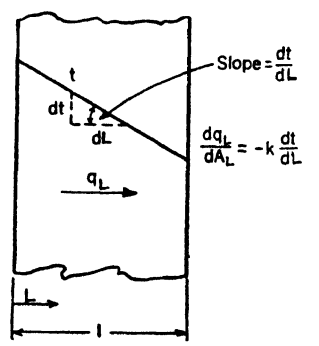


FIG. 2. THERMAL CONDUCTION IN A FLAT SLAB

These are similar to Ohm's Law for electrical flow, the current flow through a resistance being proportional to the potential difference.

Thermal Conduction Equation

Equation 1 states symbolically that the thermal conduction per unit transfer area normal to the flow, $(dq)/(dA)$, Btu per (hour) (square foot), is proportional to the temperature gradient $(dt)/(dL)$, Fahrenheit degrees per foot. The proportionality factor is termed the *thermal conductivity*, k, Btu per (hour) (square foot) (Fahrenheit degree per foot of thickness).

$$\frac{dq}{dA} = -k\frac{dt}{dL} \tag{1}$$

The minus sign on the right side of the equation is introduced to indicate positive transfer in the direction of decreasing temperature. Fig. 2 shows the physical significance of indicated quantities.

It should be emphasized that the thermal conductivity used should be expressed in consistent units; either using the inch or foot throughout.

Expressions of conductivity used in the heating field are usually

inconsistent in this sense, in that it is customary to refer to the conductivity *per square foot* but for one inch of thickness. This custom has been adopted for the reason that wall thicknesses are usually expressed in inches, whereas if expressed in feet, decimal or fractional thicknesses would result. When dealing with flat walls no complication is involved in using the inconsistent expression of conductivity. However, when curved or spherical walls are considered, considerable complication is involved. Therefore, in this discussion the consistent units of conductivity expressed in *Btu per (hour) (square foot) (Fahrenheit degrees per one foot thickness)* are used throughout. *Conductivity values obtained from Chapter 6 or Table 1 in this chapter, which are expressed in inconsistent units, must therefore be converted for use in the calculations of this chapter by dividing by 12.* As an example, the conductivity of brick, expressed in inconsistent units as 5.0 in Table 2 of Chapter 6, becomes 0.42 when

TABLE 1. APPROXIMATE UNIT THERMAL CONDUCTIVITIES[a]

Conductivity, k = Btu per (hr) (sq ft) (F deg per in.)

MATERIAL	*k*	MATERIAL	*k*
Air	0.168	Lead	240.0
Aluminum	1416.0	Nickel	408.0
Brass (70 − 30)	720.0	Soil	2.4—12.0
Cast-Iron	336.0	Steel, mild	312.0
Copper	2640.0	Water, liquid	4.08
Glass	3.6—7.32		

[a]Thermal conductivities depend to some extent on temperature. The above magnitudes are approximate only. Refer to Heat Transmission, 2nd edition, by W. H. McAdams (McGraw-Hill Co., 1942) for additional values.

used in the calculations of this chapter. Also, it should be emphasized that in order to make the calculations and applications consistent in this chapter, *all dimensions of thickness must be expressed in feet.*

Thermal Convection Equation

$$\frac{dq}{dA} = h_c (t_s - t_f) \tag{2}$$

This rate equation states that the thermal convection per unit transfer area $(dq)/(dA)$, Btu per (hour) (square foot) is proportional to the temperature difference, $(t_s - t_f)$ which is the temperature of the surface less that of the fluid. The particular fluid temperature to use for a given system will be noted under the discussion of that system. The proportionality factor is termed the *unit convection conductance* (sometimes called the film coefficient for convection), h_c, Btu per (hour) (square foot) (Fahrenheit degree). These convection conditions are illustrated in Fig. 1.

The heat transmission by free or natural convection for objects surrounded by air can be conveniently expressed as in Equation 2a:

$$q_c = C \left(\frac{1}{D}\right)^{0.2} \left(\frac{1}{T_{av}}\right)^{0.181} (t_s - t_f)^{1.27} \tag{2a}$$

where

q_c = heat transmission by convection, Btu per (square foot) (hour).
C = a constant depending upon the shape of the surface.

D = diameter of pipe or circular duct or height of vertical wall, inches. (Effect of diameter or height becomes constant at 24 in.)

T_{av} = average of wall surface and surrounding air temperature, Fahrenheit degrees absolute.

$t_s - t_f$ = temperature excess between wall surface and surrounding air, Fahrenheit degrees.

For horizontal cylinders, the value of $C = 1.016$ has been well established by various investigations. For vertical plates, the value of $C = 1.394$ has been fairly well established. Suggested values [2] of C for horizontal plates warmer than the surrounding air are 1.79 when facing upward and 0.89 when facing downward.

TABLE 2. HEAT TRANSMISSION BY FREE CONVECTION FOR LARGE VERTICAL SURFACES

Expressed in Btu per (square foot) (hour)

	TEMPERATURE DIFFERENCE BETWEEN BODY AND SURROUNDING STILL AIR AT 80 F												
F DEG	0	10	20	30	40	50	60	70	80	90	100	110	120	130
0	0	4.4	10.4	17.4	25.0	33.2	41.8	50.6	59.9	69.4	79.4	89.2	99.4	109.8
1	0.3	4.9	11.1	18.1	25.8	34.1	42.6	51.5	60.8	70.3	80.4	90.2	100.4	110.9
2	0.6	5.5	11.8	18.9	26.7	34.9	43.5	52.4	61.8	71.3	81.4	91.2	101.5	112.0
3	1.0	6.0	12.5	19.7	27.5	35.7	44.3	53.4	62.7	72.3	82.4	92.2	102.6	113.0
4	1.4	6.6	13.2	20.5	28.3	36.6	45.2	54.3	63.7	73.3	83.3	93.3	103.6	114.1
5	1.8	7.3	13.9	21.2	29.2	37.4	46.1	55.2	64.6	74.3	84.2	94.3	104.7	115.2
6	2.3	7.9	14.6	22.0	30.0	38.3	47.0	56.1	65.6	75.3	85.2	95.3	105.7	116.3
7	2.8	8.5	15.3	22.7	30.8	39.1	47.8	57.1	66.5	76.3	86.2	96.3	106.7	117.3
8	3.3	9.1	16.0	23.5	31.6	40.0	48.7	58.0	67.5	77.4	87.2	97.4	107.8	118.4
9	3.8	9.7	16.7	24.3	32.4	40.9	49.7	59.0	68.4	78.4	88.2	98.4	108.8	119.5

The heat transmission by free convection from vertical walls *24 in. or more in height* is given in Table 2 as calculated from Equation 2a for an ambient air temperature of 80 F. The values in Table 2 are not changed appreciably by a considerable change in air temperature for a given temperature excess. For instance, a change in air temperature from 80 to 40 F will increase the heat transmission given in Table 2 by only 1.3 per cent.

Table 2 can also be used for calculating the free convection rate of transmission for various commercial shapes such as pipes and ducts. These calculations are simplified by the use of the factors in Tables 3 and 4. Table 3 gives factors by which the values in Table 2 must be multiplied to obtain the free convective transfer from various shapes *whose characteristic dimensions are 24 in. or over*, and Table 4 gives the factors to be used in conjunction with the factors in Table 3 for obtaining the free convection from Table 2 for pipes and ducts *whose characteristic dimensions are less than 24 in.*

For example, the free convection transfer from a 3 in. O.D. horizontal cylinder for a temperature difference of 40 deg = 25.0 × 0.73 × 1.52 = 27.7 Btu per (square foot) (hour).

Problems in either forced convection or natural convection may be solved by the simple first-power equation if the convection coefficient is expressed as a unit conductance:

$$q_c = h_c A (t_1 - t_2) \qquad (2b)$$

where

q_c = heat transmission by convection, Btu per hour.

A = surface area, square feet.

$t_1 - t_2$ = temperature difference between the surface and the fluid Fahrenheit degrees.

h_c = unit conductance, from Table 5, Btu per (square foot) (hour) (Fahrenheit degree temperature difference.)

TABLE 3. FREE CONVECTION FACTORS FOR VARIOUS SHAPES

SHAPES	FACTOR
Horizontal cylinders 24 in. in diam. or over	0.73
Long vertical cylinders 24 in. in diam. or over	0.88
Vertical plates 24 in. in height or over	1.00
Horizontal plates warmer than air facing upward	1.28
Horizontal plates warmer than air facing downward	0.64
Horizontal plates cooler than air facing upward	0.64
Horizontal plates cooler than air facing downward	1.28

TABLE 4. FREE CONVECTION FACTORS FOR VARIOUS DIAMETER PIPES OR VARIOUS HEIGHT PLATES

Actual O.D., or height, in.	1	2	3	4	5	6	7	8
Factor	1.88	1.64	1.52	1.43	1.37	1.32	1.28	1.25
Actual O.D., or height, in.	9	10	12	14	16	18	20	22
Factor	1.22	1.19	1.15	1.11	1.09	1.06	1.04	1.02

Thermal Radiation Equation

The relation shown in Equation 3 is usually applicable to systems in which radiant exchange takes place between the surfaces of solids, as sche-

$$q_r = \sigma A_1 F_A F_E (T_1^4 - T_2^4) \qquad (3)$$

matically shown in Fig. 3. Gaseous and luminous radiation are not considered in this discussion. Equation 3 states that the net radiation per unit transfer area of surface 1, q_r/A Btu per (hour) (square foot), which *sees* surface 2 through a non-absorbing medium, is proportional to the difference of the fourth powers of the absolute surface temperatures $(T_1^4 - T_2^4)$. The proportionality factor $(\sigma F_A F_E)$ may be conveniently separated into three parts:

σ = the Stefan-Boltzmann radiation constant.

= 1730×10^{-12} Btu per (hour) (square foot) (Fahrenheit degree absolute temperature to the fourth power).

F_A = the configuration factor which is dimensionless and $\leqq 1$. This factor accounts for the shape and relative position of the two surfaces. The value of $F_A = 1$ may be used in the cases of large parallel planes, long concentric cylinders or smaller bodies in large enclosures.

F_E = the emissivity factor which is also dimensionless and $\leqq 1$. This factor accounts for the absorption and emission characteristics of the surfaces for the radiation which exists. Individual emissivities (ε) should be taken from Table 6 and applied, for either radiation or absorption, as follows:

a. For a small body in a large enclosure, use the emissivity of the small body only: $F_E = \varepsilon_1$.

b. For large parallel planes, long concentric cylinders or large enclosed bodies, use both emissivities in the equation:

$$F_E = \frac{1}{\frac{1}{\epsilon_1} + \frac{1}{\epsilon_2} - 1}$$

The radiation under black-body conditions, or for an emissivity of 1.0, is given in Table 7[3] for cold surfaces as low as −39 F to warmer surfaces as high as 139 F. The emissivities of a number of surfaces ordinarily encountered in engineering practice are shown in Table 6. For radiation table at higher temperatures, and further discussion of radiation calculations, see Chapter 31.

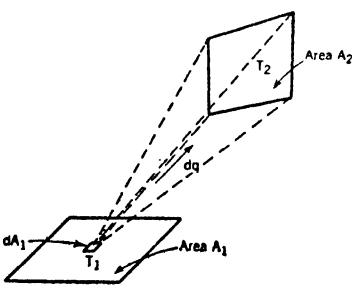


FIG. 3. RADIATION BETWEEN SURFACES

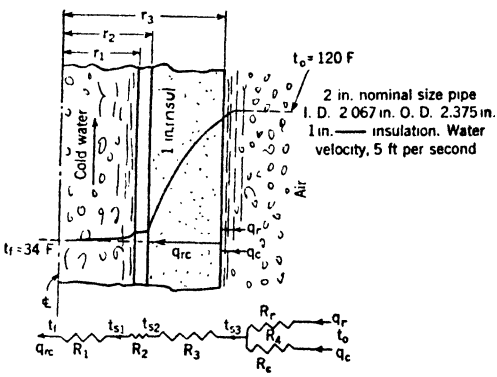


FIG. 4. HEAT TRANSFER CONDITIONS IN AN INSULATED COLD WATER LINE

NOMENCLATURE AND DIMENSIONS FOR TABLE 5

c_p = fluid unit heat capacity at constant pressure, Btu per (pound) (Fahrenheit degree).

D = cylinder diameter, feet.

G = 3600 $V_s\rho$ = fluid mass velocity, pounds per (hour) (square foot of flow cross-section).

ρ = density, pounds per cubic foot.

h_c = unit conductance for thermal convection, Btu per (hour) (square foot) (Fahrenheit degree).

k = unit thermal conductivity of the fluid, Btu per (hour) (square foot) (Fahrenheit degree per one foot thickness).

R_H = hydraulic radius of the flow cross-section = flow cross-section area per wetted perimeter, feet.

s = fin spacing, feet.

t = average fluid film temperature, Fahrenheit degree.

$t_1 - t_2$ = temperature difference surface to main fluid, Fahrenheit degree.

V_s = fluid velocity, feet per second.

μ = fluid viscosity, pounds per (hour) (foot) = viscosity in centipoises × 2.42.

Combined Convection and Radiation

It should be noted that the previous equations and tables give the heat transfer by convection and by radiation computed separately. In many

TABLE 5. APPROXIMATE UNIT CONDUCTANCES FOR THERMAL CONVECTION FOR SEVERAL FLOW SYSTEMS[a]

Expressed in Convenient Empirical Form

CASE	SYSTEM	UNIT CONDUCTANCE EQUATION[b]
	FORCED CONVECTION	
1.	Longitudinal flow in cylinders, turbulent region. Fluid being heated[c].	$\frac{h_c D}{k} = 0.0225 \left(\frac{DG}{\mu}\right)^{0.8} \left(\frac{c\mu}{k}\right)^{0.4}$ For $\left(\frac{DG}{\mu}\right) > 3000$
2.	For longitudinal air flow in cylinders case 1 reduces to[c].	$h_c = 0.0036\, G^{0.8}/D^{0.2}$ For $\left(\frac{DG}{\mu}\right) > 3000$
3.	For longitudinal water flow in cylinders case 1 reduces to[c].	$h_c = 0.00486\,(1 + 0.01t)\,\frac{G^{0.8}}{D^{0.2}}$ For $\left(\frac{DG}{\mu}\right) > 3000$
4.	Air flow normal to a single right circular cylinder.	$h_c = 0.45 \left(\frac{k}{D}\right) + 0.178\, G^{0.56} \left(\frac{k}{D}\right)^{0.44}$
5.	Air flow over staggered pipe banks.	$h_c = 0.061 \left(\frac{k}{D}\right)^{0.31} G^{0.52}$
6.	Air flow over single spheres.	$h_c = 0.040\,\frac{G^{0.52}}{D^{0.48}}$ $0 < t < 250$ F
7	Air flow over plane surfaces.	$h_c = 1 + 0.22\, V_s$ For $V_s < 16$ fps or $h_c = 0.53\, V_s^{0.8}$ 16 fps $< V_s <$ 100 fps
8.	Air flow normal to finned cylinders.	$h_c = 6.2 \left(\frac{G}{3600}\right)^{0.8} \frac{s^{0.22}}{D^{0.52}}$ $0 < t < 250$ F
	FREE CONVECTION[d]	
9.	Single horizontal right circular cylinder in air.	$h_c = 0.23 \left(\frac{t_1 - t_2}{D}\right)^{0.25}$
10.	Vertical surfaces in air.	$h_c = 0.3\,(t_1 - t_2)^{0.25}$
11.	Top surface of horizontal plates to air.	$h_c = 0.4\,(t_1 - t_2)^{0.25}$
12.	Bottom surface of horizontal plates to air.	$h_c = 0.2\,(t_1 - t_2)^{0.25}$

[a] Heat Transmission, by W. H. McAdams.

[b] Fluid properties should be evaluated at the arithmetic mean fluid temperature, $t_f = (t_{\text{surface}} + t_{\text{fluid}})$ divided by 2.

[c] These expressions are applicable to longitudinal flow in other than right circular cylinders provided the hydraulic radius is employed as the conduit dimension parameter. For non-circular cross-sections $D = 4\,R_H$.

[d] For low rates of heat transfer by free convection the exponent decreases towards zero, and for higher rates increases towards 0.33. The following equations employing an exponent equal to 0.25 are applicable in the intermediate range.

practical cases it is desirable to treat convection and radiation as a single combined process, using a first-power equation:

$$q_{rc} = h_{rc} A (t_1 - t_2) \quad (4)$$

where q_{rc} is the total heat flow due to radiation and convection, in Btu per hour. Values of h_{rc}, the surface or film conductance for combined

TABLE 6. RADIATION FACTORS OR EMISSIVITIES, ϵ.
For the determination of factor F_E in Equation 3

CLASS	SURFACES	FRACTION OF BLACK-BODY RADIATION		ABSORPTIVITY FOR SOLAR RADIATION
		At 50–100 F	At 1000 F	
1	A small hole in a large box, sphere, furnace, or enclosure	0.97 to 0.99	0.97 to 0.99	0 97 to 0.99
2	Black non-metallic surfaces such as asphalt, carbon, slate, paint, paper	0.90 to 0.98	0.90 to 0.98	0.85 to 0.98
3	Red brick and tile, concrete and stone, rusty steel and iron, dark paints (red, brown, green, etc.)	0.85 to 0.95	0.75 to 0.90	0.65 to 0.80
4	Yellow and buff brick and stone, firebrick, fire clay	0.85 to 0.95	0.70 to 0.85	0.50 to 0.70
5	White or light-cream brick, tile, paint or paper, plaster, whitewash	0.85 to 0.95	0.60 to 0.75	0.3 to 0.5
6	Window glass	0.90 to 0.95	.....	Transparent[a]
7	Bright aluminum paint; gilt or bronze paint	0.4 to 0.6	.....	0.3 to 0.5
8	Dull brass, copper, or aluminum; galvanized steel; polished iron	0.2 to 0.3	0.3 to 0.5	0.4 to 0.65
9	Polished brass, copper, monel metal	0.02 to 0.05	0.05 to 0.15	0.3 to 0.5
10	Highly polished aluminum, tin plate, nickel, chromium	0.02 to 0.04	0.05 to 0.10	0.10 to 0.40

[a]Reflects about 8 per cent

radiation and convection, are given in Chapter 6, Table 1 and Fig. 3. Complete tables for the combined heat transfer of steam and hot water radiators, pipes, coverings, etc., will be found in the appropriate chapters.

When dealing with the effect of operating temperatures upon the combined heat transfer of a given piece of equipment (as for instance a steam radiator), another form of equation is frequently used:

$$q_{rc} = B A (t_1 - t_2)^n \quad (5)$$

Values of n in this equation usually range from 1.3 to 1.5 (see Chapter 25). The chief advantage of this equation is the convenience of representing heat transfer performance on logarithmic coordinates, and the factor B should be regarded as a simple constant of proportionality.

HEAT-FLOW RESISTANCE

In most of the steady-state heat transfer problems encountered in air conditioning applications, more than one of the heat transfer mechanisms are effective, and the thermal current flows through several resistances in series or in parallel. In using the resistance concept the calculations involved are analogous to the application of Ohm's Law in electricity, *viz.*, the heat flow or thermal current is directly proportional to the thermal

TABLE 7. HEAT TRANSMISSION BY RADIATION FOR BLACK-BODY CONDITIONS[a]

Expressed in Btu per (square foot) (hour)

TEMP F DEG	0	−1	−2	−3	−4	−5	−6	−7	−8	−9
−30	59.3	58.7	58.2	57.7	57.2	56.7	56.2	55.7	55.2	54.7
−20	65.2	64.7	64.1	63.5	62.9	62.3	61.7	61.1	60.5	59.9
−10	71.4	70.8	70.1	69.5	68.9	68.3	67.7	67.1	66.4	65.8
0	78.0	77.4	76.7	76.0	75.4	74.7	74.0	73.4	72.7	72.1
	0	+1	+2	+3	+4	+5	+6	+7	+8	+9
0	78.0	78.7	79.4	80.1	80.8	81.5	82.2	82.9	83.6	84.3
10	85.0	85.7	86.5	97.2	88.0	88.7	89.4	90.2	90.9	91.7
20	92.4	93.3	94.0	94.8	95.6	96.4	97.2	98.0	98.8	99.6
30	100	101	102	103	104	105	105	106	107	108
40	109	110	111	112	112	113	114	115	116	117
50	118	119	120	121	122	123	123	124	125	126
60	127	128	129	130	131	132	133	134	135	136
70	137	138	139	140	142	143	144	145	146	147
80	148	149	150	151	152	153	154	155	156	157
90	159	160	161	162	163	164	166	167	168	169
100	170	171	173	174	175	176	178	179	180	182
110	183	184	185	187	188	189	191	192	193	195
120	196	197	199	200	201	203	204	206	207	209
130	211	212	214	215	217	218	220	221	222	224

[a]*Example:* Radiation from walls of room at 32 F to surface at − 25 F for effective emissivity of 0.95 = (102 − 62.3) 0.95 = 37.7 Btu per (square foot) (hour).

potential or temperature difference, and inversely proportional to the thermal resistance:

$$q_{rc} = \frac{t_1 - t_2}{R} \tag{6}$$

Following the electrical analogy, when there is a thermal current flowing through several *resistances in series*, the resistances are additive:

$$R_T = R_1 + R_2 + R_3 + \ldots\ldots + R_n \tag{7}$$

Similarly, conductance is the reciprocal of resistance, and for heat flow through several *resistances in parallel*, the conductances are additive:

$$C_T = \frac{1}{R_T} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} + \ldots\ldots + \frac{1}{R_n} \tag{8}$$

Practical Heat Transfer Problems

The use of these relations for resistance and conductance makes possible the solution of many practical heat transfer problems. As discussed in Chapters 6, 7 and 28, the practical analyses of heat transfer in building walls, in fin-tube coils and in pipe coverings, are usually computed by this

method. The same resistance analysis may be applied to complicated steady-state *conduction* problems. Table 8 gives the resistances in six common cases of steady-state conduction.

A complete analysis by the resistance method is well illustrated by considering the heat transfer from the air outside to the cold water inside of an insulated pipe. The temperature gradients and the nature of the resistance analysis are indicated by the two sketches of Fig. 4.

Since air is sensibly transparent to radiation, there will be some heat transfer by both radiation and convection to the outer insulation surface. The mechanisms act in parallel on the air side. The total transfer by radiation and convection then passes through the insulating layer and the pipe wall by thermal conduction, and thence by convection and radiation into main cold water streams. (Radiation is not significant on the water side as liquids are sensibly opaque to radiation, although water transmits energy in the visible region). The contact resistance between the insulation and the pipe wall is presumed to be equal to zero.

Referring to Fig. 4, the heat transferred for a given length N of pipe, q_{rc}, Btu per hour, may be thought of as flowing through the parallel resistances R_r and R_c, associated with the insulation surface radiation and convection transfer. Then the flow is through the resistance offered to thermal conduction by the insulation, R_3, through the pipe wall resistance, R_2, and into the water stream through the convection resistance, R_1. Note the analogy to the direct current electrical circuit problem. A temperature (potential) drop is required to overcome these resistances to the flow of thermal current. The total resistance to heat transfer, R_T, hour Fahrenheit degrees per Btu, is the summation of the individual resistances:

$$R_T = R_1 + R_2 + R_3 + R_4 \tag{9}$$

where the resultant parallel resistance R_4 is obtained from:

$$\frac{1}{R_4} = \frac{1}{R_r} + \frac{1}{R_c}$$

Provided the individual resistances may be evaluated, the total resistance can be obtained from this relation. Then the heat transfer for the length of pipe (N, ft) can be established by the relation:

$$q_{rc}\ (\text{Btu per hour}) = \frac{t_o - t_f}{R_T} \tag{10}$$

For a unit length of the pipe the heat transfer rate is:

$$\frac{q_{rc}}{N}\ (\text{Btu per hour foot}) = \frac{(t_o - t_f)}{R_T N} \tag{11}$$

The temperature drop, Δt, through an individual resistance may then be calculated from the relation:

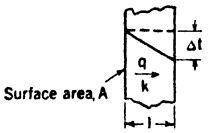
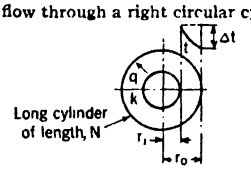
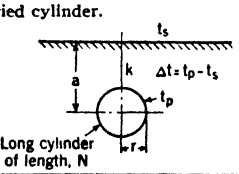
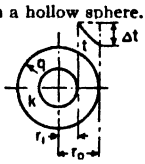
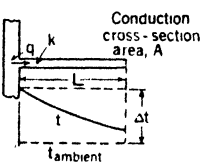
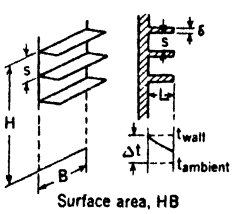
$$\Delta t = R\, q_{rc}$$

where R is the resistance in question.

The problem is now reduced to one of evaluating the individual resistances of the system. This entails suitable integration of the rate Equations 1, 2 and 3 to produce expressions of the form:

$$q = \frac{\Delta t}{R} \tag{12}$$

TABLE 8. SOLUTIONS FOR SOME STEADY-STATE THERMAL CONDUCTION PROBLEMS[a,b]

No.	SYSTEM	Expressions for the resistance R entering into the equation: $q = \Delta t/R$ (Btu per hour)
1.	Flat wall or curved wall if curvature is small (wall thickness less than 0.1 of inside diameter). 	$R = \frac{L}{kA}$
2.	Radial flow through a right circular cylinder. 	$R = \frac{\log_e \frac{r_o}{r_i}}{2\pi kN}$ (See footnote *c*).
3.	The buried cylinder. 	$R = \frac{\log_e \frac{2a}{r}}{2\pi kN}$; $R = \frac{\cosh^{-1} \frac{a}{r}}{2\pi kN}$ for $\frac{a}{r} \geq 3$ (See footnote *c*).
4.	Radial flow in a hollow sphere. 	$R = \frac{\frac{1}{r_i} - \frac{1}{r_o}}{4\pi k}$
5.	The straight fin or rod heated at one end. 	$R = \frac{m}{h_s p \tanh mL}$ (see footnotes *d* and *e*). For $ml > 2.3$, $\tanh mL \approx 1$ $m = \sqrt{h_s p/kA}$ A = conduction cross-section area. p = perimeter of cross-section A. h_s = unit conductance to the surroundings from the fin surface. k = thermal conductivity fin material. Δt = wall temperature—ambient temperature
6.	Finned surface of area HB. 	$R = \frac{(s+\delta)}{h_s\left(\frac{2}{m}\tanh ml + s\right)HB}$ $m = \sqrt{\frac{h_s p}{kA}} = \sqrt{\frac{2\,h_s}{k\delta}}$ Δt defined as in Case 5 above.

[a]The dimensions to be employed in these solutions are: length of dimension p, L, r = feet; units of k = Btu per (hour) (square foot) (Fahrenheit degree for one foot thickness); units of h, Btu per (hour) (square foot) (Fahrenheit degree); units of area, A = square feet.

[b]The thermal conductivity, k, in these solutions should be taken at the average material temperature (see Table 5).

[c]$\text{Log}_e\, x = 2.303 \log_{10} x$.

[d]This expression can also be employed as an approximation for tapered fins or of annular fins by employing average magnitudes of A and p.

[e]Tanh is the hyperbolic tangent.

where q is the heat transfer rate, and Δt is the potential drop or temperature difference through the resistance R. Table 8 lists such solutions for six different conduction systems. Table 2 in Chapter 6 and Table 1 of this chapter indicate the magnitudes of the thermal conductivities, k, to be employed in the expressions of Table 8, after dividing k by 12.

The solution applicable to the problem depicted in Fig. 4, for the calculation of R_2 and R_3, is case 2 in Table 8. Thus for a *1 ft length* of 2 in. nominal size pipe (I. D. = 2.067 in., O. D. = 2.375 in.) insulated with 1 in. of material having a conductivity of 0.025:

$$R_2 = \frac{\log_e \frac{1.188}{1.033}}{2\pi \times 26 \times 1} = 8.5 \times 10^{-4} \text{ hr Fahrenheit degree per Btu.}$$

$$R_3 = \frac{\log_e \frac{2.188}{1.188}}{2\pi \times 0.025 \times 1} = 3.9 \text{ hr Fahrenheit degree per Btu.}$$

The convection resistances to heat transfer from the pipe wall to the cold water, R_1, and from the air to the surface of the insulating material, R_c, are dependent on the flow conditions prevailing at these surfaces, and on the thermal properties of the fluids. The unit conductances for thermal convection, h_c, Btu per (hour) (square foot) (Fahrenheit degree), have been determined by test for many flow systems. These data may be employed to predict the conductances for *similar flow systems*. Table 5 summarizes some empirical equations expressing such test results.

For the problem under consideration (Fig. 4) case 3 of Table 5 is applicable for the calculation of the cold water side convection resistance R_1. Corresponding to the water velocity of 5 fps, the mass velocity is:

G = 5 (ft per sec) × 62.4 (lb per cu ft) × 3600 (sec per hr) = 11.2×10^5 lb per (hour) (square foot).

The inside diameter of the pipe D is 2.067/12 = 0.1725 ft.

The average water film temperature will be estimated as 36 F (mixed mean fluid temperature of 34 F). Then case 3, Table 5 yields:

$$h_c = 0.00486\ (1 + 0.36)\ \frac{(11.2 \times 10^5)^{0.8}}{(0.1725)^{0.2}} = 650 \text{ Btu per (hr) (sq ft) (F deg).}$$

The transfer area on which this conductance is based is the inside tube area. Associated with 1 ft length of pipe there are:

$$\pi \times \frac{2.067}{12} \times 1 = 0.542 \text{ sq ft.}$$

Thus the resistance for 1 ft of tube length is:

$$R_1 = \frac{1}{h_c \pi D \times 1} = \frac{1}{650 \times 0.542} = 2.8 \times 10^{-3} \text{ hr Fahrenheit degree per Btu.}$$

Case 9, Table 5 is applicable for calculating the free thermal convection resistance, R_c, existing between the surrounding air and the insulation. The air temperature is given as 120 F. As an approximation a 20 deg temperature difference between the air and the pipe surface will be assumed. D = 4.375/12 = 0.364 ft. Then case 9 yields:

$$h_c = 0.23 \left(\frac{20}{0.364}\right)^{0.25} = 0.63 \text{ Btu per (hour) (square foot) (Fahrenheit degree).} \quad (13)$$

This result may not be deemed conservative inasmuch as the expression is for *still* air. If, however, the air is not still, but flows at approximately 5 mph or 7 fps the mass velocity corresponds to:

$$G = 7 \times 0.07 \times 3600 = 1770 \text{ lb air per (hour) (square foot).}$$

A magnitude of $k = 0.014$ Btu per (hour) (square foot) (Fahrenheit degree) per one foot thickness applied to case 4 yields:

$$h_c = 0.45 \left(\frac{0.014}{0.364}\right) + 0.178\ (1770)^{0.56} \left(\frac{0.014}{0.364}\right)^{0.44}$$

$$= 0.017 + 2.8 = 2.8 \text{ Btu per (hour) (square foot) (Fahrenheit degree).}$$

This conductance is based on 1 sq ft of outside lagging area. Thus, since there are $\pi \times (4.375/12) = 1.14$ sq ft of outside lagging area associated with 1 ft length of pipe:

$$R_c = \frac{1}{2.8 \times 1.14} = 0.312 \text{ hr Fahrenheit degree per Btu.}$$

The radiation resistance, R_r, which acts in parallel with the convection resistance, R_c, for the transfer of heat to the surface of the insulation, may be calculated. For the purposes of this illustrative problem it will be assumed that the insulated pipe is exposed to (*sees*) surroundings, which exist at 120 F. Then the angle factor, F_A, is unity and for an estimated surface emissivity of 0.9 (see Table 6), $F_e = 0.9$. As a first approximation the insulation surface temperature will be estimated as 20 deg below the surroundings at 120 F. Then the radiation per degree of temperature difference, by Equation 3 (or more conveniently by Table 8) divided by the temperature difference will be:

$$h_r = \frac{(196 - 170)\ 0.95}{20} = 1.17 \text{ Btu per (hour) (square foot) (Fahrenheit degree).}$$

The outside surface area of the insulation associated with 1 ft of pipe length was previously calculated as 1.14 sq ft. Thus:

$$R_r = \frac{1}{1.17 \times 1.14} = 0.75 \text{ hr Fahrenheit degree per Btu.}$$

The resultant resistance of R_c and R_r acting in parallel (see Fig. 4) can now be evaluated as:

$$\frac{1}{R_4} = \frac{1}{R_c} + \frac{1}{R_r} = \frac{1}{0.312} + \frac{1}{0.75} = 4.54 \text{ Btu per (hour) (Fahrenheit degree).}$$

$$R_4 = 0.22 \text{ hr Fahrenheit degree per Btu.}$$

The over-all resistance, R_T, surroundings to cold water, is the sum of $R_1 + R_2 + R_3 + R_4 = 4.1$ hr F deg per Btu for 1 ft length of pipe. Note that the controlling resistances are R_3 and R_4 and that neglect of both R_1 and R_2 would not significantly influence the total resistance, R_T.

On the basis of this resistance calculation the heat transfer from the surroundings to the cold water may be evaluated as:

$$\frac{q_{rc}}{N} = \frac{t_o - t_f}{R_T} = \frac{120 - 34}{4.1} = 21 \text{ Btu per (hour) (foot)}$$

or about 0.175 tons of refrigeration per 100 ft of pipe.

Since the calculation is based on a 1 ft pipe length:

$$q_{rc} = 21 \text{ Btu per hour.}$$

The temperature drops through the various resistances are now readily evaluated by Equation 12 as:

$t_o - t_{s3}$ air to insulation surface $= R_4 q_{rc} = 0.22 \times 21 = 4.6$ F.
$t_{s3} - t_{s2}$ through the insulation $= R_3 q_{rc} = 3.9 \times 21 = 82$ F.
$t_{s2} - t_{s1}$ through the pipe wall $= R_2 q_{rc} = 8.5 \times 10^{-4} \times 21 = 0.02$ F.
$t_{s1} - t_f$ pipe wall to cold water $= R_1 q_{rc} = 2.8 \times 10^{-3} \times 21 = 0.06$ F.

The solution was obtained on the assumption that the air temperature and the outside temperature differed by 20 deg. In order to obtain a slightly better estimate of the rate of heat transfer the numerical solution should be repeated using the temperatures calculated from the previous listed temperature differences.

The foregoing problem serves to illustrate a general method of solving steady-state heat transfer problems. There are many problems which cannot be approximated by steady-state solutions. For instance, the problem of pipe line insulation in transient service; the behavior of automatically controlled thermoflow circuits; or the periodic absorption of solar energy by roof and wall structures during the day and nocturnal radiation to the *cold* sky at night. The transient heat transfer problem differs from the steady-state in that energy storage rates need to be considered. Thus thermal capacity in addition to resistance effects is significant. The vector sum of the thermal capacitance and resistance is the thermal impedance. It is not within the scope of this chapter to deal with these problems. There are, however, solutions available in graphical form for certain special cases. Also a general approximate method may be employed which is analogous to the treatment of capacity-resistance lumped parameter electrical circuits.

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[1]—Absorption and Extraction, by T. K. Sherwood (McGraw-Hill Co., 1937).

[2]—The Transmission of Heat by Radiation and Convection, by Griffith and Davis (*Special Report* No. 9, 1922, *Department of Scientific and Industrial Research*, His Majesty's Stationery Office, London, England).

[3]—Heat Insulation in Air Conditioning, by R. H. Heilman (*Industrial and Engineering Chemistry*, Vol. 28, July, 1936, p. 782).

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Industrial Heat Transfer, by Alfred Schack (John Wiley & Sons, 1933).

Calculation of Heat Transmission, by M. Fishenden and O. A. Saunders (His Majesty's Stationery Office, London, 1932).

Chapter 6

HEAT TRANSMISSION COEFFICIENTS OF BUILDING MATERIALS

Heat Transfer Symbols; Calculating Over-all Coefficients; Conductivity of Homogeneous Materials; Surface Conductance; Air Space Conductance; Practical Coefficients and Their Use; Computed Heat Transmission Coefficients; Roof Coefficients; Combined Ceiling and Roof Coefficients; Basement Floor, Basement Wall, and Concrete Slab Floor Coefficients, Condensation in Buildings

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THE design of conditioning or heating systems for buildings requires a knowledge of the thermal properties of the walls enclosing the space. The rate of heat flow through the walls under steady-state conditions at design temperatures is usually the basis for calculating the heat required. For a given wall under standard conditions the rate is a specific value designated as U, the *over-all coefficient of heat transmission.* It may be determined by test in a guarded hot box apparatus or it may be computed from known values of the thermal conductance of the various components. Because testing of all combinations of building materials is impracticable, the procedure and necessary data for calculation of the value of U are given in this chapter, together with tables of computed values for the more common constructions.

HEAT TRANSFER SYMBOLS

U = over-all coefficient of heat transmission (air to air); the time rate of heat flow expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference between air on the inside and air on the outside of a wall, floor, roof or ceiling). The term is applied to the usual combinations of materials in construction and also to single materials, such as window glass, and includes the surface conductance on both sides.

k = thermal conductivity; the time rate of heat flow through a homogeneous material under steady conditions through unit area per unit temperature gradient in the direction perpendicular to the area. Its value is expressed in Btu per (hour) (square foot) (Fahrenheit degree per inch). Materials are considered homogeneous when the value of k is not affected by variation in thickness or size of sample within the range normally used in construction.

C = thermal conductance; the time rate of heat flow through a material from one of its surfaces to the other per unit temperature difference *between the two surfaces.* Its value is expressed in Btu per (hour) (square foot) (Fahrenheit degree). The term is applied to specific materials as used which may be either homogeneous or heterogeneous.

f = film or surface conductance; the time rate of heat flow between a surface and the surrounding air. Its value is expressed in Btu per (hour) (square foot of surface) (Fahrenheit degree temperature difference). Subscripts i and o are used to differentiate between inside and outside surface conductances respectively.

a = thermal conductance of an air space; the time rate of heat flow through an air space per unit temperature difference *between the boundary surfaces.* Its value is expressed in Btu per (hour)(square foot of area)(Fahrenheit degree). The conductance of an air space is dependent on the temperature difference, the height, the depth, the position and the character of the boundary surfaces. The relationships are not linear and accurate values must be obtained by test and not by computation.

R = thermal resistance. Its value is expressed in Fahrenheit degrees per (Btu) (hour) (square foot). It may represent any of the following and must therefore be properly described:

$\frac{1}{U}$ = over-all or air-to-air resistance

$\frac{1}{k}$ = resistance per unit thickness (resistivity)

$\frac{1}{C}$ = resistance of a material (surface-to-surface)

$\frac{1}{f}$ = film or surface resistance

$\frac{1}{a}$ = air space resistance

CALCULATING OVER-ALL COEFFICIENTS

From Chapter 5, Equation 7, the total resistance to heat flow through a wall is equal numerically to the sum of the resistances in series. Then by definition,

$$U = \frac{1}{R_t} = \frac{1}{R_1 + R_2 + R_3 + \cdots + R_n} \tag{1}$$

where

R_1, R_2, etc. are the individual resistances of the wall components.

R_t = total resistance.

For a wall of a single homogeneous material of conductivity k and thickness x, with surface coefficients f_i and f_o

$$U = \frac{1}{R_t} = \frac{1}{\frac{1}{f_i} + \frac{x}{k} + \frac{1}{f_o}} \tag{2}$$

For a compound wall of three homogeneous materials in series, having conductivities k_1, k_2 and k_3 and thicknesses x_1, x_2 and x_3 respectively, and laid together without air spaces,

$$U = \frac{1}{R_t} = \frac{1}{\frac{1}{f_i} + \frac{x_1}{k_1} + \frac{x_2}{k_2} + \frac{x_3}{k_3} + \frac{1}{f_o}} \tag{3}$$

For a wall with air space construction and consisting of two homogeneous materials of conductivities k_1 and k_2, thicknesses x_1 and x_2, and separated by an air space of conductance a

$$U = \frac{1}{R_t} = \frac{1}{\frac{1}{f_i} + \frac{x_1}{k_1} + \frac{1}{a} + \frac{x_2}{k_2} + \frac{1}{f_o}} \tag{4}$$

In the case of types of building materials having non-uniform or irregular sections such as hollow clay tile or concrete blocks, it is necessary to use the conductance C of the section unit as manufactured instead of a conductivity k. The resistance of the section $\frac{1}{C}$ is therefore substituted for $\frac{x}{k}$ in Equations 2, 3 and 4.

CONDUCTIVITIES AND CONDUCTANCES

The method of calculating the over-all coefficient of heat transmission for a given construction is comparatively simple, but accurate values of conductivities and conductances must be used to obtain satisfactory results. In addition there are sometimes parallel heat flow paths of different resistances in the same wall, which require modification of the

formula. In such cases calculated results should be checked by test measurements.

The determination of the fundamental conductivities and conductances requires considerable skill and experience to obtain accurate results. It is recommended that thermal conductivities of homogeneous materials be determined by means of the Guarded Hot Plate [1]. For determination of conductances, a Guarded Hot Box method [2] is generally used.

Tables 1 and 2 give conductivities and conductances which are quite generally used in calculation and which have been selected from various sources. Wherever possible the properties of the material and test conditions are given. In selecting and applying heat transmission values to any construction, caution is necessary, because coefficients for the same material may differ because of variations which occur in test methods, in the materials themselves, or in the temperature of the material when tested.

Conductivity of Homogeneous Materials

Thermal conductivity is a property of a homogeneous material and of types of building materials such as lumber, brick and stone which may be considered homogeneous. Most insulating materials, except air spaces and reflective types, are of a porous nature and consist of combinations of solid matter with small air cells. The thermal conductivity of these materials will vary with density, mean temperature, size of fibers or particles, degree and extent of bond between particles, moisture present, and the arrangement of fibers or particles within the material.

The effect of density upon conductivity (at constant mean temperature) is illustrated for two fibrous materials in Fig. 1. It will be noted that for each there is an optimum density for lowest conductivity. Typical variation of conductivity with mean temperature is shown in Fig. 2.

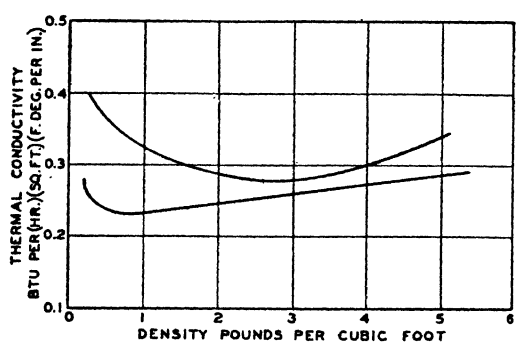


FIG. 1. TYPICAL VARIATION OF THERMAL CONDUCTIVITY WITH DENSITY—FOR FIBROUS MATERIAL

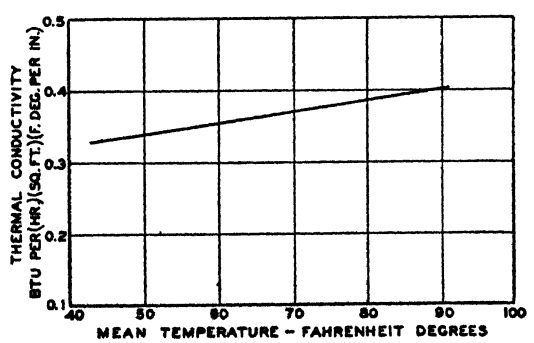


FIG. 2. TYPICAL VARIATION OF THERMAL CONDUCTIVITY WITH MEAN TEMPERATURE

TABLE 1. CONDUCTANCES (*C*) FOR SURFACES AND AIR SPACES

All conductance values expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference).

Section A. Surface Conductances for Still Air[a]

POSITION OF SURFACE	DIRECTION OF HEAT FLOW	SURFACE EMISSIVITY	
		$e = 0.83$	$e = 0.05$
Horizontal	Upward	1.95	1.16
Horizontal	Downward	1.21	0.44
Vertical		1.52*	0.74

Section B. Conductance of Vertical Spaces at Various Mean Temperatures[b]

MEAN TEMP FAHR DEG	CONDUCTANCES OF AIR SPACES FOR VARIOUS WIDTHS IN INCHES						
	0.128	0.250	0.364	0.493	0.713	1.00	1.500
20	2.300	1.370	1.180	1.100	1.040	1.030	1.022
30	2.385	1.425	1.234	1.148	1.080	1.070	1.065
40	2.470	1.480	1.288	1.193	1.125	1.112	1.105
50	2.560	1.535	1.340	1.242	1.168	1.152	1.149
60	2.650	1.590	1.390	1.295	1.210	1.195	1.188
70	2.730	1.648	1.440	1.340	1.250	1.240	1.228
80	2.819	1.702	1.492	1.390	1.295	1.280	1.270
90	2.908	1.757	1.547	1.433	1.340	1.320	1.310
100	2.990	1.813	1.600	1.486	1.380	1.362	1.350
110	3.078	1.870	1.650	1.534	1.425	1.402	1.392
120	3.167	1.928	1.700	1.580	1.467	1.445	1.435
130	3.250	1.980	1.750	1.630	1.510	1.485	1.475
140	3.340	2.035	1.800	1.680	1.550	1.530	1.519
150	3.425	2.090	1.852	1.728	1.592	1.569	1.559

Section C. Conductances and Resistances of Air Spaces Faced on One Surface with Reflective Insulation[c]

LOCATION AND POSITION OF AIR SPACE	DIRECTION OF HEAT FLOW	TEMP[d] DIFF FAHR DEG		CONDUCTANCE[e] (*C*)			RESISTANCE[e] $\left(\frac{1}{C}\right)$		
				No. of Air Spaces			No. of Air Spaces		
		Winter	Summer	1	2	3	1	2	3
Rafter Space (8 in.)									
Horizontal	Down	45			0.10	0.07		10.00	14.29
Horizontal	Up	45			0.27	0.17		3.70	5.88
Horizontal	Down		25		0.09	0.06		11.11	16.67
Horizontal	Up		25		0.24	0.16		4.17	6.25
30 deg slope	Down	45			0.15	0.10		6.67	10.00
30 deg slope	Up	45			0.25	0.17		4.00	5.88
30 deg slope	Down		25		0.13	0.09		7.69	11.11
30 deg slope	Up		25		0.23	0.14		4.35	7.14
Stud Space (3½ in.)									
Vertical[f]		30		0.34			2.94		
Vertical		40			0.23	0.13		4.35	7.69
Vertical[f]			15	0.32			3.13		
Vertical			20		0.18	0.11		5.56	9.09
Vertical[g]		30		0.46			2.17		

[a] Radiation and Convection from Surfaces in Various Positions, by G. B. Wilkes and C. M. F. Peterson (A.S.H.V.E. TRANSACTIONS, Vol. 44, 1938, p. 513).

[b] A.S.H.V.E. Research Report No. 825—Thermal Resistance of Air Spaces, by F. B. Rowley and A. B. Algren (A.S.H.V.E. TRANSACTIONS, Vol. 35, 1929, p. 165).

[c] Thermal Test Coefficients of Aluminum Insulation for Buildings, by G. B. Wilkes, F. G. Hechler and E. R. Queer (A.S.H.V.E. TRANSACTIONS, Vol. 46, 1940).

[d] Temperature difference is based on total space between plaster base and sheathing, flooring or roofing.

[e] These air space conductance and resistance values are based on one reflective surface (aluminum) having an emissivity of 0.05 facing each space and are based on total space between plaster base and sheathing, flooring or roofing. The rafter and stud spaces are divided into equal spaces.

[f] Stud space is lined on plaster base side with loose paper with aluminum on surface facing air space. The resistance of the small air space between the plaster base and paper was 0.43.

[g] Radiation and Convection Across Air Spaces in Frame Construction, by G. B. Wilkes and C. M. F. Peterson (A.S.H.V.E. TRANSACTIONS, Vol. 43, 1937, p. 351).

* The recommended surface conductance for calculating heat losses for still air for non-reflective surfaces is 1.65 Btu. For a 15 mph wind velocity, the recommended value is 6.0 Btu. These coefficients were derived from Fig. 3 which was based on tests conducted at the University of Minnesota, and apply to vertical surfaces.

TABLE 2. CONDUCTIVITIES (k) AND CONDUCTANCES (C) OF BUILDING AND INSULATING MATERIALS

These constants are expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference). Conductivities (k) are per inch thickness and conductances (C) are for thickness or construction stated, not per inch thickness.

Material	Description	Density (Lb per Cu Ft)	Mean Temp (Fahr Deg)	Conductivity or Conductance (k)	Conductivity or Conductance (C)	Resistance per Inch Thickness $\left(\frac{1}{k}\right)$	Resistance for Thickness Listed $\left(\frac{1}{C}\right)$	Authority
BUILDING BOARDS (Non-Insulating)	Compressed cement and asbestos sheets	123	86	2.70	....	0.37	.....	(1)
	Corrugated asbestos board	20.4	110	0.48	....	2.08	.....	(2)
	Pressed asbestos mill board	60.5	86	0.84	....	1.19	.....	(3)
	Gypsum board—gypsum between layers of heavy paper	62.8	70	1.41	....	0.71	.....	(3)
	⅜ in. gypsum board	.....	.....	.....	3.73	.....	0.27	
	½ in. gypsum board	.....	.....	.....	2.82	.....	0.35	
	½ in. gypsum board	53.5	90	.....	2.60	.....	0.38	(1)
FRAME CONSTRUCTION COMBINATIONS	1 in. fir sheathing and building paper	.....	30	.....	0.86	.....	1.16	(4)
	1 in. fir sheathing, building paper and yellow pine lap siding	.....	20	.....	0.50	.....	2.00	(4)
	1 in. fir sheathing, building paper and stucco	.....	20	.....	0.82	.....	1.22	(4)
	Pine lap siding and building paper, siding 4 in. wide	.....	16	.....	0.85	.....	1.18	(4)
	Yellow pine lap siding	.....	....	.....	1.28	.....	0.78	(4)
MASONRY MATERIALS Brick	Damp or wet	.....	....	5.0[g]	....	0.20	.....	(2)
	Common yellow clay brick[a]	.....	....	4.8	....	0.21	.....	(4)
	One tier yellow common clay brick, one tier face brick, approx. 8 in. thick[a]	.....	....	.....	0.77	.....	1.30	(4)
Clay Tile, Hollow	2 in. Tile, ½ in. plaster both sides	120.0	110	.....	1.00	.....	1.00	(2)
	4 in. Tile, ½ in. plaster both sides	127.0	100	.....	0.60	.....	1.67	(2)
	6 in. Tile, ½ in. plaster both sides	124.3	105	.....	0.47	.....	2.13	(2)
	8 in. Tile, average of 8 types (Walls No. 59, 63, 64, 66, 67, 90, 91, 92[a])	.....	....	.....	0.52	.....	1.92	(4)
	12 in. Clay tile wall: 8 in. x 5 in. x 12 in. and 4 in. x 5 in. x 12 in.[a]	.....	....	.....	0.26	.....	3.84	(4)
Concrete	Sand and gravel aggregate, various ages and mixes	.....	....	11.35 to 16.36	....	0.09 to 0.06	....	(5)
	Sand and gravel aggregate	142	75	12.6	....	0.08	.....	(4)
	Limestone aggregate	132	75	10.8	....	0.09	.....	(4)
	Cinder aggregate	97	75	4.9	....	0.22	.....	(4)
	Steam treated limestone slag aggregate[a]	74.6	75	2.27	....	0.44	.....	(4)
	Pumice (Mined in California) aggregate[a]	65.0	75	2.42	....	0.41	.....	(4)
	Expanded burned clay aggregate[a]	59.9	75	2.28	....	0.44	.....	(4)
	Burned clay aggregate[a]	67.1	75	2.86	....	0.35	.....	(4)
	Blast furnace slag aggregate	76.0	70	1.6	....	0.63	.....	(3)
	Expanded vermiculite aggregate	20	90	0.68	....	1.47	.....	(3)
	Expanded vermiculite aggregate	26.7	90	0.76	....	1.32	.....	(3)

AUTHORITIES:

[1] U. S. Bureau of Standards, tests based on samples submitted by manufacturers.

[2] A. C. Willard, L. C. Lichty and L. A. Harding, tests conducted at the University of Illinois.

[3] J. C. Peebles, tests conducted at Armour Institute of Technology, based on samples submitted by manufacturers.

[4] F. B. Rowley, et al, tests conducted at the University of Minnesota.

[5] A.S.H.V.E. Research Laboratory.

[6] E. A. Allcut, tests conducted at the University of Toronto.

[a] See Thermal Conductivity of Building Materials, by F. B. Rowley and A. B. Algren (University of Minnesota *Engineering Experiment Station Bulletin* No. 12).

[b] Heat Transmission Through Insulation as Affected by Orientation of Wall, by F. B. Rowley and C. E. Lund (A.S.H.V.E. TRANSACTIONS, Vol. 49, 1943, p. 331).

[c] The Effect of Convection in Ceiling Insulation, by G. B. Wilkes and L. R. Vianey (A.S.H.V.E. TRANSACTIONS, Vol. 49, 1943, p. 196).

[d] See A.S.H.V.E. RESEARCH REPORT No. 915—Conductivity of Concrete, by F. C. Houghten and Carl Gutberlet (A.S.H.V.E. TRANSACTIONS, Vol. 38, 1932, p. 47).

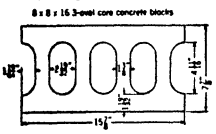
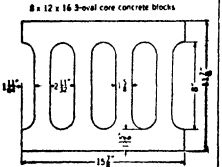
[e] See Heating, Ventilating and Air Conditioning, by Harding and Willard, revised edition, 1932.

[f] See BMS13, U. S. Department of Commerce, National Bureau of Standards, Washington, D. C.

[g] Roofing, 0.15 in. thick (1.34 lb per square foot), covered with gravel (0.83 lb per square foot), combined thickness assumed 0.25.

TABLE 2. CONDUCTIVITIES (k) AND CONDUCTANCES (C) OF BUILDING AND INSULATING MATERIALS—Continued

These constants are expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference). Conductivities (k) are per inch thickness and conductances (C) are for thickness or construction stated, not per inch thickness.

Material	Description	Density (Lb per Cu Ft)	Mean Temp (Fahr Deg)	Conductivity or Conductance		Resistance		Authority
				(k)	(C)	Per Inch Thickness ($\frac{1}{k}$)	For Thickness Listed ($\frac{1}{C}$)	
MASONRY MATERIALS —(Continued)								
Concrete—(Continued)	Expanded vermiculite aggregate	35	90	0.86	....	1.16	.....	(3)
	Expanded vermiculite aggregate	50	90	1.10	....	0.91	.....	(3)
	Concrete plank	76	75	2.5	....	0.40	.....	(3)
	Cellular concrete	40.0	75	1.06	....	0.94	.....	(3)
	Cellular concrete	50.0	75	1.44	....	0.69	.....	(3)
	Cellular concrete	60.0	75	1.80	....	0.56	.....	(3)
	Cellular concrete	70.0	75	2.18	....	0.46	.....	(3)
8 In. Concrete Blocks 	8 in. three oval core, sand and gravel aggregate[a]	126.4	40	.....	0.90	.....	1.11	(4)
	8 in. three oval core, crushed limestone aggregate[a]	134.3	40	.....	0.86	.....	1.16	(4)
	8 in. three oval core, cinder aggregate[a]	86.2	40	.....	0.58	.....	1.73	(4)
	8 in. three oval core, burned clay aggregate[a]	67.7	40	.....	0.50	.....	2.00	(4)
	8 in. three oval core, expanded blast furnace slag aggregate[a]	.....	40	.....	0.49	.....	2.04	(4)
12 In. Concrete Blocks 	12 in. three ova core, sand and gravel aggregate[a]	124.9	40	.....	0.78	.....	1.28	(4)
	12 in. three oval core, cinder aggregate[a]	86.2	40	.....	0.53	.....	1.88	(4)
	12 in. three oval core, burned clay aggregate[a]	76.7	40	.....	0.47	.....	2.13	(4)
Gypsum	3 in. solid gypsum partition tile[a]	.....	....	2.41	....	0.42	.....	(4)
	3 in. three cell gypsum partition tile[a]	.....	....	.....	0.74	.....	1.35	(4)
	4 in. three cell gypsum partition tile[a]	.....	....	.....	0.60	.....	1.67	(4)
	87½ per cent gypsum, 12½ per cent wood chips	51.2	74	1.66	....	0.60	.....	(4)
	Gypsum plaster	.....	....	3.30	....	0.30	.....	
PLASTERING MATERIALS	Gypsum plaster, ⅝ in. thick	.....	73	.....	8.80	.....	0.11	(4)
	Cement plaster	.....	....	8.00	....	0.13	.....	(2)
	Wood, lath and plaster, total thickness ¾ in.	.....	70	.....	2.50	.....	0.40	(4)
	Gypsum plaster and expanded vermiculite, 4 to 1 mix	39.9	75	0.85	....	1.18	.....	(3)
	Insulating plaster 0.9 in. thick applied to ⅝ in. gypsum board	54.0	75	.....	1.07	.....	0.93	(3)
ROOFING	Asbestos shingles	65.0	75	.....	6.0	.....	0.17	(3)
	Asphalt, composition or prepared	70.0	75	.....	6.5	.....	0.15	(3)
	Asphalt shingles	70.0	75	.....	6.5	.....	0.15	(3)
	Built-up roofing, bitumen or felt, gravel or slag surfaced[a]	.....	....	1.33	....	0.75	.....	(2)
	Slate	.....	....	10.00	....	0.10	.....	
	Wood shingles	.....	....	.....	1.28	.....	0.78	
WOODS	Balsa	20.0	90	0.58	....	1.72	.....	(1)
	Balsa	8.8	90	0.38	....	2.63	.....	(1)
	Balsa	7.3	90	0.33	....	3.03	.....	(1)
	California redwood, 0 per cent moisture[a]	28.0	75	0.70	....	1.43	.....	(4)
	Cypress	28.7	86	0.67	....	1.49	.....	(1)
	Douglas fir, 0 per cent moisture[a]	34.0	75	0.67	....	1.49	.....	(4)
	Eastern hemlock, 0 per cent moisture[a]	30.0	75	0.76	....	1.32	.....	(4)
	Long leaf yellow pine, 0 per cent moisture[a]	40.0	75	0.86	....	1.16	.....	(4)
	Mahogany	34.3	86	0.90	....	1.11	.....	(1)

See notes on Page 115.

TABLE 2. CONDUCTIVITIES (k) AND CONDUCTANCES (C) OF BUILDING AND INSULATING MATERIALS—Continued

These constants are expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference). Conductivities (k) are per inch thickness and conductances (C) are for thickness or construction stated, not per inch thickness.

Material	Description	Density (Lb per Cu Ft)	Mean Temp (Fahr Deg)	Conductivity or Conductance (k)	Conductivity or Conductance (C)	Resistance Per Inch Thickness $\left(\frac{1}{k}\right)$	Resistance For Thickness Listed $\left(\frac{1}{C}\right)$	Authority
WOODS—(Continued)	Hard maple, 0 per cent moisture[a]	46.0	75	1.05	....	0.95	.....	(4)
	Maple	44.3	86	1.10	....	0.91	.....	(1)
	Maple, across grain	40.0	75	1.20	....	0.83	.....	(3)
	Norway pine, 0 per cent moisture[a]	32.0	75	0.74	....	1.35	.....	(4)
	Red cypress, 0 per cent moisture[a]	32.0	75	0.79	....	1.27	.....	(4)
	Red oak, 0 per cent moisture[a]	48.0	75	1.18	....	0.85	.....	(4)
	Short leaf yellow pine, 0 per cent moisture[a]	36.0	75	0.91	....	1.10	.....	(4)
	Soft elm, 0 per cent moisture[a]	34.0	75	0.88	....	1.14	.....	(4)
	Soft maple, 0 per cent moisture[a]	42.0	75	0.95	....	1.05	.....	(4)
	Sugar pine, 0 per cent moisture[a]	28.0	75	0.64	....	1.56	.....	(4)
	Virginia pine	34.3	86	0.96	....	1.04	.....	(1)
	West coast hemlock, 0 per cent moisture[a]	30.0	75	0.79	....	1.27	.....	(4)
	White pine	31.2	86	0.78	....	1.28	.....	(1)
	Yellow pine	.....	...	1.00	....	1.00	.....	(3)
	Sawdust, various	12.0	90	0.41	....	2.44	.....	(1)
	Shavings, various from planer	8.8	90	0.41	....	2.44	.....	(1)
	Shavings, from maple beech and birch (coarse)	13.2	90	0.36	....	2.78	.....	(1)
INSULATING MATERIALS								
BLANKET AND BAT INSULATIONS	Chemically treated wood fibers held between layers of strong paper	3.62	70	0.25	....	4.00	.....	(3)
	Eel grass between strong paper	4.60	90	0.26	....	3.85	.....	(1)
	Eel grass between strong paper	3.40	90	0.25	....	4.00	.....	(1)
	Flax fibers between strong paper	4.90	90	0.28	....	3.57	.....	(1)
	Chemically treated hog hair between kraft paper	5.76	71	0.26	....	3.85	.....	(3)
	Chemically treated hog hair between kraft paper and asbestos paper	7.70	71	0.28	....	3.57	.....	(3)
	Hair felt between layers of paper	11.00	75	0.25	....	4.00	.....	(3)
	Kapok between burlap or paper	1.00	90	0.24	....	4.17	.....	(1)
	Stitched and creped expanding fibrous blanket	1.50	70	0.27	....	3.70	.....	(3)
	Paper and asbestos fiber with emulsified asphalt binder	4.2	94	0.28	....	3.57	.....	(1)
	Cotton insulating bat	0.875	72	0.24	....	4.17	.....	(3)
	Cotton fibers							
	Short Staple Linters, Fireproofed	6.25	90	0.25	....	4.00	.....	(1)
	Short Staple Linters, Fireproofed	4.50	90	0.24	....	4.17	.....	(1)
	Short Staple Linters, Fireproofed	2.45	90	0.24	....	4.17	.....	(1)
	Short Staple Linters, Fireproofed	1.60	90	0.26	....	3.85	.....	(1)
	Short Staple Linters, Fireproofed	0.85	90	0.29	....	3.45	.....	(1)
	Short Staple Linters, Fireproofed	0.65	90	0.30	....	3.33	.....	(1)
	Felted cattle hair	13.00	90	0.26	....	3.84	.....	(1)
	Felted cattle hair	11.00	90	0.26	....	3.84	.....	(1)
	Felted hair and asbestos	7.80	90	0.28	....	3.57	.....	(1)
	Ground paper between two layers, each $\frac{1}{8}$ in. thick made up of two layers of kraft paper (sample $\frac{1}{4}$ in. thick)	12.1	75	.....	0.40	.....	2.50	(4)
REFLECTIVE	See Table 1, Section C	.....	....	.....	....	.....	.....	
INSULATING BOARD	Made from sugar cane fiber	13.5	70	0.33	....	3.03	.....	(3)
	Made from corn stalks	15.00	71	0.33	....	3.03	.....	(3)
	Made from exploded wood fibers	17.90	78	0.32	....	3.12	.....	(4)
	Made from hard wood fibers	15.20	70	0.32	....	3.12	.....	(3)
	Made from wood fiber	15.90	72	0.33	....	3.03	.....	(3)
	Made from wood fiber	15.00	70	0.33	....	3.03	.....	(3)
	Made from wood fiber	.....	52	0.33	....	3.03	.....	(6)
	Made from wood fiber	8.50	72	0.29	....	3.45	.....	(3)
	Made from wood fiber	15.20	....	0.33	....	3.03	.....	(3)
	Made from wood fiber	16.90	90	0.34	....	2.94	.....	(1)

See notes on Page 115

TABLE 2. CONDUCTIVITIES (k) AND CONDUCTANCES (C) OF BUILDING AND INSULATING MATERIALS—Concluded

These constants are expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference). Conductivities (k) are per inch thickness and conductances (C) are for thickness or construction stated, not per inch thickness.

Material	Description	Density (Lb per Cu Ft)	Mean Temp (Fahr Deg)	Conductivity or Conductance (k)	Conductivity or Conductance (C)	Resistance: Per Inch Thickness $\left(\frac{1}{k}\right)$	Resistance: For Thickness Listed $\left(\frac{1}{C}\right)$	Authority
INSULATING MATERIALS —Continued								
INSULATING BOARD —Continued	Made from licorice root	16.1	81	0.34	....	2.94	.....	(3)
	½ in. insulating boards without special finish[f] (eleven samples)	16.5 to 21.8	90	0.33 to 0.40	....	3.03 to 2.50	....	(1)
	1 in. insulating board[a]	13.2	....	0.34	...	2.94	.....	(4)
LOOSE FILL TYPE	Made from ceiba fibers	1.90	75	0.23	....	4.35	.....	(3)
	Made from ceiba fibers	1.60	75	0.24	...	4.17	.....	(3)
	Fibrous material made from dolomite and silica	1.50	75	0.27	...	3.70	.....	(3)
	Fibrous material made from slag	9.40	103	0.27	....	3.70	.....	(1)
	Redwood bark	3.00	90	0.31	....	3.22	.....	(1)
	Redwood bark	5.00	75	0.26	....	3.84	.....	(3)
	Glass wool fibers 0.0003 in. to 0.006 in. in diameter	1.50	75	0.27	....	3.70	.....	(3)
	Granular insulation made from combined silicate of lime and alumina	4.20	72	0.24	....	4.17	.....	(3)
	Expanded vermiculite	.....	....	0.48	....	2.08	.....	(1)
	Expanded vermiculite, particle size—3 + 14	6.2	....	0.32	....	3.12	.....	(3)
	Regranulated cork about ⅛ in. particles	8.10	90	0.31	....	3.22	.....	(1)
	Hand applied granular mineral wool 2 in. to 6 in. thick; horizontal position[b]. No covering	6.05 to 7.13	....	0.30 to 0.33	....	3.33 to 3.03	....	(4)
	4 in. machine blown granular mineral wool, horizontal position[b]. No covering	5.74	....	0.30	....	3.33	.....	(4)
	Rock wool	10.0	90	0.27	....	3.70	.....	(1)
SLAB INSULATIONS	Corkboard, no added binder	14.0	90	0.34	....	2.94	.....	(1)
	Corkboard, no added binder	10.6	90	0.30	....	3.33	.....	(1)
	Corkboard, no added binder	7.0	90	0.27	....	3.70	.....	(1)
	Corkboard, no added binder	5.4	90	0.25	....	4.00	.....	(1)
	Corkboard[a]	8.7	..	0.29	....	3.45	.....	(4)
	Corkboard, asphaltic binder	14.5	90	0.32	....	3.12	.....	(1)
	Chemically treated hog hair with film of asphalt	10.0	75	0.28	....	3.57	.....	(3)
	Sugar cane fiber insulation blocks encased in asphalt membrane	13.8	70	0.30	....	3.33	.....	(3)
	Made from 85 per cent magnesia and 15 per cent asbestos	19.3	86	0.51	....	1.96	.....	(1)
	Made from shredded wood and cement	24.2	72	0.46	....	2.17	.....	(3)
	Made from shredded wood and cement[e]	29.8	....	0.77	....	1.30	.....	(4)

See notes on Page 115.

Surface Conductance

The surface conductance of a wall is the combined heat transfer to or from the wall by radiation, convection and conduction. Each of the three portions making up the total may vary independently of the others, thus affecting the total conductance. The heat transfer by radiation between two surfaces is controlled by the character of the surfaces (emissivity), the temperature difference between them, and the solid angle through which they *see* each other. The heat transfer by convection and conduction is controlled by the roughness of the surface, by air movement and temperature difference between the air and the surface.

The importance of the effect of temperature of *surrounding surfaces* on the surface conductance due to the effect on radiation is illustrated in

Table 3, which applies to a vertical surface at 80 F, with ambient air at 70 F and effective emissivity equal to 0.83 [3].

In many cases, because the heat resistance of the internal parts of the wall is high compared with the surface resistance, the surface factors are of minor importance. In other cases, *e.g.* single glass windows, the surface resistances constitute almost the entire resistance and are therefore very important. In a building heated by convection there is only a slight difference between the temperatures of the interior wall surface and the surroundings, but if the building is heated by radiant panels there may be a considerable difference [4]. (See also Chapter 31.)

The convection part of the surface conductance coefficient is affected markedly by air movement. This is illustrated by Fig. 3, which shows the surface conductances for different materials at a mean temperature of 20 F and for wind velocities up to 40 mph. These include the radiation portion of the coefficient, which for ordinary building materials under these conditions would be constant at about 0.7 Btu.

TABLE 3. VARIATION IN SURFACE CONDUCTANCE COEFFICIENT WITH DIFFERENT TEMPERATURES OF SURROUNDING SURFACE

SURROUNDING SURFACE TEMPERATURE	75 F	70 F	69 F	60 F	50 F
Convection—Btu per (hr) (sq ft)	6.6	6.6	6.6	6.6	6.6
Radiation—Btu per (hr) (sq ft)	4.4	8.6	9.6	17.0	24.9
Total—Btu per (hr) (sq ft)	11.0	15.2	16.2	23.6	31.5

Due to these variations for different conditions the selection of surface conductance coefficients for a practical building becomes a matter of judgment. In calculating the over-all heat transmission coefficients for the walls, etc. of Tables 5 to 18, 1.65 has been selected as an *average inside surface conductance* and 6.0 as an *average outside surface conductance* for a 15-mile wind. These values apply only to ordinary building materials and should not be used for bright metal surfaces having a low emissivity.

In special cases, where surface conductance coefficients become important factors in the over-all rates of heat transfer, more selective coefficients may be required. The surface conductance values given in Table 1, **Section A** are based on recent tests and are for still air conditions and surface emissivities of 0.83 and 0.05 respectively, and may be used where it is desirable to differentiate between horizontal and vertical surfaces or where coefficients applicable to low-emissivity surfaces are required.

Air Space Conductance

The transfer of heat across an air space involves the boundary surfaces as well as the intervening air, consequently the factors influencing surface conductance play an important part in determining the conductance of the air space. The coefficients given for air space conductance represent the total conductance from surface to surface.

The radiation portion of the coefficient is affected by the difference in temperature between the boundary surfaces and by their respective

emissivities and is practically independent of depth. The convection and conduction transfer is controlled by depth and shape of the air space, the roughness of the boundary surfaces, the mean temperature and the direction of heat flow. For air spaces usually employed in building construction, the radiation and convection factors vary independently of each other.

Table 1, **Section B** gives experimentally-determined conductances of vertical air spaces bounded by such materials as paper, wood, plaster, etc., having emissivity coefficients of 0.8 or higher, and having extended parallel surfaces perpendicular to the direction of heat flow. The conductances decrease as the depth is increased but change only slightly

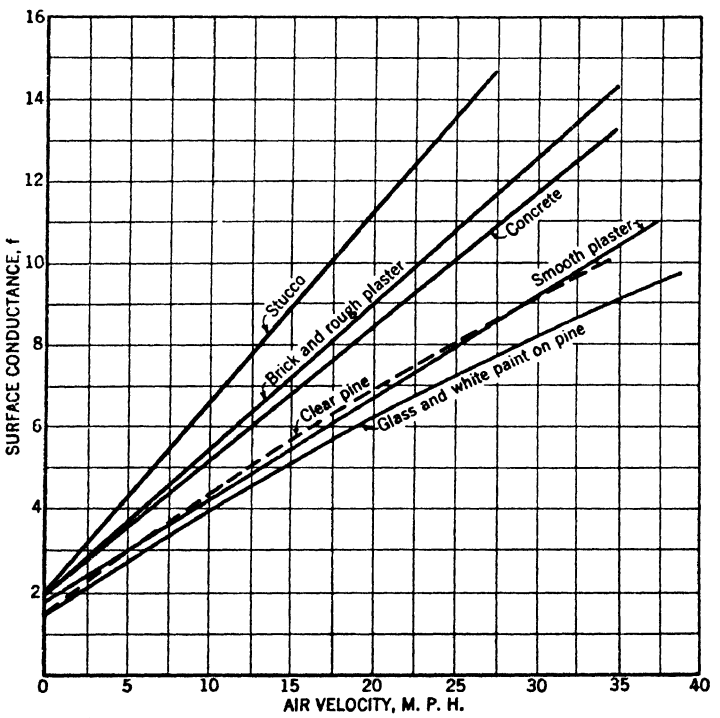


FIG. 3. CURVES SHOWING RELATION BETWEEN SURFACE CONDUCTANCES FOR DIFFERENT SURFACES AT 20 F MEAN TEMPERATURE

for spaces greater than ¾ in. Air space tests reported by Wilkes and Peterson gave conductance values for air spaces of 3⅝ in. depth having boundary surfaces with emissivity values of 0.83 as follows [5].

Vertical	1.17
Horizontal (heat flow upward)	1.32
Horizontal (heat flow downward)	0.94

Since, in buildings, the same constructions may be used for conditions where the direction of heat flow may be in one direction or its opposite, and since much of the construction involves vertical air spaces, an average value of 1.10 Btu per (hour) (square foot) (Fahrenheit degree temperature difference) was chosen for use in calculating the over-all coefficients in Tables 5 to 18 wherever air spaces ¾ in. or more in depth were involved.

If one or both boundary surfaces of an air space are faced with metals which have low emissivity surfaces, the radiant heat transfer will be greatly reduced in comparison with that occurring from surfaces of ordinary building materials. Table 1, **Section C** gives conductances and resistances of air spaces *bounded by one reflective surface* with an emissivity of 0.05. These values include heat transferred both by radiation and convection, but the radiation component is relatively small for the test conditions.

When reflective materials are installed with single or multiple air spaces, the position (vertical, horizontal or inclined) of the material and the direction of heat flow must be taken into consideration. For example, the resistance to *upward* heat flow is about one-third the resistance to *downward* heat flow in a horizontal position (Table 1, **Section C**). The difference between the conductance through vertical air spaces and that through horizontal and sloping air spaces with upward heat flow is considerably less. For upward heat flow it is recommended that a value of 0.46 be used for the conductance of horizontal or sloping air spaces bounded on one side by reflective materials having an emissivity of approximately 0.05. The same conductance value is also recommended for similar vertical air spaces.

When considering heat transfer to and from reflective surfaces in building construction, the emissivity should be known. This can be determined directly for the long wave length radiation corresponding to average room and wall temperatures. The possibility of change in emissivity with time of exposure due to surface coatings, chemical action, deposition of dust, etc. must be considered in selecting a material for use [6].

PRACTICAL COEFFICIENTS AND THEIR USE

For practical purposes it is necessary to have average coefficients that may be applied to various materials and types of construction without the necessity of making actual tests. In Table 2 coefficients are given for a group of materials which have been selected from tests by various authorities. Since there is some variation in the resulting values due to variations in materials and in test conditions, average values for the usual conditions encountered in building practice have been selected and listed in Table 4. These coefficients were used in the calculation of over-all coefficients given in Tables 5 to 18. These tables constitute typical examples of combinations frequently used, but any special constructions not given can be computed by the use of the conductivity values in Table 4 and the fundamental heat transfer formulae.

Caution

The user should realize that the average conductivity and conductance values given in Tables 2 or 4 do not necessarily apply to all products of the same general description. In using these values judgment should be exercised with regard to the extent to which the product (either as received or as applied) will comply with the tabulated values. Exact conductivities or conductances for specific materials should be obtained from the manufacturer.

Insulating Materials

In order to determine the benefit derived from the addition of insulating materials to a given construction, the over-all coefficient of heat

TABLE 4. CONDUCTIVITIES (k) AND CONDUCTANCES (C) USED IN CALCULATING HEAT TRANSMISSION COEFFICIENTS (U) IN TABLES 5 TO 18

These constants are expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference). Conductivities (k) are per inch thickness and conductances (C) are for thickness or construction stated, not per inch thickness.

MATERIAL	DESCRIPTION	CONDUCTIVITY OR CONDUCTANCE		RESISTANCE	
				Per Inch Thickness	For Thickness Listed
		(k)	(C)	$\left(\frac{1}{k}\right)$	$\left(\frac{1}{C}\right)$
AIR SPACES					
Bounded by ordinary materials	Vertical[a], ¾ in. or more in width	.....	1.10	.....	0.91
Bounded by aluminum foil	Vertical[a], ¾ in. or more in width	.....	0.46	.....	2.17
EXTERIOR FINISHES (Frame Walls)					
Brick Veneer	4 in. thick (nominal)	.....	2.27	.....	0.44
Stucco (1 in.)		12.50	.....	0.08	.....
Wood Shingles		.....	1.28	.....	0.78
Yellow Pine Lap Siding		.....	1.28	.....	0.78
INSULATING MATERIALS					
Aluminum Foil	See Air Spaces	.....	.....	.....	.....
Bats and Blankets	Made from mineral or vegetable fiber or animal hair, enclosed or open	0.27	.....	3.70	.....
Corkboard	Pure, no added binder	0.30	.....	3 33	.....
Insulating Board	Vegetable fiber	0.33	.....	3.03	.....
Mineral Wool	Fiber made from rock, slag or glass	0.27	.....	3.70	.....
Vermiculite	Expanded	0.48	.....	2.08	.....
INTERIOR FINISHES					
Composition Wallboard	⅝ in. to ¾ in. thick	0.50	.....	2.00	.....
Gypsum Plaster		3.30	.....	0.30	.....
Gypsum Board (⅜ in.)	Plain or decorated	.....	3.70	.....	0.27
Gypsum Lath (⅜ in.) and Plaster	Plaster thickness assumed ½ in.	.....	2.4	.....	0.42
Insulating Board (½ in.)	Plain or decorated	.....	0.66	.....	1.52
Insulating Board Lath (½ in.) and Plaster	Plaster thickness assumed ½ in.	.....	0.60	.....	1.67
Insulating Board Lath (1 in.) and Plaster	Plaster thickness assumed ½ in.	.....	0.31	.....	3.18
Metal Lath and Plaster	Plaster thickness assumed ¾ in.	.....	4.40	.....	0.23
Plywood (⅜ in.)	Plain or decorated	.....	2.12	.....	0.47
Wood Lath and Plaster		.....	2.50	.....	0.40
MASONRY MATERIALS					
Brick	Adobe, assumed 4 in. thick	.....	0.89	.....	1.12
Brick	Common, assumed 4 in. thick	.....	1.25	.....	0.80
Brick	Face, assumed 4 in. thick	.....	2.30	.....	0.43
Cement Mortar		12.00	.....	0.08	.....
3 in. Clay Tile (hollow)		.....	1.28	.....	0.78
4 in. Clay Tile (hollow)		.....	1.00	.....	1.00
6 in. Clay Tile (hollow)		.....	0.64	.....	1.57
8 in. Clay Tile (hollow)		.....	0.60	.....	1.67
10 in. Clay Tile (hollow)		.....	0.58	.....	1.72
12 in. Clay Tile (hollow)		.....	0.40	.....	2.50
16 in. Clay Tile (hollow)		.....	0.31	.....	3.23
Concrete	Light weight aggregate[b]	2.50	.....	0.40	.....
Concrete	Sand and gravel aggregate	12.00	.....	0.08	.....
8 in. Concrete Blocks	Hollow, cinder aggregate	.....	1.28	.....	0.78
4 in. Concrete Blocks	Hollow, cinder aggregate	.....	1.00	.....	1.00
8 in. Concrete Blocks	Hollow, gravel aggregate	.....	1.00	.....	1.00
12 in. Concrete Blocks	Hollow, gravel aggregate	.....	0.80	.....	1.25
8 in. Concrete Blocks	Hollow, cinder aggregate	.....	0.60	.....	1.66
12 in. Concrete Blocks	Hollow, cinder aggregate	.....	0.53	.....	1.88
8 in. Concrete Blocks	Hollow, light weight aggregate[b]	.....	0.50	.....	2.00
12 in. Concrete Blocks	Hollow, light weight aggregate[b]	.....	0.47	.....	2.13
Gypsum Fiber Concrete	87½ per cent gypsum and 12½ per cent wood chips	1.66	.....	0.60	.....
3 in. Gypsum Tile	Hollow	.....	0.61	.....	1.64
4 in. Gypsum Tile	Hollow	.....	0.46	.....	2.18
Stucco		12.50	.....	0.08	.....
Tile and Terrazzo	For flooring	12.00	.....	0.08	.....
Stone		12.50	.....	0.08	.....

[a] Conductance values for horizontal air spaces depend on whether the heat flow is upward or downward, but in most cases it is sufficiently accurate to use the same values for horizontal as for vertical air spaces.

[b] Expanded slag, burned clay or pumice.

TABLE 4. CONDUCTIVITIES (k) AND CONDUCTANCES (C) USED IN CALCULATING HEAT TRANSMISSION COEFFICIENTS (U) IN TABLES 5 TO 18—Concluded

These constants are expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference). Conductivities (k) are per inch thickness and conductances (C) are for thickness or construction stated, not per inch thickness.

MATERIAL	DESCRIPTION	CONDUCTIVITY OR CONDUCTANCE		RESISTANCE	
				Per Inch Thickness	For Thickness Listed
		(k)	(C)	$\left(\frac{1}{k}\right)$	$\left(\frac{1}{C}\right)$
ROOFING MATERIALS					
Asbestos Shingles		.....	6.00	.....	0.17
Asphalt Shingles		.....	6.50	.....	0.15
Built-up Roofing	Assumed thickness 3/8 in.	.....	3.53	.....	0.28
Heavy Roll Roofing		.....	6.50	.....	0.15
Slate	Assumed 1/2 in.	10.00	20.00	0.10	0.05
Wood Shingles		.....	1.28	.....	0.78
SHEATHING					
Gypsum (1/2 in.)		.....	2.82	.....	0.35
Insulating Board (25/32 in.)		.....	0.42	.....	2.37
Plywood (3/8 in.)		.....	2.56	.....	0.39
Fir or Yellow Pine (1 in.)	Actual thickness 25/32 in.	.....	1.02	.....	0.98
Fir, plus building paper	Actual thickness 25/32 in.	.....	0.86	.....	1.16
SURFACES					
Still air	Ordinary non-reflective materials, vertical	.....	1.65	.....	0.61
15 mph wind velocity	Ordinary non-reflective materials, vertical	.....	6.00	.....	0.17
WOODS					
Fir sheathing (1 in.) building paper and Yellow Pine lap siding		.....	0.50	.....	2.00
Maple or Oak		1.15	.....	0.87	.....
Yellow Pine or Fir		0.80	.....	1.25	.....

transmission U_1 of the insulated construction may be compared with the corresponding coefficient U without insulation. Attention is called to the necessity of applying the insulating material in accordance with the manufacturer's specification. The engineer must carefully evaluate the economic considerations involved in the selection of an insulating material as adapted to various building constructions. Lack of proper evaluation, or improper installation may lead to unsatisfactory results.

Computed Heat Transmission Coefficients

Computed over-all heat transmission coefficients of many common types of building construction are given in Tables 5 to 18, inclusive, each coefficient being identified by a serial number except in Table 18. For example, the coefficient U of a brick-veneer, frame wall with wood sheathing and 1/2 in. of plaster on gypsum lath is 0.27, (Wall No. 28-C in Table 5) and with 2 in. of blanket or bat insulation the coefficient would be 0.097 (No. 49-B in Table 6).

Example 1. Calculate the coefficient of heat transmission U of a brick-veneer, frame wall with wood sheathing, building paper, and 1/2 in. plaster on 3/8 in. gypsum lath, based on a wind exposure of 15 mph. Also calculate the coefficient when 2 in. of bat insulation is added, leaving an air space in the wall, and correcting for framing amounting to 15 per cent of the wall area.

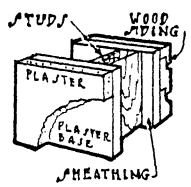
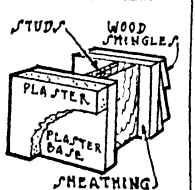
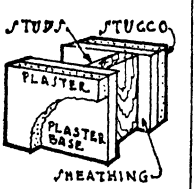
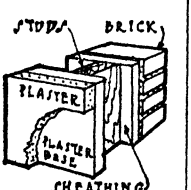
Solution: Starting from the exterior, the resistances making up the total heat resistance are (1) exterior surface, (2) brick-veneer, (3) wood sheathing 25/32 in. thick and building paper, (4) air space 3 5/8 in. wide, (5) 3/8 in. gypsum lath and plaster, (6) interior surface. Then using the values from Table 4 in Equation 4:

$$U = \frac{1}{\frac{1}{6.0} + \frac{1}{2.27} + \frac{1}{0.86} + \frac{1}{1.10} + \frac{1}{2.4} + \frac{1}{1.65}}$$

TABLE 5. COEFFICIENTS OF TRANSMISSION (*U*) OF FRAME WALLS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

NO INSULATION BETWEEN STUDS[a] (SEE TABLE 6)

EXTERIOR FINISH	INTERIOR FINISH	TYPE OF SHEATHING				WALL NUMBER
		GYPSUM (½ IN. THICK)	PLYWOOD (⅜ IN. THICK)	WOOD/ (25/32 IN. THICK) BLDG. PAPER	INSULATING BOARD (25/32 IN. THICK)	
		A	B	C	D	
WOOD SIDING (Clapboard) 	Metal Lath and Plaster[b]	0.33	0.32	0.26	0.20	1
	Gypsum Board (⅜ in.) Decorated	0.32	0.32	0.26	0.20	2
	Wood Lath and Plaster	0.31	0.31	0.25	0.19	3
	Gypsum Lath (⅜ in.) Plastered[c]	0.31	0.30	0.25	0.19	4
	Plywood (⅜ in.) Plain or Decorated	0.30	0.30	0.24	0.19	5
	Insulating Board (½ in.) Plain or Decorated	0.23	0.23	0.19	0.16	6
	Insulating Board Lath (½ in.) Plastered[c]	0.22	0.22	0.19	0.15	7
	Insulating Board Lath (1 in.) Plastered[c]	0.17	0.17	0.15	0.12	8
WOOD[d] SHINGLES 	Metal Lath and Plaster[b]	0.25	0.25	0.26	0.17	9
	Gypsum Board (⅜ in.) Decorated	0.25	0.25	0.26	0.17	10
	Wood Lath and Plaster	0.24	0.24	0.25	0.16	11
	Gypsum Lath (⅜ in.) Plastered[c]	0.24	0.24	0.25	0.16	12
	Plywood (⅜ in.) Plain or Decorated	0.24	0.24	0.24	0.16	13
	Insulating Board (½ in.) Plain or Decorated	0.19	0.19	0.19	0.14	14
	Insulating Board Lath (½ in.) Plastered[c]	0.19	0.18	0.19	0.13	15
	Insulating Board Lath (1 in.) Plastered[c]	0.14	0.14	0.15	0.11	16
STUCCO 	Metal Lath and Plaster[b]	0.43	0.42	0.32	0.23	17
	Gypsum Board (⅜ in.) Decorated	0.42	0.41	0.31	0.23	18
	Wood Lath and Plaster	0.40	0.39	0.30	0.22	19
	Gypsum Lath (⅜ in.) Plastered[c]	0.39	0.39	0.30	0.22	20
	Plywood (⅜ in.) Plain or Decorated	0.39	0.38	0.29	0.22	21
	Insulating Board (½ in.) Plain or Decorated	0.27	0.27	0.22	0.18	22
	Insulating Board Lath (½ in.) Plastered[c]	0.26	0.26	0.22	0.17	23
	Insulating Board Lath (1 in.) Plastered[c]	0.19	0.19	0.16	0.14	24
BRICK VENEER[e] 	Metal Lath and Plaster[b]	0.37	0.36	0.28	0.21	25
	Gypsum Board (⅜ in.) Decorated	0.36	0.36	0.28	0.21	26
	Wood Lath and Plaster	0.35	0.34	0.27	0.20	27
	Gypsum Lath (⅜ in.) Plastered[c]	0.34	0.34	0.27	0.20	28
	Plywood (⅜ in.) Plain or Decorated	0.34	0.33	0.27	0.20	29
	Insulating Board (½ in.) Plain or Decorated	0.25	0.25	0.21	0.17	30
	Insulating Board Lath (½ in.) Plastered[c]	0.24	0.24	0.20	0.16	31
	Insulating Board Lath (1 in.) Plastered[c]	0.18	0.18	0.15	0.13	32

[a] Coefficients not weighted; effect of studding neglected.
[b] Plaster assumed ¾ in. thick.
[c] Plaster assumed ½ in. thick.
[d] Furring strips (1 in. nominal thickness) between wood shingles and all sheathings except wood.
[e] Small air space and mortar between building paper and brick veneer neglected.
[f] Nominal thickness, 1 in.

TABLE 6. COEFFICIENTS OF TRANSMISSION (*U*) OF FRAME WALLS WITH INSULATION BETWEEN FRAMING[a,b]

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

COEFFICIENT WITH *NO* INSULATION BETWEEN FRAMING	COEFFICIENT WITH INSULATION BETWEEN FRAMING				NUMBER
	MINERAL WOOL OR VEGETABLE FIBERS IN BLANKET OR BAT FORM[c] (Thickness below)			3½ IN. MINERAL WOOL BETWEEN FRAMING[d]	
	1 IN.	2 IN.	3 IN.		
	A	B	C	D	
0.11	0.078	0.063	0.054	0.051	33
0.12	0.083	0.067	0.056	0.053	34
0.13	0.088	0.070	0.058	0.055	35
0.14	0.092	0.072	0.061	0.057	36
0.15	0.097	0.075	0.062	0.059	37
0.16	0.10	0.078	0.064	0.060	38
0.17	0.10	0.080	0.066	0.062	39
0.18	0.11	0.082	0.067	0.063	40
0.19	0.11	0.084	0.069	0.065	41
0.20	0.12	0.086	0.070	0.066	42
0.21	0.12	0.088	0.072	0.067	43
0.22	0.12	0.089	0.073	0.068	44
0.23	0.12	0.091	0.074	0.069	45
0.24	0.12	0.093	0.075	0.070	46
0.25	0.13	0.094	0.076	0.071	47
0.26	0.13	0.096	0.077	0.072	48
0.27	0.14	0.097	0.078	0.073	49
0.28	0.14	0.098	0.079	0.073	50
0.29	0.14	0.10	0 080	0.075	51
0.30	0.14	0.10	0.080	0.075	52
0.31	0.14	0.10	0.081	0.076	53
0.32	0.15	0.10	0.082	0.077	54
0.33	0.15	0.10	0.083	0.077	55
0.34	0.15	0.10	0.083	0.078	56
0.35	0.15	0.11	0.084	0.078	57
0.36	0.15	0.11	0.085	0.079	58
0.37	0.16	0.11	0.085	0.080	59
0.38	0.16	0.11	0.086	0.080	60
0.39	0.16	0.11	0.086	0.081	61
0.40	0.16	0.11	0.087	0.082	62
0.41	0.16	0.11	0.087	0.082	63
0.42	0.16	0.11	0.088	0.082	64
0.43	0.17	0.11	0.088	0.082	65
0.44	0.17	0.11	0.089	0.083	66

[a]This table may be used for determining the coefficients of transmission of frame constructions with the types and thicknesses of insulation indicated in Columns A to D inclusive between framing. Columns A, B and C may be used for walls, ceilings or roofs with only one air space between framing but are not applicable to ceilings with *no* flooring above. (See Table 11.) Column D is applicable to walls only. ***Example:*** Find the coefficient of transmission of a frame wall consisting of wood siding, ½ in. insulating board sheathing, studs, gypsum lath and plaster, with 2 in. blanket insulation between studs. According to Table 5, a wall of this construction with *no insulation* between studs has a coefficient of 0.19 (Wall No. 4D). Referring to Column B above, it will be found that a wall of this value with 2 in. blanket insulation between the studs has a coefficient of 0.084.

[b]Coefficients corrected for 2 x 4 framing, 16 in. on centers—15 per cent of surface area.

[c]Based on one air space between framing.

[d]No air space.

$$U = \frac{1}{0.17 + 0.44 + 1.16 + 0.91 + 0.42 + 0.61} = \frac{1}{3.71} = 0.27$$

When 2 in. of bat insulation is added in the air space in the wall, an air space will still be left since it was originally 3⅝ in. wide. Then,

$$U = \frac{1}{3.71 + \frac{2}{0.27}} = \frac{1}{11.11} = 0.090$$

This coefficient (0.090) applies only to the wall where no studding or framing is present and is assumed to constitute 85 per cent of the whole wall. Then for 1 sq ft of wall the heat transfer through the insulated portion is 0.85 × 0.090 or 0.0765 Btu.

In the portion of wall where framing is present, the air space will be replaced with an equivalent thickness of wood framing. Then,

$$U \text{ (through framing)} = \frac{1}{\frac{1}{6.0} + \frac{1}{2.27} + \frac{1}{0.86} + \frac{3.625}{0.80} + \frac{1}{2.4} + \frac{1}{1.65}}$$

$$U = 0.136$$

Then for 1 sq ft of wall the heat transfer through the framing is 15 per cent of 0.136 or 0.0204 Btu. The total heat transfer through 1 sq ft of wall (with 3⅝ in. framing covering 15 per cent of area) equals

$$U \text{ (corrected)} = 0.0765 + 0.0204 = 0.097 \text{ Btu}$$

This is the value shown for No. 49-B in Table 6, which is included to eliminate the need for the calculation of framing corrections when insulation is used in frame construction.

In making the calculations for values of U shown in Tables 5 to 18, the following conditions have been assumed:

Equilibrium or steady-state heat transfer, eliminating effects of heat capacity.
Surrounding surfaces at ambient air temperatures.
Exterior wind velocity of 15 mph.
Surface emissivity of ordinary building materials = 0.83.
No correction for position or direction of heat flow. (Average coefficients used).
Air spaces are ¾ in. or more in width.
Variation of conductivity with mean temperature neglected.
Corrections for framing made on basis of parallel heat flow through 2 × 4 in. (nominal) studs, 16 in. on centers, the framing covering 15 per cent of wall area.
Actual thicknesses of lumber assumed to be as follows:

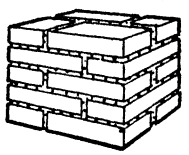
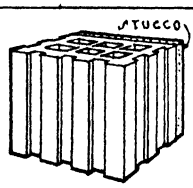
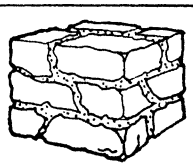
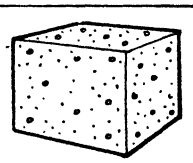
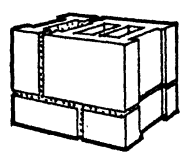
Nominal	*Actual*
1 in. (S-2-S)	25/32 in.
1½ in. (S-2-S)	1 5/16 in.
2 in. (S-2-S)	1⅝ in.
2½ in. (S-2-S)	2⅛ in.
3 in. (S-2-S)	2⅝ in.
4 in. (S-2-S)	3⅝ in.
Finish flooring, (maple or oak)	13/16 in.

Coefficients for frame construction are corrected for the effect of framing where such correction would increase the coefficients, but not where the correction would decrease the coefficients [7].

It should be noted that the effects of poor workmanship in construction and installation have an increasingly greater percentage effect on heat transmission as the coefficient becomes numerically smaller. Failure to meet design estimates may be caused by lack of proper attention to

TABLE 7. COEFFICIENTS OF TRANSMISSION (*U*) OF MASONRY WALLS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

TYPE OF MASONRY		THICKNESS OF MASONRY INCHES	INTERIOR FINISH (PLUS INSULATION WHERE INDICATED)									WALL NUMBER
			Plain Walls—No Interior Finish	Plaster (½ in.) on Walls	Metal Lath and Plaster[f] Furred[h]	Gypsum Board (⅜ in.) Decorated—Furred[h]	Gypsum Lath (⅜ in.) Plastered—Furred[h]	Insulating Board (½ in.) Plain or Decorated—Furred[h]	Insulating Board Lath Plastered—Furred[h]	Insulating Board Lath (1 in.) Plastered—Furred[h]	Gypsum Lath[g] Plastered Plus 1 in. Blanket Insulation—Furred[h]	
			A	B	C	D	E	F	G	H	I	
SOLID[a] BRICK		8	0.50	0.46	0.32	0.31	0.30	0.22	0.22	0.16	0.14	67
		12	0.36	0.34	0.25	0.25	0.24	0.19	0.19	0.14	0.13	68
		16	0.28	0.27	0.21	0.21	0.20	0.17	0.16	0.13	0.12	69
HOLLOW[b] TILE (Stucco Exterior Finish)		8	0.40	0.37	0.27	0.27	0.26	0.20	0.20	0.15	0.13	70
		10	0.39	0.37	0.27	0.27	0.26	0.20	0.19	0.15	0.13	71
		12	0.30	0.28	0.22	0.22	0.21	0.17	0.17	0.13	0.12	72
		16	0.24	0.24	0.19	0.19	0.18	0.15	0.15	0.12	0.11	73
STONE[c]		8	0.70	0.64	0.39	0.38	0.36	0.26	0.25	0.18	0.16	74
		12	0.57	0.53	0.35	0.34	0.33	0.24	0.23	0.17	0.15	75
		16	0.49	0.45	0.31	0.31	0.29	0.22	0.22	0.16	0.14	76
		24	0.37	0.35	0.26	0.26	0.25	0.19	0.19	0.15	0.13	77
POURED CONCRETE[d]		6	0.79	0.71	0.42	0.41	0.39	0.27	0.26	0.19	0.16	78
		8	0.70	0.64	0.39	0.38	0.36	0.26	0.25	0.18	0.16	79
		10	0.63	0.58	0.37	0.36	0.34	0.25	0.24	0.18	0.15	80
		12	0.57	0.53	0.35	0.34	0.33	0.24	0.23	0.17	0.15	81
HOLLOW CONCRETE BLOCKS			Gravel Aggregate									
		8	0.56	0.52	0.34	0.34	0.32	0.24	0.23	0.17	0.15	82
		12	0.49	0.46	0.32	0.31	0.30	0.22	0.22	0.16	0.14	83
			Cinder Aggregate									
		8	0.41	0.39	0.28	0.28	0.27	0.21	0.20	0.15	0.13	84
		12	0.38	0.36	0.26	0.26	0.25	0.20	0.19	0.15	0.13	85
			Light Weight Aggregate[e]									
		8	0.36	0.34	0.26	0.25	0.24	0.19	0.19	0.15	0.13	86
		12	0.34	0.33	0.25	0.24	0.24	0.19	0.18	0.14	0.13	87

[a] Based on 4 in. hard brick and remainder common brick.

[b] The 8 in. and 10 in. tile figures are based on two cells in the direction of heat flow. The 12 in. tile is based on three cells in the direction of heat flow. The 16 in. tile consists of one 10 in. and one 6 in. tile each having two cells in the direction of heat flow.

[c] Limestone or sandstone.

[d] These figures may be used with sufficient accuracy for concrete walls with stucco exterior finish.

[e] Expanded slag, burned clay or pumice.

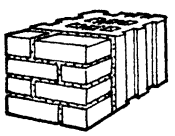
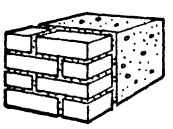
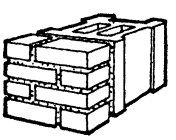
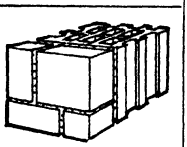
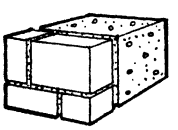
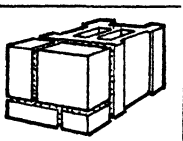
[f] Thickness of plaster assumed ¾ in.

[g] Thickness of plaster assumed ½ in.

[h] Based on 2 in. furring strips; one air space.

TABLE 8. COEFFICIENTS OF TRANSMISSION (*U*) OF BRICK AND STONE VENEER MASONRY WALLS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

TYPICAL CONSTRUCTION	FACING	BACKING	INTERIOR FINISH (PLUS INSULATION WHERE INDICATED)									WALL NUMBER
			Plain Walls—no Interior Finish	Plaster (½ in.) on Walls	Metal Lath and Plaster—Furred[a]	Gypsum Board (⅜ in.) Decorated—Furred[a]	Gypsum Lath (⅜ in.) Plastered[f]—Furred[a]	Insulating Board (½ in.) Plain or Decorated—Furred[a]	Insulating Board Lath (½ in.) Plastered[f]—Furred[a]	Insulating Board Lath (1 in.) Plastered[f]—Furred[a]	Gypsum Lath Plastered[f] Plus 1 in. Blanket Insulation—Furred[a]	
			A	B	C	D	E	F	G	H	I	
	4 in. Brick Veneer[a]	8 in. Hollow Tile[b]	0.35	0.34	0.25	0.25	0.24	0.19	0.18	0.14	0.13	88
		8 in. Hollow Tile[b]	0.34	0.32	0.25	0.24	0.23	0.19	0.18	0.14	0.13	89
		6 in. Concrete	0.59	0.54	0.35	0.35	0.33	0.24	0.23	0.17	0.15	90
		8 in. Concrete	0.54	0.50	0.33	0.33	0.31	0.23	0.23	0.17	0.15	91
		8 in. Concrete Blocks[c] (Gravel Aggregate)	0.44	0.41	0.29	0.29	0.28	0.21	0.21	0.16	0.14	92
		8 in. Concrete Blocks[c] (Cinder Aggregate)	0.34	0.33	0.25	0.24	0.24	0.19	0.18	0.14	0.13	93
		8 in. Concrete Blocks[c] (Light Weight Aggregate)[d]	0.31	0.29	0.23	0.23	0.22	0.18	0.17	0.14	0.12	94
		6 in. Hollow Tile[b]	0.37	0.35	0.26	0.26	0.25	0.19	0.19	0.15	0.13	95
		8 in. Hollow Tile[b]	0.36	0.34	0.25	0.25	0.24	0.19	0.19	0.14	0.13	96
	4 in. Cut Stone Veneer[a]	6 in. Concrete	0.63	0.58	0.37	0.36	0.34	0.25	0.24	0.18	0.15	97
		8 in. Concrete	0.57	0.53	0.35	0.34	0.33	0.24	0.23	0.17	0.15	98
		8 in. Concrete Blocks[c] (Gravel Aggregate)	0.47	0.44	0.30	0.30	0.29	0.22	0.21	0.16	0.14	99
		8 in. Concrete Blocks[c] (Cinder Aggregate)	0.36	0.34	0.25	0.25	0.24	0.19	0.19	0.15	0.13	100
		8 in. Concrete Blocks[c] (Light Weight Aggregate)[d]	0.32	0.30	0.23	0.23	0.22	0.18	0.17	0.14	0.12	101

[a] Calculations based on ½ in. cement mortar between backing and facing except in the case of the concrete backing which is assumed to be poured in place.

[b] The hollow tile figures are based on two air cells in the direction of heat flow.

[c] Hollow concrete blocks.

[d] Expanded slag, burned clay or pumice.

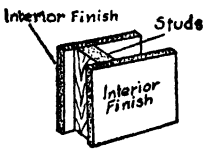
[e] Thickness of plaster assumed ¾ in.

[f] Thickness of plaster assumed ½ in.

[g] Based on 2 in. furring strips; one air space.

TABLE 9. COEFFICIENTS OF TRANSMISSION (*U*) OF FRAME PARTITIONS OR INTERIOR WALLS[a]

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on still air (no wind) conditions on both sides.

INTERIOR FINISH 	SINGLE PARTITION (Finish on one side only of studs)	DOUBLE PARTITION (Finish on both sides of studs)		PARTITION NUMBER
		NO INSULATION BETWEEN STUDS	1 IN. BLANKET[d] BETWEEN STUDS. ONE AIR SPACE.	
	A	B	C	
Metal Lath and Plaster[b]	0.69	0.39	0.16	1
Gypsum Board (⅜ in.) Decorated	0.67	0.37	0.16	2
Wood Lath and Plaster	0.62	0.34	0.15	3
Gypsum Lath (⅜ in.) Plastered[c]	0.61	0.34	0.15	4
Plywood (⅜ in.) Plain or Decorated	0.59	0.33	0.15	5
Insulating Board (½ in.) Plain or Decorated	0.36	0.19	0.11	6
Insulating Board Lath (½ in.) Plastered[c]	0.35	0.18	0.11	7
Insulating Board Lath (1 in.) Plastered[c]	0.23	0.12	0.082	8

[a]Coefficients not weighted; effect of studding neglected.

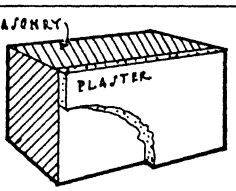
[b]Plaster assumed ¾ in. thick.

[c]Plaster assumed ½ in. thick.

[d]For partitions with other insulations between studs refer to Table 6, using values in Column B of above table in left hand column of Table 6. *Example:* What is the coefficient of transmission (*U*) of a partition consisting of gypsum lath and plaster on both sides of studs with 2 in. blanket between studs? *Solution:* According to above table, this partition with no insulation between studs (No. 4B) has a coefficient of 0.34. Referring to Table 6, it will be found that a wall having a coefficient of 0.34 with no insulation between studs, will have a coefficient of 0.10 with 2 in. of blanket insulation between studs (No. 56B).

TABLE 10. COEFFICIENTS OF TRANSMISSION (*U*) OF MASONRY PARTITIONS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on still air (no wind) conditions on both sides.

TYPE OF PARTITION 		THICKNESS OF MASONRY (INCHES)	TYPE OF FINISH			PARTITION NUMBER
			NO FINISH (Plain walls)	PLASTER ONE SIDE	PLASTER BOTH SIDES[a]	
			A	B	C	
HOLLOW CLAY TILE		3	0.50	0.47	0.43	9
		4	0.45	0.42	0.40	10
HOLLOW GYPSUM TILE		3	0.35	0.33	0.32	11
		4	0.29	0.28	0.27	12
HOLLOW CONCRETE TILE OR BLOCKS	Cinder Aggregate	3	0.50	0.47	0.43	13
		4	0.45	0.42	0.40	14
	Light Weight Aggregate[b]	3	0.41	0.39	0.37	15
		4	0.35	0.34	0.32	16
COMMON BRICK		4	0.50	0.46	0.43	17

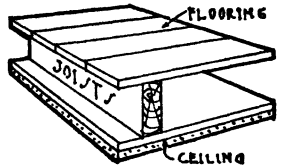
[a]2 in. solid plaster partition, $U = 0.53$.

[b]Expanded slag, burned clay or pumice.

TABLE 11. COEFFICIENTS OF TRANSMISSION (*U*) OF FRAME CONSTRUCTION CEILINGS AND FLOORS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides) and are based on still air (no wind) conditions on both sides.

TYPE OF CEILING	INSULATION BETWEEN, OR ON TOP OF, JOISTS (No Flooring Above)												WITH FLOORING[a] (On Top of Ceiling Joists)		NUMBER
	None	Insulating Board on Top of Joists		Blanket or Bat Insulation[f] Between Joists[a]			Vermiculite Insulation Between Joists[a]			Mineral Wool Insulation Between Joists[a]			Single Wood Floor[b]	Double Wood Floor[c]	
		½ In.	1 In.	1 In.	2 In.	3 In.	2 In.	3 In.	4 In.	2 In.	3 In.	4 In.			
	A	B	C	D	E	F	G	H	I	J	K	L	M	N	
No Ceiling		0.37	0.24										0.45	0.34	1
Metal Lath and Plaster[d]	0.69	0.26	0.19	0.19	0.12	0.093	0.18	0.14	0.11	0.12	0.093	0.077	0.30	0.25	2
Gypsum Board (⅜ in.) Plain or Decorated	0.67	0.26	0.18	0.19	0.12	0.092	0.18	0.13	0.10	0.12	0.092	0.077	0.30	0.24	3
Wood Lath and Plaster	0.62	0.25	0.18	0.19	0.12	0.091	0.17	0.13	0.10	0.12	0.091	0.076	0.28	0.24	4
Gypsum Lath (⅜ in.) Plastered[e]	0.61	0.25	0.18	0.19	0.12	0.091	0.17	0.13	0.10	0.12	0.091	0.076	0.28	0.24	5
Plywood (⅜ in.) Plain or Decorated	0.59	0.24	0.18	0.19	0.12	0.091	0.17	0.13	0.10	0.12	0.091	0.076	0.28	0.23	6
Insulating Board (½ in.) Plain or Decorated	0.36	0.19	0.15	0.16	0.10	0.082	0.14	0.12	0.097	0.10	0.082	0.069	0.22[h]	0.19[h]	7
Insulating Board Lath (½ in.) Plastered[e]	0.35	0.19	0.15	0.15	0.10	0.081	0.14	0.11	0.096	0.10	0.081	0.068	0.21	0.18	8
Insulating Board Lath (1 in.) Plastered[e]	0.23	0.15	0.12	0.12	0.089	0.072	0.12	0.097	0.084	0.089	0.072	0.061	0.16	0.14	9



[a] Coefficients corrected for framing on basis of 15 per cent area, 2 in. x 4 in. (nominal) framing, 16 in. on centers.

[b] 25/32 in. yellow pine or fir.

[c] 25/32 in. pine or fir sub-flooring plus 11/32 in. hardwood finish flooring.

[d] Plaster assumed ¾ in. thick.

[e] Plaster assumed ½ in. thick.

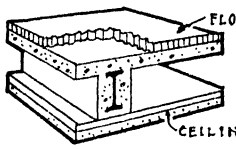
[f] Based on insulation in contact with ceiling and consequently no air space between.

[g] For coefficients for constructions in Columns M and N (except No. 1) with insulation between joists, refer to Table 6. *Example*: The coefficient for No. 3-N of Table 11 is 0.24. With 2 in. blanket insulation between joists, the coefficient will be 0.093. (See Table 6.) (Column D of Table 6 applicable only for 3⅝ in. joists.)

[h] For 25/32 in. insulating board sheathing applied to the under side of the joists, the coefficient for *single* wood floor (Column M) is 0.18 and for *double* wood floor (Column N) is 0.16. For coefficients with insulation between joists, see Table 6.

TABLE 12. COEFFICIENTS OF TRANSMISSION (U) OF CONCRETE CONSTRUCTION FLOORS AND CEILINGS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on still air (no wind) conditions on both sides.

TYPE OF CEILING 	THICKNESS OF CONCRETE[g] (INCHES)	TYPE OF FLOORING					NUMBER
		No Flooring (Concrete Bare)	Tile[a] or Terrazzo Flooring on Concrete	1/8 In. Asphalt Tile[b] Directly on Concrete	Parquet[c] Flooring In Mastic on Concrete	Double Wood Floor on Sleepers[d]	
		A	B	C	D	E	
No Ceiling	3	0.68	0.65	0.66	0.45	0.25	1
	6	0.59	0.56	0.58	0.41	0.23	2
	10	0.50	0.48	0.49	0.36	0.22	3
1/2 in. Plaster Applied to Underside of Concrete	3	0.62	0.59	0.60	0.43	0.24	4
	6	0.54	0.52	0.53	0.39	0.22	5
	10	0.46	0.44	0.45	0.34	0.21	6
Metal Lath and Plaster[e]—Suspended or Furred	3	0.38	0.37	0.37	0.30	0.19	7
	6	0.35	0.34	0.35	0.28	0.18	8
	10	0.32	0.31	0.32	0.26	0.17	9
Gypsum Board (3/8 in.) and Plaster[f]—Suspended or Furred	3	0.36	0.35	0.35	0.28	0.19	10
	6	0.33	0.32	0.33	0.27	0.18	11
	10	0.30	0.29	0.30	0.24	0.17	12
Insulating Board Lath (3/4 in.) and Plaster[f] Suspended or Furred	3	0.25	0.24	0.25	0.21	0.15	13
	6	0.23	0.23	0.23	0.20	0.15	14
	10	0.22	0.21	0.22	0.19	0.14	15

[a] Thickness of tile assumed to be 1 in.

[b] Conductivity of Asphalt Tile assumed to be 3.1.

[c] Thickness of wood assumed to be 13/16 in.; thickness of mastic, 1/8 in. (k = 4.5). Col. D may also be used for concrete covered with carpet.

[d] Based on 13/16 in. yellow pine or fir sub-flooring and 13/16 in. hardwood finish flooring with an air space between sub-floor and concrete.

[e] Thickness of plaster assumed to be 3/4 in.

[f] Thickness of plaster assumed to be 1/2 in.

[g] For other thicknesses of concrete, interpolate.

TABLE 13. COEFFICIENTS OF TRANSMISSION (U) OF CONCRETE FLOORS ON GROUND WITH VARIOUS TYPES OF FINISH FLOORING

U = 0.10[a] Btu per (hour) (square foot) (Fahrenheit degree temperature difference between the ground and the air over the floor).

[a] Until more complete data are available, it is recommended that a coefficient of 0.10 be used for all types of concrete floors on the ground, with or without insulation. For basement wall below grade, use the same average coefficient (0.10). A lower ground temperature should, however, be used for walls than floors as explained in Chapter 14. For further data see A.S.H.V.E. RESEARCH REPORT No. 1213—Heat Loss Through Basement Walls and Floors, by F. C. Houghten, S. I. Taimuty, Carl Gutberlet and C. J. Brown (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 369).

exact compliance with specifications, and a factor of safety may be employed as a precaution when it is judged desirable.

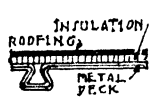
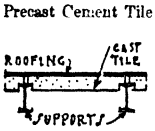
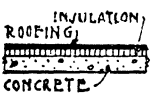
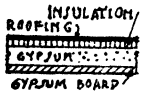
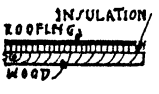
Roof Coefficients

Computations for wood shingle roofs applied over wood stripping are based on 1 by 4 in. wood strips, spaced 2 in. apart. Values for roofs containing Spanish and French clay roofing tile are assumed the same as for slate roofs. Values for pitched roofs in Table 16 apply where the roof is over a heated attic or top floor so that the heat passes directly through the roof structure, including any interior finish material.

TABLE 14. COEFFICIENTS OF TRANSMISSION (*U*) OF FLAT ROOFS COVERED WITH BUILT-UP ROOFING. NO CEILING—UNDER SIDE OF ROOF EXPOSED

(See Table 15 for Flat Roofs with Ceilings)

These coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

TYPE OF ROOF DECK	THICKNESS OF ROOF DECK (INCHES)	NO INSULATION	INSULATION ON TOP OF DECK (COVERED WITH BUILT-UP ROOFING)							NUMBER
			INSULATING BOARD (Thickness Below)				CORKBOARD (Thickness Below)			
			½ In.	1 In.	1½ In.	2 In.	1 In.	1½ In.	2 In.	
		A	B	C	D	E	F	G	H	
Flat Metal Roof Deck[a] 		1.06	0.39	0.24	0.18	0.14	0.23	0.17	0.13	
Precast Cement Tile 	1⅝ in.	0.84	0.37	0.24	0.17	0.14	0.22	0.16	0.13	2
Concrete 	2 in.	0.82	0.36	0.24	0.17	0.14	0.22	0.16	0.13	3
	4 in.	0.72	0.34	0.23	0.17	0.13	0.21	0.16	0.12	4
	6 in.	0.65	0.33	0.22	0.16	0.13	0.21	0.15	0.12	5
Gypsum Fiber Concrete[b] on ½ in. Gypsum Board 	2½ In.	0.38	0.24	0.18	0.14	0.12	0.17	0.13	0.11	6
	3½ in.	0.31	0.21	0.16	0.13	0.11	0.15	0.12	0.10	7
Wood[c] 	1 in.	0.49	0.28	0.20	0.15	0.12	0.19	0.14	0.12	8
	1½ in.	0.37	0.24	0.17	0.14	0.11	0.17	0.13	0.11	9
	2 in.	0.32	0.22	0.16	0.13	0.11	0.16	0.12	0.10	10
	3 in.	0.23	0.17	0.14	0.11	0.096	0.13	0.11	0.091	11

[a] Coefficient of transmission of bare corrugated iron (no roofing) is 1.50 Btu per (hour) (square foot of projected area) (Fahrenheit degree difference in temperature) based on an outside wind velocity of 15 mph.

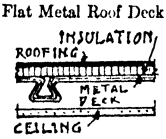
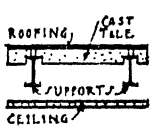
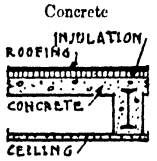
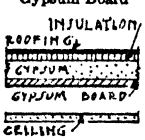
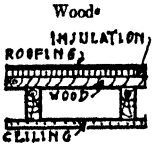
[b] 87½ per cent gypsum, 12½ per cent wood fiber. Thickness indicated includes ½ in. gypsum board.

[c] Nominal thicknesses specified—actual thicknesses used in calculations.

TABLE 15. COEFFICIENTS OF TRANSMISSION (U) OF FLAT ROOFS COVERED WITH BUILT-UP ROOFING. WITH LATH AND PLASTER CEILINGS[a]

(See Table 14 for Flat Roofs with No Ceilings)

These coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

TYPE OF ROOF DECK	THICKNESS OF ROOF DECK (INCHES)	NO INSULATION	INSULATION ON TOP OF DECK (COVERED WITH BUILT-UP ROOFING)							NUMBER
			INSULATING BOARD (Thickness Below)				COREBOARD (Thickness Below)			
			½ In.	1 In.	1½ In.	2 In.	1 In.	1½ In.	2 In.	
		A	B	C	D	E	F	G	H	
Flat Metal Roof Deck 		0.46	0.27	0.19	0.15	0.12	0.18	0.14	0.11	12
Precast Cement Tile 	1⅝ in.	0.43	0.26	0.19	0.15	0.12	0.18	0.14	0.11	13
Concrete 	2 in. 4 in. 6 in.	0.42 0.40 0.37	0.26 0.25 0.24	0.19 0.18 0.18	0.14 0.14 0.14	0.12 0.12 0.11	0.18 0.17 0.17	0.14 0.13 0.13	0.11 0.11 0.11	14 15 16
Gypsum Fiber Concrete[b] on ½ in. Gypsum Board 	2½ in. 3½ in.	0.27 0.23	0.19 0.17	0.15 0.14	0.12 0.11	0.10 0.097	0.14 0.13	0.12 0.11	0.097 0.091	17 18
Wood[c] 	1 in. 1½ in. 2 in. 3 in.	0.31 0.26 0.24 0.18	0.21 0.19 0.17 0.14	0.16 0.15 0.14 0.12	0.13 0.12 0.11 0.10	0.11 0.10 0.097 0.087	0.15 0.14 0.13 0.11	0.12 0.11 0.11 0.095	0.10 0.095 0.092 0.082	19 20 21 22

[a] Calculations based on metal lath and plaster ceilings, but coefficients may be used with sufficient accuracy for gypsum lath or wood lath and plaster ceilings. It is assumed that there is an air space between the under side of the roof deck and the upper side of the ceiling.

[b] 87½ per cent gypsum, 12½ per cent wood fiber. Thickness indicated includes ½ in. gypsum board.

[c] Nominal thicknesses specified—actual thicknesses used in calculations.

TABLE 16. COEFFICIENTS OF TRANSMISSION (U) OF PITCHED ROOFS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

TYPE OF CEILING (APPLIED DIRECTLY TO ROOF RAFTERS)	WOOD SHINGLES (ON 1 x 4 WOOD STRIPS[a] SPACED 2 IN. APART)				ASPHALT SHINGLES OR ROLL ROOFING (ON SOLID WOOD SHEATHING)[a]				SLATE OR TILE[b] (ON SOLID WOOD SHEATHING)[a]				NUMBER
	INSULATION BETWEEN RAFTERS				INSULATION BETWEEN RAFTERS				INSULATION BETWEEN RAFTERS				
	None	Blanket or Bat (Thickness Below)			None	Blanket or Bat (Thickness Below)			None	Blanket or Bat (Thickness Below)			
		1 In.	2 In.	3 In.		1 In.	2 In.	3 In.		1 In.	2 In.	3 In.	
	A	B	C[c]	D[c]	E	F	G[c]	H[c]	I	J	K[c]	L[c]	
No Ceiling Applied to Rafters	0.48[f]	0.15	0.10	0.081	0.52[f]	0.15	0.11	0.084	0.55[f]	0.16	0.11	0.085	1
Metal Lath and Plaster[d]	0.31	0.14	0.10	0.081	0.33	0.15	0.10	0.083	0.34	0.15	0.10	0.083	2
Gypsum Board (⅜ in.) Decorated	0.30	0.14	0.10	0.080	0.32	0.15	0.10	0.082	0.33	0.15	0.10	0.083	3
Wood Lath and Plaster	0.29	0.14	0.10	0.080	0.31	0.14	0.10	0.081	0.32	0.15	0.10	0.082	4
Gypsum Lath (⅜ in.) Plastered[e]	0.29	0.14	0.10	0.079	0.31	0.14	0.10	0.081	0.32	0.15	0.10	0.082	5
Plywood (⅜ in.) Plain or Decorated	0.29	0.14	0.099	0.079	0.30	0.14	0.10	0.081	0.31	0.15	0.10	0.081	6
Insulating Board (½ in.) Plain or Decorated	0.22	0.12	0.090	0.072	0.23	0.12	0.091	0.074	0.24	0.13	0.092	0.074	7
Insulating Board Lath (½ in.) Plastered[e]	0.22	0.12	0.088	0.072	0.22	0.12	0.090	0.073	0.23	0.12	0.091	0.074	8
Insulating Board Lath (1 in.) Plastered[e]	0.16	0.10	0.078	0.064	0.17	0.10	0.079	0.065	0.17	0.10	0.080	0.066	9

[a] Coefficients corrected for framing on basis of 15 per cent area, 2 in. x 4 in. (nominal), 16 in. on centers.

[b] Figures in Columns I, J, K and L may be used with sufficient accuracy for rigid asbestos shingles on wood sheathing. Layer of slater's felt neglected.

[c] Sheathing and wood strips assumed $^{25}/_{32}$ in. thick.

[d] Plaster assumed ¾ in. thick.

[e] Plaster assumed ½ in. thick.

[f] No air space included in 1-A, 1-E or 1-I; all other coefficients based on one air space.

TABLE 17. COMBINED COEFFICIENTS OF TRANSMISSION (U) OF PITCHED ROOFS[a] AND HORIZONTAL CEILINGS—BASED ON CEILING AREA[b]

Coefficients are expressed in Btu per (hour) (square foot of ceiling area) (Fahrenheit degree difference in temperature between the air on the two sides), and are based on an outside wind velocity of 15 mph.

CEILING COEFFICIENT[f] (FROM TABLE 11)	TYPE OF ROOFING AND ROOF SHEATHING						NUMBER
	WOOD SHINGLES ON WOOD STRIPS[d]			ASPHALT SHINGLES[e] OR ROLL ROOFING ON WOOD SHEATHING[c]			
	No Roof Insulation (Rafters Exposed) (U_r = 0.48)	½ In. Insulating Board on Under Side of Rafters (U_r = 0.22)	1 In. Insulating Board on Under Side of Rafters (U_r = 0.16)	No Roof Insulation (Rafters Exposed) (U_r = 0.53)	½ In. Insulating Board on Under Side of Rafters (U_r = 0.23)	1 In. Insulating Board on Under Side of Rafters (U_r = 0.17)	
	A	B	C	D	E	F	
0.10	0.085	0.073	0.066	0.087	0.074	0.067	19
0.11	0.092	0.078	0.07	0.094	0.079	0.071	20
0.12	0.099	0.082	0.074	0.10	0.083	0.075	21
0.13	0.11	0.087	0.078	0.11	0.088	0.079	22
0.14	0.11	0.091	0.081	0.11	0.093	0.083	23
0.15	0.12	0.096	0.084	0.12	0.097	0.086	24
0.16	0.13	0.10	0.087	0.13	0.10	0.089	25
0.17	0.13	0.10	0.090	0.13	0.10	0.092	26
0.18	0.14	0.11	0.093	0.14	0.11	0.095	27
0.19	0.14	0.11	0.095	0.15	0.11	0.098	28
0.20	0.15	0.11	0.098	0.15	0.12	0.10	29
0.21	0.15	0.12	0.10	0.16	0.12	0.10	30
0.22	0.16	0.12	0.10	0.17	0.12	0.11	31
0.23	0.16	0.12	0.10	0.17	0.12	0.11	32
0.24	0.17	0.13	0.11	0.18	0.12	0.11	33
0.25	0.17	0.13	0.11	0.18	0.13	0.11	34
0.26	0.18	0.13	0.11	0.19	0.13	0.11	35
0.27	0.18	0.13	0.11	0.19	0.13	0.12	36
0.28	0.19	0.14	0.12	0.19	0.14	0.12	37
0.29	0.19	0.14	0.12	0.20	0.14	0.12	38
0.30	0.20	0.14	0.12	0.20	0.14	0.12	39
0.34	0.21	0.15	0.12	0.22	0.15	0.13	40
0.35	0.22	0.15	0.13	0.22	0.15	0.13	41
0.36	0.22	0.15	0.13	0.23	0.15	0.13	42
0.37	0.23	0.15	0.13	0.23	0.16	0.13	43
0.45	0.25	0.17	0.13	0.26	0.17	0.14	44
0.59	0.29	0.18	0.14	0.30	0.19	0.15	45
0.61	0.29	0.18	0.15	0.31	0.19	0.15	46
0.62	0.30	0.19	0.15	0.31	0.19	0.15	47
0.67	0.31	0.19	0.15	0.33	0.20	0.16	48
0.69	0.31	0.19	0.15	0.33	0.20	0.16	49

[a]Calculations based on ⅓ pitch roof (n = 1.2) using the following formula:

$$U = \frac{U_r \times U_{ce}}{U_r + \frac{U_{ce}}{n}}$$

U = combined coefficient to be used with ceiling area.
U_r = coefficient of transmission of the roof.
U_{ce} = coefficient of transmission of the ceiling.
n = the ratio of the area of the roof to the area of the ceiling.

[b]Use ceiling area (not roof area) with these coefficients.

[c]Coefficients in Columns D, E and F may be used with sufficient accuracy for tile, slate and rigid asbestos shingles on wood sheathing.

[d]Based on 1 x 4 in. strips spaced 2 in. apart.

[e]Sheathing assumed ⅝ in. thick.

[f]Values of U_{ce} to be used in this column may be selected from Table 11.

TABLE 18. COEFFICIENTS OF TRANSMISSION (U) OF DOORS, WINDOWS, SKYLIGHTS AND GLASS BLOCK WALLS

Coefficients are expressed in Btu per (hour) (square foot) (Fahrenheit degree difference in the temperature between the air inside and outside of the door, window, skylight or wall) and are based on an outside wind velocity of 15 mph.

Section A. Windows and Skylights		SINGLE	DOUBLE	TRIPLE
	U	1.13[ac]	0.45[ae]	0.281[ae]

Section B. Solid Wood Doors[bc]	NOMINAL THICKNESS INCHES	ACTUAL THICKNESS INCHES	U EXPOSED DOOR	U[d] WITH GLASS STORM DOOR
	1	25/32	0.69	0.42
	1¼	1 1/16	0.59	0.38
	1½	1 5/16	0.52	0.35
	1¾	1 3/8	0.51	0.35
	2	1 5/8	0.46	0.32
	2½	2 1/8	0.38	0.28
	3	2 5/8	0.33	0.25

Section C. Hollow Glass Block Walls	DESCRIPTION	U STILL AIR BOTH SIDES	U STILL AIR INSIDE 15 MPH OUTSIDE
	Smooth surface glass blocks 7¾ x 7¾ x 3⅞ in. thick	0.40	0.49
	Ribbed surface glass blocks 7¾ x 7¾ x 3⅞ in. thick	0.38	0.46

[a]See Heating, Ventilating and Air Conditioning, by Harding and Willard, revised edition, 1932.

[b]Computed using $C = 1.15$ for wood; $f_i = 1.65$ and $f_o = 6.0$.

[c]It is sufficiently accurate to use the same coefficient of transmission for doors containing thin wood panels as that of single panes of glass, namely, 1.13 Btu per (hour) (square foot) (degree difference between inside and outside air temperatures).

[d]These values may also be used with sufficient accuracy for wood storm doors. Neglect storm doors if loose and use values for exposed doors.

[e]Air spaces assumed to be ¾ in. or more in width.

Combined Ceiling and Roof Coefficients

If the attic space between ceiling and roof is unheated, the combined coefficient from room air below the ceiling to exterior air can be calculated from the following formula.

$$U = \frac{U_r \times U_{ce}}{U_r + \frac{U_{ce}}{n}} \qquad (5)$$

where

U = combined coefficient to be used with ceiling area.

U_r = coefficient of transmission of roof.

U_{ce} = coefficient of transmission of ceiling.

n = ratio of roof area to ceiling area.

It should be noted that the over-all coefficient U should be multiplied by the ceiling area to determine heat loss and not by the roof area. Values of U_r and U_{ce} should be calculated using a value of 2.2 (the reciprocal of one-half the air space resistance) rather than 1.65 for the conductances of surfaces facing the attic, since the attic is equivalent to an air space.

If the attic contains windows, dormers and vertical wall spaces and if their area is small compared to that of the roof, they may be considered part of the roof area. For accuracy, the sum of the coefficients of each

individual section multiplied by its percentage of the total area should be used as U_r. Where attic wall areas are large it is preferable to estimate the attic temperature as illustrated in Chapter 14 and calculate the heat loss through the ceiling by multiplying the value of U_{ce} for the ceiling by the difference in temperature above and below the ceiling.

Basement Floor, Basement Wall and Concrete Slab Floor Coefficients

The heat transfer through basement walls and floors to the ground is dependent on the temperature difference between the air within and that of the ground, on the material constituting the wall or floor, and on the conductivity of the surrounding earth. The conductivity of the earth will vary with local conditions and is usually unknown. Tests [8] at the A.S.H.V.E. Research Laboratory indicate a heat flow of approximately 2.0 Btu per (hour) (square foot) through an uninsulated concrete basement floor with a temperature difference of 20 F between ground temperature and the air temperature 6 in. above the floor. Based on this result, a coefficient of 0.10 Btu per (hour) (square foot) (Fahrenheit degree difference) is recommended for calculation where it is desirable to allow for the small basement floor heat loss, *e.g.* for heated basements.

For basement walls the same coefficient may be used, but due to closer proximity to the surface of the ground, the temperature difference for winter design conditions will be greater than for the floor. The test results indicate a unit area heat loss, at mid-height of the basement wall, approximately twice that of the same floor area.

For concrete slab floors laid in contact with the ground at grade level, recent tests [9] indicate that for small floor areas (equal to that of a house 25 ft square) the heat loss may be calculated as proportional to the length of exposed edge rather than total area. This amounts to 0.81 Btu per (hour) (lineal foot of exposed edge) (Fahrenheit degree difference between the inside air temperature and the average outside air temperature). It should be noted that this may be appreciably reduced by insulating the edges of the floor from the abutting wall.

CONDENSATION IN BUILDINGS

Water vapor in the air within a building condenses if it comes in contact with surfaces at or below its dew-point temperature. It also will be transmitted into or through a wall, floor or ceiling, if a vapor pressure difference exists between the opposite sides, at a rate determined by the permeability of the materials encountered [10] (see Table 17 Chapter 15). Building practice must take account of these facts in avoiding (1) surface condensation on interior building surfaces (walls, ceilings, roofs or glass) and (2) interstitial condensation or accumulation of condensation in the voids within the structure. The conditions under which surface condensation will take place are directly dependent on surface temperature and upon the relative humidity of the air in contact. Limiting maximum relative humidities for walls, roofs or glass having transmission coefficients up to 1.2 Btu for outside temperatures from −30 F to 40 F and for 70 F inside temperature may be obtained from Fig. 4 [11].

Surface condensation may be controlled by air conditioning, ventilation for the purpose of removing water vapor, particularly from laundries and from kitchens during lengthy periods of cooking, elimination of sources of vapor such as unvented gas stoves, or by local application of heat or insulation to raise surface temperatures.

Interstitial condensation results from vapor transmission which is dependent on vapor pressure differential and the ratio of the rate at which vapor may enter the materials of the structure to that at which it passes out of the structure. The proper installation of a vapor barrier on the warm side of the structure, where the higher vapor pressure usually exists, will reduce greatly the amount of vapor entering the building construction and will minimize the possibility of objectionable condensation. Such a barrier may consist of a coated paper applied under the plaster, a coated plaster base, or a vapor-resistant finish applied to the interior wall surface [12]. A vapor barrier is tentatively defined as a

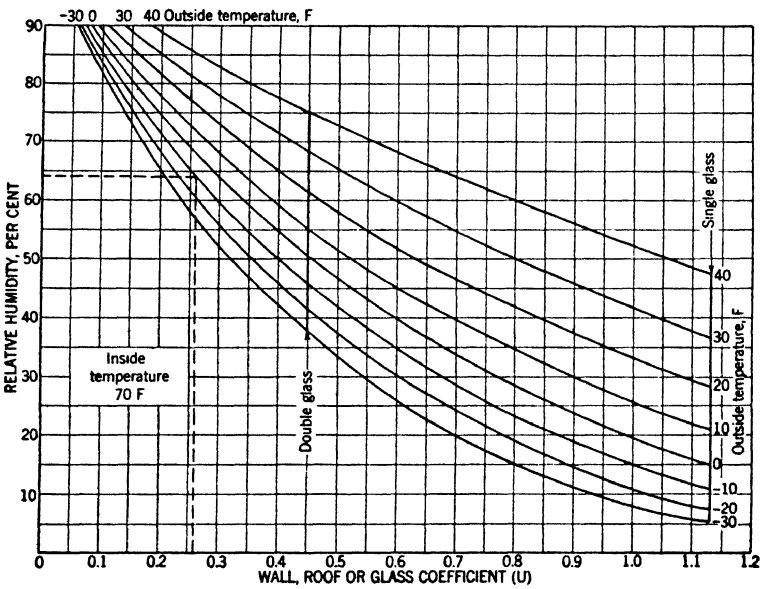


FIG. 4. PERMISSIBLE RELATIVE HUMIDITIES FOR VARIOUS TRANSMISSION COEFFICIENTS

material having a water vapor permeability not exceeding 1.25 grains per (hour) (square foot) (inch of Hg vapor pressure differential).

To prevent condensation on the under side of roofs above attic spaces over insulated ceilings, ventilation with outside air may be provided through suitable louvers or other roof ventilators.

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Chapter 7

PERFORMANCE OF AIR HEATING AND COOLING COILS

Performance of Heating and Dry Cooling Coils, Over-all Coefficient of Heat Transfer, Performance of Dehumidifying Coils, External Film Coefficient, Internal Film Coefficient, Determining Size of Cooling Coil

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THE surfaces described in this chapter are for heating or cooling an air stream under the conditions of forced convection. Such surfaces may be made up of a number of banks of tubes assembled in the field or the entire assembly may be factory constructed. They may be made of either bare or finned tubing, but regardless of their construction they are generally referred to as *coils*. A description of the types, application, and selection of such coils is given in Chapter 25. Therefore, this chapter is confined to the theoretical considerations which affect the calculation of the performance of these coils.

PERFORMANCE OF HEATING AND DRY COOLING COILS

The performance of heating and dry cooling coils depends in general upon:

1. The over-all coefficient of heat transfer from the fluid within the coil to the air it heats or cools.

2. The mean temperature difference between the fluid within the coil and the air flowing over the coil.

3. The physical dimensions of the coil.

Thus, for any one definite operating condition, the heating or cooling capacity of a given coil is expressed by the following basic formula:

$$q_t = U \times (MTD) \times A \times N \qquad (1)$$

where

q_t = total heat transferred by the coil, Btu per (hour) (square foot of coil face area).

U = over-all coefficient of heat transfer, Btu per (hour) (square foot of external coil surface) (Fahrenheit degree temperature difference between the fluid within the coil and the air flowing over the coil).

MTD = mean temperature difference, Fahrenheit degrees, between the fluid within the coil and the air passing over it. (This is commonly taken as the logarithmic mean temperature difference.)

A = external surface area of the given coil, square feet per (square foot of coil face area) (row of coil depth).

N = number of rows of coil depth.

Over-all Coefficient of Heat Transfer

Of all factors affecting the performance of heating or dry cooling coils, the over-all coefficient of heat transfer is the most difficult to determine as it is influenced by several factors which depend upon coil design and conditions of operation.

Considering any coil, whether of bare pipe or of finned type, the over-all heat transfer coefficient for a given size and design of coil can always be

considered as a combined effect of three individual heat transfer coefficients, namely:

1. The film coefficient of heat transfer between air and the external surface of the coil, usually given in Btu per (hour) (square foot external surface) (Fahrenheit degree mean temperature difference).
2. The coefficient of heat transfer through the coil material—tube wall, fins, ribs, etc.
3. The film coefficient of heat transfer between the internal surface of the coil and the fluid flowing within the coil, usually given in Btu per (hour) (square foot internal surface) (Fahrenheit degree mean temperature difference).

These three individual coefficients acting in series result in an over-all coefficient of heat transfer in accordance with the basic laws given in Chapters 5 and 6. For a *bare pipe* coil the over-all coefficient of heat transfer, whether for heating or for cooling (without dehumidification), can be expressed by a simplified basic formula as follows:

$$U = \frac{1}{\frac{R}{h_r} + \frac{L}{k} + \frac{1}{h_a}} \tag{2}$$

where

U = over-all coefficient of heat transfer, Btu per (hour) (square foot external surface) (Fahrenheit degree mean temperature difference between air and fluid within the coil).

h_r = film coefficient of heat transfer between the internal surface of the coil and the fluid flowing within the coil, Btu per (hour) (square foot internal surface) (Fahrenheit degree mean temperature difference between that surface and the average fluid temperature).

h_a = film coefficient of heat transfer between air and the external surface of the coil, Btu per (hour) (square foot external surface) (Fahrenheit degree mean temperature difference between the mass of air and the external surface).

k = conductivity of material from which the bare pipe is constructed, Btu per (hour) (square foot) (Fahrenheit degree per inch thickness).

L = thickness of tube wall, inches.

R = ratio between external and internal surface of the bare tube, usually varying from 1.03 to 1.15 for the tube used in typical heating or cooling coils. This ratio R is inserted in the formula in order to place internal fluid coefficient of heat transfer on the basis of external surface.

Frequently, when pipe or tube walls are thin and of material having high conductivity (as is the case in construction of typical heating and cooling coils) the term L/k in Equation 2 becomes negligible and is generally disregarded. (The effect of the term L/k in typical bare pipe heating or cooling coils seldom exceeds 1 to 2 per cent of the over-all coefficient). Thus, in its simplest form, for bare pipe:

$$U = \frac{1}{\frac{R}{h_r} + \frac{1}{h_a}} \tag{3}$$

For finned coils the formula[1] for the over-all coefficient of heat transfer can be conveniently written:

$$U = \frac{1}{\frac{R}{h_r} + \frac{1}{\eta h_a}} \tag{4}$$

in which the term η, called the *fin efficiency*, is introduced to allow for the resistance to heat flow encountered in the fins.

The term R, in this case, is the ratio of *total* external surface to internal surface. For typical designs of finned coils for heating or cooling, this ratio varies from 10 to 30. Term R is again introduced to place the internal surface coefficient of heat transfer on a basis of external surface.

In the discussions which follow, coefficients h_r and ηh_a will be considered separately, and also various ways of combining them will be outlined.

The performances of all heating and dry cooling coils are influenced by these same factors. But, when cooling coils operate wet or act as dehumidifying coils, the performance cannot be predicted on the basis of over-all coefficients and an analysis must be made on the basis of individual film coefficients as will be explained.

PERFORMANCE OF DEHUMIDIFYING COILS

When a cooling coil operates with a surface temperature which is below the dew-point of the air entering the coil, moisture is condensed and the air leaves the coil with a humidity ratio lower than it had when

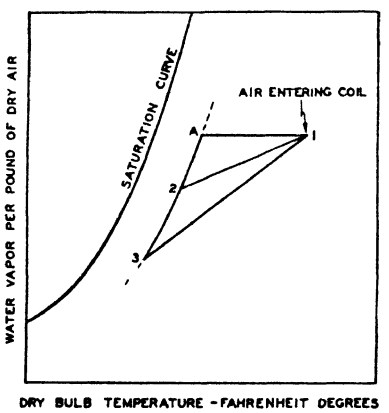

FIG. 1. PERFORMANCE OF DEHUMIDIFYING COIL

it entered the coil. To understand the performance of surface coils under such conditions, assume that air enters a cooling coil at conditions corresponding to point 1 in Fig. 1. As long as the surface temperature of the coil is above the dew-point, the air is cooled without dehumidification, and its condition leaving the coil will be somewhere on line 1-A. Its exact position on this line depends on the air velocity and the external film coefficient as well as upon the surface temperature. When the surface temperature just equals the dew-point, the air leaves with conditions represented by point A. If the surface temperature is below the dew-point, condensation takes place, and the air has a final condition somewhere along the line A-2-3 which is a line at a constant horizontal distance from the saturation curve. It should be understood that the line 1-A-2-3 is not intended to represent the path of the condition of the air as it passes through the coil from row to row. It is simply the path traced by the exit air conditions as the surface temperature is gradually reduced with other conditions remaining constant[2].

In the process of dehumidification, since heat is being transferred to the coil surface by two different mechanisms, (convection and condensation), it is evident that an over-all coefficient of heat transfer cannot be determined by the same method used for heating and for dry cooling coils. However, if it is assumed that the sensible heat transfer of a dehumidifying coil is unaffected by the presence of moisture on its surface, Equation 5 may be obtained to express this part of the heat

transfer in terms of the external film coefficient and the surface temperature.

$$q_s = h_a \times A \times N \times (MTD_a) \tag{5}$$

where

q_s = sensible heat transferred, Btu per (hour) (square foot of coil face area).
t_1 = dry-bulb temperature of air entering coil, Fahrenheit degrees.
t_2 = dry-bulb temperature of air leaving coil, Fahrenheit degrees.
t_s = average temperature of coil external surface, Fahrenheit degrees.
MTD_a = logarithmic mean temperature difference between air and coil surface = $\dfrac{t_1 - t_2}{\log_e \dfrac{t_1 - t_s}{t_2 - t_s}}$

If Equation 5 is combined with another equation expressing sensible heat transfer in terms of mass velocity and temperature difference, the variables may be arranged in the following form (which is useful for the solution of dehumidification problems and for the determination of h_a from test data):

$$\frac{h_a A N (t_1 - t_2)}{\log_e \dfrac{t_1 - t_s}{t_2 - t_s}} = 0.243 G (t_1 - t_2)$$

or,

$$\frac{h_a A N}{0.243G} = \log_e \frac{t_1 - t_s}{t_2 - t_s} \tag{6}$$

where

0.243 = specific heat of humid air, Btu per (pound) (Fahrenheit degree).
G = air mass velocity, pounds per (hour) (square foot of coil face area).

An examination of Fig. 1 will reveal that when t_s is at the dew-point of the entering air:

$$\frac{t_1 - t_s}{t_a - t_s} = \frac{t_1 - t_{dp1}}{t_a - t_{dp1}}$$

and when t_s is below the dew-point:

$$\frac{t_1 - t_s}{t_2 - t_s} = \frac{t_1 - t_{dp1}}{t_2 - t_{dp2}}$$

Therefore, Equation 6 may be written in its most useful form as:

$$\frac{h_a A N}{0.243G} = \log_e \frac{t_1 - t_{dp1}}{t_2 - t_{dp2}} = \log_e \frac{t_1 - t_s}{t_2 - t_s} \tag{7}$$

where

t_a = minimum dry-bulb possible without dehumidification, Fahrenheit degrees.
t_{dp1} = dew-point of air entering coil, Fahrenheit degrees.
t_{dp2} = dew-point of air leaving coil, Fahrenheit degrees.

This equation may be used to establish a line as A-2-3 for a given coil if h_a is known for the coil, or it *may be used to determine h_a from test data for the purpose of rating coils.* The use of this equation for coil selection is illustrated in Example 1 at the end of the chapter. Equation 7 is also important as a means of determining the external film coefficient.

External Film Coefficient

While formulas have been developed expressing the film coefficient h_a for air passing parallel to a plane surface, they cannot be used directly

for fins on tubes because of air turbulence and because of the temperature gradient prevalent from the edge of a fin to its center. It is therefore necessary to make tests to evaluate the combined term ηh_a. The term, ηh_a, will be written merely h_a in this discussion as there is no necessity for separately evaluating η and because values of h_a are usually applied only to the particular coils for which tests are made.

The air side coefficient, h_a, of a coil of particular dimensions is an exponential function of the mass velocity of the air:

$$h_a = Z G^n \tag{8}$$

where

h_a = film coefficient of heat transfer, Btu per (hour) (square foot external surface) (Fahrenheit degree mean temperature difference between air and average surface temperature).

G = air mass velocity, pounds per (hour) (square foot of coil face area).

Z and n = constants which depend upon both air turbulence and surface arrangement.

Evaluation of constants Z and n may be accomplished through the use of test data in Equation 7 which gives values of h_a directly from the results of any *wet coil test.* If h_a, calculated in this manner, is plotted against values of G which prevailed during the tests a straight line should result on logarithmic coordinates. The slope of this line is the value of n. The value of Z may then be determined by direct substitution in Equation 8.

For finned coils of different designs, values of Z and n are extremely variable, depending on the particular design and arrangement of the coil surface. Therefore, it is desirable that these constants be determined directly from test data for each type of coil surface.

Internal Film Coefficient

The internal film coefficient, h_r which appears in Equation 3, is evaluated in various ways, depending upon the nature of the fluid, and whether the fluid is changing state.

When evaporating refrigerants are used in tubes, the temperature of the fluid is fairly constant, being affected principally by pressure drop through the tubes, by superheat of the evaporated refrigerant, and by the presence of oil in solution. To obtain maximum coil capacity it is necessary to keep the pressure drop through the tubes at a minimum, to keep the superheat as low as possible without carrying liquid back to the compressor, and to arrange for good separation and return of oil to the compressor. Another important factor is the removal of gas to keep the tube surface flooded with liquids as much as possible. The internal film coefficient is markedly increased by heavy heat loads, because the increased turbulence and gas velocity cause good contact of the liquid with the tubes. Values of h_r usually lie between 150 and 450. For rating of dehumidifying coils, satisfactory results are obtainable by first determining the average external surface temperature from Equation 7, and then using the difference between the external film temperature and the refrigerant for evaluating h_r in Equation 9.

$$h_r = \frac{q_t}{\frac{A N}{R}(t_s - t_r)} \tag{9}$$

where

h_r = internal film coefficient of heat transfer, Btu per (hour) (square foot of internal tube surface) (Fahrenheit degree).

t_r = average refrigerant temperature, Fahrenheit degrees.

The term $(t_s - t_r)$ is commonly written Δt. To evaluate h_r by this method the same tests that were required to determine h_a may be used.

When water is the cooling medium in tubes, the rate of heat transfer is a function of its velocity, which influences the number of contacts of the water molecules with the tube surface, per unit of time. Increased water velocity and reduced tube diameter cause increased heat transfer. Heat transfer is also greater at higher temperatures of the water. The basic formula for the film coefficient of heat transfer for flow of water in smooth tubes is as follows:

$$h_r = 1.5\ (t + 100)\ \frac{V^{0.8}}{D^{0.2}} \qquad (10)$$

where

V = water velocity, feet per second.

D = internal diameter of tube, inches.

t = average water temperature, Fahrenheit degrees.

Equation 10 should not be used when Reynolds Number is less than 2000.

Since, in the case of finned tubes using water as a refrigerant, test values of h_r based on the calculated surface temperature for the entire coil may be lower than those obtained by use of Equation 10, actual test results are preferred if available.

When saturated steam is condensed in the tubes of coils, the film coefficient h_r varies from 1000 to 2000, depending on freedom from air in the steam, and upon good drainage of the tubes. The coefficient is fairly constant for a particular coil, giving values of Δt that are directly proportional to q_t. However, if water coil test results are analyzed on a row-by-row basis good agreement with Equation 10 will result.[3]

The use of turbulence promoters increases the value of h_r for liquids in tubes at the expense of pressure drop. The increase obtained depends upon the type of turbulence promoter and the rate of flow. No general statement can be made regarding their use and it is best to refer to detailed papers on this subject for further information.[3,4]

Determining Size of Cooling Coil

To illustrate the use of individual film coefficients in coil calculations, the procedure for selecting the proper size cooling coil and for determining exit air condition, coil surface temperature, total coil load and refrigerant temperature is outlined in Example 1.

Example 1. An industrial application requires the cooling of a certain quantity of air from a condition of 102 F dry-bulb and 85 F wet-bulb to a final condition of 80.5 F dry-bulb and 73 F wet-bulb. The air velocity across the coil is to be 400 fpm and coil data are as follows: h_a = 10.7 at 400 fpm, h_r = 325, external surface area = 15 sq ft per (square foot of face) (row of coil depth), ratio of external surface area to internal surface area = 15.

Solution. (1) Lay out the problem psychrometry as indicated in Fig. 2 and note that the minimum horizontal distance between the load ratio line and the saturation curve is 1.8 F dry-bulb at point A Fig. 2. This means that $t_2 - t_{dp2}$ in Equation 7 must not be less than 1.8. Therefore, Equation 7 should be solved for N to determine the proper number of rows to be used for the coil.

$$\frac{h_a A N}{0.243 G} = \log_e \frac{t_1 - t_{dp1}}{t_2 - t_{dp2}} = \log_e \frac{102 - 80}{1.8} = \log_e 12.22 = 2.5$$

Then substituting values for h_a, A, and G, N may be found as follows:

$$\frac{10.7 \times 15N}{0.243 \times 1740} = 2.5 \text{ from which, } N = 6.58$$

(2) This establishes the maximum whole number of coil rows that can be used as 6 and it is now possible to determine the actual location of the exit air conditions from Equation 7 by solving for the actual value of $t_2 - t_{dp2}$ for a 6 row coil.

$$\frac{10.7 \times 15 \times 6}{0.243 \times 1740} = \log_e \frac{102 - 80}{t_1 - t_{dp2}} = 2.275$$

This establishes values of 9.78 for $\frac{t_1 - t_{dp1}}{t_2 - t_{dp2}} = R$ and 2.25 for $t_2 - t_{dp2}$.

(3) Next, the exit air condition at 57.3 F dry-bulb and 56 F wet-bulb as shown at B, is found by locating a point on the load ratio line at a horizontal distance of 2.25 dry-bulb degrees from the saturation curve.

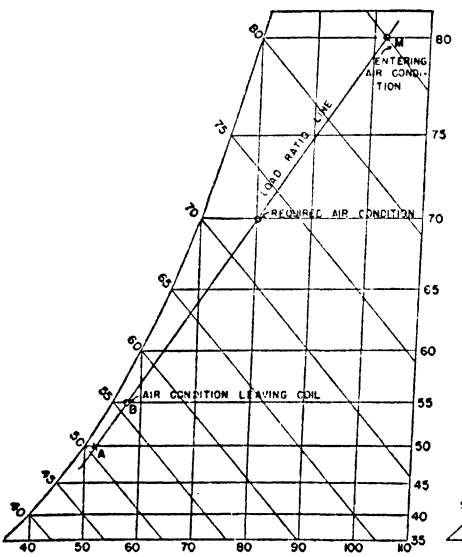

FIG. 2. PSYCHROMETRIC LAYOUT FOR COIL SELECTION

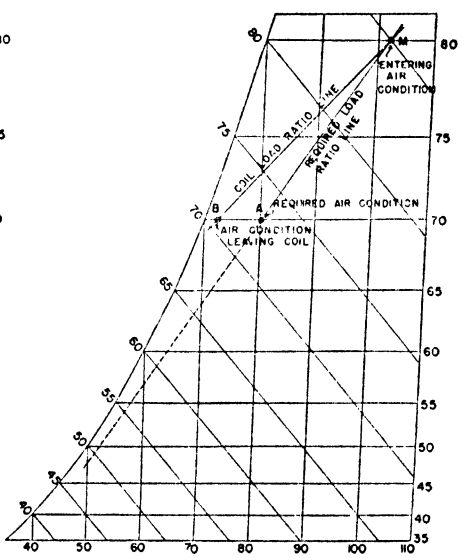

FIG. 3. PSYCHROMETRIC LAYOUT FOR COIL SELECTION USING REHEAT

(4) The surface temperature may now be found from Equation 7 which may also be written as:

$$t_s = \frac{Bt_2 - t_1}{B - 1}$$

where

$$B = \frac{t_1 - t_{dp1}}{t_2 - t_{dp2}}$$

$$t_s = \frac{9.78 \times 57.3 - 102}{8.78} = 52.3$$

(5) The total coil load may be calculated from the enthalpy difference across the coil and the air quantity using the weight of dry air instead of the weight of the mixture.

$$q_t = G_a (h_1 - h_2)$$
$$= 1700 (49.24 - 23.77) = 43{,}200 \text{ Btu per (hr) (sq ft of face area)}$$

where

G_a = Weight of dry air per (hour) (square foot of coil face area).
h_1 = enthalpy of air vapor mixture entering coil, Btu per pound of dry air.
h_2 = enthalpy of air vapor mixture leaving coil, Btu per pound of dry air.

(6) The refrigerant temperature may be found from Equation 9

$$\frac{43{,}200}{15 \times 6 \times \frac{325}{15}} = (t_s - t_r) = 22.1$$

Therefore, $t_r = (52.3 - 22.1) = 30.2$.

Thus a coil 6 rows deep operating at a refrigerant temperature of 30.2 F and a face velocity of 400 fpm is required and it will carry a total load of 43,200 Btu per (hour) (square foot of face area). The air conditions leaving the coil are too low for the conditions of the problem and therefore it is necessary to by-pass air at the entering condition to obtain the desired result of 80.5 F dry-bulb and 73 F wet-bulb.

Although the preceding solution is satisfactory, it may be more desirable in some cases to use a higher refrigerant temperature and employ reheat to obtain the desired load ratio. Such a solution is shown in Fig. 3. In this case the coil load ratio line intersects the saturation curve and therefore a coil of any depth may be selected.

If a coil depth of 6 rows is maintained, the exit air conditions for the coil are indicated at point B Fig. 3 as 72.3 F dry-bulb and 70.8 F wet-bulb and the surface temperature will be:

$$t_s = \frac{9.78 \times 72.3 - 102}{8.78} = 69.0$$

The coil load will be: $q_t = 1700\ (49.24 - 34.66) = 24{,}800$ Btu per (hour) (square foot of face area) and the refrigerant temperature will be found from Equation 9:

$$\frac{24{,}800}{15 \times 6 \times \frac{325}{15}} = (t_s - t_r) = 12.7$$

Therefore, $t_r = 69.0 - 12.7 = 56.3$.

Thus, for the case where reheat is used, a coil 6 rows deep operating at a refrigerant temperature of 56.3 F is required. The total coil load will be 24,800 Btu per (hour) (square foot of face area) but the actual effective load will be less by the amount of reheat required. Therefore, for a given load, a larger coil and more refrigerating capacity are required when reheat is used.

LETTER SYMBOLS USED IN CHAPTER 7

η = fin efficiency.
A = external area of coil, square feet per (square foot of coil face area) (row of coil depth).
$B = \frac{t_1 - t_{dp1}}{t_2 - t_{dp2}}$
D = internal diameter of tube, inches.
G = air mass velocity, pounds per (hour) (square foot of coil face area).
G_a = dry air mass velocity, pounds dry air per (hour) (square foot of coil face area).
h_1 = enthalpy of air-vapor mixture entering coil, Btu per pound of dry air.
h_2 = enthalpy of air-vapor mixture leaving coil, Btu per pound of dry air.
h_a = film coefficient of heat transfer between air and external coil surface, Btu per (hour) (square foot external surface) (Fahrenheit degree mean temperature difference between air and coil).
h_r = film coefficient of heat transfer between fluid and internal coil surface, Btu per (hour) (square foot internal surface) (Fahrenheit degree mean temperature between fluid and surface).

k = conductivity of pipe or tube material, Btu (square foot) (hour) (Fahrenheit degree per inch thickness).

L = thickness of tube wall, inches.

MTD = abbreviation—mean temperature difference between fluid in coil and air passing over coil, Fahrenheit degrees.
NOTE: MTD—usually logarithmic mean.

MTD_a = logarithmic mean temperature difference between air and coil surface.

N = number of rows of coil depth.

n = a constant, exponent of G in Equation 8, obtained by plotting, on logarithmic coordinates, G against values of h_a. The value of n is the slope of the line.

q_s = sensible heat transferred, Btu per (hour) (square foot of coil face area).

q_t = total heat transferred by coil, Btu per (hour) (square foot of face area).

R = ratio between external and internal surface of tube.

t = average water temperature, Fahrenheit degrees.

t_1 = dry-bulb temperature of air entering coil, Fahrenheit degrees.

t_2 = dry-bulb temperature of air leaving coil, Fahrenheit degrees.

t_a = minimum dry-bulb temperature possible without dehumidification, Fahrenheit degrees.

t_{dp1} = dew-point of air entering coil, Fahrenheit degrees.

t_{dp2} = dew-point of air leaving coil, Fahrenheit degrees.

t_r = average refrigerant temperature, Fahrenheit degrees.

t_s = average temperature of external surface of coil, Fahrenheit degrees.

$\Delta t = t_s - t_r$.

U = over-all coefficient of heat transfer, Btu per (hour) (square foot of external coil surface) (Fahrenheit degrees temperature difference between fluid in coil and air flowing over coil).

V = water velocity, feet per second.

Z = a constant for use in Equation 8 obtained by plotting on logarithmic coordinates G against values of h_a.

NOTE: Numerical subscripts refer to condition entering and leaving respectively.

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Chapter 8

AIR LEAKAGE

Causes of Infiltration, Infiltration Due to Wind Pressure, Infiltration Through Walls, Window and Door Leakage, Crack Method, Air Change Method, Infiltration Due to Temperature Difference, Sealing of Vertical Openings

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THE air leakage which takes place through various apertures in buildings must be considered in heating and cooling calculations, and properly evaluated. This *infiltration* as it is sometimes designated takes place through cracks around doors and windows, through solid walls and through fireplaces and chimneys. Although the latter sources of leakage may be considerable, they are often neglected on the assumption that dampers would be closed during periods of extreme cold weather or else that the fireplace will be in use at such times and will therefore contribute to the heat supplied and lessen the heating load.

CAUSES OF INFILTRATION

The displacement of heated air in buildings by unheated outside air is due to two causes, namely, (1) the pressure exerted by the wind and (2) the difference in density of outside and inside air because of differences in temperature. The former is generally referred to as *infiltration* and the latter as *stack* or *chimney effect.*

In either case an exact estimate of the amount of infiltration under design conditions is difficult to make. The complicating factors include (1) variations in building construction particularly as to width of crack or size of openings through which air leakage takes place, (2) the variations in wind velocity and direction, (3) the exposure of the building with respect to air leakage openings and with respect to adjoining buildings, (4) the variations in outside temperatures which influence the chimney effect, (5) the relative area and resistance of openings on the windward and leeward sides and on the lower floors and on the upper floors, and (6) the influence of a planned air supply and the related outlet vents. Tight construction is essential for preventing large heat loss due to infiltration.

INFILTRATION DUE TO WIND PRESSURE

The wind causes a pressure to be exerted on one or two sides of a building. As a result, air comes into the building on the windward side through cracks or porous construction, and a similar quantity of air leaves on the leeward side through like openings. In general the resistance to air movement is similar on the windward to that on the leeward side. This causes a building up of pressure within the building and a lesser air leakage than that experienced in single wall tests as determined in the laboratory. It is assumed that actual building leakages owing to this building up of pressure will be 80 per cent of laboratory test values. While there are cases where this is not true, tests in actual buildings substantiate the factor for the general case. Mechanical ventilating systems are frequently designed to produce positive or negative pressures in an enclosure which are greater or lower than prevalent wind pressures. In such designs, if the rate at which air is specified to be introduced to or removed from the enclosure by positive means exceeds the infiltration rate, it is common practice to use the greater value in determining the heating capacity to warm the outside air.

Infiltration Through Walls

Data on infiltration through brick and frame walls are given in Table 1[1]. The brick walls listed in this table are walls which show poor workmanship and which are constructed of porous brick and lime mortar. For good workmanship, the leakage through hard brick walls with cement-lime mortar does not exceed one-third the values given. These tests indicate that plastering reduces the leakage by about 96 per cent; a heavy coat of cold water paint, 50 per cent; and 3 coats of oil paint carefully applied, 28 per cent. The infiltration through walls ranges from 6 to 25 per cent of that through windows and doors in a 10-story office building, with imperfect sealing of plaster at the baseboards of the rooms. With perfect sealing the range is from 0.5 to 2.7 per cent or a practically negligible quantity, which indicates the importance of good workmanship in proper sealing at the baseboard. It will be noted from Table 1, that the infiltration through properly plastered walls can be neglected.

The value of building paper when applied between sheathing and

TABLE 1. INFILTRATION THROUGH WALLS[a]

Expressed in cubic feet per square foot per hour

TYPE OF WALL	WIND VELOCITY, MILES PER HOUR					
	5	10	15	20	25	30
8½ in. Brick Wall[b] .. Plain	2	4	8	12	19	23
8½ in. Brick Wall[b] .. Plastered[c]	0.02	0.04	0.07	0.11	0.16	0.24
13 in. Brick Wall[b] .... Plain	1	4	7	12	16	21
13 in. Brick Wall[b] .... Plastered[c]	0.01	0.01	0.03	0.04	0.07	0.10
13 in. Brick Wall[b] .... Plastered[d]	0.03	0.10	0.21	0.36	0.53	0.72
Frame Wall, with lath and plaster[e] ..	0.03	0.07	0.13	0.18	0.23	0.26

[a]The values given in this table are 20 per cent less than test values to allow for building up of pressure in rooms and are based on test data reported in the papers listed in chapter footnotes.

[b]Constructed of porous brick and lime mortar—workmanship poor.

[c]Two coats prepared gypsum plaster on brick.

[d]Furring, lath, and two coats prepared gypsum plaster on brick.

[e]Wall construction: Bevel siding painted or cedar shingles, sheathing, building paper, wood lath and three coats gypsum plaster.

shingles is indicated by Fig. 1, which represents the effect on outside construction only, without lath and plaster. The effectiveness of plaster properly applied is no justification for the use of low grade building paper or of the poor construction of the wall containing it. Not only is it difficult to secure and maintain the full effectiveness of the plaster but also it is highly desirable to have two points of high resistance to air flow with an air space between them. The infiltration indicated in Fig. 1 is that determined in the laboratory and should be multiplied by the factor 0.80 to give proper working values.

Window and Door Leakage

There are two methods of estimating air leakage through window and door cracks, namely, (1) the crack method and (2) the air change method. The crack method is generally regarded as being more accurate than the purely arbitrary air change method, provided the variables such as crack width and clearance, can be properly evaluated.

Crack Method

The crack method is based on known air leakage factors for various types of windows and widths of crack and clearance. The wind velocity and length of crack are also considered when the crack method is employed. The amount of infiltration for various types of windows is given in Table 2[2]. The fit of double-hung wood windows is determined by crack and clearance. Crack thickness is equivalent to one-half the difference between the inside window frame dimension and the outside sash width. The difference between the width of the window frame guide and the sash thickness is considered as the clearance. The length of the perimeter opening or crack for a double-hung window is equal to three times the width plus two times the height, or in other words, it is the outer sash perimeter length plus the meeting rail length. Not all the window crack in any given room is necessarily used in estimating the infiltration heat

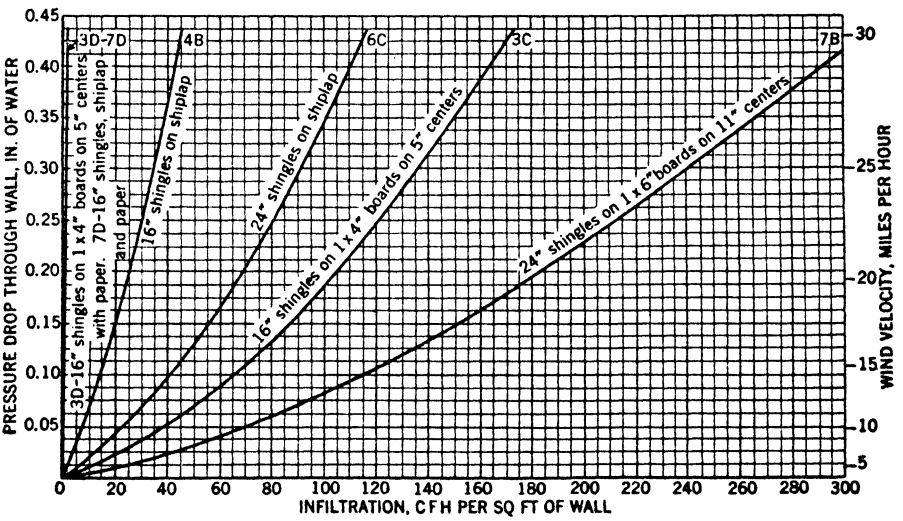

FIG. 1. INFILTRATION THROUGH VARIOUS TYPES OF SHINGLE CONSTRUCTION

loss by the crack method. The length of crack to be selected in any given case depends on the number of exposed sides as explained in Chapter 14.

Values of leakage shown in Table 2 for the average double-hung wood window were determined by using, on nine windows tested in the laboratory, the average measured crack and clearance of a large number of windows found in a field survey. In addition, the table gives figures for a poorly fitted window. All of the figures for double-hung wood windows are for the *unlocked* condition. Just how a window is closed, or fits when it is closed, has considerable influence on the leakage. The leakage will be high if the sash are short, if the meeting rail members are warped, or if the frame and sash are not fitted squarely to each other. It is possible to have a window with approximately the average crack and clearance that will have a leakage at least double that of the figures shown. Values for the average double-hung wood window in Table 2 are considered to be easily obtainable figures provided the workmanship on the window is good. Should it be known that the windows under consideration are poorly fitted, the larger leakage values should be used. Locking a window

TABLE 2. INFILTRATION THROUGH WINDOWS

Expressed in Cubic Feet per Foot of Crack per Hour[a]

TYPE OF WINDOW	REMARKS	WIND VELOCITY, MILES PER HOUR					
		5	10	15	20	25	30
Double-Hung Wood Sash Windows (Unlocked)	Around frame in masonry wall—not calked[b]	3	8	14	20	27	35
	Around frame in masonry wall—calked[b]	1	2	3	4	5	6
	Around frame in wood frame construction[b]	2	6	11	17	23	30
	Total for average window, non-weatherstripped, 1/16-in. crack and 3/64-in. clearance.[c] Includes wood frame leakage[d]	7	21	39	59	80	104
	Ditto, weatherstripped[d]	4	13	24	36	49	63
	Total for poorly fitted window, non-weatherstripped, 1/32-in. crack and 3/32-in. clearance.[e] Includes wood frame leakage[d]	27	69	111	154	199	249
	Ditto, weatherstripped[d]	6	19	34	51	71	92
Double-Hung Metal Windows[f]	Non-weatherstripped, locked	20	45	70	96	125	154
	Non-weatherstripped, unlocked	20	47	74	104	137	170
	Weatherstripped, unlocked	6	19	32	46	60	76
Rolled Section Steel Sash Windows[k]	Industrial pivoted, 1/16-in. crack[g]	52	108	176	244	304	372
	Architectural projected, 1/32-in. crack[h]	15	36	62	86	112	139
	Architectural projected, 3/64-in. crack[h]	20	52	88	116	152	182
	Residential casement, 1/64-in. crack[i]	6	18	33	47	60	74
	Residential casement, 1/32-in. crack[i]	14	32	52	76	100	128
	Heavy casement section, projected, 1/64-in. crack[j]	3	10	18	26	36	48
	Heavy casement section, projected 1/32-in. crack[j]	8	24	38	54	72	92
Hollow Metal, vertically pivoted window[f]		30	88	145	186	221	242

[a] The values given in this table, with the exception of those for double-hung and hollow metal windows, are 20 per cent less than test values to allow for building up of pressure in rooms, and are based on test data reported in the papers listed in chapter footnotes.

[b] The values given for frame leakage are per foot of sash perimeter as determined for double-hung wood windows. Some of the frame leakage in masonry walls originates in the brick wall itself and cannot be prevented by calking. For the additional reason that calking is not done perfectly and deteriorates with time, it is considered advisable to choose the masonry frame leakage values for calked frames as the average determined by the calked and non-calked tests.

[c] The fit of the average double-hung wood window was determined as 1/16-in. crack and 3/64-in. clearance by measurements on approximately 600 windows under heating season conditions.

[d] The values given are the totals for the window opening per foot of sash perimeter and include frame leakage and so-called *elsewhere* leakage. The frame leakage values included are for wood frame construction but apply as well to masonry construction assuming a 50 per cent efficiency of frame calking.

[e] A 1/32-in. crack and clearance represent a poorly fitted window, much poorer than average.

[f] Windows tested in place in building.

[g] Industrial pivoted window generally used in industrial buildings. Ventilators horizontally pivoted at center or slightly above, lower part swinging out.

[h] Architecturally projected made of same sections as industrial pivoted except that outside framing member is heavier, and it has refinements in weathering and hardware. Used in semi-monumental buildings such as schools. Ventilators swing in or out and are balanced on side arms. 1/32-in crack is obtainable in the best practice of manufacture and installation, 3/64-in. crack considered to represent average practice.

[i] Of same design and section shapes as so-called *heavy section casement* but of lighter weight. 1/64-in. crack is obtainable in the best practice of manufacture and installation, 1/32-in. crack considered to represent average practice.

[j] Made of heavy sections. Ventilators swing in or out and stay set at any degree of opening. 1/64-in. crack is obtainable in the best practice of manufacture and installation, 1/32-in. crack considered to represent average practice.

[k] With reasonable care in installation, leakage at contacts where windows are attached to steel framework and at mullions is negligible. With 1/64-in. crack, representing poor installation, leakage at contact with steel framework is about one-third, and at mullions about one-sixth of that given for industrial pivoted windows in the table.

generally decreases its leakage, but in some cases may push the meeting rail members apart and increase the leakage. On windows with large clearances, locking will usually reduce the leakage.

Wood casement windows may be assumed to have the same unit leakage as for the average double-hung wood window when properly fitted. Locking, a normal operation in the closing of this type of window, maintains the crack at a low value.

For metal pivoted sash, the length of crack is the total perimeter of the movable or ventilating sections. Frame leakage on steel windows may be neglected when they are properly grouted with cement mortar into brick work or concrete. When they are not properly sealed, the linear feet of sash section in contact with steel work at mullions should be figured at 25 per cent of the values for industrial pivoted windows as given in Table 2.

When storm sash are applied to well fitted windows, very little reduction in infiltration is secured, but the application of the sash does give an air space which reduces the heat transmission and helps prevent the frosting of the windows[3]. By applying storm sash to poorly fitted windows, a reduction in leakage of 50 per cent may be obtained, the effect so far as air leakage is concerned being roughly equivalent to that obtained by the installation of weatherstrips.

Door Leakage

Doors vary greatly in fit because of their large size and tendency to warp. For a well fitted door, the leakage values for a poorly fitted double-hung wood window may be used. If poorly fitted, twice this figure should be used. If weatherstripped, the values may be reduced one-half. A single door which is frequently opened, such as might be found in a store, should have a value applied which is three times that for a well fitted door. This extra allowance is for opening and closing losses and is kept from being greater by the fact that doors are not used as much in the coldest and windiest weather.

The infiltration rate through swinging and revolving doors is generally a matter of judgment by the engineer making cooling load determinations and in the absence of adequate research data the values given in Table 3 represent current engineering practice[4]. These values are based on the average number of persons in a room at a specified time, which may also

TABLE 3. INFILTRATION THROUGH OUTSIDE DOORS FOR COOLING LOADS[a]

Expressed in Cubic Feet per Minute per Person Entering Room

APPLICATION	PAIR 36 IN. SWINGING DOORS, SINGLE ENTRANCE[b]	APPLICATION	PAIR 36 IN. SWINGING DOORS, SINGLE ENTRANCE[b]
Bank	7.5	Hospital Room	3.5
Barber Shop	4.5	Lunch Room	5.0
Broker's Office	7.0	Men's Shop	3.5
Candy and Soda	6.0	Office	3.0
Department Store	8.0	Office Building	2.0
Dress Shop	2.5	Public Building	2.5
Drug Store	7.0	Restaurant	2.5
Furrier	2.5	Shoe Store	3.5

[a]For doors located in only one wall or where doors in other walls are of revolving type.

[b]Vestibules with double pair swinging doors, infiltration may be assumed 75 per cent of swinging door values.

Infiltration for 72 in. revolving doors may be assumed 60 per cent of swinging door values.

be the same occupancy assumed for determining the outside ventilation requirements outlined in Chapters 12 and 15.

Air Change Method

The amount of air leakage is sometimes roughly estimated by assuming a certain number of air changes per hour for each room, the number of changes assumed being dependent upon the type, use and location of the room, as indicated in Table 4. This method may be used to advantage as a check on the calculations made in the more exact manner. On the other hand, where it is not possible to determine or pre-determine with accuracy the width of crack or clearance of windows, or where other sources of air leakage cannot readily be evaluated, as is often the case, the use of the air change method may be justified.

The values in Table 4 may be used with reasonable accuracy for residences and are the requirements for each room. The total infiltration allowance for the entire building should be one-half the sum of the infiltration allowances of the individual rooms, since whatever air enters on the windward side generally leaves the building on the leeward side and the infiltration requirements therefore do not exist simultaneously on all sides or in all rooms. An allowance of one air change per hour for all sources of air leakage for the entire volume may be considered average for a well constructed residence.

The air leakage for vestibules due to opening and closing of doors is sometimes based on the air change method, even though the air leakage estimates for other rooms are based on the crack method. Except for vestibules and reception halls, it is not advisable to attempt to apply the air change method to factories and industrial and commercial buildings because of wide variations in the type and percentage of fenestration which is the principal source of air leakage in such buildings.

INFILTRATION DUE TO TEMPERATURE DIFFERENCE

The air exchange due to temperature difference, inside to outside, is a chimney effect, causing air to enter through openings at lower levels and to leave at higher levels[5]. Although it is not appreciable in low buildings, this loss should be considered in tall, single story buildings with openings near the ground level and near the ceiling. Also in tall, multi-story buildings it may be a considerable item unless the sealing between various floors and rooms is quite perfect.

In tall buildings, temperature difference or chimney effect will produce a head that will add to the effect of the wind at lower levels and subtract from it at higher levels. On the other hand, the wind velocity at lower

TABLE 4. AIR CHANGES TAKING PLACE UNDER AVERAGE CONDITIONS EXCLUSIVE OF AIR PROVIDED FOR VENTILATION[a]

KIND OF ROOM OR BUILDING	NUMBER OF AIR CHANGES TAKING PLACE PER HOUR	KIND OF ROOM OR BUILDING	NUMBER OF AIR CHANGES TAKING PLACE PER HOUR
Rooms, 1 side exposed	1	Rooms with no windows or outside doors	½ to ¾
Rooms, 2 sides exposed	1½	Entrance Halls	2 to 3
Rooms, 3 sides exposed	2	Reception Halls	2
Rooms, 4 sides exposed	2	Bath Rooms	2
		Stores	1 to 3

[a]For rooms with weatherstripped windows or storm sash, use ½ these values, where applicable.

levels may be somewhat abated by surrounding obstructions. Furthermore, the chimney effect is reduced in multi-story buildings by the partial isolation of floors, thereby preventing free upward movement, so that wind and temperature difference may seldom cooperate to the fullest extent. Making the rough assumption that the *neutral zone*[6] is located at mid-height of a building, and that the temperature difference is 70 F, Equations 1 and 2 may be used to determine an equivalent wind velocity to be used in connection with Tables 1 and 2 that will allow for both wind velocity and temperature difference:

$$V_e = \sqrt{V^2 - 1.75\,a} \quad (1)$$

$$V_e = \sqrt{V^2 + 1.75\,b} \quad (2)$$

where

V_e = equivalent wind velocity to be used in conjunction with Tables 1 and 2.
V = wind velocity upon which infiltration would be determined if temperature difference were disregarded.
a = distance of windows under consideration from mid-height of building if *above* mid-height, feet.
b = distance if *below* mid-height, feet.

The coefficient 1.75 allows for about one-half the temperature difference head.

For buildings of unusual height, Equation 1 would indicate negative infiltration at the highest stories, which condition may, at times, actually exist.

Sealing of Vertical Openings

In tall, multi-story buildings, every effort should be made to seal off vertical openings such as stair-wells and elevator shafts from the remainder of the building. Stair-wells should be equipped with self-closing doors, and, in exceptionally high buildings, should be closed off into sections of not over 10 floors each. Plaster cracks should be filled. Elevator enclosures should be tight and solid doors should be used.

If the sealing of the vertical openings is made effective, no allowance need be made for the chimney effect. Instead, the greater wind movement at the greater heights makes it advisable to install additional heating surface on the upper floors above the level of neighboring buildings, this additional surface being increased as the height is increased. One arbitrary rule is to increase the heating surface on floors above neighboring buildings by an amount ranging from 5 per cent to 20 per cent. This extra heating surface is required only on the windward side and on windy days, and hence automatic temperature control is especially desirable with such installations.

In stair-wells that are open through many floor levels although closed off from the remainder of each floor by doors and partitions, the stratification of air makes it advisable to increase the amount of heating surface at the lower levels and to decrease the amount at higher levels. One rule is to calculate the heating surface of the entire stair-well in the usual way and to place 50 per cent of this in the bottom third, the normal amount in the middle third and the balance in the top third.

Infiltration and Air for Combustion

Infiltration in residences normally supplies the air required for combustion by fuel burning appliances, but in some residences weather-

stripping, sealing and caulking may reduce infiltration to the point that special openings must be provided to supply adequate air to the heating appliances.

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Chapter 9

NATURAL VENTILATION

Wind Forces, Temperature Difference Forces, Heat Removal, Openings, Windows, Doors, Skylights, Roof Ventilators, Stacks, Principles of Control, General Rules, Dairy Barn Ventilation, Garage Ventilation

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VENTILATION by natural forces finds application in industrial plants, public buildings, schools, dwellings, garages, and in farm buildings.

The natural forces available for moving air into, through, and out of buildings are: (*a*) wind forces, and (*b*) the difference in temperature between the air inside and outside a building. The air movement may be caused by either of these forces acting alone or by a combination of the two, depending upon atmospheric conditions, building design and location. The ventilating results obtained will vary, from time to time, due to variation in the velocity and direction of the wind and the temperature difference. The arrangement, location, and control of the ventilating openings should be such that the two forces act cooperatively rather than in opposition.

WIND FORCES

In considering the use of natural wind forces for producing ventilation, account must be taken of: (1) average wind velocity, (2) prevailing wind direction, (3) seasonal and daily variations in velocity and direction, and (4) local wind interference by nearby buildings, hills or other obstructions of similar nature.

Values are given in Table 2, Chapter 15 for the average wind velocities for the months June to September in various localities throughout the United States, while Table 1, Chapter 14, lists similar values for the winter. In almost all localities the summer wind velocities are lower than those in the winter, and in about two-thirds of the localities the prevailing direction is different during the summer and winter. While the tables give no average velocities below 5 mph, there will be times when the velocity is lower, even in localities where the seasonal average is considerably above 5 mph. There are relatively few places where the velocity falls below one-half of the average for many hours per month. Consequently, if the natural ventilating system is designed for wind velocities of one-half of the average seasonal velocity, it should prove satisfactory in almost every case.

Equation 1 may be used for calculating the quantity of air forced through ventilation openings by the wind, or for determining the proper size of such openings to produce given results:

$$Q = EAV \qquad (1)$$

where

Q = air flow, cubic feet per minute.

A = free area of inlet openings, square feet.

V = wind velocity, feet per minute, = miles per hour × 88.

E = effectiveness of openings. (E should be taken at 0.50 to 0.60 for perpendicular winds and 0.25 to 0.35 for diagonal winds[1].)

The accuracy of the results obtained by the use of Equation 1 depends upon the placing of the openings, as the formula assumes that ventilating

openings have a flow coefficient slightly greater than that of a square-edged orifice. If the openings are not advantageously placed with respect to the wind, the flow per unit area of the openings will be less and, if unusually well placed, the flow will be slightly more than that given by the formula. Inlets should be placed to face directly into the prevailing wind, while outlets should be placed in one of the five places listed:

1. On the side of the building directly opposite the direction of the prevailing wind.
2. On the roof in the low pressure area caused by the jump of the wind (see Fig. 1).

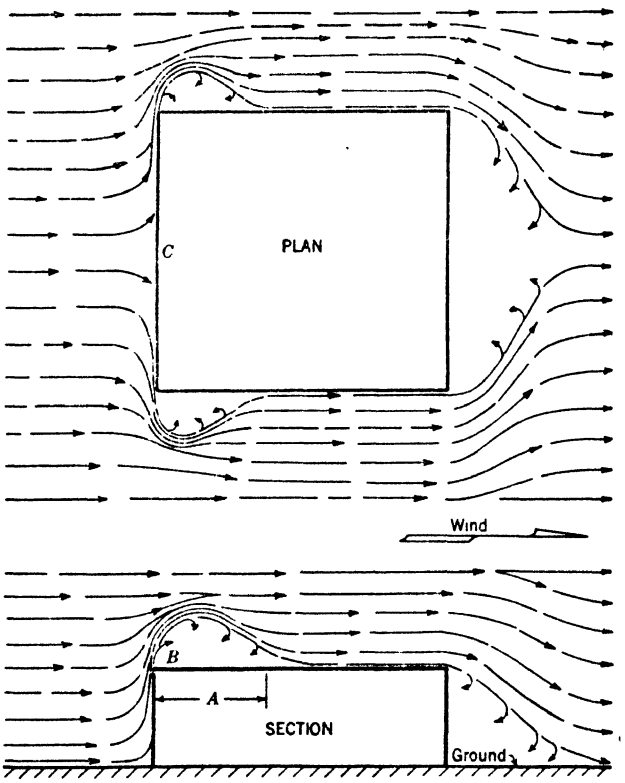

FIG. 1. THE JUMP OF WIND FROM WINDWARD FACE OF BUILDING. (*A*—LENGTH OF SUCTION AREA; *B*—POINT OF MAXIMUM INTENSITY OF SUCTION; *C*—POINT OF MAXIMUM PRESSURE)

3. On the sides adjacent to the windward face where low pressure areas occur.
4. In a monitor on the side opposite from the wind.
5. In roof ventilators or stacks.

TEMPERATURE DIFFERENCE FORCES[2]

The stack effect produced within a building when the outdoor temperature is lower than the indoor temperature is due to the difference in weight of the warm column of air within the building and cooler air outside. The flow due to stack effect is proportional to the square root of the draft head, or approximately:

$$Q = 9.4\, A \sqrt{h\,(t - t_o)} \qquad (2)$$

where

Q = air flow, cubic feet per minute.
A = free area of inlets or outlets (assumed equal), square feet.
h = height from inlets to outlets, feet.
t = *average* temperature of indoor air in height h, Fahrenheit degrees.
t_o = temperature of outdoor air, Fahrenheit degrees.
9.4 = constant of proportionality, including a value of 65 per cent for effectiveness of openings. This should be reduced to 50 per cent (constant = 7.2) if conditions are not favorable.

HEAT REMOVAL

In problems of heat removal, knowing the amount of heat to be removed and having selected a desirable temperature difference, the amount

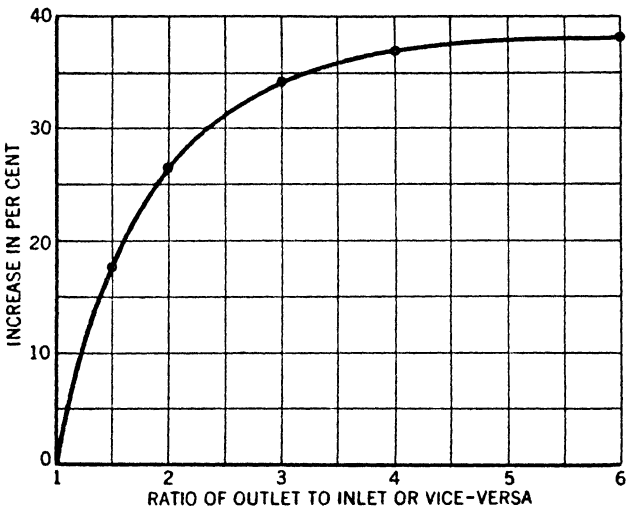

FIG. 2. INCREASE IN FLOW CAUSED BY EXCESS OF ONE OPENING OVER ANOTHER

of air to be passed through the building per minute to maintain this temperature difference can be determined by means of Equation 3.

$$H = 0.0175\ Q\ (t - t_o) \qquad (3)$$

where

H = heat removed, Btu per minute.
Q = air flow, cubic feet per minute.
$t - t_o$ = inside-outside temperature difference, Fahrenheit degrees.

EFFECT OF UNEQUAL OPENINGS

The largest flow per unit area of openings is obtained when inlets and outlets are equal, and the equations given previously are based on this condition. Increasing outlets over inlets, or vice-versa, will increase the air flow, but not in proportion to the added area. When solving problems having an unequal distribution of openings, use the smaller area, either inlet or outlet, in the equations and add the increase as determined from Fig. 2.

COMBINED FORCES OF WIND AND TEMPERATURE

Equations for determining the air flow due to temperature difference and wind have already been given. It must be remembered that when

both forces are acting together, even without interference, the resulting air flow is not equal to the sum of the two estimated quantities. The flow through any opening is proportional to the square root of the sum of the heads acting on that opening.

When the two heads are about equal in value and the ventilating openings are operated so as to coordinate them, the total air flow through the building is about 10 per cent greater than that produced by either head acting independently under conditions ideal to it. This percentage decreases rapidly as one head increases over the other and the larger will predominate.

The wind velocity and direction, the outdoor temperature, or the indoor distribution, cannot be predicted with certainty, and refinement in calculations is not justified; consequently, a simplified method can be

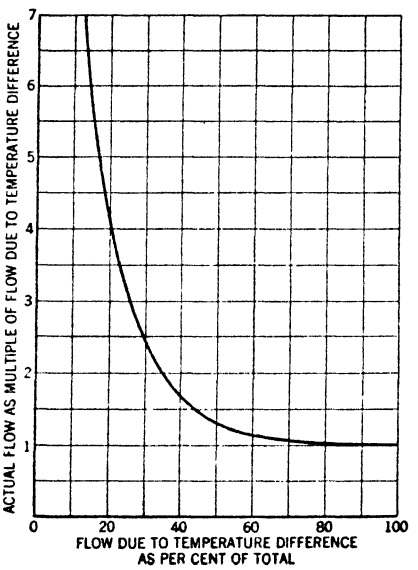

FIG. 3. DETERMINATION OF FLOW CAUSED BY COMBINED FORCES OF WIND AND TEMPERATURE DIFFERENCE

used. This may be done by using the equations and calculating the flows produced by each force separately under conditions of openings best suited for coordination of the forces. Then, by determining, as a percentage, the ratio of the flow produced by temperature difference to the sum of the two flows, the actual flow due to the combined forces can be approximated from Fig. 3.

Example 1. Assume a drop forge shop, 200 ft long, 100 ft wide, and 30 ft high. The cubical content is 600,000 cu ft, and the height of the air outlet over that of the inlet is 30 ft. Oil fuel of 18,000 Btu per pound is used in this shop at the rate of 15 gal per hour (7.75 lb per gal). Desired summer temperature difference is 10 deg and the prevailing wind is 8 mph perpendicular to the long dimension. What is the necessary area for the inlets and outlets, and what is the rate of air flow through the building?

Solution for Temperature Difference Only. The heat $H = \frac{15 \times 7.75 \times 18{,}000}{60} =$ 34,875 Btu per minute.

By Equation 3, the air flow required to remove this heat with an average temperature difference of 10 deg is:

$$Q = \frac{H}{0.0175\ (t - t_o)} = \frac{34{,}875}{0.0175 \times 10} = 199{,}286 \text{ cfm.}$$

This is equal to about 20 air changes per hour. From Equation 2 the inlet (or outlet) opening area should be:

$$A = \frac{Q}{9.4\sqrt{h\ (t - t_o)}} = \frac{199{,}286}{9.4\sqrt{30 \times 10}} = 1224 \text{ sq ft.}$$

The flow per square foot of inlet or outlet would be 199,286 ÷ 1224 = 163 cfm with all windows open.

Solution for Wind Only. With 1,224 sq ft of inlet openings distributed around the sidewalls, there will be about 410 sq ft in each long side and 202 sq ft in each end. The outlet area will be equally distributed on the two sides of the monitor, or 612 sq ft on each side. With the wind perpendicular to the long side, there will be 410 sq ft of opening in its path for inflow and 612 in the lee side of the monitor for outflow with the windward side closed. The air flow, as calculated by Equation 1, will be:

$$Q = 0.60 \times 410 \times 704 = 173{,}200 \text{ cfm.}$$

This gives 17.3 air changes per hour, which should be more than ample when there is no heat to be removed.

Solution for Combined Heads. Since the windward side of the monitor is closed when the wind is blowing, the flow due to temperature difference must be calculated for this condition, using Fig. 2. This chart shows that when inlets are twice the size of the outlets, in this case 1,224 sq ft in the sidewalls and 612 sq ft in the monitor, the flow will be increased 26.5 per cent over that produced by equal openings. Using the smaller opening and the flow per square foot obtained previously, the calculated amount for this condition will be:

$$612 \times 163 \times 1.265 = 126{,}200 \text{ cfm.}$$

Adding the two computed flows:

Temperature Difference	= 126,200 =	42 per cent.
Wind	= 173,200 =	58 per cent.
Total	299,400 =	100 per cent.

From Fig. 3, it is determined that when the flow, due to temperature difference, is 42 per cent of the total, the actual flow, due to the combined forces, will be about 1.6 times that calculated for temperature difference alone, or 201,920 cfm.

The original flow, due to temperature difference alone, was 199,286 cfm with all openings in use. The effect of the wind is to increase this to 201,920 cfm even though half of the outlets are closed.

A factor of judgment is necessary in the location of the openings in a building, especially those in the roof, where heat, smoke and fumes are to be removed. Usually windward monitor openings should be closed, but if the wind is low enough for the temperature head to overcome it, all windows may be opened.

TYPES OF OPENINGS

Types of openings may be classified as: (1) windows, doors, monitor openings and skylights, (2) roof ventilators, (3) stacks connecting to registers, and (4) specially designed inlet or outlet openings.

Windows, Doors and Skylights

Windows have the advantage of transmitting light, as well as providing ventilating area when open. Their movable parts are arranged to open in various ways; they may open by sliding either vertically or horizontally, by tilting on horizontal pivots at or near the center, or by swinging on pivots at the top, bottom or side. Regardless of their design, the air flow per square foot of opening may be considered to be the same under the same conditions. The type of pivoting should receive consideration

from the standpoint of weather protection, and certain types may be advantageous in controlling the distribution of incoming air. Deflectors are sometimes used for the same purpose, and these devices should be considered a part of the ventilation system.

Roof Ventilators

The function of a roof ventilator is to provide a storm and weather proof air outlet. These are actuated by the same forces of wind and temperature head, which create flow through other types of openings. The capacity of a ventilator depends upon four things: (1) its location on the roof, (2) the resistance it and the duct work offer to air flow, (3) the height of draft, and (4) the efficiency of the ventilator in utilizing the kinetic energy of the wind for inducing flow by centrifugal or ejector action.

For maximum flow induction, a ventilator should be located on that part of the roof where it will receive the full wind without interference. If ventilators are installed within the suction region created by the wind passing over the building, or in a light court, or on a low building between two high buildings, their performance will be seriously influenced. Their normal ejector action, if any, may be completely lost.

The base of the ventilator should be of a taper-cone design to produce the effect of a bell-mouth nozzle whose coefficient of flow is considerably higher than that of a square-entrance orifice. If a grille is provided at the base, or if the base or structural members present obstructions, additional resistance is introduced, and the base opening should be increased in size accordingly.

Air inlet openings located at lower levels in the building should be at least equal to, and preferably larger than the combined throat areas of all roof ventilators. The air discharged by a roof ventilator depends on wind velocity and temperature difference, and, in general, its performance will be the same as any monitor opening located in the same place but, due to the four capacity factors already mentioned, no simple formula can be devised for expressing ventilator capacity.

Roof ventilators may be classified as stationary, pivoting or oscillating, and rotating. Generally, these have a round throat, but the continuous-ridge ventilator, or so-called heat valve, would fall in the stationary classification. When selecting roof ventilators, some attention should be given to ruggedness of construction, storm proofing features, dampers and damper operating mechanisms, possibility of noise, original cost, and maintenance.

Natural ventilation units may be used to supplement power-driven supply fans, and under favorable weather conditions it may be possible to stop the power-driven units. Units are not subject to code tests for ratings. Generally they must be selected from manufacturers' tables. It is, therefore, very important to consider the reliability of the ratings used.

Controls

Gravity ventilators may have dampers controlled by hand, thermostat, or wind velocity, in combination with a fan. The thermostat station may be located anywhere in the building, or it may be located within the ventilator itself. The purpose of wind velocity control is to obtain a definite volume of exhaust regardless of the natural forces, the fan motor being energized when the natural exhaust capacity falls below a certain minimum, and again shut off when the wind velocity rises to the point where this minimum volume can be supplied by natural forces.

Stacks

Stacks or vertical flues are really chimneys which function through the effects of the wind and temperature difference. Like the roof ventilator, the stack outlet should be located so that the wind may act upon it from any direction. With little or no wind, the chimney effect depends entirely on temperature difference to produce a removal of air from the rooms where the inlet openings are located.

GENERAL RULES

A few of the important requirements in addition to those already outlined are:

1. Inlet openings in the building should be well distributed, and should be located on the windward side near the bottom, while outlet openings are located on the leeward side near the top. Outside air will then be supplied to the zone to be ventilated.

2. Inlet openings should not be obstructed by buildings, trees, sign boards, etc. outside nor by partitions inside.

3. Greatest flow per square foot of total opening is obtained by using inlet and outlet openings of nearly equal areas.

4. In the design of window ventilated buildings, where the direction of the wind is quite constant and dependable, the orientation of the building together with amount and grouping of ventilation openings can be readily arranged to take full advantage of the force of the wind. Where the wind's direction is quite variable, the openings should be arranged in sidewalls and monitors so that, as far as possible, there will be approximately equal areas on all sides. Thus, no matter what the wind's direction, there will always be some openings directly exposed to the pressure force and others to a suction force, and effective movement through the building will be assured.

5. Direct short circuits between openings on two sides at a high level may clear the air at that level without producing any appreciable ventilation at the level of occupancy.

6. In order that temperature difference may produce a motive force, there must be vertical distance between openings. That is, if there are a number of openings available in a building, but all are at the same level, there will be no motive head produced by temperature difference, no matter how great that difference might be.

7. In order that the force of temperature difference may operate to maximum advantage, the vertical distance between inlet and outlet openings should be as great as possible. Openings in the vicinity of the neutral zone are less effective for ventilation.

8. In the use of monitors, windows on the windward side should usually be kept closed, since, if they are open, the inflow tendency of the wind counteracts the outflow tendency of temperature difference. Openings on the leeward side of the monitor result in cooperation of wind and temperature difference.

9. In an industrial building where furnaces that give off heat and fumes are to be installed, it is better to locate them in the end of the building exposed to the prevailing wind. The strong suction effect of the wind at the roof near the windward end will then cooperate with temperature difference, to provide for the most active and satisfactory removal of the heat and gas laden air.

10. In case it is impossible to locate furnaces in the windward end, that part of the building in which they are to be located should be built higher than the rest, so that the wind, in splashing therefrom, will create a suction. The additional height also increases the effect of temperature difference to cooperate with the wind.

11. The intensity of suction or the vacuum produced by the jump of the wind is greatest just back of the building face. The area of suction does not vary with the wind velocity, but the flow due to suction is directly proportional to wind velocity.

12. Openings much larger than the calculated areas are sometimes desirable, especially when changes in occupancy are possible, or to provide for extremely hot days. In the former case, free openings should be located at the level of occupancy for psychological reasons.

13. In single story industrial buildings, particularly those covering large areas, natural ventilation must be accomplished by taking air in and out of the roof openings. Openings in the pressure zones can be used for inflow and openings in the suction zone, or openings in zones of less pressure, can be used for outflow. The ventilation is accomplished by the manipulation of openings to get air flow through the zones to be ventilated.

DAIRY BARN VENTILATION[3]

A successful barn ventilating system is one which continuously supplies the proper amount of air required by the stock, with proper distribution and without drafts, and one which removes the excessive heat, moisture, and odors, and maintains the air at a proper temperature, relative humidity, and degree of cleanliness.

Barn temperatures below freezing and above 80 F affect milk production. Milk producing stock should be kept in a barn temperature between 45 and 50 F. Dry stock, at reduced feeding, may be kept in a barn 5 to 10 deg higher. Calf barns are generally kept at 60 F, while hospital and maternity barns usually have a temperature of 60 F or somewhat higher.

The heat produced by a cow of an average weight of 1000 lb may be taken as 3000 Btu per hour. The average rate of moisture production by a cow giving 20 lb of milk per day is 15 lb of water per day, or 4375 grains per hour. To set a standard of permissible relative humidity for cow barns is difficult. For 45 F an average relative humidity of 80 per cent is satisfactory, with 85 per cent as a limit.

Where the barn volume and construction permit adequate heating by the stabled animals, the air supply need not be heated. The air should be supplied through or near the ceiling. It is better to have the exhaust openings near the floor as larger volumes of warm air are then held in the barn and there is better temperature control with less likelihood of sudden change in barn temperature.

If a cow weighs 1000 lb and produces 3000 Btu of heat per hour, and if a barn for the cow has 600 cu ft of air space with 130 sq ft of building exposure, one cow will require 2600 to 3550 cu ft per hour of ventilation, depending on the temperature zone in which the barn is located. The permissible heat losses through the structure, based on one cow and depending on the temperature zone, vary between 0.043 and 0.066 Btu per (hour) (cubic foot of barn space), and 0.197 to 0.305 Btu per (hour) (square foot of barn exposure).

GARAGE VENTILATION

On account of the hazards resulting from carbon monoxide and other physiologically harmful or combustible gases or vapors in garages, the importance of proper ventilation of these buildings cannot be overemphasized. During the warm months of the year, garages are usually ventilated adequately because the doors and windows are kept open. As cold weather sets in, more and more of the ventilation openings are closed and consequently on extremely cold days the carbon monoxide concentration runs high.

Many garages can be satisfactorily ventilated by natural means, particularly during the mild weather when doors and windows can be kept open. However, the A.S.H.V.E. Code of Minimum Requirements for Heating and Ventilating Garages, adopted in 1935, states that natural ventilation may be employed for the ventilation of storage sections where it is practical to maintain open windows or other openings at all times. The code specifies that such openings shall be distributed as uniformly as possible in at least two outside walls, and that the total area of such openings shall be equivalent to at least 5 per cent of the floor area. The code further states that where it is impracticable to operate such a system of natural ventilation, a mechanical system shall be used which shall

provide for either the supply of 1 cu ft of air per minute from out-of-doors for each square foot of floor area, or for removing the same amount and discharging it to the outside as a means of flushing the garage[4].

Research

Research on garage ventilation, undertaken by the A.S.H.V.E. Committee on Research at Washington University, St. Louis, Mo., and at the University of Kansas, Lawrence, Kans., in cooperation with the A.S.H.V.E. Research Laboratory, and at the A.S.H.V.E. Research Laboratory, has resulted in authoritative papers on the subject.

Some of the conclusions from work at the Laboratory are listed in the following statements:

1. Upward ventilation results in a lower concentration of carbon monoxide at the breathing line and a lower temperature above the breathing line than does downward ventilation, for the same rate of carbon monoxide production, air change and the same temperature at the 30-in. level.

2. A lower rate of air change and a smaller heating load are required with upward than with downward ventilation.

3. In the average case upward ventilation results in a lower concentration of carbon monoxide in the occupied portion of a garage than that obtained with mixing of the exhaust gases and the air supplied. However, the variations in concentration from point to point, together with the possible failure of the advantages of upward ventilation to accrue, suggest the basing of garage ventilation on complete mixing and an air change sufficient to dilute the exhaust gases to the allowable concentration of carbon monoxide.

4. The rate of carbon monoxide production by an idling car is shown to vary from 25 to 50 cu ft per hour, with an average rate of 35 cu ft per hour.

5. An air change of 350,000 cu ft per hour per idling car is required to keep the carbon monoxide concentration down to one part in 10,000 parts of air.

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Chapter 10

AIR CONTAMINANTS

Classification of Air Contaminants; Sizes of Airborne Particles; Air Pollution by Smoke, Ash and Cinders; Smoke Abatement; Odor Nuisance; Maximum Allowable Concentrations of Industrial Air Contaminants; Flammable Gases and Vapors; Combustible Dusts; Atmospheric Pollen; Airborne Bacteria

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THE normal constituents of the earth's atmosphere are oxygen, nitrogen, carbon dioxide, water vapor, argon, small or negligible amounts of other inert gases, hydrogen, variable traces of ozone, and small quantities of microscopic and submicroscopic solid matter, sometimes called *permanent atmospheric impurities*. From the viewpoint of the air conditioning engineer, all other airborne substances may be termed *contaminants*. This term is applied preferably, however, to undesirable or chance impurities, since the occasion may arise for adding to the air controlled amounts of substances such as: solid or gaseous diluents for the prevention of explosions; germicidal mists or aerosols for bacteria control; masking substances for odor control; or a substitute for one of the normal gases, as, for example, when helium is used to replace nitrogen in atmospheres for compressed air workers or divers.

The control of air quality is one of the functions of complete air conditioning, and some knowledge of the composition, concentration and properties of air contaminants under various circumstances is therefore essential.

Air contaminants arise from the normal processes of wear, erosion, windstorm, sea-spray evaporation, thermal disintegration, earthquake, volcanic eruption, combustion, manufacturing, transportation, agriculture, and the biochemical or biological processes of life. They are classified at various times as organic and inorganic, visible or invisible, microscopic or macroscopic, particulate or gaseous, toxic or harmless, beneficial or destructive. The following classification is based chiefly upon the origin or method of formation of air contaminants, using distinctions that are necessarily arbitrary in some cases.

CLASSIFICATION OF AIR CONTAMINANTS

Dusts, Fumes, and Smokes are solid particulate air contaminants.

Dusts are solid particles projected into the air by natural forces, such as wind, volcanic eruption or earthquake, and by mechanical or man-made processes, such as crushing, grinding, milling, drilling, demolition, shovelling, conveying, screening, bagging and sweeping. Some of these forces *produce* dust from larger masses, while the others simply *disperse* materials that are already in dust or pulverized form. Generally, particles are not called *dust* unless they are smaller than about 100 microns in size. Dusts may be of *mineral* type, such as rock, ore, metal, sand; *vegetable*, such as grain, flour, wood, cotton, pollen; or *animal*, such as wool, hair, silk, feathers, leather.

Fumes are solid particles commonly formed by the condensation of vapors from normally solid materials such as molten metals. Metallic fumes generally occur as the oxides in air because of the highly reactive nature of finely divided matter. Fumes may also be formed by sublimation, distillation, calcination, or chemical reaction, whenever such processes create airborne particles predominately below the 1 micron size. Fumes permitted to *age* tend to flocculate into clumps or aggregates of much larger size and this tendency may facilitate removal from air under controlled conditions.

Smokes are the extremely small solid particles produced by incomplete combustion of organic substances such as tobacco, wood, coal, oil, tar and other carbonaceous

materials. The term *smoke* is commonly applied to the mixture of solid, liquid and gaseous products of combustion, although the technical literature prefers to distinguish between such components as soot or carbon particles, fly-ash, cinders, tarry matter, unburned gases, and gaseous combustion products. The finest particulate constituents are characteristically much less than 1 micron in size, often in the range of 0.1 to 0.3 micron.

Mists and Fogs are liquid particulate air contaminants.

Mists are very small airborne droplets of materials that are ordinarily liquid at normal temperatures and pressures. They may be formed by atomizing, spraying, splashing, mixing, violent chemical reaction, electrolytic evolution of gas from a liquid, or escape of a dissolved gas upon release of pressure. The very small droplets expelled or atomized into the air by sneezing constitute mists containing microorganisms that become air contaminants.

Fogs are limited by some classifications to airborne droplets formed by condensation from the vapor state. This arbitrary distinction between mist and fog is of minor importance, as both terms are used to indicate the particulate state of airborne liquids (occasionally termed *aerosols*). *Fog nozzles* are so named because of their ability to produce extra fine droplets as compared to the mist from ordinary spray devices. The highly volatile nature of some liquids quickly reduces their airborne droplets from the mist to the fog range, and eventually to the vapor phase until the air becomes saturated with that liquid. Many droplets in fogs or clouds are microscopic and submicroscopic in size, and may be conceived as the transition state between the larger mists and the vapors.

Vapors and Gases are non-particulate air contaminants.

Vapors are the gaseous phase of substances that are either liquid or solid in their commonly known state, examples being gasoline, kerosene, benzene, carbon tetrachloride, mercury, iodine, camphor. Vapors may be changed to the solid or liquid form by increasing the pressure, decreasing the temperature or applying both processes simultaneously. They are removed from the air by condensation with less difficulty than are the gases.

Gases are normally formless fluids which tend to occupy a space or enclosure completely and uniformly at ordinary temperatures and pressures. The following substances qualify as gases: oxygen, nitrogen, carbon dioxide, carbon monoxide, hydrogen, ammonia, sulfur dioxide. Gases, likewise, may be solidified or liquefied by the proper control of temperature and pressure.

The preceding classification is not suitable for the airborne living organisms, which range in size from the submicroscopic viruses to the largest pollen grains, not considering the smallest insect life. Bacteria range from about 0.2 to 5 microns in size, fungus spores from 1 to 10 microns, and pollen from 5 to 150 microns.

SIZES OF AIRBORNE PARTICLES

Fig. 1 is a graphic tabulation of the properties of airborne solids and liquids arranged according to size on the micron scale. There are 25,400 microns in 1 inch.

Particles larger than 10 microns are unlikely to remain suspended in air currents of moderate strength, but settle out by gravity at speeds dependent upon the shape, the size and specific gravity of the particle, the wind velocity, the orientation of the collecting surface, and the topography. These larger particles are of major interest to the engineer in the solution of nuisance problems, but it is usually the smaller particles, or those below 10 microns, that remain in the air long enough to be of hygienic as well as economic significance.

The great bulk of industrial dust particles is of the order of 1 micron in size. Tremendous numbers are also present in the sub-microscopic range below 0.5 micron, but those below 0.1 micron are not believed at

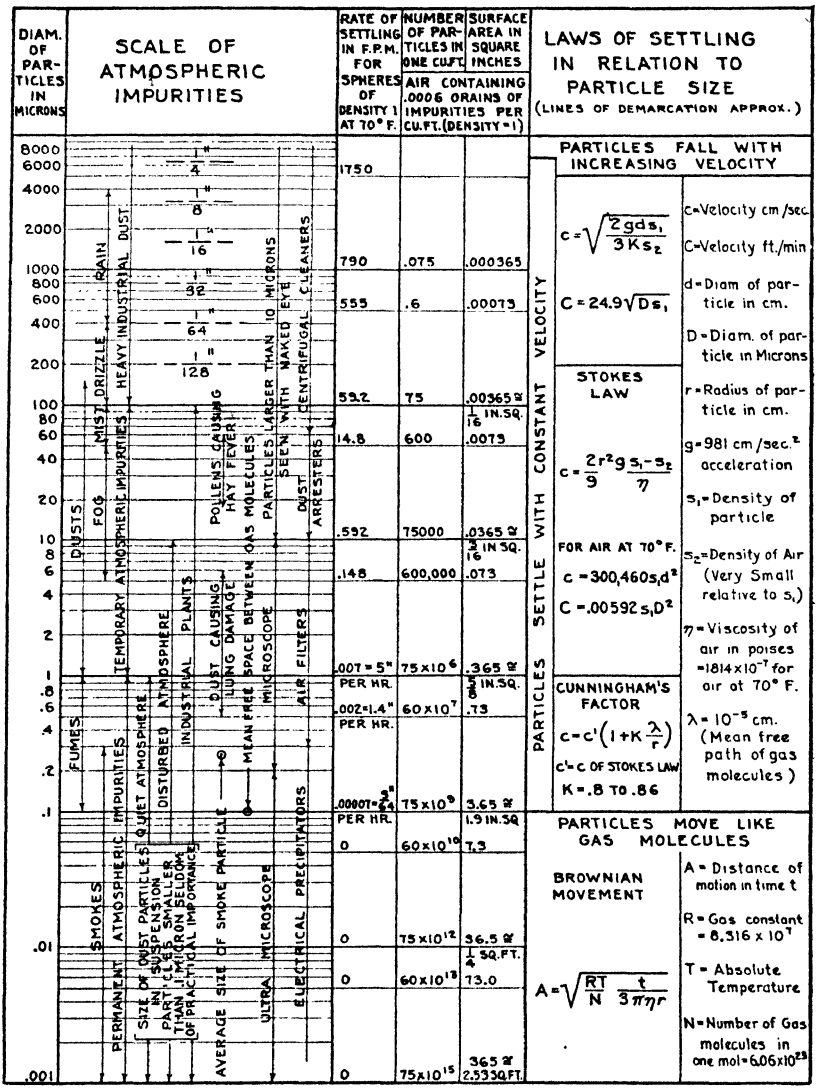

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FIG. 1. SIZES AND CHARACTERISTICS OF AIRBORNE PARTICULATE MATTER

present to be of any practical importance, possibly due to their exceedingly small mass in comparison with the balance of airborne matter. In fact, particles this small may become the *permanent* atmospheric impurities that have little if any opportunity of settling because of the continual motion imparted to them by air currents and the molecular activity of their supporting gases (Brownian Movement).

The survey [1] of atmospheric pollution in 14 American cities conducted from 1931 to 1933 indicated the average size of outdoor dust particle to be 0.5 micron, as collected by the Owens jet dust counter and measured under the microscope. The inability of the *light field* microscope to

reveal particles in the 0.1 micron vicinity may have influenced the determination of average particle size.

The lower limit of particle size visible to the naked eye cannot be stated definitely. It depends not only upon the individual eye, but also upon the shape and color of the particle, the intensity and quality of the light, and the nature of the background or the opportunity for contrast. Under ideal conditions a particle of 10-micron size might be recognized, while under less favorable conditions it may be impossible to distinguish a particle smaller than 50 microns. The lower limit of visibility probably ranges from 10 to 50 microns.

Dusts, powders and granular materials are frequently classified by reference to the size of screens used for separation. Particles above 40 microns are said to be the *screen sizes* and those below, the *sub-screen* or microscopic sizes. The approximate or theoretical sizes of particles corresponding to the mesh scale of the U. S. Standard Sieve Series are given in Table 1.

Microscopic examination of screened dust indicates that the average diameter of a sample of irregular particles may be substantially larger than the openings of the screen through which it has passed, if the particle

TABLE 1. RELATION OF SCREEN MESH TO PARTICLE SIZE

U. S. Standard Sieve Mesh.....	400	325	200	140	100	60	35	18
Nominal Sieve Opening in Microns.....	37	44	74	105	149	250	500	1000

shapes deviate considerably from the spherical form [2]. The smallest dimension of many such particles will correspond with the maximum permissible distance between the wires of commercial screens made to *ASTM* Standard specifications. Screening does not give sharp separation into size groups, and accordingly such a classification is statistical rather than absolute.

AIR POLLUTION BY SMOKE, ASH AND CINDERS

The total airborne solids settling in urban areas are usually reported as *soot fall* in tons per (square mile) (month). Such data published for the cities in this country range from 20 to 200 tons per (square mile) (month). To the air conditioning engineer this information may indicate the effectiveness of smoke abatement or fuel combustion control methods in his locality, but it does not provide a suitable index of the suspended dust that air cleaners in a ventilating system are expected to capture [3, 4, 5]. Gravimetric or weight data of the type given in Table 2 are preferable. In some cases airborne particle counts may be necessary, as for pollen, bacteria, spores, and insoluble dusts causing illness or lung disease.

Dust concentrations by weight cannot be converted readily to concentrations by particle count because of the variability of particle size, shape and specific gravity, and the inherent characteristics of dust counting and weighing procedures. One milligram of dust per cubic

meter of air may represent dust counts from 1 million to 100 million particles per cubic foot of air (lightfield microscope technic) according to the size distribution of the airborne dust sample. Information of this type for a specified application is best obtained by simultaneous sampling for both counting and weighing and noting carefully at the time all factors that might affect the reproducibility of the count-weight ratio.

Smoke Abatement

Successful abatement of atmospheric pollution caused by smoke requires the combined efforts of the combustion engineer, industrial executive, public health officer, city planning commission and the community at large. Electrification of industry and railroads, increases in the use of domestic oil and gas furnaces, and segregation of industrial districts is gradually providing effective aid in the solution of this problem. In the large cities where nuisance from smoke, fly-ash and cinders is more serious, limited areas obtain some relief by the use of district heating.

Time, temperature and turbulence are fundamental requirements for smokeless combustion. Increase of any one of these factors will reduce

TABLE 2. DUST CONCENTRATION RANGES

LOCATION	GRAINS PER 1000 CU FT[a]	MILLIGRAMS PER CUBIC METER
Rural and suburban districts	0.02–0.2	0.05– 0.5
Metropolitan district	0.04–0.4	0.1– 1.0
Industrial districts	0.1 –2.0	0.2 – 5.0
Ordinary factories or workrooms	0.2 –4.0	0.5 –10
Excessively dusty factories or mines	4–400	10–1000
Minimum explosive concentrations	4000–200,000	10,000–500,000

[a]1 grain per 1000 cu ft = 2.3 milligrams per cubic meter.
1 oz per cubic foot = 1 gram per liter = 1000 grams per cubic meter.

the quantity of smoke discharged, although excessive turbulence in furnances may increase the output of ash and cinders. Special care must be taken in hand firing the bituminous coals. (See Chapters 16, 17 and 18 for further discussion on fuel burning technic).

Legislative measures at the present time are largely concerned with reduction of the visible smoke discharged from chimneys of boiler plants. Practically all ordinances limit the number of minutes in any one hour that smoke of a specified density may be discharged, as measured by comparison with a Ringelmann Chart (Chapter 11, Instruments and Measurements). Ordinances generally do not make specific provision for control of the corrosive and irritant gases, such as oxides of sulphur and nitrogen discharged with the gases of combustion. Where high sulfur coals are burned, sulfur gases present a serious hazard to property, health and vegetation.

In foggy weather the accumulation of these gases in the lower strata of the atmosphere may be such as to cause irritation of the eyes, nose and respiratory passages, and possibly even more dangerous consequences. The Meuse Valley (Belgium) fog disaster (1930) has become a classic example in the history of gaseous air pollution. It is believed that sulfur dioxide and other toxic gases released in a rare combination of atmospheric

calm and dense fog were responsible for about 60 human deaths, injuries to several hundred persons, and also the death of many domestic and wild animals.

Absorption of Solar Radiation

The absorption of solar ultraviolet light by smoke and soot, is recognized as a health problem in many industrial cities. Measurements of solar radiation in Baltimore [6] by actinic methods demonstrated that ultraviolet light intensity in the country was 50 per cent greater than in the city. In New York City [7] a loss as great as 50 per cent in visible light was found by photo-electric cell.

ODOR NUISANCE

A problem companionate with smoke abatement is the control of odor nuisance in the neighborhood of industrial plants discharging noxious or offensive air contaminants. Community planning and zoning will avoid much of the difficulty in the future, but meanwhile many industrial cities must resort to corrective measures by requiring the installation of air cleaning devices, the alteration of manufacturing processes, or by legal termination of the offensive operation in residential or commercial districts.

The control of outdoor odor nuisance is especially troublesome because of the extremely minute quantities of contaminant that are capable of offending through a wide area. New industrial chemicals with strange or unfamiliar odors tend to receive much more attention from the neighborhood than the customary odors generated by well known processes and raw materials. Methods of odor control currently in use include charcoal adsorption, scrubbing towers and air washers, chlorination, condensation, masking, passage of the odorous air through combustion chambers, and best of all, substitution of less offensive materials whenever possible [8, 9, 10, 11].

The control of air quality within buildings ventilated for human occupancy is discussed in Chapter 12. Tobacco smoke odors, cooking odors and body odors are air contaminants of the nuisance type which now command a decisive position in the standards of air quality for indoor comfort. However, the engineer will find, at times, that odors originating *outside* buildings in industrial or business districts may determine the kind and capacity of equipment he must provide for a high quality air supply installation.

INDUSTRIAL AIR CONTAMINANTS

Many industrial processes are sources of contaminants. Their control is an important function of the ventilating or air conditioning engineer, because the atmosphere within buildings is the medium whereby such finely divided matter is dispersed and transported from the source to remote locations where it may cause property damage, nuisance, fire, explosion, disease and even death.

Tables 3, 4 and 5 give the maximum allowable concentrations for industrial air contaminants as currently accepted in most sections of the country. They apply to *exposures of 8 hours per day*, and refer to the quantities of contaminant permissible in the *workers' breathing zone.* Some of these figures may be altered as the result of continuous research, and some may differ from those in force in a few cities or states. The

TABLE 3. PHYSIOLOGICAL RESPONSE TO GASES AND VAPORS[a]
Concentrations in Parts of Substance per Million Parts of Air by Volume (ppm)

SUBSTANCE	RAPIDLY FATAL	DANGEROUS TO LIFE IN ½ TO 1 HR	MAXIMUM ALLOWABLE CONCENTRATION FOR DAILY EXPOSURES
Acrolein	2,000	100	0.5
Ammonia	5,000	2,500	100
Amyl acetate	.....	.....	200
Aniline	.....	200	5
Arsine	250	10	0.05
Benzene (benzol)	20,000	5,000	100[b]
Bromine	500	40	1
Butyl acetate	.....	10,000	200
Carbon dioxide	100,000	50,000	5,000
Carbon disulfide	2,000	1,000	20[b]
Carbon monoxide	4,000	1,000	100[b]
Carbon tetrachloride	50,000	.....	50
Chlorine	1,000	10	1
Dichlorobenzene	.....	.....	50
Dichloroethyl ether	.....	500	15
Ether (diethyl)	.....	35,000	400
Ethyl acetate	40,000	10,000	400
Ethyl alcohol	.....	.....	1,000
Ethylene dichloride	.....	4,000	100
Formaldehyde	.....	.....	10[b]
Gasoline	.....	.....	500
Hydrogen chloride	1,000	.....	10
Hydrogen cyanide	200	100	20
Hydrogen fluoride	.....	50	3
Hydrogen sulfide	600	200	20[b]
Methyl acetate	.....	.....	200
Methyl alcohol (Methanol)	.....	.....	200[b]
Methyl bromide	20,000	2,000	20
Methyl chloride	150,000	20,000	100
Methylene chloride	.....	.....	500
Monochlorobenzene	.....	.....	75
Nitrobenzene	.....	.....	1
Nitrogen oxides	300	100	25[b]
Phosgene	50	5	1
Phosphine	1,000	400	0.05
Styrene	.....	.....	400[b]
Sulfur dioxide	400	150	10
Tetrachloroethane	7,000	.....	5
Tetrachloroethylene	.....	.....	100
Toluene (toluol)	20,000	5,000	200
Trichloroethylene	.....	.....	200[b]
Turpentine	.....	.....	100
Xylene (xylol)	20,000	5,000	200[b]

[a]Adapted from: Manual of Industrial Hygiene, by W. M. Gafafer et al, U. S. Public Health Service (W. B. Saunders Co., 1943); Analytical Chemistry of Industrial Poisons, Hazards and Solvents, by M. B. Jacobs (Interscience Publishers, 1941); Noxious Gases, by Henderson and Haggard (Reinhold Publishing Co., N. Y., 1943). 1947 report of the Committee on Threshold Limits of the American Conference of Governmental Industrial Hygienists; and other authoritative sources.
[b]Adopted by the *American Standards Association* (American Standard Z-37).

prudent engineer will design equipment using these values as the *upper* limits of air contamination, and will incorporate a reasonable margin of safety in his estimates of ventilation capacity.

Information on the properties and effects, with respect to health, of

TABLE 4. MAXIMUM ALLOWABLE CONCENTRATIONS OF DUSTS, FUMES AND MISTS[a]

SUBSTANCE	MILLIGRAMS PER CUBIC METER, DAILY EXPOSURES[b]
Antimony	0.1
Arsenic; arsenic trioxide	0.15[c]
Cadmium, and compounds	0.1[c]
Chlorodiphenyls	1.0
Chromic acid mist and Chromates (as CrO_3)	0.1
Fluorides	2.5
Lead; lead carbonate; lead chloride; lead nitrate; lead oxides; lead sulfate	0.15[c]
Manganese, and compounds	6.0[c]
Mercury, and compounds	0.1
Pentachloronaphthalene	0.5
Selenium	0.1
Tellurium	0.1
Trichloronaphthalene	5.0
Trinitrotoluene	1.5
Zinc oxide fume	15.0

[a]Adapted from: Manual of Industrial Hygiene, by W. M. Gafaier, et al, U. S. Public Health Service (W. B. Saunders Company, 1943); and other authoritative sources.
[b]1 milligram per cubic meter = 0.44 grain per 1000 cu ft.
[c]Adopted by the *American Standards Association* (American Standard Z-37).

TABLE 5. MAXIMUM ALLOWABLE CONCENTRATIONS OF DUSTS[a]

SUBSTANCE	MILLION PARTICLES PER CUBIC FOOT OF AIR, DAILY EXPOSURES[b]
Aluminum oxide abrasive	15–100
Asbestos	5
Carborundum (silicon carbide)	15–100
Cement (Portland)	50–100
Coal (less than 5 per cent quartz)	50–100
Dusts containing less than 10 per cent *free* silica	10–100
Granite	10– 25
Gypsum (hydrated calcium sulfate)	50–100
Limestone (calcium carbonate)	50–100
Marble (calcium carbonate)	50–100
Mica	10–100
Nuisance dusts (non-toxic, non-silica)	50–100
Quartz (silicon dioxide)	5
Sand (silica, silicon dioxide)	5
Sandstone	5
Silica (*free* or uncombined silicon dioxide)	5
Silicates (combined silicon dioxide)	15–100
Slate	15–100
Talc	10– 50
Total (maximum concentration for mixed dusts)	50–100

[a]Adapted from: Study of Asbestosis in Asbestos Textile Industry, U. S. Public Health Service Bulletin No. 241, 1938; Industrial Dust, by Drinker and Hatch (McGraw Hill Book Co., 1936); Industrial Code Bulletin No. 35, New York State Department of Labor; recommendations of state and local industrial hygiene agencies compiled by the American Conference of Governmental Industrial Hygienists; and other authoritative sources.
[b]Includes only particles from 1 to 10 microns approximately, as determined by the light field microscope counting technic, using the 10× objective. Dark field counts (and the corresponding allowable concentrations) are anywhere from 2 to 100 times the light field counts for the same sample, according to the proportion of dust smaller than 1 micron (See Industrial Dust, Chapter VII, by Drinker and Hatch, McGraw Hill Book Co.).

specific industrial air contaminants has developed rapidly within the past decade into an extensive literature. Some of the more readily available publications are listed at the end of this chapter.

TABLE 6. APPROXIMATE LIMITS OF FLAMMABILITY OF SINGLE GASES AND VAPORS IN AIR AT ORDINARY TEMPERATURES AND PRESSURES[a]

GAS OR VAPOR	LOWER LIMIT PER CENT BY VOLUME	UPPER LIMIT PER CENT BY VOLUME	*Closed Cup* FLASH POINT F DEG[c]
Acetaldehyde	4.0	57	−17
Acetone	2.1	13.0	0
Acetylene[b]	2.5	80	.....
Allyl alcohol	2.4	.....	70
Ammonia	16.0	27.0	.....
Amyl alcohol	1.2	.....	91
Amyl chloride	1.4	.....	.....
Amylene	1.6	.....	.....
Benzene (benzol)	1.4	8.0	12
Benzyl chloride	1.1	.....	140
Butane	1.6	8.5	−76
Butyl acetate	1.7	15.0	72
Butyl alcohol	1.7	.....	84
Butylene	1.7	9.0	.....
Carbon disulfide	1.0	50	−22
Carbon monoxide	12.5	74	.....
Crotonaldehyde	2.1	15.5	55
Cyclohexane	1.3	8.4	1
Cyclopropane	2.4	10.3	.....
Decane	0.67	2.6	115
Dichloroethylene (1, 2)	9.7	12.8	43
Diethyl selenide	2.5	.....	.....
Dioxan	2.0	22.2	65
Ethane	3.1	15.0	.....
Ether (diethyl)	1.7	48.0	−20
Ethyl acetate	2.2	11.5	24
Ethyl alcohol	3.3	19.0	55
Ethyl bromide	6.7	11.3	.....
Ethyl cellosolve	2.6	15.7	104
Ethyl chloride	3.6	14.8	−58
Ethylene	3.0	34.0	.....
Ethylene dichloride	6.2	15.9	56
Ethyl formate	2.7	16.5	−4
Ethyl nitrite	3.0	.....	−31
Ethylene oxide	3.0	80	.....
Furfural (125 C)	2.1	.....	140
Gasoline	1.3	6.5	−50
Heptane	1.0	6.0	25
Hexane	1.2	6.9	−7
Hydrogen cyanide	5.6	40.0	0
Hydrogen	4.1	74	.....
Hydrogen sulfide	4.3	45.5	.....
Illuminating gas	5.3	31.0	.....
Iso-butyl alcohol	1.7	.....	82
Iso-pentane	1.3	.....	.....
Iso-propyl acetate	1.8	7.8	43
Iso-propyl alcohol	2.5	.....	53
Methane[b]	5.0	15.0	.....

[a]Adapted from: Limits of Inflammability of Gases and Vapors, by H. F. Coward and G. W. Jones (U. S. Bureau of Mines Bulletin No. 279, 1939); Properties of Flammable Liquids, Gases and Solids (Associated Factory Mutual Fire Ins. Cos., January, 1940); and National Fire Codes for Flammable Liquids, Gases, Chemicals and Explosives—1945 (*National Fire Protection Association*).

[b]Turbulent mixture.

[c]*Closed cup* refers to the equipment used in flash point determinations.

TABLE 6. APPROXIMATE LIMITS OF FLAMMABILITY OF SINGLE GASES AND VAPORS IN AIR AT ORDINARY TEMPERATURES AND PRESSURES[a] (Continued)

GAS OR VAPOR	LOWER LIMIT PER CENT BY VOLUME	UPPER LIMIT PER CENT BY VOLUME	*Closed Cup* FLASH POINT F DEG[c]
Methyl acetate	3.1	15.5	15
Methyl alcohol	6.0	36.5	54
Methyl bromide	13.5	14.5	.....
Methyl butyl ketone	1.2	8.0	.....
Methyl chloride	8.0	19.7	.....
Methyl cyclohexane	1.1	.....	25
Methyl ethyl ether	2.0	10.1	−35
Methyl ethyl ketone	1.8	11.5	30
Methyl formate	5.0	22.7	−2
Methyl propyl ketone	1.5	8.2	.....
Natural gas	4.8	13.5	.....
Naphtha (benzine)	1.1	6.0	20–45
Naphthalene	0.9	.....	174
Nonane	0.74	2.9	88
Octane	0.84	3.2	56
Paraldehyde	1.3	.....	.....
Pentane	1.4	8.0	.....
Propane	2.4	9.5	.....
Propyl acetate	1.8	8.0	58
Propyl alcohol	2.5	.....	59
Propylene	2.0	11.1	.....
Propylene dichloride	3.4	14.5	59
Propylene oxide	2.1	21.5	.....
Pyridine (70 C)	1.8	12.4	68
Toluene (toluol)	1.3	7.0	40
Turpentine	0.8	.....	95
Vinyl ether	1.7	27.0	.....
Vinyl chloride	4.0	22.0	.....
Water gas (variable)	6.0	70	.....
Xylene (xylol)	1.0	6.0	63

FLAMMABLE GASES AND VAPORS

Adequate ventilation is a primary requirement for eliminating or minimizing the hazard of fire or explosion due to gases and vapors. The need for good ventilation is not removed by the use of other precautions, such as the elimination of known ignition sources, segregation of hazardous operations, adoption of safe building construction, and installation of automatic alarms. Some safety engineers regard overventilation of an operation employing flammable liquids as a legitimate operating charge for the privilege or necessity of using a dangerous process. However, it is not possible to apply a reasonable safety factor to the ventilation estimate without consideration of the concentrations of gases or vapors that approach the danger point. Safety engineers prefer to limit the concentration to ¼ or ⅛ of the lower explosive limit, and this fact should be given full weight in determining the capacity and design of ventilating equipment. Rarely should consideration be given to *operation above the upper explosive limit* in the open areas of buildings or rooms—even though unoccupied—because the danger of temporary drop of gas concentration to a point within the explosive range is too great.

The ability of a flammable liquid to form explosive mixtures is determined largely by its vapor pressure, volatility, or rate of evaporation. *Flash point* is a convenient method of expressing this property in terms of the temperature scale. It may be defined as the temperature to which a combustible liquid must be heated to produce a flash of flame when a small flame is passed across the surface of the liquid. The higher the flash point, the more safely can the liquid be handled. Liquids with flash points under 70 F should be regarded as highly flammable.

The upper and lower limits of flammability of gases and vapors, and the flash points of the corresponding liquids are given in Table 6.

Methods for estimating the flammable limits of mixtures of gases or vapors must be applied with caution; the reader is referred to other publications for this information [12, 13].

Design of equipment for the control of combustible anesthetics is outlined in Chapter 13. Construction of equipment for handling air containing flammable substances, or operating in atmospheres so contaminated, is discussed in Chapter 46.

It is customary to report the concentrations of flammable gases or vapors in per cent by volume, or *volume per cent.* Comparison with concentrations on the *part per million* scale used in chemical, medical or industrial hygiene literature is readily made by the conversion: 1 per cent = 10,000 ppm (parts of contaminant per million parts of air, by volume, or in other words, cubic feet of contaminant per million cubic feet of air). It will be noted in Table 6 that nearly all of the substances listed have lower explosive limits above 1.0 per cent, while the *maximum allowable concentrations* for gases and vapors in Table 3 are below 1000 ppm or 0.1 per cent in most cases. Therefore, control of toxic or injurious vapors in workrooms to levels below their maximum allowable concentrations for health usually requires much more effective ventilation than for the prevention of a fire hazard.

COMBUSTIBLE DUSTS

A dust explosion is essentially a sudden pressure rise caused by the very rapid burning of airborne dust. The primary explosion often originates from a small amount of dust in suspension exposed to a source of ignition, and the pressure and vibration it creates may be sufficient to dislodge large accumulations of dust on horizontal ledges or surfaces of the building and equipment, thereby creating a secondary explosion of great force. Thus the air conditioning engineer is involved for two reasons: (1) to obtain a movement of dust-laden air into exhaust hoods or openings and through ventilating or pneumatic conveying ducts in a manner that will prevent accumulation of highly flammable dust at points where it could ignite inside the equipment; and (2) to so design *process ventilation* as to prevent the escape of dust which might settle on horizontal surfaces and become a potential source of disaster at some distance from the dusty operation. (See Chapter 46).

The intensity of a dust explosion depends upon: the chemical and thermal properties of the dust; the particle size and shape; the concentration in air; the proportion of inert dust in the air; the moisture content and composition of the air; the size and temperature of the ignition source; and the degree of dispersion of the dust cloud. Investigations on the explosibility of dusts require a determination of the maximum pressure developed during an explosion of a known air concentration, as well as

determination of the rate of pressure rise. Investigators frequently experience difficulty in obtaining dust suspensions of uniform dispersion, and this should be kept in mind when comparing results from several sources [14].

The minimum explosive concentrations of airborne dusts already tested range from 0.01 to 0.5 oz per cubic foot, or 10 to 500 grams per cubic meter of air. Maximum pressures generated have been reported as high as 500 psi, although they are more likely to be of the order of 50 psi. Investigations on the flammable characteristics of dusts are currently made at 0.1 and 0.5 oz per cubic foot [15-21].

ATMOSPHERIC POLLEN

The properties of pollen grains discharged by weeds, grasses and trees and responsible for hay fever are of special interest to engineers who design equipment for their removal from indoor air (see Allergic Disorders in Chapter 13, and Air Cleaning Devices, Chapter 33). Whole grains and fragments transported by the air range chiefly between 10 and 50 microns in size, but some have been measured as small as 5 microns and others over 100 microns in diameter. Ragweed pollen grains are fairly uniform in size within the range of 15 to 25 microns.

Pollen grains can be removed from the air more readily than the particles of dust prevalent in outdoor air and found near dusty industrial processes, since the latter predominate in the range of 0.1 to 10 microns in size.

Most grains are quite hygroscopic and therefore vary in weight with the humidity. Illustrations and data on individual pollen grains are available in the botanical literature [22, 23, 24]. The geographical distribution of plants known to produce hay fever is also recorded [25, 26].

The quantity of pollen grains in the air is generally estimated by exposing an adhesive-coated glass plate outdoors for 24 hr and then counting calibrated areas under the microscope. Methods are available for determining the number of grains in a measured volume of air [25, 27, 28] but their greater accuracy has not caused them to replace the more simple *gravity slide method* used for most pollen counts. Counting technics vary somewhat, but the daily pollen counts reported in local newspapers during the hay fever season usually represent the number of grains found on 1.8 sq cm of a 24-hr *gravity slide.*

Hay fever sufferers may notice the first symptoms when the pollen count is 10 to 25, and in some localities the maximum figures for the seasonal peak may approach 1000 for a 24-hr period, depending upon the sampling and reporting methods of the laboratory. Translation of gravity counts by special formulas to a volumetric basis, or the number of grains per cubic yard or per cubic foot of air, is still uncertain because of the complexity of the modifying factors. When such information is important, it is best obtained directly by a volumetric instrument. The number of pollen grains per cubic yard of air evidently varies from 2 to 20 times the number found on 1 sq cm of a 24-hr gravity slide, depending on grain diameter, shape, specific gravity, wind velocity, humidity and physical placement of the collecting plate [29, 30, 31].

AIRBORNE BACTERIA

Study of the occurrence and significance of micro-organisms in the atmospheres of the indoor world is currently absorbing the energies of a

substantial number of physicians, bacteriologists, aerobiologists, physicists, public health workers, engineers and hospital personnel. Some data are available on the types and quantities of bacteria found in a variety of occupied and unoccupied spaces, but it is not possible at present to use this information as a conclusive index of the potential health hazard of a given environment. The reported number of airborne organisms may vary from 1 to 1000 per cubic foot of air, influenced somewhat by the method of testing [32]. Many are attached to the dust particles which are also present in the air.

Where it seems advisable or desirable to control the bacterial content of rooms, public conveyances or buildings, highly effective methods are available (see Chapter 13), and their extended use may do much to assist the workers in this field in accumulating the necessary mass of evidence that will decide the practical value of air sterilization for the control of communicable disease. It is now well established that ultraviolet radiation is commercially feasible for the protection or preservation of pharmaceuticals, cosmetics, and food products.

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Chapter 11

INSTRUMENTS AND MEASUREMENTS

Temperature Measurement, Pressure Measurement, Measurement of Air Movement, Air Change Measurements, Measurement of Relative Humidity, Dust Determination, Heat Transfer Through Building Materials, Measurement of Heat Exchange for Comfort Conditions, Combustion Analysis, Smoke Density Measurements, Sound and Vibration Measurements

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THIS chapter presents a description of many test instruments used for heating, ventilating and air conditioning tests and presents a discussion of their use.

TEMPERATURE MEASUREMENT

Changes in the intensity of heat may be determined by several methods[1] such as measuring the change in volume of a liquid, the change in internal pressure of a confined gas, the current set up between dissimilar metals joined in a circuit, or the change in resistance of an electrical circuit.

Thermometers

The most common method used is the change in volume of a liquid such as mercury or alcohol enclosed in glass. Mercurial thermometers may be used for measuring temperatures from −40 F to approximately 1000 F. The lower limit is set by the freezing point of mercury. Since the boiling point of mercury is only about 675 F, the space above the mercury in thermometers designed for higher temperatures must be filled with an inert gas under pressure. Alcohol thermometers may be used for temperatures from −94 F to +248 F.

The more accurate thermometers have divisions etched on the stem and are preferred for test purposes due to their low heat capacity. During their manufacture, the freezing and boiling points of water are first marked while the thermometer is immersed in a test bath. The required divisions between these points, whether Centigrade or Fahrenheit, are then marked and etched on the stem. In spite of these precautions the probable error in etched stem thermometers is plus or minus one scale division, which makes calibration after manufacture necessary for most test work. Such thermometers are usually calibrated for complete stem immersion.

When incompletely immersed, a stem correction should be made. At ordinary atmospheric temperatures the correction is negligibly small, but it usually is important when measuring high temperatures such as those of steam and flue gas. The emergent stem correction may be calculated by the equation:

$$K = 0.00009\, D\, (t_1 - t_2) \qquad (1)$$

where

K = correction to be added, Fahrenheit degrees.
D = number of degrees on the thermometer scale which are not immersed.
t_1 = temperature indicated on the thermometer, Fahrenheit degrees.
t_2 = temperature of the non-immersed mercury column, Fahrenheit degrees.
0.00009 = difference in the coefficient of expansion of the mercury and glass.

Since the bulb has considerable area, radiant energy may affect the temperature readings [2]. Whenever the thermometer bulb is subjected to radiation from a hotter or colder surface, there may be heat gain or loss through the medium whose temperature the thermometer is supposed to indicate. This error can be minimized by surrounding the bulb with a bright polished screen.

Errors may also be avoided: (*a*) by allowing the thermometer time to reach equilibrium, (*b*) by providing sufficient circulation to give a true average temperature of the medium observed, and (*c*) by reading with the eye at the same level as the top of the liquid, *i.e.*, avoiding parallax.

Industrial type thermometers are available for permanent installations in ducts and pipes. Because of the heat capacity and conductance of the jackets of these instruments, they do not follow the fluctuations in a medium of varying temperature as well as the etched stem thermometer.

Thermometer Wells

Where temperatures of fluids or gases in vessels or conduits are to be measured, it is often necessary to resort to thermometer wells. These are especially designed to contain thermometers and thermocouples. Since the well separates the temperature sensitive element from the medium to be observed, large errors may result from their improper use [3]. These errors may be due both to poor heat transfer from the wall of the well to the sensitive element, and also to the tendency of heat to travel along the length of the well itself. To improve heat transfer in the case of thermometers, the well should be filled with a liquid of minimum practical viscosity. For medium temperatures a light mineral oil is satisfactory. Excessive conduction can be prevented by making the projecting head of the well as small as possible and the walls as thin as possible. After the thermometer is in place, the external head of the well and the wall of the conduit in the vicinity of the well should be covered with insulating material.

Thermocouples and Resistance Thermometers

When two dissimilar metals are joined at two points and a temperature difference exists between these junctions, an electromotive force is developed. By maintaining the cold junction at a constant temperature (or providing equivalent electrical compensation), the magnitude of the electromotive force developed is a direct measure of the temperature of the warm junction. By proper selection of metals, any temperature up to 2900 F may be measured. Readings are obtained by means of a potentiometer or sensitive galvanometer which may be calibrated in degrees. If a potentiometer is used, there is no current flowing through the thermocouple wires at the time of measurement and therefore the resistance of the thermocouple circuit does not affect the accuracy of the reading. If a galvanometer is used instead of a potentiometer, the instrument is usually built with a high internal resistance to minimize the effect of the resistance of the thermocouple circuit and, also, special lead wires of known resistance are used to connect the galvanometer to the thermocouples. The basic potentiometer circuits are shown in Fig. 1. The thermocouple leads A-B are so connected that their polarity opposes that of battery C. If the position of E on the graduated slide wire rheostat DF is adjusted until galvanometer G shows no current flowing, resistance DE will indicate directly the voltage generated by the thermocouple. In order to correct for variations in voltage from battery C,

switch S is momentarily thrown over to the standard cell circuit and rheostat R is then adjusted so that the galvanometer shows zero current. Battery C then exerts the known voltage of the standard cell at DH.

Calibration of thermocouples for high temperatures may be made against known melting points of metals. Radiation effects may be minimized by using *the smallest size of wires consistent with mechanical strength.* The use of small wires also makes the thermocouple sensitive to minute fluctuations in temperature. Wires of No. 33 B & S gage are small enough to be sensitive and to minimize radiation effects while still rugged enough for many purposes. The effect of radiation upon thermocouple readings may be eliminated by using several couples of different diameters and plotting the readings obtained against the diameters. The true temperature reading is obtained by drawing a smooth curve through the plotted points and extending the curve to intersect

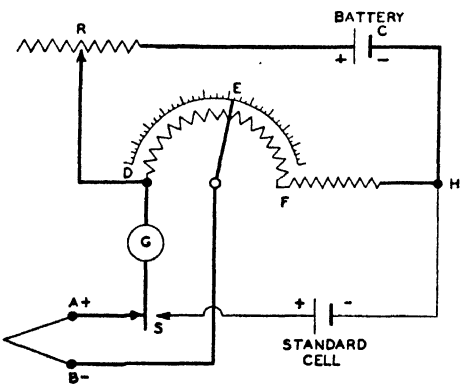

FIG. 1. BASIC CIRCUIT AND CONNECTIONS FOR THERMOCOUPLE AND POTENTIOMETER

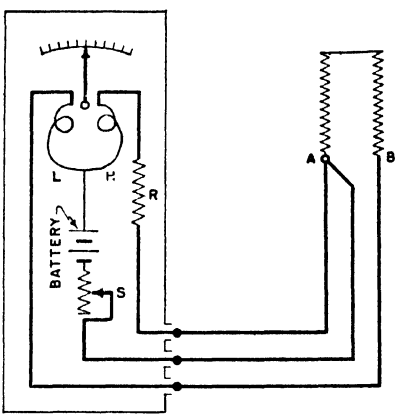

FIG. 2. TYPICAL RESISTANCE THERMOMETER CIRCUIT AND CONNECTIONS

the zero diameter axis [4]. The temperature reading at point of intersection is the true temperature.

By the use of thermocouples, temperatures at remote points may be indicated or recorded on conveniently located instruments; average temperature may be readily obtained by connecting several couples in parallel or in series; and temperatures may be obtained within thin materials, narrow spaces, or otherwise inaccessible locations.

Thermocouples in series with every alternate junction maintained at a common temperature will give an emf which, divided by the number of couples to give the average emf[5] per couple, may be used to find the average temperature.

Thermocouples in parallel having the similar metals of a number of couples connected together and run to a common cold junction will cause an indication on a potentiometer which is the true emf only if the electrical resistances of the parallel junctions are the same [5, 6].

Temperatures of surfaces below red heat are difficult to determine by any other means than thermocouples. For this purpose, a thermocouple of fine wires is preferable to minimize the possibility of error due to the conduction of heat along the wires. It may be attached to a metal surface in any of several ways. For permanent installations, soldering, brazing or peening may be desirable. A small hole is drilled for the peening

operation; the thermocouple is inserted and the metal is peened to retain it. The fact that the thermocouple is in electric contact with the surface is unimportant in usual circuits. For temporary arrangements, couples may be attached by means of surgical or cellophane tape. For many boiler or furnace surfaces, furnace cement serves very well. The thermocouple may be attached by means of the cement when the surface is cold and must be treated gently and usually supported until the cement dries, due to heat, and hardens—after which it has ample strength. It is good practice to use as little cement as possible, and also to plaster the wires to the surface for an inch or so from their junction to avoid errors due to heat conduction along the wire. Electric insulation between the wires should be perfect except at the junction since, otherwise, the indicated emf will be between those existing at the junction and at the short circuit.

Resistance thermometers depend for their operation upon the change of electric resistance of metal with change in temperature. The resistance generally increases with rising temperature. Their use largely parallels that of thermocouples, although readings tend to be unstable above 950 F. Two-lead temperature elements are not recommended, since they do not permit correction for lead resistance. Three leads to each resistor are necessary to obtain consistent readings.

A typical circuit used by several manufacturers is shown in Fig. 2. In this design a differential galvanometer is used, in which coils L and H exert opposing forces on the indicating needle. Coil L is in series with the thermometer resistance AB, and coil H is in series with the constant resistance R. As the temperature falls, the resistance of AB decreases allowing more current to flow through coil L than through coil H. This causes an increase in the force exerted by coil L, pulling the needle down to a lower reading. Likewise, as the temperature rises the resistance of AB increases, causing less current to flow through coil L than through coil H. This forces the indicating needle to a higher reading. Rheostat S must be adjusted occasionally to maintain a constant flow of current.

As compared to the thermocouple the resistance thermometer does not require a cold junction, and it can be simply scaled for more accurate measurements; but, generally because of its construction it is more costly and is apt to have considerable lag. It gives best results when used to measure steady or slowly changing temperature. For accurate results the entire thermometer coil must be exposed to the temperature to be measured.

Pyrometers

For measuring high temperatures, as in furnaces, *pyrometers* are often used. Radiation pyrometers concentrate the radiant energy on a thermopile, and the reading is obtained on a galvanometer or potentiometer. Optical pyrometers require visual matching of a narrow spectral band, usually red, emitted by the object with that from a standard electric lamp.

PRESSURE MEASUREMENT

Barometer

The most accurate barometer for determining the atmospheric pressure is the mercurial type, consisting of a tube over 30 in. long closed at the top and standing in a mercury well. The barometric pressure is expressed as the height of the mercury column above the level of the mercury in the

well. Such barometers are equipped with an adjustment to compensate for change in level of mercury in the well. The reading should be taken at the top of the meniscus and is obtained on a Vernier scale.

Correction for variation of the density of the mercury column and for expansion of the brass scale, which are usually calibrated for 32 F mercury and 62 F scale temperature, should be made by subtracting from the observed height in inches the value of C determined by Equation 2.

$$C = \frac{h\,(t - 28.630)}{(1.1123\,t - 10978)} \qquad (2)$$

where

C = correction to be subtracted, inches of mercury.
h = observed height, inches of mercury.
t = observed temperature of the barometer, Fahrenheit degrees.

Standard atmospheric pressure at sea level is 29.921 in. Hg. Since normal atmospheric pressure decreases about 0.01 in. Hg for each 10 ft increase in elevation, it is important to make a correction if the elevation of the barometer is not that of the test apparatus. In many cases the barometric reading may be obtained from a nearby Weather Bureau Station, in which case inquiry should be made as to whether the value is as observed or corrected to sea level.

Atmospheric pressure may also be measured by an aneroid barometer which is easily portable. In this type, variations in atmospheric pressure bend the thin surface of a sealed box or tube. The aneroid type is not as accurate as the mercurial and needs frequent calibration. Most of the pressure gages used in engineering work indicate the difference between the pressure being measured and the atmospheric pressure. Such pressures are called gage pressures. Absolute pressure may be obtained by adding barometric pressure and gage pressure algebraically.

Pressure Gages

The Bourdon type gage is a widely used device for measuring pressures. The Bourdon tube is elliptical in cross-section and circular in form, and is connected by suitable linkage to a pointer which moves over a dial. An increase in pressure tends to straighten the tube and a decrease has the opposite effect. When used with high temperature steam, the tube must be protected by a water seal. When used with ammonia it must be made of steel or other material not attacked by this substance. When used for sub-atmospheric pressure, the gage is known as a vacuum gage, and is usually graduated in inches of mercury. For pressures above atmospheric, it is termed a pressure gage and is graduated usually in pounds per square inch.

Occasionally, gages are graduated in feet of water. Some, made to indicate either pressure or vacuum, are termed compound gages. Calibration is usually made by means of a dead weight tester, consisting of a platform and weights resting on a piston acting on oil in a cylinder. The pressure at all points in the fluid is determined from the area of the piston and the total weight resting on the oil. Adjustments are provided in the gage linkage to make necessary corrections. A correction chart may be used for accurate work.

Manometers

For measuring low pressures or differences in pressure between two points as in a duct system, the vertical U tube is a simple and accurate

gage and is used for test work with water or with various fluids such as mercury, kerosene, or alcohol. Readings are usually in inches of one of these fluids, and must be arithmetically converted into inches of water or other standard units. The glass tube used to form the manometer should be chemically clean and the bore should not be less than $\frac{3}{16}$ in. A modified form of the *U* tube manometer using mercury as the fluid, can be constructed to measure absolute pressures directly [7].

For measuring pressure differences of a few inches of water, or less, *U* gages are often set at an angle for scale amplification. In commercial gages of this type, commonly termed *draft gages*, only one tube of small bore is used and the other leg is replaced by a reservoir. Although the

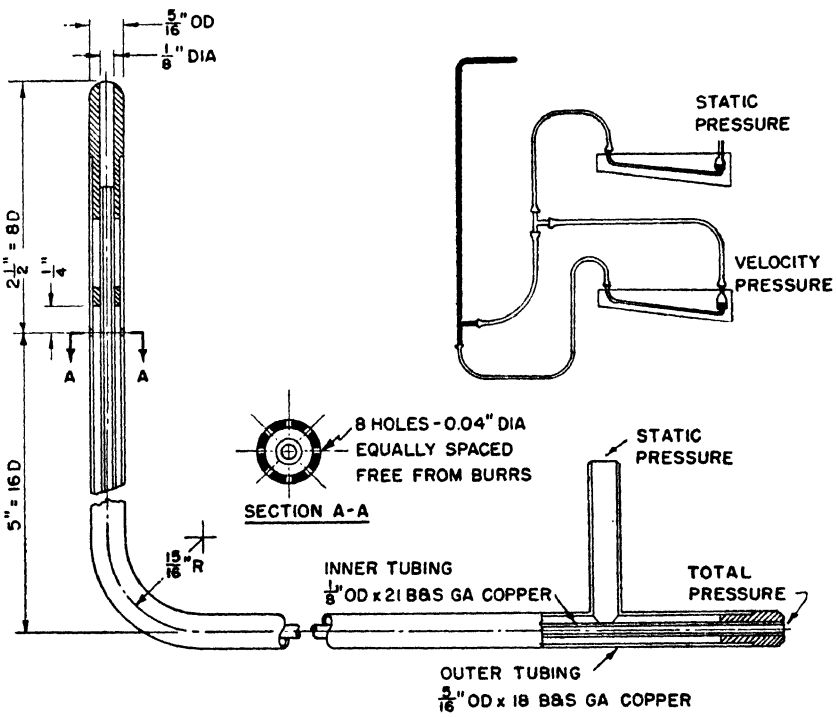

FIG. 3. STANDARD PITOT TUBE

scale is calibrated to read in inches of water, a fluid having the density and characteristics of kerosene is often used. It is necessary, in such a gage, to use a fluid having the same gravity as that for which the gage was originally calibrated, or to apply a correction if another fluid is used. Such gages may be checked one against another to detect errors in gravity of fluid. For more accurate calibration the gage may be checked against a micromanometer or a calibrating device known as a hook gage [8]. The accuracy of a draft gage is dependent on the slope of the tubes and consequently the base of the gage must be leveled carefully. It is not desirable to use a slope of less than 1 in 10.

Where pressures are read under extreme conditions of temperature and calibration is possible only at normal temperature it is necessary to correct for the change in density of the liquid in the manometer [9].

For measuring low pressure differences to within 0.001 in. of water very sensitive *micromanometers* are available, such as the Illinois or Wahlen,

the Trimount, and the Emswiler [10, 11]. Calibration of these is impossible, and readings are converted to pressure units by fundamental calculations involving the specific gravity of the fluids used and the design principles involved.

Static Holes and Tubes

For measuring air flow by means of orifices or static tubes the type of openings used for pressure measurement and their location are quite as important as the accuracy of the gage or manometer. Where velocities are low, as in plenum chambers, or where the flow is free of large eddies and parallel to the walls of the conduit, a carefully drilled hole cleared of burrs and at right angles to the stream will give accurate readings [12]. For high accuracy the drilled depth of this hole through the wall should be at least one or preferably two diameters, and four such holes or taps around the periphery of the duct should be provided. Diametrically opposite pairs of taps are connected together, and then such pairs are manifolded together. An alternate method involves the use of the Pitot tube, shown in Fig. 3. This instrument should be pointed up stream, parallel with the air flow.

Where the flow is not axial or parallel to the side walls of the duct a very close approximation of the static pressure and the flow direction can be obtained by a Fechheimer tube [13].

MEASUREMENT OF AIR MOVEMENT

The problem of measuring air movement may be divided into three main parts: air confined in ducts, air circulating in free spaces, and air entering or leaving such space through openings such as grilles. Other gases may be measured by the same methods, but emphasis here is on air measurements [14].

For determining the velocity, and therefore the volume of air flowing in a duct, the Standard Pitot Tube [8] shown in Fig. 3 is probably most often used. When connected as illustrated, this instrument will give readings of both static and velocity pressure directly. From the latter the air velocity may be found from tables, or calculated from the following relation:

$$V = 1096.5 \sqrt{\frac{h_v}{d}} \qquad (3)$$

where

V = velocity, feet per minute.
h_v = velocity pressure, inches of water.
d = density of air, pounds per cubic foot.

Air flow in a duct is seldom uniform. In general the velocity is lowest near the edges or corners, and greatest at or near the center. For this reason a large number of readings should be taken in the manner shown in Fig. 4. In the case of round ducts not less than 20 should be taken along two diameters at centers of equal annular areas. In rectangular ducts the readings should be taken in the center of equal areas over the cross-section of the duct. The number of spaces should not be less than 16 and need not be more than 64. When less than 64 are taken the number of equal spaces should be such that the centers of the areas are not more than 6 in. apart. In determining the average velocity in the duct from

the readings given, the calculated individual velocities or the square roots of the velocity heads must be averaged. It is incorrect to use the average velocity head for this purpose.

To meet special conditions, different sized Pitot tubes which are geometrically similar to the standard tube can be used. Pulsating or disturbed flow will give erroneous results and, if possible, the Pitot tube should be located at least 7½ diameters downstream from a possible disturbance such as that caused by a turn or a criss-cross type of flow straightener should be installed in the duct 1½ diameters ahead of the Pitot tube [8]. Flow straighteners do not equalize flow velocity across a duct. They merely serve to improve the precision of measurements. Equilization can be effected if desirable for measuring purposes by the use of wire netting, perforated plates or cloth screens across the duct.

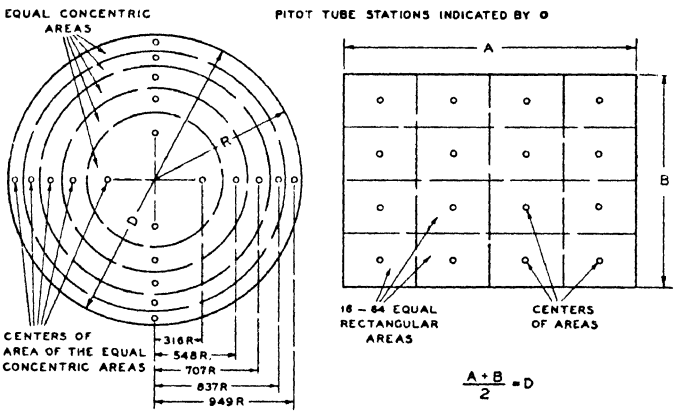

FIG. 4. PITOT TUBE TRAVERSE FOR ROUND AND RECTANGULAR DUCTS

The velocities used in many ducts are too low for measurement by means of pressure gages and it therefore becomes necessary to resort to other types of instruments.

Many forms of Pitot tubes other than the one described have been used and calibrated [15]. A double-ended tube [16], one end pointing down-stream, and one up-stream, is sometimes used for low velocities, but it should be carefully calibrated for accurate results. A special form of this tube design consists of two straight ⅛ in. tubes soldered together, closed at the end, and with a 0.04 in. hole in each tube opposite the line of contact. This tube is useful in exploring velocities on exhaust inlets, such as on hoods placed around grinding wheels.

Application of the Pitot tube is often inconvenient when velocities are low because the resultant velocity pressures become so small that extraordinary means are necessary for measuring them. In addition, velocity surveys of the whole cross-sectional area of a duct are inexpedient when numerous test runs are in prospect. Chiefly for these reasons orifices are favored for much test work. There are two types: the plate orifice and the shaped orifice or nozzle. Plate orifices are simple to construct and convenient to use in that a frame can be made to support them in the duct such that one can be removed and another inserted when it is desirable to use an orifice of a different size. Their disadvantage lies in the fact that a coefficient considerably less than unity must be applied to their indications because of the effect of the vena contracta.

Other information on orifices and their use is contained in Chapter 4, Fluid Flow. Shaped orifices or nozzles have the advantage if well made that their discharge coefficients are close to unity so that the probability of large errors is less. Orifices of this type have been adopted for several specific purposes and designs are described in the A.S.H.V.E. Unit Heater [17] and Unit Ventilator Codes [18] and in A.S.R.E. Circular 13 [19] entitled "Standard Methods of Rating and Testing Air Conditioning Equipment". In some instances nozzles are used in multiple so that the capacity of the testing equipment can be changed by shutting off the flow through one or more nozzles. An apparatus designed for testing the air flow and capacity of air conditioning equipment is described by Wile [20] in an article in which pertinent information on nozzle discharge coefficients, Reynolds numbers, and the resistance of perforated plates is also presented. Such apparatus in some laboratories is commonly referred to as a *code tester.*

The Venturi meter is like the nozzle except for the addition of a downstream transition section that reduces the pressure drop through the measuring apparatus.

The thin-plate square-edged orifice has a coefficient of approximately 0.60. The exact value depends on the location of the connections, the pressure drop, the diameter ratio of orifice to pipe, and the sharpness of the edge [21, 22].

Another method of air measurement uses the thermal electric principle where, by means of a measured amount of current, heat is put into the air stream. The weight of air flowing is calculated from the heat equivalent of the electrical input and the temperature rise of the air. Heat should be applied uniformly to the mass of air passing, and the small temperature rise must be determined accurately.

In certain applications the air velocity through a duct, heater coil, or heating unit may be most conveniently obtained by computation from the heat given up by the coil and the temperature rise (measured by thermocouples) of the air passing through. It is essential to have a uniform flow over the entire inlet and outlet of the heater at the plane of temperature measurement.

Air Currents in Free Spaces

The measurement of air current velocities within enclosed spaces such as the rooms of a house is usually a tedious undertaking. However, useful data can be obtained by using the instruments described in following paragraphs if they are maintained in calibration and the user understands the operation and limitations of the instruments [23].

One of the instruments useful for determining the velocity of air currents in free spaces is the Kata-thermometer. It is essentially an alcohol thermometer with a large bulb. The stem has two marks, one corresponding to 95 F, and the other 100 F. The instrument is heated above 100 F and then the time in seconds required for it to cool from 100 to 95 when located in the air current gives a measure of the non-directional velocity. It is important to have the Kata-thermometer dry before taking the reading. Each Kata has its own factor etched on the stem, and this factor must be used with its cooling formula or chart for obtaining the velocity. The Kata-thermometer is useful in exploring ventilated spaces to determine whether the proper air movement and distribution are being maintained. It is also used in determining the cooling power of the atmosphere; since it loses heat by radiation and convection when

dry, and by radiation, convection, and evaporation when the bulb is equipped with a wetted cloth covering [24].

Another instrument for measuring low velocity air currents is the heated thermometer anemometer [25]. This consists of a mercurial glass thermometer with a resistance winding on the bulb. Current is supplied from an external source in a measured amount. The difference between the temperature of this heated thermometer and that of an ordinary thermometer at the same location, together with the current supplied, makes it possible to calculate the non-directional velocity of the air stream.

The heated thermocouple anemometer employs a thermocouple instead of a thermometer [26].

Another instrument is the hot wire anemometer which has been made in several patterns. In general, a measured current is supplied to raise the temperature of a fine bare wire above the temperature of the surrounding air. With the use of a very fine wire, minute fluctuations in velocity may be measured, and the area exposed to radiant exchange with heated or cooled surfaces is at a minimum. This instrument is easily adapted to remote reading or recording. A group of them may be connected together to give the average velocity in a space, or the velocity at individual points within a test space, by suitable switching arrangements [27, 28].

Deflecting Vane Anemometer

The deflecting vane anemometer consists of a pivoted vane enclosed in a case, against which air exerts a pressure as it passes through the instrument from an up-stream to a down-stream opening. The movement of the vane is resisted by a hair spring and a damping magnet. The instrument gives instantaneous readings of directional velocities on an indicating scale. When used in fluctuating velocities, it is necessary to average visually the swings of the needle to obtain average velocities. This instrument is very useful for studying mixing of air in a room [29] and in locating and measuring peak velocities that may be objectionable. Various attachments are available, such as the double tube arrangement for obtaining velocities in ducts, and a device for measuring static pressures. Each instrument and the attachments for it must receive individual calibration.

Propeller or Revolving Vane Anemometer

The propeller or revolving vane anemometer consists of a light revolving wheel connected through a gear train to a set of recording dials that read the linear feet of air passing in a measured length of time. It is made in various sizes, 3 in., 4 in., and 6 in. being most common. Each instrument requires individual calibration. At low velocities the friction drag of the mechanism is considerable. In order to compensate for this, a gear train that overspeeds is commonly used. For this reason the correction is often additive at the lower range and subtractive at the upper range with the least correction in the middle range of velocities. Most of these are not sensitive enough for use below 200 fpm.

Measurement of Velocities at Inlets and Outlets of Ducts

In the field it is often desirable to make volume measurements at the face of the supply openings. It is rare to have access to the interior of duct sections where the flow is sufficiently uniform for measurement. For accuracy the instrument and its application should be checked on a similar approach and grille in the laboratory before use in the field.

Tests have shown that the propeller type anemometer can be used successfully on most of the common types of supply grilles [30, 31]. The core area is divided into equal squares, and the anemometer is held against the face of the grille for the same length of time in each. To get the air volume in cubic feet per minute, the average corrected velocity in feet per minute thus obtained is multiplied by the average of the gross and net free area of the grille (core) in square feet.

On exhaust openings, the anemometer traverse is made as described previously. The air volume may be determined by multiplying the corrected velocity in feet per minute by the gross core area of the grille in square feet and by a coefficient for average conditions of 0.85 [32].

When a propeller type anemometer is held in a stream of varying velocities, it tends to indicate higher than the true average, that is, the speed of the propeller is nearer to the top velocity in its area than it is to the minimum velocity. This is the main reason for the large difference in ratings of unit ventilators by the anemometer method and by air volume measurements in a duct approach to the inlet [33].

Any of the other anemometers described can be used within their range at the face of supply grilles when properly applied. In principle it is a case of finding the velocity at many points and using the average thus found with the correct discharge area at that cross-section. The deflecting vane anemometer equipped with a jet on the end of a rubber tube has been found especially convenient and accurate on supply grilles[34]. On modern air conditioning grilles the core area is used without a correction coefficient when the jet is held one inch away from the face of the grille. At this distance the constriction due to the thin bars has disappeared since the small air jets have reunited, and the air stream has not yet spread beyond the core dimensions. With deflecting grilles the exploring jet should be turned to the angle giving a maximum reading. With suitable traversing tips and calibration, this instrument may also be used on exhaust grilles if proper grille factors are applied [35].

Smoke is a qualitative tool which is very useful in studying air movements. Satisfactory smoke can be obtained from titanium tetra-chloride (which, however, is very irritating to nasal membranes) or by mixing potassium chlorate and powdered sugar (a non-irritating smoke) and firing the mixture with a match. This latter process evolves considerable heat and it should be confined in a pan away from flammable materials. The titanium tetra-chloride smoke lends itself to spot determinations, particularly for leakage through casings and ducts, as it can be easily handled in a small pistol-like ejector. The fumes of aqua ammonia and of sulfuric acid, if permitted to mix, form a white precipitate which is useful for some purposes. Two bottles, one containing ammonia water and the other acid, are connected to a common nozzle by means of rubber tubing. Air is forced over the surfaces of the liquids in the bottles by means of a syringe and the two streams, upon mixing at the nozzle, form a white cloud.

AIR CHANGE MEASUREMENTS

Atmospheric air contains a certain amount of carbon dioxide. Its concentration is increased within enclosures by the carbon dioxide given off by occupants. The total air change through open windows, infiltration, and mechanical ventilation, may be measured by the carbon dioxide concentration but absorption of CO_2 by walls and other materials may introduce errors [36] and consequently some investigators prefer hydrogen

to CO_2 for such tests. Since occupants also give off moisture, the increase in humidity may also be used as an index of ventilation. Usually more direct methods of measuring air supply and air distribution are in favor.

MEASUREMENT OF RELATIVE HUMIDITY

Wet- and dry-bulb mercurial thermometers are commonly used in the form of a sling psychrometer to determine relative humidity. The wet-bulb wick and water for wetting it must be clean, and the temperature of the water should preferably be slightly above the wet-bulb temperature. An air stream velocity of 900 fpm is recommended, although higher velocities will result in greater accuracy [37]. This velocity is obtained with the sling psychrometer by whirling it rapidly, followed by reading the wet-bulb thermometer quickly before its indication changes. Owing to the human element involved in this method, more accurate results are obtained with types of psychrometers in which air is drawn over the thermometers by a fan, or by a bulb operated aspirator. In ducts, the air flow itself gives the proper evaporating conditions. Several observations should be made until the minimum temperature is reached. Relative humidity may be obtained from tables or psychrometric charts [38]. Although it is common practice to use the charts which are based on a barometric pressure of 29.92 in. Hg, a correction for barometric pressure is necessary for extreme accuracy. This correction is made by multiplying the relative humidity as determined from the chart by the ratio of the observed barometric pressure and the standard barometric pressure.

For temperatures below 32 F, the water on the wick is allowed to freeze, during which time the temperature will drop below the true wet-bulb. A thin film of ice is more desirable than a thick one, and it is satisfactory to remove the wick and freeze a thin film directly on the bulb. Care must be taken to read the temperatures accurately due to the slight wet-bulb depressions. Tables for ice conditions must be used [39].

Dew-point apparatus for humidity measurements consists of a polished plated container cooled by the evaporation of a volatile liquid within. The temperature at which the first slight water vapor forms on the polished surface is the dew-point. If the temperature is below 32 F, the deposit will appear as frost. Another method of determining humidity is by chemical means in which the water vapor is removed by a drying agent and weighed on a chemical balance. A thermal conductivity method is available for temperatures above 212 F or for extremely low humidities [40].

DUST DETERMINATION

The measurement of dust is complicated by the many kinds involved. Some of the collecting methods are impingement on viscous surfaces, impingement at high velocity under water, collection on porous crucibles or filter paper through which air passes, and electric precipitation. Determination may be by direct weighing of samples or by microscopic counting. A commonly used method employs the Smith-Greenburg impinger which collects samples in water or alcohol and in which particles are counted under a microscope in various cells such as the Hatch or Dunn cells. Another method employs the Lewis [41] sampling tube with the analytical determination of the increase in weight of a porous crucible. All reports should state the method of sampling and counting. The A.S.H.V.E. Code for Testing and Rating Air Cleaning Devices Used in General Ventilation Work specifies the porous crucible method [42].

At the National Bureau of Standards, sampling tubes are used upstream and downstream of an air cleaner under test whereby samples of air can be drawn through filter papers to afford an evaluation of the comparative effectiveness of the cleaner in arresting dust [43].

Other instruments for evaluating dust, including the konimeter, are described by Drinker and Hatch [44].

HEAT TRANSFER THROUGH BUILDING MATERIALS

The A.S.H.V.E. Standard Test Code for Heat Transmission Through Walls [45] describes the construction and use of the guarded hot box for determining over-all heat transmission coefficients of built-up sections including surface resistances. This apparatus consists of inner and outer insulated boxes, each having one open side which is sealed tightly against the wall specimen to be tested. The outer box serves as a guard and a zero temperature difference is maintained between the inner box and the air space separating it from the outer box. Electric heaters are provided to maintain any desired temperature within the boxes while at the same time the outer surface of the wall specimen is subjected to a low temperature. A common method of applying this low temperature is to fit the specimen into an opening in the wall of a refrigerated room. The air temperature difference between the two sides of the specimen, and the rate of heat input to the guarded hot box are measured. From these data an over-all heat flow coefficient can be calculated.

The Nicholls heat meter is very useful for determining the heat flow through walls of buildings [46]. This apparatus consists of a guarded plate on both sides of which are mounted a series of thermocouples. The plate is calibrated so that the rate of heat flow through it can be determined by observing the temperature difference between the two surfaces. In use, the meter is clamped tightly against the surface of the wall in question, and readings of heat flow of accuracy sufficient for many test purposes may be obtained.

In June 1942, the A.S.H.V.E. adopted a standard test procedure for determining the conductivity of materials by use of the guarded hot plate [47]. This method is adapted to homogeneous materials, and conductivities obtained do not include surface coefficients. The method involved is one in which two identical samples are arranged one on each side of a heated plate having a guard and a central test section. The resulting sandwich is placed between cold plates. In operation the same temperature is maintained in the guard section and test section of the heated plate and a lower temperature is maintained in each of the cold plates from a common source of cold water. Thermal conductivity is determined by measuring the amount of heat supplied to the center or guarded portion of the hot plate, the temperatures at the hot and cold surfaces and the thickness of the specimen. The apparatus requires careful, precise construction and its operation requires care and skill. The actual design of basic types of hot plates is described in an *A.S.T.M.* publication [48].

MEASUREMENT OF HEAT EXCHANGE FOR COMFORT CONDITIONS

Several instruments have been devised to measure the effect of various factors as they relate to the comfort of the body [49]. The principal ones are

the Kata-thermometer, Dufton's eupatheoscope, Vernon's globe thermometer, Winslow and Greenburg's thermo-integrator, and Yaglou's heated globe [50, 51]. These instruments were designed to obtain a quantitative measurement of the thermal exchange between the human body and its environment.

COMBUSTION ANALYSIS

The analysis of flue gases to determine completeness and efficiency of combustion is usually made chemically with an Orsat apparatus. This consists of a measuring burette, a leveling bottle, and three pipettes. Carbon dioxide is absorbed in the first pipette by potassium hydroxide, oxygen in the second by potassium pyrogallate, and carbon monoxide in the third by cuprous chloride. A known volume of gas is drawn in, and after each of the three absorptions the reduced volume is again measured in the burette. Pressure and temperature of the gas sample are kept constant while measuring. Several passes are made through each pipette which contains tubes or glass beads to increase the wetted surface. It is essential that each reaction be completed before the next reaction is started. Since the life of the reagents is limited, it is well to keep a record of the number of samples tested. Care is needed in operation to prevent the pulling of reagents out of the pipettes into the capillary tubing and burette. Many types of recording gas analyzers are available and are usually found in the larger boiler plants.

The concentration of carbon dioxide is a measure of the excess air in a plant's flue gases and this is an important factor which concerns the efficiency of fuel utilization. In larger boiler plants carbon dioxide recorders are installed which operate in several ways. The basic principles involved are chemical absorption, thermal conductivity and difference in density between the flue gas and the atmosphere. Thermal conductivity apparatus for either indicating or recording carbon dioxide concentration in flue gas are available on the market. Instruments of this type have advantages of convenience and, under some circumstances, of accuracy compared to the better known Orsat apparatus. Methods of sampling flue gases for test purposes as well as of approximating their average temperature are contained in the $I=B=R$ Codes [52].

Carbon Monoxide Measurement

The Orsat apparatus may be used for determining amounts of carbon monoxide of 2/10 of 1 per cent or more. For very low concentration of carbon monoxide, indicators and recorders depend on measurement of the heating effect of combustion of carbon monoxide to dioxide in the presence of a catalyst. The temperature rise is measured by a thermopile, the junctions of which are buried in the catalyst [53]. Such instruments are used to determine the presence of carbon monoxide in quantities as low as 1/100 of 1 per cent.

For indicating low ranges of CO as for combustion products from gas appliances discharged into occupied spaces the colorimetric method developed at the National Bureau of Standards is satisfactory [54, 55].

SMOKE DENSITY MEASUREMENTS

Smoke density may be judged by assigning to it the number of the Ringelmann Smoke Chart which appears to have the same color when

observed at a distance of 50 ft. The charts are numbered 1 to 4 and are made of black lines cross-ruled on white as given in Table 1.

TABLE 1. RINGELMANN SMOKE CHART SPACINGS

NUMBER OF CARD	THICKNESS OF LINES, MM	DISTANCE IN CLEAR BETWEEN LINES, MM
1	1.0	9.0
2	2.3	7.7
3	3.7	6.3
4	5.5	4.5

Photo-electric Cell

The photo-electric cell is used in some apparatus developed for smoke density recording in large plants. The same device is included in the testing equipment for domestic oil burners described in *National Bureau of Standards*, Commercial Standard CS75-42 [56]. Under *Laboratory Tests* this publication contains the following section: "Smoke Determination. —After combustion has reached equilibrium, the amount of smoke in the flue gases, when viewed lengthwise through 4 feet of the smoke pipe in accordance with the *Underwriters' Laboratories, Inc.*, Standard for Domestic Oil Burners (Subject 296), March 1934 and subsequent revisions, shall not reduce the output of a standard photoelectric cell from 9 microamperes, with a clear smoke pipe, to less than 8 microamperes." The commercial standard also requires that during a test after installation, the burner shall operate without visible smoke at the chimney top.

A method of evaluating smoke produced by pot type oil burners was developed for the *Institute of Cooking and Heating Appliance Manufacturers* by R. N. St. John. A glass rod is interposed between a light source and a photo-sensitive cell both before and after being exposed to the flue gases from a heating device. The diminution of the light transmitted by the rod due to the deposit of soot on its surface causes a reduction in the cell emf which is taken as an index of the concentration of smoke in the flue gases. A description of the method is contained in National Bureau of Standards Commercial Standard CS104-46 [57].

Sound and Vibration Measurements

Approximate measurements of sound intensity can be made by aural methods. The ear is used to compare the measured noise with sounds of known strength.

Electrical devices in which the ear plays no part furnish the most satisfactory means of measuring noise intensities. The sound meter consists essentially of a microphone coupled to an amplifier designed with an ear-like response. The output of the microphone is read on a sensitive direct current milliammeter graduated to read directly in decibels. Instruments of this type if connected with suitable band pass filters can be used to study the intensity of the sound over its entire range of frequencies.

Electrical instruments are available for measuring the frequency, amplitude and acceleration of a vibrating mass. They are usually more convenient and accurate than the vibrating-reed tachometer and the seismic type displacement meters and accelerometers which can also be used for this purpose. Sound level meters are discussed in several text books [58, 59] and standards [60].

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Chapter 12

PHYSIOLOGICAL PRINCIPLES

Chemical Vitiation of Air, Physical Impurities in Air, Thermal Interchanges Between the Body and Its Environment, High Temperature Hazards, Acclimatization, Upper Limits of Heat for Men at Work, Application of Physiologic Principles to Air Conditioning Problems, Effective Temperature Index and Comfort Zones

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VENTILATION is defined in part as *the process of supplying air to, or removing air from, any space by natural or mechanical means.* The word in itself implies quantity, but air must be of the proper quality also. The term *air conditioning* in its broadest sense implies control of any or all of the physical or chemical qualities of the air. The A.S.H.V.E. Code of Minimum Requirements for Comfort Air Conditioning [1] defines it "as the process by which simultaneously the temperature, moisture content, movement and quality of the air in enclosed spaces intended for human occupancy may be maintained within required limits. If an installation cannot perform all of these functions, it shall be designated by a name that describes only the function or functions performed."

CHEMICAL VITIATION OF AIR

People living indoors bring about certain physical and chemical changes in the air about them. The oxygen content of the air diminishes and the carbon dioxide increases, but these changes are too slight to be significant except in air tight spaces as in submarines. Organic matter which is usually perceived as odors comes from the body or clothes. Moisture and heat are given off by the body. There is no evidence of any toxic volatile material given off by man to the ambient air. Stale air may be offensive because of odors and may induce loss of appetite and loss of energy. Objectionable body odors have the same effects. These reasons, whether esthetic or physiological, usually make it desirable in the design of air conditioning systems to provide for the elimination or control of odors arising from occupancy, cooking, or other sources. This may be accomplished by introducing odor-free air in sufficient quantities to reduce odor concentrations by dilution to a level which is not objectionable. Odor-free air may be outdoor air or air which has been cleared of odors by sorption, washing, or other appropriate means.

In the case of vitiation by a few hazardous gases such as carbon monoxide from heating, cooking, and certain industrial processes, no satisfactory chemical treatment for the elimination of the impurity has been found. The only really satisfactory solution is elimination at the source by local exhaust ventilation; or, if this is impossible, reduction to a safe concentration by dilution. (See Chapter 10.) In the case of contamination by other matter, including volatile vapors and gases, chemical treatment for the removal or reduction of the impurities has been made available through air cleaning methods, which are discussed in Chapter 33 on Air Cleaning Devices.

When the only source of contamination is the human occupant, the minimum quantity of outdoor air needed appears to be that required to remove objectionable body odors, or tobacco smoke. The concentration of body odor in a room, in turn, depends upon a number of factors, including the dietary and hygienic habits of the occupants (frequently

reflecting their socio-economic status), the outdoor air supply, air space allowed per person, odor adsorbing capacity of air conditioning processes, and temperature and relative humidity. Perception of odor has been found to vary as the logarithmic function of the odor intensity, or inversely with the logarithmic function of the amount of outdoor air supplied and the air space per person.

The relation between air supply and occupancy has been reported by the Harvard School of Public Health [2] (Table 1) and the A.S.H.V.E. Research Laboratory [3]. Outdoor air requirements for removal of objectionable tobacco smoke odors are not accurately known but available information and current practice indicate the need of 15 cfm per person or more [4].

The total quantity of outside air to be circulated through an enclosure is often governed chiefly by physical considerations for controlling temperature, air distribution, and air velocity. Other factors which must be taken into consideration include the type and usage of the building, locality, climate, height of rooms, floor area, window area, extent of occupancy, and the operation of the system distributing the air supply. Frequently, some of these factors, particularly the need for air movement and good distribution, may be satisfied by recirculation of inside air rather than outside air.

It will be noted that, with adequate air space, the rate of air change indicated in Table 1 is from 10 to 30 cfm per person. In rooms occupied by only a few persons such an air change will be automatically attained in cold weather by normal leakage around doors and windows, and can easily be secured in warm weather by the opening of windows. With a space allotment of 400 cu ft per person, only 1½ air changes per hour are necessary to provide a ventilation rate of 10 cfm per person.

Therefore, in the ordinary dwelling with adequate cubic space allotment, no special provision for controlling chemical purity of the air is necessary (aside from removal of fumes from heating appliances). For such conditions, the control of air temperature is the major consideration.

In more crowded rooms (large offices, large workrooms, auditoriums), the cubic space per person is less and it is usually impossible to admit untempered outside air without creating drafts. Here, mechanical ventilation is essential for removal of the heat and moisture produced by the occupants.

The present data regarding the effect of cubic space on ventilation requirements are not universally accepted. The Code of Minimum Requirements for Comfort Air Conditioning [1] prescribes definite minimum requirements which should be familiar to the designing engineer. It should be emphasized, however, that the code fixes *minimum*, rather than *adequate* requirements.

Notwithstanding the rapid advance made in air conditioning some persons still believe there is a stimulating quality in outdoor air (particularly country, mountain and seashore air) under ideal weather conditions, which is lacking in artificially conditioned air. It is apparent, however, that modern air conditioning insures control of the phenomena of nature for the service and comfort of man independently of weather conditions. Freedom of movement, action and thought, together with the variability of stimuli experienced by persons under ideal conditions in the country, mountains or seashore, undoubtedly have some stimulating effect. Various experimenters have attempted to duplicate the invigorating qualities of outdoor air by the use of ozone, ionization, or

TABLE 1. MINIMUM OUTDOOR AIR REQUIREMENTS TO REMOVE OBJECTIONABLE BODY ODORS UNDER LABORATORY CONDITIONS [2]

TYPE OF OCCUPANTS	AIR SPACE PER PERSON CU FT	OUTDOOR AIR SUPPLY CFM PER PERSON
Heating season with or without recirculation. Air not conditioned.		
Sedentary adults of average socio-economic status	100	25
	200	16
	300	12
	500	7
Laborers	200	23
Grade school children of average socio-economic status	100	29
	200	21
	300	17
	500	11
Grade school children of lower socio-economic status	200	38
Children attending private grade schools	100	22
Heating season. Air humidified by means of centrifugal humidifier. Water atomization rate 8 to 10 gph. Total air circulation 30 cfm per person.		
Sedentary Adults	200	12
Summer season. Air cooled and dehumidified by means of a spray dehumidifier. Spray water changed daily. Total air circulation 30 cfm per person.		
Sedentary Adults	200	<4

ultra-violet light, but results to date have been inconclusive or negative [5].

Ozone in amounts of 0.01 to 0.05 ppm of air is allowable in comfort air conditioning. Above this limit there is a pungent, unpleasant odor and perhaps respiratory distress, depression, and stupor [6].

PHYSICAL IMPURITIES IN AIR

Dust particles of almost any type can produce irritation of the mucous membranes of the nose and throat if present in high concentrations. Certain dusts may be very harmful, but coal dust is tolerated well. The effects of various industrial dusts, pollens, etc. are discussed in Chapter 10.

A certain part of the dissemination of disease in confined spaces is caused by the emission of pathogenic organisms from infected persons. (See Chapter 13.)

While in some instances it may be possible to reduce the physical impurities of the air by dilution from a non-contaminated source, such a source is rarely available. Frequently outside air contains a higher concentration of physical impurities than indoor air. Therefore, it is usually desirable to reduce the concentration of physical impurities by air cleaning methods. (See Chapter 33.)

THERMAL INTERCHANGES BETWEEN THE BODY AND ITS ENVIRONMENT

Body temperature depends upon the balance between heat production and heat loss. Heat resulting from oxidation in the body (metabolism)

maintains the body temperature well above that of the surrounding air in a cool or cold environment. At the same time, heat is constantly lost from the body by radiation, convection and evaporation. Since, under ordinary conditions, the body temperature is maintained at its normal level of about 98.6 F, the heat production must be balanced by the heat loss. During work the body temperature may rise; in fact, afternoon temperatures of normal persons average 1 deg above the resting value of the morning whether working or not.

The fundamental thermodynamic processes concerned in heat interchanges between the body and its environment may be described by the equation:

$$M = \pm S + E \pm R \pm C \qquad (1)$$

where

M = rate of metabolism, heat produced within the body.
S = rate of storage, change in intrinsic body heat.
E = rate of evaporative heat loss.
R = rate of radiative heat loss or gain.
C = rate of convective heat loss or gain.

The rate of metabolism, M, is always positive. The storage, S, may be either positive or negative, depending upon whether heat is being stored or depleted owing to a rise or fall in body temperature. Under ordinary circumstances (when the dew-point of the air is below the body surface temperature) the evaporation loss, E, is always positive; that is, heat from metabolism supplies this loss. R and C are positive when body surface temperature is above that of walls and air, and negative when it is below.

DuBois[7], after careful calorimeter studies on fasting, nude men, plotted the partition of body heat loss and heat production as a function of temperature. Fig. 1 shows some disparity between heat production and heat loss. This disparity is S in Equation 1. In the central range of the experiments, S was quite low and no increase in heat loss by vaporization was apparent. Within the range 81 to 86 F a zone of easy regulation of body heat exists for nude persons which may be called a *zone of thermal neutrality* in contrast with the chilling effect noted in the cooler part of the curve, the *zone of body cooling*, and in contrast with the *zone of evaporative regulation* at higher temperatures. In the narrow range of the neutral zone most men feel comfortable under similar conditions (nude and at rest). In this neutral zone the regulation of body temperature is accomplished by automatic variation in the blood flow to the skin, especially of the hands, feet, and head, to vary the radiation and convection losses as required to balance heat loss and heat production.

At lower temperatures throughout the *zone of body cooling* there is a progressive fall in the skin temperature, especially in feet and hands, which implies a diversion of blood from the skin into deeper organs, and a progressively greater loss of intrinsic body heat ($-S$), until the body temperature falls enough to induce shivering. The muscular activity of shivering increases heat production and so makes good the excessive heat loss, maintaining body temperature nearly normal. In cool environments heat loss by evaporation from skin and respiratory tract remains almost constant at about 25 per cent of the heat produced in resting or slightly active subjects.

In the zone of evaporative regulation the burden of heat regulation is assumed by evaporation, radiation and convection losses already being

maximal from the warm skin, flooded by maximal cutaneous blood flow. In such hot conditions the pulse rate rises. When sweat first appears it covers only part of the body, especially the head and neck, and gradually extends to drench the entire body surface. All factors which affect the evaporation of water from the skin affect heat regulation in the zone of evaporative regulation. Relative humidity and air motion are most important. With dry-bulb temperature above body temperature, air motion facilitates evaporative heat loss by removing hot humid air from contact with the skin and replacing it with relatively drier air.

Heat regulation in man requires an intact set of sensory nerves, a normal sympathetic nerve supply to sweat glands and blood vessels, a great many sweat glands, and a circulatory system capable of carrying heat from muscles and viscera to the skin by circulation of the blood.

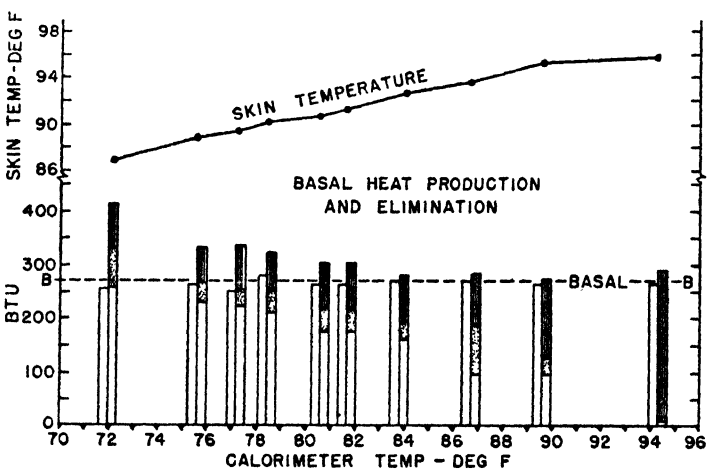

FIG. 1. HEAT LOSS FROM HUMAN BEINGS BY EVAPORATION, RADIATION, AND CONVECTION[a]

[a]Normal control, naked, in calorimeter at temperatures from 72.8 to 94.1 F. First column in each experiment represents heat production as determined by indirect calorimetry, the second column, heat elimination. The portion marked with vertical lines represents vaporization, the dotted area convection, the unmarked area radiation. The skin temperature represents the average reading of 18 spots on the surface.

The human body possesses remarkable powers of adaptation to a narrow range of atmospheric conditions around an ideal optimum where storage is zero, and metabolism and skin and tissue temperature are at optimum values. Under these conditions, the body experiences a sensation of comfort. As skin and body-tissue temperatures rise or fall above or below an optimum, complex adaptive mechanisms come into play, chiefly associated with redistribution of blood supply between the skin and deeper tissues (in a cold environment) and with sweat secretion (in a hot environment). These reactions are governed by nervous or chemical stimuli from both skin and internal tissues. Nerves from the skin carry the sense impressions to the brain and the response comes back over another set of nerves, the motor nerves, to the musculature and to all the active tissues in the body, including the endocrine glands. In this way, a two-sided mechanism controls the body temperature by (1) regulation of internal heat production (chemical regulation), and (2) regulation of heat loss by means of automatic variation in the rate of cutaneous circu-

lation and by operation of the sweat glands (physical regulation). The reactions involved in cold and in hot environments are on the whole radically different in nature. The mechanisms of adjustment involved are extremely complex and, while they are receiving considerable study, a complete understanding of their operation is still lacking.

Some of the phenomena of body temperature control are shown graphically in Fig. 2. The dotted curves, from a study at the John B. Pierce Laboratory of Hygiene [8], are for subjects lightly clothed in a semi-reclining position and give the relation between the dry-bulb temperature of the environment (with about 45 per cent relative humidity) and the metabolic rate (heat production), the rate of heat dissipation by radiation and convection combined, and the latent heat loss due

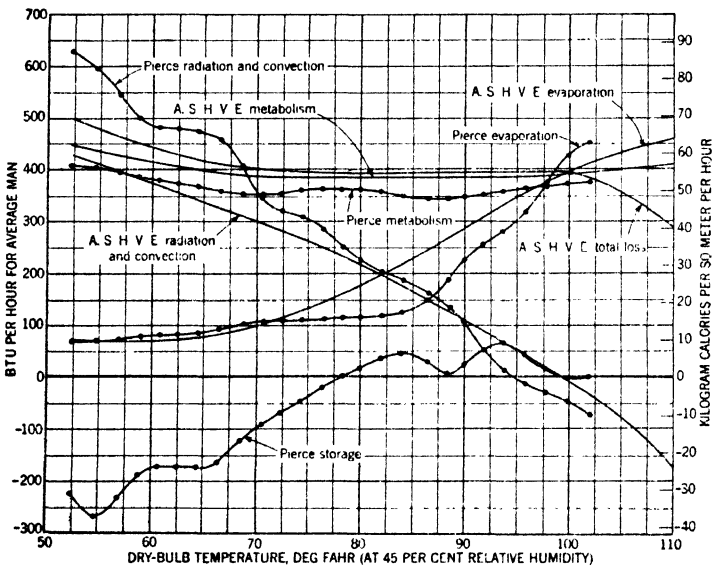

FIG. 2. RELATION BETWEEN METABOLISM, STORAGE, EVAPORATION, RADIATION PLUS CONVECTION, AND OPERATIVE TEMPERATURE FOR THE CLOTHED SUBJECT

to evaporation from the skin and the respiratory tract. The smooth line curves from the work of the A.S.H.V.E. Research Laboratory [9] give the same relationships for healthy, male subjects (18 to 24 years of age), seated at rest and dressed in customary winter indoor clothing. The Pierce Laboratory data for the semi-reclining subjects also include the rate of heat storage (either positive or negative) due to a rise or fall in body temperature. For the normally clothed subjects, a curve gives the total heat loss (that is, the sum of the radiation, convection and evaporative losses). Here, storage is given by the difference between the metabolism and total heat loss.

The small difference between the metabolic rates for the two groups of subjects may be accounted for by difference in activity. Heat exchange between the body and the environment by radiation and convection is greater for the lightly clothed subject, both for cool conditions where there is excessive heat loss, and for very warm conditions where there is transfer of heat from the atmosphere to the body. The two curves for

evaporative loss serve to show how physiological control uses evaporation of perspiration to maintain equilibrium at high temperatures. Below 75 F for the normally clothed subject, and below 85 F for the lightly clothed subject, evaporation loss is minimal and constant. Above these temperatures control is obtained by the availability of perspiration for evaporation. The difference in the curves above 75 F is probably largely determined by the difference in clothing and activity. In temperatures well above 95 F radiation and convection change from positive to negative. Even the greatly increased evaporative heat loss ceases to take care of heat production plus radiation and convection gains. Heat storage results with a consequent rise in body temperature and metabolic rate. This may be accounted for by increased chemical reaction with rise in temperature, and indicates the point where a breakdown in thermal equilibrium begins. Survival time is limited when the accelerated metabolic rate raises body temperature to 105 F.

TABLE 2. PHYSIOLOGICAL RESPONSES TO HEAT OF MEN AT REST AND AT WORK[a]

Effective Temp	Actual Cheek Temp (Fahr Deg)	Men at Rest			Men at Work 90,000 ft-lb of Work per Hour			
		Rise in Rectal Temp (Fahr Deg per Hr)	Increase in Pulse Rate (Beats per Min per Hr)	Approximate Loss in Body Weight by Perspiration (Lb per Hr)	Total Work Accomplished (Ft-Lb)	Rise in Body Temp (Fahr Deg per Hr)	Increase in Pulse Rate (Beats per Min per Hr)	Approximate Loss in Body Wt by Perspiration (Lb per Hr)
60	.....	.....	.....	....	225,000	0.0	6	0.5
70	.....	0.0	0	0.2	225,000	0.1	7	0.6
80	96.1	0.0	0	0.3	209,000	0.3	11	0.8
85	96.6	0.1	1	0.4	190,000	0.6	17	1.1
90	97.0	0.3	4	0.5	153,000	1.2	31	1.5
95	97.6	0.9	15	0.9	102,000	2.3	61	2.0
100	99.6	2.2	40	1.7	67,000	4.0[b]	103[b]	2.7[b]
105	104.7	4.0	83	2.7	49,000	6.0[b]	158[b]	3.5[b]
110	.....	5.9[b]	137[b]	4.0[b]	37,000	8.5[b]	237[b]	4.4[b]

[a]Data by A.S.H.V.E. Research Laboratory.

[b]Computed value from exposures lasting less than one hour.

HIGH TEMPERATURE HAZARDS

Studies at the A.S.H.V.E. Research Laboratory [10] and elsewhere during the past two decades have made available much information dealing with the physiological effects of hot atmospheres on workers and means of alleviating the distress and hazards associated therewith. Table 2 gives some of the physiological responses of men at rest and at work to hot environments. Frequent and continued exposure of workers to hot environments results in physiological derangement affecting the leucocyte count of the blood, and other factors dealing with man's mechanism of defense against infection [10].

Wherever S (Equation 1) becomes strongly positive and body temperature rises progressively men will continue to work until body temperature reaches 101 to 103 F. When these body temperatures are exceeded men work with declining efficiency and are liable to heat exhaustion, heat cramps, or heat stroke.

Heat exhaustion is a circulatory failure in which the venous return to the heart is reduced so that fainting results [11]. Early symptoms of heat

exhaustion may include fatigue, headache, dizziness when erect, loss of appetite, nausea, abdominal distress, vomiting, shortness of breath, flushing of face and neck, pulse rate above 150, fever well above 102 F, glazed eyes, and mental disturbances as apathy, poor judgment, irritability and which usually precede fainting (syncope) [12]. Recovery is usually prompt when the man is removed to a cool place and kept lying down for a time, unless he has some other illness such as heart disease.

Heat cramps are painful muscle spasms in extremities, back and abdomen due, at least in part, to excessive loss of salt in sweating. Formerly common in hot industries, this manifestation of illness due to heat is now greatly reduced by drinking water containing 0.1 per cent salt, or by proper use of salt tablets. Heat cramps are readily alleviated by administration of salt solution intravenously.

Heat stroke or sun stroke is a serious effect of exposure to great heat. The body temperature climbs rapidly to excessive levels often above 105 F when for unknown reasons free sweating suddenly stops. At such high temperatures coma appears and death may be imminent. Emergency measures are required to reduce the excessive body temperature by cooling quickly to avoid irreparable damage to the brain [13].

The deleterious physiologic effects of high temperatures exert a powerful influence upon physical activity, accidents, sickness and mortality. Both laboratory and field data show that physical work in warm atmospheres is a great effort, and that production falls progressively as the temperature rises.

ACCLIMATIZATION

When men move to deserts or to jungles some adaptation to the climate takes place. If work is gradually increased day by day and if the men can get plenty of water and salt, and can sleep each night, acclimatization may be complete in 7 to 10 days. The acclimatized man works with a lower heart rate, lower skin and rectal temperature, and more stable blood pressure than when unacclimatized. The process of acclimatization requires work in the heat [12].

In recent tests made at the A.S.H.V.E. Research Laboratory [14], subjects were required to perform light work under very hot conditions for a 4-hr period each day. It was found that the ability of a new subject to endure these conditions showed daily improvement for a period of at least 2 weeks. However, after acclimatization was completed, a recess of several days had no effect on the endurance of the subject. Individuals differ widely in their capacity to acclimatize. Acclimatized men lose these capacities in a few weeks of temperate climate, even though they are vigorously active. Acclimatization to dry heat increases the capacity to sweat and conserves salt by secreting a dilute sweat [15].

Deterioration of performance and other ill effects of heat may arise during prolonged exposure to heat when men cannot get sufficient rest and sleep each day. Acclimatization to extreme conditions involves a strain upon the heat regulating system and interferes with the normal physiologic functions of the human body. Thousands of years in the heat of Africa do not seem to have acclimatized the Negro to a temperature exceeding 80 F. The same holds true of northern races with respect to cold, although the effects are mitigated by artificial control. Some persons regard the unnecessary endurance of cold as a virtue. They believe that the human organism can adapt itself to a wide range of air

TABLE 3. UPPER LIMITS OF ENVIRONMENTAL CONDITIONS FOR ACCLIMATIZED, HEALTHY, YOUNG MEN IN MILITARY SERVICE

ENVIRONMENT	REACTIONS AT THE END OF 4 HR	
	Rectal Temp F	Pulse rate
Relatively Easy	Below 101	Below 130
Difficult	101 to 102	130 to 145
Impossible	Above 102	Over 145

conditions with no apparent discomfort or injury to health. In the light of present knowledge of air conditioning these views are not justified.

The adaptive level changes somewhat with the season. There are also marked differences between the sexes. In the cold zone the thickness of thermal insulating tissues of women is almost double that of men, although the sensory responses to cold are similar. In the hot zone, the threshold of sweating is higher for women. The thickness and insulating value of the clothing worn are also important factors in the determination of the comfort level.

UPPER LIMITS OF HEAT FOR MEN AT WORK

In very hot conditions humidity is the limiting factor and the wet-bulb temperature assumes great importance. In 1905 Haldane recognized that 88 F wet-bulb was the limit of endurance for coal miners and later observers have concurred.

A study was made at the Armored Medical Research Laboratory [16] to determine the upper limits of environmental conditions under which a man can perform certain work. Thirteen enlisted men, thoroughly acclimatized to the hot conditions, served as subjects. During each test, the subjects were required to march for 4 hr at the rate of 3 mph, carrying 20 lb packs under a wide range of environmental conditions which were rated as relatively easy, difficult, and impossible, on the basis of the physiological reactions of the subjects at the end of the 4-hr period as shown in Table 3 and Fig. 3.

Recognition of the need of air conditioning for workers in hot industries is growing rapidly. The choice of the type of system to be used in

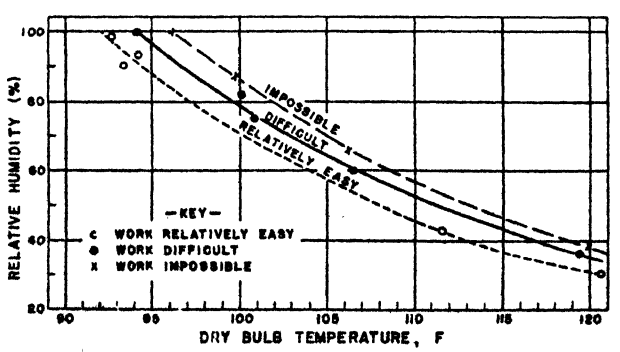

FIG. 3. HEAT ENDURANCE OF ACCLIMATIZED SUBJECTS WORKING AT A SPECIFIC RATE [16]

any given instance must be determined by the air conditioning engineer after a study of conditions. In some hot industries where few workers are engaged in large spaces the worker himself, rather than the atmosphere, can be cooled by placing him in a small booth, and blowing cooled air over him, or by circulating cooled air through a loose-fitting suit [17].

The A.S.H.V.E. Laboratory has studied the effects of walls of higher temperature than the air [14]. The findings are in part shown in Fig. 4. Mean radiant temperatures up to 40 deg above the dry-bulb did not influence physiologic processes much. For example, at 84 deg ET and 40 deg elevation in MRT, 1 deg ET change was equivalent to a 4 deg rise in MRT. Similarly, at a constant ET of 90 deg and with MRT elevations of 0 and 40 deg, 1 deg increase in ET was equivalent to 7.5 deg and 11 deg rise in MRT respectively. Under ordinary *still air* conditions the effects of air temperature and MRT appear to be interdependent. Various authorities give 0.3 to 1 deg increase of room temperature to compensate for 1 deg depression of the MRT.

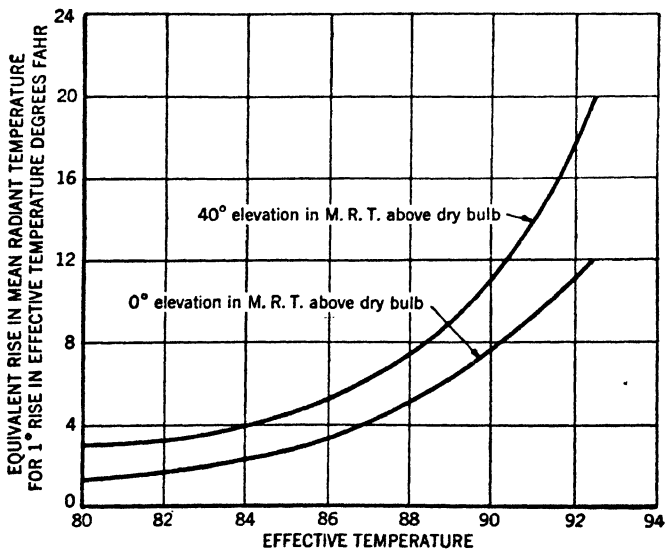

FIG. 4. EVALUATION OF EFFECT OF MRT ELEVATION IN TERMS OF EFFECTIVE TEMPERATURE

APPLICATION OF PHYSIOLOGIC PRINCIPLES TO AIR CONDITIONING PROBLEMS

In order to estimate cooling loads in occupied spaces it is necessary to know the metabolic rate (heat production) of man. This has been studied extensively and found to remain relatively constant per unit of body surface area in a subject fasting and resting quietly after a good night's sleep. The rate is high in children, and diminishes gradually with age; it increases in certain diseases and in the presence of fever. The metabolic rate is somewhat lower in women. Heat production goes up sharply with work and varies widely in different persons doing the same work. Table 4 and Figs. 5, 6, and 7 give sufficient basic data for estimating heat production and heat loss under various conditions.

EFFECTIVE TEMPERATURE INDEX AND COMFORT ZONES

There is no precise physiologic observation by which comfort can be evaluated. Mean skin temperature offers some promise. The zone of thermal neutrality differs with clothing, season, activity, and all the other factors controlling heat production (Table 5). The comfort zone is very similar to the zone of thermal neutrality.

Sensations of warmth or cold depend, not only on the temperature of the surrounding air as registered by a dry-bulb thermometer, but also

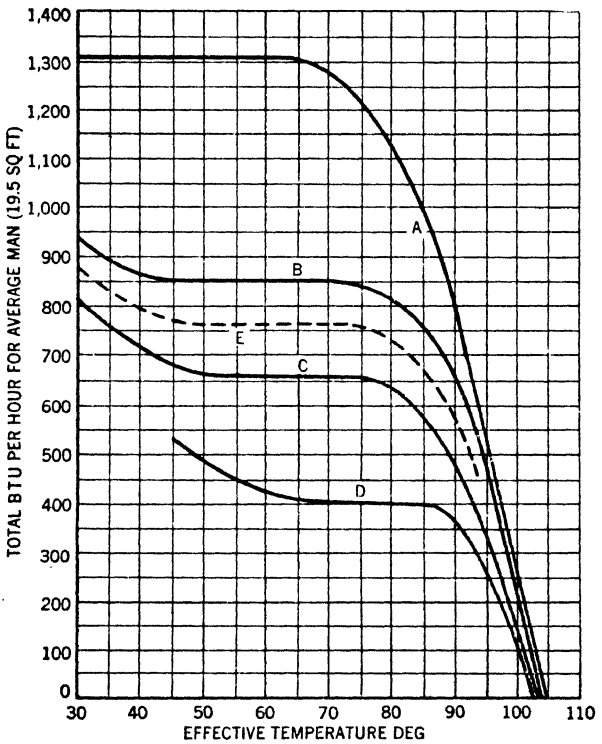

FIG. 5. RELATION BETWEEN TOTAL HEAT LOSS FROM THE HUMAN BODY AND EFFECTIVE TEMPERATURE FOR STILL AIR[a] [10]

[a]Curve *A*—Persons working, metabolic rate 1310 Btu per hour. Curve *B*—Persons working, metabolic rate 850 Btu per hour. Curve *C*—Persons working, metabolic rate 660 Btu per hour. Curve *D*—Persons seated at rest, metabolic rate of 400 Btu per hour. Curves *B* and *D* based on test data covering a wide temperature range. Curves *A* and *C* based on test data at an Effective Temperature of 70 deg and extrapolation of Curves *B* and *D*. All curves are averages of values for high and low relative humidities; variation due to humidity is small.

upon the temperature indicated by a wet-bulb thermometer, upon air movement, and upon radiation effects. Dry air at a relatively high temperature may feel cooler than air of lower temperature with a high moisture content. Air motion makes any moderate condition feel cooler. Radiation to cold or from warm surfaces is another important factor under certain conditions.

Combinations of temperature, humidity, and air movement which induce the same feeling of warmth are called thermo-equivalent conditions. A series of studies [18] at the A.S.H.V.E. Research Laboratory established the equivalent conditions for practical use. This scale of thermo-

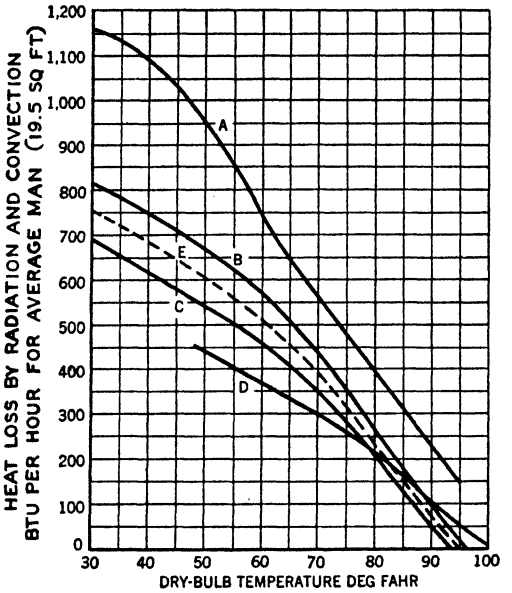

FIG. 6. RELATION BETWEEN RADIATION AND CONVECTION LOSS FROM THE HUMAN BODY AND DRY-BULB TEMPERATURE FOR STILL AIR[a 10]

[a] Loc. Cit. See footnote a, Fig. 5.

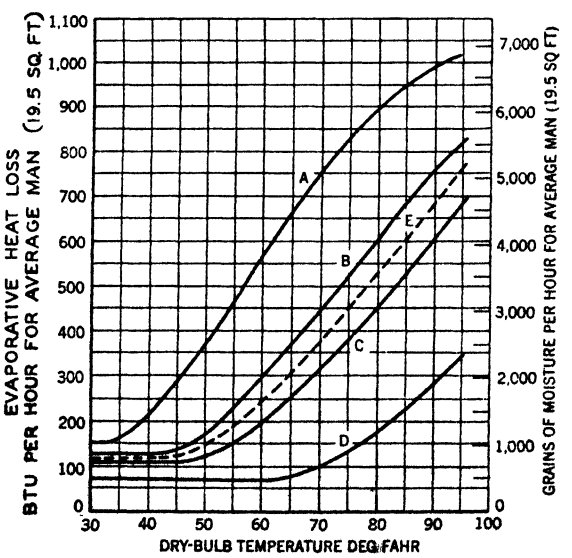

FIG. 7. EVAPORATIVE HEAT AND MOISTURE LOSS FROM THE HUMAN BODY IN RELATION TO DRY-BULB TEMPERATURE FOR STILL AIR CONDITIONS[a 10]

[a] Loc. Cit. See footnote a, Fig. 5.

TABLE 4. METABOLIC RATES OF MEN AT DIFFERENT ACTIVITIES[a]

ACTIVITY	AVG TOTAL METABOLIC RATE BTU PER HOUR
Sleeping	255
Awake, quiet	300
Seated, at rest	380
Standing, at ease	430
Walking, 2 mph	760
Walking, 4 mph	1400
Maximum Exertion	3000–4800

[a]Data were compiled from actual tests at the A.S.H.V.E. Research Laboratory and from published reports of other investigators.

equivalent conditions not only indicates the sensation of warmth, but also to a considerable degree determines the physiological *effects* on the body induced by heat or cold. For this reason, it is called the *effective temperature* scale or index, and it denotes sensory heat level.

Effective temperature is an empirically determined index of the degree of warmth perceived on exposure to different combinations of temperature, humidity, and air movement. It was determined by trained subjects who compared the relative warmth of various air conditions in two adjoining conditioned rooms by passing back and forth from one room to the other.

The numerical value of the index for any given air conditions is fixed by the temperature of slowly moving (15 to 25 fpm air movement) saturated air which induces a like sensation of warmth or cold. Thus, any air condition has an effective temperature of 60 deg, when it induces a sensation of warmth like that experienced in slowly moving air at 60 deg

TABLE 5. COMPARISON OF COMFORT RANGES WITH ZONE OF THERMAL NEUTRALITY

INVESTIGATORS	EFFECTIVE TEMPERATURE		OPERATIVE TEMP	REMARKS
	OPTIMUM LINE	RANGE	RANGE	
		Comfort Zone		
Houghten and Yaglou	66	63–71		Winter non-basal; at rest, normally clothed. Men and women.
Yaglou and Drinker	71	66–75		Summer non-basal; at rest and normally clothed. Men.
Yaglou	72.5	66–82		Entire year; non-basal; at rest and stripped to waist. Men.
Keeton et al	75	74–76		Entire year; basal, nude. Steady state (9 hr exposure). Men and women.
		Zone of Thermal Neutrality		
DuBois and Hardy	75	73.2–76.9		Basal; nude; men.
	71.8	64.8–76.0		Basal; clothed; men.
Winslow, Herrington and Gagge			84.0–87.8	Non-basal; at rest; nude; men.
			74 –84	Non-basal; at rest; clothed; men.

saturated with moisture. The *effective temperature index* cannot be measured directly but is determined from dry- and wet-bulb temperatures and air motion observations by reference to an Effective Temperature Chart (see Figs. 8, 9, and 10) or tables.

Fig. 8 gives the effective temperature for any combination of dry- and wet-bulb temperatures for *still air* (15 to 25 fpm) conditions. Charts similar to Fig. 8 for air velocities of 300 and 500 fpm have been presented in some of the earlier editions of the GUIDE. Fig. 9 is another form of

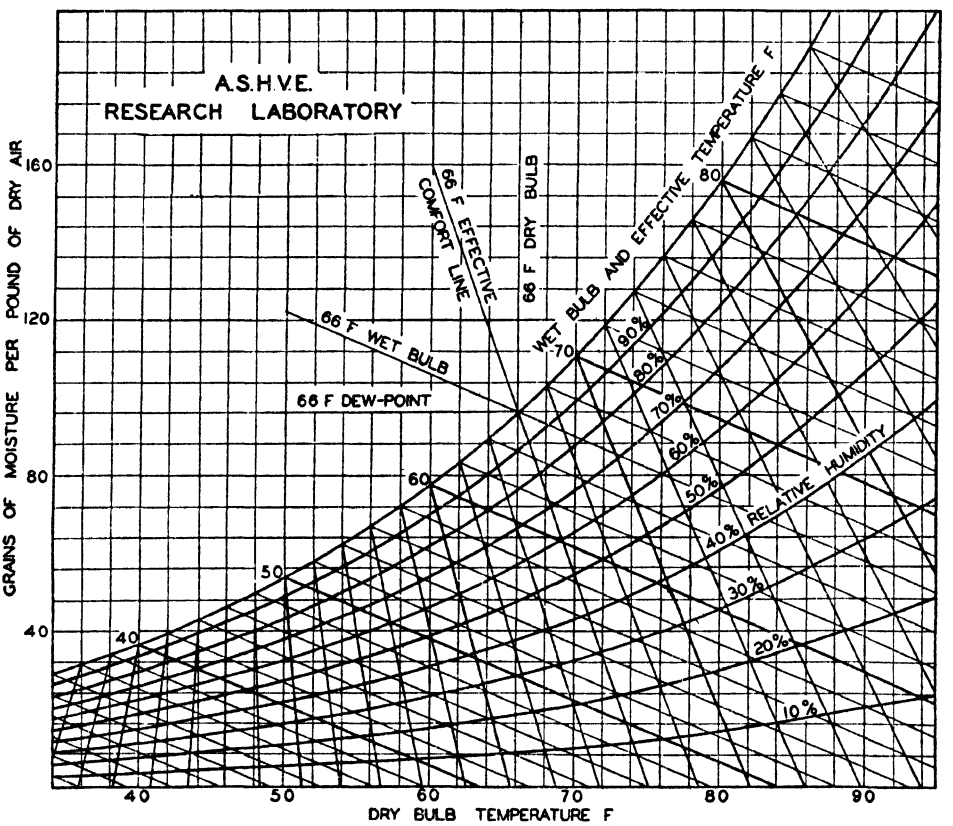

FIG. 8. PSYCHROMETRIC CHART, PERSONS AT REST, NORMALLY CLOTHED, IN STILL AIR

effective temperature chart embodying all three variables; dry-bulb and wet-bulb temperatures, and air velocity.

As stated previously, effective temperature is an index of the degree of warmth experienced by the body. An effective temperature line is, therefore, a line defining the various combinations of conditions which will induce like sensations of warmth. It does not necessarily follow that like sensations of comfort will also be experienced along the entire length of an effective temperature line. Some degree of discomfort is likely to be experienced at very high or very low relative humidities, regardless of the effective temperature. It has also been found that the optimum effective temperature varies with the season, and is lower in winter than in summer.

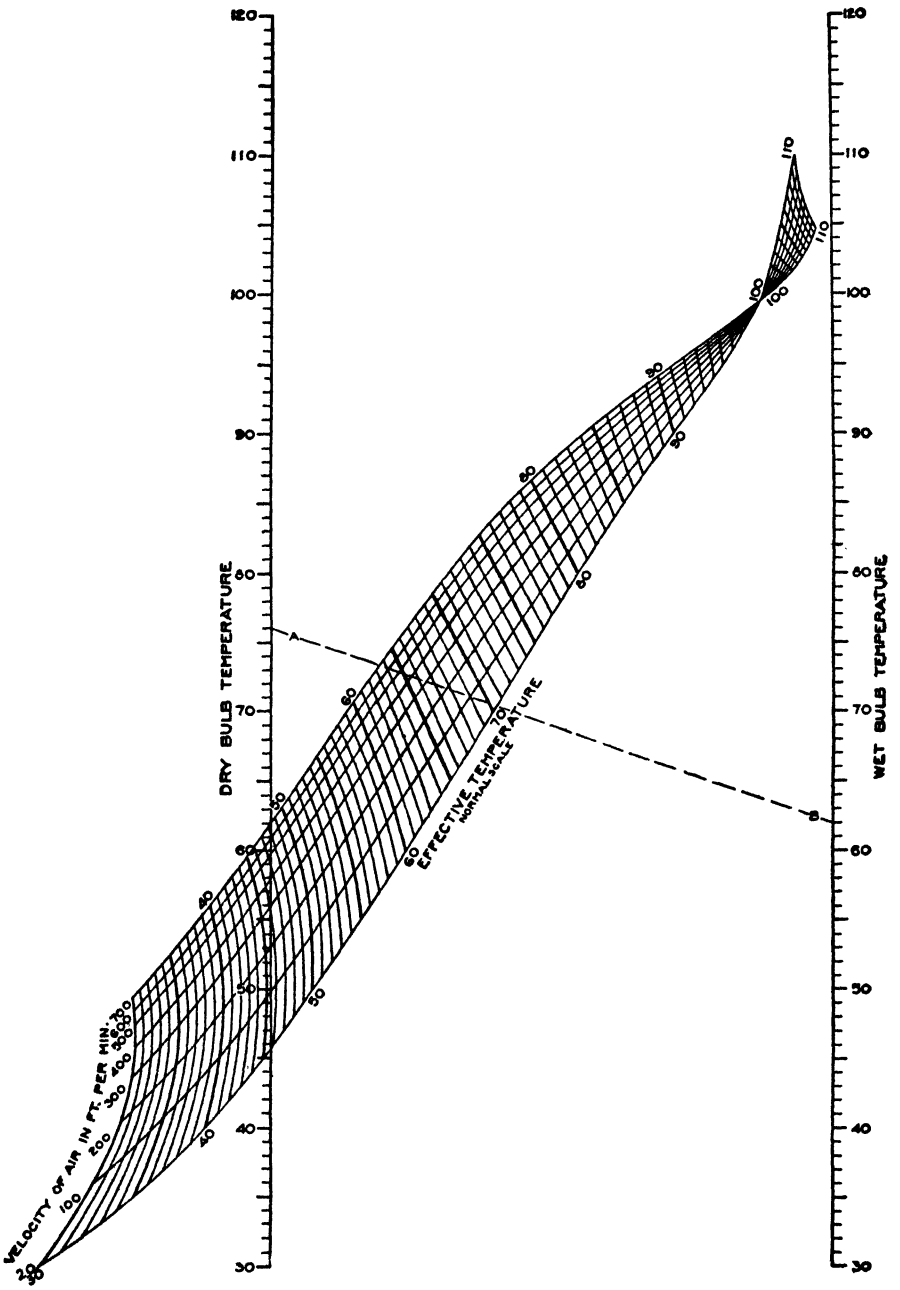

FIG. 9. EFFECTIVE TEMPERATURE CHART SHOWING NORMAL SCALE OF EFFECTIVE TEMPERATURE, APPLICABLE TO INHABITANTS OF THE UNITED STATES UNDER FOLLOWING CONDITIONS:

A. Clothing: Customary indoor clothing. *B. Activity:* Sedentary or light muscular work. *C. Heating Methods:* Convection type, *i.e.*, warm air, direct steam or hot water radiators, plenum systems.

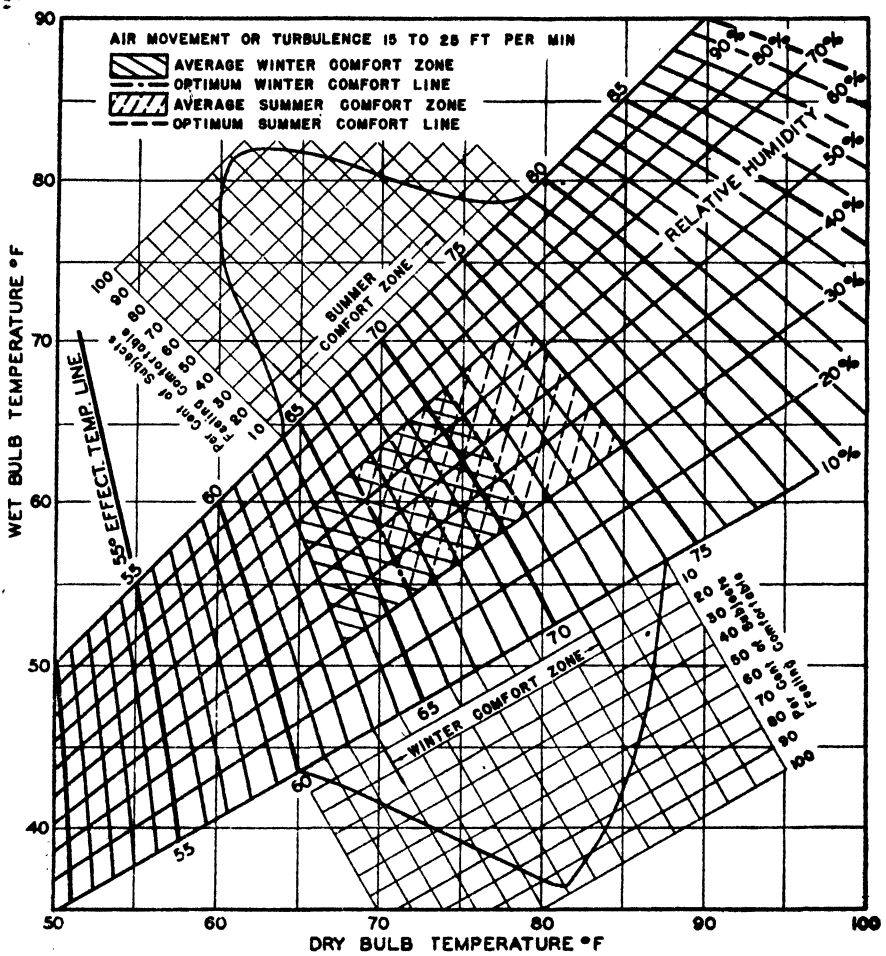

FIG. 10. A.S.H.V.E. COMFORT CHART FOR STILL AIR

Note.—Both summer and winter comfort zones apply to inhabitants of the United States only. Application of winter comfort line is further limited to rooms heated by central station systems of the convection type. The line does not apply to rooms heated by radiant methods. Application of summer comfort line is limited to homes, offices and the like, where the occupants become fully adapted to the artificial air conditions. The line does not apply to theaters, department stores, and the like where the exposure is less than 3 hours. The optimum summer comfort line shown pertains to Pittsburgh and to other cities in the northern portion of the United States and Southern Canada, and at elevations not in excess of 1000 ft above sea level. An increase of one deg ET should be made approximately per 5 deg reduction in north latitude.

Tests [10] made at the A.S.H.V.E. Research Laboratory in very hot conditions with subjects doing light work were in very close agreement with the effective temperature chart. Other work [16] under similar environmental conditions, but with subjects walking 3 mph and carrying 20 lb packs indicated that the effective temperature lines should be more nearly horizontal. It therefore appears that the slope of the ET lines may vary depending upon the rate of work being performed.

Fig. 10, shows the A.S.H.V.E. Comfort Chart [18]. The summer and winter *comfort zones* indicate conditions under which 50 per cent or more of the people are comfortable. The summer comfort zone extends from 66 ET to 75 ET; a maximum of 98 per cent of the subjects were com-

fortable at 71 ET. The winter comfort zone extends from 63 ET to 71 ET with a maximum of 97 per cent feeling comfortable at 66 ET. The 71 ET and 66 ET lines are referred to, respectively, as the summer and winter comfort lines.

The comfort zones and lines as shown in Fig. 10 are based on research prior to 1932. Later studies [19] by the A.S.H.V.E. Research Laboratory indicate a desirable winter effective temperature of 67 deg, and this finding is confirmed by current practice. The shape of the curve showing the per cent of subjects comfortable in winter also justifies this conclusion, since a drop of only one degree from the 66 ET line seriously reduced the percentage of subjects comfortable. Systems should be designed to assure comfort for the maximum possible number [20].

The comfort zones in Fig. 10 are located between the 30 per cent and 70 per cent relative humidity lines. There is some evidence that the zones could be extended somewhat beyond these limitations.

Radiation from occupants to room surfaces and between the occupants has an important bearing on the feeling of warmth and may alter to some measurable degree the optimum conditions for comfort previously indicated. Since the mean radiant temperature of a space is affected by cold walls and windows, as well as by the warm surfaces of heating units placed within the room or imbedded in the walls, these factors must be compensated. Likewise, in densely occupied spaces, such as classrooms, theaters and auditoriums, temperatures somewhat lower than those indicated by the comfort line may be desirable because of counter-radiation between the bodies of occupants in close proximity to each other. Such radiation will also elevate the mean radiant temperature of the room.

Many field studies [19] have been made to determine the optimum indoor effective temperature for both winter and summer in several metropolitan districts of the United States and Canada in cooperation with the managements of offices employing large numbers of workers (Fig. 11). On the whole women of all age groups studied prefer an effective temperature for comfort 1.0 deg higher than men. All men and women over 40 years of age prefer a temperature 1 deg ET higher than that desired by persons below this age. The persons serving in all of these studies were representative of office workers dressed for air conditioned spaces in the summer season and engaged in the customary office activity.

On the basis of present knowledge, for different geographical regions and age groups, the most popular temperature varies from a low of 66 deg ET in winter to a high of 73 deg ET in summer. The spread for summer comfort is 69 to 73 deg ET.

The A.S.H.V.E. Technical Advisory Committee on Sensations of Comfort, ascribes a spread of 3 deg in the optimum effective temperature for summer cooling to geographical location. However, it should be recognized that variations in sensation of comfort among individuals may be greater for any given location, as shown in Fig. 11, than variations due to a difference in geographical location. The available information indicates that changes in weather conditions over a period of a few days do not alter the optimum indoor temperature. In general, people experiencing low or high temperatures over an extended period of time become acclimated to lower or higher indoor temperatures respectively.

Sudden chilling (shock) of persons entering a cooled and air conditioned space during the summer months, may at times be important. It is due to the rapid evaporation of perspiration which accumulated on the skin

and in the clothing during previous subjection to hot and humid outside conditions. While studies [21] have shown that for healthy individuals this *shock* is not harmful under some conditions it may be unpleasant or even harmful. People entering and remaining in cooled spaces for short periods, 15 min or less, may be satisfied with less cooling. For long occupancy very little deviation from the optimum effective temperature is indicated.

An exit shock upon re-entering a warm atmosphere is equally plausible. Experiments at the A.S.H.V.E. Research Laboratory [22] indicated no demonstrable harm to a healthy individual. Acclimatization occurred

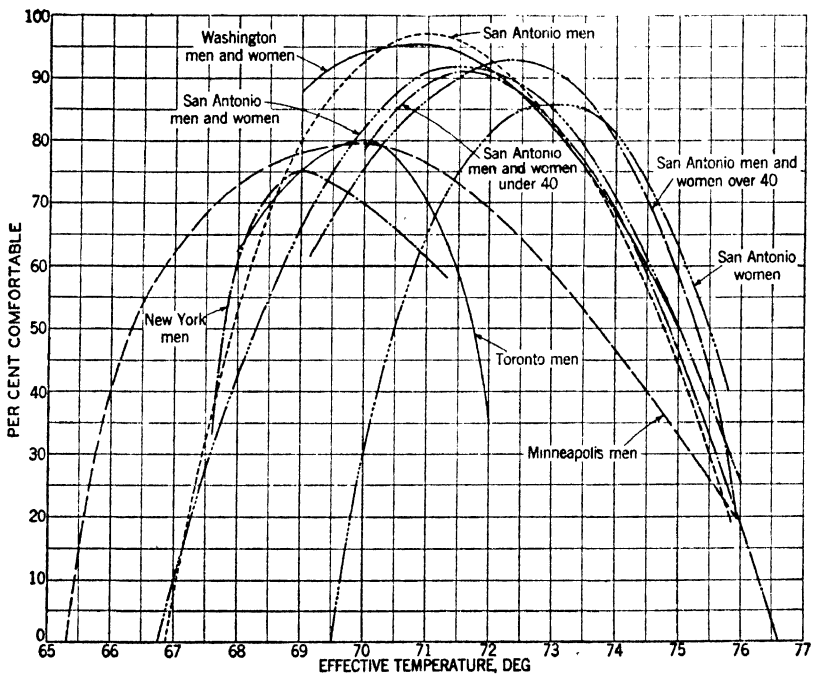

FIG. 11. RELATION BETWEEN EFFECTIVE TEMPERATURE AND PERCENTAGE OBSERVATIONS INDICATING COMFORT

as soon as normal perspiration was established. Mild exercise shortened the adaptation time.

A great number of persons seem to be fairly content in summer with a higher plane of indoor temperature. Studies by the University of Illinois [23] in cooperation with the A.S.H.V.E. Committee on Research indicate that effective temperatures as high as 74.5 deg are acceptable in the living quarters of a residence, and while this condition is not representative of optimum comfort it provides sufficient relief in hot weather to be acceptable to the majority of users, in the interest of economy. Individual differences of comfort among the minority should be counteracted by suitable clothing.

Satisfactory comfort conditions for persons at work [24] vary depending upon the rate of work and the amount of clothing worn. In general, the

greater the degree of activity, the lower the effective temperature necessary for comfort.

For prematurely born infants, the optimum temperature varies from 100 to 75 F, depending upon the stage of development. The optimum relative humidity for these infants is placed at 65 per cent [25]. No data are yet available on the optimum air conditions for full term infants and young children up to school age. Satisfactory air conditions for these age groups are assumed to vary from 75 to 68 F with natural indoor humidities. For children (having high metabolism) at school, in winter clothes, 70 F has been considered correct, while in a gymnasium 55 F has been recommended.

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Chapter 13

AIR CONDITIONING IN THE PREVENTION AND TREATMENT OF DISEASE

Control of Airborne Infection, Value of Air Cooling Under Tropical Conditions, Treatment of Disease, Operating Rooms, Nurseries for Premature Infants, Fever Therapy, Cold Therapy, Allergic Disorders, Oxygen Therapy, General Hospital Air Conditioning

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THE late war has caused an increase of interest in the preventive aspects of air conditioning. It has re-emphasized the importance of the control of airborne infection and has demonstrated the value of air cooling under tropical conditions for the prevention of heat rash, for promoting proper rest and sleep, and in the convalescence of patients.

CONTROL OF AIRBORNE INFECTION

Any program of air sanitation is influenced by a number of factors. In the winter months, the closing of doors, windows and other means of access to the outside air to conserve warmth as well as the crowding of persons indoors provides conditions conducive to a high incidence of contagion. This seasonal phenomenon, illustrated in Fig. 1 which represents a study made by the U. S. Public Health Service, will concern the ventilating engineer in so far as air quality, determined by temperature, humidity, air replenishment and type of air movement and by freedom from contamination, is a major intrinsic factor. Apart from the seasonal picture of airborne contagion are such extrinsic factors as rate of turnover of personnel and the marked susceptibility of the recruit in comparison with permanent personnel [1] as shown in Fig. 2 by studies of military personnel housed in barracks. These extraneous variables and the factor of contact infection (direct spray) tend to complicate any evaluation of the effectiveness of air sanitation for elimination of microorganisms in droplet-nuclei and droplet-dust. Thus, control measures may eliminate consistently 90 per cent of airborne organisms in laboratory tests, but cannot effect a decrease in actual incidence of infection exceeding 30 per cent. Thirty per cent may be the maximal reduction in infection possible by air treatment methods. The distinction should be clearly drawn, therefore, between the effectiveness of a procedure in laboratory tests and its effectiveness and applicability in actually reducing the incidence of airborne disease.

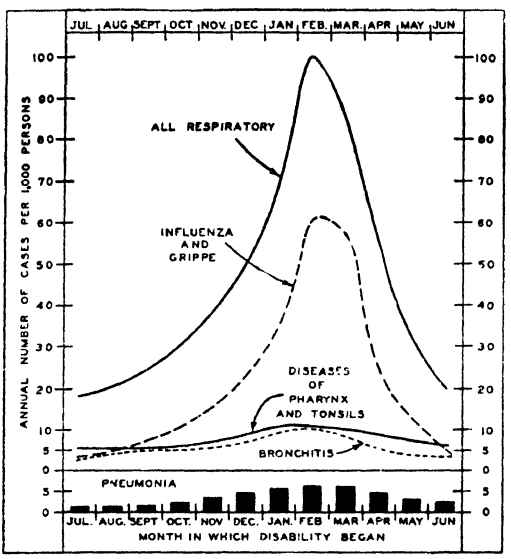
The following sequence of events has been postulated as occurring in a large proportion of intra-ward infections: (*a*) ejection of relatively large protected infective particles from patients, (*b*) rapid venting or settling of these particles so that those remaining airborne are in low concentration, (*c*) survival of infective particles to permit the accumulation of high concentrations on surfaces, (*d*) repeated reintroduction of infective particles into the air under the stimulus of ward activities or by air currents of the order of 50 fpm over the floor, and (*e*) extension of infective areas by air turbulence throughout the ward or hospital. The most important link in this probable infection chain has been demonstrated to be the reintroduction of particles into the air [2].

Intensive studies on air disinfection have indicated two distinct control

measures, (*a*) suppression of dust and lint, and (*b*) disinfection of droplet-nuclei.

Well controlled, large scale tests of the various methods of air sterilization conducted in barracks [3, 4] have confirmed the importance of dust control in minimizing the spread of airborne disease, a consideration which has guided the practices of ventilating engineers for a number of years. The importance of the dust factor has been emphasized by many engineers and has been convincingly demonstrated by subsequent bacteriologic studies aboard ships.

Treatment of floors and bedclothes with oil emulsions has proved effective in reducing bacterial dispersion by as much as 90 per cent in Army barracks and station hospitals [4]. The incidence of acute respiratory



Occurrence of diseases causing disability for 8 consecutive days or longer in a group of 100,000 wage earners (10 per cent women) in different industries.

[a]Graph obtained from Dean K. Brundage, U. S. Public Health Service.

FIG. 1. STUDY OF AVERAGE MONTHLY FREQUENCY (1921-1926 INCLUSIVE) OF SPECIFIED RESPIRATORY DISEASES[a]

infections was from 10 to 30 per cent lower in barracks with oiled floors and bedclothes than it was in control barracks which received no special treatment. More recent studies, however, have yielded inconsistent results.

No simple method for disinfecting droplet-nuclei has yet been devised. Under favorable laboratory conditions, propylene glycol in concentrations of 0.07 to 0.14 milligrams per liter, and triethylene glycol in a concentration of 0.0045 milligrams per liter were highly germicidal for most airborne bacteria in clean air when the relative humidity was between 40 and 60 per cent [5, 6, 7]. Under practical conditions, however, particularly in the presence of dust in the air, glycol effectiveness is much reduced. The use of other chemical aerosols that have been tried is limited by their toxicity, odor, or destructiveness to fabrics and metals.

Ultraviolet radiation of floors and upper air has been studied exten-

sively at the Naval Training Center, Sampson, N. Y. In barracks housing naval recruits, hospital admissions for respiratory infections (mostly *catarrhal fever*) were 25 per cent lower in a group of men exposed to ultraviolet radiation—(2537 Angstrom Units, 1 to 7 ergs per (cm ^{2}) (sec) at bed level)—than they were in adjacent control barracks without ultraviolet radiation [8]. A combination of ultraviolet radiation and dust control measures is believed to be more effective than when either one of the two is used alone, but the proof for this has yet to come.

The present status (1947) is admirably reviewed by the Committee on Sanitary Engineering of the National Research Council [9], and by a subcommittee of the American Public Health Association [10]. Both committees feel that the problem of air disinfection is still in the experimental stage, and that present evidence does not warrant the use of ultraviolet radiation or glycol vapors in public buildings and industries in the hope of reducing respiratory infections. Much more experimentation is needed for arriving at a definite conclusion.

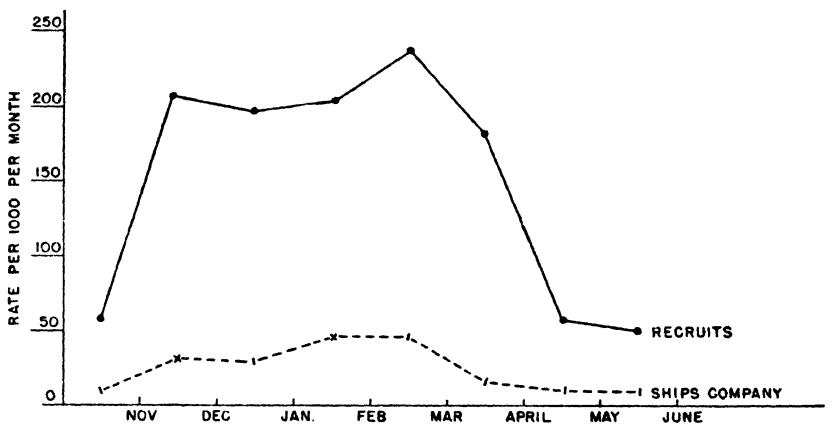


FIG. 2. MONTHLY INCIDENCE OF ACUTE RESPIRATORY ILLNESS AMONG NAVAL RECRUITS AND SHIP'S COMPANY (PERMANENT PERSONNEL) [1]

VALUE OF AIR COOLING UNDER TROPICAL CONDITIONS

The commissioning of a class of naval hospital ships with all wards, laboratories and living spaces air cooled is a notable achievement to provide better treatment of patients, especially those suffering from extensive burns, by control of environmental factors. Although statistics are not at hand to indicate the deaths or retarded recoveries of patients due to lack of air cooling in ships operating in tropical waters, it is generally agreed among competent observers that high temperature and humidity are major factors in prolonging disability and increasing mortality of the sick and injured. Physiologic data obtained on healthy men, moreover, show the large loss of body fluids and the stress on the cardiovascular system in terms of increased pulse rate when these men are continuously subjected to high temperatures. Even at rest about 50 cc of fluid per hour are lost as sweat [11] through intact skin. In burn patients the difficulty, encountered in temperate climates, of maintaining fluid and electrolyte balance is tremendously augmented by the additional evaporative fluid loss in hot environments.

Frequently from 50 to 75 per cent of personnel aboard naval vessels operating in tropical waters are afflicted with heat rash to a degree that interferes with rest and sleep. In carefully controlled experiments [11] it was possible to produce a fulminating type of rash in all men living continuously at an effective temperature of 85 (90 F dry-bulb and 83 F wet-bulb). In the control group, 12 out of 24 hr were spent in a relatively cool atmosphere of 75 ET (80 F dry-bulb, and 70 F wet-bulb). These men either remained free from heat rash or occasionally developed a mild form. Thus, intermittent cooling to a degree which prevented sweating in men at rest eliminated a serious handicap to good performance of duty.

In both laboratory tests and aboard hospital ships a relatively cool living environment of 76 to 78 ET provided an atmosphere conducive to rest and sleep without sweating. Berthing spaces tended to have extremely low odor levels. Motivation, initiative and alertness, in contrast to the usual irritability and lack of incentive incident to residence in tropical climate, were maintained [12].

Little has been done, however, to obtain practical methods for application of air conditioning under heavy heat loads and on the enormous scale that would be needed to modify life in the tropics. It is not improbable that cooled houses in a tropical climate, if used consistently for one generation, might modify the whole character of a population. The obvious advantages of part time cooling on personnel to promote rest and sleep in tropical areas would provide a prophylactic measure of great potential importance.

TREATMENT OF DISEASE

In the past few years considerable progress has been made in using air conditioning as an adjunct in the treatment of various diseases. Among the important applications are those in operating rooms, nurseries for premature infants, maternity and delivery rooms, children's wards, clinics for arthritic patients, heat therapy, cold therapy, oxygen therapy, X-ray rooms, the control of allergic disorders, and for the physiological effects in industry.

OPERATING ROOMS

The widest application of air conditioning in hospitals is in operating rooms. Complete air conditioning of operating wards is important because winter humidification helps reduce the danger of anesthetic gases; summer cooling with some dehumidification is needed to eliminate excessive fatigue and to protect the patient and operating personnel; and finally, filtering aids the removal of allergens from the operating room air.

Reducing Explosion Hazard

Explosion hazards in operating rooms began with the introduction of modern anesthetic gases and apparatus. Ether administered by the old drop method gives rise to an explosive mixture, but in practice this method is still regarded as comparatively safe. When ether is mixed with pure oxygen, or nitrous oxide in certain concentrations, the explosion hazard may be as great as with ethylene-oxygen, or cyclopropane-oxygen mixtures.

Of the anesthetic gases nitrous oxide alone does not explode but supports combustion. Ether, vinyl ether, ethylene, and cyclopropane are as potentially dangerous as gasoline or illuminating gas in the home [13].

Chloroform does not explode violently in contact with flame but decomposes to liberate phosgene. All of the anesthetic gases and vapors except ethylene are heavier than air. Although the incidence of injury or death from explosion is negligible compared with other hazards in the operating room, the dramatic features surrounding an explosion justify continued investigation to eliminate the hazard.

During the course of ethylene anesthesia, the mixture, usually 80 per cent ethylene and 20 per cent oxygen, is so rich that the danger of explosion is slight in the immediate vicinity of the face mask, but leakage of ethylene into the air may accumulate to any lower concentration, and thus introduce a serious hazard. The most dangerous period is at the end of the operation when the patient's lungs and the anesthesia apparatus are customarily *washed out* with oxygen with or without the addition of carbon dioxide. Even when this procedure is omitted, it is difficult in practice to avoid dilution of the anesthetic gas with air during the normal course of breathing following the administration. In either case the mixture would pass through the explosion range and extraordinary precaution is necessary for the safety of the patient and operating personnel.

In a study [14] of 230 anesthetic explosions and fires, 70 per cent of the explosions and 60 per cent of the deaths were caused by igniting agents other then static sparks. In 1941 the *National Fire Protection Association* [15] made certain recommendations for safe practice based on available information. Some of these recommendations are:

Windows should be kept closed so that the air conditioning system can prevent pooling of explosive anesthetic gases. Twelve air changes per hour and a humidity of 55 per cent are advised. If a higher humidity were compatible with the well being of the patient and personnel, it should be maintained. All electrical installations should comply with the standards set by the *National Electrical Code* for use in explosive situations. Cautery equipment should not be used in hazardous locations. To prevent static sparks, all bodies in an operating room should be conductive or coupled. It is essential that adequate grounding be provided for the floor and every object in the operating room. Conductive rubber should be used on shoes, leg tips, operating table coverings and all rubber parts of the anesthesia equipment. All furniture in contact with the floor should be metal. In the absence of complete grounding facilities, the simple method of intercoupling patient, operating table, anesthetist and gas machine at ground potential may be used.

Experience has shown that neither high humidity nor intercoupling devices have eliminated the danger from static electric discharge. The removal of gas concentrations from the operating table area by means of specially devised exhaust ventilation should be thoroughly tested. Portable duct systems as installed aboard ship should be acceptable. Serious explosions can occur in a closed system but proper precautions will reduce this hazard to a minimum.

It should be realized that when a room and the occupants have been completely grounded there is always the possibility that the patient or the operator might receive a dangerous shock if a short circuit developed in any of the electrical equipment.

A comprehensive study of the explosion problem and of the general causes and prevention of operating room hazards by the *University of Pittsburgh*, the A.S.H.V.E. Research Laboratory, and the *U. S. Bureau of Mines* has led to a fruitful attempt to eliminate the explosive range of

cyclopropane, one of the best but most difficult gases to handle. The use of helium as a diluent in the total gaseous mixture controls the oxygen concentration by displacement and, because of its flame quenching properties, it is the ideal gas for this purpose. In addition, a gaseous mixture containing helium is more difficult to ignite by electric discharges and this quality also increases the safety factor of anesthetic administration.

Operating Room Conditions

Little is known about optimum air conditions for maintaining normal body temperatures during anesthesia and the immediate post-operative period. An anesthetized patient displays dilation of blood vessels in the skin resulting in profuse sweating and (it has been believed) inability to regulate body temperature. From this it was concluded that all anesthetized patients suffered considerable heat loss, although there may be little more than 0.8 F variation in the rectal temperature during the course of the operation [16]. The severe physiological effects, such as excessive sweating and rapid pulse, of high operating room temperatures on attendants and patients during the hot months signify the need for proper cooling. A comparison of surgeons' statements who operate in both air conditioned and non-air conditioned rooms strongly indicates that the recuperative power of the patient is greater when operated upon in air conditioned rooms [16].

Although the comfortable air conditions for the operators are not identical with those for the patient, it is usually not difficult to compromise within a range of 55 to 60 per cent relative humidity and 72 to 80 F temperature. The work just cited reported that 68 to 70 F effective temperature not only furnished comfort for the operating room workers, but apparently prevented exhaustion of the patient as evidenced by rapid convalescence in the recovery ward. Additional heat may be furnished to the patient locally or by suitable covering according to body temperature in individual cases.

In the control of airborne infection in the operating room the prevention of dispersal of infectious materials into the air, control of dust and proper ventilation supersede attempts to remove or kill pathogenic organisms. The bacterial content of conditioned operating rooms is generally lower than that of non-conditioned rooms.

Bacterial counts aboard an air conditioned submarine were found to be exceptionally low and not cumulative with time although all of the air was recirculated for more than 12 hours [17] without replenishment. The removal of bacteria by the process of air cooling and condensation of moisture out of air merits further study [18].

The degree of air contamination can be reduced by proper ventilation if velocity of air over the floor does not exceed 50 fpm. Research is in progress on the use of filtered air flowing through a system of mechanical cleaners which protect the patient against infection from attendants and from bacteria-containing air in the corridor or ward [19].

Operations may be postponed on allergic patients during asthmatic manifestations through fear of complications. The removal of air-borne allergens, therefore, is in some cases an important function of the air conditioning system in preparing patients for operation.

Central system air conditioning plants and unit air conditioners prove satisfactory in operating rooms when producing between 8 and 12 air changes per hour of filtered and properly conditioned air without recirculation during the course of anesthesia. A separate exhaust fan system is

usually necessary to confine and remove the gases and odors. Double windows are desirable and often necessary to prevent condensation and frosting on the glass in cold weather and to minimize drafts. The air flow of 8 to 12 air changes in operating rooms should: (1) reduce the concentration of the anesthetic to well below the pharmacologic threshold in the vicinity of the operating personnel, (2) remove the great amounts of heat and sometimes moisture, from sterilizing equipment if inside the operating room, from the powerful surgical lights, from solar heat, and from the bodies of the operatives, and (3) provide extra capacity for quickly preparing the room for emergency operations. Much can be gained by thermal insulation of sterilizing equipment and by thorough exhaust ventilation of sterilizing rooms adjoining the operating rooms.

Too great a difference in temperature between the operating room and the final hospital destination of the patient, including corridors and elevators, is conducive to infections of the upper part of the respiratory tract and post-operative pneumonia. A suggested remedy is a recovery ward in which conditions closely approximate those of the operating room and in which the patients remain from one to four days. Satisfactory conditions in the recovery ward not only hasten convalescence, but dispel the fear frequently found in patients who must undergo operations during the hot seasons.

Experience has shown that a few hours after the operation the temperature of the post-operative room can be decreased a few degrees below that of an overheated operating room to stimulate recovery.

NURSERIES FOR PREMATURE INFANTS

One of the most important requirements in the care of premature infants is the stabilization of body temperature. This is necessary because their heat regulating systems are not fully developed; the metabolism is low and the infants generally exhibit marked inability to maintain normal body temperatures. The resistance to infection is low and mortality rate high.

Air Conditioning Requirements

The optimum air conditions for growth and development of premature infants were determined by extensive research [20] at the Children's Hospital, Boston, Mass., using four valid criteria, namely, stability of body temperature, gain in weight, incidence of digestive syndromes, and mortality. Individual temperature requirements varied widely (from 72 to 100 F) according to the constitutional state of the infants and body weights. The optimum relative humidity was about 65 per cent, and the air movement less than 20 fpm.

A single nursery conditioned to 77 F and 65 per cent relative humidity was found to fulfill satisfactorily the requirements of the majority of premature infants. Additional heat for weak (or debilitated) infants may be furnished in the cribs or by means of electric incubators placed inside the conditioned nursery, and the temperature adjusted according to individual requirements. In this way multiplicity of chambers and of air conditioning apparatus is obviated; the infants in the heated beds derive the benefit of breathing cool humid air, and the nurses and doctors need not expose themselves to extreme conditions.

Importance of Humidity: Although external heat is an important factor in the maintenance of normal body temperature, humidity appears

to be of equal or greater importance. When the premature nurseries at the Children's Hospital were kept at relative humidity between 25 and 50 per cent for two weeks or longer, the body temperature became unstable, gain in weight diminished, the incidence of gastro-intestinal disturbances increased, and the mortality rose. On the other hand, continuous exposure to air conditions with 55 to 65 per cent relative humidity gave satisfactory results over a period of years. The initial physiologic loss of body weight (loss occurring within first four days of life) was found to vary inversely with the humidity. In the old nurseries with natural humidity it averaged 12.4 per cent of the birth weight; in the conditioned nurseries it was 8.9 per cent with 25 to 49 per cent relative humidity, and 6.0 per cent with 50 to 75 per cent relative humidity. The number of days required to regain the birth weight was correspondingly maximum in the old nursery and minimum in the conditioned nurseries under high humidity.

Maximum gains in body weight occurred in the conditioned nurseries under high humidity (55 to 65 per cent) in infants weighing less than 5 lb. The gains were less under low humidity (25 to 50 per cent) in the same nurseries, and in the old nurseries prior to the installation of air conditioning apparatus.

The incidence and severity of digestive syndromes, with diarrhea, persistent vomiting, diminishing gain or loss of body weight, and other symptoms, were generally from two to three times as high under low as under high humidity.

Summarizing, the best chances for life in premature infants are created by maintaining a relative humidity of 65 per cent in the nursery and by providing a uniform environmental temperature just sufficiently high to keep the body temperature within normal limits. Medical and nursing care are, of course, factors of equal and sometimes of greater importance.

Air Conditioning Equipment

Many of the installations now in use are of the central system type providing for filtration, for humidification and heating in cold weather, and for cooling and dehumidification in hot weather. A ventilation rate, between 8 and 12 air changes, is desirable to remove odors and maintain uniformity of temperatures in extremes of weather. Recirculation should not be used in these wards owing to odors and the possibility of infection. There should be a frequent change in spray water.

Control of Airborne Infection

The protection of the premature and older infant against infection is of the utmost importance. It was found in one installation equipped with air conditioning, germicidal lights and mechanical barriers that air conditioning alone did not prevent the spread of respiratory cross-infections. Bactericidal ultraviolet light barriers and air conditioning or mechanical barriers and air conditioning were efficient[21].

FEVER THERAPY

Artificial production of fever in man is an imitation of nature's way of overcoming invading pathogenic organisms. The action may be direct and specific by destruction of the invading organism within the safe limit of human temperatures, or indirect in the case of heat resistant

organisms, by general mobilization of the defensive mechanisms of the body, which retard or neutralize the activity of pathogenic bacteria and their toxins.

Although the action may be direct and specific by destruction of the invading organisms within the safe human limits, fever therapy exerts much of its benefit through the improvement of the mechanism of bodily defense. A serious challenge to the theory on which fever therapy is based comes from the demonstration that high fever causes a reduction in the concentration of circulating antibodies in experimental animals. Clinically, it has been shown that there is no change in the per cent of phagocytes which engulf bacteria in patients during fever therapy, although the action of the complement fixing antibodies may be temporarily diminished.

Patients for fever therapy should be carefully selected. The most serious complications which may arise are heat stroke, heat exhaustion and circulatory collapse. The chief minor complications are spasm, heat cramps, fever blisters and mild dehydration.

The limits of induced systemic fever are usually between 104 and 107 F (rectal), and the duration from 3 to 8 hours at a time. The total period of fever treatment varies with the type of the organism involved from a few hours to 50 or more.

The diseases which respond favorably to artificial fever therapy are gonorrhea and its complications (which include arthritis, pelvic infections in women, and involvement of the eye), syphilis, chorea, infectious arthritis (non-gonorrheal), encephalitis, and some forms of asthma. There are other conditions which show promise under this treatment; but the most striking results are seen in gonorrhea and syphilis, since the causative organisms can be destroyed at temperatures compatible with human life.

Equipment for Production of Fever

Artificial fever can be induced by injections of various crystalloid or colloid substances, bacterial products of typhoid and malarial organisms, or by physical methods using hot baths, radiant heat cabinets, hot humidified air cabinets, or by short wave diathermy in combination with a cabinet.

The relative advantages of various methods have been evaluated clinically [22]. Among the devices for the production of fever by physical means, the one most widely used is the hot humid air or *air conditioned* cabinet. This apparatus was developed at the Kettering Institute for Medical Research at Miami Valley Hospital in Dayton, Ohio.

In the earlier studies of the Society, temperatures were elevated more easily using saturated atmospheres. A fever therapy apparatus [23] using these same principles has proved efficient as a means of inducing and maintaining fever in a body with small likelihood of burns because of the comparatively low dry-bulb temperatures.

When heat is necessary in treating legs or arms, such media as short or long wave diathermy, infrared, water baths, etc. have been used extensively. A recent development, a saturated atmosphere heating unit, similar to one previously described has proven satisfactory, because heat may be administered over longer periods which render deep heating possible without fear of burns or shocks. Local heating has been somewhat satisfactory in relieving the painful symptoms of peripheral vascular disease. Some investigators employ short wave diathermy within the

cabinet during the induction phase. When the desired body temperature has been reached by electrical induction, the atmosphere of the enclosure is kept at saturation to prevent heat loss, thus maintaining the patient's temperature at the desired point. The two underlying principles in the production of fever by the hot, humid air cabinet are: (1) the transfer of heat by conduction from the circulating hot air to the body and (2) prevention of heat loss. The latter is more important. In an atmosphere of high humidity, the heat loss by evaporation is markedly decreased.

COLD THERAPY

In contrast to fever therapy the use of cold as a means of anesthesia and treatment is of established importance. Refrigeration anesthesia is being more widely used and the advantages of the method claimed by Allen have been completely confirmed [24].

It has been demonstrated that the cooling of limbs and other parts with ice-water or ice, cracked or pulverized, down to near the freezing point (5 C or 40 F) is harmless. Freezing must be avoided. There is a temporary retardation or suspension of life, with resumption of cellular activity as the temperature returns to normal. A human limb can remain bloodless and anesthetic below a tourniquet for at least 8 hr and perhaps up to 48 hr without injury, while the rest of the body remains warm. Where amputation is indicated it can thus be done without pain, loss of blood or strength and also without shock. There is no apparent interference with the subsequent healing of the stump. Refrigeration anesthesia is of importance not only in amputation but also in the control of hemorrhage, pain, infection and shock during the transportation of patients with traumatized limbs.

Apart from the advantages of cold in amputations, cryotherapy has been beneficial in the treatment of burns and arterial obstruction, and essential in the treatment of frostbite and immersion foot. It has been used successfully for dental anesthesia. The principle of hibernation in which the body as a whole is cooled for as much as five days in air temperatures between 50 to 60 F and applied to such conditions as morphine addiction, leukemia, and schizophrenia continues to be experimental. Prolonged cold therapy which keeps the body temperature below 95 F depresses the vital processes and is fraught with danger.

The methods used for refrigeration depending upon available facilities are as follows [24]:

(1) Cracked or shaved ice which is simple and has the advantage of not freezing tissues. However, it is cumbersome and sloppy to handle and is unsuited to prolonged treatments.

(2) Use of ice in a pail for immersion of local parts.

(3) Special boxes for holding ice with padded or curtained openings for the limb.

(4) Bare ice bags and cloth bags for iced wet dressings for prolonged treatments and convenience.

(5) A double chambered cabinet using dry ice has been constructed.

(6) Electrical refrigerating apparatus, consisting of a compact noiseless unit that pumps fluid to various types of applications, is available. The applicators may be in the form of blankets containing rubber tubes suitable for covering the entire body or all or part of a limb. Special applicators are available for insertion into various body cavities and for inducing dental anesthesia.

(7) An air chamber at regulated temperature for treatments of frostbite and immersion foot, and amputation stumps.

The electrical apparatus is costly but has the advantages of thermostatic regulation, light weight, freedom of movement, and permits prolonged treatments with heat as well as cold over the range of temperatures therapeutically desirable.

ALLERGIC DISORDERS

Although there is some division of opinion over the ultimate cause of allergy, the prevailing belief is that it is due to an inherited or acquired hypersensitiveness to pollen or other foreign proteins in certain individuals who react abnormally to the offending substance. The reaction may be induced by inhalation, eating, or absorption (through the skin) of the allergens. Some of the clinical manifestations are hay fever, asthma, eczema, and contact dermatitis.

Symptoms of Hay Fever and Asthma

The respiratory tract is the usual site of allergic manifestations, *e.g.* hay fever and asthma. In hay fever, the nose and eyes are red and itchy, and there is considerable discharge. Nasal obstruction is the most common and distressing symptom. The severity of the symptoms varies widely from day to day depending chiefly on the amount of pollen in the air.

Seasonal asthma comes in attacks. The most popular theory concerning the mechanism of action is that the offending substance irritates the nerve endings in mucous membranes of the respiratory tract, causing spasmodic contraction of the small bronchioles of the lungs, which interferes with breathing, particularly with expiration. Non-seasonal allergic disturbances are sometimes attributed to house or street dusts, fungi, odors, animal dander, irritating gases, and heat or cold, particularly sudden temperature changes. It is often stated in the literature that heat regulation in asthmatic individuals tends to be unstable, with a tendency toward the subnormal. Many allergic cases who are apparently well develop their attacks when cold weather appears, or upon changing from warm to cool outdoor air.

Air Conditioning Apparatus

In recent years considerable effort has been directed toward the elimination of the principal cause of allergy from the air of enclosures by filtration or other air conditioning processes capable of removing pollens, in the hope of providing relief to individuals who fail to respond to medical treatment (desensitization or immunization).

Paper or cloth filters, mounted in inexpensive window or floor units, prove quite satisfactory in many cases, but since dust and smoke frequently cause asthmatic attacks, it is desirable that an air filter, to be of full value in the treatment of asthma, should remove all possible dusts and pollens regardless of size or amount. Electrostatic air cleaners are more efficient than most commonly used types for capturing very fine dust.

Although the chief remedial factor in the treatment by conditioned air is the filtration of pollen, a certain amount of cooling and dehumidification appears to be desirable. A comfortable temperature between 70 and 75 F and a relative humidity well below 50 per cent proved satisfactory[25]. Direct drafts, overcooling or overheating are apt to initiate or aggravate the symptoms.

Limitations of Air Conditioning Methods

The results obtained with air filtration or other air conditioning processes in the control of allergic conditions are fairly comparable to those obtained by desensitization treatment so long as the patients remain in the pollen free atmosphere. But while specific desensitization is preventive and in a few instances curative, for all practical purposes filtration gives only temporary relief. In mild cases sleeping in an air conditioned space may make it possible for the individual to pass more comfortable days. With rare exceptions, the symptoms recur on exposure to pollen laden air. Moreover the usefulness of air conditioning methods is limited because all cases are not caused by air-borne substances. Cases of bacterial asthma do not respond to treatment with filtered air.

Despite these limitations air conditioning methods possess definite advantages in the simplicity of treatment, convenience, and under certain conditions almost immediate relief [26]. Pollen cases are usually relieved of most of their symptoms within 1 to 3 hr after exposure to properly filtered air. A pollen-free atmosphere is especially valuable when desensitization has given little or no relief, and when desensitization is not advisable owing to intercurrent illness.

OXYGEN THERAPY

Oxygen therapy is the principal measure employed for preventing and relieving the distressing symptoms of anoxemia, which is a deficiency in the oxygen content of the blood. Some of the more important conditions in which oxygen treatment is believed to be beneficial are pneumonias, anemia, heart affections, post-operative pulmonary disturbances, certain mental disturbances, asphyxia, asthma and atelectasis in new-born infants.

The effectiveness of oxygen therapy depends upon the manner of administration. Three common methods, catheter, face mask or tent [27] are employed.

The necessity of air conditioning in oxygen therapy arises from the fact that oxygen is too expensive a gas to waste in the ventilation of oxygen tents and oxygen chambers. The oxygen rich atmosphere in these enclosures is therefore reconditioned in a closed circuit by removal of excess heat, moisture, and carbon dioxide given off from the occupants being treated.

Oxygen Tents

In oxygen tents the air enriched with oxygen is usually circulated by means of a small motor blower which sends the air over soda lime to remove carbon dioxide and then over ice to remove excess heat and moisture. The concentration of oxygen in the tent is regulated by means of a pressure reducing valve and flow meter. In an inadequately cooled tent, high temperatures and humidities are inevitable, increasing the discomfort of the patient and imposing an added strain on an already overburdened heart. Oxygen therapy under such conditions may do more harm than good. An ice melting rate of approximately 10 lb per hour gives satisfactory results in patients with fever in a medium size oxygen tent.

Oxygen tents are confining to the patient. They may terrify the restless and delirious patient. Medical and nursing care is complicated, as the tent must be opened or removed with attendant loss of oxygen.

Oxygen concentrations of 50 per cent or more are difficult to maintain, and it is a problem to keep the temperature and humidity low enough in hot weather. However, with attention to details, the patient can be made quite comfortable.

Oxygen Chambers

The conventional oxygen chamber is an air-tight sheet metal enclosure of fire-proof construction, large enough to accommodate one or two patients. Trap doors or curtains are provided for the personnel, food and service, to avoid loss of oxygen. Glass windows in the ceiling and walls admit light from outside the chamber. The air conditioning system may be of the gravity type, or of the fan type using mechanical refrigeration or air drying agents.

The temperature and humidity requirement in oxygen therapy depends primarily upon the physical condition of the patient, and secondarily upon the type of disease. In pneumonias[28] prescribed conditions should be a temperature of 60 to 75 F, humidity 20-50 per cent, moderate air movement, oxygen concentration of 50 per cent, and carbon dioxide of less than one per cent.

Oxygen in Aviation

An important application of the principle of oxygen therapy is in aviation. At the present time all high altitude military airplanes in this country are provided with gaseous oxygen equipment and military personnel are required to utilize oxygen at all times while in flight above 15,000 ft, or between 12,000 to 15,000 ft for longer than two hours, or between 10,000 to 12,000 ft for longer than six hours. The use of oxygen in commercial aviation will depend on the height and duration of the flights as well as the state of health of the passengers. The necessity for portable, comfortable equipment, the possible fire hazards due to smoking, and the use of oxygen on sleeper planes are some of the difficulties facing civil airline operators. The pressure cabin airplane is a solution to the problem.

GENERAL HOSPITAL AIR CONDITIONING

Complete conditioning of a large hospital involves a capital investment and running expenses which may not be justified. In clean and quiet districts, the requirements of almost all general and private wards during the cool season of the year can be satisfactorily fulfilled by the use of conventional heating equipment in conjunction with window air supply and gravity or mechanical exhaust. Insulation against heat and sound is much more important than humidification in winter; it will also help in keeping the building cool in warm weather. Excessive outside noise and dust may require the use of silencers and air filters in the openings.

Cooling and dehumidification in warm weather are important. In new hospitals particularly, the desirability of cooling certain sections of the building should be given serious consideration. Financial reasons may preclude the cooling of the entire building, but the needs of the average hospital can be met by the use of built-in room coolers and a few portable units which can be wheeled from ward to ward when needed.

In the North and certain sections of the Pacific Coast, cooling is needed but a few days during summer, while in the South, it can be used to advantage from May to October, and in tropical climates almost continuously throughout the year.

Aside from comfort and recuperative power of the patients, cooling is of great assistance in the treatment of fevers in the new-born and in post-operative cases, in enteric disorders, fevers, heat stroke, heart failure, and in a variety of other ailments which often accompany summer heat waves.

Problem of Odors

The evacuation of battle casualties in aircraft and their subsequent hospitalization have stimulated efforts to minimize odors arising from draining wounds, old odorous casts, and gangrenous wounds. For aircraft, chemical sprays and vapors, perfumes, oxidizing gases and ventilation methods are unsatisfactory. An ideal deodorant would purify the air by means of odor adsorption so that subsequently the air can be recirculated. Based upon the effectiveness of activated carbon commercially and industrially to adsorb odors, individual adsorption units have been used successfully. In hospital wards the question of superiority of adsorption methods for elimination of odors over other methods remains to be answered. The present status of the problem is that the commercial aspect is highly controversial.

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Chapter 14

HEATING LOAD

General Procedure, Design Outdoor Weather Conditions, Inside Temperatures, Attic Temperatures, Temperatures in Unheated Spaces, Ground Temperatures, Basement Temperatures and Heat Loss, Transmission Heat Loss, Infiltration Loss, Selection of Wind Velocities, Auxiliary Heat Sources, Intermittently Heated Buildings, Residence Heat Loss Problems

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IN the design of a heating system, an estimate must be made of the maximum probable heat loss of each room or space to be heated, based on maintaining a specified inside air temperature during periods of design outdoor weather conditions. The heat losses may be divided into two groups, namely (1) the transmission losses or heat losses through the confining walls, floor, ceiling, glass or other surfaces and (2) the infiltration losses or heat losses due to air leakage through cracks and crevices, around doors and windows, opening of doors and windows or heat required by outside air used for ventilation.

GENERAL PROCEDURE

The general procedure for calculating heat losses of a structure is:

1. Select the design outdoor weather conditions: temperature, wind direction and wind velocity. The data on climatic conditions given in Table 1 and the isotherms of average design temperature in Fig. 1 will be useful but should be applied with judgment as suggested in the section Design Outdoor Weather Conditions.

2. Select the inside air temperature, at the 60-in. breathing line or the 30-in. line which is to be maintained in the building during the coldest weather. (See Table 2).

3. Estimate temperatures in adjacent unheated spaces and the attic. The attic temperature need not be estimated if the combined roof and ceiling coefficient is used.

4. Select or compute the heat transmission coefficients for outside walls and glass; also for inside walls, floors, or top-floor ceilings, if these are next to unheated space; include roof if next to heated space. (See Chapter 6).

5. Measure amount of net outside wall, glass and roof next to heated spaces, as well as any cold walls, floors or ceilings next to unheated space. Such measurements are made from building plans, or from the actual building, using inside dimensions.

6. Compute the heat transmission losses for each kind of wall, glass, floor, ceiling and roof in the building by multiplying the heat transmission coefficient in each case by the area of the surface in square feet and the temperature difference between the inside and outside air. (See Items 1, 2, and 3).

7. Select unit values and compute the heat equivalent of the infiltration of cold air taking place around outside doors and windows. These unit values depend on the kind or width of crack, wind velocity, and the temperature difference between the inside and outside air; the result expresses the heat required to warm up the cold air leaking into the building per hour. (See Chapter 8).

8. When mechanical exhaust fans are used and the replacement air is drawn from outside the heat required to raise this air to room temperature is added to the infiltration loss. If the mechanically exhausted air quantity is equal to, or greater than, the natural infiltration rate, the infiltration loss should be disregarded.

9. The sum of the heat losses by transmission (Item 6) through the outside wall and glass, as well as through any cold floors, ceilings or roof, plus the heat equivalent (Item 7) of the cold air entering by infiltration, or required to replace mechanical exhaust, represents the total heat loss equivalent for any building.

DESIGN OUTDOOR WEATHER CONDITIONS

There are no hard and fast rules for selecting the design outdoor weather conditions to be used for a given locality or type of building or heating system,

and the problem is to some extent a matter of judgment and experience. The outside design temperature is seldom taken as the lowest temperature, or even the lowest daily mean temperature ever recorded in a given locality. Such temperatures are rarely repeated in successive years. Likewise the wind direction and velocity prevailing at the time of design outside conditions frequently are entirely different from those prevailing during the winter season.

The A.S.H.V.E. Technical Advisory Committee on Weather Design Conditions has recommended the adoption for heating load calculations of an *outside design temperature which is equalled or exceeded during 97½ percent of the hours in December, January, February and March.*

Complete data of this nature is not available but Column 7, Table 1, lists this recommended design temperature based on airport station readings for the period indicated, generally a five year period 1935-1939 inclusive. It is pointed out that in most cases these stations are outside of the city and that these data would apply primarily to rural areas. A comparison of the lowest recorded temperatures, with due regard to the period of record, makes it possible to determine an equivalent design temperature for city stations. In general the use of the airport data for buildings within an adjacent city will not make any appreciable difference in design load.

The calculation of these design temperatures is being carried on but due to the extensive amount of work involved will not be completed for some time. It should also be noted that the period of record for the stations listed occurred in what is known as a warm cycle and when longer periods are used it is expected that many of these design temperatures will be somewhat lower.

Because of the limited data available, design temperatures in common use are listed in Column 9. Many of these values were furnished by A.S.H.V.E. members—the balance were taken from an ACRMA Bulletin[1], manufacturers' publications and other sources[2], and a few were estimated. The map, Fig. 1, shows isotherms approximated for these design temperatures. They may be used as a guide for localities not listed in the table. Interpolation between these lines is suggested and due consideration must be given to elevations and other local conditions.

Column 8 of the table gives the maximum wind velocity which occurred with temperatures the same as, and lower than, those shown in Column 7. Winter average velocities for all temperatures are given in Column 10.

Column 6 lists the average annual minimum temperature which is the average of readings of the one lowest temperature occurring for each year the station has been in existence. It is of interest as a guide to the lowest temperature to be encountered except for an occasional extreme of short duration.

Finally, large differences in climate occur within relatively small distances of Weather Bureau stations in hilly and mountainous regions. The designer must use experience and judgment to deal properly with this factor.

INSIDE TEMPERATURES

The inside air temperature which must be maintained within a building is understood to be the dry-bulb temperature at the breathing line, 5 ft above the floor, or the 30-in. line, and not less than 3 ft from the outside walls. Inside air temperatures, usually specified, vary in accordance

TABLE 1. WINTER CLIMATIC CONDITIONS[a]

COL. 1 STATE	COL. 2 STATION[b]	COL. 3 ELEVATION[c] FT	COL. 4 PERIOD OF RECORD[d]	COL. 5 LOWEST TEMP. ON RECORD[d] °F	COL. 6 Average ANNUAL MIN. TEMP.[e] °F	COL. 7 DESIGN DRY-BULB TEMP. ON TAC 97½% BASIS[f] °F	COL. 8 WIND VEL. AT DESIGN TEMP.[g] MPH	COL. 9 DESIGN DRY-BULB TEMP. IN COMMON USE[h] °F	COL. 10 AVG. WIND VEL.-DEC. JAN.-FEB.[i] MPH
Ala.	Anniston CO	733	1893-1947	−10				5	
	Birmingham CO	711	1893-1945	−10	12			10	8.0
	Birmingham AP	615	1939-1947	−10		21	7.4		
	Mobile CO	143	1872-1947	−1	22			15	9.9
	Mobile AP	219	1940-1947	13		30	8.5		
	Montgomery CO	293	1872-1947	−5				10	7.5
	Montgomery AP	226	1938-1944	9					
Ariz.	Flagstaff CO	6957	1899-1947	−25	−15			−10	7.7
	Kingman AP	3473	1935-1939[d]			22	8.6		
	Phoenix CO	1122	1895-1947	16	26			25	5.3
	Phoenix AP	1112	1937-1947	21		31	5.6		
	Tucson CO		Up to 1946	6				25	5.2
	Tucson AP	2561	1935-1939[d]			30	6.3		
	Winslow CO	4853	Up to 1946	−19				−10	
	Winslow AP	4899	1932-1947	−18		6	7.5		
	Yuma CO	146	1876-1946[d]	22				30	6.7
Ark.	Fort Smith CO	545	1882-1945	−15	6			10	8.1
	Fort Smith AP	463	1945-1947	7					
	Little Rock CO	451	1879-1942	−12	10			5	8.3
	Little Rock AP	282	1942-1947	7		21	6.6		
Cal.	Bakersfield AP	499	1937-1946[d]	23		33	5.6	25	
	Burbank AP	740	1931-1947	21		35	4.9		
	Daggett AP	1925	1935-1939[d]			27	8.5		
	Eureka CO	115	1886-1947	20				30	7.3
	Fresno CO	387	1887-1939	17				25	5.4
	Fresno AP	281	1939-1947	23		32	4.5		
	Los Angeles CO	534	1877-1947	28	37			35	6.3
	Oakland AP	21	1929-1947	23		36	7.5	30	
	Red Bluff CO	341[e]	1877-1934	17					6.0
	Red Bluff AP	346	1944-1947	25					
	Redding AP	579	1935-1939[d]	17		32	7.1		
	Sacramento CO	116	1877-1947	17				30	7.2
	Sacramento AP	22	1938-1947	22					
	San Diego CO	90	1871-1940	25				35	6.3
	San Diego AP	34	1939-1947	34		43	5.8		
	San Francisco CO	62	1875-1947	27	37			35	7.5
	San Jose CO	100[e]	Up to 1946	22				25	
	Williams AP	124	1935-1939[d]			29	8.3		
Col.	Denver CO	5398	1871-1947	−29	−11			−10	7.6
	Denver AP	5379	1934-1947	−30		0	8.8		
	Grand Junction CO	4587[e]	1889-1945[d]	−21	−2			−15	4.4
	Pueblo CO	4770	1889-1938[d]	−27				−20	8.0
	Pueblo AP	4810	1939-1947	−26		2	6.4		
Conn.	Hartford CO	229	1905-1940	−18				0	8.9
	Hartford AP	20	1940-1947	−24		4	8.3		
	New Haven CO	180	1872-1946[d]	−15	−1			0	9.4
	New Haven AP	17	1943-1947	−4		11	8.1		
D of C.	Washington CO	128	1871-1947	−15	−1			0	7.9
	Washington AP	20	1935-1939[d]			14	7.4		
Fla.	Apalachicola CO	23	1922-1947	18				25	8.4
	Jacksonville CO	104	1871-1947	10	29			25	9.1
	Jacksonville AP	29	1938-1947	16		31	7.0		
	Key West CO	23	1871-1947	42				45	10.6
	Key West AP	48	1939-1947	42					
	Miami CO	253	1896-1947	27				35	9.8
	Miami AP	13	1940-1947	28		45	7.3		
	Pensacola CO	67	1879-1947	7				20	11.2
	Pensacola AP	113	1943-1947	20					
	Tampa CO	111	1890-1940[d]	19				30	8.5
	Tampa AP	12	1941-1946	31					
	Titusville AP	52	1935-1939[d]			38	6.5		
Ga.	Atlanta AP	1020	1878-1945[d]	−8	12	22	10.2	10	11.7
	Augusta CO	195	1871-1946[d]	3				10	6.5
	Augusta AP	424	1939-1947	10					
	Macon CO	408	1899-1947	7				15	6.6
	Macon AP	432	1939-1947	8					
	Savannah CO	115	1871-1945	8	22			20	9.6
	Savannah AP	56	1939-1947	16		29	7.7		
Idaho	Boise CO	2818	1864-1939[d]	−28				−10	9.1
	Boise AP	2849	1939-1947	−13		5	4.5		
	Burley AP	4150	1935-1939[d]			2	8.8		
	Idaho Falls AP	4744	1935-1939[d]			−7	7.6		
	Lewiston CO	763	1900-1944	−23	1			5	4.1
	Pocatello CO	4522	1899-1947	−28	−12			−5	9.5
	Pocatello AP	4467	1938-1947	−23		6	7.2		
Ill.	Cairo CO	319	1872-1947	−16				0	9.9
	Chicago CO	601[e]	Up to 1946	−23	−8			−10	12.0
	Chicago AP	615	1935-1939[d]			−3	11.7		
	Moline AP	594	1935-1939[d]			−6	10.8	−10	
	Peoria AP	660	1935-1939[d]			6	10.7	−10	8.1

Blank spaces indicate data not yet completed.

TABLE 1. WINTER CLIMATIC CONDITIONS[a]—(CONTINUED)

Col. 1 State	Col. 2 Station[b]	Col. 3 Elevation[c] ft	Col. 4 Period of Record[d]	Col. 5 Lowest Temp. on Record[d] °F	Col. 6 Average Annual Min. Temp.[e] °F	Col. 7 Design Dry-Bulb Temp. on TAC 97½% Basis[f] °F	Col. 8 Wind Vel. at Design Temp.[g] Mph	Col. 9 Design Dry-Bulb Temp. in Common Use[h] °F	Col. 10 Avg. Wind Vel.-Dec. Jan.-Feb.[i] Mph
Ill.	Springfield CO	603	1879-1947	−24	−7			−10	11.8
	Springfield AP	608	1930-1947	−19		−2	11.6		
Ind.	Evansville CO	464	1897-1940	−16	1				9.7
	Fort Wayne CO	885	1911-1941	−24				−10	10.3
	Helmer AP	970	1935-1939[d]			−1	11.5		
	Indianapolis CO	816	1871-1946[d]	−25	−6			−10	11.3
	Indianapolis AP	800	1932-1946[d]	−18		2	11.4		
	Terre Haute CO	1146	1893-1946[d]	−18					10.2
	Terre Haute AP	589		−11					
Iowa	Charles City CO	1023	1891-1945[d]	−34					7.9
	Davenport CO	648	1872-1947	−27				−15	10.5
	Des Moines CO	805	1878-1945[d]	−30				−15	10.1
	Des Moines AP	979	1935-1939[d]			−8	14.5		
	Dubuque CO	740	1874-1947	−32	−17			−20	7.1
	Keokuk CO	637	1871-1945[d]	−27					8.3
	Sioux City CO	1093[e]	1889-1944	−35	−20			−20	11.6
	Sioux City AP	1098	1940-1946[d]	−24					
Kansas	Concordia CO	1425	1885-1947	−25	−13			−10	7.7
	Dodge City CO	2515	1942-1947	−26	−10			−10	10.5
	Dodge City AP	2599	1874-1942	−26					
	Topeka CO	991	1887-1947	−25				−10	9.6
	Topeka AP	883	1946-1947	−21					
	Wichita CO	1497	1888-1939	−22				−10	12.2
	Wichita AP	1423	1939-1947	−10		6	14.7		
Ky.	Louisville CO	563	1871-1947	−20	−5			0	9.9
	Louisville AP	544	1937-1947	−15		9	8.8		
La.	New Orleans CO	85	1874-1947	7	26			20	8.6
	New Orleans AP	8	1937-1947	19		36	12.8		
	Shreveport AP	179	1935-1939[d]		16	27	8.9	20	8.8
Maine	Eastport CO	100	1873-1947	−23	−15			−10	12.5
	Portland CO	69	1885-1940	−21	−6			−5	10.4
	Portland AP	65	1940-1947	−39					
Md.	Baltimore CO	114	1871-1947	−7	8			0	8.1
	Baltimore AP	43	1935-1939[d]			13	8.9		
Mass.	Boston CO	356	1870-1935[d]	−18	−3			0	12.4
	Boston AP	45	1936-1947	−14		8	12.3		
	Nantucket CO	45	1886-1947	−6				0	14.8
	Nantucket AP	48	1946-1947	12					
Mich.	Alpena CO	615	Up to 1946	−28	−12			−10	11.0
	Detroit CO	1000	1873-1933	−24	−11			10	12.0
	Detroit AP	632	1935-1939[d]			4j	11.0		
	Escanaba CO	645	1878-1945[d]	−32				−15	9.3
	Grand Rapids CO	706	1891-1946[d]	−24				−10	11.9
	Lansing CO	861	1910-1947	−25				−10	10.0
	Lansing AP	863	1940-1947	−10					
	Marquette CO	721	1874-1947	−27	−13			−10	10.7
	Sault St. Marie CO	724[e]	1888-1942[d]	−37				−20	8.9
Minn.	Duluth CO	1133	1874-1947	−41	−28			−25	13.4
	Duluth AP	1413	1941-1947	−33					
	Minneapolis CO	945	1890-1947	−34	−23			−20	11.3
	Minneapolis AP	873	1938-1947	−31					
	St. Paul CO	951	1871-1933	−41				−20	9.5
	St. Paul AP	708	1937-1947	−26		−15	9.9		
Miss.	Meridian CO	410	1889-1947	−6				10	5.7
	Meridian AP	298	1939-1947	−7					
	Vicksburg CO	316	1874-1947	−1	18			10	8.3
	Vicksburg AP	266	1941-1947	10					
Mo.	Columbia CO	739	1889-1947	−26				−10	8.9
	Columbia AP	787	1939-1947	−18					
	Kansas City CO	741[e]	1889-1940	−22				−10	10.2
	Kansas City AP	780	1935-1939[d]			2	10.6		
	St. Louis CO	646	1871-1947	−22	−2			0	11.7
	St. Louis AP	597	1930-1947	−19		3	10.8		
	Springfield AP	1270	1935-1939[d]		−5	8	11.0		10.9
Mont.	Billings AP	3584	1935-1939[d]		−30	−17	9.1	−25	12.4
	Butte CO	5700*	1894-1931	−34				−20	
	Butte AP	5538	1931-1947	−52		−18	4.8		
	Havre CO	2498	1880-1947	−57	−36			−30	9.4
	Helena CO	4175[e]	1880-1940[d]	−42				−20	7.3
	Kalispell CO	3004	1897-1947	−34				−20	5.2
	Miles City CO	2400	1892-1942[d]	−49				−35	5.6
	Miles City AP	2629[e]	1935-1939[d]			−18	8.4		
Neb.	Lincoln CO	1189	1887-1947	−29	−13			−10	10.6
	Lincoln AP	1185	1933-1947	−26		−2	12.7		
	North Platte CO	2815	1874-1947	−35	−17			−20	8.3
	North Platte AP	2788	1935-1939[d]			−9	10.7		
	Omaha CO	1219	1873-1935	−32				−10	9.6
	Omaha AP	1009	1935-Pres.	−21		−8	11.5		
	Valentine CO	2627	1889-1947	−38				−25	9.3

*Approximate value.

TABLE 1. WINTER CLIMATIC CONDITIONS[a]—(CONTINUED)

Col. 1 State	Col. 2 Station[b]	Col. 3 Elevation[c] ft	Col. 4 Period of Record[d]	Col. 5 Lowest Temp on Record[d] °F	Col. 6 Average Annual Min. Temp.[e] °F	Col. 7 Design Dry-Bulb Temp. on TAC 97½% Basis[f] °F	Col. 8 Wind Vel. at Design Temp.[g] Mph	Col. 9 Design Dry-Bulb Temp. in Common Use[h] °F	Col. 10 Avg. Wind Vel.-Dec. Jan.-Feb.[i] Mph
Nev.	Elko AP	5079	1935-1939[d]			−4	4.0		
	Las Vegas AP	1882	1937-1947	8		23	5.3		
	Reno CO	4588	1905-1942	−19				−5	6.0
	Reno AP	4417	1940-1947	−16		7	3.6		
	Winnemucca CO	4293	1871-1947	−36	−10			−15	8.1
N. H.	Concord CO	343	1871-1941	−35	−15			−15	6.0
	Concord AP	359	1941-1947	−37					
N. J.	Atlantic City CO	45	1874-1947	−9	6			5	15.9
	Camden AP	20	1935-1939[d]			12	9.5		
	Newark AP	15	1931-1947	−14		10	11.6	0	
	Sandy Hook CO	19	1914-1938[d]	−11				0	16.1
	Trenton CO	144	1866-1946	−14				0	11.0
N. M.	Albuquerque CO	5022	1931-1933	5				0	7.3
	Albuquerque AP	5319	1933-1947	−6		16	7.1		
	El Morro AP	7120	1935-1939[d]			−6	4.6		
	Rodeo AP	4116	1935-1939[d]			25	8.4		
	Roswell CO	3643	1905-1947	−29				−10	7.1
	Tucumcari AP	4054	1935-1939[d]			13	9.2		
N. Y.	Albany CO	114	1874-1947	−24	−11			−10	10.4
	Albany AP	280	1938-1947	−22		0	9.6		
	Binghamton CO	915	1891-1946	−28				−10	6.8
	Binghamton AP	836	1942-1947	−17					
	Buffalo CO	693[c]	1873-1945[d]	−20	−4			−5	17.1
	Buffalo AP	726	1935-1939[d]			3	14.0		
	Canton CO	458	1889-1947	−43				−25	10.6
	Elmira AP	948	1935-1939[d]			5	8.0		
	Ithaca CO	888	1879-1947	−24				−15	11.3
	New York CO	425	1871-1947	−14	−3			0	16.8
	Oswego CO	363	1871-1943	−23				−10	12.3
	Rochester CO	609	1872-1947	−22				−5	10.1
	Rochester AP	560	1935-1939[d]	−16		4	11.9		
	Syracuse CO	465	1928-1940	−24				−10	11.3
	Syracuse AP	404	1940-1947	−26		−1	8.9		
N. C.	Asheville CO	2280	1902-1947	−6				0	9.5
	Charlotte CO	809	1878-1947	−5				10	7.3
	Charlotte AP	757	1939-1947	−3		22	7.5		
	Greensboro AP	896	1928-1947	−7		17	7.8	10	
	Raleigh CO	405	1944-1947	−2	13			10	7.8
	Raleigh AP	446	1935-1939[d]			20	8.5		
	Wilmington CO	78	1871-1947	5	18			15	8.1
N. D.	Bismarck CO	1675	1875-1940	−45	−31			−30	9.1
	Bismarck AP	1655	1940-1947	−38		−24	7.1		
	Devils Lake CO	1481	1904-1947	−46	−33			−30	10.1
	Dickinson AP	2599	1935-1939[d]			−20	12.4		
	Fargo AP	900	1935-1939[d]			−25	10.9	−25	
	Pembina AP	830	1935-1939[d]			−30	11.9		
	Williston CO	1919	1879-1947	−50				−35	8.4
Ohio	Akron CO		1887-1931[d]	−20				−5	
	Akron AP	104	1935-1939[d]			9	10.6		
	Cincinnati CO	772	1870-1947	−17				0	8.5
	Cincinnati AP	488	1931-1947	−14		7	8.0		
	Cleveland CO	669	1871-1946[d]	−17	−2			0	15.0
	Cleveland AP	813	1940-1946[d]	−5		6	13.8		
	Columbus CO	812	1878-1946[d]	−20				−10	11.6
	Columbus AP	820	1939-1947	−15	−3	4	10.5		
	Dayton CO	1086	1883-1943	−28				0	10.9
	Dayton AP	1002	1940-1947	−11					
	Sandusky CO	608	1878-1946[d]	−16				0	11.0
	Toledo CO	668	1871-1947	−16				−10	12.1
	Toledo AP	626	1940-1947	−13		4	12.1		
Okla.	Ardmore AP	762	1935-1939[d]			18	9.7		
	Oklahoma City CO	1264	1890-1947	−17	2			0	11.5
	Oklahoma City AP	1311	1939-1947	−10		14	14.7		
	Tulsa AP	686	1932-1947	−5		13	11.3	0	
	Waynoka AP	1529	1935-1939[d]			10	11.3		
Ore.	Arlington AP	881	1935-1939[d]			7	7.8		
	Baker CO	3501	1889-1947	−25	−17			−5	5.9
	Baker AP	3374	1939-1947	−19		3	6.4		
	Eugene CO	366	1890-1942[d]	−4				15	
	Eugene AP	368	1942-1947	9		23	5.3		
	Medford CO	1428[c]	1911-1929	−10				5	4.3
	Medford AP	1343	1929-1947	−3		23	4.3		
	Portland CO	98	1874-1947	−2	18			10	7.3
	Portland AP	25	1940-1947	3		22	8.0		
	Roseburg CO	523	1877-1947	−6				10	3.9
Pa.	Curwensville AP	2219	1943-1947	−10		0	13.5		
	Erie CO	771	1873-1946	−16				−5	13.6
	Erie AP	736	1935-1939[d]			6	12.1		
	Harrisburg CO	335[c]	1888-1938[d]	−14				0	7.9
	Harrisburg AP	339	1935-1939[d]			7	9.0		

TABLE 1. WINTER CLIMATIC CONDITIONS[a]—(CONTINUED)

Col. 1 State	Col. 2 Station[b]	Col. 3 Elevation[c] ft	Col. 4 Period of Record[d]	Col. 5 Lowest Temp. on Record[d] °F	Col. 6 Average Annual Min. Temp.[e] °F	Col. 7 Design Dry-Bulb Temp. on TAC 97½% Basis[f] °F	Col. 8 Wind Vel. at Design Temp.[g] Mph	Col. 9 Design Dry-Bulb Temp. in Common Use[h] °F	Col. 10 Avg. Wind Vel.-Dec. Jan.-Feb.[i] Mph
Pa.	Philadelphia CO	200	1871-1947	−11	6			0	11.0
	Philadelphia AP	18	1940-1947	1					
	Pittsburgh CO	929	1875-1947	−20	−2			0	11.7
	Pittsburgh AP	1284	1935-1947	−16		6	12.1		
	Reading CO	311	1913-1947	−14				0	9.1
	Scranton CO	877	1901-1947	−19				−5	7.6
	Sunbury AP	448	1935-1939[d]			7	7.1		
R. I.	Block Island CO	46	1881-1947	−10				0	18.0
	Providence CO	77	1904-1947	−17	1			0	12.1
S. C.	Charleston CO	59	1871-1947	7	22			15	10.5
	Charleston AP	51	1940-1947	14		26	6.9		
	Columbia CO	401	1887-1947	−2	19			10	8.1
	Columbia AP	227	1939-1947	9					
	Greenville CO	1006[e]	Up to 1946	−5				10	8.4
S. D.	Huron CO	1342	1881-1938	−43	−26			−20	10.6
	Huron AP	1287	1938-1947	−30					
	Rapid City CO	3309	1888-1947	−34	−21			−20	7.8
	Rapid City AP	3220	1939-1947	−27					
Tenn.	Chattanooga CO	952	1879-1947	−10				10	7.6
	Chattanooga AP	675	1940-1947	6		19	6.2		
	Knoxville CO	1024	1871-1942	−16	2			0	7.2
	Knoxville AP	1007	1942-1947	1					
	Memphis CO	348	1872-1941	−9	9			0	9.3
	Memphis AP	267	1941-1947	1		19	8.9		
	Nashville CO	714	1871-1947	−13				0	9.8
	Nashville AP	610	1939-1947	−15		14	7.3		
Texas	Abilene CO	1748	1885-1944	−6				15	10.1
	Abilene AP	1756	1940-1947	−9		20	10.4	−5	
	Amarillo CO	3686	1892-1941	−16				−10	12.1
	Amarillo AP	3595	1941-1947	−7		11	12.9		
	Austin CO	625	1897-1942	−1				20	8.0
	Austin AP	625	1942-1947	13					
	Brownsville CO	140	1922-1943	12				30	10.2
	Brownsville AP	25	1943-1947	30					
	Corpus Christi CO	21	1887-1942[d]	11				20	11.0
	Corpus Christi AP	45	1943-1946[d]	23					
	Dallas CO	732	1913-1940	−3				0	10.6
	Dallas AP	520	1940-1947	5		23	8.8		
	Del Rio CO	1020	1905-1947	12				15	7.9
	El Paso CO	3792	1880-1942	−5	16			10	8.9
	El Paso AP	3956	1939-1947	11		26	8.6		
	Fort Worth CO	708	1898-1939[d]	−8	12			10	10.4
	Fort Worth AP	728	1940-1947	4					
	Galveston CO	128	1871-1947	8				20	11.2
	Galveston AP	9	1939-1947	14					
	Houston CO	198	1888-1947	5				20	10.5
	Houston AP	73	1932-1947	5		33	9.2		
	Palestine CO	555	1881-1947	−6				15	8.0
	Port Arthur CO	64	1917-1947	11				20	10.5
	Port Arthur AP	21	1944-1947	24					
	San Antonio CO	770[e]	1885-1941	4	21			20	8.3
	San Antonio AP	800	1942-1947	17		32	7.6		
	Waco AP	513	1931-1947	7		26	11.6		
	Wink AP	2811	1935-1939[d]			23	8.5		
Utah	Milford AP	5095	1935-1939[d]			−2	7.7		
	Modena CO	5472	1901-1947	−32	−15			−15	9.3
	Salt Lake City CO	4346	1874-1947	−20	2			−10	7.9
	Salt Lake City AP	4254	1928-1947	−30		7	7.4		
Vt.	Burlington CO	409	1884-1943	−29	−17			−10	11.7
	Burlington AP	335	1943-1944	−23					
Va.	Cape Henry CO	24	1874-1947	5				10	13.1
	Lynchburg CO	644	1874-1944	−7	8			5	8.1
	Lynchburg AP	951	1944-1947	7					
	Norfolk CO	91	1871-1947	2	15			15	10.1
	Richmond CO	180	1897-1947	−3	10			15	8.1
	Richmond AP	172	1929-1947	−12		15	7.1		
	Roanoke AP	1194	1935-1939[d]			21	8.2		
Wash.	Ellensburg AP	1731	1935-1939[d]			1	3.8		
	North Head CO	199	1884-1947	11				20	16.3
	Seattle CO	104	1890-1947	3	20			15	9.7
	Seattle AP	47	1928-1947	3		24	6.3		
	Spokane CO	2030	1881-1941	−30	−5			−15	6.2
	Spokane AP	1974	1941-1947	−7		4	5.1		
	Tacoma CO	279	1897-1947	7				15	7.9
	Tatoosh Is. CO	110	1883-1947	7				15	19.9
	Yakima CO	1160	1938-1946	−15				−5	4.1
	Yakima AP	1066	1944-1947	−4					
W. Va.	Elkins CO	1969[e]	1898-1944	−28	−8			−10	6.1
	Parkersburg CO	685	1888-1947	−27	−1			−10	7.1

TABLE 1. WINTER CLIMATIC CONDITIONS[a]—(CONCLUDED)

Col. 1 State	Col. 2 Station[b]	Col. 3 Elevation[c] Ft	Col. 4 Period of Record[d]	Col. 5 Lowest Temp. on Record[d] °F	Col. 6 Average Annual Min. Temp.[e] °F	Col. 7 Design Dry-Bulb Temp. on TAC 97½% Basis[f] °F	Col. 8 Wind Vel. at Design Temp.[g] Mph	Col. 9 Design Dry-Bulb Temp. in Common Use[h] °F	Col. 10 Avg. Wind Vel.-Dec. Jan.-Feb.[i] Mph
Wisc.	Green Bay CO	598	1886-1947	−36	−18			−20	10.6
	La Crosse CO	725	1872-1947	−43	−21			−25	8.9
	La Crosse AP	677	1943-1947	−28		−17	6.9		
	Madison CO	1008	1858-1947	−29				−15	10.1
	Madison AP	884	1935-1939[d]			−8	9.1		
	Milwaukee CO	744	1870-1947	−25	−12			−15	12.1
	Milwaukee AP	707	1927-1947	−29		−6	11.9		
Wyo.	Cheyenne CO	6144	1873-1935	−38				15	13.3
	Cheyenne AP	6161	1935-1947	−34		−3	11.1		
	Lander CO	5448	1891-1946	−40	−12			−18	3.9
	Lander AP	5568	1946-1947	−14					
	Rock Springs AP	6746	1932-1942	−33		−7	9.1		
Alta.	Edmonton	2219[c]	Up to 1943	−57	−41			−40	7.5
B. C.	Vancouver	22[c]	Up to 1943	2	13			10	4.5
	Victoria	228[c]	Up to 1943	−2	19			5	12.6
Man.	Winnipeg	786[c]	Up to 1943	−54	−38			−35	10.1
N. B.	Fredericton	164[c]	Up to 1943	−35	−25			−20	9.1
N. S.	Yarmouth	136[c]	Up to 1943	−12	0			−5	14.3
Ont.	London	912[c]	Up to 1943	−27	−14			−5	10.3
	Ottawa	294[c]	Up to 1943	−35	−24			−20	8.4
	Port Arthur	644[c]	Up to 1943	−40	−29			−30	8.0
	Toronto	379[c]	Up to 1943	−26	−11			−10	13.6
P. E. I.	Charlottetown	186[c]	Up to 1943	−27	−13			−10	9.8
Que.	Montreal	187[c]	Up to 1943	−29	−18			−15	11.3
	Quebec	296[c]	Up to 1943	−34	−23			−20	13.3
Sask.	Prince Albert	1414[c]	Up to 1943	−70	−47			−45	5.1
Y. T.	Dawson	1062[c]	Up to 1943	−68	−54			−45	3.7
Newf.	St. Johns	428[c]	Up to 1943	−21	−5			−10	12

[a] United States Data compiled from U. S. Weather Bureau Records for years indicated, and Canadian data from Meteorological Service of Canada corrected to 1946.

[b] Col. 2. The stations followed by letters AP are airport stations, all others are city office stations and are followed by letters CO.

[c] Col. 3. The elevations marked c are ground elevations of the station. All other elevations given are the actual elevations of the thermometer bulb above mean sea level.

[d] Col. 4. The periods of record indicated apply only to the lowest temperature ever recorded shown in Col. 5, and generally extend from a summer month of the first year indicated through the spring months of the last year indicated. The periods marked by d terminated in December of the year indicated.

[e] Average of readings of one lowest temperature obtained for each year.

[f] It should be noted that Col. 7 applies only to airports, as these data for city stations are not available at this time. The temperature shown is the minimum hourly out-door temperature which has been equalled or exceeded 97½ per cent of the total hours in December, January and February for the period of record. It is pointed out that in most cases the airport stations are outside of the city and these data would apply primarily to rural areas.

[g] Col. 8 indicates the average wind velocity which occurred at temperatures the same as, and lower, than the temperatures shown in Col. 7.

[h] Col. 9 records design temperatures in use by A.S.H.V.E. Members as reported by Chapter Secretaries for the various stations. Where these were not available the design temperatures from an ACRMA publication and various other sources have been inserted.

[i] The wind velocities indicated in Col. 10 are repeated from the 1947 Guide with a few additions and corrections where other weather data have been made available.

[j] The bulletin published by A.S.H.V.E. for annual weather data of Detroit indicates 6 as design temperature.

with the use to which the building is to be put and Table 2 presents values which conform to good practice.

The proper dry-bulb temperature to be maintained depends upon the relative humidity and air motion, as explained in Chapter 12. In other words, a person may feel warm or cool at the same dry-bulb temperature, depending on the relative humidity and air motion. The optimum winter *effective temperature* for sedentary persons, as determined at the A.S.H.V.E. Research Laboratory, is 66 deg.

As explained in Chapter 12 for so-called still air conditions, a relative humidity of approximately 50 per cent is required to produce an effective temperature of 66 deg when the dry-bulb temperature is 70 F. However, even where provision is made for artificial humidification, the relative

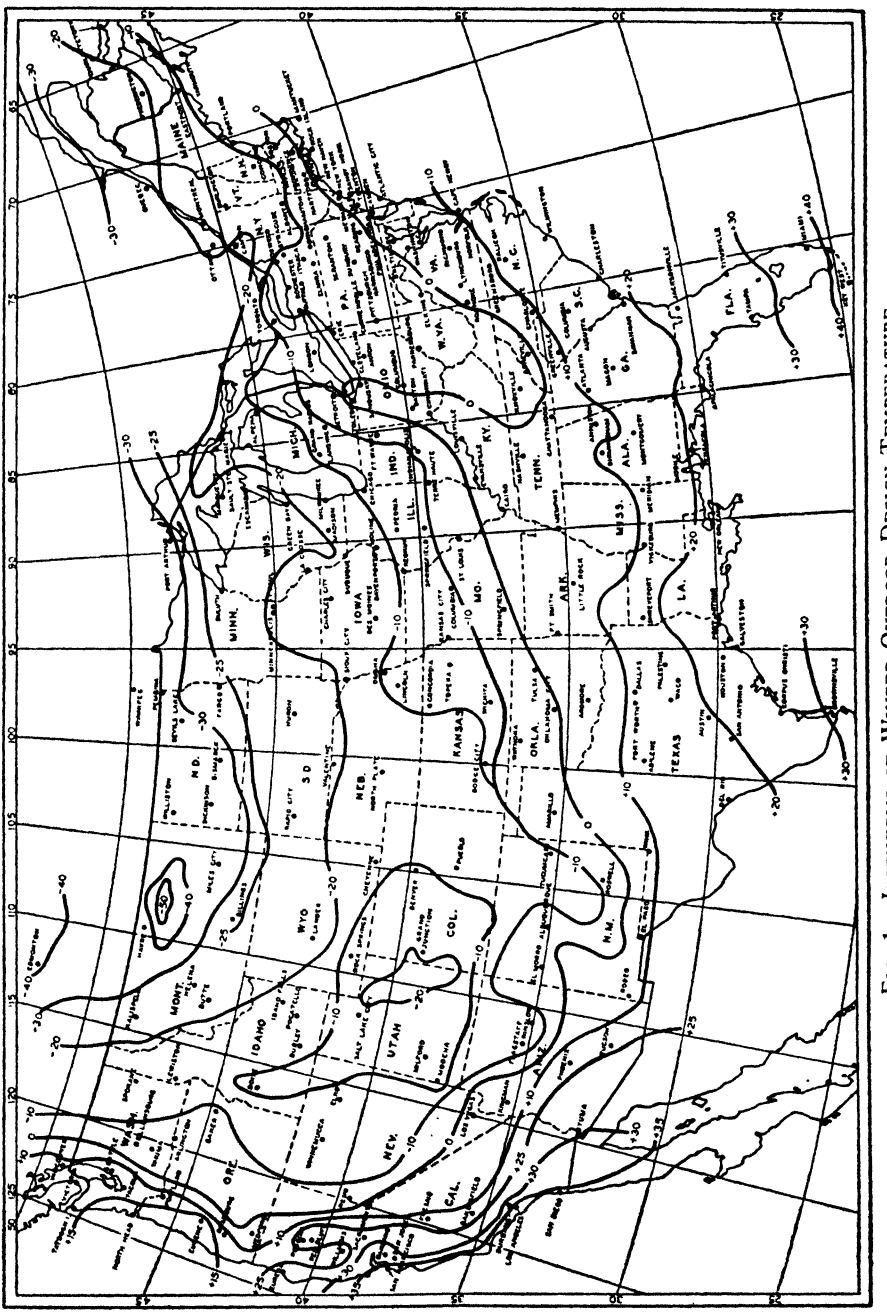

FIG. 1. ISOTHERMS OF WINTER OUTDOOR DESIGN TEMPERATURE

humidity is seldom maintained higher than 40 per cent during the extremely cold weather, and where no provision is made for humidification, the relative humidity may be 20 per cent or less. Consequently, in using the figures listed in Table 2, consideration should be given to the actual relative humidity to be maintained if provision is to be made for humidification.

Temperature at Proper Level: In making the actual heat loss computations, however, for the various rooms in a building it is often necessary to modify the temperatures given in Table 2 so that the air temperature at the proper level will be used. By *air temperature at the proper level* is meant, in the case of walls, the air temperature at the mean height between floor and ceiling; in the case of glass, the air temperature at the mean height of the glass; in the case of roof or ceiling, the air temperature at the mean height of the roof or ceiling above the floor of the heated room; and in the case of floors, the air temperature at the floor level.

Temperature at Ceiling: The air temperature at the ceiling is generally higher than at the breathing level due to stratification of air resulting from the tendency of the warmer or less dense air to rise. An allowance for this fact should be made in calculating ceiling heat losses, particularly in the

TABLE 2. WINTER INSIDE DRY-BULB TEMPERATURES USUALLY SPECIFIED[a]

TYPE OF BUILDING	DEG F	TYPE OF BUILDING	DEG F
SCHOOLS—		THEATERS—	
Class rooms	70–72	Seating space	68–72
Assembly rooms	68–72	Lounge rooms	68–72
Gymnasiums	55–65	Toilets	68
Toilets and baths	70		
Wardrobe and locker rooms	65–68	HOTELS—	
Kitchens	66	Bedrooms and baths	70
Dining and lunch rooms	65–70	Dining rooms	70
Playrooms	60–65	Kitchens and laundries	66
Natatoriums	75	Ballrooms	65–68
		Toilets and service rooms	68
HOSPITALS—			
Private rooms	70–72	HOMES	70–72
Private rooms (surgical)	70–80	STORES	65–68
Operating rooms	70–95	PUBLIC BUILDINGS	68–72
Wards	68	WARM AIR BATHS	120
Kitchens and laundries	66	STEAM BATHS	110
Toilets	68	FACTORIES AND MACHINE SHOPS	60–65
Bathrooms	70–80	FOUNDRIES AND BOILER SHOPS	50–60
		PAINT SHOPS	80

[a]The most comfortable dry-bulb temperature to be maintained depends on the relative humidity and air motion. These three factors considered together constitute what is termed the *effective temperature*. (See Chapter 12.) When relative humidity is not controlled separately, optimum dry-bulb temperature for comfort will be slightly higher than shown in Table 2.

case of high ceilings. However, the exact allowance to be made may be somewhat difficult to determine as it depends on many factors, including (1) the type of heating system, (2) ceiling height, and (3) the inside-outside temperature differential. The type of heating system is particularly important as the temperature gradient from floor to breathing-level to ceiling may depend to a large extent on whether direct radiation, unit heaters or warm air is used, and in the latter case, whether the circulation is by gravity, auxiliary fan or forced air. Although with properly adjusted air flow the temperature differential with unit heaters can be reduced to a minimum, it is possible with improper adjustment that it may be increased over that which would normally result without mechanical circulation of the air.

It would be difficult from present available information to establish rules for determining the temperature difference to use in all cases. However, for residences and other structures having ceiling heights under 10 ft, the comparatively small temperature differential between the

breathing level and ceiling may generally be neglected without serious error. For higher ceilings where specific test data are not available, an allowance of approximately 1 per cent per foot of height above the breathing level may be made for ceiling heights up to 15 ft and approximately 1/10 of 1 deg per foot of height above this level. The values in Table 3 are calculated on this basis. For direct radiation and gravity warm air systems, the allowance should be increased from 50 per cent to 100 per cent over those given in Table 3. These rules should, however, be used with considerable discretion.

Temperature at Floor Level: According to the University of Illinois Research Residence tests [3], the temperature at the floor level ranged from about 2½ to 6 deg below that at the breathing level, or somewhat greater than the difference between the breathing level and ceiling

TABLE 3. APPROXIMATE TEMPERATURE DIFFERENTIALS BETWEEN BREATHING LEVEL AND CEILING, APPLICABLE TO CERTAIN TYPES OF HEATING SYSTEMS[a]

CEILING HEIGHT (FT)	BREATHING LEVEL TEMPERATURE (5 FT ABOVE FLOOR)									
	60	65	70	72	74	76	78	80	85	90
10	3.0	3.3	3.5	3.6	3.7	3.8	3.9	4.0	4.3	4.5
11	3.6	3.9	4.2	4.3	4.4	4.6	4.7	4.8	5.1	5.4
12	4.2	4.6	4.9	5.0	5.2	5.3	5.5	5.6	6.0	6.3
13	4.8	5.2	5.6	5.8	5.9	6.1	6.2	6.4	6.8	7.2
14	5.4	5.9	6.3	6.5	6.7	6.8	7.0	7 2	7.7	8.1
15	6.0	6.5	7.0	7.2	7.4	7.6	7.8	8.0	8.5	9.0
16	6.1	6.6	7.1	7.3	7.5	7.7	7.9	8.1	8.6	9.1
17	6.2	6.7	7.2	7.4	7.6	7.8	8.0	8.2	8.7	9.2
18	6.3	6.8	7.3	7.5	7.7	7.9	8.1	8.3	8.8	9.3
19	6.4	6.9	7.4	7.6	7.8	8.0	8.2	8.4	8.9	9.4
20	6.5	7.0	7.5	7.7	7.9	8.1	8.3	8.5	9.0	9.5
25	7.0	7.5	8.0	8.2	8.4	8.6	8.8	9.0	9.5	10.0
30	7.5	8.0	8.5	8.7	8.9	9.1	9.3	9.5	10.0	10.5
35	8.0	8.5	9.0	9.2	9.4	9.6	9.8	10.0	10.5	11.0
40	8.5	9.0	9.5	9.7	9.9	10.1	10.3	10.5	11.0	11.5
45	9.0	9.5	10 0	10.2	10.4	10.6	10.8	11.0	11 5	12.0
50	9.5	10.0	10.5	10.7	10.9	11.1	11.3	11.5	12.0	12.5

[a]The figures in this table are based on an increase of 1 per cent per foot of height above the breathing level (5 ft) up to 15 ft and 1/10 of one degree for each foot above 15 ft. This table is generally applicable to forced air types of heating systems. For direct radiation or gravity warm air, increase values 50 per cent to 100 per cent.

temperatures. Tests at the University of Wisconsin [4] indicated a somewhat smaller differential between the floor and breathing level temperatures. As a general rule, if the breathing level to ceiling temperature differential is neglected (as with ceiling heights under 10 ft), the breathing level-floor differential may also be neglected as the two are somewhat compensating, especially where both floor and ceiling heat losses are calculated for the same space. In other cases, the 10 ft temperature differentials in Table 3 may be used in arriving at the floor heat loss, these differentials to be subtracted from the breathing level temperature.

ATTIC TEMPERATURES

Frequently it is necessary to estimate the attic temperature, and in such cases Equation 1 can be used for this purpose.

$$t_a = \frac{A_c U_c t_1 + t_o (A_r U_r + A_w U_w + A_g U_g)}{A_r U_r + A_w U_w + A_g U_g + A_c U_c} \qquad (1)$$

where

t_a = attic temperature, Fahrenheit degrees.
t_i = inside temperature near top floor ceiling, Fahrenheit degrees.
t_o = outside temperature, Fahrenheit degrees.
A_c = area of ceiling, square feet.
A_r = area of roof, square feet.
A_w = area of net vertical attic wall surface, square feet.
A_g = area of attic glass, square feet.
U_c = coefficient of transmission of ceiling, based on surface conductance of 2.20 (upper surface, see Chapter 6). 2.20 = reciprocal of one-half the air space resistance.
U_r = coefficient of transmission of roof, based on surface conductance of 2.20 (lower surface, see Chapter 6).
U_w = coefficient of transmission of vertical wall surface.
U_g = coefficient of transmission of glass.

Example 1. Calculate the temperature in an unheated attic, assuming the following conditions: $t_i = 70$; $t_o = 10$; $A_c = 1000$; $A_r = 1200$; $A_w = 100$; $A_g = 10$; $U_r = 0.50$; $U_c = 0.40$; $U_w = 0.30$; $U_g = 1.13$.

Solution: Substituting these values in Equation 1:

$$t_a = \frac{(1000 \times 0.40 \times 70) + 10\,[(1200 \times 0.50) + (100 \times 0.30) + (10 \times 1.13)]}{(1200 \times 0.50) + (100 \times 0.30) + (10 \times 1.13) + (1000 \times 0.40)}$$

$$t_a = \frac{34{,}413}{1041} = 33.1 \text{ F.}$$

Equation 1 neglects the effect of any interchange of air such as would take place through attic vents or louvers intended to preclude attic condensation. However, according to tests [5], such venting of attics by means of small louvers or other small openings does not appreciably reduce the attic temperature and may be neglected without serious error. The attic temperature may be calculated in the usual manner by means of Equation 1, allowing the full value of the roof. The error resulting from this assumption will generally be considerably less than if the roof were neglected (as is sometimes the practice) and the attic temperature assumed to be the same as the outside temperature. When relatively large louvers are installed as is customary in the southern states, the attic temperature is often assumed as the average between inside and outside temperatures.

For a shorter, approximate method of calculating heat losses through attics, the combined ceiling and roof coefficient may be used as described in Chapter 6, page 136.

TEMPERATURES IN UNHEATED SPACES

The heat loss from heated rooms into unheated rooms or spaces must be based on the estimated or assumed temperature in such unheated spaces. This temperature will generally range between the inside and outside temperatures, depending on the relative areas of the surfaces adjacent to the heated room and exposed to the outside. If the respective surface areas adjacent to the heated room and exposed to the outside are approximately the same, and if the coefficients of transmission are approximately equal, the temperature in the unheated space may be assumed to be the mean of the inside and outside design temperatures. If, however, the surface areas and coefficients are unequal, the temperature in the unheated space should be estimated by means of Equation 2.

$$t_u = \frac{t(A_1U_1 + A_2U_2 + A_3U_3 + \text{etc.}) + t_o\,(A_aU_a + A_bU_b + A_cU_c + \text{etc.})}{A_1U_1 + A_2U_2 + A_3U_3 + \text{etc.} + A_aU_a + A_bU_b + A_cU_c + \text{etc.}} \quad (2)$$

where

t_u = temperature in unheated space, Fahrenheit degrees.

t = inside design temperature of heated room, Fahrenheit degrees.

t_o = outside design temperature, Fahrenheit degrees.

A_1, A_2, A_3, etc. = areas of surface of unheated space adjacent to heated space, square feet.

A_a, A_b, A_c, etc. = areas of surface of unheated space exposed to outside, square feet.

U_1, U_2, U_3, etc. = coefficients of transmission of surfaces of A_1, A_2, A_3, etc.

U_a, U_b, U_c, etc. = coefficients of transmission of surfaces A_a, A_b, A_c, etc.

Example 2. Calculate the temperature in an unheated space adjacent to a heated room having surface areas (A_1, A_2, and A_3) in contact therewith of 100, 120, and 140 sq ft and coefficients (U_1, U_2, and U_3) of 0.15, 0.20, and 0.25 respectively. The surface areas of the unheated space exposed to the outside (A_a and A_b) are respectively 100 and 140 sq ft and the corresponding coefficients are 0.10 and 0.30. The sixth surface is on the ground and is neglected in this example. Assume $t = 70$ and $t_o = -10$.

Solution. Substituting in Equation 2:

$$t_u = \frac{70[(100\times0.15)+(120\times0.20)+(140\times0.25)]+-10[(100\times0.10)+(140\times0.30)]}{(100\times0.15)+(120\times0.20)+(140\times0.25)+(100\times0.10)+(140\times0.30)}$$

$$t_u = \frac{4660}{126} = 37 \text{ F.}$$

The temperatures in unheated spaces having large glass areas and with two or more surfaces exposed to the outside (such as sleeping porches and sun parlors), are generally assumed to be the same as outside.

GROUND TEMPERATURES

Ground temperatures to be assumed for estimating basement heat losses will usually differ in the case of basement walls and floors, the temperatures under the floors being generally higher than those adjacent to walls.

Temperatures Adjacent to Basement Walls

Ground temperatures near the surface and under open spaces vary with the climate, the season of the year and the depth below the surface. The nearer the surface (during the cold weather) the lower the temperature. Frost will penetrate to a depth of over 4 ft in some localities if not protected by snow. A thick blanket of snow will result in a higher ground temperature near the surface. Consequently ground temperatures near the surface may be higher in cold climates where the snow remains on the ground for a greater length of time than in more moderate climates where the snow melts away periodically during the winter.

Complete data for various localities are not as yet available but in estimating heat losses through vertical walls below grade, it is advisable not to assume average ground temperatures above 32 F in northern climates when estimating heat losses from heated basements. This is for the mean height of the basement wall. Since the recommended wall coefficient for basement walls in contact with the soil is only 0.10, any small variation in the assumed ground temperature will not materially affect the calculated heat loss.

Temperatures Under Basement Floors

The temperature under basement floors [6] is influenced by the heat from the basement or protected from the influence of atmospheric conditions by the basement. In computing losses through basement floors the ground temperatures may be assumed the same as the approximate water temperature at depths of 30 to 60 ft given in Fig. 3, Chapter 37. Test results indicate that the heat losses through basement floors are frequently over-estimated [7].

BASEMENT TEMPERATURES AND HEAT LOSS

The allowance to be made for basement heat loss depends on whether the basement is to be heated or not.

If the basement is *heated* and a specified temperature is to be maintained, the heat loss should be estimated in the usual manner, based on the proper wall and floor coefficients (see Chapter 6) and the outside air and ground temperatures. Heat loss through windows and walls above grade should be based on outside temperatures and the proper air-to-air coefficients. Heat loss through basement walls below grade should be based on the floor and wall coefficients for surfaces in contact with the soil and on the proper ground temperature.

If a basement is completely below grade and is *not heated*, the temperature in the basement will normally range between that in the rooms above and the ground temperature. Basement windows will of course lower the basement temperature when it is colder outside and any heat given off by the heating plant will increase the basement temperature. In any case, the exact basement temperature is likely to be a somewhat indeterminate quantity, if the basement is not heated. Since the basement temperature will generally be lower than that of the rooms above, an allowance should theoretically be made for the loss from the rooms above through the floor over the basement.

The temperature in crawl spaces below floors will vary greatly depending on the number and size of wall vents, the quantity of heating pipes and the type of insulation. It is therefore necessary to analyze the conditions and select an appropriate temperature by judgment.

TRANSMISSION HEAT LOSS

The basic formula for the loss of heat by transmission through any surface is given in Equation 3.

$$H_t = A\,U\,(t - t_o) \qquad (3)$$

where

H_t = heat loss transmitted through the wall, roof, ceiling, floor, or glass, Btu per hour.

A = area of wall, glass, roof, ceiling, floor, or other exposed surfaces, square feet.

U = coefficient of transmission, air to air, Btu per (hour) (square foot) (Fahrenheit degree temperature difference) (Chapter 6).

t = inside temperature near surface involved which may not necessarily be the so-called breathing line temperature, Fahrenheit degrees.

t_o = outside temperature, or temperature of adjacent unheated space or of the ground, Fahrenheit degrees.

Example 3. Calculate the transmission loss through an 8 in. brick wall having an area of 150 sq ft if the inside temperature (t) is 70 F and the outside temperature (t_o) is −10 F.

Solution. The coefficient of transmission (U) of a plain 8 in. brick wall is 0.50 (Chapter 6, Table 7). The area (A) is 150 sq ft. Substituting in Equation 3:

$$H_t = 150 \times 0.50 \times [70 - (-10)] = 6000 \text{ Btu per hour.}$$

Transmission Loss Through Ceilings and Roofs

The transmission heat loss through top floor ceilings, attics, and roofs may be estimated by either of two methods:

1. By substituting in Equation 3 the ceiling area (A), the inside-outside temperature difference ($t - t_o$) and the proper value of (U):

   a. *Flat roofs.* Select the coefficient of transmission of the ceiling and roof from Tables 14 or 15, Chapter 6, or use appropriate coefficients in Equation 1 if side walls extend appreciably above the ceiling of the floor below.

   b. *Pitched roofs.* Select the combined roof and ceiling coefficient from Table 17, Chapter 6 or calculate the combined roof and ceiling coefficient by means of Equation 5, Chapter 6, where this formula is applicable as explained in Chapter 6.

2. By estimating the attic temperature (based on the inside and outside design temperatures) by means of Equation 1, and substituting for t_o in Equation 3, the value of t_a thus obtained, together with the ceiling area (A) and the ceiling coefficient (U). This applies to *pitched roofs.* In the case of *flat roofs* it is not necessary to calculate the attic temperatures as the ceiling-roof heat loss can be determined as per paragraph 1a.

INFILTRATION HEAT LOSS

The infiltration heat loss includes (1) the *sensible heat loss* or the heat required to warm the outside air entering by infiltration and (2) the *latent heat loss* or the heat equivalent of any moisture which must be added.

Sensible Heat Loss

The formula for the heat required to warm the outside air which enters a room by infiltration to the temperature of the room, is given in Equation 4.

$$H_s = 0.240\, Qd\, (t - t_o) \qquad (4)$$

where

H_s = heat required to raise temperature of air leaking into building from t_o to t, Btu per hour.

0.240 = specific heat of air.

Q = volume of outside air entering building, cubic feet per hour (see Chapter 8).

d = density of air at temperature t_o, pounds per cubic foot.

It is sufficiently accurate to use $d = 0.075$ in which case Equation 4 reduces to

$$H_s = 0.018\, Q\, (t - t_o) \qquad (4a)$$

The volume of outside air entering per hour (Q) depends on the wind velocity and direction, the width of crack or size of openings, the type of openings and other factors, as explained in Chapter 8. Where the crack method is used for estimating leakage, it is more convenient to express the air leakage heat loss in terms of the crack length:

$$H_s = B\, L\, (t - t_o) \qquad (4b)$$

where

B = air leakage per (hour) (foot of crack) (Chapter 8) for the wind velocity and type of windows or door crack involved multiplied by 0.018.

L = length of window or door crack to be taken into consideration, feet.

Example 4. What is the infiltration heat loss per hour through the crack of a 3 x 5 ft average, double-hung, non-weatherstripped, wood window, based on a wind velocity of 15 mph? Assume inside and outside temperatures to be 70 F and zero respectively.

Solution. According to Table 2, Chapter 8, the air leakage through a window of this type (based on 1/16 in. crack and 3/64 in. clearance) is 39 cu ft per foot of crack per hour. Therefore, $B = 39 \times 0.018 = 0.70$. The length of crack ($L$) is $(2 \times 5) + (3 \times 3)$, or 19 ft; $t = 70$ and $t_o = 0$. Substituting in Equation 4b,

$$H_s = 0.70 \times 19 \times (70 - 0) = 931 \text{ Btu per hour.}$$

Number of Air Changes to be used for Computations

In the opinion of many engineers the crack method is inferior in practical results to the air change method. Estimates of the number of air changes require careful judgment regarding construction and conditions under consideration, that is; whether they are better than, or worse than, the average conditions assumed in Table 4, Chapter 8.

Crack Length to be Used for Computations

For designers who prefer to use the crack method the basis of calculation is as follows: The amount of crack used for computing the infiltration heat loss should not be less than half of the total crack in the outside walls of the room. For a building having no partitions, whatever wind enters through the cracks on the windward side must leave through the cracks on the leeward side. Therefore, take one-half the total crack for computing each side and end of the building. In a room with one exposed wall, take all the crack; with two exposed walls, take the wall having the most crack; and with three or four exposed walls, take the wall having the most crack; but in no case take less than half the total crack.

The total infiltration loss of a building having partitions will not be equal to the sum of the infiltration losses of the various rooms, since at any given time infiltration will take place only on the windward side or sides and not on the leeward side. Therefore, if a building has more than one room which is divided by interior walls or partitions, it is sufficiently accurate to use half of the total infiltration losses for determining the total heat requirements.

Latent Heat Loss

When it is intended to add moisture to air leaking into a room for the maintenance of proper winter comfort conditions, it is necessary to determine the heat equivalent to evaporate the required amount of water vapor, which may be calculated by the equation:

$$H_l = Q\,d\left(\frac{m_i - m_o}{7000}\right) h_{fg} \qquad (5)$$

where

H_l = heat required to increase moisture content of air leaking into building from m_o to m_i, Btu per hour.

Q = volume of outside air entering building, cubic feet per hour.

d = density of air at temperature t_i, pounds per cubic foot.

m_i = vapor density of inside air, grains per pound of dry air.
m_o = vapor density of outside air, grains per pound of dry air.
h_{fg} = latent heat of vapor at m_i, Btu per pound.

If the latent heat of vapor (h_{fg}) is assumed to be 1060 Btu per pound, Equation 5 reduces to

$$H_l = 0.0114\ Q\ (m_i - m_o) \qquad (5a)$$

Equations 4a, 4b and 5a may also be used for determining the sensible and latent heat gains due to infiltration in cooling load computations.

SELECTION OF WIND VELOCITIES

The effect of wind on the heating requirements of any building should be given consideration under two heads:

1. Wind movement increases the heat transmission of walls, glass, and roof, affecting poor walls to a much greater extent than good walls.

2. Wind movement materially increases the infiltration of cold air through the cracks around doors and windows, and even through the building materials themselves.

Theoretically as a basis for design, the most unfavorable combination of temperature and wind velocity should be chosen. It is entirely possible that a building might require more heat on a windy day with a moderately low outside temperature than on a quiet day with a much lower outside temperature. However, the combination of wind and temperature which is the worst would differ with different buildings, because wind velocity has a greater effect on buildings which have relatively high infiltration losses. It would be possible to compute the heating load for a building for several different combinations of temperature and wind velocity which records show to have occurred and to select the worst combination; but designers generally do not feel that such a degree of refinement is justified.

Therefore, since Table 1 lists the average velocity of winds occurring at temperatures equalled or exceeded 97½ per cent of the winter period for each locality, this value should be the basis for estimating infiltration losses. When using the air change method it will not be necessary to consider the wind velocities. Designers employing the crack method generally used values corresponding to a 15-mile wind. Due to the small effect of the wind velocity on the transmission coefficient, the values in Chapter 6, based on a 15-mile wind may be used at all times.

Exposure Factors

Many designers use empirical exposure factors to increase the calculated heat loss of rooms or spaces on the side or sides of the building exposed to the prevailing winds. However, according to a survey made in 1943, many GUIDE users have found that the use of exposure factors is not necessary as the GUIDE method of calculating heat losses provides an ample heat loss allowance. Therefore exposure factors may be regarded as *factors of safety* for the rooms or spaces exposed to the prevailing winds, to allow for additional capacity for these rooms or spaces, or to *balance the radiation*, particularly in the case of multi-story buildings. Although the exposure allowance is frequently assumed to be 15 per cent, the actual allowance to be made, if any, must to a large extent be a matter of experience and judgment of the designer, since there are at present no authentic test data available from which rules could be developed for the many conditions encountered in practice.

As stated previously, the value of U in the tables of Chapter 6 is based on a wind velocity of 15 mph and the surface resistance for this wind velocity (0.17) is sufficiently low so that higher wind velocities will decrease the surface resistance to a negligible degree and therefore have only a slight effect on the average over-all coefficient. On the other hand, infiltration losses vary almost directly as the wind velocity, as will be apparent from the factors in Table 2 of Chapter 8. The more exact method therefore would be to differentiate among the various exposures more accurately by calculating the infiltration and transmission losses separately for the different sides of the building, using different assumed wind velocities for the infiltration losses on the various sides.

AUXILIARY HEAT SOURCES

The heat supplied by persons, lights, motors and machinery should always be ascertained in the case of theaters, assembly halls, and industrial plants, but allowances for such heat sources must be made only after careful consideration of all local conditions. In many cases, these heat sources should not be allowed to affect the size of the installation at all, although they may have a marked effect on the operation and control of the system. In general, it is safe to say that where audiences are involved, the heating installation must have sufficient capacity to bring the building up to the stipulated inside temperature before the audience arrives. In industrial plants, quite a different condition exists, and heat sources, if they are always available during the period of human occupancy, may be substituted for a portion of the heating installation. In no case should the actual heating installation (exclusive of heat sources) be reduced below that required to maintain at least 40 F in the building.

TABLE 4. HEAT EQUIVALENTS OF VARIOUS SOURCES[a]

Machinery (Motor in room = Motor Hp/efficiency x 2544		Btu/hr.
Machinery (Motor outside room) = Motor Hp x 2544		Btu/hr.
Electric Lights	= Kilowatts x 3413	Btu/hr.
Gas (Producer = 150) (Manufactured = 535) (Natural = 1000)		Btu/cu ft.

[a]Additional values are given in Chapter 15, Table 23.

Electric Motors and Machinery

Motors and the machinery which they drive, if both are located in the room, convert all of the electrical energy supplied into heat, which is retained in the room if the product being manufactured is not removed until its temperature is the same as the room temperature.

If power is transmitted to the machinery from the outside, then only the heat equivalent of the brake horsepower supplied is used. In some mills this is the chief source of heating and it is frequently sufficient to overheat the building even in zero weather, thus requiring cooling by ventilation the year 'round. Table 4 shows the heat output equivalent of various sources of heat in a factory. For information concerning the heat supplied by persons, refer to data given in Chapter 12. For appliances see Table 23, Chapter 15.

INTERMITTENTLY HEATED BUILDINGS

In the case of intermittently heated buildings additional heat is required for raising the temperature of the air, the building materials and

the material contents of the building to the specified inside temperature. The rate at which this additional heat must be supplied depends upon the heat capacity of the structure and its material contents and upon the time in which these are to be heated [8].

This additional heat may be figured and allowed for as conditions require, but inasmuch as the heating system proportioned for taking care of the heat losses will usually have a capacity about 100 per cent greater than that required for average winter weather, and inasmuch as most buildings may either be continuously heated or have more time allowed for heating-up during the few minimum temperature days, no allowance is usually made except in the size of boilers or furnaces. For churches, auditoriums and other intermittently heated buildings, additional capacity should be provided.

RESIDENCE HEAT LOSS PROBLEMS

Example 5. Calculate the heat loss of the residence shown in Fig. 2 located in the vicinity of Chicago. From Table 1, design outdoor conditions are −10 F and 12 mph wind velocity. Inside temperature from Table 2 is assumed to be 70 F. The attic is unheated. Assume ground temperature to be 50 F (see Fig. 3, Chapter 37) under basement and garage floors and 32 F adjoining basement walls. Estimate infiltration losses by the air change method. No wall, ceiling or roof insulation is to be considered in this problem, but all first and second floor windows, except in the garage are to have storm sash. The building is constructed as follows (heat transmission coefficients U are in parentheses):

Walls: Brick veneer, building paper, wood sheathing, studding, metal lath and plaster (0.28). Walls of dormer over garage, same except wood siding in place of brick veneer (0.26).

Attic Walls: Brick veneer, building paper, wood sheathing on studding (0.42).

Basement Walls: 10 in. concrete (0.10).

Roof: Asphalt shingles on wood sheathing on rafters (0.53).

Ceiling (Second floor): Metal lath and plaster (0.69).

Windows: Double-hung wood windows with storm sash (0.45). Steel casement sash in basement (1.13).

Floor (Bedroom D): Maple finish flooring on yellow pine sub-flooring; metal lath and plaster ceiling below (0.25).

Floor (Basement and Garage): 4 in. stone concrete on 3 in. cinder concrete (0.10).

Solution: The calculations for this problem are given in Table 5, and a summary of the results in Table 6. The values in column F of Table 5 were obtained by multiplying together the figures in columns C, D, and E. The heat losses are calculated to the nearest 10 Btu. See reference notes for Table 5 for further explanation of data.

Attention is called to the summary of heat losses (Table 6) for the uninsulated residence. As storm windows are used in this instance the *glass* and *door* transmission heat losses of 20.7 per cent are relatively small. The infiltration losses of 14.1 per cent are also comparatively small because the storm windows are equivalent to weatherstripping. In this problem, the wall, ceiling and floor transmission losses comprise 65.2 per cent of the total.

Example 6. Calculate the heat loss of residence shown in Fig. 2 based on the same conditions as in *Example 5* but having construction improved or insulated to obtain coefficients as follows:

Walls, 0.13; *Walls of Dormer over Garage*, 0.12; *Attic Walls*, 0.28; *Walls Adjoining Garage*, 0.18; *Basement Walls (Recreation Room)*, 0.10.

Roof, 0.53

Ceiling (Second Floor), 0.15

Windows (Same as in *Example 5*).

Floor (Bedroom D), 0.18.

Solution: The procedure for calculating the heat losses is similar to that for *Example 5*. A summary of the results is given in Table 7.

NOTES FOR TABLE 5.

[a]The inside-outside temperature difference is 70− (−10) or 80 F except where otherwise noted.

[b]Volume of infiltration, cfh = (no. air changes) x (floor or ceiling area) x (ceiling height).

[c]From equation 4a, p. 245.

[d]The ceiling heat losses are calculated by estimating the attic temperature and then calculating the loss through the ceiling using the proper temperature difference. This unheated attic is not ventilated during winter months. The attic temperature is estimated from Equation 1 to be 30.2 F when the outside temperature is −10 F and room temperature is 70 F. The temperature difference is then 70−30. 2 or 39.8 deg. For the insulated residence, attic temperature becomes 4.6 F and temperature difference 70−4.6=65.4 deg.

[e]Temperature in garage assumed to be 35 F.

[f]Coefficient for wall adjoining garage calculated on basis of metal lath and plaster on both sides of studs. (U=0.39).

[g]One half of value from Table 4, Chapter 8, for storm windows or weatherstripping.

[h]Exposed on two sides, weatherstripped windows offset by fire-place. Use 1½.

[i]Window on one side weatherstripped but double-doors are hard to close tightly. Hence conservative value of 1½.

[j]Assuming kitchen vent, door to vestibule usually open, allow full table value of 1½.

[k]One half value in Table 4, Chapter 8, increased to 1½ by nearby outside door in vestibule.

[l]Full value in Table 4, Chapter 8, to allow for frequent opening of outside door.

[m]Two sides exposed, large doors but large volume. Use value 1½ as given in Table 4, Chapter 8.

[n]Two small unweatherstripped windows in protected location, but fireplace, indicate 1 change.

[o]Since garage is assumed colder than ground, heat gain results should be subtracted from heat losses elsewhere.

[p]Heat losses from these rooms into garage are heat gains for garage.

[q]Neglect heat loss to basement, as losses from boiler, piping, etc. will probably keep basement near, if not above, 70 F.

[r]Upstairs hall ceiling figured with downstairs. Heat should be provided downstairs for both.

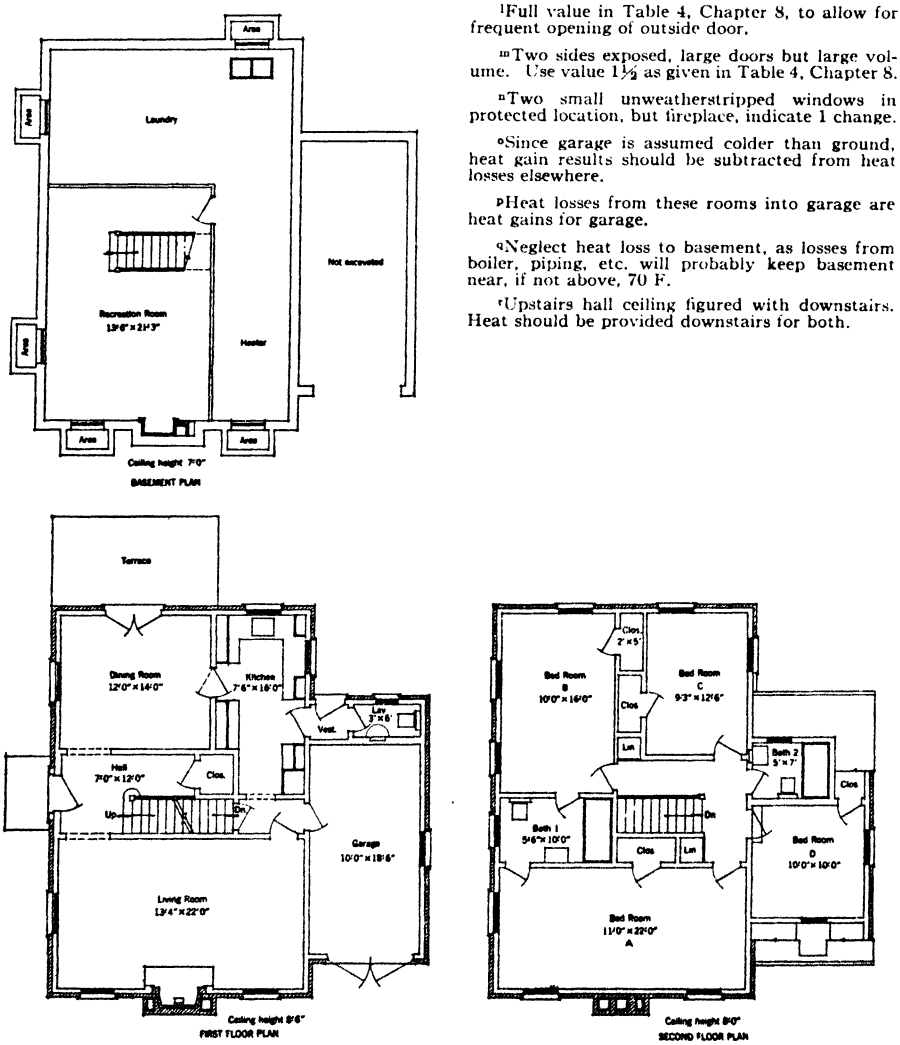

FIG. 2. FLOOR PLANS OF RESIDENCE

TABLE 5. HEAT LOSS CALCULATION SHEET FOR UNINSULATED RESIDENCE (FIG. 2)

A	B	C	D	E	F	G
ROOM OR SPACE	PART OF STRUCTURE OR INFILTRATION AIR CHANGES	NET AREA OR AIR VOLUME	COEFFICIENT	TEMP. DIFF.[a]	HEAT LOSS (Btu per hour)	TOTALS (Btu per hour)
Bedroom A and Closet	Walls	238 sq ft	0.28	80	5330	
	Glass	40 sq ft	0.45	80	1440	
	Ceiling	252 sq ft	0.69	39.8[d]	6910	
	Infiltration (¾)[g]	1510 cfh[b]	0.018[c]	80	2180	15,860
Bedroom B and Closet	Walls	156 sq ft	0.28	80	3490	
	Glass	40 sq ft	0.45	80	1410	
	Ceiling	170 sq ft	0.69	39.8[d]	4660	
	Infiltration (¾)[g]	1020 cfh[b]	0.018	80	1470	11,060
Bedroom C and Closet	Walls	114 sq ft	0.28	80	2560	
	Glass	27 sq ft	0.45	80	970	
	Ceiling	129 sq ft	0.69	39.8[d]	3540	
	Infiltration (¾)[g]	874 cfh[b]	0.018[c]	80	1260	8,330
Bedroom D and Closet	Walls	118 sq ft	0.28	80	2650	
	Glass	20 sq ft	0.45	80	720	
	Ceiling	110 sq ft	0.69	39.8[d]	3020	
	Floor over garage	110 sq ft	0.25	35[e]	960[p]	
	Infiltration (¾)[g]	660 cfh[b]	0.018[c]	80	950	8,300
Bathroom 1	Walls	30 sq ft	0.28	80	670	
	Glass	14 sq ft	0.45	80	500	
	Ceiling	55 sq ft	0.69	39.8[d]	1510	
	Infiltration (1)[g]	440 cfh[b]	0.018[c]	80	630	3,310
Bathroom 2	Walls	79 sq ft	0.28	80	1640	
	Glass	9 sq ft	0.45	80	320	
	Ceiling	35 sq ft	0.69	39.8[d]	960	
	Floor over garage	35 sq ft	0.25	35[e]	310[p]	
	Infiltration (1)[g]	280 cfh[b]	0.018[c]	80	400	3,630
Living Room	Walls	267 sq ft	0.28	80	5980	
	Walls (adjoining garage)	94 sq ft	0.39[f]	35[e]	1280[p]	
	Glass	50 sq ft	0.45	80	1800	
	Floor	294 sq ft				
	Infiltration (1½)[h]	3745 cfh[b]	0.018	80	5100	14,460
Dining Room	Walls	166 sq ft	0.28	80	3720	
	Glass (doors)	35 sq ft	1.13	80	3160	
	Glass (windows)	20 sq ft	0.45	80	720	
	Floor	168 sq ft				
	Infiltration (1½)[i]	2140 cfh[b]	0.018[c]	80	3080	10,680
Kitchen and Entrance to Garage	Walls	96 sq ft	0.28	80	2150	
	Walls (adjoining garage)	51 sq ft	0.39[f]	35[e]	700[p]	
	Glass	18 sq ft	0.45	80	650	
	Door	17 sq ft	0.51	35	300	
	Floor	125 sq ft				
	Infiltration (1½)[j]	1595 cfh[b]	0.018[c]	80	2300	6,100
Lavette and Vestibule	Walls	82 sq ft	0.28	80	1840	
	Walls (adjoining garage)	85 sq ft	0.39[f]	35[e]	1160[p]	
	Glass	9 sq ft	0.45	80	320	
	Door	19 sq ft	0.51	80	780	
	Floor	30 sq ft				
	Infiltration (1½)[k]	383 cfh[b]	0.018[c]	80	550	4,650
Entrance Hall	Walls	39 sq ft	0.28	80	870	
	Door	21 sq ft	0.38	80	640	
	Ceiling[r]	87 sq ft	0.69	39.8[d]	2390	
	Infiltration (2)[l]	1110 cfh[b]	0.018[c]	80	1600	5,500
Garage	Walls	167 sq ft	0.28	45[e]	2110	
	Glass	53 sq ft	1.13	45	2700	
	Doors	44 sq ft	0.51	45	1010	
	Infiltration (1½)[m]	2360 cfh[b]	0.018[c]	45	1910	
	Floor (heat gain)	185 sq ft	0.10	−15	−280[o]	
	Gain adjoining rooms				−4410[p]	3,040
Recreation Room[q]	Walls	220 sq ft	0.10	38	840	
	Glass	8 sq ft	1.13	80	720	
	Floor	287 sq ft	0.10	20	570	
	Infiltration (1)[n]	2010 cfh[b]	0.018[c]	80	2890	5,020
					TOTAL	99,940

TABLE 6. SUMMARY OF HEAT LOSSES OF UNINSULATED RESIDENCE (*Btu Per Hour*)

ROOM OR SPACE	WALLS	CEILING AND ROOF	FLOOR	GLASS AND DOOR	INFILTRATION	TOTALS
Bedroom A	5330	6910	.....	1440	2180	15,860
Bedroom B	3490	4660	.....	1440	1470	11,060
Bedroom C	2560	3540	.....	970	1260	8,330
Bedroom D	2650	3020	960	720	950	8,300
Bathroom 1	670	1510	.....	500	630	3,310
Bathroom 2	1640	960	310	320	400	3,630
Living Room	7260	.....	.....	1800	5400	14,460
Dining Room	3720	.....	.....	3880	3080	10,680
Kitchen	2850	.....	.....	950	2300	6,100
Lavette	3000	.....	.....	1100	550	4,650
Entrance Hall	870	2390	.....	640	1600	5,500
Garage	−1030[a]	−1270[b]	−280[c]	3710	1910	3,010
Recreation	840	.....	570	720	2890	5,020
Design Totals	33,850	21,720	1,560	18,190	24,620	99,940
Operating Totals[d]	33,850	21,720	1,560	18,190	12,310	87,630
Percentages[e]	38.6	24.8	1.8	20.7	14.1	100.0

[a] Wall heat loss of 2110 Btuh minus wall heat gains of 1280, 700 and 1160 Btuh. [b] Heat gains of 960,310 Btuh. [c] Heat gain. [d] Based on ½ computed infiltration. [e] Based on Operating Totals.

TABLE 7. SUMMARY OF HEAT LOSSES OF INSULATED RESIDENCE (*Btu Per Hour*)

ROOM OR SPACE	WALLS	CEILING AND ROOF	FLOOR	GLASS AND DOOR	INFILTRATION	TOTALS
Bedroom A	2480	2460	.....	1440	2180	8,560
Bedroom B	1620	1660	.....	1440	1470	6,190
Bedroom C	1190	1260	.....	970	1260	4,680
Bedroom D	1230	1080	690	720	950	4,670
Bathroom 1	310	540	.....	500	630	1,980
Bathroom 2	760	250	220	320	400	1,950
Living Room	3370	.....	.....	1800	5400	10,570
Dining Room	1730	.....	.....	3880	3080	8,690
Kitchen	1320	.....	.....	950	2300	4,570
Lavette	1390	.....	.....	1100	550	3,040
Entrance Hall	410	850	.....	640	1600	3,500
Garage	−470[a]	−910[b]	−280[c]	3710	1910	3,960
Recreation	840	.....	570	720	2890	5,020
Design Totals	16,180	7,190	1,200	18,190	24,620	67,380
Operating Totals[d]	16,180	7,190	1,200	18,190	12,310	55,070
Percentages[e]	29.4	13.0	2.2	33.0	22.4	100.0

[a] Wall heat loss of 980 Btuh minus wall heat gains of 590,320,540 Btuh. [b] Heat gains 690,220 Btuh. [c] Heat gain. [d] Based on ½ computed infiltration. [e] Based on Operating Totals.

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6—A.S.H.V.E. RESEARCH REPORT No. 1213—Heat Loss Through Basement Walls and Floors, by F. C. Houghten, S. I. Taimuty, Carl Gutberlet and C. J. Brown (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 369).

7—Measurements of Heat Losses from Slab Floor, by R. S. Dill, W. C. Robinson and H. E. Robinson (*U. S. Department of Commerce, National Bureau of Standards*, Building Materials and Structures Report BMS 103).

8—Heat Requirement Tables for Intermittently Heated Buildings. (*Engineering Experiment Station Bulletin*, No. 60, *A. and M. College of Texas*, College Station, Texas) contains a set of tables applicable to either intermittent heating or cooling. Further information may be found in a paper, A Method of Compiling Tables for Intermittent Heating, by Elmer G. Smith (A.S.H.V.E. JOURNAL SECTION, *Heating, Piping and Air Conditioning*, June, 1942, p. 386).

Chapter 15

COOLING LOAD

Cooling Load Calculations; Design Conditions; Instantaneous Heat Load; Solar and Sky Radiation, and Heat Transmission Losses; Principles of Periodic Heat Flow; Glass Areas and Design Tables; Load from Interior Partitions; Ceiling and Floors; Load from Outside Air, Ventilation or Infiltration; Heat Sources Within Space; Moisture Heat Load; Regional Air Quantity; Example Cooling Load Calculation

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THE variables affecting cooling-load calculations are numerous, often difficult to define precisely, and always intricately inter-related. Most of the components of the cooling load vary in magnitude over a wide range during a 24-hour period and as the cyclic changes in load components are not usually in phase with each other, careful analysis is required to establish the resultant maximum cooling load for a building or zone. A zoned system must often handle peak loads in different zones at different hours.

Economic considerations must be particularly influential in the selection of equipment for cooling season operation in comfort air conditioning and this fact, coupled with present inadequacies in available data and knowledge of the air-conditioning art, places a premium on the experienced judgment essential to successful design or practice. Variations in the weather, building occupancy and other factors affecting load necessitate carefully coordinated controls to regulate simultaneously the components and the equipment to maintain the desired room conditions.

The calculation procedures presented in this chapter deal with the various instantaneous rates of heat gain both sensible and latent, in a conditioned space. There may be an appreciable difference between the net instantaneous rate of heat gain and the total cooling load at any instant. This difference is caused by the storage and subsequent release of heat by the structure and its contents. This thermal-storage effect may be quite important in determining an economical cooling equipment capacity. The lack of any adequate means of treating this storage quantitatively in its entirety for a complete structure must be recognized in judging the procedures and data presented for calculating individual components of the net rate of instantaneous heat gain.

Solar heating calculations involve the same principles as cooling load calculations. Many of the data on solar radiation given in this chapter are useful in calculations for solar heating.

COOLING LOAD CALCULATIONS

Summer cooling load calculations, whether for industrial or comfort applications, require consideration of the following factors:

A. *Design Conditions:* (1) Indoor conditions. (2) Outdoor conditions. (3) Ventilation rate.

B. *Instantaneous Heat Load, Sensible and Latent:* (1) Load from solar radiation, sky radiation and from outdoor-indoor temperature differential for glass areas and exterior, walls and roofs, modified by periodic heat flow or lag factors depending on the type of structure. (2) Load due to heat gain through interior partitions, ceilings and floors. (3) Load due to ventilation either natural or mechanical. (4) Load due to heat sources within the conditioned space such as people, lights, power equipment and appliances. (5) Load due to moisture transfer through permeable building materials. (6) Miscellaneous heat sources.

C. *Determination of Air Quantity and Apparatus Dew-Point.*

TABLE 1. TYPICAL COMMERCIAL DESIGN ROOM CONDITIONS FOR SUMMER AVERAGE PEAK LOAD IN COMFORT AIR CONDITIONING[a]

TYPE OF INSTALLATION	DRY-BULB TEMP	WET-BULB TEMP[b]	RELATIVE HUMIDITY PER CENT	GRAINS PER LB[b]	EFFECTIVE TEMP[c]
Deluxe Application	78	65	50	72.7	72.2
Normal Application	80	67	51	78.5	74.0
15 to 40 min Occupancy	82	68	49	80.0	75.3

[a]Values in Table 1 are for *peak load* conditions. It is general practice to operate a system at approximately 76 F and 50 per cent relative humidity at other than peak load.

[b]Psychrometric data for standard barometric pressure.

[c]Fig. 10, Chapter 12, air movement 15 to 25 fpm.

These factors will be discussed in turn. The material presented leads to an illustrative procedure for a cooling-load calculation, and a numerical example is given to demonstrate the calculations involved.

DESIGN CONDITIONS

Indoor Conditions

Indoor air conditions for human health and comfort have been and continue to be the subject of much discussion and research.

The effective temperature index, explained in Chapter 12 is probably the best available source of design criteria for comfort air conditioning systems for buildings or enclosures in which the air and inside surface temperatures remain substantially equal; a condition that can safely be assumed for most ordinary comfort air conditioning installations. Other sources of design specifications are to be found in the requirements of codes and ordinances, and in the varied long-term experiences of manufacturers, contractors, and engineering specialists.

Past experience, cumulative over many years, indicates that indoor design conditions for which summer air-conditioning equipment is selected, should not exceed a temperature of 80 F or a relative humidity of 50 per cent for the average job in the United States. If these conditions are exceeded, complaints of discomfort may be expected, especially with continuous occupancy. For very brief occupancy only, a slightly higher peak-load design temperature may be employed. In regard to the lower limit of humidity, complaints are not encountered for store installations operated down to 35 per cent relative humidity or, for office jobs, somewhat lower. These observations apply to normal commercial practice in this country only; for extremes such as tropical or very hot regions it is regarded as more practicable to design for a peak-load outdoor-indoor temperature difference of about 15 to 20 F.

Table 1 offers typical design conditions for average requirements encountered. The *deluxe* figures would also apply in general for localities having a summer outdoor design temperature of 90 F or less; and the *15 to 40 min* occupancy values or even somewhat higher dry-bulb temperatures would indicate acceptable conditions for very hot localities. Table 1 *is to be used with good judgment*, for there is no universal rule which may be applied to indoor design conditions.

Guarantees of conditions to be maintained for summer operation are based upon a definite set of load conditions. At other than the guarantee load, the conditions produced by a system are determined by the balance of imposed load and equipment capacity and by the method adopted for

TABLE 2. ILLUSTRATIVE TEMPERATURES AND RELATIVE HUMIDITIES APPLICABLE TO INDUSTRIAL AIR CONDITIONING[a]

CLASSIFICATION	MATERIALS, LOCATION OR PROCESS	TEMPERATURE F	RELATIVE HUMIDITY %
Employe Efficiency	General Machine Shop Work	78–80	50
	Drafting Rooms	78–80	50
	Offices	78–80	50
Storage Prior to Manufacturing	Rough Castings	80	50
	Ceramic Materials	60–80	50
	Pharmaceutical Powders	70–80	30–35
	Sugar	80	35
	Paper	75–80	35
	Electrical Goods	60–80	35–50
	Flour	60–75	55–65
	Rubber	60–75	40–50
	Grains	60	30–45
	Hardened Aluminum Alloys	0 to −30	
Manufacturing Process	Machine Tool Oil Cooling	70–90	
	Precision Parts Honing Machinery	75–80	40–55
	Ceramic Molding	80	60
	Manufacturing of Electrical Wiring	60–80	35–50
	Assembly Line	65–80	40–50
	Gage Rooms	78	50
	Instrument Calibration	68	50–55
	Match Manufacturing	72–74	50
Research and Development	Paper Testing Laboratory	60–80	55–65
	Textile Testing Laboratory	70	65
	Special Process Temperature Boxes	−100 to +170	
	Chemical Laboratories	78	50
	Fibres and Plastics	70–75	50–65
	Drafting	78–80	45–50
	Temperature Shock Tests	−80 to +150	

[a]Taken from the article, "Indoor Climate and Refrigeration for Post-War Industry," by E. K. Heglin, *Cleveland Engineering*, Vol. 40, No. 27, July 3, 1947, p. 5.

regulating the system operation. Complete specifications of indoor design conditions would include part-load and overload operation, particularly from the viewpoint of economy.

In the field of *industrial air conditioning*, indoor design conditions are established by the requirements of goods and processes, in addition to the comfort and efficiency of the workers. No generally-applicable specifications are possible, as each job has its own special requirements. Table 2 offers illustrative general information.

The indoor design conditions suggested have had reference to conditions to be maintained at the level of occupancy. For extremely high ceilings in public or industrial buildings, only the zone from 10 to 15 ft above the floor may be cooled to the full extent. The air temperature at the ceiling would be much higher, and this should be kept in mind when calculating the convective portion of the roof heat gain. A reduction of outdoor-to-indoor air temperature differential may be assumed in such instances; radiation from the inner roof surface is not diminished.

Outdoor Conditions

Summer climatic conditions and suggested design wet-bulb and dry-bulb temperatures are given in Table 3 for various locations in the United States. The highest temperature ever recorded is for the period of record shown. In some cases it should be noted that this period of record is comparatively short and higher temperatures may be expected. In making comparisons for other localities than those shown in Table 3 due consideration must be given to elevation.

Column 6 of Table 3 indicates the design dry-bulb temperature suggested by the A.S.H.V.E. Technical Advisory Committee on Weather

Design Conditions. This temperature is the maximum hourly outdoor temperature which has been equalled or exceeded 2½ per cent of the total hours of June, July, August and September for the period of record, in this case the 5 year period 1935-1939, and should not be confused with the period of record given in Column 4 which applies only to highest temperature ever recorded. Since all of these data are based on airport records they are not necessarily applicable to cities.

The data given in Columns 7 and 8 were obtained from local A.S.H.V.E. Chapter Secretaries and represent the design temperatures in local use. Where such information was not available it was taken from a publication of the A.C.R.M.A. [1] and from various other sources.

The Technical Advisory Committee on Weather Design Conditions has suggested that wet-bulb design be taken as that wet-bulb temperature which has been equalled or exceeded 5 per cent of the hours during months of the period of record. While not available for the 1948 edition of THE GUIDE due to the tremendous task of compiling these data it is hoped that they will be available for some stations for future editions.

The wind velocity to be used in design should be that wind velocity which accompanies the design temperatures in each instance and since these data are not available the average summer wind velocities are reprinted from THE GUIDE 1947. It is pointed out that this is not necessarily the velocity which coincides with the design temperatures but it may be of some service to the designer.

Ventilation Rate

The introduction of outside air is necessary for proper ventilation of conditioned spaces. Chapter 12 suggests *minimum* outdoor-air requirements for representative applications; but it is to be emphasized that minimum requirements are not necessarily *adequate* requirements for all psychological attitudes and physiological responses.

Local codes and ordinances frequently specify ventilation requirements for public places and for industrial installations.

Recommended and minimum ventilation rates for the most common applications are summarized in Table 4. For further general applications, a basis of estimating the cfm per person may be taken as:

1.	People not smoking	7-½	*Recommended*	5 *Minimum*
2.	People smoking	40	*Recommended*	25 *Minimum*

The cooling load necessitated by the introduction of outside air for ventilation is determined once the indoor and outdoor design conditions are fixed. Calculations will be discussed subsequently.

INSTANTANEOUS HEAT LOAD

The total cooling load is frequently divided for convenience into two components; *sensible heat* and *latent heat.* While this subdivision is not imperative, past practice has found it convenient.

A gain of *sensible heat* is considered to occur when there is a direct addition of heat to the enclosure by any one or all of the mechanisms of conduction, convection, and radiation. A gain of *latent heat* is considered to occur when there is an addition of water vapor to the air of the enclosure. For example, when the humidity in an enclosure is increased by water vapor emitted by human occupants, or by water vapor resulting from a process such as cooking, the heat required to vaporize the water does *not*

TABLE 3. SUMMER CLIMATIC CONDITIONS[a]

Suggested Design Wet-Bulb and Dry-Bulb Temperatures

Col. 1 State	Col. 2 Station[b]	Col. 3 Elevation[c] Ft	Col. 4 Period of Record[d]	Col. 5 Highest Temp. Ever Recorded[d] °F	Col. 6 Design Dry-Bulb Temp. on T.A.C. 2½% Basis[e] °F	Col. 7 Design Dry-Bulb Temp in Common Use[f] °F	Col. 8 Design Wet-Bulb Temp. in Common Use[f] °F	Col. 9 Average Summer Wind Velocity[g] Mph
Ala.	Anniston CO	733	1893-1947	105	.....	95	78	.....
	Birmingham CO	711	1893-1945	107	.....	95	78	5.2
	Birmingham AP	615	1939-1947	103	94	.....	.....	.....
	Mobile CO	143	1872-1947	103	.....	95	80	8.6
	Mobile AP	219	1940-1947	104	92	.....	.....	.....
	Montgomery CO	293	1872-1947	107	.....	95	78	.....
	Montgomery AP	226	1938-1944[d]	103	.....	.....	.....	.....
Ariz.	Flagstaff CO	6957	1899-1947	93	.....	90	65	.....
	Kingman AP	3473	1935-1939	107	99	.....	.....	.....
	Phoenix CO	1122	1895-1947	118	.....	105	76	6.0
	Phoenix AP	1112	1933-1947	117	107	.....	.....	.....
	Tucson AP	2561	1935-1939	112	102	105	72	.....
	Winslow CO	4853	Up to 1946	107	.....	100	70	.....
	Winslow AP	4899	1937-1947	103	95	.....	.....	.....
	Yuma CO	146	1876-1946	120	.....	110	78	.....
Ark.	Fort Smith CO	545	1882-1945	113	.....	95	76	12.0
	Fort Smith AP	463	1945-1947	107	.....	.....	.....	.....
	Little Rock CO	451	1879-1942[d]	110	.....	95	78	6.0
	Little Rock AP	282	1942-1947	107	97	.....	.....	.....
Calif.	Bakersfield AP	499	1937-1946	113	104	105	70	.....
	Burbank AP	740	1931-1947[d]	111	94	.....	.....	.....
	Daggett AP	1925	1935-1939	113	104	.....	.....	.....
	Eureka CO	132	1886-1947	85	.....	90	65	.....
	Fresno CO	387	1887-1939	115	.....	105	70	7.9
	Fresno AP	281	1939-1947	111	103	.....	.....	.....
	Los Angeles CO	534	1877-1947	109	.....	90	70	6.0
	Oakland AP	21	1929-1947	102	80	85	65	.....
	Red Bluff CO	305[e]	1877-1934	115	.....	100	70	.....
	Red Bluff AP	346	1944-1947	112	.....	.....	.....	.....
	Redding AP	579	1935-1939	112	101	.....	.....	.....
	Sacramento CO	116	1877-1947	114	.....	100	72	5.0
	Sacramento AP	22	1938-1947	108	.....	.....	.....	.....
	San Diego CO	90	1871-1940	110	.....	85	68	.....
	San Diego AP	34	1939-1947	106	79	.....	.....	.....
	San Francisco CO	62	1875-1947	101	.....	85	65	11.0
	San Jose CO	100	Up to 1946	106	.....	91	70	.....
	Williams AP	124	1935-1939	116	103	.....	.....	.....
Colo.	Denver CO	5398	1871-1947	105	.....	95	64	6.9
	Denver AP	5379	1934-1947	104	93	.....	.....	.....
	Durango CO	6558	Up to 1946	...	.....	95	65	.....
	Grand Junction CO	4587[e]	Up to 1946	105	.....	95	65	6.1
	Pueblo CO	4770	1889-1938	104	.....	95	65	.....
	Pueblo AP	4810	1939-1947	104	95	.....	.....	.....
Conn.	Hartford CO	229	1905-1940[d]	101	.....	93	75	.....
	Hartford AP	20	1940-1947	98	88	.....	.....	.....
	New Haven CO	180	1872-1947	101	.....	95	75	7.3
	New Haven AP	17	1943-1947	94	84	.....	.....	.....
D. C.	Washington CO	128	1871-1947	106	.....	95	78	5.2
	Washington AP	20	1935-1939	106	92	.....	.....	.....
Fla.	Apalachicola CO	23	1922-1947	102	.....	95	80	.....
	Jacksonville CO	104	1871-1947	104	.....	95	78	8.6
	Jacksonville AP	29	1938-1947	105	94	.....	.....	.....
	Key West CO	23	1871-1947	100	.....	98	78	.....
	Key West AP	48	1939-1947	95	.....	.....	.....	.....
	Miami CO	253	1896-1947	96	.....	91	79	6.4
	Miami AP	13	1940-1947	100	89	.....	.....	.....
	Pensacola CO	67	1879-1947	103	.....	95	78	.....
	Pensacola AP	113	1943-1947	105	.....	.....	.....	.....
	Tampa CO	111	1890-1940	98	.....	95	78	7.0
	Tampa AP	12	1941-1946[d]	98	.....	.....	.....	.....
	Titusville AP	52	1935-1939	98	90	.....	.....	.....
Ga.	Atlanta AP	1020	1935-1939	102	93	95	76	8.5
	Augusta CO	195	1871-1946	106	.....	98	76	.....
	Augusta AP	424	1939-1947	105	.....	.....	.....	.....
	Macon CO	408	1899-1947	105	.....	95	78	.....
	Macon AP	432	1939-1947	102	.....	.....	.....	.....
	Savannah CO	115	1871-1945[d]	105	.....	95	78	7.8
	Savannah AP	56	1939-1947	105	93	.....	.....	.....
Idaho	Boise CO	2818	1864-1939	112	.....	95	65	5.9
	Boise AP	2849	1939-1947	109	95	.....	.....	.....
	Burley AP	4150	1935-1939	104	94	.....	.....	.....
	Idaho Falls AP	4744	1935-1939	100	88	.....	.....	.....
	Lewiston CO	763	1900-1944[d]	117	.....	95	65	.....
	Pocatello CO	4522	1899-1947	105	.....	95	65	.....
	Pocatello AP	4467	1938-1947	103	92	.....	.....	.....
Ill.	Cairo CO	319	1872-1947	106	.....	98	78	.....
	Chicago CO	601	Up to 1946	.....	.....	95	75	10.0
	Chicago AP	615	1935-1939	107	92	.....	.....	.....
	Moline AP	594	1932-1947	106	94	96	76	.....

TABLE 3. SUMMER CLIMATIC CONDITIONS[a] (CONTINUED)

Suggested Design Wet-Bulb and Dry-Bulb Temperatures

COL. 1 STATE	COL. 2 STATION[b]	COL. 3 ELEVATION[c] FT	COL. 4 PERIOD OF RECORD[d]	COL. 5 HIGHEST TEMP. EVER RECORDED[d] °F	COL. 6 DESIGN DRY-BULB TEMP. ON T.A.C. 2½% BASIS[e] °F	COL. 7 DESIGN DRY-BULB TEMP. IN COMMON USE[f] °F	COL. 8 DESIGN WET-BULB TEMP. IN COMMON USE[f] °F	COL. 9 AVERAGE SUMMER WIND VELOCITY[g] MPH
Ill.	Peoria AP	660	1935–1939	111	94	96	76	8.2
	Springfield CO	603	1879–1947	110	.....	98	77	.....
	Springfield AP	608	1930–1947	109	96	....	....	....
Ind.	Evansville CO	464	1897–1940	108	.....	95	78	6.9
	Fort Wayne CO	885	1911–1941[d]	106	.....	95	75	.....
	Helmer AP	970	1935–1939	107	89	..	..	....
	Indianapolis CO	816	1871–1946	106	.....	95	76	9.0
	Indianapolis AP	800	1932–1946	107	91	.. ..	..	...
	Terre Haute CO	1146	1893–1946	110	.....	95	78	....
	Terre Haute AP	589	1941–1946	103	.....	....	.	.....
Iowa	Davenport CO	648	1872–1947	111	.....	95	78	.....
	Des Moines AP	979	1935–1939	111	95	95	78	6.6
	Dubuque CO	740	1874–1947	110	.. .	95	78	....
	Keokuk CO	637	1872–1946	113	.. ..	95	78	.
	Sioux City CO	1093[c]	1889–1944[d]	111		95	78	
	Sioux City AP	1098	1940–1946	108	. .	....	.	.....
Kans.	Concordia CO	1425	1885–1947	116		95	78	....
	Dodge City CO	2515	1874–1942[d]	109	.	95	78	..
	Dodge City AP	2599	1942–1947	109		....	.	....
	Topeka CO	991	1887–1947	114	. .	100	78	.....
	Topeka AP	883	1946–1947	108	....	..	.	...
	Wichita CO	1497	1888–1939	114	. .	100	75	11.4
	Wichita AP	1423	1939–1947	109	100		.	..
Ky.	Louisville CO	563	1871–1947	107	. .	95	78	8.0
	Louisville AP	544	1937–1947	103	93		.	.....
La.	New Orleans CO	85	1874–1947	102	....	95	80	6.2
	New Orleans AP	8	1937–1947	100	93		.	.....
	Shreveport AP	179	1935–1939	109	98	100	78	5.8
Maine	Eastport CO	100	1873–1947	93	.....	90	70	.....
	Portland CO	69	1885–1940	103	. .	90	73	7.3
	Portland AP	65	1940–1947	99	...	....	.	.....
Md.	Baltimore CO	114	1871–1947	107	....	95	78	6.9
	Baltimore AP	43	1935–1939	105	91	...	.	.....
Mass.	Boston CO	356	1870–1935	104	.	92	75	12.5
	Boston AP	45	1936–1947	101	87	.	.	. .
	Nantucket CO	45	1886–1947	92	. .	95	75	..
	Nantucket AP	48	1946–1947	82	.	...	.	....
Mich.	Alpena CO	615	1874–1946	104	....	95	75	...
	Detroit CO	1000	1873–1933	104	.	95	75	10.2
	Detroit AP	632	1934–1947	105	89	..	73[h]	....
	Lansing CO	861	1910–1947	102		95	75	.. .
	Lansing AP	863	1940–1947	98		...	..	.....
	Marquette CO	721	1874–1947	108	. .	93	73	.....
Minn.	Duluth CO	1133	1874–1947	106	.	93	73	.....
	Duluth AP	1413	1941–1947	95		..	.	
	Minneapolis CO	945	1890–1947	108	.	95	75	8.4
	Minneapolis AP	873	1938–1947	104	. .	. .	..	.....
	St. Paul CO	951	1871–1933	104	.	95	75	.....
	St. Paul AP	708	1937–1947	104	91	.	..	.....
Miss.	Meridian CO	410	1889–1947	105	..	95	79	6.2
	Meridian AP	298	1939–1947	105	....	....	.	.....
	Vicksburg CO	316	1874–1947	104	. .	95	78	6.2
	Vicksburg AP	266	1941–1947	104	. .	...	.	.....
Mo.	Columbia CO	739	1889–1947	111	.. ..	100	78	.....
	Columbia AP	787	1939–1947	102	....	....	.	.....
	Kansas City AP	780	1935–1939	112	101	100	76	9.5
	St. Louis CO	646	1871–1947	110	....	95	78	9.4
	St. Louis AP	597	1930–1947	111	97	.. ..	. .	...
	Springfield AP	1270	1935–1939	105	96	.	.	8.7
Mont.	Billings AP	3584	1935–1947	106	92	90	66	.....
	Butte AP	5538	1931–1947	100	85	....	....	.....
	Havre CO	2498	1880–1947	108	. . .	95	70	.....
	Helena CO	4175	1880–1940	103	.....	95	67	8.0
	Kalispell CO	3004	1897–1947	101	..	95	65	.....
	Miles City AP	2629	1935–1939	108	97	....	.	.....
Nebr.	Lincoln CO	1189	1887–1947	115	....	95	78	9.3
	Lincoln AP	1185	1933–1947	115	101	....	....	.....
	North Platte CO	2815	1874–1947	109	....	95	78	8.8
	North Platte AP	2788	1935–1939	109	98	....	....	.....
	Omaha CO	1219	1873–1935[d]	111	....	95	78	.....
	Omaha AP	1009	1935–1947	114	98	....	....	.....
	Valentine CO	2627	1889–1947	110	....	95	78	.....
Nev.	Elko AP	5079	1935–1939	102	92	.....	.....	.....
	Las Vegas AP	1882	1937–1947	117	108	....	....	.....
	Reno CO	4588	1905–1942	106	.....	95	65	7.4
	Reno AP	4417	1940–1947	105	93	....	....	.....
	Winnemucca CO	4293	1871–1947	108	.....	95	65	.....
N. H.	Concord CO	343	1871–1941[d]	102	.....	90	73	5.6
	Concord AP	359	1941–1947	99	.....	.....	.....	.....

TABLE 3. SUMMER CLIMATIC CONDITIONS[a] (CONTINUED)

Suggested Design Wet-Bulb and Dry-Bulb Temperatures

Col. 1 State	Col. 2 Station[b]		Col. 3 Elevation[c] Ft	Col. 4 Period of Record[d]	Col. 5 Highest Temp. Ever Recorded[d] °F	Col. 6 Design Dry-Bulb Temp. on T.A.C. 2½% Basis[e] °F	Col. 7 Design Dry-Bulb Temp. in Common Use[f] °F	Col. 8 Design Wet-Bulb Temp. in Common Use[f] °F	Col. 9 Average Summer Wind Velocity[g] Mph
N. J.	Atlantic City	CO	45	1874-1947	104	...	95	78	...
	Camden	AP	20	1935-1939	105	91	...	...	...
	Newark	AP	15	1931-1947	104	89	95	75	...
	Trenton	CO	144	1866-1946	106	...	95	78	10.0
N. M.	Albuquerque	CO	5022	1931-1933[d]	99	...	95	70	7.6
	Albuquerque	AP	5319	1933-1947	101	93	...	...	...
	El Morro	AP	7120	1935-1939	97	84	...	...	...
	Rodeo	AP	4116	1935-1939	104	97	...	...	...
	Roswell	CO	3643	1905-1947[d]	107	...	95	70	...
	Tucumcari	AP	4054	1935-1939	107	97	...	...	...
N. Y.	Albany	CO	114	1874-1947	104	...	93	75	7.1
	Albany	AP	280	1938-1947	99	88	...	...	...
	Binghamton	CO	915	1891-1946	103	...	95	75	...
	Binghamton	AP	836	1942-1947	97	...	...	...	...
	Buffalo	AP	726	1935-1939	95	86	93	73	12.2
	Canton	CO	458	1906-1947	99	...	90	73	12.9
	Elmira	AP	948	1935-1939	96	88	...	...	...
	New York	CO	425	1871-1947	102	...	95	75	12.9
	Oswego	CO	363	1871-1947	100	...	93	73	...
	Rochester	CO	609	1872-1947	102	...	95	75	...
	Rochester	AP	560	1935-1939	98	89	...	...	...
	Syracuse	CO	465	1902-1940	102	...	93	75	...
	Syracuse	AP	404	1940-1947	97	88	...	...	...
N. C	Ashville	CO	2280	1902-1947	99	...	93	75	5.6
	Charlotte	CO	809	1878-1947	103	...	95	78	...
	Charlotte	AP	757	1939-1947	103	93	...	...	...
	Greensboro	AP	896	1928-1947	101	91	95	78	...
	Raleigh	CO	405	1887-1947	104	...	95	78	5.9
	Raleigh	AP	446	1944-1947	102	93	...	...	...
	Wilmington	CO	78	1871-1947	103	...	95	78	6.9
N. D.	Bismarck	CO	1675	1875-1940	114	...	95	73	8.8
	Bismarck	AP	1655	1940-1947	109	96	...	...	...
	Devils Lake	CO	1481	1904-1947	112	...	95	70	...
	Dickinson	AP	2599	1935-1939	112	94	...	...	...
	Fargo	AP	900	1935-1939	115	93	95	75	...
	Pembina	AP	830	1935-1939	109	92	...	...	...
	Williston	CO	1919	1879-1947	110	...	95	73	...
Ohio	Akron	AP	104	1935-1939	101	88	95	75	...
	Cincinnati	CO	772	1870-1947	108	...	95	78	5.6
	Cincinnati	AP	488	1931-1947	108	94	...	...	...
	Cleveland	CO	669	1871-1946	100	...	95	75	11.2
	Cleveland	AP	813	1930-1946	107	90	...	...	...
	Columbus	CO	812	1878-1946	106	...	95	76	...
	Columbus	AP	820	1939-1947	100	90	...	...	...
	Dayton	CO	1086	1883-1943[d]	108	...	95	78	...
	Dayton	AP	1002	1940-1947	99	...	...	...	...
	Sandusky	CO	608	1878-1946	105	...	95	75	...
	Toledo	CO	668	1871-1947	105	...	95	75	...
	Toledo	AP	626	1940-1947	100	91	...	...	...
Okla.	Ardmore	AP	762	1935-1939	110	99	...	...	...
	Oklahoma City	CO	1264	1890-1947	113	...	101	77	10.1
	Oklahoma City	AP	1311	1939-1947	109	99	...	...	...
	Tulsa	AP	680	1932-1947	109	100	101	77	...
	Waynoka	AP	1529	1935-1939	115	103	...	...	...
Ore.	Arlington	AP	881	1935-1939	111	95	...	...	...
	Baker	CO	3501	1889-1947	104	...	90	66	...
	Baker	AP	3374	1939-1947	103	90	...	...	...
	Eugene	CO	366	1890-1942	104	...	90	68	...
	Eugene	AP	368	1942-1947	105	88	...	...	...
	Medford	CO	1428	1911-1929	110	...	95	70	...
	Medford	AP	1348	1929-1947	115	95	...	...	...
	Portland	CO	98	1874-1947	107	...	90	68	6.6
	Portland	AP	25	1940-1947	105	87	...	...	...
	Roseburg	CO	523	1877-1947	109	...	90	66	...
Pa.	Curwensville	AP	2219	1943-1947	90	82	...	...	...
	Erie	CO	771	1873-1946	98	...	93	75	...
	Erie	AP	736	1935-1939	96	85	...	...	...
	Harrisburg	AP	339	1935-1939	103	91	95	...	...
	Philadelphia	CO	200	1871-1947	106	...	95	78	9.7
	Philadelphia	AP	18	1940-1947	100	...	...	...	...
	Pittsburgh	CO	929	1875-1947	103	...	95	75	9.0
	Pittsburgh	AP	1284	1935-1947	102	88	...	...	...
	Reading	CO	311	1913-1947	105	...	95	75	...
	Scranton	CO	877	1901-1947	103	...	95	75	...
	Sunbury	AP	448	1935-1939	101	89	...	...	...
R. I.	Block Island	CO	46	1881-1947	93	...	95	75	...
	Providence	CO	77	1904-1947	100	...	93	75	10.0
S. C.	Charleston	CO	59	1871-1947	104	...	95	78	9.9
	Charleston	AP	51	1940-1947	103	91	...	...	...

TABLE 3. SUMMER CLIMATIC CONDITIONS[a] (CONCLUDED)

Suggested Design Wet-Bulb and Dry-Bulb Temperatures

COL. 1 STATE	COL. 2 STATION[b]	COL. 3 ELEVATION[c] FT	COL. 4 PERIOD OF RECORD[d]	COL. 5 HIGHEST TEMP. EVER RECORDED[d] °F	COL. 6 DESIGN DRY-BULB TEMP. ON T.A.C. 2½% BASIS[e] °F	COL. 7 DESIGN DRY-BULB TEMP. IN COMMON USE[f] °F	COL. 8 DESIGN WET-BULB TEMP. IN COMMON USE[f] °F	COL. 9 AVERAGE SUMMER WIND VELOCITY[g] MPH
S. C.	Columbia CO	401	1887–1947	106	.....	95	75	.....
	Columbia AP	227	1939–1947[d]	104	.....	.....	.....	.....
S. D.	Huron CO	1342	1881–1938[d]	111	.....	95	75	10.0
	Huron AP	1287	1938–1947	110	.....	.....	.....	.....
	Rapid City CO	3309	1888–1947	106	.....	95	70	7.3
	Rapid City AP	3220	1939–1947	108	.....	.....	.....	.....
Tenn.	Chattanooga CO	952	1879–1947	103	.....	95	76	6.5
	Chattanooga AP	675	1940–1947	105	94	.....	.....	.....
	Knoxville CO	1024	1871–1942[d]	104	.....	95	75	5.8
	Knoxville AP	1007	1942–1947	102	94	.....	.....	.....
	Memphis CO	348	1872–1941[d]	106	.....	95	78	7.4
	Memphis AP	267	1941–1947	105	96	.....	.....	.....
	Nashville CO	714	1871–1947	106	.....	95	78	.....
	Nashville AP	610	1939–1947	104	.....	.....	.....	.....
Texas	Abilene CO	1748	1885–1944[d]	111	.....	100	74	.....
	Abilene AP	1756	1940–1947	109	97	.....	.....	.....
	Amarillo CO	3686	1892–1941	107	.....	100	72	11.5
	Amarillo AP	3595	1941–1947	106	96	.....	.....	.....
	Austin CO	625	1897–1942	109	.....	100	78	.....
	Austin AP	625	1942–1947	104	.....	.....	.....	.....
	Brownsville CO	140	1922–1943[d]	102	.....	100	80	7.0
	Brownsville AP	25	1943–1947	100	.....	.....	.....	.....
	Corpus Christi CO	21	1887–1942	105	.....	102	95	.....
	Corpus Christi AP	45	1943–1946	101	.....	.....	.....	.....
	Dallas CO	732	1913–1940	110	.....	100	78	9.4
	Dallas AP	520	1940–1947	109	99	.....	.....	.....
	Del Rio CO	1020	1905–1947	111	.....	100	78	.....
	El Paso CO	3792	1887–1942	106	.....	100	69	8.6
	El Paso AP	3956	1939–1947	104	97	.....	.....	.....
	Fort Worth CO	708	1898–1939	112	.....	100	78	9.4
	Fort Worth AP	728	1940–1947	110	.....	.....	.....	.....
	Galveston CO	128	1871–1947	101	.....	95	80	9.7
	Galveston AP	9	1939–1947	101	.....	.....	.....	.....
	Houston CO	198	1888–1947	108	.....	95	78	7.7
	Houston AP	73	1932–1947	105	93	.....	.....	.....
	Palestine CO	555	1881–1947	108	.....	100	78	.....
	Port Arthur CO	64	1917–1947	102	.....	95	79	.....
	Port Arthur AP	21	1944–1947	98	.....	.....	.....	.....
	San Antonio CO	770	1885–1941[d]	107	.....	100	78	7.3
	San Antonio AP	800	1942–1947	104	98	.....	.....	.....
	Waco AP	513	1931–1947	111	98	.....	.....	.....
	Wink AP	2811	1935–1939	110	99	.....	.....	.....
Utah	Milford AP	5095	1935–1939	103	94	.....	.....	.....
	Modena CO	5472	1901–1947	101	.....	95	65	.....
	Salt Lake City CO	4346	1874–1947	105	.....	95	65	8.2
	Salt Lake City AP	4254	1928–1947	106	95	.....	.....	.....
Vt.	Burlington CO	409	1884–1943[d]	100	.....	90	73	8.9
	Burlington AP	335	1943–1947	101	.....	.....	.....	.....
Va.	Cape Henry CO	24	1874–1947	104	.....	95	78	.....
	Lynchburg CO	644	1874–1944	106	.....	95	75	.....
	Lynchburg AP	951	1944–1947	100	.....	.....	.....	.....
	Norfolk CO	91	1871–1947	105	.....	95	78	10.9
	Richmond CO	180	1897–1947	107	.....	95	78	6.2
	Richmond AP	172	1929–1947	104	92	.....	.....	.....
	Roanoke AP	1194	1935–1939	103	90	95	76	.....
Wash.	Ellensburg AP	1731	1935–1939	105	90	.....	.....	.....
	North Head CO	199	1884–1947	97	.....	85	65	.....
	Seattle CO	104	1890–1947	100	.....	85	65	8.1
	Seattle AP	47	1928–1947	99	81	.....	.....	.....
	Spokane CO	2030	1881–1941[d]	108	.....	93	65	6.5
	Spokane AP	1974	1941–1947	104	92	.....	.....	.....
	Tacoma CO	279	1897–1947	98	.....	85	64	.....
	Tatoosh Island CO	110	1883–1947	88	.....	.....	.....	.....
	Yakima CO	1160	1928–1946	110	.....	95	65	.....
	Yakima AP	1066	1944–1947	103	.....	.....	.....	.....
W. Va.	Parkersburg CO	685	1888–1947	106	.....	95	75	5.3
Wisc.	Green Bay CO	598	1886–1947	104	.....	95	75	9.1
	LaCrosse CO	725	1872–1947	108	.....	95	75	6.4
	LaCrosse AP	677	1943–1947	96	91	.....	.....	.....
	Madison CO	1008	1858–1947	107	.....	95	75	8.1
	Madison AP	884	1935–1939	106	89	.....	.....	.....
	Milwaukee CO	744	1870–1947	105	.....	95	75	10.4
	Milwaukee AP	707	1927–1947	106	87	.....	.....	.....
Wyo.	Cheyenne CO	6144	1873–1935	100	.....	95	65	9.2
	Cheyenne AP	6161	1935–1947	100	89	.....	.....	.....
	Lander CO	5448	1891–1946	102	.....	95	65	.....
	Lander AP	5568	1936–1947	97	.....	.....	.....	.....
	Rock Springs AP	6746	1932–1942	98	87	.....	.....	.....

NOTES FOR TABLE 3

[a]Data compiled from U. S. Weather Bureau Data and various other sources.

[b]Column 2. The station designation AP or CO indicates airport or city office station respectively.

[c]Column 3. The elevations marked c are ground elevations of the station. All other elevations given are the actual elevations of the thermometer bulb above mean sea level.

[d]The periods of record indicated apply only to the highest temperature ever recorded shown in Column 5, and do not necessarily include all of the summer months of the first year indicated. The last year indicated includes July or August except those marked d which terminate prior to July of that year.

[e]It should be noted that Column 6 applies only to airports, as these data for city stations are not available at this time. The temperature shown is the maximum hourly outdoor temperature which has been equalled or exceeded 2½ per cent of the total hours of June, July, August and September for the 5 year period 1935-1939 inclusive. It is pointed out that in most cases the airport stations are outside of the city, and that these data would apply primarily to rural areas.

[f]Columns 7 and 8 record wet and dry-bulb temperatures in use by A.S.H.V.E. Members as reported by Chapter Secretaries for various stations. Where such values were not available, the design temperatures published by A.C.R.M.A. or obtained from various other sources, have been inserted.

[g]The average wind velocities indicated in Column 9 are repeated from the 1947 Guide with a few additions and corrections where other weather data have been made available. In general these velocities are averages for the months of June through September.

[h]The bulletin published by A.S.H.V.E. for the annual weather data of Detroit indicates 73 F as the design wet-bulb temperature which has been equalled or exceeded 5 per cent of the hours for period 1935-1939.

[i]Blank spaces indicate data not available.

come from the air. Maintenance of a constant humidity ratio in a sealed enclosure requires the condensation of water vapor in the cooling apparatus at a rate equal to its rate of addition within the enclosure. The rate of heat removal from this condensing vapor would be substantially equal to the product of the rate of condensation and the latent heat of condensation; this product, expressed in Btu per hour, would be called a *latent heat* load.

TABLE 4. VENTILATION STANDARDS[a]

APPLICATION	SMOKING	CFM PER PERSON		CFM PER SQ FT OF FLOOR
		Recommended	Minimum[b]	Minimum[b]
Apartment Average	Some	20	10	.....
Deluxe	Some	30	25	0.33
Banking Space	Occasional	10	7½	.....
Barber Shops	Considerable	15	10	.....
Beauty Parlors	Occasional	10	7½	.....
Brokers' Board Rooms	Very Heavy	50	20	.....
Cocktail Bars	Heavy	40	25	.....
Corridors (Supply or Exhaust)		.....	.....	0.25
Department Stores	None	7½	5	0.05
Directors' Rooms	Extreme	50	30	.....
Drug Stores[d]	Considerable	10	7½	.....
Factories[e,o]	None	10	7½	0.10
Five and Ten Cent Stores	None	7½	5	.....
Funeral Parlors	None	10	7½	.....
Garages[e]		.....	.....	1.0
Hospitals Operating Rooms[e,f]	None	.....	.....	2.0
Private Rooms	None	30	25	0.33
Wards	None	20	10	.....
Hotel Rooms	Heavy	30	25	0.33
Kitchens Restaurant		.....	.....	4.0
Residence		.....	.....	2.0
Laboratories[d]	Some	20	15	.....
Meeting Rooms	Very Heavy	50	30	1.25
Offices General	Some	15	10	.....
Private	None	25	15	0.25
Private	Considerable	30	25	0.25
Restaurant Cafeteria[d]	Considerable	12	10	.....
Dining Room[d]	Considerable	15	12	.....
School Rooms[e]	None	.....	.....	.....
Shop, Retail	None	10	7½	.....
Theater[e]	None	7½	5	.....
Theater	Some	15	10	.....
Toilets[e] (Exhaust)		.....	.....	2.0

[a]Taken from present-day practice or large air conditioning companies. [b]When minimum is used, take the larger of the two. [e]See local codes which may govern. [d]May be governed by exhaust. [e]May be governed by special sources of contamination or local codes. [f]All outside air recommended to overcome explosion hazard of anesthetics.

As a further example, the infiltration of outdoor air with a high dry-bulb temperature and a high humidity ratio and the corresponding escape of room air at a lower dry-bulb temperature and a lower humidity ratio would increase both the *sensible heat load* and the *latent heat load.*

SOLAR AND SKY RADIATION AND TRANSMISSION LOSSES

Magnitude of Solar Radiation—Calculation Tables

If a plane surface were set perpendicular to the rays of the sun (*e.g.*, for *normal incidence*) outside the earth's atmosphere, it would receive solar radiation of about 420 Btu per (hr) (sq ft). A similar receiving surface on the surface of the earth would receive radiant energy at a considerably lower rate because a large part of the radiation entering the atmosphere is *scattered* in passing through the air, moisture, smoke, and dust which comprise the earth's envelope. Also, some of the atmospheric constituents, notably water vapor, carbon dioxide, and ozone, *absorb* radiant energy. This absorption and scattering cause different proportionate reductions from outer-atmosphere radiation intensity with different wavelengths. An exact analysis of these phenomena is beyond the practical purposes of air-conditioning load estimates; the important principle to remember is that the radiation reaching the surface of the earth comprises the sum of two components, namely:

I_n = The *direct radiation* (at normal incidence), which is the *transmitted fraction* of the net sun radiation received by the outer atmosphere, and

I_s = The *sky* or *diffuse* radiation coming *from the atmosphere itself* as a consequence of the scattering and absorption which give rise, in part, to a re-radiation to the earth. The diffuse radiation does not strike only at normal incidence; it strikes at *all* angles from which the sky *sees* the surface in question.

Standardized, practical-purpose values of the *direct* solar radiation incident upon a plane perpendicular to the sun's rays at the earth's surface have been proposed by P. Moon.[2] Table 5 gives these data; they are representative of a *clear* summer day at about sea-level elevation. (For industrial areas, I_n values will be slightly less than Table 5, with the greatest decrease occurring at low solar altitudes towards evening.)

Practical design data on *sky* radiation are meager. Table 6 presents a basis of estimates for *clear* summer days in terms of the direct solar radiation to sky radiation ratio.

The *solar altitude* is the angle (see Fig. 1) between the sun's rays and the horizontal.

In the usual application the receiving surface (*e.g.*, building roof or wall) will not be perpendicular to the rays of the sun. The intensity of the

TABLE 5. PROPOSED STANDARD VALUES OF I_n, DIRECT SOLAR RADIATION RECEIVED AT NORMAL INCIDENCE, AT THE EARTH'S SURFACE[a, b]

SOLAR ALTITUDE, β DEG	I_n BTU PER (HR) (SQ FT)	SOLAR ALTITUDE, β DEG	I_n BTU PER (HR) (SQ FT)	SOLAR ALTITUDE, β DEG	I_n BTU PER (HR) (SQ FT)
5	65	30	234	60	276
10	122	35	245	70	283
15	165	40	253	80	289
20	196	45	260	90	294
25	219	50	266		

[a] Calculated using the following assumptions: barometric pressure of 760 mm Hg (29.921 in.); depth of precipitable water of 20 mm (0.787 in.); dust particles, by counting, 300 per cc; partial pressure of the ozone layer in the atmosphere of 2.8 mm Hg (0.110 in.). This is representative of a *clear* summer day.

[b] For sea level. As an approximate altitude correction, *add* 1 per cent for each 1000 ft altitude.

TABLE 6. APPROXIMATE RATIO OF DIRECT SOLAR RADIATION TO SKY RADIATION RECEIVED ON A HORIZONTAL SURFACE ON CLEAR DAYS IN EASTERN STATES[a]

SOLAR ALTITUDE, β DEG	RATIO e	SOLAR ALTITUDE, β DEG	RATIO e	SOLAR ALTITUDE, β DEG	RATIO e
0	0	40	3.84	70	5.63
10	1.40	50	4.55	80	5.90
20	2.30	60	5.20	90	6.10
30	3.10				

[a]For rough estimates assume that the sky radiation on a *vertical* surface is one half of that on a horizontal surface. Sky radiation may be assumed independent of vertical-surface orientation.

direct radiation incident upon a surface, Btu per (hour) (square foot of absorbing surface), which is oriented with an angle of incidence θ for the sun's rays, is

$$I_d = KI_n, \tag{1}$$

where I_d = Intensity of incident direct radiation, Btu per (hour) (square foot of absorbing surface).

I_n = Intensity of direct radiation on a plane normal to the sun's rays, Btu per (hour) (square foot), (from Table 5).

K = Cosine of the angle of incidence θ.

The angle of incidence (see Fig. 2) is the angle between the sun's rays and the normal to the absorbing surface.

For *horizontal* surfaces the magnitude of K is determined by the time of year, the time of day (sun's position), and the latitude of the location concerned. For *vertical* surfaces, a fourth factor is needed: the *azimuth* of the surface. The azimuth (see Fig. 3) is the angle, measured clockwise, from the south to the exterior side of the wall in question.

Complete tabulated calculations are available for magnitudes of the factor K, extending over all latitudes, all azimuths, all months of the year, and all hours of the day.[3] Illustrative excerpts are given in Tables 7 and 8. Data of this type are valuable for all manner of problems involving solar radiation, and not only for cooling-load calculations.

The reader is warned that values of K from Tables 7 and 8 include only the *direct* radiation; *sky* radiation must be calculated separately and added to the direct radiation (see Table 6).

The use of Tables 5, 6, 7, and 8 requires that the relation between solar altitude and mean sun time be available in convenient form. Table 9 provides this information.

The preceding discussion has been concerned only with *incident* radiation. When radiation is incident upon a surface, part is reflected, part is absorbed, and, if the material transmits radiant energy, part is transmitted. Moreover, the building surfaces themselves *send out* radiant

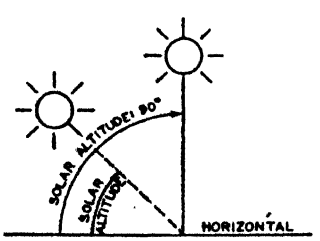

FIG. 1. DEFINITION OF SOLAR ALTITUDE

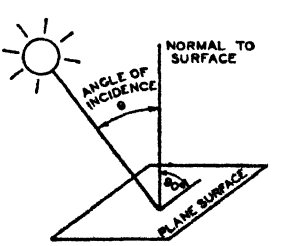

FIG. 2. DEFINITION OF ANGLE OF INCIDENCE

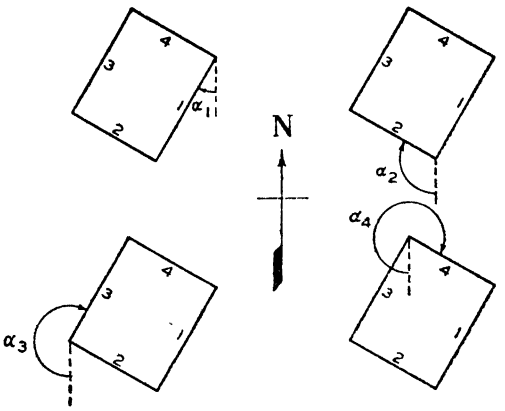

FIG. 3. DEFINITION OF AZIMUTH

The azimuth angle α is always measured clockwise from the south to the exterior side of the wall in question.

energy to the sky and to the surroundings. The heat balance on an outer surface, for a unit time interval, may be expressed as follows:

$$\left.\begin{matrix}\text{Heat entering}\\ \text{outer surface}\end{matrix}\right\} = \left\{\begin{matrix}\text{Incident direct}\\ \text{solar radiation}\end{matrix}\right. + \left\{\begin{matrix}\text{Incident sky}\\ \text{radiation}\end{matrix}\right. - \left\{\begin{matrix}\text{Reflected direct}\\ \text{radiation}\end{matrix}\right. - \left\{\begin{matrix}\text{Reflected sky}\\ \text{radiation}\end{matrix}\right. - \left\{\begin{matrix}\text{Radiation emitted}\\ \text{to sky by surface}\end{matrix}\right. \pm \left\{\begin{matrix}\text{Air-to-surface}\\ \text{convection}\end{matrix}\right. \quad (2)$$

The convective heat transfer may be either to or from the surface, depending upon whether the air temperature is higher or lower than the surface temperature. No term has been included to represent radiation exchange with other objects in the surroundings, as this effect is not usually of significant magnitude relative to the others.

In practical calculations, the *difference* between incident and reflected radiation is computed by multiplying the incident radiation by a factor called the absorptivity or the emissivity; see Table 6 and Equation 3, Chapter 5. Convection is calculated as explained in Chapters 5 and 6.

The daytime radiation emitted to the sky by a surface is not usually calculated as a separate item in practical air-conditioning work. Its effect may be roughly accounted for by an adjustment of the magnitude of the absorptivity factor for solar radiation, and this approach is often followed in making emissivity measurements for building materials exposed to

TABLE 7. VALUES OF K FOR HORIZONTAL PLANES IN NORTH LATITUDES[a] DURING THE PERIOD MAY 2-AUGUST 10

LOCAL MEAN SUN TIME[b]		NORTH LATITUDE—DEGREES					
A.M.	P.M.	25	30	35	40	45	50
5	7	.....	.....	.....	.034	.070	.106
6	6	.145	.171	.196	.220	.242	.262
7	5	.365	.382	.395	.406	.414	.418
8	4	.570	.578	.581	.580	.574	.564
9	3	.747	.746	.740	.729	.712	.689
10	2	.882	.876	.863	.843	.817	.785
11	1	.967	.957	.940	.915	.884	.845
12		.996	.985	.966	.940	.906	.866

[a]Figured for solar declination of 20 deg. [b]The relation between local mean sun time and civil time may be obtained from Weather Bureau offices in various localities.

TABLE 8. VALUES OF K FOR VERTICAL PLANES IN NORTH LATITUDES DURING THE PERIOD MAY 2-AUGUST 10

Latitude[a] Deg	Local Mean Sun Time[b] A.M. → / P.M. →	Azimuth Scales for Values of K in Ordinary Type[c] 0 / 180	15 / 165	30	45	60	75	90	105	120	135	150	165	180
30	6 / 6	.940	.831	.666	.455	.213	*.043*	*.296*	*.529*	*.726*	*.874*	*.962*	*.984*	*.940*
	7 / 5	.908	.832	.699	.518	.303	.066	*.175*	*.404*	*.605*	*.765*	*.873*	*.922*	*.908*
	8 / 4	.814	.770	.674	.532	.354	.151	*.061*	*.270*	*.480*	*.619*	*.735*	*.802*	*.814*
	9 / 3	.664	.651	.593	.495	.363	.207	.036	*.137*	*.301*	*.444*	*.557*	*.632*	*.664*
	10 / 2	.470	.482	.462	.410	.331	.229	.111	*.015*	*.139*	*.254*	*.352*	*.425*	*.470*
	11 / 1	.243	.276	.289	.283	.258	.217	.158	.089	.015	*.061*	*.132*	*.194*	*.243*
	12 / 12	.000	.045	.087	.123	.150	.168	.174	.168	.150	.123	.087	.045	.000
45	5 / 7	.908	.770	.579	.349	*.095*	*.165*	*.414*	*.635*	*.812*	*.934*	*.993*	*.984*	*.908*
	6 / 6	.940	.845	.693	.493	.260	.010	*.242*	*.477*	*.679*	*.835*	*.935*	*.970*	*.940*
	7 / 5	.908	.859	.751	.592	.393	.167	*.070*	*.302*	*.514*	*.691*	*.821*	*.895*	*.908*
	8 / 4	.814	.809	.750	.639	.485	.298	.090	*.123*	*.329*	*.512*	*.660*	*.763*	*.814*
	9 / 3	.664	.701	.689	.631	.530	.392	.228	.048	*.135*	*.309*	*.461*	*.583*	*.664*
	10 / 2	.470	.540	.574	.568	.524	.444	.334	.201	.054	*.096*	*.240*	*.368*	*.470*
	11 / 1	.243	.338	.411	.455	.468	.449	.400	.323	.225	.111	*.011*	*.131*	*.243*
	12 / 12	.000	.109	.211	.299	.366	.408	.423	.408	.366	.299	.211	.109	.000
	P.M. → / A.M. →	360 / 180	345 / 195	330 / 210	315 / 225	300 / 240	285 / 255	270 / 270	255 / 285	240 / 300	225 / 315	210 / 330	195 / 345	180 / 360
	Time	Azimuth Scales for Values of K in Italicized Type												

[a] Values for 30 deg latitude may be employed over the range 25 deg to 35 deg. Values for 45 deg latitude may be employed over the range 40 deg to 50 deg. Interpolation will yield values for the range 35 deg to 40 deg latitude.

[b] The relation between local mean sun time and civil time may be obtained from Weather Bureau offices in various localities.

[c] Values in ordinary type are for azimuths 0 to 180 deg. Values in italic type are for azimuths 180 to 360 deg.

the sun and sky. During the night, however, the emitted radiation becomes very important.

Radiation Exchange with the Night Sky

When a building surface is exposed to a *clear* night sky, the net exchange of radiant energy is *from* the surface to the sky. This acts to decrease the load on an air-conditioning system. For practical calculations, it will serve to cite Brunt's equation as given by Haurwitz [4],

$$q_s = 0.173\,\varepsilon \left(\frac{T}{100}\right)^4 (0.56 - 0.47\sqrt{P_d}) \qquad (3)$$

where q_s = Net radiation exchange between a surface and the night sky, Btu per (hour) (square foot).

ε = Emissivity of the surface, dimensionless (for the surface temperature involved, and *not* for solar radiation).

T = Surface temperature, (Fahrenheit degrees absolute).

P_d = Partial pressure of the atmospheric water vapor at the earth's surface, inches of mercury.

Equation 3 is not applicable to either extremely low or extremely high values of P_d; (P_d is the saturation pressure corresponding to the dew point). Clouds will decrease appreciably the magnitude of this radiation exchange. Calculations from Brunt's equation should be reduced by a factor of ⅔ to ⅓ where cloudiness is involved. For vertical surfaces the resultant should be reduced about ½.

The Sol-Air Temperature

A convenient way of combining the effects of solar and sky radiation, solar absorptivity, temperature, and air movement is to use the concept of sol-air temperature. The sol-air temperature, t_e, is the temperature of

TABLE 9. RELATION BETWEEN LOCAL MEAN SUN TIME AND SOLAR ALTITUDE DURING THE PERIOD MAY 2-AUGUST 10 FOR NORTH LATITUDES

LOCAL MEAN SUN TIME		SOLAR ALTITUDE					
		NORTH LATITUDE— DEGREES					
A.M.	P.M.	25	30	35	40	45	50
5	7	0	0	0	2.	4.	6
6	6	8.5	10.	11.	12.5	14.	15.
7	5	21.5	22.5	23.5	24.	24.5	24.5
8	4	35.	34.5	35.5	35.5	35.	34.5
9	3	48.5	48.	47.5	47.	45.5	43.5
10	2	62.	61.	59.5	57.5	55.	51.5
11	1	75.5	73.	70.	66.	62.	57.5
12		85.	80.	75.	70.	65.	60.

outdoor air which, in contact with the weather side of a material that is receiving no solar or sky radiation, would give the same rate of heat entry into that surface as would exist with the actual combination of incident solar and sky radiation and convective heat transfer.

In order to calculate the rate of heat transfer into an outside building surface for any instant of time, it is necessary to consider:

1. The intensity of direct solar radiation striking the surface.
2. The absorptivity of the surface for direct solar radiation.
3. The intensity of sky radiation striking the surface.
4. The absorptivity of the surface for sky radiation.
5. The rate at which the surface emits radiation to the sky.
6. The temperature of the surrounding air.
7. The temperature of the outer building surface.
8. The unit convective conductance for heat transfer between the air and the building surface. The magnitude of the convective conductance depends upon the position of the surface and the velocity of the wind or air currents.

The simultaneous consideration of all these effects is too complex for practical application and therefore the sol-air temperature is developed as follows:

1. The equation for the rate of heat transfer into the weather side of a sunlit building material at any instant is written:

$$\left(\frac{q}{A}\right)_L = bI_t + f_o\,(t_o - t_L) \text{ Btu per (hour) (square foot).} \tag{4}$$

where b = Absorptivity of weather side of material for incident solar and sky radiation, dimensionless.
I_t = Rate of incidence of solar and sky radiation, Btu per (hour) (square foot).
t_o = Outside air temperature, Fahrenheit degrees.
t_L = Temperature of weather surface of the material, Fahrenheit degrees.
f_o = Unit convective conductance, Btu per (hour) (square foot) (Fahrenheit degree).

2. The sol-air temperature is defined as:

$$t_e = t_o + \frac{bI_t}{f_o} \tag{5}$$

3. Then, the instantaneous rate of heat entry into the weather side of the structure becomes:

$$\left(\frac{q}{A}\right)_L = f_o\,(t_e - t_L) \text{ Btu per (hour) (square foot)} \tag{6}$$

Example 1. If $t_a = 90$ F, $b = 0.7$, $I = 200$ Btu per (hour) (square foot), and $f_o = 4$, find the sol-air temperature, t_e. Substituting these values in Equation 5:

$$t_e = 90 + \frac{0.7\ (200)}{4} = 125\ \text{F}.$$

Thus the instantaneous rate of entry of heat into the weather side of this material is precisely the same as if the air temperature were 125 F with no solar and sky radiation exchange with the surface.

The preceding sol-air concept is intended for non-glass building areas. For glass surfaces a similar method could be developed, with the addition of terms to account for absorption within the material and outward radiation from the interior space. It is customary, however, to treat glass separately; see section on Glass Areas in this chapter.

The sol-air temperature is a composite quantity the magnitude of which is influenced by each of the variables entering its defining equation. Establishing its magnitude for design calculations is part of the broad problem of determining weather-design data. Sufficient studies have been completed, however, to produce some sol-air data of practical value.

Data of the U. S. Weather Bureau for the 10-year period from 1932 through 1941 have been studied for New York, N. Y.,[5] and Lincoln, Nebr.[6] Only simultaneous values of the air temperature and solar and sky radiation have been combined in determining design values of the sol-air temperature for various surfaces at different times of day in these localities. Since the 24-hour average of the sol-air temperature is greater in July than for any other month at both stations, the sol-air temperature at each hour in July, which was equalled or exceeded at that hour only 16 times in 310 observations, was chosen as the *design* sol-air temperature.

Summer design sol-air temperatures are given in Table 10 for New York, N. Y.; Table 11 gives similar data for Lincoln, Nebr. These data may be taken as representative for similar places in northern latitudes in the United States.

Tables 10 and 11, referring to New York for an industrial area and to Lincoln, Nebr., for a non-industrial area, can be used to determine sol-air temperatures for other locations and conditions by applying corrections as explained in the following paragraphs (using the same symbols as given in Tables 10 and 11 but indicated by (') for other conditions):

1. To adjust the data in Tables 10 and 11 for the variation of I_t with latitude:

a. Compute I'_t for the latitude in question from the data presented previously in this chapter. (For smoky industrial areas, decrease the direct radiation from Table 5 by 15 to 20 per cent for afternoon hours.)

b. Determine the difference $(I'_t - I_t)$ and multiply this by 0.25. Find $I_t = (f_o/b)$ $(t_e - t_o)$ from Tables 10 and 11.

c. Add (algebraically) the difference 0.25 $(I'_t - I_t)$ to the data tabulated.

2. To adjust the data in Tables 10 and 11 for variations in t_o:

a. Establish the magnitude of t'_o at the locality in question.

b. Determine the difference $(t'_o - t_o)$.

c. Add (algebraically) the difference $(t'_o - t_o)$ to the data tabulated.

3. To adjust the data in Tables 10 and 11 to other magnitudes of b/f_o than 0.25:

a. For New York or Lincoln, merely interpolate or extrapolate the tabulated data by direct proportion, using the column for $b/f_o = 0$.

b. For other localities, first determine $t'_e = t'_o + b/f_o\, I'_t$ for $b/f_o = 0$ and $b/f_o = 0.25$. Then interpolate or extrapolate by direct proportion as before.

Sol-air data for a particular locality may be adjusted for different azimuths of the vertical surface in question in a similar manner; although,

TABLE 10. SUMMER DESIGN SOL-AIR TEMPERATURES FOR NEW YORK, N. Y. (NORTH LATITUDE 40°46′; ELEVATION 180 FT)

MEAN SUN TIME	SOL-AIR TEMPERATURE, t_e FAHRENHEIT DEGREES					
	Any Surface[b]	Horizontal	North	East	South	West
Ratio[a]: $\frac{b}{f_o}$	0	0.25	0.25	0.25	0.25	0.25
12 midnight	79	79	79	79	79	79
1 a.m.	78	78	78	78	78	78
2	77	77	77	77	77	77
3	77	77	77	77	77	77
4	76	76	76	76	76	76
5	76	76	76	76	76	76
6	76	81	80	89	77	77
7	80	96	85	106	82	82
8	82	110	85	114	86	85
9	86	127	90	120	97	90
10	88	137	92	114	104	92
11	90	148	94	106	111	94
12 noon	92	155	97	97	115	98
1 p.m.	93	154	98	98	117	108
2	94	152	99	99	112	126
3	94	144	99	99	102	136
4	94	136	99	99	99	145
5	93	121	103	97	97	140
6	90	106	106	93	93	134
7	88	93	102	90	90	115
8	85	85	85	85	85	85
9	83	83	83	83	83	83
10	82	82	82	82	82	82
11	81	81	81	81	81	81
24-hr avg. t_m	84.8	106.4	88.5	92.3	90.7	96.5

[a] b = surface absorptivity, dimensionless.
f_o = unit convective conductance, Btu per (hr) (sq ft) (F deg).
[b] Values in this column are magnitudes of t_o, the outdoor air temperature.

TABLE 11. SUMMER DESIGN SOL-AIR TEMPERATURES FOR LINCOLN, NEBR. (NORTH LATITUDE 40°50′; ELEVATION 1225 FT)

MEAN SUN TIME	SOL-AIR TEMPERATURE, t_e FAHRENHEIT DEGREES					
	Any Surface[b]	Horizontal	North	East	South	West
Ratio[a]: $\frac{b}{f_o}$	0	0.25	0.25	0.25	0.25	0.25
12 midnight	89	89	89	89	89	89
1 a.m.	88	88	88	88	88	88
2	86	86	86	86	86	86
3	84	84	84	84	84	84
4	84	84	84	84	84	84
5	82	82	82	82	82	82
6	81	87	88	100	82	82
7	82	103	93	125	85	85
8	88	124	94	137	92	92
9	93	143	98	142	104	98
10	96	160	102	138	115	102
11	100	172	106	129	125	106
12 noon	102	178	108	115	130	108
1 p.m.	104	180	110	110	132	119
2	106	178	112	112	131	137
3	107	170	113	113	126	150
4	107	158	112	112	117	158
5	106	142	113	110	110	157
6	105	126	117	108	108	149
7	102	109	113	104	104	128
8	98	99	98	98	98	98
9	94	94	94	94	94	94
10	92	92	92	92	92	92
11	90	90	90	90	90	90
24-hr avg. t_m	94.4	121.6	98.6	105.9	102.1	106.6

[a] b = surface absorptivity, dimensionless.
f_o = unit convective conductance, Btu per (hr) (sq ft) (F deg).
[b] Values in this column are magnitudes of t_o, the outdoor air temperature.

all things considered, a simple interpolation between the four points of the compass should serve for all but the most accurate calculations.

An example of the use of the tables in determining sol-air temperature is given.

Example 2. Find the summer design sol-air temperature in New York, N. Y., for a west wall which has a solar absorptivity of 0.7, at a sun time of 3:00 p. m.

$$\text{Use } f_o = 4; \text{ then } \frac{b}{f_o} \text{ for this wall is } \frac{0.7}{4.0} \text{ or } 0.175.$$

From Table 10: for $\frac{b}{f_o} = 0$, $t_e = 94$ F; for $\frac{b}{f_o} = 0.25$, $t_e = 136$ F; and by linear interpolation for this wall:

$$t_e = 94 + \frac{0.175}{0.25}(136 - 94) = 94 + 29 = 123 \text{ F}.$$

Sol-air temperatures are especially helpful in the calculation of periodic heat transfer, as will be illustrated in the material which follows.

PRINCIPLES OF PERIODIC HEAT FLOW

Calculation principles for periodic heat flow are dealt with briefly in this section; in the section which follows, practical tables will be given to facilitate rapid design estimates.

Time Lag

The fundamental analysis of periodic heat flow is complicated when compared with steady-state calculations on account of the time-variable storage of heat from point to point through a wall or roof. The cyclic variation of outdoor conditions produces a related cyclic variation of temperature and heat flow throughout each structural section exposed to the weather. The cyclic variations undergo a progressive *shift in phase* and *decrease in amplitude* in going through a wall with constant conditions maintained in the indoor space.

By a *shift in phase* is meant that as the cyclic temperature wave passes through the wall, the time of occurrence of the maximum temperature at any point shifts farther and farther behind the time of the outer-surface maximum for successive positions through the wall. The resultant *time lag* between the outer-surface and inner-surface maximum temperatures is important, for it may be the determining factor in fixing the time of the maximum cooling load.

By a *decrease in amplitude* is meant that as the cyclic temperature wave passes through the wall, the difference between the maximum temperature of a cycle and the mean temperature of the cycle, which is the amplitude of the wave by definition, decreases progressively as the wave passes through the wall. The magnitude of the *temperature amplitude* at the inner wall surface is necessary for the determination of the instantaneous rate of heat transfer to the indoor space.

Practical design data for periodic heat flow comprise a means of determining the time lag and amplitude decrement for different wall constructions and any given outdoor cycle of sol-air temperature. Both analytical and experimental studies have been made on this problem[7]. While the analytical solution has been written, it is far too detailed for direct use in rapid practical work; and the extensive numerical work required to establish a basis for simplified calculations has been only

TABLE 12. PERIODIC HEAT FLOW DATA FOR HOMOGENEOUS WALLS OR ROOFS

MATERIAL	THICKNESS, IN.	OVER-ALL COEFFICIENT, BTU PER (HR) (SQ FT) (°F) U[a]	THERMAL RESISTANCE OF SOLID MATERIAL, (HR) (SQ FT) (°F)/BTU $\frac{L}{k}$	TIME LAG, HR	FACTOR, λ, IN EQUATION 5			
					Horizontal and North	East	South	West
Stone	8	0.67	0.64	5.5	0.51	0.36	0.48	0.42
	12	0.55	0.96	8.0	0.28	0.19	0.26	0.22
	16	0.47	1.28	10.5	0.17	0.10	0.15	0.13
	24	0.36	1.92	15.5	0.06	0.03	0.05	0.04
Solid Concrete	2	0.98	0.17	1.1	0.93	0.87	0.92	0.89
	4	0.84	0.33	2.5	0.79	0.68	0.76	0.72
	6	0.74	0.50	3.8	0.61	0.46	0.58	0.51
	8	0.66	0.67	5.1	0.49	0.33	0.46	0.39
	12	0.54	1.00	7.8	0.29	0.17	0.26	0.22
	16	0.46	1.33	10.2	0.17	0.09	0.15	0.12
Common Brick	4	0.60	0.80	2.3	0.83	0.75	0.81	0.78
	8	0.41	1.60	5.5	0.51	0.39	0.49	0.44
	12	0.31	2.40	8.5	0.26	0.17	0.25	0.21
	16	0.25	3.20	12.0	0.13	0.08	0.12	0.10
Face Brick	4	0.77	0.44	2.4	0.81	0.70	0.78	0.74
Wood	½	0.68	0.62	0.17	1.0	1.0	1.0	1.0
	1	0.48	1.25	0.45	1.0	0.99	0.99	0.99
	2	0.30	2.50	1.3	0.98	0.91	0.96	0.94
Insulating Board	½	0.42	1.51	0.08	1.0	1.0	1.0	1.0
	1	0.26	3.03	0.23	1.0	1.0	1.0	1.0
	2	0.14	6.05	0.77	1.0	1.0	1.0	1.0
	4	0.08	12.1	2.7	0.83	0.74	0.81	0.76
	6	0.05	18.2	5.0	0.64	0.49	0.61	0.55

[a] Based upon an outdoor combined film coefficient of 4.0 and an indoor combined film coefficient of heat transfer of 1.65 Btu per (hour) (square foot) (Fahrenheit degree).

partially completed. The method reported by Mackey and Wright [7] will be adopted as the basis for the design procedure recommended here.

Homogeneous Walls or Roofs, Constant Indoor Temperature

For walls or roofs of a single, homogeneous material, the *instantaneous* rate of heat gain within an enclosure where the indoor air temperature is held constant is, approximately,

$$\frac{q}{A} = U\,(t_m - t_i) + \lambda\, U\,(t_e^* - t_m) \text{ Btu per (hour) (square foot)} \qquad (7)$$

where t_m = 24-hr average sol-air temperature for the particular value of $\frac{b}{f_o}$, Fahrenheit degrees.

λ = Amplitude decrement factor, a variable that depends upon the thickness, material, and orientation of the wall or roof; see Table 12 for values.

t_e^* = Sol-air temperature at a time earlier than the time for which the heat gain is being found by an amount that is equal to the time lag of the wall or roof, Fahrenheit degrees; see Table 12 for values of time lag.

U = Over-all coefficient of heat transfer of the wall or roof, Btu per (hour) (square foot) (Fahrenheit degree),

$$\frac{1}{\frac{1}{f_i} + \frac{1}{f_o} + \frac{L}{k}} = \frac{1}{\frac{1}{1.65} + \frac{1}{4} + \frac{L}{k}} = \frac{1}{0.856 + \frac{L}{k}}$$

L = Thickness of building material, feet.

k = Thermal conductivity of building material, Btu per (hour) (square foot) (Fahrenheit degree per foot).

f_i = Film coefficient of heat transfer of indoor air Btu per (hour) (square foot) (Fahrenheit degree).

TABLE 13. APPROXIMATE TIME OF MAXIMUM RATE OF HEAT ENTRY INTO WEATHER SIDE OF WALLS OR ROOFS IN NEW YORK, N. Y., AND IN LINCOLN, NEBR. [a,b]

SURFACE	Horizontal roof	North wall	East wall	South wall	West wall
SUN TIME	12 noon to 1:00 p.m.	6:00 p.m.	9:00 a.m.	1:00 p.m.	4:00 p.m.

[a] Mid-summer; solar absorptivities of weather surface of 0.4 or greater.

[b] For a completely shaded surface, the time of maximum rate of heat entry into the weather side is the time of maximum temperature of the outdoor air, which is at approximately 3:00 p. m., sun time, in both localities.

The time at which the maximum occurs in the rate of heat entry into the *outside* surface of walls or roofs is taken as the time at which the peak point occurs in the sol-air temperature cycle (mean *sun time* is used in the sol-air cycles). Table 13 gives these time data. Adding the time lag to the time from Table 13 will give the time of the maximum rate of heat entry into the conditioned space. The corresponding maximum rate of heat entry follows from Equation 7 with t_e* being the maximum temperature of the sol-air cycle.

An example in the use of Tables 10, 11, and 12 follows:

Example 3. Find the instantaneous design rate of heat gain through an 8-in. west wall of common brick ($b = 0.7, f_o = 4$) located in New York, N. Y., at 9:30 p. m. sun time, when the temperature of the indoor air is constant at 80 F.

From Table 12, $U = 0.41$, the time lag is 5.5 hr, and $\lambda = 0.44$.

By linear interpolation on the basis of the value of b/f_o in Table 10,

$$t_m = 84.8 + \frac{0.175}{0.25}(96.5 - 84.8) = 93 \text{ F.}$$

The design sol-air temperature at a time earlier than 9:30 p. m. by the time lag (at 4:00 p. m.) for a west wall in New York, N. Y., is, from Table 10,

$$t'_e = 94 + \frac{0.175}{0.25}(145 - 94) = 129.7 \text{ F.}$$

From Equation 7, the instantaneous design rate of heat gain is

$$\frac{q}{A} = 0.41\,[(93 - 80) + 0.44\,(129.7 - 93)]$$

= 11.9 Btu per hour for each square foot of sunlit surface.

From Table 12, the time lag is 5.5 hr. From Table 13, the time of maximum rate of heat entry for a west wall is 4:00 p. m. The time of maximum instantaneous rate of heat gain by the enclosure, as far as the west wall is concerned, is then 4:00 p. m. plus 5.5 hr or 9:30 p. m. (This is *sun time*.) The computed rate is therefore the maximum.

Composite Walls or Roofs, Constant Indoor Temperature

A composite wall or roof is made up of two or more layers of different materials. Since the analytical solution for this type of construction has not been reduced to simple and practical terms, it is necessary at present to utilize approximate procedures. In accord with the results of comparative calculations, the following procedures are suggested [7].

To find the time lag for a composite construction:

a. Find the time lag for each layer from Table 12.

b. Add the individual time lags, recognizing that this sum will always be *less* than the true time lag for the actual composite wall.

c. To the sum from (b), *add* an *arbitrary* additional lag of ½ to 1 hr to obtain the estimated lag for the actual construction. For two-layer and light construction walls,

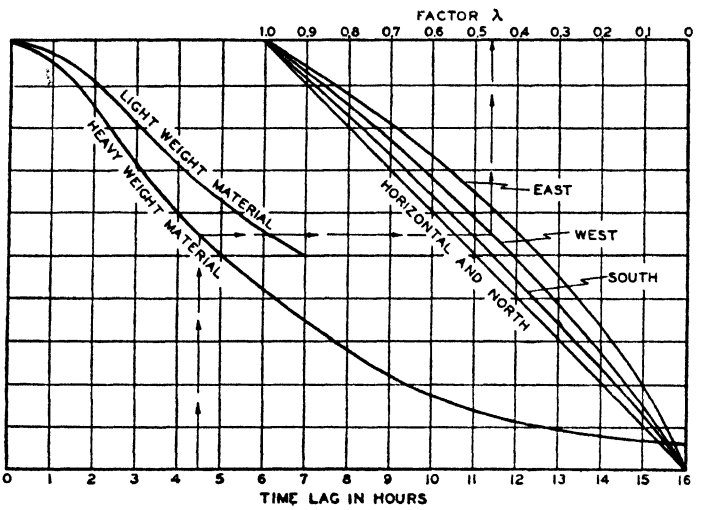

FIG. 4. APPROXIMATE VALUE OF THE AMPLITUDE DECREMENT FACTOR λ FOR USE IN EQUATION 7

the ½-hr value will be suitable while, for walls of three or more layers, or very heavy construction, the 1-hr value is preferred. For intermediate conditions, individual judgment is the only guide. (Computed time lags should not be considered to be accurate closer than to about the nearest hour by this method.)

To find the amplitude decrement factor, λ, for composite construction:

Having determined the time lag and the orientation, use Fig. 4. (Note also that the factor λ for a composite construction should never exceed the *product* of the factors for the individual layers.)

One valuable result of the analytical studies made to date on composite walls has been the demonstration of the effect of the *order* of the materials. Other factors remaining the same, the use of the material of lower density on the weather side will increase the time lag and decrease the instantaneous maximum rate of heat gain.

Two examples are given to show how to estimate, roughly, the instantaneous rate of heat gain through sunlit composite walls or roofs.

Example 4. Estimate the maximum instantaneous design rate of heat gain from a horizontal roof in New York, N. Y., that is made up of black built-up roofing on the weather side ($b = 1$; $f_o = 4$; thermal resistance = 0.28), 1 in. of insulating board, and 4 in. of concrete with no ceiling, when the temperature of the indoor air is 80 F.

The over-all coefficient of heat transfer for this construction is:

$$U = \frac{1}{0.25 + 0.28 + 3.03 + 0.33 + 0.61} = 0.22$$ Btu per (hour) (square foot) (Fahrenheit degree).

If the time lag of the built-up roofing be ignored, the sum of the time lags of the individual layers is, from Table 12, (0.23 + 2.5) or 2.73 hr.

Actually, the time lag will be between 0.5 hr and 1.0 hr greater than this, so assume a time lag of 3.5 hr.

From Table 12, the homogeneous concrete roof having a time lag of 3.5 hr would have a value of λ of about 0.65; use this value for the composite roof.

From Fig. 4, λ is approximately 0.65.

With values of t_m and t_e^* found from Table 10, as in previous examples, use Equation 7 and find the maximum design instantaneous rate of heat gain as:

$$\frac{q}{A} = 0.22\,[(106.4 - 80) + 0.65\,(155 - 106.4)] = 13 \text{ Btu per (hr) (sq ft)}.$$

The maximum instantaneous rate of heat gain from this roof would occur at about 3:30 p. m., sun time.

Example 5. Estimate the maximum instantaneous design rate of heat gain from a south wall in Lincoln, Nebr., consisting of 4 in. of face brick ($b = 0.7$; $f_o = 4$), 4 in. of common brick, furred, with an air space (thermal resistance = 0.75), and finished on the inside with ¾ in. of plaster on metal lath (thermal resistance = 0.23); the temperature of the indoor air is constant at 80 F.

The over-all coefficient of heat transfer for this construction is:

$$U = \frac{1}{0.25 + 0.44 + 0.80 + 0.75 + 0.23 + 0.61} = 0.32 \text{ Btu per (hr) (sq ft) (F deg)}.$$

From Table 12, the sum of the time lags for the face brick and the common brick is (2.4 + 2.3) or 4.7 hr. The actual time lag will be slightly greater than this, and a value of 5.5 hr will be assumed.

From Fig. 4, λ is approximately 0.45.

By interpolation in Table 11, $t_m = 99.8$ F, and $t_e^* = 123.6$ F. From Equation 7 the maximum instantaneous design rate of heat gain is:

$$\frac{q}{A} = 0.32\,[(99.8 - 80) + 0.45\,(123.6 - 99.8)] = 9.8 \text{ Btu per (hr) (sq ft)}.$$

The time of this heat gain is about 6:30 p. m., sun time.

Those concerned with a further study of the details of cooling-load estimates in particular relation to periodic heat flow will find much of value and interest in the reports of experimental studies of these problems [7, 8, 9, 10]. It should be pointed out that the analytical procedures presented here yield generally *higher* rates of heat gain than reported for Pittsburgh in early A.S.H.V.E. experimental studies. Current authoritative opinion, however, is that the analytical calculations are *to be preferred*, all factors considered.

Simplified Procedure and Design Tables for Roof and Wall Areas

Good judgment in cooling-load estimates requires that recognition be given to the relative importance of the load component due to periodic heat flow. The magnitude of the second term in Equation 7, relative to the first term indicates the relative portion of the structural heat-inflow load assignable to periodic heat flow. The total heat-transmission load represented by both terms in Equation 7 might vary from, say 10 per cent to 50 per cent of the total cooling load in various applications. The *periodic* term is continually passing through a *cyclic variation*, from zero to a positive maximum, to zero, to a negative maximum, to zero again, and so on. Surfaces with different exposures pass through these cycles with maximum points at different times of the day. It seems reasonable to consider, for conventional structures, that the *periodic* term would not exceed about 20 per cent of the total design-estimate cooling load. Hence, elaborate and highly accurate calculation procedures are without practical justification.

To establish a simple procedure, re-arrange Equation 7 to read

$$\frac{q}{A} = U\,[t_m + \lambda\,(t_e^* - t_m) - t_i] \qquad (8)$$

Let $t_m + \lambda\,(t_e^* - t_m) = t_p$, a *net* equivalent outdoor temperature for combined periodic and mean heat flow. Magnitudes of t_p will vary cyclically with time.

Then,

$$\frac{q}{A} = U\,(t_p - t_i) \qquad (9)$$

which is a simple form analogous to the steady-state equations of Chapters 5 and 6. In steady-state calculations for heating loads, the design outdoor temperature is a constant; here, t_p varies with time, wall construction, wall orientation, and heat-transfer boundary conditions expressed as sol-air temperature data.

To make Equation 9 of maximum practical convenience, there are needed, for representative wall and roof constructions and for sample weather-design conditions, data giving values of U and t_p for a design-day cooling cycle.

The available information on these quantities is sufficient to establish usable data in preliminary form, and continuing A.S.H.V.E. research is expected to improve and extend these data.

Values of U. The values of U for use in Equation 9 are listed in Table 12 for a few constructions. Other values are given in Chapter 6. Note, however, that Table 12 is based upon $f_o = 4.0$ Btu per (hr) (sq ft) (F deg), whereas the values in Chapter 6 are based upon $f_o = 6.0$. The question of which value of f_o is the more satisfactory is the subject of some controversy at the moment. The difference in U is not a critical one, however, in view of the inevitable approximations which enter into cooling-load estimates, and hence the tables of Chapter 6 may be used without correction where necessary.

Values of t_p. The sol-air data for New York City, Table 10, are recommended as the basis for determinations of t_p. (These data may be adjusted for latitude, air temperature, and (b/f_o) as previously explained.) Magnitudes of the factor λ, and the time lag needed to obtain t_e^* may be estimated as previously indicated. Calculations then follow directly from the defining equation,

$$t_p = t_m + \lambda (t_e^* - t_m) \tag{10}$$

It is expected that *design tables* may be made available in due time which will give values of t_p directly and make detailed calculations unnecessary.

GLASS AREAS—DESIGN TABLES

In order to clearly set forth the principles involved in calculating heat transfer through glass areas the general instantaneous heat-balance relation will be presented. Fig. 5 shows this schematically. The net heat gain for the indoor space is the result of several contributing phenomena.

In discussing the heat gain through glass, there are three dimensionless quantities which require definition:

a = Absorptivity of glass, or fraction of incident radiation intensity which is absorbed within the glass itself.

τ = Transmissivity of glass, or fraction of incident radiation intensity which is transmitted through the glass.

r = Reflectivity of glass, or fraction of incident radiation intensity which is reflected at the surface.

It is necessary that

$$a + \tau + r = 1 \tag{11}$$

These quantities vary with wave length and angle of incidence, primarily; and they are determined by the properties and thickness of the glass material concerned. Data are obtainable from glass manufacturers for their various products. The dependence of these quantities upon wave length has important practical consequences; for example, common

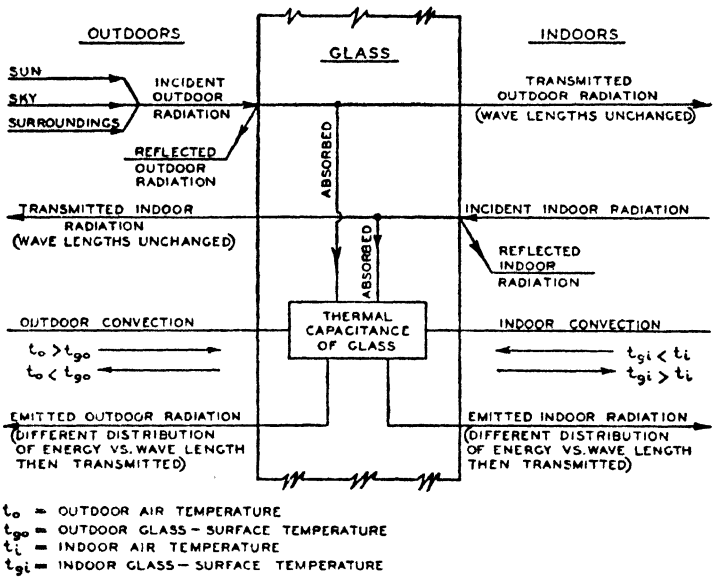

FIG. 5. INSTANTANEOUS HEAT-BALANCE CONDITIONS ON A GLASS SECTION

window glass transmits a large portion of incident *solar* radiation, whereas it transmits outward only a very small portion of the indoor radiation falling upon the inside surface because this latter is principally in the longer wave lengths.

A recent analysis has served to demonstrate the effects of the various controlling variables upon the heat gain from glass in relation to air-conditioning problems [11]. The practical results for a single sheet of common window glass will be cited here. For average conditions, the design equation for the instantaneous rate of heat transfer from the indoor glass surface to the conditioned space (for single sheets of common window glass only) in Btu per (hour) (square foot of sunlit surface) was found to be:

$$\left(\frac{q}{A}\right) = 1.04\,(t_o - t_i) + 0.022\,I_d + 0.0165\,I_s + \tau_d I_d + 0.778\,I_s. \qquad (12)$$

where t_o = Outdoor air temperature, Fahrenheit degrees.
t_i = Indoor air temperature, Fahrenheit degrees.
I_d = Intensity of solar or direct radiation on the outer glass surface, Btu per (hour) (square foot of sunlit surface).
I_s = Intensity of sky radiation on the outer glass surface.
τ_d = Transmissivity of the glass for solar radiation, dimensionless, given as a function of the angle of incidence in Table 14.

TABLE 14. TRANSMISSIVITY OF SINGLE-SHEET COMMON WINDOW GLASS FOR DIRECT SOLAR RADIATION

ANGLE OF INCIDENCE[a] DEG	TRANSMISSIVITY τ_d	ANGLE OF INCIDENCE[a] DEG	TRANSMISSIVITY τ_d	ANGLE OF INCIDENCE[a] DEG	TRANSMISSIVITY τ_d
0	0.87	50	0.83	80	0.41
20	0.86	60	0.77	90	0
40	0.85	70	0.65		

[a]Of Direct Solar Radiation.

Similar equations with other numerical constants apply to other types of glass or glass areas in other arrangements. (Heat-absorbing glass or glass in multiple layers, for example).

Equation 12 may be clarified further by explanations of the numerical constants involved:

1.04 = Over-all unit conductance for heat transfer under *summer* conditions, Btu per (hour) (square foot) (Fahrenheit degree). (Note that this is the transmittance U taken at 1.13 for winter conditions in Chapter 6.)

0.022 = Fraction of I_d which is absorbed and then transferred to the indoor space from the indoor glass surface, dimensionless. (Note that, of the total absorption, part goes inside and part goes outside.)

0.0165 = Fraction of I_s which is absorbed and then transferred to the indoor space from the indoor glass surface, dimensionless.

0.778 = transmissivity of the glass for sky radiation, dimensionless.

Magnitudes of the quantities I_d, I_s and t_o entering into Equation 12 would depend upon the time of the day, time of the year, atmospheric conditions, latitude of the receiving surface, and the orientation of the receiving surface. Principles and data needed for the calculation of I_d and I_s have been given previously in this chapter. Weather data, such as the sol-air temperatures in Tables 10 and 11, give data on t_o throughout a design day.

Table 15 has been prepared to expedite practical calculations of the heat gain through glass areas; tabulated values are magnitudes of the sum $(0.022\ I_d + 0.0165\ I_s + \tau_d I_d + 0.778\ I_s)$ from Equation 12 for a solar declination of 18 deg. This declination corresponds to a nominal August 1 design day, although the values tabulated may be used with safety to represent average conditions from July 15th to August 15th.

It is possible to use the heat-gain data of Table 15 for other single-thickness glass materials than common window glass through the introduction of approximate correcting factors. Table 16 gives such factors. The range of transmissivities in Table 16 extends from high-transmission crystal-like glass to low-transmission heat-absorbing glass. The transmissivity of 0.87 is that of common window glass.

By using two or more layers of glass separated by air spaces, the absorptivity is increased and the transmissivity decreased. Values for some combinations appear in the literature [11]. A rough approximation which holds fairly well until the angle of incident radiation becomes large is that the transmissivity of the combination is the product of the transmissivities of the component layers, while the absorptivity of the combination is the absorptivity of the outer glass plus the product of the absorptivity of the inner glass and the transmissivity of the outer.

Heat-gain quantities from Table 15 may also be used for other times of the year than August 1 if a correction is made for solar declination. Solar heating calculation for glass areas can also be based upon these data. Table 17 gives solar declinations for various times of the year. The rule for procedure is the following:

To find the radiation heat gain for some declination of the sun other than 18 deg use the latitude in Table 15 equal to that of the locality in question plus (18 deg—solar declination involved).

For example, consider that the instantaneous heat gain is required for Philadelphia in the middle of June. The latitude of Philadelphia is 40 deg North. The solar declination in mid-June is about 23.5 deg. The section of Table 15 to be used is then that for a latitude of 40 + (18 − 23.5) = 34.5 deg; say 35 deg.

Caution: This method gives only approximate values and its use should be limited. It may be used for Eastern and Western exposures for all hours 8:00 a.m. to 4:00 p.m.

TABLE 15. INSTANTANEOUS RATES OF HEAT GAIN DUE TO SOLAR AND SKY RADIATION FOR SINGLE SHEETS OF UNSHADED COMMON WINDOW GLASS [a, b]

Computed for Solar Declination of 18 Deg—August 1

Note: *To determine the total instantaneous rate of heat gain add the term 1.04* $(t_o - t_i)$ *to the values shown in the table (see Equation 12).*

SUN TIME	SOLAR ALTITUDE β DEG	INSTANTANEOUS RATE OF HEAT GAIN, BTU PER HOUR FOR EACH SQUARE FOOT OF UNSHADED GLASS								
		N	NE	E	SE	S	SW	W	NW	Horizontal
					25 Deg North Latitude					
6 a.m.	7.5	19	77	84	40	3	3	3	3	12
7	20.5	26	146	173	98	10	10	10	10	68
8	34.0	18	148	193	121	13	13	13	13	143
9	47.5	15	118	172	120	16	15	15	15	205
10	61.5	16	67	124	95	22	16	16	16	252
11	74.5	16	25	57	57	25	16	16	16	282
12	83.0	16	16	16	25	28	25	16	16	293
1 p.m.	74.5	16	16	16	16	25	57	57	25	282
2	61.5	16	16	16	16	22	95	124	67	252
3	47.5	15	15	15	15	16	120	172	118	205
4	34.0	18	13	13	13	13	121	193	148	143
5	20.5	26	10	10	10	10	98	173	146	68
6	7.5	19	3	3	3	3	40	84	77	12
					30 Deg North Latitude					
6 a.m.	9.0	22	88	97	47	4	4	4	4	15
7	21.5	23	146	176	105	11	11	11	11	74
8	34.5	16	140	194	130	14	14	14	14	144
9	47.5	15	104	171	133	20	15	15	15	205
10	60.0	16	53	126	112	33	16	16	16	248
11	72.0	16	19	56	74	42	16	16	16	277
12	78.0	16	16	16	34	45	34	16	16	288
1 p.m.	72.0	16	16	16	16	42	74	56	19	277
2	60.0	16	16	16	16	33	112	126	53	248
3	47.5	15	15	15	15	20	133	171	104	205
4	34.5	16	14	14	14	14	130	194	140	144
5	21.5	23	11	11	11	11	105	176	146	74
6	9.0	22	4	4	4	4	47	97	88	15
					35 Deg North Latitude					
6 a.m	10.0	21	97	109	53	4	4	4	4	19
7	22.5	19	143	179	110	11	11	11	11	79
8	34.5	14	133	194	140	15	14	14	14	144
9	46.5	15	90	170	144	28	15	15	15	200
10	58.5	16	38	126	128	47	16	16	16	243
11	68.5	16	16	56	91	62	17	16	16	269
12	73.0	16	16	16	45	68	45	16	16	279
1 p.m.	68.5	16	16	16	17	62	91	56	16	269
2	58.5	16	16	16	16	47	128	126	38	243
3	46.5	15	15	15	15	28	144	170	90	200
4	34.5	14	14	14	14	15	140	194	133	144
5	22.5	19	11	11	11	11	110	179	143	79
6	10.0	21	4	4	4	4	53	109	97	19
					40 Deg North Latitude					
5 a.m.	1.5	7	18	17	6	1	1	1	1	2
6	11.5	23	106	120	62	5	5	5	5	24
7	23.0	15	141	181	118	11	11	11	11	82
8	34.5	14	122	194	147	19	14	14	14	145
9	45.5	15	76	172	156	42	15	15	15	196
10	56.0	16	30	125	144	66	16	16	16	235
11	64.5	16	16	53	110	85	22	16	16	261
12	68.0	16	16	16	62	94	62	16	16	269
1 p.m.	64.5	16	16	16	22	85	110	52	16	261
2	56.0	16	16	16	16	66	144	125	30	235
3	45.5	15	15	15	15	42	156	172	76	196
4	34.5	14	14	14	14	19	147	194	122	145
5	23.0	15	11	11	11	11	118	181	141	82
6	11.5	23	5	5	5	5	62	120	106	24
7	1.5	7	1	1	1	1	6	17	18	2

TABLE 15. INSTANTANEOUS RATES OF HEAT GAIN DUE TO SOLAR AND SKY RADIATION FOR SINGLE SHEETS OF UNSHADED COMMON WINDOW GLASS [a, b] (CONCLUDED)

SUN TIME	SOLAR ALTITUDE β DEG	INSTANTANEOUS RATE OF HEAT GAIN, BTU PER HOUR FOR EACH SQUARE FOOT OF UNSHADED GLASS								
		N	NE	E	SE	S	SW	W	NW	Horizontal
45 Deg North Latitude										
5 a.m.	2.0	9	23	23	8	1	1	1	1	2
6	12.5	22	111	129	68	6	6	6	6	28
7	23.0	13	135	182	121	11	11	11	11	82
8	33.5	14	116	192	153	24	14	14	14	141
9	44.0	15	63	168	166	55	15	15	15	189
10	53.0	16	22	123	154	88	16	16	16	225
11	60.0	16	16	56	127	113	30	16	16	249
12	63.0	16	16	16	76	119	76	16	16	256
1 p.m.	60.0	16	16	16	30	113	127	56	16	249
2	53.0	16	16	16	16	88	154	123	22	225
3	44.0	15	15	15	15	55	166	168	63	189
4	33.5	14	14	14	14	24	153	192	116	141
5	23.0	13	11	11	11	11	121	182	135	82
6	12.5	22	6	6	6	6	68	129	111	28
7	2.0	9	1	1	1	1	8	23	23	2
50 Deg North Latitude										
5 a.m.	4.5	18	48	48	17	2	2	2	2	5
6	13.5	22	119	139	75	6	6	6	6	32
7	23.5	11	131	183	127	11	11	11	11	84
8	33.0	13	103	190	161	30	13	13	13	138
9	42.0	14	51	165	173	69	14	14	14	179
10	50.0	16	19	122	166	109	16	16	16	214
11	56.0	16	16	55	138	133	41	16	16	235
12	58.0	16	16	16	92	140	92	16	16	242
1 p.m.	56.0	16	16	16	41	133	138	55	16	235
2	50.0	16	16	16	16	109	166	122	19	214
3	42.0	14	14	14	14	69	173	165	51	179
4	33.0	13	13	13	13	30	161	190	103	138
5	23.5	11	11	11	11	11	127	183	131	84
6	13.5	22	6	6	6	6	75	139	119	32
7	4.5	18	2	2	2	2	17	48	48	5

[a] Table compiled from solar radiation transmission data developed by A.S.H.V.E. Research Laboratory[2] and direct intensity values developed by Moon[1], recently enlarged and revised by the A.S.H.V.E. Research Laboratory.

[b] For relatively clear atmosphere at sea level. For hazy atmosphere values may be reduced 10 per cent. Above sea level add one per cent per 1000 ft elevation.

inclusive, and for all exposures from 10:00 a.m. to 2:00 p.m. inclusive. For Southern exposures at 8:00 a.m. or at 4:00 p.m. the error may be ±15 per cent. At noon this method gives accurate results; the error becomes progressively larger as the time differs from noon.

In regard to *glass blocks*, data on the over-all unit conductances for heat transfer by convection and conduction are given in Table 18, Chapter 6; these will serve also for cooling load calculations for shaded or north-exposure walls. (Steady-state calculations as suggested there take no account of the time lag present with periodic cycles of air temperature.)

The results of experimental observations [12] on heat gains through glass-block sections are given in Table 18. Tabulated heat-gain rates are based upon a constant indoor-air temperature of 78 F and a maximum outdoor-air temperature of 95 F for the design day chosen. The values given are approximate, and intended for estimates only; they are *averages* for *four* representative glass block designs, two with smooth exterior faces and two with ribbed exterior faces.

TABLE 16. RATIO OF INSTANTANEOUS RATE OF HEAT GAIN THROUGH SINGLE THICKNESS OF HEAT ABSORBING SUNLIT GLASS TO HEAT GAIN FOR COMMON GLASS AS GIVEN IN TABLE 15

TRANSMISSIVITY[a]	APPROXIMATE RATIO	TRANSMISSIVITY[a]	APPROXIMATE RATIO	TRANSMISSIVITY[a]	APPROXIMATE RATIO
0.90	1.02	0.70	0.85	0.40	0.60
0.87	1.0	0.60	0.76	0.30	0.52
0.80	0.93	0.50	0.68	0.20	0.45

[a]For direct solar radiation at normal incidence.

TABLE 17. APPROXIMATE SOLAR DECLINATIONS IN DEGREES

DATE	DECLINATION	DATE	DECLINATION	DATE	DECLINATION
April 1	4.5	June 1	22.0	Aug. 1	18.0
April 15	10.0	June 15	23.5	Aug. 15	14.0
May 1	15.0	July 1	23.0	Sept. 1	8.5
May 15	19.0	July 15	21.5	Sept. 15	3.0

TABLE 18. TOTAL INSTANTANEOUS RATES OF HEAT GAIN FOR GLASS BLOCKS [12] ON DESIGN DAY OF AUGUST 1

(Values tabulated include solar and sky radiation, convection, and conduction averaged for four types of blocks)

MEAN SUN TIME	TOTAL INSTANTANEOUS RATE OF HEAT GAIN, BTU PER HOUR FOR EACH SQUARE FOOT OF SUNLIT GLASS BLOCK					
	Vertical Surface Facing					
	East	West	South			
North Latitude, Deg	30 to 45	30 to 45	30	35	40	45
7 a.m.	61	.....	−4.5	−2.0	−0.5	1.0
8	78	.....	0.0	2.0	4.0	5.0
9	74	5.0	5.0	7.0	10	12
10	58	6.5	11	15	18	21
11	45	7.5	17	22	26	32
12 noon	37	11	22	28	34	41
1 p.m.	30	22	25	32	39	46
2	24	35	26	32	39	47
3	20	55	24	30	37	45
4	16	77	20	26	32	41
5	13	86	15	20	25	34
6	11	55	9.5	14	18	26
7	8	19	3.5	7.0	11	18

Shading of Glass Areas—Design Tables

The effects and possibilities of shading should be carefully investigated whenever the heat gain from glass is a large portion of the cooling load.

Vertical glass which is not mounted in the plane of the building surface is partially shaded by the *setback*. If a vertical window of height l and width w be set back from the plane of the building a distance s, the fraction of the total area of the window which receives *direct* solar radiation is:

$$G_f = 1 - r_1 \tan \beta - r_2 \tan \gamma + r_1 r_2 \tan \beta \tan \gamma \qquad (13)$$

where

$r_1 = s/l$, $r_2 = s/w$, β = solar altitude, and γ is the difference between the azimuth angles of the wall in question and of the horizontal projection of the sun's rays. (γ is always equal to or less than 90 deg.)

TABLE 19. VALUES OF THE AZIMUTH-DIFFERENCE ANGLE, γ, DEGREES, FOR WINDOW-REVEAL SHADING CALCULATIONS (SEE EQUATION 12)

Computed for solar declination of 18 deg—August 1

N. LATITUDE DEGREES	MEAN SUN TIME	WINDOW ORIENTATION						
		NE	E	SE	S	SW	W	NW
30	6 a. m.	61	74	29	Shade	Shade	Shade	Shade
	7	54	81	36	....	....	....	....
	8	47	88	43	....	....	....	....
	9	39	84	51	6	....	....	....
	10	28	73	62	17	....	....	....
	11	7	52	83	38	....	....	....
	12 N	Shade	0	45	90	45	0	....
	1 p. m.	....	Shade	Shade	38	83	52	7
	2	....	....	....	17	62	73	28
	3	....			6	51	84	39
	4				Shade	43	88	47
	5				....	36	81	54
	6				....	29	74	61
40	6 a. m.	59	76	31	Shade	Shade	Shade	Shade
	7	50	85	40	....	....	....	....
	8	40	85	50	5	....	....	....
	9	27	74	61	16	....	....	....
	10	14	59	76	31	....	....	....
	11	Shade	35	80	55	....	....	....
	12 N	....	0	45	90	45	0	....
	1 p. m.	....	Shade	10	55	80	35	....
	2	....	....	Shade	31	76	59	14
	3	....	....	....	16	61	74	27
	4	....	....	....	5	50	85	40
	5	....	....	....	Shade	40	85	50
	6	....	....	....	....	31	76	59
50	6 a. m.	57	78	33	Shade	Shade	Shade	Shade
	7	45	90	45	0	....	....	....
	8	33	78	57	12	....	....	....
	9	20	65	70	25	....	....	....
	10	3	48	87	42	....	....	....
	11	Shade	26	71	65	19	....	....
	12 N	....	0	45	90	45	0	....
	1 p. m.	....	Shade	19	65	71	26	....
	2	....	....	Shade	42	87	48	3
	3	....	....	....	25	70	65	20
	4	....	....	....	12	57	78	33
	5	....	....	....	0	45	90	45
	6	....	....	....	Shade	33	78	57

Solar altitudes are given in Table 15 for various latitudes and an August 1 design day. Values of the angle γ are given in Table 19 for the August 1 design day. Special cases not covered by the tabulated data may be solved analytically[13]; however, the design conditions chosen will yield a satisfactory approximation if used without correction for estimates at any time during the summer period.

Example 6. Estimate the instantaneous rate of sky and solar radiation heat gain from a west window 3 ft wide by 5 ft high with a setback of 6 in. for August 1 and a north latitude of 40 deg at 3 p. m. (sun time).

From Table 15, the instantaneous rate of sky and solar radiation heat gain per square foot of sunlit glass is 172 Btu per hour. From the same table, the solar altitude is 45.5 deg. From Table 19, the angle γ is 16 deg, from Equation 13, the fraction of the total window area that is receiving direct solar radiation is:

$$G_f = 1 - 0.1 \tan 45.5 - 0.167 \tan 16 + 0.0167 \tan 45.5 \tan 16.$$
$$= 1 - 0.102 - 0.048 + 0.005 = 0.855.$$

Although the *sky* radiation is not reduced in proportion to the shaded portion, since the sky radiation is small this fact may be neglected, and hence instantaneous sky-and solar-radiation heat gain for this window is:

$$q = 3 \times 5 \times 0.855(172) = 2206 \text{ Btu per hour.}$$

TABLE 20. EFFECT OF SHADING UPON TOTAL (RADIATION, CONDUCTION AND CONVECTION) RATES OF INSTANTANEOUS HEAT GAIN THROUGH SINGLE THICKNESS OF COMMON WINDOW GLASS[a]

TYPE OF SHADING	FINISH	FRACTION OF GAIN THROUGH UNSHADED WINDOW
Outside Shading Screen: metal slats 0.050 in. wide, spaced 0.063 in. apart and set at 17 deg angle with horizontal.	Dark	0.20-0.35
Canvas Awning	Dark	0.25-0.35
Outside Venetian Blind: slats at 45 deg, extended as an awning without sides to cover approximately two-thirds of window.	Light	0.35-0.50
Inside Roller Shade: fully drawn.	Aluminum	Approx. 0.45
Outside Venetian Blind: slats at 45 deg, fully covering window.	Aluminum	Approx. 0.3
Inside Venetian Blind: slats at 45 deg, fully covering window.	Aluminum	0.65-0.80
Inside Roller Shade: half drawn.	Buff	Approx. 0.7
Inside Roller Shade: half drawn.	Dark	0.90-0.95

[a]These factors are not accurate for heat absorbing glass or glass blocks.

A window such as the one in Example 6 above would customarily be provided with an additional shading means for use particularly when directly sunlit. Conventional shading devices include *awnings*, *shades*, and *screens* of various types.

In Table 20 are given the ratios of the instantaneous rates of heat gain from windows shaded by different indoor and outdoor shading fixtures to the rate of heat gain from unshaded glass according to tests [13] at the A.S.H.V.E. Research Laboratory. There are a number of variables affecting these ratios such as color, fit, solar altitude, and angle of incidence of the solar radiation. These values, therefore, must be considered as approximate, only, and will have to be used with considerable judgment. An inside shade is effective to the extent of its reflectivity, since the portion of the solar radiation directly transmitted by the glass that is absorbed by the shade is transferred by convection to the room air and by radiation to the solid surfaces of the room.

Instantaneous Heat Gains vs. Instantaneous Cooling Loads

The difference between instantaneous heat gain and instantaneous cooling load has been mentioned previously; its practical importance is sufficient to warrant further consideration.

Fig. 6 offers a simplified schematic illustration showing how the *radiative* part of the instantaneous heat gain is first absorbed by solid objects and is not encountered by the conditioning equipment as a cooling load

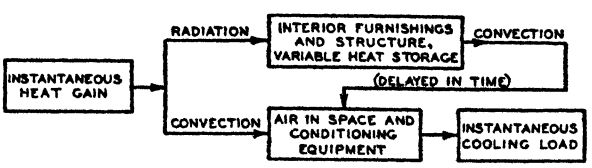

FIG. 6. ORIGIN OF THE DIFFERENCE BETWEEN THE MAGNITUDES OF THE INSTANTANEOUS HEAT GAIN AND INSTANTANEOUS COOLING LOAD

The radiation absorbed by the interior furnishings and structure reaches the conditioning equipment after a considerable delay in time.

until some later time when it finally appears in the air-stream entering the equipment. While it is true that some lag also is inherent in convective heat transfer and the time required to change the air in the conditioned space, this is usually of the order of a few minutes to perhaps half an hour. Heat storage in the interior furnishings and structure increases according to the proportion of the instantaneous heat gain which is in the form of radiation, and also as the thermal capacitance of the objects and materials involved is increased.

Constituents of the total instantaneous heat gain which have appreciable radiation components include those due to: glass areas, exposed walls and roofs, lighting, appliances, and people.

No comprehensive data are presently available for use in design load estimates to evaluate the interior load-lag effect. Hence, practical judgment and experience offer the only basis of procedure. Until the needed data become available, it is recommended that the non-continuous load be averaged over two or three hours previous to the time of maximum load, when determining the total instantaneous cooling load where a large portion of the heat gain is radiant. This suggestion applies only to conditions near the time of maximum heat gain, as the heat stored within the structure would necessarily appear in the cooling load eventually, but if it appears at a time when the gain from outside is relatively low the equipment will be able to maintain satisfactory conditions within the range of maximum capacity.

LOAD FROM INTERIOR PARTITIONS, CEILINGS, AND FLOORS

Whenever a conditioned space is adjacent to another space in which a different temperature prevails, the transfer of heat through the separating structural section must be considered. Calculations are made according to the relation

$$q = U_i A_i (t_x - t_i) \text{ Btu per hour.} \qquad (14)$$

where U_i = Coefficient of over-all heat transfer between the adjacent and the conditioned space, Btu per (hour) (square foot) (Fahrenheit degree).
A_i = Area of separating section concerned, square feet.
t_x = Air temperature in adjacent space, Fahrenheit degrees.
t_i = Air temperature in conditioned space, Fahrenheit degrees.

Magnitudes of U_i may be obtained from Chapter 6. The temperature t_x may have any value over a considerable range, according to conditions in the adjacent space. Where nothing is known except that the adjacent space is of conventional construction and contains no heat sources, it is recommended that the difference $(t_x - t_i)$ be taken as the difference between the outdoor-air and conditioned-space design dry-bulb temperatures *minus* 5 Fahrenheit degrees. In some cases it may be that the air temperature in the adjacent space will correspond closely to the outdoor air temperature at all times. Under these latter conditions, the heat gain through the partition will be periodic in nature and the value of $(t_p - t_i)$ for Equation 9 should be used as for a shaded wall.

For floors directly in contact with the ground, or over an underground basement that is neither ventilated nor warmed, the heat transfer may be neglected for cooling-load estimates.

LOAD FROM OUTSIDE AIR - VENTILATION AND INFILTRATION

Ventilation. Data for determining the necessary ventilation rate have been presented previously in this chapter. Total requirements should

TABLE 21. INFILTRATION THROUGH 72-INCH REVOLVING DOOR AND 36-INCH SWINGING DOOR[a,b,c]

(*Cubic Feet per Person per Passage*)

USAGE	FREELY-REVOLVING DOOR	DOOR EQUIPPED WITH BRAKE
Infrequent	75	60
Average	60	50
Heavy	40	40
36-Inch Swinging Door	100	

[a]These figures are based on the assumption that there is no wind pressure and that swinging doors are in use in one wall only. Any swinging doors in other walls should be kept closed to insure air conditioning in accordance with these recommended standards.

[b]For summer cooling, use Table 2 to calculate the requirements for both ventilation and infiltration, and use the larger quantity. The quantity of air should be not less than that required by local ordinance, nor less than that drawn from the space by any exhaust fans which may be used. For normal ceiling heights, the quantity of outside air supplied should be not less than one air change per hour.

[c]From Application Engineering Standards for Air Conditioning for Comfort. *Air Conditioning & Refrigerating Machinery Association, Inc.*, Washington, D. C. Used by permission.

be checked against the volume of the conditioned space, and in no case should the ventilation air rate be less than one air change per hour.

Infiltration. The principles of infiltration calculations have been discussed in Chapter 8, with emphasis on the heating season. For the cooling season, infiltration calculations are limited to doors and windows.

To compute cooling-load infiltration for windows, use the data of Table 2, Chapter 8, for a wind velocity of 10 mph. Note that for double-hung windows the length of crack is three times the width plus twice the height; while for metal-sash windows the crack length is the total perimeter of the movable or ventilating sections. In calculating window infiltration for an entire structure, it is not necessary to consider the total crack length on all sides of the building, for the wind would not act simultaneously on all sides at once. In no case, however, should less than half of the total crack length be figured. Consideration of the prevailing wind direction will aid judgment in this question.

Cooling-load infiltration for doors may be obtained from Table 21, shown above[14]. For conditions other than those covered, the notes appended to Table 21 will provide a basis for estimates. The tabulated data may also be used as the basis of estimates for interior doors between an air-conditioned and a non-air-conditioned space.

Infiltration load must be included whenever the new air introduced through the system is not sufficient to maintain excess pressure within the enclosure to overcome the infiltration. Whenever economically feasible it is desirable to introduce sufficient outdoor air through the air-conditioning equipment to maintain a constant outward escape of air and thus eliminate the infiltration portion of the load. The pressure maintained must, of course, be sufficient to overcome wind pressure through cracks and door openings. When this condition prevails it is not necessary to include any infiltration load.

Total Outside Air Load. To determine the design cooling load caused by the introduction of outside air, the maximum rate of outside-air entry is first established. In some applications the use of special exhausters from the conditioned space may add to the outdoor-air requirements in determining the maximum rate. Once this design quantity is established, and with the design indoor and outdoor air states known, the cooling load may be computed. There are several methods in use, the more accurate

of these require rather detailed calculations. Refer to Chapter 3, Page 59, under section on Cooling Load and Chapter 43 in section on Apparatus Dew Point. The following equations are considered to be sufficiently accurate for use at usual design conditions as their accuracy is within 1 per cent.

$$\textit{Sensible Load} \quad q_s = Q \times 60 \times 0.244 \times 0.075 \left(1 - \frac{0.00923}{0.62}\right)(t_o - t_i) = Q \times 1.08\,(t_o - t_i), \text{ Btu per hour} \tag{15}$$

$$\textit{Latent Load} \quad q_e = Q \times 60 \times 0.075 \times 1076\,(W_o - W_i) = Q \times 4840\,(W_o - W_i), \text{ Btu per hour} \tag{16}$$

$$\textit{Total Load} \quad q_t = q_s + q_e \tag{17}$$

where Q = Rate of entry of outside air, cubic feet per minute.

t_o = Outdoor dry-bulb temperature, Fahrenheit degrees.

t_i = Indoor dry-bulb temperature, Fahrenheit degrees.

W_o = Outdoor humidity ratio, pounds moisture per pound of dry air.

W_i = Indoor humidity ratio, pounds moisture per pound of dry air.

0.075 = Standard air density, pounds per cubic foot.

0.244 = A constant approximating the specific heat of dry air corrected for moisture Btu per (pound) (Fahrenheit degree).

1076 = A factor approximating the average Btu released in condensing one pound of water vapor from air.

Standard air weight (0.075 lb per cu ft) is recommended for use in all calculations as this is the basis for rating fans and its consistent use keeps all parts of the calculations in conformity.

Actually the outdoor air used for ventilation would pass through the conditioning equipment and be cooled and dehumidified to a lower temperature and humidity ratio than room conditions before entering the room; but for heat-balance purposes the cooling load chargeable to the outdoor air is that corresponding to the difference between the outdoor and indoor air conditions.

Example 10. For outdoor design conditions of 95 F dry-bulb and 75 F wet-bulb and indoor design conditions of 80 F dry-bulb and 67 F wet-bulb and for the supply of outdoor air at the rate of 1000 cfm and the exhaust of room air at the corresponding rate, calculate the total, sensible and latent heat gains substituting in Equation 15:

$$q_s = 1000 \times 1.08\,(95 - 80) = 16{,}200 \text{ Btu per hr.}$$

From psychrometric data $W_o = 0.01413$, $W_i = 0.01122$.

Substituting in Equations 15 and 16:

$$q_e = 1000 \times 4840\,(0.01413 - 0.01122) = 14{,}100 \text{ Btu per hr.}$$

$$q_t = q_s + q_e = 30{,}300 \text{ Btu.}$$

HEAT SOURCES WITHIN THE CONDITIONED SPACE

People. The rates at which heat and moisture are given off by human beings under different states of activity are given in Chapter 12. In many applications these sensible and latent heat gains become a large fraction of the total load. Appreciable variations in heat-emission rates must be recognized according to the age and sex of the individual, state of activity, environmental influences, and duration of occupancy (since for short occupancy the extra heat and moisture brought in by people may be a significant factor).

TABLE 22. RATES OF HEAT GAIN FROM OCCUPANTS OF CONDITIONED SPACES[a]

DEGREE OF ACTIVITY	TYPICAL APPLICATION	TOTAL HEAT ADULTS, MALE BTU/HR	TOTAL HEAT ADJUSTED[b] BTU/HR	SENSIBLE HEAT BTU/HR	LATENT HEAT BTU/HR
Seated at Rest	Theater-Matinee	390	330	180	150
	Theater-Evening	390	350	195	155
Seated, Very Light Work	Offices, Hotels, Apartments	450	400	195	205
Moderately Active Office Work	Offices, Hotels, Apartments	475	450	200	250
Standing, Light Work; or Walking Slowly	Department Store, Retail Store				
	Dime Store	550	450	200	250
Walking; Seated;	Drug Store				
Standing; Walking Slowly	Bank	550	500	200	300
Sedentary Work	Restaurant[c]	490	550	220	330
Light Bench Work	Factory	800	750	220	530
Moderate Dancing	Dance Hall	900	850	245	605
Walking 3 mph; Moderately Heavy Work	Factory	1000	1000	300	700
Bowling[d]	Bowling Alley				
Heavy Work	Factory	1500	1450	465	985

[a]*Note:* Tabulated values are based on 80 F room dry-bulb temperature. For 78 F room dry-bulb, the total heat remains the same, but the sensible heat values should be increased by approximately 10 per cent and the latent heat values decreased accordingly.

[b]*Adjusted total heat gain* is based on normal percentage of men, women, and children for the application listed, with the postulate that the gain from an adult female is 85 per cent of that for an adult male and that the gain from a child is 75 per cent of that for an adult male.

[c]Adjusted total heat value for *sedentary work, restaurant*, includes 60 Btu per hour for food per individual (30 Btu sensible and 30 Btu latent).

[d]For *bowling* figure one person per alley actually bowling and all others as sitting (400 Btu per hour) or standing (550 Btu per hour).

The *use factor* is the ratio of the wattage in use, for the conditions under which the load estimate is being made, to the total installed wattage. For commercial applications such as stores, the use factor would be unity.

While Chapter 12 should be referred to for detailed information, Table 22 in this chapter summarizes the most useful data representing conditions commonly encountered.

Lighting. In general, the instantaneous rate of heat gain from electric lighting [15] may be calculated from the following relation:

$$q_{el} = \begin{Bmatrix}\text{total light}\\ \text{wattage}\end{Bmatrix} \times \begin{Bmatrix}\text{use}\\ \text{factor}\end{Bmatrix} \times \begin{Bmatrix}\text{special allow-}\\ \text{ance factor}\end{Bmatrix} \times 3.41, \text{ Btu per hour.} \quad (18)$$

The *total light wattage* is obtained from the ratings of all fixtures installed, both for general illumination and for display use.

The *special allowance factor* is introduced to care for fluorescent fixtures and for fixtures which are either ventilated or installed so that only part of their heat goes to the conditioned space. For *fluorescent fixtures*, the special allowance factor is recommended to be taken as 1.20 in order to allow for power consumed in the *ballast*. For *ventilated fixtures*, *recessed fixtures*, and the like, manufacturer's or other data [15] must be sought to establish the fraction of the total wattage which may be expected to enter the conditioned space.

Power. When equipment of any sort is operated within the conditioned space by electric motors, the heat equivalent of this operation must be considered in the cooling load. The general equation for calculating this load is:

$$q_{em} = \left(\frac{\text{Horsepower Rating}}{\text{Motor Efficiency}}\right) \times \left(\frac{\text{Load}}{\text{Factor}}\right) \times 2544, \text{ Btu per hour.} \quad (19)$$

TABLE 23. RATE OF HEAT GAIN FROM APPLIANCES Without Hoods[a,b]

APPLIANCE	CAPACITY	OVER-ALL DIMENSIONS (LESS LEGS AND HANDLES; LAST DIMENSION IS HEIGHT) INCHES	CONTROL A—AUTOMATIC M—MANUAL	MISCELLANEOUS DATA	MANUFACTURER'S RATING, WATTS	BTU/HR	MAINTAINING RATE BTU PER HOUR	RECOMMENDED RATE OF HEAT GAIN BTU PER HOUR		
								SENSIBLE	LATENT	TOTAL
Restaurant Electrical Appliances										
Coffee Brewer and Warmer	½ gal		M M	Brewer 660 w Warmer 90 w	600 90	2000 300	306	900 230	220 60	1120 290
Coffee Brewer Unit with Tank	½ gal	20 x 30 x 26		2000 w Water heater, 2960 w brewer	4960	17000		4800	1200	6000
Coffee Urn	3 gal 5 gal	12 x 23 x 21 18 (Diam.) x 37	A A	Nickel plated Nickel plated	4500 5000	15000 17000	2600 3600	2200 3400	1500 2300	3700 5700
Doughnut Machine		22 x 22 x 57	A	Exhaust System	4700	16000		5000	0	5000
Egg Boiler	2 cups	10 x 13 x 25	M		1100	3750		1200	800	2000
Food Warmer, with Plate Warmer, per sq ft of top surface			A	Insulated, separate heat unit for each pot; plate warmer in base	400	1350	500	350	350	700
Food Warmer, alone, per sq ft of top surface			A		300	1000	400	200	350	550
Fry Kettle	11½ lb fat	12 (Diam.) x 14	A		2600	8900	1100	1600	2400	4000
Fry Kettle	25 lb fat	16 x 18 x 12	A	Area 12 x 14 in	7000	24000	2000	3800	5700	9500
Griddle, Frying		18 x 18 x 8	A	Area 18 x 14 in.	2350	8000	2800	3100	1700	4800
Griddle, Frying		24 x 20 x 10	A	Area 23 x 18 in.	4000	13500	5000	5300	2900	8200
Grill, Meat		14 x 14 x 10	A	Area 10 x 12 in.	3000	10250	1900	3900	2100	6000
Grill, Sandwich		13 x 14 x 10	A	Area 12 x 12 in.	1650	5600	1900	2700	700	3400
Roll Warmer		23 x 23 x 29	A	Three drawers	1000	3400	900	2400	300	2700
Toaster, continuous	360 slices/hr	15 x 15 x 28	A	2 slices wide	2200	7500	5000	5100	1300	6400
Toaster, continuous	720 slices/hr	20 x 15 x 28	A	4 slices wide	3000	10250	6000	6100	2600	8700
Toaster, pop-up	216 slices/hr	12 x 11 x 9	A	4 slice	2450	8400	2000	4900	900	5800
Waffle Iron	20 waffles/hr	12 x 13 x 10	A	7 in. diam. waffle	750	2500	600	1100	750	1850

Restaurant Gas-Burning Appliances

Coffee Brewer and Warmer	½ gal		M M	Brewer Warmer		3400 500	500	1450 400	350 100	1790 500
Coffee Brewer Unit with Tank	4½ gal Tank	19 x 30 x 26		4 Brewers and Tank				7200	1800	9000
Coffee Urn	3 gal 5 gal	12 x 23 x 21 18 (Diam) x 37	A A	Nickel plated Nickel plated			3100 4700	2500 3900	2500 3900	5000 7800
Food Warmer, per sq ft of top surface			M	Water bath		2000	900	850	430	1280
Fry Kettle	15 lb fat	12 x 20 x 18	A	Area 10 x 10		14250	3000	4200	2800	7000
Fry Kettle	28 lb fat	15 x 35 x 11	A	Area 11 x 16		24000	4500	7200	4800	12000
Grill		22 x 14 x 17	M	Insulated, Grill surface of 1.4 sq ft Top burner 22,000 Btu/hr Bottom burner 15,000 Btu/hr		37000		14400	3600	18000
Stoves, Short Order Open Top, per sq ft top Closed Top, per sq ft top Fry Top, per sq ft top			 M M M	 Ring type burners Ring type burners Tubular type burners		 14000 11000 12000		 4200 3300 3600	 4200 3300 3600	 8400 6600 7200
Toaster, Continous	360 slices/hr	15 x 15 x 28	A	2 slices wide		12000	10000	7700	3300	11000
Toaster, Continous	640 slices/hr	20 x 15 x 28	A	4 slices wide		20000	14000	12000	5000	17000

Restaurant Steam-Heated Appliances

Coffee Urn	3 gal 5 gal	12 x 23 x 21 18 (Diam.) x 37	T T	Nickel plated Nickel plated				2400 3400	1600 2300	4000 5700
Coffee Urn	3 gal 5 gal	12 x 23 x 21 18 (Diam.) x 37	M M	Nickel plated Nickel plated				2600 3700	2600 3700	5200 7400
Food Warmer, per sq ft of top surface			T					400	500	900
Food Warmer, per sq ft of top surface			M					450	1150	1600

[a]For restaurant appliances, miscellaneous electrical and miscellaneous gas burning appliances.

[b]When these appliances are hooded and provided with adequate exhaust, use 50 per cent of recommended rate of heat gain from unhooded appliances.

TABLE 23. RATE OF HEAT GAIN FROM APPLIANCES Without Hoods [a,b] (CONCLUDED)

APPLIANCE	CAPACITY	OVER-ALL DIMENSIONS (LESS LEGS AND HANDLES; LAST DIMENSION IS HEIGHT) INCHES	CONTROL A—AUTOMATIC M—MANUAL	MISCELLANEOUS DATA	MANUFACTURER'S RATING WATTS	BTU/HR	MAINTAINING RATE BTU PER HOUR	RECOMMENDED RATE OF HEAT GAIN BTU PER HOUR		
								SENSIBLE	LATENT	TOTAL
Miscellaneous Electrical Appliances										
Hair Dryer, Blower Type			M	Fan, 165 w; Low, 915 w; High, 1580 w	1580	5400		2300	400	2700
Hair Dryer, Helmet Type			M	Fan, 80 w; Low, 300 w; High, 710 w	705	2400		1870	330	2200
Permanent Wave Machine			M	60 heaters at 25 w each, 36 in normal use	1500	5000		850	150	1000
Neon Sign, per linear ft of tube				½ in. outside diam. ⅜ in. outside diam.				30 60		30 60
Sterilizer, Instrument			A	For physicians; thermostat cuts off 550 w before boiling	1100	3750		650	1200	1850
Miscellaneous Gas-Burning Appliances										
Burners, Laboratory										
Small Bunsen		7/16 in. Barrel	M	Manufactured Gas		1800		960	240	1200
Small Bunsen		7/16 in. Barrel	M	Natural Gas		3000		1680	420	2100
Fishtail		7/16 in. Barrel	M	Manufactured Gas		3500		1960	490	2450
Fishtail		7/16 in. Barrel	M	Natural Gas		5500		3080	770	3850
Large Bunsen		1½ in. Mouth	M	Adjustable orifice		6000		3350	850	4200
Cigar Lighter			M	Continuous Flame		2500		900	100	1000
Hair Dryer, 5 helmets			A	Heater and fan blowing air to helmets		33000		15000	4000	19000
Stoves, Oven				Insulated, modern		25000	6000	7200	1800	9000
				Not insulated		25000	8500	9200	2300	11500

[a] For restaurant appliances, miscellaneous electrical and miscellaneous gas burning appliances.

[b] When these appliances are hooded and provided with adequate exhaust, use 50 per cent of recommended rate of heat gain from unhooded appliances.

It is assumed that both the motor and the driven equipment are within the conditioned space. If the motor is without the space, then *do not divide* by the motor efficiency in Equation 19. The *load factor* is merely the fraction of the rated load which is being delivered under the conditions of the cooling-load estimate. *Motor efficiencies* may be approximated as follows: about 50 to 60 per cent at ⅛ hp rating, increasing to 80 per cent at 1 hp, and to 88 per cent at 10 hp and above.

Appliances. Care must be taken in a cooling-load estimate to properly account for the heat gain from all appliances, electrical, gas, or steam. Table 23 presents recommended data [16]. Note that the *maintaining rate* in Table 23 is the heat input required to maintain the appliance at the normal operating temperature even though it is not being used; *i.e.*, no coffee is being made, no toast is being made, no food is being cooked in the fry kettle, etc. The maintaining rate is useful in setting up a lower limit to the heat gain to a room from the appliance when in operation.

Experienced judgment must be used in the application of data given in Table 23. Consideration must be given to the heat contributed by appliances which are in use at the time of peak load. The quantity of heat will depend upon whether products of combustion are vented to a flue, whether they escape into the space to be conditioned, or whether appliances are hooded allowing part of the heat to escape through a stack. There are no generally accepted data available on the effects of venting and shielding heating appliances but it is believed that, when they are properly hooded with a positive fan exhaust system through the hood, 50 per cent of the heat will be carried away and 50 per cent dissipated in the space to be conditioned. The same effectiveness of the hood should be figured for both latent and sensible heat.

LOAD FROM MOISTURE TRANSFERRING THROUGH PERMEABLE BUILDING MATERIALS

The diffusion of moisture through all common building materials is a natural phenomenon which is always present to a greater or lesser degree. The rate of moisture transfer through unit area of a material may be expressed as proportional to the *vapor pressure difference* between the adjacent air on the two sides of the material, and proportional to an overall moisture transfer coefficient called the *permeability* of the material. Permeability is a characteristic of the material and of the surface transfer conditions prevailing for moisture transfer; its magnitude is expressed as (grains of moisture) per (square foot) (hour) (inch of mercury vapor pressure difference). Permeability values [17] are given in Table 24.

In the usual comfort air-conditioning application, it is common practice to neglect moisture transfer through walls, for the actual rate is quite small and the corresponding latent-heat load is hardly significant. So-called *vapor barriers* are frequently employed in modern construction for the purpose of keeping moisture transfer to a minimum, particularly because of the deteriorating and insulation-destroying effects of moisture.

Industrial jobs, on the other hand, frequently call for a quiet low moisture content to be maintained in a conditioned space. Here the matter of moisture transfer cannot be neglected; indeed, it is quite possible to have the latent-heat load accompanying this transfer be of greater magnitude than any other latent-heat load. The equation for computing this load is:

$$\left(\frac{q_m}{A}\right) = (\text{Permeability}) \times \left(\begin{matrix}\text{Vapor Pressure}\\ \text{Difference, In. Hg}\end{matrix}\right) \times 1076, \text{ Btu per (hr) (sq ft)}. \quad (20)$$

The factor 1076 is defined in list of symbols at Equation 17. (Sensible cooling of the water vapor is included in the factor 1076).

The only means of preventing moisture transfer is to use a vapor proof wall or to apply a special lining, which is vapor proof. All openings in moisture proof construction must be equipped with special gaskets to prevent entrance of moisture.

When moisture transfer contributes an appreciable part of the latent-heat load, it is recommended that estimates should be made intentionally liberal in order to avoid later difficulties with insufficient dehumidifying capacity. Storage spaces, for example, would require sufficient dehumidifying capacity to handle the moisture brought in with goods to be stored in addition to moisture leaking in subsequently.

MISCELLANEOUS HEAT LOADS

This designation is intended to cover the various small heat gains from exposed piping, ducts, work done by circulating fan, and unforeseen contingencies. Where sufficient data are available these various heat gains may be estimated individually. In the majority of cases, however, common practice is to lump these factors together and combine them with a *safety factor* according to the experience and judgment of the estimator. On this basis, a small safety factor is added to the calculated cooling load to compensate for miscellaneous effects. No rules can be given for this procedure as experience in air conditioning is indispensable for application of suitable safety factors.

REQUIRED AIR QUANTITY THROUGH CONDITIONING EQUIPMENT

The procedure for determining the required air quantity is based upon the thermodynamic principles of Chapter 3 and the use of the Mollier diagram supplied with THE GUIDE, or a psychrometric chart. Readers are advised to review these principles, paying particular attention to the illustrative examples of cooling load calculations, and to refer to the section on Apparatus Dew Point in Chapter 43.

Calculation of the cooling load for a conditioned space is equivalent to making a heat balance for the space, in which all heat, moisture, and outdoor air are treated as directly entering the space; and then the desired conditions are maintained by considering a certain quantity of air to be withdrawn from the space, passed through the conditioning equipment, and returned to the space with such a temperature and humidity ratio that its net effect will be to counterbalance or *remove* the given entering amounts of heat and water vapor. This quantity of *indoor air* which is considered to be circulated in this manner is called the *required air quantity* and its determination is normally part of every cooling-load estimate. The procedure is as follows:

1. Determine the total sensible and latent heat loads in Btu per hour for the space.

2. Compute the quantity called the *specific enthalpy of the water removed*, q_w, from the relation

$$q_w = \left(\frac{\text{Space sensible load}}{\text{Space latent load}}\right) \times 1076 \text{ Btu/lb.} \qquad (21)$$

Note that the ratio (Space latent load) ÷ 1076 is the equivalent of the required rate of water-vapor removal, in pounds per hour. If the rate of water-vapor removal is known, it may be used directly in Equation 21.

TABLE 24. PERMEABILITY OF VARIOUS MATERIALS TO WATER VAPOR

GROUP	MATERIAL	PERMEABILITY GRAINS PER (SQ FT) (HR) (INCH HG)
1[a]	Plaster base and plaster, ¾ in.	14.7
	Fir sheathing, ¾ in.	2.9
	Waterproof paper[b]	49.1
	Pine lap siding	4.9
	Paint film	3.4
	Sugar cane fiberboard, ¾ in.	12.5
	Brick masonry, 4 in.	1.1
2[c]	Foil-surfaced reflective insulation, double-faced	0.08 to 0.13
	Roll roofing—smooth, 40 to 65 lb per roll 108 sq ft	0.13 to 0.17
	Duplex or laminated papers, 30-30-30	1.37 to 2.58
	Duplex or laminated papers, 30-60-30	0.52-0.86
	Duplex paper, coated with metallic oxides	0.52-1.29
	Insulation backup paper, treated	0.86-3.42
	Plaster, wood lath	11.00
	Plaster, 3 coats of lead and oil	3.68 to 3.84
	Plaster, 2 coats of aluminum paint	1.15
	Plaster, fiberboard or gypsum lath	19.73 to 20.57
	Plywood, ⅜ in., 5-ply Douglas fir	2.67 to 2.74
	Plywood, 2 coats of asphalt paint	0.43
	Plywood, 2 coats of aluminum paint	1.29
	Gypsum lath with metallic aluminum backing	0.09-0.39
	Insulating lath and sheathing, board type	25.68 to 34.27
	Insulating sheathing, surface-coated	3.03 to 4.36
	Insulating cork blocks, 1 in.	6.19
	Mineral wool, unprotected, 4 in.	29.07
	Sheathing paper, asphalt impregnated, glossy	0.17-2.05

[a]Calculating Vapor and Heat Transfer Through Walls, by L. G. Miller (*Heating and Ventilating* 35, No. 11, 56, November, 1938).

[b]Light weight slaters felt used to keep rain from drifting through. Not used as a vapor barrier.

[c]How to Overcome Condensation in Building Walls and Attics, by L. V. Teesdale (*Heating and Ventilating*, Vol. 36, No. 4, April, 1939).

3. Locate the state point of the room air (design wet-bulb and dry-bulb temperatures) on the Mollier diagram. From this state point draw a line intersecting the saturation line, using the slope established by the protractor on the Mollier diagram for the particular value of q_w prevailing. This line is the *condition line* for the process.

4. Read the temperature where the condition line from step 3 intersects the saturation line. This is called the *apparatus dewpoint*.

5. Compute the *required air quantity* from the relation

$$Q_{ra} = \frac{\text{(Space sensible load)}}{1.08\left[\left(\begin{matrix}\text{Space}\\ \text{dry-bulb}\end{matrix}\right) - \left(\begin{matrix}\text{Apparatus}\\ \text{dewpoint}\end{matrix}\right)\right] \times \left(\begin{matrix}\text{Coil}\\ \text{efficiency}\end{matrix}\right)} \qquad (22)$$

The magnitude of Q_{ra} is substantially the quantity, cfm, of cooled and dehumidified air for which the distribution system must be designed.

The numerical factor 1.08 is derived from the product 1 cfm × 60 min. × 0.244 × $0.075\left(1 - \frac{0.00923}{0.62}\right)$ = 1.08, assuming an average supply air dewpoint of 55 F. Since standard air density (0.075) includes the weight of the water vapor it is desirable to reduce it to the basis of dry air by the last factor where 0.00923 = humidity ratio of air at 55 F dewpoint, and 0.62 = ratio of density of water vapor to dry air at same temperature and pressure. Refer to Chapter 25 for coil selection.

Note that the product [(Space dry-bulb) − (Apparatus dewpoint)] × (Coil efficiency) is equal to the dry-bulb range through which the conditioned air is cooled. Hence, in rare instances when the *condition line* of the process may not intersect the saturation line, any other convenient reference temperature on the *condition line* may be used instead, provided that the coil efficiency is specified accordingly on the proper basis.

EXAMPLE—COOLING LOAD CALCULATION

An effective means of summarizing the calculation procedure will be the use of an illustrative example. While condensed calculation forms are commonly employed for work of this nature, an outline will be used here in order to facilitate explanatory comments.

Example 11. A one-story office building Fig. 7 is located in an eastern state near 40 deg latitude. The adjoining buildings on the north and west are not conditioned and the air temperature within them is known to be substantially equal to the outdoor air temperature at any time of the day.

South wall construction: 8 in. concrete block, 4 in. brick veneer, ½ in. plaster on walls. (Table 8, Chapter 6, No. 92B, $U = 0.41$.)

East wall and outside north wall construction: 8 in. concrete block, ½ in. plaster on walls. (Table 7, Chapter 6, No. 82B, $U = 0.52$.)

West wall and adjoining north party wall construction: 13 in. solid brick, no plaster:

$$\frac{1}{U} = \frac{1}{1.65} + \frac{13}{5} + \frac{1}{1.65} \text{ or, } U = 0.263. \text{ Use } U = 0.26.$$

Roof construction: 2½ in. flat roof deck of 2 in. gypsum fiber concrete on gypsum board surfaced with built-up roofing. (Table 14, Chapter 6, No. 6A, $U = 0.38$.)

Floor construction: 4 in. concrete on ground.

Window: 3 ft x 5 ft, non-opening type, with Venetian blinds for those on south wall. Approximately 4 in. reveal on all windows.

Front doors: Two 2 ft-6 in. x 7 ft (glass panels).

Side doors: Two 2 ft-6 in. x 7 ft (½ glass panels).

Rear doors: Two 2 ft-6 in. x 7 ft (glass panels).

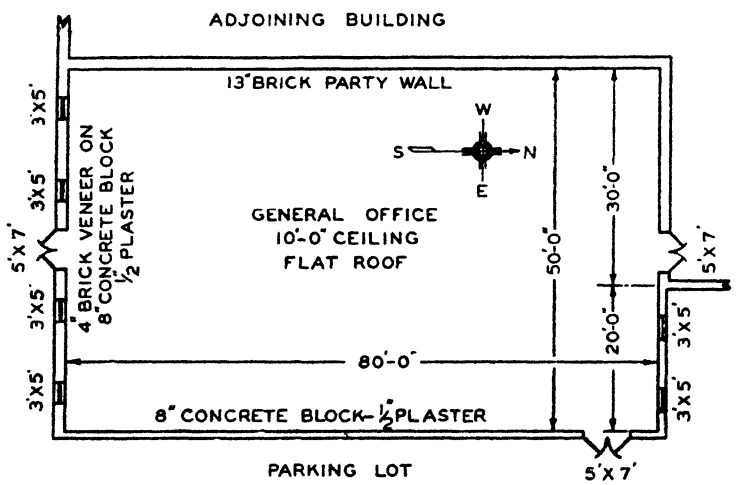

FIG. 7. PLAN OF ONE-STORY OFFICE BUILDING

Outside design conditions: Sol-air temperature cycle corresponding to New York City, Table 10, this chapter; maximum dry-bulb 95 F, wet-bulb 78 F; $W_o = 0.0169$ lbs vapor per lb dry air; $h_o = 41.38$ Btu per lb dry air.

Indoor design conditions: Dry-bulb 80 F, wet-bulb 65 F; $W_i = 0.0098$ lbs vapor per lb dry air; $h_i = 29.95$ Btu per lb dry air.

Occupancy: 85 office workers.

Lights: 12,000 watts fluorescent, 4,000 watts tungsten.

Fan motor: 7½ hp.

Conditioning equipment to be located in adjoining structure to north.

Required: Total, sensible, and latent maximum cooling loads and required air quantity through conditioning equipment.

Solution. From Table 4 the recommended ventilation rate is 15 cfm per person.

Total necessary = 85 × 15 = 1275 cfm or 76,500 cu ft per hr.

Check: Room volume is 40,000 cu ft = 1.91 air changes per hr.

Estimated Time of Maximum Cooling Load.

For this job, judgment indicates that the greatest single contribution to the cooling load will be from the roof. Hence, the time of the maximum cooling load will be the time of the maximum heat gain through the roof. In some cases, there would be no clear-cut evidence of this nature and consequently it would be necessary to estimate the load for several successive times and then to select the maximum.

From Table 12, estimate the roof time lag as 2 hours. From Table 13, take the time of the maximum rate of heat entry as 1:00 p. m. The estimated time of maximum interior heat gain follows as 3:00 p. m. (This may be slightly different than 3:00 p. m. civil time.)

Heat Gain Through Outer Wall and Roof Areas.

The first step is to determine values of t_p using Tables 10 and 12 and Fig. 4 as follows:

t_m (24 hr average) is read directly from Table 10.

The time lag is approximated from Table 12 for exterior walls.

South wall: Estimate 4 in. common brick as 2.3 hr, 8 in. concrete block and ½ in. plaster (equivalent to 6 in. of solid concrete) as 3.8 hr, plus 1 hr for heavy construction = approximately 7 hrs.

East wall and exposed North wall: Estimate 8 in. concrete block and ½ in. plaster as 3.8, plus 1 hr = approximately 5 hrs.

The time of maximum rate of heat entry is entered in the next column as the time earlier than 3:00 p. m. by the amount of the time lag. t_e* is read from Table 10. Factor λ is read from Fig. 4, and t_p is calculated from Equation 10.

The tabulation of the values obtained is given in the following table.

Section	t_m F[a]	Time Lag Hr	Time of Max. Heat Entry	t_e* F	Factor λ	t_p F
Roof (light const.)	106.4	2	1 p. m.	154	0.91	150
South wall	90.7	7	8 a. m.	86	0.30	89
East wall	92.3	5	10 a. m.	114	0.35	100
Exposed north wall	88.5	5	10 a. m.	92	0.50	90

*For $(b/f_o) = 0.25$.

Next, for an indoor temperature t_i = 80 F, the rates of heat gain may be calculated and tabulated.

Section	Net Area Sq Ft	U Btu/(Hr) (Sq Ft) (F Deg)	$(t_p - t_i)$ F Deg	q Btu Per Hr
Roof	4000	0.38	70	106,400
South wall	405[a]	0.41	9	1,490
East wall	765[a]	0.52	20	7,950
Exposed north wall	170[a]	0.52	10	880
			Total	116,720

[a]Calculated from gross wall area less windows and doors.

Determine Heat Gain Through Party Wall and Inside Door Areas.

For the door, estimate U = 0.59, from Chapter 6, Table 9, No. 5A. Space temperature at 3:00 p. m. is, from Table 10, 94 deg F. Neglect the time lag for the door and take $(t_p - t_i)$ = 94 − 80 = 14 F deg.

The party wall will be treated as if it were an outside wall in the shade, which corresponds to (b/f_o) = 0 in Table 10. From Table 12, time lag = 9.5 hr, λ = 0.23.

$$t_p = 84.8 + 0.23\ (76 - 84.8) = 82.8\ \text{F}.$$

Section	Net Area Sq Ft	U Btu/(Hr) (Sq Ft) (F Deg)	$(t_o - t_i)$ F Deg	q Btu Per Hr
Party wall	1065[a]	0.26	2.8	775
Door	35	0.59	14	290
			Total	1065

[a]Calculated from gross wall area less door area.

Heat Gain Through Glass Areas.

In computing the load for 3:00 p. m., only the south windows and doors will be exposed to direct sunlight. Table 15 and Equation 12 will give the total heat gain from the glass areas. The window reveals will slightly shade the south windows; the fraction of window area receiving direct radiation is obtained from Equation 13 by substituting values as follows:

$r_1 = s/l = 4/60$; $r_2 = 4/36$; $\beta = 45.5$ deg, $\tan \beta = 1.02$.

$\gamma = 16$ deg, $\tan \gamma = 0.287$.

$$G_f = 1 - \frac{4}{60} \times 1.02 - \frac{4}{36} \times 0.287 + \frac{4}{60} \times \frac{4}{36} \times 1.02 \times 0.287 = 0.902.$$

The south doors will be considered entirely sunlit. The outdoor air temperature is 94 F at 3:00 p. m. From Table 20 the inside Venetian blind factor is taken as 0.75. Referring to Table 15 the instantaneous heat gain due to solar and sky radiation for 40 deg n. latitude for south exposure at 3:00 p.m. is read as 42 Btu per sq ft. These figures are tabulated below. $60 \times 0.902 \times .75 \times 42 = 1705$ Btu per hr. The normal transmission $60 \times 1.04\ (94 - 80) = 874$. The sum of these heat gains is totaled in last column. The remaining doors and windows are calculated in a similar manner.

Location	Area Sq Ft	Fraction Sunlit	Inside Venetian Blind Shading Factor	Solar Heat Gain Btu/Sq Ft	Radiation Heat Gain[a] Btu/Hr	Normal Heat Transfer Btu/Hr	Total Heat Gain Btu/Hr
South windows	60	0.902	0.75	42.	1705.	874.	2579.
South doors	35	1.00	.....	42.	1470.	510.	1980.
East[b]	18	.....	.....	15.	27.		
doors	35	.....	.....	.....	270.	510.	780.
North windows	30	.....	.....	15.	450.	437.	887.
						Total	6226.

[a]See Equation 12 and the note under caption of Table 15.

[b]Doors are ½ glass. Calculate sky radiation for glass portion and normal transmission for entire door assuming $U = 1.04$ for wood portion as well as glass

In some jobs it would be proper to increase (or decrease) the instantaneous radiation heat gain by a load-lag factor. The reason for not doing so in this case is that the solar gain is of a low magnitude and reference to the table indicates that 0.8 of the previous hour would not affect the results materially.

Heat Gain From Ventilation and Infiltration.

Since the necessary ventilation rate of 1275 cfm is greater than one air change per hour, it will be satisfactory for determining the ventilation component of the heat gain.

Window infiltration will be taken as negligible since the windows do not open and the ventilation rate is almost 2 changes per hour which is sufficient to prevent normal expected infiltration through closed windows with storm sash.

Door infiltration requires some judgment. Assume that for each person passing through the double doors, the infiltration will be 100 cu ft of outdoor air, see Table 21. Assume that the outside doors will be used at the rate of 10 persons per hour, and the inside doors at the rate of 30 persons per hour. Total infiltration will then be $40 \times 100 = 4000$ cfh or 67 cfm.

The design rate of entry of outside air is then

$$Q = 1275 + 67 = 1342 \text{ cfm.}$$

The sensible, latent and total loads are determined from Equations 15, 16 and 17, respectively at 3:00 p. m. (Table 10) $t_o = 94$, $t_i = 80$, $W_o = 0.0169$, $W_i = 0.0098$.

$q_s = 1342 \times 1.08\ (94 - 80) = 21{,}700$ Btuh.

$q_e = 1342 \times 4840\ (0.0169 - 0.0098) = 46{,}100$ Btuh.

$q_t = q_s + q_e = 21{,}700 + 46{,}100 = 67{,}800$ Btuh.

Heat Gain from Sources Within the Conditioned Space.

For the occupants, use the data of Table 22 for moderately active office work.

Sensible heat = $85 \times 200 = 17{,}000$ Btu per hr.

Latent heat = $85 \times 250 = 21{,}250$ Btu per hr.

Total = 38,250 Btu per hr.

For the *lighting*, use Equation 18 with a use factor of unity, and a special allowance factor of 1.20 for the fluorescents and of unity for the tungsten globes.

$q_{el} = (12{,}000 \times 1.20 + 4000) \times 3.41 = 62{,}700$ Btu per hr.

For the *fan motor*, use Equation 19 with a load factor of unity and do not introduce the motor efficiency because of the motor being external to the space.

$$q_{em} = 7.5 \times 2544 = 19{,}100 \text{ Btu per hr.}$$

Moisture Permeation, Miscellaneous Allowance, and the Load-Lag Estimate.

Moisture permeation will be negligible, since this is a comfort job with a good building construction.

There would be some heat gain in the ductwork, but this would not be great because of the short run involved. Practical judgment on this job would suggest that no adjustment for load lag need be made to the load as computed. While it is true that inside radiation forms an important part of the total heat gain, it is advisable to be conservative in recognizing the effect of the large, flat, hot roof on the *comfort sensations of the occupants*. Radiation from the relatively low ceiling, augmented by heat absorption from the lighting fixtures, would produce a sensation of warmth in excess of the nominal effective temperature (see Chapter 12) established by the wet-bulb and dry-bulb temperatures. Hence, it is not desirable to take advantage of every small decrease possible in the peak design load, especially since the peak occurs in mid-afternoon when everything would be rather well warmed.

Total Loads and Required Air Quantity Through Conditioning Equipment.

The total loads are summarized below.

Load Component	Sensible, Btu Per Hour	Latent, Btu Per Hour
Outer walls and roof	116,720	
Party wall and inside door	1,065	
Glass areas	6,226	
Ventilation and infiltration	21,700	46,100
Occupants	17,000	21,250
Lighting	62,700	
Motor	19,100	
Totals	244,511	67,350
Grand Total		311,861

Compute the *specific enthalpy of the water removed* from Equation 22.

$$q_w = \frac{244{,}500}{67{,}350} \times 1076 = 3900 \text{ Btu per lb.}$$

From the Mollier diagram, determine that the *apparatus dewpoint* is 47.9 F. (Refer to Chapters 3 and 43.)

In computing the effective air quantity, assume a coil efficiency of 85 per cent. Then,

$$Q_{ra} = \frac{244{,}500}{1.08\ (80 - 47.9) \times 0.85} = 8300 \text{ cfm.}$$

(Refer to Chapter 25 for coil selection and efficiency.)

LETTER SYMBOLS USED IN CHAPTER 15

β = solar altitude, degrees.

γ = difference between the azimuth angle of an outdoor wall and the azimuth angle of the horizontal projection of the sun's rays, degrees.

ε = surface emissivity, the ratio of the heat emission by radiation from a surface to the radiation from a perfectly black surface, dimensionless.

λ = amplitude decrement factor, a variable depending on thickness, material, and orientation of the wall or roof dimensionless.

θ = angle of incidence for sun's rays striking a surface, degrees.

τ = fraction of incident radiant energy transmitted through a glass section, dimensionless.

A = area across which heat is being transferred, square feet.

a = fraction of incident radiant energy absorbed within a glass section, dimensionless.

b = fraction of incident radiant energy absorbed by a non-transparent surface, dimensionless.

e = ratio of direct solar radiation to sky radiation falling on a horizontal surface, dimensionless.

f_o = unit convective conductance for outdoor surface = film coefficient of heat transfer of outdoor air, Btu per (square foot) (hour) (Fahrenheit degree).

G_f = fraction of total window area receiving direct solar radiation when shaded by window reveal, dimensionless.

h_i = enthalpy of indoor air per pound of dry air, Btu per pound.

h_o = enthalpy of outdoor air per pound of dry air, Btu per pound.

I_d = direct solar radiation incident upon a surface at any angle of incidence, Btu per (square foot) (hour).

I_n = direct solar radiation incident on a surface at normal incidence, Btu per (square foot) (hour).

I_s = sky radiation incident upon a surface, Btu per (square foot) (hour).

$I_t = I_s + I_d$, Btu per (square foot) (hour).

K = cosine of angle of incidence for direct solar radiation striking a surface, dimensionless.

k = thermal conductivity of building material, Btu per (square foot) (hour) (Fahrenheit degree per foot).

L = thickness of building material, feet.

l = height of window, feet.

P_d = partial pressure of atmospheric water vapor at earth's surface, inches of mercury.

Q = rate of entry of outdoor air, cubic feet per minute.

Q_{ra} = required air quantity through conditioning equipment, cubic feet per minute.

q = instantaneous rate of heat transfer, Btu per hour.

q_e = instantaneous latent heat load, Btu per hour.

q_s = instantaneous sensible heat load, Btu per hour.

$q_t = q_e + q_s$, Btu per hour.

q_w = specific enthalpy of water vapor removed (used on Mollier diagram) Btu per pound.

r = fraction of incident radiation reflected from glass surface, dimensionless.

T = absolute temperature, (F deg + 460).

t_e = sol-air temperature, Fahrenheit degrees.

t_e^* = sol-air temperature at a time earlier than the time for which heat gain is being found by an amount that is equal to the time lag of the wall or roof, Fahrenheit degrees.

t_i = indoor air temperature, Fahrenheit degrees.

t_L = temperature of outer surface of building, Fahrenheit degrees.

t_m = 24-hr cyclic average sol-air temperature, Fahrenheit degrees.

$t_p = t_m + (t_e^* - t_m)$, *net* equivalent outdoor temperature for combined periodic and mean heat flow, Fahrenheit degrees.

U = over-all coefficient of heat transfer of a structural section, Btu per (square foot) (hour) (Fahrenheit degree).
v_o = volume of outdoor air per pound of dry air, cubic feet.
w = width of window, feet.
W_i = humidity ratio of indoor air, pounds moisture per pound of dry air.
W_o = humidity ratio of outdoor air, pounds moisture per pound of dry air.

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Chapter 16

FUELS AND COMBUSTION

Classification of Coals, Cokes, Fuel Oils, and Gas, Dustless Treatment of Coal, Fundamental Principles of Combustion, Heat of Combustion, Air Required for Combustion, Excess Air, Heat Balance, Firing Methods, Secondary Air, Draft Requirements, Draft Regulation, Furnace Volume, Combustion of Gas, Soot, Condensation and Corrosion

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FUELS may be classified according to their physical state as solid, liquid, or gaseous. The principal fuels used for domestic heating are coal, oil, and gas. However, coke, wood, kerosene, sawdust, briquettes, and other substances are used for heating in special applications or in localities where an adequate supply is available. Experiments are in progress in the use of a colloidal suspension of coal particles in fuel oil, but this fuel has not attained wide-spread usage as yet. The choice of fuel is usually based on dependability, cleanliness, availability, economy, operating requirements, and control.

CLASSIFICATION OF COALS

Coal has a complex composition that makes classification into clear-cut types difficult. Chemically it consists of carbon, hydrogen, oxygen, nitrogen, sulfur, and a mineral residue called ash. A chemical analysis provides some indication of the quality of a coal, but does not define its burning characteristics sufficiently. The coal user is interested principally in the available heat per pound of coal, in the handling and storing properties, the amount of ash and dust produced and the burning characteristics. A description of the relationship between the qualities of coals and these characteristics requires considerable space; a treatment applicable to heating boilers is given in a Bureau of Mines Bulletin .[1]

There are two forms of coal analysis; namely, the *proximate analysis* and the *ultimate analysis*. In the *proximate analysis* the proportions of moisture, volatile matter, fixed carbon, sulfur, and ash are determined. This analysis is more easily made and is satisfactory for indicating most of the characteristics which are of interest to the user. For the proximate analysis the moisture is determined by observing the loss of weight of a sample of coal when dried at about 220 F. To determine the volatile matter, the dried sample is heated to about 1750 F in a closed crucible, and the loss of weight is noted. The remaining sample is then burned in an open crucible, and the accompanying loss of weight represents the fixed carbon. The unburned residue is ash. Although determined separately, the sulfur content is frequently reported with the proximate analysis because the usefulness of a coal for certain purposes depends on its sulfur content.

In the *ultimate analysis*, which is difficult to make, the percentages of carbon, hydrogen, oxygen, nitrogen, sulfur, and ash in the coal sample are determined. It is used for detailed studies of fuels and in computing a heat balance when required in testing of heating devices. Typical ultimate analyses of the various kinds of coal are shown in Table 1.[2]

Other important qualities of coals are the screen sizes, ash fusion temperature, friability, caking tendency, and the qualities of the volatile matter. In considering these factors the following points are of interest.

TABLE 1. TYPICAL ULTIMATE ANALYSES FOR COALS

RANK	BTU PER LB		CONSTITUENTS, PER CENT						
	Moist, Mineral-matter-free[a]	Moist, as Received	Oxygen	Hydrogen	Carbon	Nitrogen	Sulfur	Ash	$\frac{O_2+}{H_2+C}$
Anthracite	14,600	12,910	5.0	2.9	80.0	0.9	0.7	10.5	87.9
Semi-Anthracite	15,200	13,770	5.0	3.9	80.4	1.1	1.1	8.5	89.3
Low-Volatile Bituminous	15,350	14,340	5.0	4.7	81.7	1.4	1.2	6.0	91.4
Medium-Volatile Bituminous	15,200	13,840	5.0	5.0	79.0	1.4	1.5	8.1	89.0
High-Volatile Bituminous *A*	14,500	13,090	9.2	5.3	73.2	1.5	2.0	8.8	87.7
High-Volatile Bituminous *B*	13,500	12,130	13.8	5.5	68.0	1.4	2.1	9.2	87.3
High-Volatile Bituminous *C*	12,000	10,750	21.0	5.8	60.6	1.1	2.1	9.4	87.4
Sub Bituminous *A*									
Sub Bituminous *B*	10,250	9,150	29.5	6.2	52.5	1.0	1.0	9.8	88.2
Sub Bituminous *C*	9,000	8,940	35.8	6.5	46.7	0.8	0.6	9.6	89.0
Lignite	7,500	6,900	44.0	6.9	40.1	0.7	1.0	7.3	91.0

[a] $\left(\frac{100}{100 - 1.1 \text{ Ash}}\right)$ (Btu as received).

The volatile products given off by coals when they are heated differ materially in the ratios by weight of the gases to the oils and tars. No heavy oils or tars are given off by anthracite, and very small quantities are given off by semi-anthracite. As the volatile matter in the coal increases to as much as 40 per cent of ash and moisture-free coal, increasing amounts of oils and tars are released. For coals of higher volatile content, the relative quantity of oils and tars decreases and is therefore low in the sub-bituminous coals and in lignite. The percentage of ash and its fusion temperature do not indicate the composition or distribution of its constituents.

A classification of coals is given in Table 2, and a brief description of the kinds of fuel is given in the following paragraphs, but it should be recognized that there are no distinct lines of demarcation between the kinds, and that they graduate into each other.

Anthracite is a clean, dense, hard coal which creates little dust in handling. It is comparatively hard to ignite but it burns freely when well started. It is non-caking, it burns uniformly and smokelessly with a short flame, and it requires no attention to the fuel bed between firings. It is capable of giving a high efficiency in the common types of hand-fired furnaces. A tabulation of the quality of the various anthracite sizes will be found in a Bureau of Mines Report [3]. Standard anthracite sizing specifications are shown in Table 3.

Semi-anthracite has a higher volatile content than anthracite. It is not so hard and ignites somewhat more easily; otherwise its properties are similar to those of anthracite.

Semi-bituminous coal is soft and friable, and fines and dust are created by handling it. It ignites somewhat slowly and burns with a medium length of flame. Its caking properties increase as the volatile matter increases, but the coke formed is relatively weak. Having only half the volatile matter content of the more abundant bituminous coals it can be burned with less production of smoke, and it is sometimes called *smokeless coal.*

The term *bituminous coal* covers a large range of coals and includes many types having distinctly different composition, properties, and burning characteristics. The coals range from the high-grade bituminous coals of the East to the poorer coals of the West. Their caking properties range from coals which completely melt, to those from which the volatiles and tars are distilled without change of form, so that they are classed as non-caking or free-burning. Most bituminous coals are strong and non-friable enough to

permit of the screened sizes being delivered free from fines. In general, they ignite easily and burn freely; the length of flame varies with different coals, but it is long. Much smoke and soot are possible, if improperly fired, especially at low rates of burning.

Sub-bituminous coals occur in the western states; they are high in moisture when mined and tend to break up as they dry or when exposed to the weather; they are liable to ignite spontaneously when piled or stored. They ignite easily and quickly and have a medium length flame, are non-caking and free-burning; the lumps tend to break into small pieces if poked; very little smoke and soot are formed.

Lignite is of woody structure, very high in moisture as mined, and of low heating value; it is clean to handle. It has a greater tendency than the sub-bituminous coals to disintegrate as it dries, and it also is more liable to spontaneous ignition. Freshly mined lignite, because of its high moisture, ignites slowly. It is non-caking. The char left after the moisture and volatile matter are driven off burns very easily, like charcoal. The lumps tend to break up in the fuel bed and pieces of char falling into the ashpit continue to burn. Very little smoke or soot is formed.

TABLE 2. CLASSIFICATION OF COALS BY RANK[a]

Legend: F.C. = Fixed Carbon. V.M. = Volatile Matter. Btu = British thermal units.

CLASS	GROUP	LIMITS OF FIXED CARBON OR BTU MINERAL-MATTER-FREE BASIS	REQUISITE PHYSICAL PROPERTIES
I. Anthracite	1. Meta-anthracite	Dry F.C., 98 per cent or more (Dry V.M., 2 per cent or less)	Non-agglomerating[b]
	2. Anthracite	Dry F.C., 92 per cent or more and less than 98 per cent (Dry V.M., 8 per cent or less and more than 2 per cent)	
	3. Semi-anthracite	Dry F.C., 86 per cent or more and less than 92 per cent (Dry V.M., 14 per cent or less and more than 8 per cent)	
II. Bituminous[d]	1. Low volatile bituminous coal	Dry F.C., 78 per cent or more and less than 86 per cent (Dry V.M., 22 per cent or less and more than 14 per cent)	Either agglomerating[b] or non-weathering[f]
	2. Medium volatile bituminous coal	Dry F.C., 69 per cent or more and less than 78 per cent (Dry V.M., 31 per cent or less and more than 22 per cent)	
	3. High volatile *A* bituminous coal	Dry F.C., less than 69 per cent (Dry V.M., more than 31 per cent); and moist[c] Btu, 14,000[e] or more	
	4. High volatile *B* bituminous coal	Moist[c] Btu, 13,000 or more and less than 14,000[e]	
	5. High volatile *C* bituminous Coal	Moist Btu, 11,000 or more and less than 13,000[e]	
III. Sub-bituminous	1. Sub-bituminous *A* coal	Moist Btu, 11,000 or more and less than 13,000[e]	Both weathering and non-agglomerating[b]
	2. Sub-bituminous *B* coal	Moist Btu, 9500 or more and less than 11,000[e]	
	3. Sub-bituminous *C* coal	Moist Btu, 8300 or more and less than 9500[e]	
IV. Lignitic	1. Lignite	Moist Btu less than 8300	Consolidated
	2. Brown coal	Moist Btu less than 8300	Unconsolidated

[a]This classification does not include a few coals which have unusual physical and chemical properties and which come within the limits of fixed carbon or Btu of the high-volatile bituminous and sub-bituminous ranks. All of these coals either contain less than 48 per cent dry, mineral-matter-free fixed carbon or have more than 15,500 moist, mineral-matter-free Btu.

[b]If agglomerating, classify in low-volatile group of the bituminous class.

[c]Moist Btu refers to coal containing its natural bed moisture but not including visible water on the surface of the coal.

[d]It is recognized that there may be non-caking varieties in each group of the bituminous class.

[e]Coals having 69 per cent or more fixed carbon on the dry, mineral-matter-free basis shall be classified according to fixed carbon, regardless of Btu.

[f]There are three varieties of coal in the high-volatile *C* bituminous coal group, namely, Variety 1, agglomerating and non-weathering; Variety 2, agglomerating and weathering; Variety 3, non-agglomerating and non-weathering.

Adapted from *A.S.T.M.* Standards, 1937, Supplement, p. 145, *American Society for Testing Materials* Philadelphia.

DUSTLESS TREATMENT OF COAL

The practice of treating the more friable coals to allay the dust they create is increasing. The coal is sprayed with various petroleum products, a solution of calcium chloride or a mixture of calcium and magnesium chlorides.

The coal is usually treated at the mine, but sometimes by the local distributor just before delivery. The salt solutions are sprayed under high pressure, using from 2 to 4 gal or from 5 to 10 lb of the salt per ton of coal, depending on its friability and size. Oil for the dustless treatment of coal is also applied under high pressure, in concentrations of 1 to 8 qt per ton of coal, depending upon the characteristics of the coal and oil.

Dustless treatments which are of such a corrosive nature that they may damage coal handling or burning equipment should not be used.

CLASSIFICATION OF COKES

Coke is produced by the distillation of the volatile matter from coal. The type of coke depends on the coal or mixture of coals used, the temperatures and time of distillation and, to some extent, on the type of retort or oven; coke is also produced as a residue from the destructive distillation of oil.

High-temperature cokes. Coke as usually available is of the high-temperature type, and contains between 1 and 2 per cent volatile matter. High-temperature cokes are subdivided into *beehive coke* of which comparatively little is now sold for domestic use, *by-product coke*, which covers the greater part of the coke sold, and *gas-house coke.* The differences among these three cokes are relatively small; their denseness and hardness decrease and friability increases in the order named. In general, the lighter and more friable cokes ignite and burn the more easily.

Low-temperature cokes are produced at low coking temperatures, and only a portion of the volatile matter is distilled off. Cokes as made by various processes under development have contained from 10 to 15 per cent volatile matter. In general, these cokes ignite and burn more readily than high-temperature cokes. The properties of various low-temperature cokes may differ more than those of the various high-temperature cokes because of the differences in the quantities of volatile matter and because some may be light and others briquetted.

Petroleum cokes, which are obtained by coking the residue left from the distillation of petroleum, vary in the amount of volatile matter they contain, but all have the common property of a very low ash content, which necessitates the use of refractory pieces to protect the grates from being burned.

TABLE 3. STANDARD ANTHRACITE SIZING SPECIFICATIONS[a]

SIZE	TEST MESH, IN.		ROUND MESH			MAXIMUM IMPURITIES, PER CENT	
			Oversize	Undersize			
	Through	Over	Max. Per Cent	Max. Per Cent	Min. Per Cent	Slate[b]	Bone
Broken	4⅜	3¼	.....	15	7½	1½	2
Egg	3¼ to 3	2⅞	5	15	7½	1½	2
Stove	2⅞	1⅝	7½	12½	7½	2	3
Nut	1⅝	15/16	7½	10	5	3	4
Pea	15/16	⅝	10	15	7½	4	5
Buckwheat	⅝	5/16	10	15	7½	12 Ash	
Rice	5/16	3/16	10	15	7½	13 Ash	
Barley	3/16	3/32	10	20	10	.....	

[a]Approved and adopted by *Anthracite Committee*, State Street Building, Harrisburg, Pa.

[b]When slate content on Broken to Pea inclusive is less than above standards, bone content may be correspondingly increased, but slate content specified above shall not be exceeded in any event and the total maximum impurities shall not exceed those above specified.

TABLE 4. DETAILED REQUIREMENTS FOR FUEL OILS[a]

GRADE[b]	FLASH POINT F DEG		POUR POINT F DEG	WATER AND SEDIMENT PER CENT	CARBON RESIDUE PER CENT	ASH PER CENT	DISTILLATION TEMPERATURES F DEG				VISCOSITY SECONDS			
							10 Per Cent Point	90 Per Cent Point		End Point	Saybolt Universal at 100 F		Saybolt Furol at 122 F	
	Min.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Min.	Max.	Max.	Min.	Max.	Min.
No. 1 Fuel oil—a distillate oil for use in burners requiring a volatile fuel.	100 or Legal	165	0[c]	Trace	0.05 on 10% Residuum[d]		410			560[e]				
No. 2 Fuel oil—a distillate oil for use in burners requiring a moderately volatile fuel.	110 or Legal	190	10[c]	0.05	0.25 on 10% Residuum[f]		440	600						
No. 3 Fuel oil—a distillate oil for use in burners requiring a low viscosity fuel.	110 or Legal	230	20[c]	0.10	0.15 Straight			675	600[g]		45			
No. 5 Fuel oil—an oil for use in burners requiring a medium viscosity fuel.	130 or Legal			1.00		0.10						50	40	
No. 6 Fuel oil—an oil for use in burners equipped with preheaters permitting a high viscosity fuel.	150			2.00[h]									300	45

[a]Recognizing the necessity for low sulfur fuel oils used in connection with heat-treatment, non-ferrous metal, glass and ceramic furnaces and other special uses, a sulfur requirement may be specified in accordance with the following table:

GRADE OF FUEL OIL	SULFUR, MAX. PER CENT
No. 1	0.5
No. 2	0.5
No. 3	0.75
No. 5	No Limit
No. 6	No Limit

Other sulfur limits may be specified only by mutual agreement between the buyer and seller.

[b]It is the intent of these classifications that failure to meet any requirement of a given grade does not automatically place an oil in the next lower grade unless in fact it meets all requirements of the lower grade.

[c]Lower or higher pour points may be specified whenever required by conditions of storage or use. However, these specifications shall not require a pour point lower than 0 F under any conditions.

[d]For use in other than sleeve type blue flame burners carbon residue on 10 per cent residuum may be increased to a maximum of 0.12 per cent. This limit may be specified by mutual agreement between the buyer and seller.

[e]The maximum end point may be increased to 590 F when used in burners other than sleeve type blue flame burners

[f]To meet certain burner requirements the carbon residue limit may be reduced to 0.15 per cent on 10 per cent residuum.

[g]The minimum distillation temperature of 600 F for 90 per cent may be waived if *A.P.I.* gravity is 26 or lower.

[h]Water by distillation, plus sediment by extraction. Sum, maximum 2.0 per cent. The maximum sediment by extraction shall not exceed 0.50 per cent. A deduction in quantity shall be made for all water and sediment in excess of 1.0 per cent.

TABLE 5. APPROXIMATE GRAVITY AND CALORIFIC VALUE OF STANDARD GRADES OF FUEL OIL

COMMERCIAL STANDARD NO.	APPROXIMATE GRAVITY RANGE *A.P.I.*	CALORIFIC VALUE BTU PER GALLON
1	38-40	136,000
2	34-36	138,500
3	28-32	141,000
5	18-22	148,500
6	14-16	152,000

CLASSIFICATION OF FUEL OILS

Fuel oils are produced by distillation from crude petroleum after gasoline, naphtha, and other lighter products have been removed. Fuel oil is composed chemically of about 85 per cent carbon and 12½ per cent hydrogen with small amounts of oxygen, nitrogen, and sulfur. Oils are classified according to their specific gravity, but specific gravity alone is not a sufficient index of the properties that are important for heating purposes. Other characteristics that must be considered in the choice of a fuel oil are the flash point, pour point, water and sediment content, carbon residue, ash, sulfur content, distillation temperatures, and viscosity.

The flash point and distillation characteristics are important relative to easy ignition and complete gasification of the oil in a burner. A low pour point and low water content are of interest in connection with the storage of the fuel in outdoor tanks, while a low viscosity permits easy passage through a small orifice. The sediment, carbon residue, and ash content should be low to prevent clogging of strainers and accumulation of unburned material in the burner. The sulfur content may be of importance because of the corrosive effect of sulfur compounds in the burner and heating appliance or in special commercial processes.

The Commercial Standard Specifications for Fuel Oils (CS 12-40) of the *U. S. Department of Commerce* are given in Table 4. These specifications conform to *American Society for Testing Materials* Tentative Specifications for Fuel Oils D 396-38T.

The relationship between the *A.P.I.* gravity of fuel oils and their calorific value is given in Table 5. Fuel oil grades No. 1, No. 2 and No. 3 only are used in domestic heating equipment. Grades No. 5 and No. 6 are used in commercial and industrial burners and usually require preheating.

CLASSIFICATION OF GAS

Gas is broadly classified as being either *natural* or *manufactured.* Natural gas is a mechanical mixture of several combustible and inert gases rather than a chemical compound. Manufactured gas as distributed is usually a combination of certain proportions of gases produced by two or more processes. Representative properties of gaseous fuels commonly used in domestic heating are presented in Table 6.

Natural gas is the richest of the gases and contains from 80 to 95 per cent methane, with small percentages of the other combustible hydrocarbons. In addition, it contains from 0.5 to 5.0 per cent of CO_2, and from 1 to 12 or 14 per cent of nitrogen. The heat value varies from 1000 to 1200 Btu per cubic foot, the majority of natural gases averaging about 1000 Btu per cubic foot. Table 6 shows typical values for the

TABLE 6. REPRESENTATIVE PROPERTIES OF GASEOUS FUELS, BASED ON GAS AT 60 F AND 30 IN. HG.

GAS	BTU PER CU FT		SPECIFIC GRAVITY, AIR = 1.00	AIR REQUIRED FOR COMBUSTION, (CU FT)	PRODUCTS OF COMBUSTION				THEORETICAL FLAME TEMPERATURE, (F DEG)
					Cubic Feet			ULTIMATE CO_2 Dry Basis	
	High (Gross)	Low (Net)			CO_2	H_2O	Total with N_2		
Natural gas—California	1200	1085	0.67	11.26	1.24	2.24	12.4	12.2	3610
Natural gas—Mid-Continental	970	870	0.57	9.17	0.97	1.92	10.2	11.7	3580
Natural gas—Ohio	1130	1025	0.65	10.70	1.17	2.16	11.8	12.1	3600
Natural gas—Pennsylvania	1130	1025	0.71	11.70	1.30	2.29	12.9	12.3	3620
Retort coal gas	570	510	0.42	5.00	0.50	1.21	5.7	11.2	3665
Coke oven gas	590	520	0.42	5.19	0.51	1.25	5.9	11.0	3660
Carbureted water gas	540	495	0.65	4.37	0.74	0.75	5.0	17.2	3815
Blue water gas	300	280	0.53	2.26	0.46	0.51	2.8	22.3	3800
Anthracite producer gas	135	125	0.85	1.05	0.33	0.19	1.9	19.0	3000
Bituminous producer gas	150	140	0.86	1.24	0.35	0.19	2.0	19.0	3160
Oil gas	575	510	0.35	4.91	0.47	1.21	5.6	10.7	3725

four main oil fields, although values from any one field vary materially.

Table 6 also gives the calorific values of the more common types of manufactured gas. Most states have legislation which controls the distribution of gas and fixes a minimum limit to its heat content. The gross or higher calorific value usually ranges between 520 and 545 Btu per cubic foot, with an average of 535. A given heat value may be maintained and yet leave considerable latitude in the composition of the gas so that as distributed the composition is not necessarily the same in different districts, nor at successive times in the same district. However, in any community the variations in gas composition are held within suitable limits so that the performance of approved gas appliances will not be adversely affected.

FUNDAMENTAL PRINCIPLES OF COMBUSTION

Combustion may be defined as the chemical combination of a substance with oxygen with a resultant evolution of heat. The rate of combustion depends partly upon the specific rate of reaction of the combustible substance with oxygen, partly upon the rate at which oxygen is supplied, and upon the temperature obtained due to surrounding conditions.

Complete combustion is obtained when all of the combustible elements in the fuel are oxidized with all of the oxygen with which they can combine. All of the oxygen supplied may not be utilized.

Perfect combustion is defined as the result of supplying the required

amount of oxygen for combination with all of the combustible elements of the fuel and utilizing all of the oxygen so supplied.

The oxygen required for the process of combustion is obtained from air which is a mechanical mixture of oxygen, nitrogen and small amounts of carbon dioxide, water vapor and inert gases. These inert gases are generally included with the nitrogen, and for engineering purposes the values given herewith may be used.

	By Volume, Per Cent	By Weight, Per Cent
Oxygen, O_2	20.9	23.15
Nitrogen, N_2	79.1	76.85

The combination of oxygen with the combustible elements and compounds of a fuel is in accordance with fixed laws. In the case of perfect combustion the reactions and resultant combinations are shown in Table 7.

The most important condition governing the process of combustion is temperature. It is necessary to bring a combustible substance to its ignition temperature before it will unite in chemical combination with oxygen to produce combustion. The ignition temperatures for several of the combustible constituents of fuels are presented in Table 7.

HEAT OF COMBUSTION

As previously stated, the process of combustion results in the evolution of heat. The heat generated by the complete combustion of a unit of fuel is constant for a given combination of combustible elements and compounds, and is known as the *heat of combustion*, *calorific value*, or *heating value* of the fuel. The heat of combustion of the several substances found in the more common fuels is given in Table 7.

The calorific value of a fuel may be determined either by direct measurement of the heat evolved during combustion in a calorimeter, or it may be computed from the ultimate analysis and the heat of combustion of the several chemical elements in the fuel. When the heating value of a fuel is determined in a calorimeter the water vapor is condensed and the latent heat of vaporization is included in the heating value of the fuel. The heating value so determined is termed the *gross* or *higher* heating value and this is what is ordinarily meant when the heating value of a fuel is specified. In burning the fuel, however, the products of combustion are not cooled to the dew-point and the higher heating value cannot be utilized.

When combustion is complete, the carbon in the fuel unites with oxygen to form carbon dioxide, CO_2, the hydrogen unites with oxygen to form water vapor, H_2O, and the nitrogen, being inert, passes through the reaction without change. When combustion is incomplete, some of the carbon may unite with oxygen to form carbon monoxide, CO, and some of the hydrogen and hydrocarbon gases may not be burned at all. When carbon monoxide or other combustible gases are present in the flue gases, considerably less heat is produced per unit of fuel consumed, and a lower combustion efficiency is obtained. Incomplete combustion may result from any or all of the following three conditions:

1. **Inadequate air supply.**
2. **Insufficient mixing of the air and gases.**
3. **A temperature too low to produce ignition or maintain combustion.**

TABLE 7. GENERAL DATA OF COMBUSTIBLE ELEMENTS AND COMPOUNDS [a]

SUBSTANCE	MOLECULAR SYMBOL	CHEMICAL REACTION OF COMBUSTION	IGNITION TEMPERATURE[a] F DEG	CALORIFIC VALUE			THEORETICAL OXYGEN AND AIR REQUIREMENTS			
				Btu per Lb		Btu per Cu Ft[b]	Lb per Lb		Cu Ft per Cu Ft	
				Higher	Lower	Higher	O_2	Air	O_2	Air
Carbon (to CO)	—	$2C + O_2 = 2CO$	—	3950	—	—	1.332	5.763	—	—
Carbon (to CO_2)	—	$2C + 2O_2 = 2CO_2$	—	14093	—	—	2.664	11.527	—	—
Sulfur (to SO_2)	—	$S + O_2 = SO_2$	—	3983	—	—	0.998	4.285	—	—
Sulfur (to SO_3)	—	$2S + 3O_2 = 2SO_3$	—	5940	—	—	1.497	6.428	—	—
Carbon Monoxide	CO	$2CO + O_2 = 2CO_2$	1166-1319	4347	—	321.8	0.571	2.471	0.5	2.382
Methane	CH_4	$CH_4 + 2O_2 = CO_2 + 2H_2O$	1260-1380	23879	21520	1013.2	3.990	17.265	2.0	9.528
Acetylene	C_2H_2	$2C_2H_2 + 5O_2 = 4CO_2 + 2H_2O$	763-824	21500	20776	1499	3.073	13.297	2.5	11.911
Ethylene	C_2H_4	$C_2H_4 + 3O_2 = 2CO_2 + 2H_2O$	986-1123	21644	20295	1613.8	3.422	14.807	3.0	14.293
Ethane	C_2H_6	$2C_2H_6 + 7O_2 = 4CO_2 + 6H_2O$	990-1120	22320	20432	1792	3.725	16.119	3.5	16.675
Hydrogen	H_2	$2H_2 + O_2 = 2H_2O$	1063-1166	60958[c]	51571[c]	325	7.937	34.344	0.5	2.382
Hydrogen Sulfide	H_2S	$2H_2S + 3O_2 = 2H_2O + 2SO_2$	599-608	7100	6545	647	1.409	6.097	1.5	7.146
Propane	C_3H_8	$C_3H_8 + 5O_2 = 3CO_2 + 4H_2O$	950-1080	21661	19944	2590	3.629	15.703	5.0	23.821
n-Butane	C_4H_{10}	$2C_4H_{10} + 13O_2 = 8CO_2 + 10H_2O$	890-1020	21308	19680	3370	3.579	15.487	6.5	30.967
Commercial Propane	—	—	—	21650	—	2500	—	—	—	—
Commercial Butane	—	—	—	21400	—	3200	—	—	—	—

[a] Values in table taken chiefly from page 51 of Fuel Flue Gases published by *American Gas Association*.
[b] Gas measured at 60 F and 30 in. Hg.
[c] Value from *National Bureau of Standards*.

TABLE 8. APPROXIMATE THEORETICAL AIR REQUIREMENTS

SOLID FUEL	POUNDS AIR PER POUND FUEL
Anthracite	9.6
Semi-bituminous coal	11.2
Bituminous coal	10.3
Lignite	6.2
Coke	11.2

FUEL OIL	POUNDS AIR PER GALLON FUEL
Commercial Standard No. 1	102.6
Commercial Standard No. 2	104.5
Commercial Standard No. 3	106.5
Commercial Standard No. 5	112.0
Commercial Standard No. 6	114.2

GASEOUS FUELS	CUBIC FEET AIR PER CUBIC FOOT GAS
Natural gas	10.0
Mixed, natural and water gas	4.4
Carbureted water gas	4.4
Water gas, coke	2.1
Coke oven gas	5.2

AIR REQUIRED FOR COMBUSTION

The weight of air required for perfect combustion of a pound of fuel may be determined by use of the ultimate analysis of the fuel as applied to Equations 1 and 2. The various elements are expressed in percentages by weight.

Solid and Liquid Fuels:

$$\text{Pounds air required per pound fuel} = 34.56\left[\frac{C}{3} + \left(H - \frac{O}{8}\right) + \frac{S}{8}\right] \quad (1)$$

Gaseous Fuels:

$$\text{Pounds air required per pound fuel} = 2.46\,CO + 34.56\,H_2 + 17.28\,CH_4 + 13.29\,C_2H_2 + 14.81\,C_2H_4 + 16.13\,C_2H_6 + 6.10\,H_2S - 4.32\,O_2 \quad (2)$$

When the analysis is given on a volumetric basis the equation is expressed as follows:

$$\text{Cubic feet air required per cubic foot gas} = 2.39\,(CO + H_2) + 9.56\,CH_4 + 11.98\,C_2H_2 + 14.35\,C_2H_4 + 16.74\,C_2H_6 - 4.78\,O_2 \quad (3)$$

Equations 4 and 5 may be used as approximate methods of determining the theoretical air requirement for any fuel.

$$\text{Pounds air required per pound fuel} = 0.755 \times \frac{\text{Heating value (Btu per pound)}}{1000} \quad (4)$$

$$\text{Cubic feet air required per unit fuel} = \frac{\text{Heating value (Btu per unit)}}{100} \quad (5)$$

Approximate values for the theoretical air required for different fuels are given in Table 8.

It is customary to make use of the analysis of the products of combustion to determine the amount of flue gas produced and the actual amount of air supplied for combustion. The analysis of flue gases has been well described in various publications of the *Bureau of Mines* and

in the literature and the details of Orsat manipulation need not be considered in this discussion. (See Chapter 11.)

The weight of dry flue gas per pound of fuel burned is used in combustion loss calculations and may be determined by Equation 6.

$$\text{Pounds dry flue gas per pound fuel} = \frac{11\ CO_2 + 8\ O_2 + 7\ (CO + N_2)}{3\ (CO_2 + CO)} \times C \qquad (6)$$

Values for CO_2, O_2, CO, and N_2 are percentages by volume from the flue gas analysis and C is the weight of carbon burned per pound of fuel corrected for carbon in the ash.

EXCESS AIR

Since one measure of the efficiency of combustion is the relation existing between the amount of air theoretically required for *perfect* combustion and the amount of air actually supplied, a method of determining the latter factor is of value. Equation 7 will give reasonably accurate results, for most solid and liquid fuels, for determining the amount of air supplied per pound of fuel.

$$\text{Pounds dry air supplied per pound of fuel} = \frac{3.04\ N_2}{(CO_2 + CO)} \times C \qquad (7)$$

Values for CO_2, CO, and N are percentages by volume from the flue gas analysis and C is the weight of carbon burned per pound of fuel corrected for carbon in the ash.

The difference between the air actually supplied for combustion and the theoretical air required is known as excess air.

$$\text{Per cent excess air} = \frac{\text{Air supplied} - \text{Theoretical air}}{\text{Theoretical air}} \qquad (8)$$

Since the calculation is usually made from Orsat analysis, Equation 9 will be found to be a convenient statement of this relationship.

$$\text{Per cent excess air} = \frac{100\left(O_2 - \frac{CO}{2}\right)}{N_2 \times 0.264 - \left(O_2 - \frac{CO}{2}\right)} \qquad (9)$$

In this formula the symbols represent volumetric percentages of the flue gas constituents as determined by analysis.

Due to the different carbon-hydrogen ratios of the different fuels the maximum CO_2 attainable varies. Representative values for complete combustion of several fuels are given in Table 9.

TABLE 9. REPRESENTATIVE MAXIMUM CO_2 VALUE

FUEL	THEORETICAL CO_2	CO_2 USUALLY ATTAINED IN PRACTICE
Coke	21.00	12-14
Anthracite	20.20	12-14
Bituminous Coal	18.20	13
No. 2 Fuel Oil	15.00	10.5
No. 6 Fuel Oil	16.50	13.5
Natural Gas	12.00	9.7
Coke Oven Gas	11.00	8.5

To produce heat efficiently with any of the common fuels the following requirements must be observed:

1. Adequate heat absorbing surface is necessary.
2. The heat transfer surfaces must be clean.
3. A minimum of excess air should be used.
4. The combustion air and the combustible gases produced by the fuel must be well mixed.
5. The quantity of combustible gases escaping to the stack must be kept small.

If insufficient heating surface is provided in a heating appliance, or if the heat transfer surfaces are covered with soot, ash or scale, the flue gas temperature will be excessive and the amount of sensible heat passing up the stack will be unnecessarily large. Too much excess air dilutes the flue gases excessively and increases the sensible flue gas loss, while a deficiency of air will cause some combustible gases to pass out of the appliance unburned. The highest combustion efficiency is not always obtained by supplying enough excess air to reduce the incomplete combustion loss to zero, but the incomplete combustion loss should be kept small. If the secondary air is not well mixed with the combustible gases, some incomplete combustion may still occur. Unnecessary secondary air also dilutes the flue gases and increases the sensible heat escaping up the chimney. Some excess air is always required in the practical operation of heating plants. It is considered good practice, under usual operating conditions, to supply from 25 to 50 per cent excess air, depending upon the fuel used.

HEAT BALANCE

In analyzing the performance of a heating appliance, it is frequently desirable to make an accounting, insofar as possible, of the disposition of all the heat units in the fuel used. Such an accounting is sometimes called a *heat balance*. The several components of the heat balance may either be expressed in terms of Btu per pound of fuel used or as a percentage of the calorific value of the fuel. The components of the heat balance are listed in items 1 to 7.

1. Useful heat transferred to heating medium and usually evaluated by determining the rate of flow of the heating fluid through the heating device and the change in enthalpy of the fluid (heat added) between the inlet and outlet.

2. Heat loss in the dry chimney gases.

$$h_1 = w_g c_p (t_g - t_a) \tag{10}$$

3. Heat loss in water vapor formed by the combustion of hydrogen.

$$h_2 = \frac{9H_2}{100} (1091.8 + 0.455\, t_g - t_a) \tag{11}$$

4. Heat loss in water vapor in the air supplied for combustion.

$$h_3 = 0.455\, M\, w_a (t_g - t_a) \tag{12}$$

5. Heat loss from incomplete combustion.

$$h_4 = 10143\, C \left(\frac{CO}{CO_2 + CO}\right) \tag{13}$$

6. Heat loss from unburned carbon in the ash or refuse.

$$h_5 = 14093 \left(\frac{C_u}{100} - C\right) \tag{14}$$

7. Radiation and all other unaccounted for losses.

Since the radiation and convection losses from a heating appliance are not usually determined by direct measurement, they, together with any other losses not measured, are determined by subtracting the total of items 1 to 6 inclusive from the heat of combustion of the fuel. Frequently, when there is *CO* in the flue gases there also will be small amounts of unburned hydrogen and hydrocarbon gases in the products of combustion. The loss represented by these unburned gases may easily be as large as that resulting from the presence of carbon monoxide. In this event item 7 of the heat balance would also include this unmeasured loss.

Symbols used in Equations 10 to 14 inclusive are:

h_1 = heat loss in the dry chimney gases, Btu per pound of fuel.
h_2 = heat loss in water vapor from combustion of hydrogen, Btu per pound of fuel.
h_3 = heat loss in water vapor in combustion air, Btu per pound of fuel.
h_4 = heat loss from incomplete combustion of carbon, Btu per pound of fuel.
h_5 = heat loss from unburned carbon in the ash, Btu per pound of fuel.
w_g = weight of dry flue gas per pound of fuel (from Equation 6), pounds.
c_p = mean specific heat of flue gases at constant pressure (c_p ranges from 0.242 to 0 254 for flue gas temperatures from 300 F to 1000 F)[2], Btu per pound.
t_g = temperature of flue gases at exit of heating device, Fahrenheit degrees.
t_a = temperature of combustion air, Fahrenheit degrees.
H_2 = percentage of hydrogen in fuel by weight from ultimate analysis of fuel as fired.
1091.8 = enthalpy of saturated water vapor at a temperature of 70 F, Btu per pound.
M = humidity ratio of combustion air, pounds of water vapor per pound of dry air.
w_a = weight of combustion air per pound of fuel used, pounds, from Equations 1, 2, 8, and 9.
C = weight of carbon burned per pound of fuel corrected for carbon in ash, pounds.

$$C = \frac{WC_u - W_a C_a}{100\ W} \qquad (15)$$

where

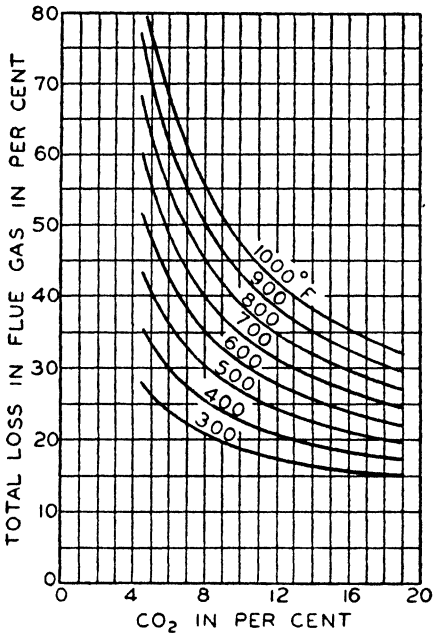
C_u = percentage of carbon in the fuel by weight from the ultimate analysis.
CO, CO_2 = percentages of CO, CO_2 in flue gases by volume.
W_a = weight of ash and refuse, pounds.
C_a = per cent of combustible in ash by weight (combustible in ash is usually considered to be carbon).
W = weight of fuel used, pounds.

The flue gas losses listed as items 2, 3, and 4 of the heat balance may be determined with considerable accuracy from the curves shown in Fig. 1 [2] in many cases. The values of the losses plotted for fuel oil were computed from the ultimate analysis of a typical fuel oil used in domestic burners, while those plotted for the several ranks of coal were computed from the typical ultimate analyses shown in Table 1. The curves for medium volatile bituminous coal may be used for high volatile bituminous coal with negligible error. No curves are shown for gaseous fuel because various natural gases and manufactured gases vary considerably in their composition.

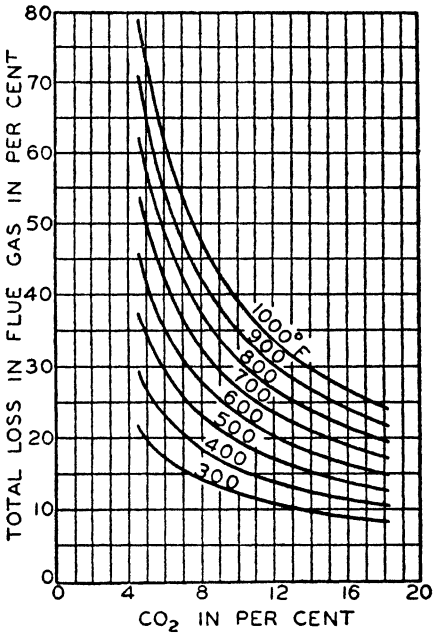
FIRING METHODS FOR ANTHRACITE

An anthracite fire should never be poked or disturbed, as this serves to bring ash to the surface of the fuel bed where it may melt into clinker.

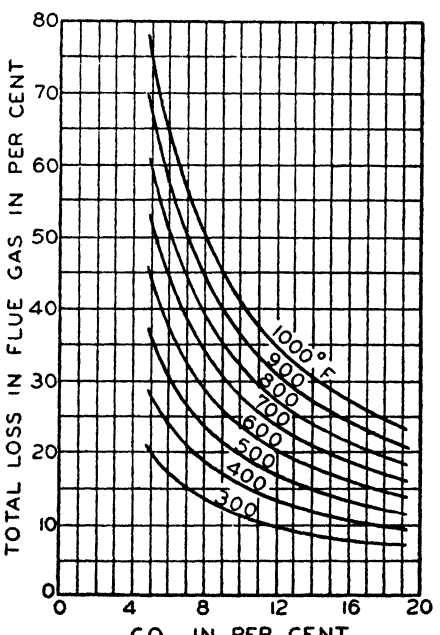
Egg size is suitable for large fire-pots (grates 24 in. and over) if the fuel



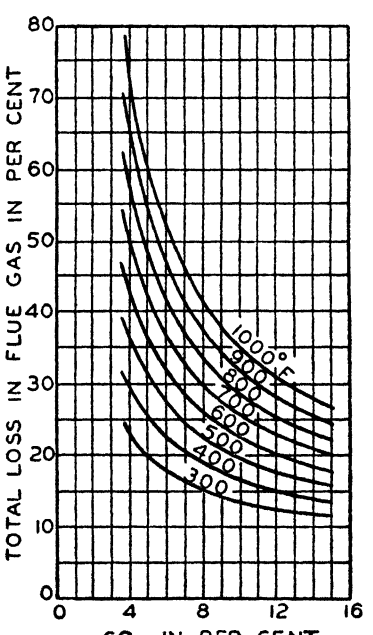
LIGNITE



MEDIUM-VOLATILE BITUMINOUS



ANTHRACITE



FUEL OIL

FIG. 1. FLUE GAS LOSSES WITH VARIOUS FUELS[8]

can be fired at least 16 in. deep. For best results this coal should be fired deeply.

Stove size coal is the proper size of anthracite for many boilers and furnaces used for heating buildings. It burns well on grates at least 16 in. in diameter and 12 in. deep. The fuel should be fired deeply and uniformly.

Chestnut size coal is in demand for fire-pots up to 20 in. in diameter, with a depth of from 10 to 15 in.

Pea size coal is often an economical fuel to burn. When fired carefully, pea coal can be burned on standard grates. Care should be taken to shake the grates only until the first bright coals begin to fall through the grates. The fuel bed, after a new fire has been built, should be increased in thickness by the addition of small charges until it is at least level with the sill of the fire-door. A satisfactory method of firing pea coal consists of drawing the red coals toward the front end and piling fresh fuel toward the back of the fire-box.

Pea size coal requires a strong draft and therefore the best results generally will be obtained by keeping the choke damper open and regulating solely by means of the cold air check and the air inlet damper.

Buckwheat size coal for best results requires more attention than pea size coal, and in addition the smaller size of the fuel makes it more difficult to burn on ordinary grates. Greater care must be taken in shaking the grates than with the pea coal on account of the danger of the fuel falling through the grate. In house heating furnaces the coal should be fired lightly and more frequently than pea coal. When banking a buckwheat coal fire it is advisable after coaling to expose a small spot of hot fire by putting a straight poker down through the bed of fresh coal. This will serve to ignite the gas that will be distilled from the fresh coal and prevent delayed ignition within the fire-pot, which in some cases, depending upon the thickness of the bed of fresh coal, is severe enough to blow open the doors and dampers of the furnace. Where frequent attention can be given and care exercised in manipulation of the grates this fuel can be burned satisfactorily without the aid of any special equipment.

In general it will be found more satisfactory with buckwheat coal to maintain a uniform heat output and consequently to keep the system warm all the time, rather than to allow the system to cool off at times and then to attempt to burn the fuel at a high rate while warming up. A uniform low fire will minimize the clinker formation and keep the clinker in an easily broken up condition so that it readily can be shaken through the grate. Forced draft and small mesh grates are frequently used for burning buckwheat anthracite. For greater convenience, domestic stokers are used.

Buckwheat anthracite No. 2, or rice size, is used principally in stokers of the domestic, commercial and industrial type. No. 3 buckwheat anthracite, or barley, has no application in domestic heating.

FIRING METHODS FOR BITUMINOUS COAL

A commonly recommended procedure for firing domestic heating units, called the side-bank method, requires the movement of live coals to one side or the back of the grate, and placing the fresh fuel charge on the opposite side. The results are a more uniform release of volatile gases, and the subjection of these gases to the high temperature of the red coals. If the fresh charge is covered with a layer of fine coal, still better results may be obtained because of slower release of volatile matter.

Bituminous coal should never be fired over the entire fuel bed at one time. A portion of the glowing fuel should always be left exposed to ignite the gases leaving the fresh charge.

The importance of firing bituminous coal in small quantities at short intervals is discussed in a U. S. Bureau of Mines technical paper[1]. Better combustion is obtained by this method in that the fuel supply is maintained more nearly proportional to the air supply.

If the coal is of the caking kind the fresh charge will fuse into one solid mass which can be broken up with the stoking bar and leveled from 20 min to one hour after firing, depending on the temperature of the fire-box. Care should be exercised when stoking not to bring the bar up to the surface of the fuel as this will tend to bring ash into the high temperature zone at the top of the fire, where it will melt and form clinker. The stoking bar should be kept as near the grate as possible and should be raised only enough to break up the fuel. With fuels requiring stoking it may not be necessary to shake the grates, as the ash is usually dislodged during stoking.

It is acknowledged that it may be difficult to apply the outlined methods to domestic heating boilers of small size, especially when frequent attendance is impractical. The adherence to these methods insofar as practical, however, will result in better combustion.

The output obtained from any heater with bituminous coal will usually exceed that obtained with anthracite, since bituminous coal burns more rapidly than anthracite and with less draft. Bituminous coal, however, will usually require frequent attention to the fuel bed.

Preventing Smoke

In general, time, temperature and turbulence are the essential requirements for smokeless combustion. Anything that can be done to increase any one of these factors will reduce the quantity of smoke discharged. Especial care must be taken in hand-firing bituminous coals.

Checker or alternate firing, in which the fuel is fired alternately on separate parts of the grate, maintains a higher furnace temperature and thereby decreases the amount of smoke.

Coking and firing, in which the fuel is first fired close to the firing door and the coke pushed back into the furnace just before firing again, produces the same effect. The volatiles as they are distilled thus have to pass over the hot fuel bed where they will be burned if they are mixed with sufficient air and are not cooled too quickly by the heat-absorbing surfaces of the boiler.

Steam or compressed air jets, admitted over the fire, create turbulence in the furnace and bring the volatiles of the fuel more quickly into contact with the air required for combustion. These jets are especially helpful for the first few minutes after each firing. *Frequent firings* of small charges shorten the smoking period and reduce the density. *Thinner fuel beds* on the grate increase the effective combustion space in the furnace, supply more air for combustion, and are sometimes effective in reducing the smoke emitted, but care should be taken that holes are not formed in the fire. A *lower volatile coal* or a higher *A.P.I.* gravity oil always produces less smoke than a high volatile coal or low *A.P.I.* gravity oil used in the same furnace and fired in the same manner.

The installation of more modern or better designed fuel burning equipment, or a change in the construction of the furnace, will often reduce

smoke. The installation of a Dutch oven which will increase the furnace volume and raise the furnace temperature often produces satisfactory results.

In the case of new installations, the problem of smoke abatement can be solved by the selection of the proper fuel-burning equipment and furnace design for the particular fuel to be burned and by the proper operation of that equipment. Constant vigilance is necessary to make certain that the equipment is properly operated. In old installations the solution of the problem presents many difficulties, and a considerable investment in special apparatus is often necessary.

Lower rates of combustion per square foot of grate area will reduce the quantity of solid matter discharged from the chimney with the gases of combustion. The burning of coke, coking coal, and sized coal from which the extremely fine coal has been removed will not as a general rule produce as much dust and cinders as will result from the burning of non-coking coals and slack coals when they are burned on a grate.

Modern boiler installations are usually designed for high capacity per square foot of ground area because such designs give the lowest cost of construction per unit of capacity. Designs of this type discharge a large quantity of dust and cinders with the gases of combustion, and if pollution of the atmosphere is to be prevented, some type of catcher must be installed.

FIRING METHODS FOR SEMI-BITUMINOUS COAL

The *Pocahontas Operators' Association* recommends the central cone method of firing, in which the coal is heaped on to the center of the bed forming a cone, the top of which should be level with the middle of the firing door. This allows the larger lumps to fall to the sides, and the fines to remain in the center and be coked. The poking should be limited to breaking down the coke without stirring, and to gently rocking the grates. It is recommended that the slides in the firing door be kept closed, as the thinner fuel bed around the sides allows enough air to get through.

FIRING METHODS FOR COKE

Coke ignites less readily than bituminous coal and more readily than anthracite and burns rapidly with little draft. In order to control the air admitted to the fuel it is very important that all openings or leaks into the ashpit be closed tightly. A coke fire responds rapidly to the opening of the dampers. This is an advantage in warming up the system, but it also makes it necessary to watch the dampers more closely in order to prevent the fire from burning too rapidly. In order to obtain the same interval of attention as with other fuels a deep fuel bed always should be maintained when burning coke. The grates should be shaken only slightly in mild weather and should be shaken only until the first red particles drop from the grates in cold weather. The best size of coke for general use, for small fire-pots where the fuel depth is not over 20 in., is that which passes over a 1 in. screen and through a 1½ in. screen. For large fire-pots where the fuel can be fired over 20 in. deep, coke which passes over a 1 in. screen and through a 3 in. screen can be used, but a coke of uniform size is always more satisfactory. Large sizes of coke should be either mixed with fine sizes or broken up before using.

SECONDARY AIR

When bituminous coal is hand-fired in a furnace the volatile matter in the fuel distills off leaving coke on the grate. The product of combustion of the coke is CO_2 and under certain conditions some CO may arise from the bed. The combustion of the volatile matter and the CO may amount to the liberation of from 40 to 60 per cent of the heat in the fuel in the combustion space over the fuel bed.

The air that passes through the fuel bed is called *primary air* and the air that is admitted over the fuel bed in order to burn the volatile matter and CO is called *secondary air.*

This process of combustion is illustrated in Fig. 2 [4]. The free oxygen of the air passes through the grate and the ash above it and burns the carbon in the lower 3 or 4 in. of the fuel bed forming carbon dioxide. This layer noted as the oxidizing zone is indicated by the symbols CO_2 and O_2. Some of the carbon dioxide of the oxidizing zone is reduced to carbon monoxide in the upper layer of the fuel bed noted as the reducing zone and indicated by the symbols CO_2 and CO. The gases leaving the fuel

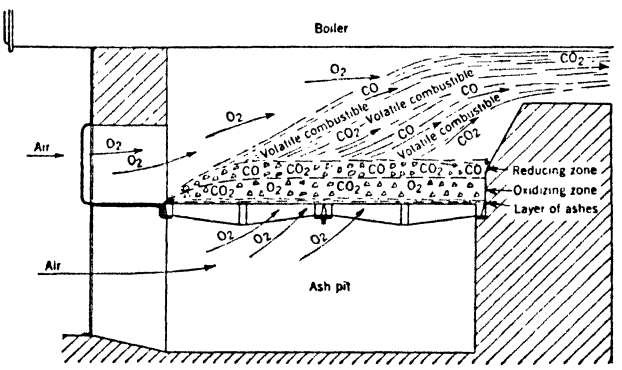


FIG. 2. COMBUSTION OF FUEL IN A HAND-FIRED FURNACE

bed are mainly carbon monoxide, carbon dioxide, nitrogen, and a small amount of free oxygen. Free oxygen is admitted through the firing door in an attempt to burn carbon monoxide and the volatile combustible distilled from the freshly fired fuel.

The division of the total into primary and secondary air necessary to produce the same rate of burning and the same excess air depends on a number of factors which include size and type of fuel, depth of fuel bed, and size of fire-pot.

Size of the fuel is a very important factor in fixing the quantity of secondary air required for non-caking coals. With caking coals it is not so important because small pieces fuse together and form large lumps. Fortunately a smaller size fuel gives more resistance to air flow through the fuel bed and thus automatically causes a larger draft above the fuel bed, which draws in more secondary air through the same slot openings, but, nevertheless, the smallest size of fuel will require the largest secondary air openings. For certain sizes of fuel no secondary air openings are required, and for large sizes, too much excess air may pass through the fuel bed.

In general, the efficiency of domestic hand-fired furnaces and boilers burning either anthracite or bituminous coal can be increased for an

hour or two after firing, if some secondary air is admitted through the slots of the fire door. However, unless the slots are closed when secondary air is no longer beneficial, the decrease in efficiency during the remainder of the firing cycle because of excess air may more than offset the gain resulting from the secondary air at the beginning of the firing period. Unless the secondary air can be readjusted between firings, it is probable that a greater average efficiency will be obtained for domestic hand-fired devices by leaving the secondary air slots closed at all times. There is usually an appreciable amount of air leakage around the firing door and secondary air slots of domestic furnaces and boilers.

When attention is given between firings the efficiency of combustion can be appreciably raised by admitting secondary air over a bituminous coal fire to burn the gases and reduce the smoke. The smoke produced is a good indicator, and that opening is best which reduces the smoke to a minimum. Too much secondary air will cool the gases below the ignition point, and prove harmful instead of beneficial.

Secondary air that enters the combustion chamber too far removed from the zone of combustion will also be harmful, for the oxygen in the secondary air will not react with any unburned gases unless the mixture is subjected to high temperatures.

The air requirements of oil and gas burners are discussed in Chapter 17, Automatic Fuel Burning Equipment.

DRAFT REQUIREMENTS

The draft required to effect a given rate of burning the fuel is dependent on the following factors:

1. Kind and size of fuel.
2. Grate area.
3. Thickness of fuel bed.
4. Type and amount of ash and clinker accumulation.
5. Amount of excess air present in the gases.
6. Resistance offered by the boiler passes to the flow of the gases.
7. Accumulation of soot in the passes.

Insufficient draft will necessitate additional manipulation of the fuel bed and more frequent cleanings to keep its resistance down. Insufficient draft also restricts the control that can be accomplished by adjustment of the dampers.

The quantity of excess air present has a marked effect on the draft required to produce a given rate of burning. If the excess is caused by holes in the fuel bed, or an extremely thin fuel bed, it is often possible to produce a higher rate of burning by increasing the thickness of the bed. The thickness of the fuel bed should not, however, be increased too much because the increased draft resistance will reduce the rate of primary air supply and the rate of burning.

For amount of draft required see Chapter 19, Chimneys and Draft Calculations.

DRAFT REGULATION

Because of the varying heating load demands present in most installations it is necessary to vary the rate of fuel burning. The maintenance of the proper air supply for the various rates of burning is accomplished

by regulation of the drafts. Correct and incorrect methods of draft regulation are shown in Fig. 3. The air enters through the ashpit draft door, firing door, and by leaks in the setting, whereas the gases leave only through the uptake. By throttling the gases with the damper in the uptake all the air entering by each of the three intakes is reduced in the same proportion, thus maintaining about the same per cent of excess air. If the ashpit draft door is closed, the air admitted through the ashpit is reduced, while it is increased through the other two intake openings, resulting in an increase of excess air. A considerable increase in the efficiency of hand-fired furnaces and boilers can be realized by regulating the air supply with the damper in the smokepipe instead of the ashpit damper. Use of the ashpit damper is required, of course, for low rates of combustion.

Methods of control of draft conditions when burning oil or gas are noted in Chapter 17, Automatic Fuel Burning Equipment.

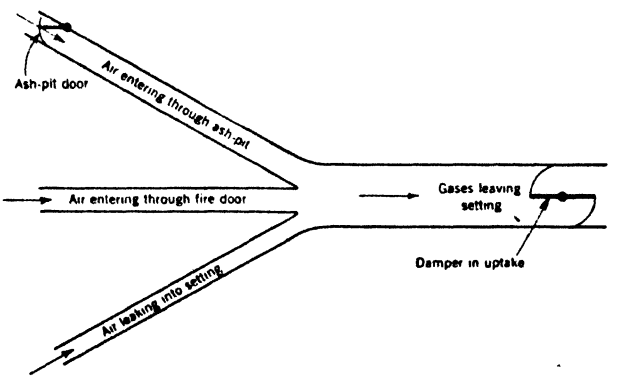


FIG. 3. CORRECT AND INCORRECT METHODS OF DRAFT REGULATION IN A HAND-FIRED FURNACE

FURNACE VOLUME

The principal requirements for a *hand-fired furnace* are that it shall have enough grate area and correctly proportioned combustion space. The amount of grate area required is dependent upon the desired combustion rate.

The furnace volume is influenced by the kind of coal used. Bituminous coals, on account of their long-flaming characteristic, require more space in which to burn the gases of combustion completely than do the coals low in volatile matter. For burning high volatile coals provision should be made for mixing the combustible gases thoroughly, so that combustion is complete before the gases come in contact with the relatively cool heating surfaces. An abrupt change in the direction of flow tends to mix the gases of combustion more thoroughly. Anthracite requires comparatively little combustion space.

COMBUSTION OF GAS

The majority of gas burners utilized in central domestic heating plants are of the Bunsen type and operate with a non-luminous flame. In this

type of burner part of the air required for combustion is mixed with the gas as primary air, the air and gas mixture being fed to the burner ports. Additional secondary air is introduced around the flame by draft inspiration. In the luminous flame burner, which is sometimes used, all of the air for combustion is brought in contact with the flame as secondary air. This secondary air should be brought into intimate contact with the gas.

Some makes of burners use radiants or refractories to convert some of the energy in the gas to radiant heat. The radiants also serve as baffles in directing the flow of the products of combustion.

The quantity of air given in Table 6 is that required for theoretical combustion, but with a properly designed and installed burner the excess air can be kept low. In order to insure freedom from carbon monoxide under conditions which may obtain in installations, it is customary to design gas burning appliances for a supply of 30 to 35 per cent of excess air. In individual installations in which flue gas analyses are made, the excess air is sometimes reduced to approximately 20 per cent. The division of the air into primary and secondary is a matter of burner design, the pressure of gas available, and the type of flame desired.

The air gas ratio has a decided effect upon flame propagation. It is necessary that the gas will flow out of the burner ports fast enough so that the flame cannot travel back into the burner head, i.e. *flash back*, but the velocity must not be so high that it blows the flame away from the port.

The maximum and minimum flow speeds from burner ports which may be permitted are known to be very close together when air-gas mixtures in theoretical proportions are being supplied to the burner. As the air-gas ratio is lowered, and the mixture becomes more *gas rich*, the limiting speeds become farther apart, until with 100 per cent gas, in an all-yellow flame, flash back cannot occur and a much higher velocity is needed to blow off the flames.

SOOT

The deposit of soot on the flue surfaces of a boiler or heater acts as an insulating layer over the surface and reduces the heat transmission to the water or air. The *Bureau of Mines Report of Investigations* No. 3272 [5] shows that the loss of seasonal efficiency is not so great as has been believed and usually is not over 6 per cent because the greater part of the heat is transmitted through the combustion chamber surfaces. The *Bureau of Standards Report* BMS 54 [6] points out that, although the decrease in efficiency of an oil fired boiler due to soot deposits is relatively small, the attendant increase in stack temperature may be considerable.

The soot accumulation clogs the flues, reduces the draft, and may prevent proper combustion. Soot can probably be most effectively removed by a jet of compressed air or by means of a brush. However, it has been found that copper chloride, lead chloride, tin chloride, zinc chloride, common salt and some other salts are partially effective in removing soot from furnaces and boilers when properly used. [7]

CONDENSATION AND CORROSION

Sulfur dioxide or sulfur trioxide formed by the combustion of sulfur in fuels is the principal corroding element in flue gases, and becomes active whenever moisture is present for the formation of sulfurous or sulfuric acid. It is necessary, therefore, to maintain a flue gas temperature in excess of the dew-point temperature of the flue gases in all parts of

TABLE 10. AVERAGE FLUE GAS DEW-POINT FOR VARIOUS FUELS[8]

TYPE OF FUEL	AVERAGE DEW-POINT TEMPERATURE, F
Anthracite	68
Semi-Bituminous Coal	84
Bituminous Coal	93
Oil	111
Natural Gas	127
Manufactured Gas	137

appliances unless they are made of materials that will resist these corrosive influences. It is usually desirable to maintain a flue gas temperature above the dew-point temperature throughout the heating appliance and the chimney or smokestack because of these same corrosive effects. The average dew-point temperatures of the flue gases from the several fuels, when burned with the amount of excess air usually supplied to insure complete combustion, are shown in Table 10.

LETTER SYMBOLS USED IN CHAPTER 16

h_1 = heat loss in the dry chimney gases, Btu per pound of fuel.
h_2 = heat loss in water vapor from combustion of hydrogen, Btu per pound of fuel.
h_3 = heat loss in water vapor in combustion air, Btu per pound of fuel.
h_4 = heat loss from incomplete combustion of carbon, Btu per pound of fuel.
h_5 = heat loss from unburned carbon in the ash, Btu per pound of fuel.
w_g = weight of dry flue gas per pound of fuel (from Equation 6), pounds.
c_p = mean specific heat of flue gases at constant pressure.
t_g = temperature of flue gases at exit of heating device, Fahrenheit degrees.
t_a = temperature of combustion air, Fahrenheit degrees.
H_2 = percentage of hydrogen in the fuel by weight from ultimate analysis of fuel as fired.
M = humidity ratio of combustion air, pounds of water vapor per pound of dry air.
w_a = weight of combustion air per pound of fuel used, pounds.
C = weight of carbon burned per pound of fuel corrected for carbon in ash, pounds.
C_u = percentage of carbon in the fuel by weight from the ultimate analysis.
CO, CO_2 = percentages of CO, CO_2 in the flue gases by volume.
W_a = weight of ash and refuse, pounds.
C_a = per cent of combustibles in ash and refuse by weight.
W = weight of fuel used, pounds.

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Chapter 17

AUTOMATIC FUEL BURNING EQUIPMENT

Classification of Stokers, Combustion Process and Adjustments, Furnace Design, Classification of Oil Burners, Combustion Chamber Design, Classification of Gas-Fired Appliances, Combustion Process, Ratings, Fuel Burning Rates

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AUTOMATIC mechanical equipment for the combustion of solid, liquid, and gaseous fuels is considered in this chapter.

MECHANICAL STOKERS

A mechanical stoker is a device that feeds a solid fuel into a combustion chamber, provides a supply of air for burning the fuel under automatic control and, in some cases, incorporates a means of removing the ash and refuse of combustion automatically. Coal can be burned more efficiently by a mechanical stoker than by hand firing because the stoker provides a uniform rate of fuel feed, better distribution in the fuel bed and positive control of the air supplied for combustion.

CLASSIFICATION OF STOKERS ACCORDING TO CAPACITY

Stokers may be classified according to their coal feeding rates. The following classification has been made by the *U. S. Department of Commerce*, in cooperation with the *Stoker Manufacturers Association.*

Class 1. Capacity under 61 lb of coal per hour.
Class 2. Capacity 61 to 100 lb of coal per hour.
Class 3. Capacity 101 to 300 lb of coal per hour.
Class 4. Capacity 300 to 1200 lb of coal per hour.
Class 5. Capacity 1200 lb of coal per hour and over.

Class 1 Stokers

These stokers are used primarily for home heating and are designed for quiet, automatic operation. Simple, trouble-free construction and attractive appearance are desirable characteristics of these small units.

A common stoker in this class (Fig. 1) consists essentially of a coal hopper, a screw for conveying the coal from the hopper to the retort, a fan which supplies the air for combustion, a transmission for driving the coal feed worm, and an electric motor for supplying power for coal feed and air supply.

Air for combustion is admitted to the fuel through tuyeres at the top of the retort which may be either round or rectangular. Stokers in this class are made for burning anthracite, bituminous, semi-bituminous, and lignite coals, and coke. The *U. S. Department of Commerce* has issued commercial standards for household anthracite stokers [1].

Units are available in either the hopper type, as shown in Fig. 1 or in the bin-feed type as shown in Figs. 2 and 3. Some stokers, particularly those designed for use with anthracite, automatically remove ash from the ash pit and deposit it in an ash receptacle as shown in Fig. 3. Most of the bituminous models, however, require removal of the ash from the fuel bed after it is fused into a clinker.

Stokers in this class feed coal to the furnace intermittently in accordance with temperature or pressure demands. A special control is used

to insure sufficient stoker operation to maintain a fire during periods when no heat is required. Where year-round domestic hot water is supplied by a boiler and indirect water heater connected to a storage tank, the stoker will usually be called on to operate often enough to maintain the fire.

Stoker-Fired Boiler and Furnace Units

Boilers, air conditioners, and space heaters especially designed for stokers are available having design features closely coordinating the heat absorber and the stoker. Although efficient and satisfactory performance can be obtained from the application of stokers to existing boilers and furnaces, some of the combination stoker-fired units (Fig. 4) are more compact and attractive in appearance.

Class 2 and 3 Stokers

Stokers in this class are usually of the screw feed type without auxiliary plungers or other means of distributing the coal. They are used extensively for heating plants in apartments and hotels, also, for industrial

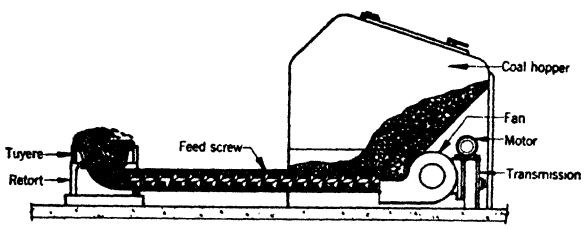

FIG. 1. UNDERFEED STOKER, HOPPER TYPE, CLASS 1

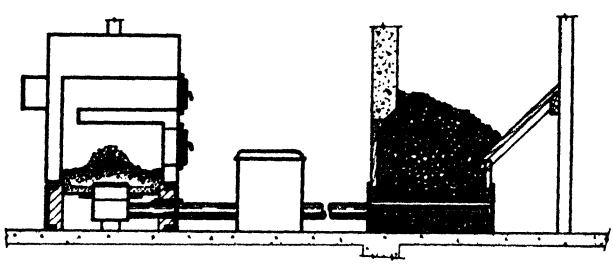

FIG. 2. UNDERFEED STOKER, BIN FEED TYPE, CLASS 1

plants. They are of the underfeed type and are available in both the hopper type, as illustrated in Fig. 5, and the bin feed type, shown in Fig. 6. These units also are built in plunger feed type with an electric motor or a steam or hydraulic cylinder coal feed drive.

Stokers in this class are available for burning all types of anthracite, bituminous and lignite coals. The tuyere and retort design varies according to the fuel and load conditions. Stationary type grates are used on bituminous models and the clinkers formed from the ash accumulate on the grates surrounding the retort.

Anthracite stokers in this class are equipped with moving grates which discharge the ash into a pit below the grate. This ash pit may be located on one or both sides of the grate and on some installations is of sufficient capacity to hold the ash for several weeks' operation.

Class 4 Stokers

Stokers in this group vary widely in details of design and several methods of feeding coal are employed. The underfeed stoker is widely used, although a number of the overfeed types are used in the larger sizes. Bin-feed, as well as hopper models, are available in both underfeed and overfeed types.

Class 5 Stokers

The prevalent stokers in this field are: (1) underfeed side cleaning, (2) underfeed rear cleaning, (3) overfeed flat grate, and (4) overfeed inclined grate.

Underfeed side cleaning stokers are made in sizes up to approximately 500 boiler horsepower. They are not so varied in design as those in the smaller classes, although the principle of operation is similar. A stoker of this type is illustrated in Fig. 7.

The rear cleaning underfeed stoker is usually of the multiple retort design and is used in some of the largest industrial plants and central power stations. Zoned air control has been applied to these stokers, both longitudinally and transversely of the grate surface.

The overfeed flat grate stoker is represented by the various chain—or traveling-grate stokers. A typical traveling-grate stoker is illustrated in Fig. 8.

Another distinct type of overfeed flat-grate stoker is the spreader (Figs. 9 and 10) type in which coal is distributed either by rotating paddles or by air over the entire grate surface. This type of stoker is adapted to a wide range of fuels and has a wide application on small sized fuels, and on fuels such as lignites, high-ash coals, and coke breeze.

The overfeed inclined-grate stoker operates on the same general combustion principle as the flat-grate stoker, the main difference being that rocking grates, set on an incline, are provided in the former to advance the fuel during combustion.

Combustion Process

In anthracite stokers of the Class 1 underfeed type, burning takes place entirely within the stoker retort. The refuse of combustion spills over the edge of the retort into an ash pit or receptacle from which it may be removed either manually or automatically.

Larger underfeed anthracite stokers operate on the same principle, except that the retort is rectangular and the refuse spills over only one or two sides of the grate. Anthracite for stoker firing is usually the No. 1 buckwheat or No. 2 buckwheat size.

Because the majority of the smaller bituminous coal stokers operate on the underfeed principle, a general description of their operation is given. When the coal is fed into the retort, it moves upward toward the zone of combustion and is heated by conduction and radiation from the burning fuel in the combustion zone. As the temperature of the coal rises, it gives off moisture and occluded gases, which are largely non-combustible. When the temperature increases to around 700 or 800 F the coal particles become plastic, the degree of plasticity varying with the type of coal.

A rapid evolution of the combustible volatile matter occurs during and directly after the plastic stage. The distillation of volatile matter continues above the plastic zone where the coal is coked. The strength and porosity of the coke formed will vary according to the size and characteristics of the coal. While some of the ash fuses into particles on the surface

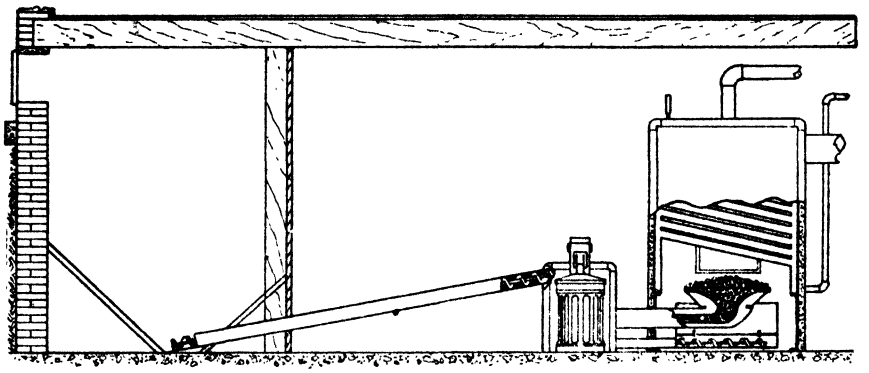

FIG. 3. UNDERFEED ANTHRACITE STOKER WITH AUTOMATIC ASH REMOVAL, BIN TYPE

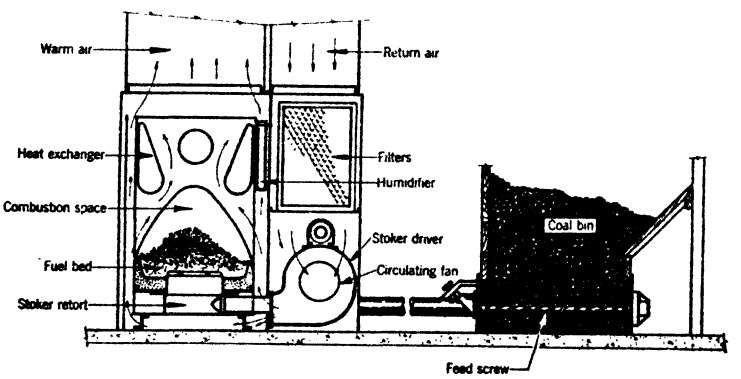

FIG. 4. STOKER-FIRED WINTER AIR CONDITIONING UNIT

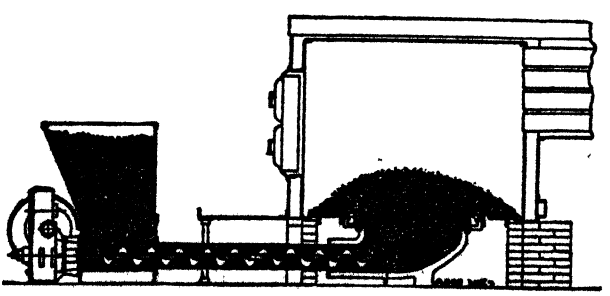

FIG. 5. UNDERFEED SCREW STOKER, HOPPER TYPE, CLASS 2, 3 OR 4

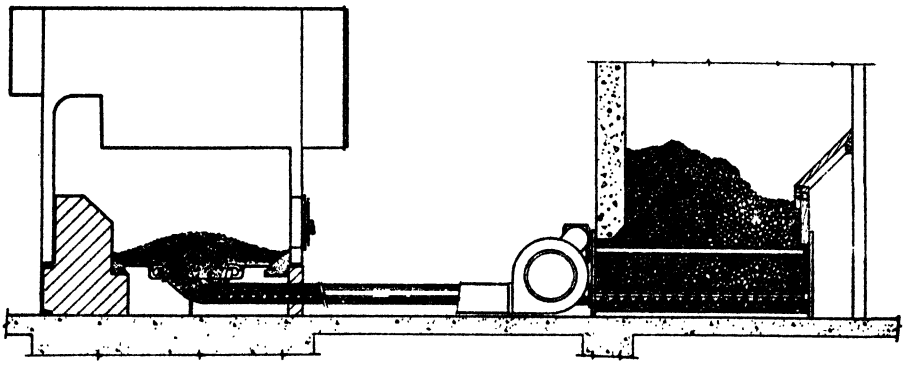

FIG. 6. UNDERFEED SCREW STOKER, BIN TYPE, CLASS 2, 3 OR 4

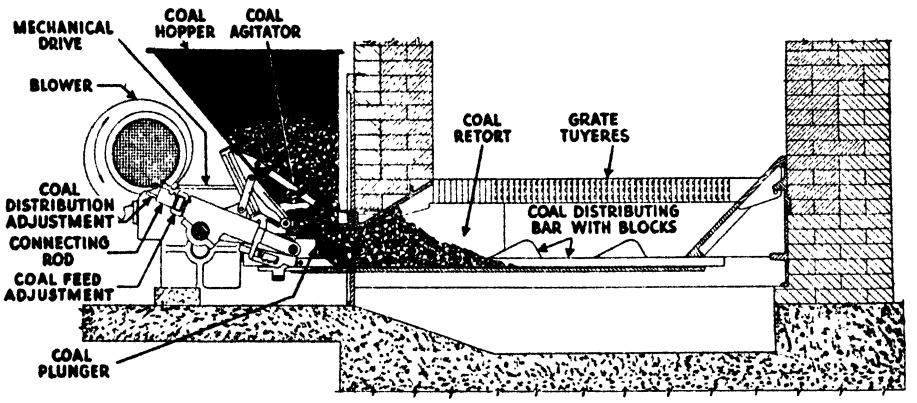

FIG. 7. UNDERFEED SIDE CLEANING STOKER

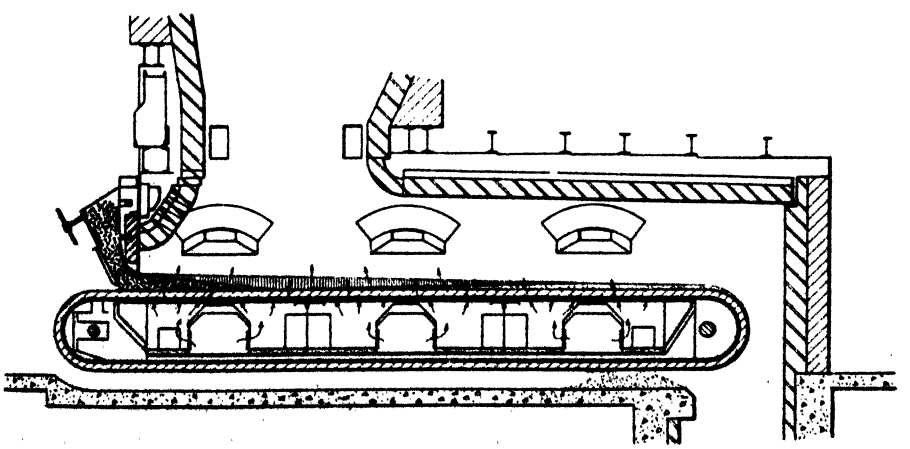

FIG. 8. OVERFEED TRAVELING-GRATE STOKER

of the coke as it is released, most of it remains on the hearth or grates and, as this ash layer becomes thicker with time, that portion exposed to the higher temperatures surrounding the retort fuses into a clinker. The temperature in the fuel bed, the chemical composition and homogeneity of the ash, and the time of heating govern the degree of fusion.

Most bituminous coal stokers of Classes 1, 2, 3 and 4 require manual removal of the ash in clinker form.

In the underfeed side-cleaning stokers the fuel is introduced at the front of the furnace to one or more retorts, and is advanced away from the retort as combustion progresses, while finally the ash is disposed of at the sides. This type of stoker is suitable for all bituminous coals while in the smaller sizes it is suitable for small sizes of anthracite. In this type of stoker the fuel is delivered to a retort beneath the fire and is raised into the fire. During this process the volatile gases are released, are mixed with air, and pass through the fire where they are burned. The ash may be continuously or periodically discharged at the sides.

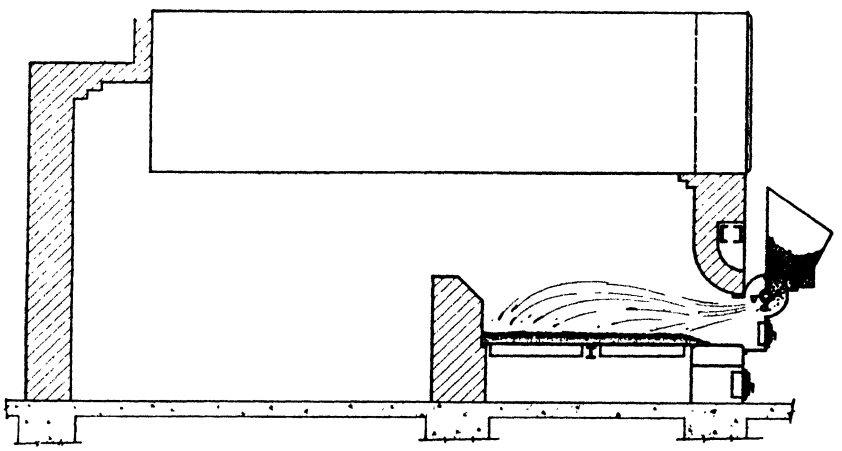

FIG. 9. OVERFEED SPREADER STOKER (ROTOR TYPE)

The underfeed rear-cleaning stoker accomplishes combustion in much the same manner as the side-cleaning type, but consists of several retorts placed side by side and filling up the furnace width, while the ash disposal is at the rear. In principle, its operation is the same as the side cleaning underfeed type.

Overfeed flat-grate stokers receive fuel at the front of the grate in a layer of uniform thickness and move it horizontally to the rear of the furnace. Air is supplied under the moving grate to carry on combustion at a sufficient rate to complete the burning of the coal near the rear of the furnace. The ash is carried over the back end of the stoker into an ash pit beneath. This type of stoker is suitable for small sizes of anthracite or coke breeze, and also for bituminous coals, the characteristics of which make it desirable to burn the fuel without disturbing it. This type of stoker requires an arch over the front of the fuel bed to maintain ignition of the incoming fuel and, frequently, a rear combustion arch.

In addition to the use of rocking grates, the overfeed inclined-grate stoker is provided with an ash plate on which ash is accumulated and

dumped periodically. This type of stoker is suitable for all types of coking fuels but preferably for those of low volatile content. Its grate action keeps the fuel bed broken up thereby allowing free passage of air. Because of its agitating effect on the fuel it is not desirable for badly clinkering coals. It usually should be provided with a front arch to ignite the volatile gases.

Combustion Adjustments

The coal feeding rate and air supply to the stoker should be regulated so as to maintain a balance between the load demand and the heat liberated by the fuel. Under such conditions no manual attention to the fuel bed should be required, other than the removal of clinker in stokers which operate on this principle of ash removal.

As in all combustion processes, the maintenance of the correct proportions of air and fuel is essential. It is desirable to supply the minimum amount of air required to properly burn the fuel at the rate of feed.

While there may be only slight variations in the rate at which the coal is being fed due to variations in the size or density of the coal, there may

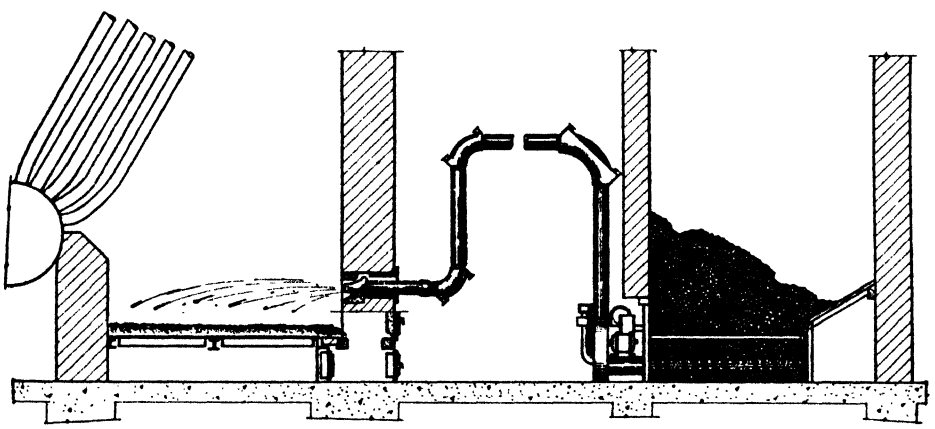

FIG. 10. OVERFEED SPREADER STOKER (PNEUMATIC TYPE)

be wide variations in the rate of air flow as the result of changes in fuel bed resistance. These changes in resistance may be caused by changes in the porosity of the fuel bed due to variations in size or friability of the coal, ash and clinker accumulation, and variations in depth of the fuel bed. Because of this variable fuel bed resistance, many bituminous stokers, even in the smaller domestic sizes, incorporate air controls which automatically compensate for these changes in resistance and maintain a constant air fuel ratio. The efficiency of combustion may be determined by analyzing the flue gases as explained in Chapters 11 and 16.

It is desirable on most stoker installations to provide automatic draft regulation in order to reduce air infiltration and provide better control during the banking, or off, periods of the stoker.

Furnace Design

Although there is considerable variation in stoker, boiler, and furnace design, the stoker industry, from long-time experience, has established certain rules for the proportioning of furnaces for domestic, and commercial stokers. The stoker installer and designer of stoker-fired equipment should give careful consideration to these factors.

The *Stoker Manufacturers Association* has published standard recommendations on setting heights for stokers having capacities up to 1200 lb of coal per hour[2].

The empirical formulas for determining these setting heights are:

For burning rates up to 100 lb coal per hour

$$H = 0.1125\ B + 15.75 \quad (1)$$

For burning rates from 100 to 1200 lb coal per hour

$$H = 0.03\ B + 24 \quad (2)$$

where

H = minimum setting height, inches, measured from dead plates to crown sheet for steel boilers. For cast-iron boilers height may be $\frac{7}{8}\ H$.

B = burning rate coal per hour, pounds.

Standards for minimum firebox dimensions and base heights have been formulated by the *Stoker Manufacturers Association* as shown in Fig. 11[2].

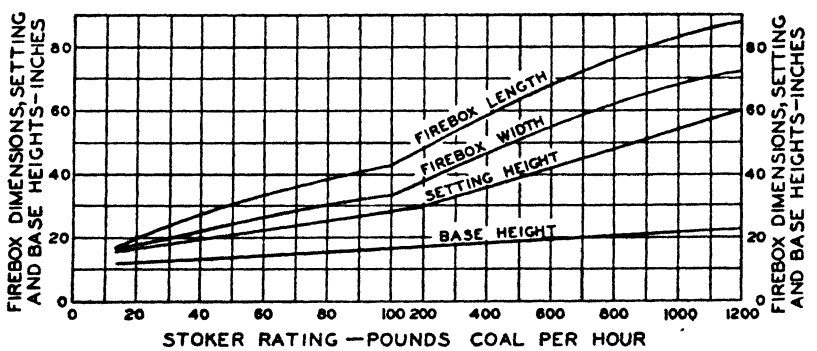

FIG. 11. SUGGESTED MINIMUM FIREBOX DIMENSIONS AND BASE HEIGHTS[a]

[a]For reference in selecting or designing boilers and furnaces for stoker firing. Dimensions shown are for net inside clearance at grate level using coal with heating value of not less than 12,000 Btu per pound. Under certain conditions smaller fireboxes will permit satisfactory performance but these dimensions are preferred normal minimums.

In considering these recommendations, it should be understood that they show the average recommended minimum. There are many factors affecting the proper application of stokers to various types of boilers and furnaces, and, in certain instances, setting height or firebox dimensions shown in the standards may be modified without impairing performance. Such modification rests with the experience of the installer, or designer, with a particular stoker, the type of fuel used, and the construction of the boiler or furnace.

Installation of stokers (particularly smaller sizes) from the side of the boiler or furnace will sometimes facilitate clinker removal.

Rating and Sizing Stokers

The capacity or rating of small underfeed stokers is usually stated as the burning rate in pounds of coal per hour. Codes for establishing uniform methods of rating anthracite and bituminous coal stokers have been adopted by the *Stoker Manufacturers Association*[3].

The Association also has adopted a uniform method of selecting stokers that is published in convenient tables and charts[2]. The required capacity of the stoker is calculated as follows:

$$\frac{\text{Load (Btu per hour)}}{\text{Heating value of coal (Btu per pound)} \times \text{over-all efficiency of stoker and boiler or furnace}} = \text{Stoker burning rate required (pounds of coal per hour)}$$

In determining the total load placed on a stoker-fired boiler by a steam or hot water heating system, a piping and pick-up factor of 1.33 is commonly used in sizing the stoker, but this factor should be increased at times due to unusual conditions.

Controls

The heat delivery from the stoker of the smallest household type to the largest industrial unit can be regulated accurately with fully automatic controls. The smaller heating applications are controlled normally by a

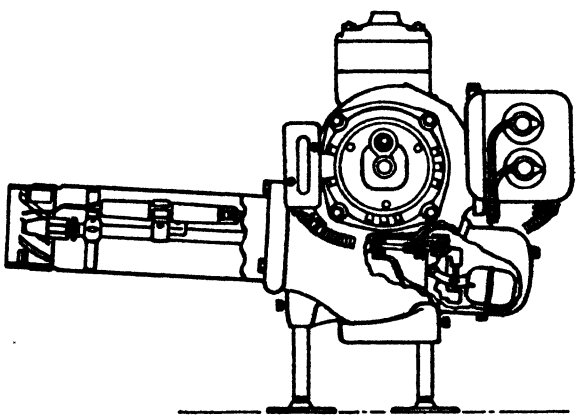

FIG. 12. LOW PRESSURE ATOMIZING OIL BURNER

thermostat placed in the building to be heated. Limit controls are supplied to prevent excessive temperature or pressure being developed in the furnace or boiler and refueling controls are used to maintain ignition during periods of low heat demand. Automatic low water cut-outs are recommended for use with all automatically-fired steam boilers. (See Chapter 34.)

DOMESTIC OIL BURNERS

An oil burner is a mechanical device for producing heat automatically from liquid fuels. Two methods are employed for the preparation of the oil for the combustion process; atomization, and vaporization. The simpler types of burners depend upon the natural chimney draft for supplying the air for combustion. Other burners provide mechanical air supply or a combination of atmospheric, and mechanical. Ignition is accomplished by an electrical spark or hot wire, or by an oil or gas pilot. Some burners utilize a combination of these methods. Continuously operating burners may use manual ignition. Burners of different types

operate with luminous or non-luminous flame. Operation may be intermittent, continuous with high-low flame, or continuous with graduated flame.

CLASSIFICATION OF BURNERS

Domestic oil burners may be classified by type of design or operation into the following groups: pressure atomizing or gun, rotary, and vaporizing or pot. These are further classified as mechanical draft, and natural draft.

Pressure Atomizing (Gun Type)

Gun type burners may be divided into two classes, low-pressure, and high-pressure atomization. In the first group, a mixture of oil and primary air is pumped as a spray through the nozzle at a pressure of 2 to 7 lb per square inch. Secondary air is supplied by a fan. Ignition is obtained by means of a high-voltage electric spark used alone, or as primary ignition for a gas pilot. Various features of a low pressure atomizing burner are shown in Fig. 12.

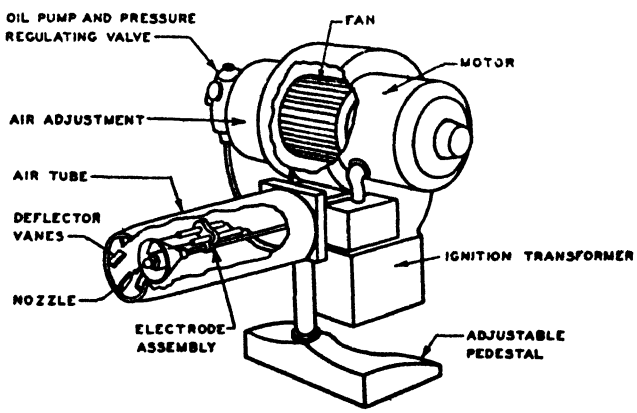

FIG. 13. HIGH-PRESSURE ATOMIZING OIL BURNER

The high-pressure atomizing type, illustrated in Fig. 13, is characterized by an air tube, usually horizontal, with oil supply pipe centrally located in the tube and arranged so that a spray of atomized oil is introduced, at about 100 lb per square inch, and mixed in the combustion chamber with the air stream emerging from the air tube. A variety of patented shapes is employed at the end of the air tube to influence the direction and speed of the air and thus the effectiveness of the mixing process.

This type of burner utilizes a fan to supply the air for combustion, and ignition is established by a high-voltage electric spark that may be operative continuously while the burner is running, or just at the beginning of the running period. Gun type burners operate on the intermittent *on-off* principle, and with a luminous flame.

The combustion process is completed in a chamber constructed of refractory material, or stainless steel, this being a part of the installation. Pressure-atomizing burners generally use the distillate oils, No. 1, 2 or 3 grade. (See Chapter 16.)

Rotary Type

This class of burners may be divided into two groups: vertical, and horizontal. Most of the smaller rotary burners are of the vertical type, and use the lighter distillate oils, No. 1 or 2 grade.

The most distinguishing feature of vertical rotary burners is the principle of flame application. These burners are of two general types: the center flame and wall flame. In the former type (Fig. 14), the oil is atomized by being thrown from the rim of a revolving disc or cup and the flame burns in suspension with a characteristic yellow color. Combustion is supported by means of a bowl-shaped chamber or hearth. The wall flame burner (Fig. 15) differs in that combustion takes place in a ring of stainless steel or refractory material, which is placed around the hearth. Dependent upon combustion adjustment, these burners may operate with either a semi-luminous or non-luminous flame.

Both types of vertical rotary burners are further characterized by their installation within the ash pit of the boiler or furnace. Various types of

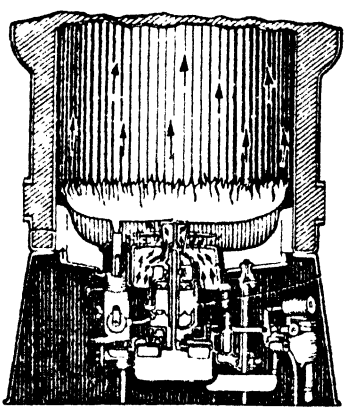

FIG. 14. CENTER FLAME VERTICAL ROTARY BURNER

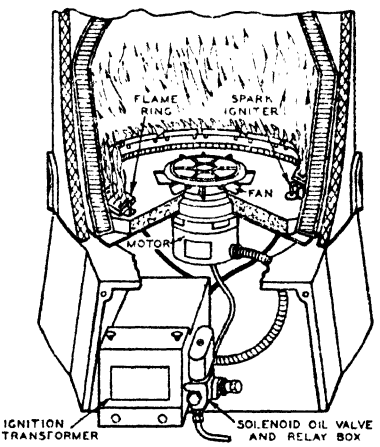

FIG. 15. WALL FLAME VERTICAL ROTARY BURNER

ignition are utilized, gas and electric, either spark or hot wire. The air for combustion is supplied partially by natural draft, and partially by fan effect of the central spinner element.

Horizontal rotary burners are used principally to burn the heavier oils, Nos. 5 and 6 grades, principally in larger commercial and industrial installations, although domestic sizes are available. Such burners are of the mechanical atomizing type, using rotating cups which throw the oil from the edge of the cup at high velocity into the surrounding stream of air delivered by the blower (Fig. 16).

Horizontal rotary burners commonly use a combination electric-gas ignition system, or are lighted manually. Primary air for combustion is supplied by a blower, and secondary air, often introduced through a checkerwork in the combustion chamber, is controlled by chimney draft. These burners operate with a luminous flame, usually on high-low or continuous setting.

In larger installations, burners may be installed in multiple in a common combustion chamber. Because of the high viscosity oils used in these

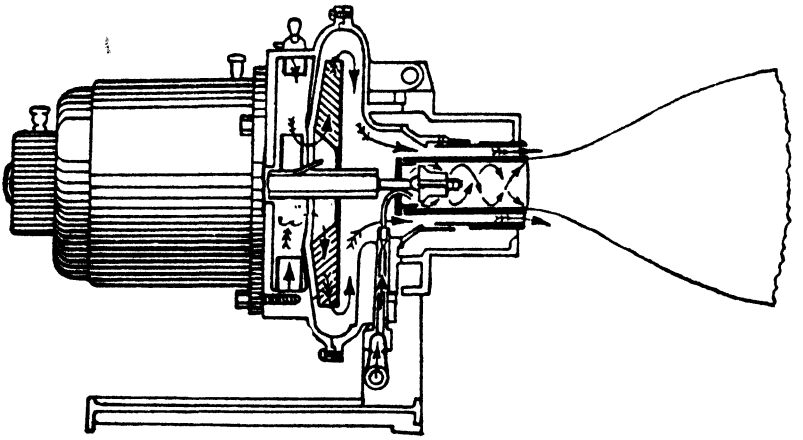

FIG. 16. HORIZONTAL ROTATING CUP OIL BURNER

burners, it is customary to preheat the oil between the tank and the burner. Preheating when delivering from tank car, or truck, is often required in cold weather.

Vaporizing Burners

This type burner transforms the oil into a combustible vapor by the application of heat from a plate, or cracking chamber. The class may be subdivided into burners supplying combustion air mechanically, and those utilizing the natural chimney draft. Vaporizing pot-type burners are generally restricted to the use of the lighter distillates but some will operate with No. 3 oil.

These burners are designed for continuous or intermittent operation, with manual ignition, and the rate of burning is controlled by a metering valve. They are also available with electric ignition and thermostatic controls. Flame may be luminous or non-luminous, dependent upon adjustment. A burner of this type is illustrated in Fig. 17.

Vaporizing burners of the natural draft type are used as the firing device in integral space heaters, water heaters, or furnace units. Some types have also been applied successfully to conversion installations.

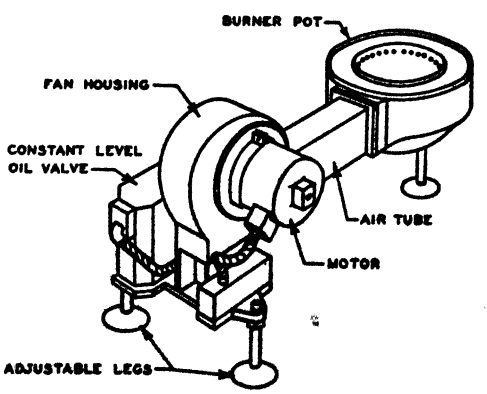

FIG. 17. VAPORIZING POT-TYPE BURNER

Oil-Fired Boiler and Furnace Units

A number of types of specially designed oil-fired boiler-burner and furnace-burner units are available. Various locations of burners will be noted in such units; some having the combustion chamber and burner at the top, some at the bottom, and some at the center of the appliance. One type of boiler-burner unit is shown in Fig. 18. The coordinated design of boiler (or furnace) and burner elements insures the optimum in operating characteristics, and the maintenance of balanced performance. This type of equipment usually has more heating surface, better flue proportions and gas travel than conventional boilers or furnaces. Some

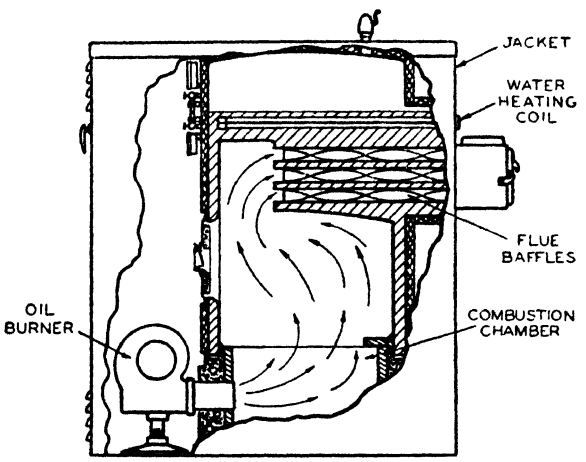

FIG. 18. TYPICAL BOILER-BURNER UNIT

of the better conversion installations, however, may equal the unit type in performance.

Operating Requirements for Mechanical Draft Oil Burners

The *U. S. Department of Commerce* in conjunction with the oil burner industry has established commercial standards for automatic mechanical draft oil burners for domestic installations which cover installation requirements and performance tests[4].

Combustion Process

Efficient combustion must produce a clean flame and use a relatively small excess of air, *i.e.*, between 25 and 50 per cent. This can be done only by vaporizing the oil quickly and completely, and mixing it vigorously with air in a combustion chamber hot enough to support the combustion. A vaporizing burner prepares the oil, for combustion, by transforming the liquid fuel to the gaseous state by the application of heat. This is accomplished before the oil vapor mixes with air to any extent and, if the air and oil vapor temperatures are high and the fire pot hot, a clear blue flame is produced.

In an atomizing burner the oil is mechanically separated into very fine particles so that the surface exposure of the liquid to the radiant heat of the combustion chamber is vastly increased and vaporization proceeds quickly. The result is the ability to burn more and heavier oil within a given combustion space. Because the air enters the combustion chamber

with the liquid fuel particles, mixing, vaporization and burning occur all at once in the same space. This produces a luminous flame. A deficient amount of air is indicated by a dull red or dark orange flame with smoky tips.

An excessive supply of air may produce a brilliant white flame or a short ragged flame with incandescent sparks flashing through the combustion space. While extreme cases may be detected, it is not possible to distinguish, by eye, the effect of the finer adjustment which competent installation requires.

Combustion Adjustments

The present-day oil burner with mechanical oil and air supply, properly installed and equipped with an automatic draft regulator, is capable of maintaining efficient combustion for a considerable period following the initial adjustments of oil and air. Eventually certain changes may occur, however, that will cause the per cent of excess air to decrease below allowable limits. A decrease in air supply while the oil delivery remains constant, or an increase in oil delivery while the air supply remains constant, will make the mixture of oil and air too rich for clean combustion. The more efficient the adjustment the more critical it will be. The oil and air supply rates must remain constant.

The following factors may influence the oil delivery rate: (1) changes in oil viscosity due to temperature change or variations in grade of oil delivered, (2) erosion of atomizing nozzle, (3) fluctuations in by-pass relief pressures, and (4) possible variations in methods of atomization. Any change due to partial stoppage of oil delivery will increase the proportion of excess air. This will result in less heat, reduced economy and possibly a complete interruption of service.

The following factors may influence the air supply: (1) changes in combustion draft due to a variety of causes (*i.e.*, changes in chimney draft because of weather changes, seasonal changes, back drafts, failure or inadequacy of automatic draft regulator, use of chimney for other purposes, possible stoppage of the chimney, and changes in draft resistance of boiler due to partial stoppage of the flues), and (2) changes in air inlet adjustments at the fan.

Air leakage into the boiler or furnace setting should be reduced to a minimum. The amount of air leakage will be determined by the draft in the combustion chamber. It is important that this draft should be reduced as low as is consistent with the proper disposal of the gases of combustion. When using mechanical draft burners with average conditions, the combustion chamber draft should not be allowed to exceed 0.02-0.05 in. water. An automatic draft regulator is very helpful in maintaining such values.

Even though a fan is generally used to supply the air for combustion, in most oil burners, the importance of a proper chimney should not be overlooked. The chimney should have sufficient height and size to insure that the draft will be uniform within the limits given if maximum efficiency throughout the heating season is to be maintained.

Measurement of the Efficiency of Combustion

Since efficient combustion is based upon a clean flame and definite proportions of oil and air employed, it is possible to determine the results by analyzing the combustion gases. It is usually sufficient to analyze only for carbon dioxide (CO_2). A showing of 10 to 12 per cent indicates

the best adjustment if the flame is clean. Most of the good installations show from 8 to 10 per cent CO_2. Taking into account the potential hazard of low excess air (high CO_2), a setting to give 10 per cent CO_2 constitutes a reasonable standard for most oil burners.

Combustion Chamber Design

With burners requiring a refractory combustion chamber the size and shape should be in accordance with the manufacturer's instructions. It is important that the chamber shall be as nearly air tight as is possible, except when the particular burner requires a secondary supply of air for combustion.

The atomizing burner is dependent upon the surrounding heated refractory or firebrick surfaces to vaporize the oil and support combustion. Unsatisfactory combustion may be due to inadequate atomization and mixing. A combustion chamber can only compensate for these things to a limited extent. If liquid fuel continually reaches some part of the firebrick surface, a carbon deposit will result. The combustion chamber should enclose a space having a shape similar to the flame but large enough to avoid flame contact. The nearest approach in practice is to have the bottom of the combustion chamber flat, but far enough below the nozzle to avoid flame contact, the sides tapering from the air tube at the same angle as the nozzle spray and the back wall rounded. A plan view of the combustion chamber resembles in shape the outline of the flame. In this way as much firebrick as possible is close to the flame so it may be kept hot. This insures quick vaporization, rapid combustion and better mixing by eliminating dead spaces in the combustion chamber. An overhanging arch at the back of the fire pot is sometimes used to increase the flame travel and give more time for mixing and burning, and sometimes to prevent the gases from going too directly into the boiler flues. When good atomization and vigorous mixing are achieved by the burner, combustion chamber design becomes a less critical matter. Where secondary air is used, combustion chamber design is quite important. When installing some of the vertical rotary burners the manufacturer's instructions must be followed carefully when installing the hearth, as in this class successful performance depends upon this factor.

Boiler Settings

As the volume of space available for combustion is a determining factor in oil consumption, it is general practice to remove grates and extend the combustion chamber downward to include or even exceed the ash pit volume; in new installations the boiler may be raised to make added volume available. Approximately 1 cu ft of combustion volume should be provided for every developed boiler horsepower, and in this volume from 1.5 to 2.5 lb of oil per hour can properly be burned. This corresponds to an average liberation of about 38,000 Btu per cubic foot per hour. At times much higher fuel rates may be satisfactory. For best results, care should be taken to keep the gas velocity below 40 fps. Where checkerwork of brick is used to provide secondary air, good practice calls for about 1 sq in. of opening for each pound of oil fired per hour. Such checkerwork is best adapted to flat flames, or to conical flames that can be spread over the floor of the combustion chamber. The proper bricking of a large or even medium sized boiler for oil firing is important and frequently it is advisable to consult an authority on this subject. The essential in combustion chamber design is to provide against flame impingement upon either metallic or firebrick surfaces. Manufacturers of

oil burners usually have available detailed plans for adapting their burners to various types of boilers, and such information should be utilized.

Controls

Controls for oil burner operation, including devices for the safety and protection of a boiler or furnace, are fully described in Chapter 34.

GAS-FIRED HEATING EQUIPMENT

A gas burner is defined by the *American Gas Association* as "a device for the final conveyance of the gas, or a mixture of gas and air, to the combustion zone." Burners used for domestic heating are of the atmospheric injection, yellow flame, or power burner types.

The use of gas has resulted in the production of a number of types of domestic gas heating appliances, and systems. These may be classified

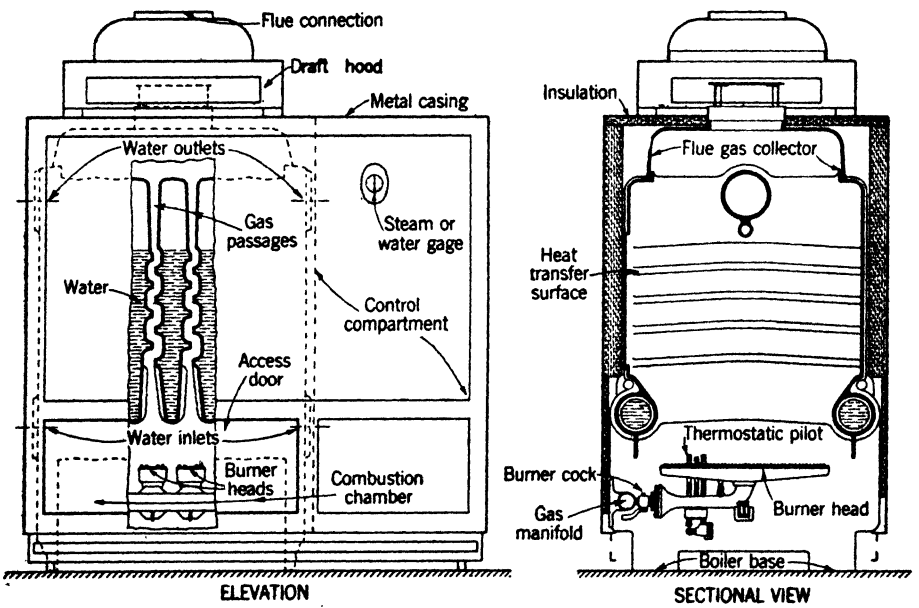

FIG. 19. GAS-FIRED BOILER

in types designed for central heating plants, and those for unit application. Gas-designed units and conversion burners are available for the several kinds of central systems. Unit heaters, space heaters and circulators may be had for installation in the space being heated.

Central Heating Systems

Boilers and furnaces specially designed for gas-firing incorporate design features for obtaining maximum efficiency and performance. Small flue passes to secure good heat transfer, the use of materials resistant to the corrosive effects of products of combustion, and draft hoods are notable features. Control equipment includes gas pressure regulators, thermostatic pilots, and limit controls designed to protect the appliance and to insure safety of operation. A boiler designed for gas-burning is illustrated in Fig. 19.

Conversion burners are usually complete burner and control units designed for installation in existing boilers and furnaces. Burner heads

are of circular or rectangular shape in order to fit in the space available. The control equipment is generally the same as for gas boilers and furnaces. Various baffles made of clay radiants or metal are used for the purpose of guiding the products of combustion along the heating surface in the firebox or flues. Automatic air dampers are supplied on many models to prevent flow of air into the firebox when the burner is not operating. A typical gas conversion burner is shown in Fig. 20.

Burners of this type are available in sizes ranging from 80,000 to 500,000 Btu per hour capacity. Burners of even larger capacity, for use with natural gas in large steel boilers, are usually engineered by the local utility or contractor. They are available in an infinite number of sizes because the burner may be an assembly of multiple burner heads filling the entire firebox.

Domestic sizes of conversion burners should be installed with due attention to the method of venting. Draft hoods, conforming to Ameri-

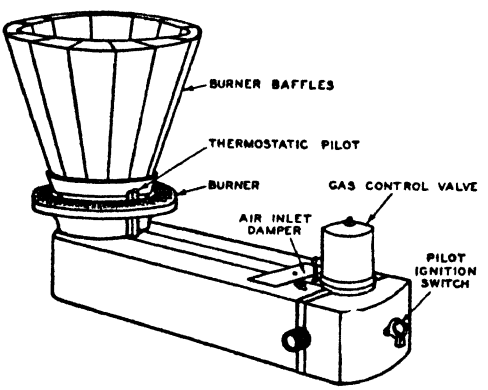

FIG. 20. TYPICAL GAS CONVERSION BURNER

can Standard Requirements, should be installed in place of the dampers used with a solid fuel.

One form of central heating system is the warm air floor furnace[5]. The use of these furnaces is adaptable to mild climates. They are used for heating first floors, or where heat is required in only one or two rooms. A number may be used to provide heat for the entire building where all rooms are on the ground floor, thus giving the heating system flexibility. With the usual type the register is installed in the floor, the heating element and gas piping being suspended below.

Unit Type Heaters

Space heaters may be used for auxiliary heating, but in many cases are installed for furnishing heat to entire buildings. With the exception of wall heaters, they are semi-portable.

Parlor heaters or *circulators* are usually of the cabinet type. They heat the room entirely by convection, *i.e.*, the cold air of the room is drawn in near the base, passes up inside the jacket around a heating section, and out of the heater at, or near, the top. These heaters cause a continuous circulation of the air in the room during the time they are in operation.

The burners are located in the base at the bottom of an enclosed combustion chamber. The products of combustion pass around baffles within the heating element, and out the flue at the back near the top. They are well adapted for residence room heating and also for stores and offices.

Radiant heaters give off a considerable portion of their heat in the form of radiant energy emitted by an incandescent refractory that is heated by a Bunsen flame. They are made in numerous shapes and designs and in sizes ranging from two to fourteen or more radiants. An atmospheric burner is supported near the center of the base. Others have a group of small atmospheric burners supported on a manifold attached to the base. Most radiant heaters are portable; however, there are also types which are encased in a jacket that fits into the wall with a grilled front.

Gas-fired steam and hot water radiators are other types of room heating appliances. They are made in a large variety of shapes and sizes and are similar in appearance to the ordinary steam or hot water radiator. A separate combustion chamber is provided in the base of each radiator and is usually fitted with a one-piece burner. They may be secured in either the vented or unvented types, and with steam pressure, thermostatic or room temperature controls.

Warm air radiators are similar in appearance to steam or hot water radiators. They are usually constructed of sheet metal hollow sections. The products of combustion circulate through the sections and are discharged from a flue or into the room, depending upon whether the radiator is of the vented or unvented type.

Unit heaters are used extensively for heating large spaces such as stores, garages, and factories. These heaters consist of a burner, heat exchanger, fan for distributing the air, draft hood, thermostatic pilot, and controls for burners and fan. They are usually mounted in an elevated position from which the heated air is directed downward by louvers. Some unit heaters are suspended from the ceiling, and others are free-standing floor units of the heat tower type.

Unit heaters are available in two types, classified according to their use, with, or without ducts. Only those types of unit heaters tested and approved as warm air furnaces can be connected safely to ducts, as they have sufficient blower capacity to deliver an adequate air supply against duct resistance and are equipped with limit controls.

Combustion Process and Adjustments

Most domestic gas burners are of the atmospheric injection (Bunsen) type in which primary air is introduced, and mixed with the gas in the throat of the mixing tube. A ratio of about 3 parts primary air to 1 part gas for manufactured gas, and a 5½ to 1 ratio for natural gas, are generally used as theoretical values. The amount of excess air required in practice depends upon several factors, notably: uniformity of air distribution and mixing, direction of gas travel from burner, and the height and temperature of combustion chamber.

Secondary air is drawn into gas appliances by natural draft. As with other fuels, excess secondary air constitutes a loss, and should be reduced to a proper minimum, which usually cannot be less than 25 to 35 per cent if the appliance is to meet *A.S.A.* approval. Yellow flame burners depend upon secondary air, alone, for combustion.

The flame produced by atmospheric injection burners is non-luminous. Air shutter adjustments for manufactured gas should be made by closing

the air shutter until yellow flame tips appear and then by opening the air shutter to a final position at which the yellow tips just disappear. This type of flame obtains ready ignition from port to port and also favors quiet flame extinction. When burning natural gas the air adjustment is generally made to secure as blue a flame as obtainable.

Little difficulty should be had in maintaining efficient combustion when burning gas. The fuel supply is normally held to close limits of variation in pressure and calorific value and the rate of heat supply is nominally constant. Because the force necessary to introduce the fuel into the combustion chamber is an inherent factor of the fuel, no draft by the chimney is required for this purpose. The use of a draft hood insures the maintenance of constant low draft condition in the combustion chamber with a resultant stability of air supply. A draft hood is also helpful in controlling the amount of excess air and preventing back drafts that might extinguish the flame. (See Chapter 16.)

Due to the use of draft hoods and gas pressure regulators both the input and combustion conditions of gas appliances are maintained quite uniform until deposits of dirt, corrosion, or scale accumulate in the air inlet openings, burner ports, or on the heating surface. Periodic cleaning is necessary to keep any gas appliance in proper operating condition.

Measurement of the Efficiency of Combustion

The efficiency of combustion may be judged from the percentage of carbon dioxide (CO_2), oxygen (O_2) and carbon monoxide (CO) in the flue gases. The CO_2 and O_2 may be obtained by means of an Orsat apparatus but the CO must be determined by more accurate equipment. It is customary to use simple indicators to determine whether CO is present and to make adjustments of the appliances to reduce the CO below 4/100 of one per cent before continuing tests in which the CO_2 and O_2 can then be found by use of the Orsat apparatus. Since the ultimate CO_2 for any gas depends on the total hydrogen content the quality of the combustion should not be judged from the value of the CO_2 in the flue gas without reference to the ultimate CO_2 obtainable. Practical values of CO_2 will usually be from 8 to 14 per cent depending on the gas used.

Ratings for Gas Appliances

Input rating for a gas appliance is established by demonstrating that the appliance can meet the Approval Requirements of the *A.S.A.* The tests are conducted at the *A.G.A. Testing Laboratories.* Output rating is determined from the approved input and an average efficiency stated in the Approval Requirements and is the heat available at the outlet.

Sizing Gas-Fired Heating Plants

Although gas-burning equipment usually is completely automatic, maintaining the temperature of rooms at a predetermined figure, there are some manually controlled installations. In order to overcome effectively the starting load and losses in piping, a manually-controlled gas boiler should have an output as much as 100 per cent greater than the equivalent standard radiation which it is expected to serve.

Boilers under thermostatic control, however, are not subject to such severe pick-up loads and consequently, it is possible to use a lower selection factor. For a gas-fired boiler or furnace under thermostatic control a factor of 20 to 25 per cent is usually sufficient for pick-up allowance.

In those installations, in mild climates where 100 per cent outside air is used, furnaces should be of larger size in order to provide adequate capacity and quick pick-up under intermittent heating conditions.

The factor to be allowed for loss of heat from piping will vary somewhat, the proportionate amount of piping installed being greater for small installations than for large ones. For selection factors to be added to installed radiation under thermostatic control see Chapter 18.

Appliances used for heating with gas should bear the approval seal of the *A.G.A. Testing Laboratories* on the manufacturer's nameplate, together with the official input and output ratings. It is not permissible to operate a gas heating unit above its stated rating. It may be necessary to operate below this rating at elevations above 3,000 ft.

Installations should be made in accordance with recommendations shown in the publications of the *American Gas Association.*

Controls

Temperature controls for gas burners are described in Chapter 34. Some central heating plants are equipped with push-button or other manual control. The main gas valve may be of either the snap action or throttling type. Automatic electric ignition is available.

FUEL BURNING RATES

The burning rate for automatic fuel burning devices is determined by the gross heat output required of the boiler, or furnace, to carry the net heating load plus allowances for system losses, and pick-up. General values for these allowances previously have been noted. Detailed information for piping and pick-up allowances for steam, and hot water systems is given in Chapter 18 and for warm air systems in Chapters 21 and 22.

When the gross output, operating efficiency, and heat value of the fuel are known, the required rate of burning can be determined by means of Figs. 21, 22 and 23 for the several fuels.

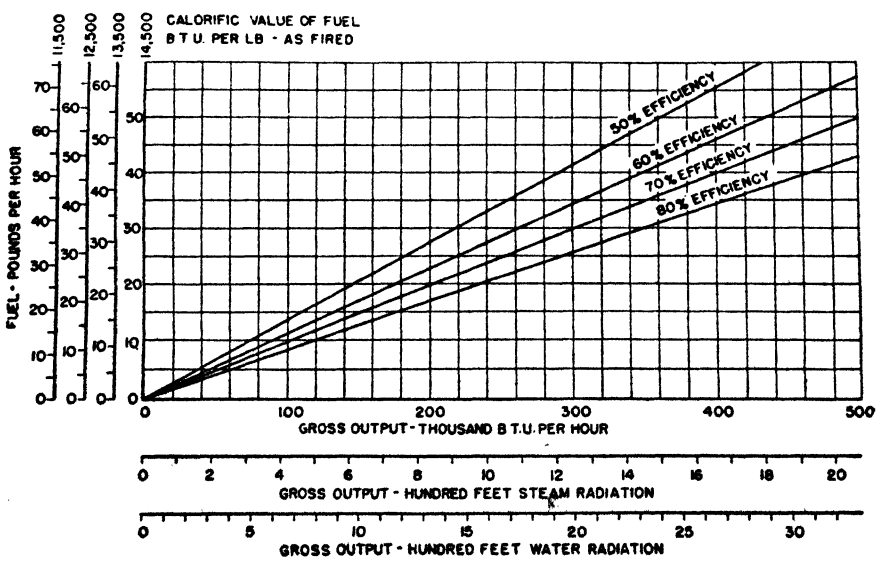

FIG. 21. COAL FUEL BURNING RATE CHART

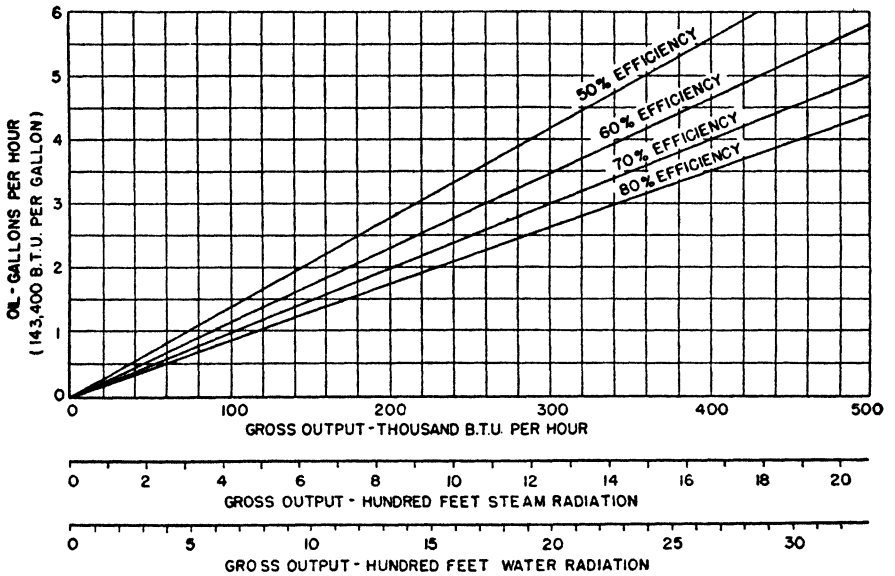

FIG. 22. OIL FUEL BURNING RATE CHART[a]

[a]This chart is based upon No. 3 oil having a heat content of 143,400 Btu per gallon. If other grades of oil are used multiply the value obtained from this chart by the following factors: No. 1 oil (139,000 Btu per gallon) 1.032; No. 2 oil (141,000 Btu per gallon) 1.017; No. 4 oil (144,500 Btu per gallon) 0.992; No. 5 oil (146,000 Btu per gallon) 0.982; and No. 6 oil (150,000 Btu per gallon) 0.956.

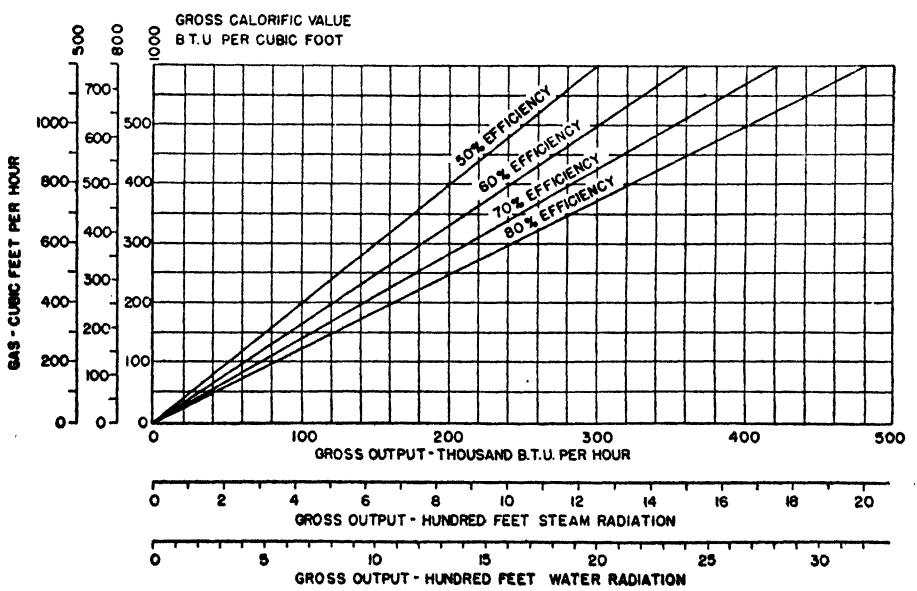

FIG. 23. GAS FUEL BURNING RATE CHART

As the rate of fuel burning is directly proportional to the load for a given efficiency, these charts can be extended by moving the decimal points the same number of digits in both vertical and horizontal scales.

The correct fuel burning rate can be determined directly from the several charts for oil or gas burning installations, as these customarily operate on a strictly intermittent basis. These fuel burning devices usually introduce the fuel at a single fixed rate during the *on* periods and this rate should be sufficient to carry the gross load. In the case of coal stokers, which are usually capable of variable rates of firing, it is desirable to operate at as low a rate as weather conditions will permit, but the maximum firing rate of the stoker should be sufficient to carry the gross load. This rate may be determined by the same method as used for oil or gas.

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Chapter 18

HEATING BOILERS AND FURNACES

BOILERS: Construction, Types, Design Considerations, Testing and Rating Codes, Efficiency, Rating, Selection, Space Limitations, Connections and Fittings, Erection, Operation and Maintenance. FURNACES: Types, Materials and Construction, Ratings, Testing and Rating Codes, Efficiency, Design Considerations, Humidification Equipment

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IN presenting the subject of Boilers and Furnaces this chapter is divided into two parts; the first dealing with boilers and the second treating warm air furnaces.

HEATING BOILERS

Steam and hot water boilers for low pressure heating are built in a wide variety of types and sizes, many of which are illustrated in the *Catalog Data Section*. They are made of steel or cast-iron.

CONSTRUCTION

The only code governing the construction of low-pressure heating steel and cast-iron boilers that has gained recognition on a national basis is the *ASME* Boiler Construction Code for Low Pressure Heating Boilers. Some states and municipalities have their own codes which apply locally but these are usually patterned after the *ASME* Code.

The maximum allowable working pressures are limited by the *ASME* Code to 15 psi for steam and 30 psi for hot water heating boilers. Hot water boilers may be used for higher working pressures, for heating purposes, or for hot water supply when designed and tested for the higher pressure.

TYPES OF HEATING BOILERS

Heating boilers are classified in a number of different ways, such as:

(*a*) According to materials of construction. These are steel and cast-iron. Very few non-ferrous boilers are made.

(*b*) According to the fuels for which the boilers are designed. These are coal, hand fired or stoker fired; oil; gas; or wood. Some boilers are designed specifically for one fuel but many boilers are designed for more than one fuel.

(*c*) According to the specific purpose or application for which the boiler is used, such as space heating or domestic hot water supply.

(*d*) According to the design or construction of the boiler such as, sectional, round, fire-tube, water-tube, magazine feed, Scotch, etc.

Cast-Iron Boilers

Cast-iron boilers are generally classified as:

(*a*) Square or rectangular boilers with vertical sections and rectangular grates commonly known as sectional boilers.

(*b*) Round boilers with horizontal pancake sections and circular grates.

Cast-iron boilers are usually shipped in sections and assembled at the place of installation. In the majority of boilers the sections are assembled with push nipples and tie rods. Many sectional boilers are provided with

large push nipples at top to permit the circulation of water between adjacent sections at both the water line and bottom of the boiler, which is necessary to enable the use of an indirect water heater with the boiler for summer-winter hot water supply. Round and sectional boilers may be increased in size by the addition of sections and corresponding plate work.

Small sectional type boilers are available with *wet-base* construction, wherein the ashpit or combustion chamber sides and bottom are surrounded by extensions of the water legs of the boiler sections and thus no separate base is required. This type of construction permits the boiler to be set directly on a wood or composition floor without danger of fire. The *wet-base* also provides some additional heating surface.

Capacities of cast-iron boilers range generally from capacities required for small residences up to about 12,000 sq ft of steam radiation. There are a few boilers made with capacities up to 18,000 sq ft of steam radiation. For larger loads, boilers must be installed in multiple.

Steel Boilers

Steel boilers may be of the fire-tube type, in which the gases of combustion pass through the tubes and the boiler water circulates around them, or of the water-tube type, in which the gases circulate around the tubes and the water passes through them.

Either the fire-tube or water-tube type may be designed with integral water jacketed furnaces or arranged for refractory lined brick or refractory lined jacketed furnaces. Those with integral water jacketed furnaces are called portable firebox boilers and are the most commonly used type. They are usually shipped in one piece, ready for piping. Refractory furnaces are usually installed in refractory lined furnace boilers after they are set in place.

Capacities of steel boilers range from those required for small residences up to about 35,000 sq ft of steam radiation.

Boilers for Special Applications

One of these is known as the *magazine feed boiler* developed for the burning of small sizes of anthracite and coke and has a large fuel carrying capacity which results in longer firing periods than would be the case with the standard types burning coal of buckwheat size. Special attention must be given to proper chimney sizes and connections when installing in order to insure adequate draft.

Boilers for *hot water supply* are classified as direct, if the water heated passes through the boiler, and as indirect, if the water heated does not come in contact with the water or steam in the boiler.

Direct heaters are built to operate at the pressures found in city supply mains and are tested at pressures from 200 to 300 lb per square inch. The life of direct heaters depends almost entirely on the scale-forming properties of the water supplied and the temperatures maintained. If low water temperatures are maintained the life of the heater will be much longer due to decreased scale formation and minimized corrosion. Direct water heaters in some cases are designed to burn refuse and garbage.

Indirect heaters generally consist of steam boilers in connection with heat exchangers of the coil or tube types which transmit the heat from the steam to the water. This type of installation has the following advantages:

1. The boiler operates at low pressure.

2. The boiler is protected from scale and corrosion.

3. The scale is formed in the heat exchanger in which the parts to which the scale is attached can be cleaned or replaced. The accumulation of scale does not affect efficiency although it will affect the capacity of the heat exchanger.

4. Discoloration of water may be prevented if the water supply comes in contact with only non-ferrous metal.

Where a steam or a forced circulation hot water heating system is installed, the domestic hot water may be heated by an indirect heater attached to the boiler. For most satisfactory performance in the steam system, this heater is placed just below the water line of the boiler. In a forced circulation hot water system, it should be located as high as possible with respect to the boiler.

BOILER DESIGN CONSIDERATIONS

Furnace Design

Good efficiency and proper boiler performance are dependent on correct furnace design. There must be sufficient volume for burning the particular fuel which is used, and means to obtain a thorough mixing of air and gases at a high temperature and at a velocity low enough to permit complete combustion of all the volatiles. For hand fired boilers, the furnace volume should be large enough to hold sufficient fuel for reasonably long firing periods. (See Chapters 16 and 17.)

Heating Surface

Boiler heating surface is that portion of the surface of the heat transfer apparatus in contact with the fluid being heated on one side and the gas or refractory being cooled on the other side. Heating surface on which the fire shines is known as *direct* or radiant surface and that in contact with hot gases only as *indirect* or convection surface. The amount of heating surface, its distribution, and the temperatures on either side thereof influence the capacity of any boiler.

Direct heating surface is more valuable than indirect per square foot because it is subjected to a higher temperature and also, in the case of solid fuel, because it is in position to receive the full radiant energy of the fuel bed.

The effectiveness of the heating surface depends on its cleanliness, its location in the boiler, and the shape of the gas passages. The area of the gas passages must not be so small as to cause excessive resistance to the flow of gases where natural draft is employed. Inserting baffles so that the heating surface is arranged in series with respect to the gas flow increases boiler efficiency and reduces stack temperature, but increases the draft loss through the boiler.

Heat Transfer Rate

Practical average over-all heat transfer rates expressed in Btu absorbed per square foot of surface per hour will average about 3300 for hand fired boilers and 4000 for mechanically fired boilers when operating at *design load*. When mechanically fired boilers are operating at *maximum load* as defined in this chapter under heading *Selection of Boilers*, these values will run between 5000 and 6000. Boilers operating under favorable conditions at these heat transfer rates will give exit gas temperatures that

are considered consistent with good practice, although there are boilers which have high efficiencies and also operate at higher transmission rates.

TESTING AND RATING CODES

The Society has adopted four solid fuel testing codes, a solid fuel rating code, and an oil fuel testing code.

ASHVE Standard and Short Form Heat Balance Codes for Testing Low-Pressure Steam Heating Solid Fuel Boilers—Codes 1 and 2—(Revision of June, 1929) [1], are intended to provide a method for conducting and reporting tests to determine heat efficiency and performance characteristics.

ASHVE Performance Test Code for Steam Heating Solid Fuel Boilers —Code No. 3—(Edition of 1929)[1] is intended for use with ASHVE Code for Rating Steam Heating Solid Fuel Hand-Fired Boilers [2]. The object of this test code is to specify the tests to be conducted and to provide a method for conducting and reporting tests to determine the efficiencies and performance of the boiler.

The ASHVE Standard Code for Testing Steam Heating Boilers Burning Oil Fuel [3], (Adopted June, 1932), is intended to provide a standard method for conducting and reporting tests to determine the heating efficiency and performance characteristics when oil fuel is used with steam heating boilers.

In 1938 the Society adopted a Standard Code for Testing Stoker-Fired Steam Heating Boilers [4], (Adopted June, 1938), which is intended to provide a test method for determining the efficiency and performance characteristics of any stoker and boiler combination burning any type of solid fuel such as anthracite or bituminous coal.

The *Steel Boiler Institute, Inc.* has adopted (June 12, 1945) a Rating Code for Commercial Steel Boilers and Residential Steel Boilers and for Testing Oil-Fired Residential Steel Boilers. The commercial boilers (defined as those having 129 to 2500 sq ft of heating surface) are rated in

TABLE 1. *SBI* NET RATING DATA FOR RESIDENTIAL STEEL BOILERS—OIL FIRED[a]

SBI NET RATING			Minimum Furnace Volume Cu Ft	Heating Surface Sq Ft
Sq Ft Steam	Sq Ft Water	Btu		
275	440	66000	2.5	16
320	510	77000	2.9	19
400	640	96000	3.6	24
550	880	132000	5.0	32
700	1120	168000	6.4	41
900	1440	216000	8.2	53
1100	1760	264000	10.0	65
1300	2080	312000	11.8	77
1500	2400	360000	13.6	88
1800	2880	432000	16.4	106
2200	3520	528000	20.0	129
2600	4160	624000	23.6	153
3000	4800	720000	27.3	177

[a]Stoker-fired and Gas-fired *SBI* Net Rating not greater than Oil-fired. Hand-fired, *SBI* Net Rating (Steam) not greater than 14 times the square feet of heating surface.

TABLE 2. *SBI* RATINGS FOR COMMERCIAL STEEL BOILERS

MECHANICALLY FIRED								HEATING SURFACE SQ FT	HAND FIRED						MINIMUM GRATE AREA SQ FT	FLOW TAPPINGS	
SBI Rating			*SBI* Net Rating			MINIMUM FURNACE VOLUME CU FT	MINIMUM FURNACE HEIGHT[a] IN.		*SBI* Rating			*SBI* Net Rating				STEAM OUTLET I.P.S. IN.	STEAM RETURN I.P.S. IN.
SQ FT STEAM	SQ FT WATER	BTU	SQ FT STEAM	SQ FT WATER	BTU				SQ FT STEAM	SQ FT WATER	BTU	SQ FT STEAM	SQ FT WATER	BTU			
2,190	3,500	526,000	1,800	2,880	432,000	15.7	26	129	1,800	2,880	432,000	1,500	2,400	360,000	7.9	6	3
2,680	4,280	643,000	2,200	3,520	528,000	19.2	28	158	2,200	3,520	528,000	1,830	2,930	439,000	8.9	6	3
3,160	5,050	758,000	2,600	4,160	624,000	22.6	29¼	186	2,600	4,160	624,000	2,170	3,470	521,000	9.7	6	3
3,650	5,840	876,000	3,000	4,800	720,000	26.1	29½	215	3,000	4,800	720,000	2,500	4,000	600,000	10.5	6	3
4,250	6,800	1,020,000	3,500	5,600	840,000	30.4	30	250	3,500	5,600	840,000	2,920	4,670	700,000	11.4	6	3
4,860	7,770	1,166,000	4,000	6,400	960,000	34.8	30½	286	4,000	6,400	960,000	3,330	5,330	800,000	12.2	6	3
5,470	8,750	1,313,000	4,500	7,200	1,080,000	39.1	31¼	322	4,500	7,200	1,080,000	3,750	6,000	900,000	13.4	6	3
6,080	9,720	1,459,000	5,000	8,000	1,200,000	43.5	31¾	358	5,000	8,000	1,200,000	4,170	6,670	1,000,000	14.5	6	3
7,290	11,660	1,750,000	6,000	9,600	1,440,000	52.1	32¾	429	6,000	9,600	1,440,000	5,000	8,000	1,200,000	16.4	8	4
8,500	13,600	2,040,000	7,000	11,200	1,680,000	60.8	34	500	7,000	11,200	1,680,000	5,830	9,330	1,400,000	18.1	8	4
10,330	16,520	2,479,000	8,500	13,600	2,040,000	73.8	35½	608	8,500	13,600	2,040,000	7,080	11,330	1,700,000	20.5	8	4
12,150	19,440	2,916,000	10,000	16,000	2,400,000	86.8	37½	715	10,000	16,000	2,400,000	8,330	13,330	2,000,000	22.5	8	4
15,180	24,280	3,643,000	12,500	20,000	3,000,000	108.5	40¼	893	12,500	20,000	3,000,000	10,420	16,700	2,500,000	25.6	8	4
18,220	29,150	4,373,000	15,000	24,000	3,600,000	130.2	43	1,072	15,000	24,000	3,600,000	12,500	20,000	3,000,000	28.4	8	4
21,250	34,000	5,100,000	17,500	28,000	4,200,000	151.8	46	1,250	17,500	28,000	4,200,000	14,580	23,330	3,500,000	30.9	8	4
24,290	38,860	5,830,000	20,000	32,000	4,800,000	173.5	48¾	1,429	20,000	32,000	4,800,000	16,670	26,670	4,000,000	33.2	8	4
30,360	48,570	7,286,000	25,000	40,000	6,000,000	216.9	54½	1,786	25,000	40,000	6,000,000	20,830	33,330	5,000,000	37.4	10	6
36,430	58,280	8,743,000	30,000	48,000	7,200,000	260.3	60½	2,143	30,000	48,000	7,200,000	25,000	40,000	6,000,000	41.2	10	6
42,500	68,000	10,200,000	35,000	56,000	8,400,000	303.6	66	2,500	35,000	56,000	8,400,000	29,170	46,670	7,000,000	44.7	10	6

[a] Bituminous Stoker Fired.

square feet (steam) on the basis of heating surface with limitations set for grate area, furnace volume, and furnace height. The residential boilers (defined as those having not more than 177 sq ft of heating surface) are rated on tests for oil-fired boilers, with limitations in relation to heating surface and testing conditions. Stoker-fired and gas-fired *residential* boilers are rated (*SBI* Net Rating) not in excess of the oil-fired rating. Hand-fired residential boilers are rated (*SBI* Net Rating) not greater than 14 times the heating surface.

Tables 1 and 2 show the *SBI* ratings of residential and commercial steel boilers respectively.

The *Institute of Boiler and Radiator Manufacturers* has adopted a Code [5] for rating cast-iron heating boilers based upon performance obtained under controlled test conditions. This Code applies to all sectional cast-iron heating boilers except those of magazine feed type.

The *Gross I=B=R* Output is obtained by test and is subject to certain limiting factors. For hand fired boilers, the number of boilers of a series to be tested, the minimum over-all efficiency, the minimum time limit (the time an *Available Fuel Charge* will last when burned at a rate which will produce the *Gross I=B=R Output*), the chimney area and height, and the draft in the stack are all subject to the limits established in the Code. Tests are run using anthracite coal of standard specification. Bituminous coal and coke ratings are the same as for anthracite coal.

For automatically fired boilers, the number of boilers of a series to be tested, the flue gas temperature and analysis, the minimum over-all efficiency, the draft loss through the boiler, and the heat release in the combustion chamber are subject to limitation by the Code [5]. Automatically fired boiler ratings are established by oil fired tests using gun type oil burners and commercial grade No. 2 fuel oil. Stoker fired and gas fired ratings (where no *A.G.A.* Rating is published) are based on the *Gross I=B=R Output* obtained by oil fired tests.

The *Net I=B=R Rating* is determined from the *Gross I=B=R Output* by applying specified *Piping and Pickup Factors* which range from 2.36 to 1.40 for hand fired boilers and from 1.56 to 1.288 for automatically fired boilers. In both cases, the factor decreases as the boiler size increases. Table 3 is abstracted from the *I=B=R Rating Tables* in the Code and illustrates the relationship between *Net I=B=R Rating* and *Gross I=B=R Output.*

The *American Gas Association* has adopted a method of rating gas designed boilers based upon performance under tests. This is described in Approval Requirements for Central Heating Gas Appliances.

The *Heating, Piping and Air Conditioning Contractors National Association* has adopted a method of rating boilers based on their physical characteristics for those boilers that are not rated in accordance with the *SBI* or *I=B=R* Codes. Ratings are expressed on a Net Load basis in square feet of steam radiation.

BOILER EFFICIENCY

The term *efficiency* as used for guarantees of boiler performance is usually construed as follows:

1. *Solid Fuels.* The efficiency of the *boiler* alone is the ratio of the heat absorbed by the water and steam in the boiler per pound of combustible burned on the grate to the calorific value of 1 lb of combustible as fired. The *combined* efficiency of *boiler, furnace*

TABLE 3. $I=B=R$ RATING TABLE

NET $I=B=R$ RATING			HAND-FIRED					AUTOMATIC-FIRED			
Sq Ft Steam	1000 Btu	Piping Factor	Piping and Pickup[a] Factor	Gross $I=B=R$ Output 1000 Btu	Time Available Fuel Will Last, Hr	Maximum Stack Height[b] Ft	Minimum Stack Area[b] Sq In.	Piping and Pickup[a] Factor	Gross $I=B=R$ Output 1000 Btu	Minimum Stack Area[b] Sq In.	Maximum Allowable Draft Loss
1	2	3	4	5	6	7	8	9	10	11	12
100	24.0	1.300	2.360	56.6	7.50	29.0	50.0	1.560	37.4	50.0	0.044
250	60.0	1.293	2.341	140.5	6.77	33.0	50.0	1.548	92.9	50.0	0.051
400	96.0	1.275	2.268	217.7	6.32	36.5	50.0	1.525	146.4	50.0	0.058
550	132.0	1.260	2.201	290.5	5.99	39.5	50.0	1.507	198.9	50.0	0 065
700	168.0	1.248	2.139	359.4	5.73	42.0	54.0	1.492	250.7	50.0	0.072
850	204.0	1.236	2.084	425.1	5.50	44.0	68.5	1.478	301.5	50.0	0.078
1000	240 0	1.225	2.039	489.4	5.32	46.0	82.0	1.466	351.8	52.0	0.084
1150	276	1.215	2.001	552	5.15	47.5	95.5	1.454	401	63.0	0.090
1300	312	1.205	1.967	614	4.99	49.0	110.0	1.444	451	73.5	0.096
1450	348	1.198	1.939	675	4.85	50.5	122.5	1.434	499	84.0	0.102
1600	384	1.190	1.914	735	4.73	52.0	135.0	1.424	547	95.0	0.108
1750	420	1.182	1.891	794	4.60	53.0	147.0	1.416	595	105.0	0.113
1900	456	1.177	1.872	854	4.49	54.5	160.0	1.408	642	115.0	0.118
2050	492	1.169	1.855	913	4.41	55.5	172.0	1.401	689	125.0	0.124
2200	528	1.162	1.837	970	4.34	56.5	185.0	1.394	736	135.0	0.130
2350	564	1.158	1.821	1027	4.29	58.0	196.0	1.388	783	145.0	0.136
2500	600	1.152	1.805	1083	4.24	59.0	207.5	1.382	829	155.0	0.141
2650	636	1.148	1.789	1138	4.19	60.0	219.0	1.376	875	165.0	0.146
2800	672	1.142	1.774	1192	4.15	61.0	231.0	1.369	920	173.5	0.152
2950	708	1.139	1.759	1245	4.11	62.0	242 0	1.364	966	183.5	0.157
3100	744	1.136	1.744	1298	4.07	63.0	253.0	1.359	1011	192.5	0.162
3250	780	1.132	1.730	1349	4.03	64.0	264.0	1.354	1056	202.5	0.167
3400	816	1.129	1.717	1401	4.00	64.5	275.0	1.349	1101	211.5	0.172
3550	852	1.128	1.704	1452	4.00	65.5	286.0	1.344	1145	221.0	0.178
3700	888	1.122	1.691	1502	4.00	66.5	296.0	1.339	1189	230.0	0.183
3850	924	1.121	1.678	1550	4.00	67.5	306.0	1.335	1234	239.5	0.188
4000	960	1.120	1.666	1599	4.00	68.0	315.0	1.331	1278	249.0	0.192
4200	1008	1.120	1.650	1663	4.00	69.0	326.0	1.325	1336	261.5	0.200
4400	1056	1.120	1.634	1726	4.00	70.0	337.0	1.320	1394	274.0	0.206
4600	1104	1.120	1.620	1788	4 00	70.5	349.0	1.314	1451	285.5	.....
4800	1152	1.120	1.605	1849	4.00	71.5	358.0	1.310	1509	297.0	.....
5000	1200	1.120	1.590	1908	4.00	72.5	367.0	1.305	1566	308.0	.....
5200	1248	1.120	1.577	1968	4.00	73.0	376.0	1.301	1624	318.5	.....
5400	1296	1.120	1.564	2027	4.00	74.0	385.0	1.297	1681	329.5	.....
5600	1344	1.120	1.552	2086	4.00	74.5	393.0	1.294	1739	339.0	.....
5800	1392	1.120	1.539	2142	4.00	75.5	402.0	1.291	1797	350.0	.....
6000	1440	1.120	1.526	2197	4.00	76.0	409.0	1.290	1858	359.0	.....
6200	1488	1.120	1.514	2253	4.00	77.0	417	1.289	1918	369	.....
6400	1536	1 120	1.502	2307	4.00	77.5	425	1.288	1978	377	.....
6600	1584	1.120	1.491	2362	4.00	78.0	431	1.288	2040	386	.....
6800	1632	1.120	1.480	2415	4.00	79.0	438	1.288	2102	395	.....
7000	1680	1.120	1.470	2470	4.00	79.5	446	1.288	2164	405	.....
7500	1800	1.120	1.447	2605	4.00	81.5	464	1.288	2318	426	.....
8000	1920	1.120	1.426	2738	4.00	83.0	481	1.288	2473	446	.....
8500	2040	1.120	1.409	2874	4.00	85.0	497	1.288	2628	467	.....
9000	2160	1.120	1.400	3024	4.00	87.0	515	1.288	2782	486	.....
9500	2280	1.120	1.400	3192	4.00	89.0	535	1.288	2937	504	.....
10000	2400	1.120	1.400	3360	4.00	91.5	555	1.288	3091	522	.....
11000	2640	1.120	1.400	3696	4.00	95.0	595	1.288	3400	560	.....
12000	2880	1.120	1.400	4032	4.00	99.0	634	1.288	3709	596	.....
13000	3120	1.120	1.400	4368	4.00	103.0	673	1.288	4019	633	.....
14000	3360	1.120	1.400	4704	4.00	106.5	712	1.288	4328	668	.....
15000	3600	1.120	1.400	5040	4.00	109.5	751	1.288	4637	704	.....
16000	3840	1.120	1.400	5376	4.00	112.5	789	1.288	4946	740	.....
17000	4080	1.120	1.400	5712	4.00	115.5	827	1.288	5255	776	.....
18000	4320	1.120	1.400	6048	4.00	118.0	863	1.288	5564	810	.....
19000	4560	1.120	1.400	6384	4.00	120.0	899	1.288	5873	844	.....
20000	4800	1.120	1.400	6720	4.00	120.0	900	1.288	6182	877	.....

[a]Includes pickup allowance and correction for difference between test and operating conditions.
[b]To be specified in catalog.

and grate is the ratio of the heat absorbed by the water and steam in the boiler per pound of fuel as fired to the calorific value of 1 lb of fuel as fired.

2. *Liquid and Gaseous Fuels.* The *combined* efficiency of boiler, furnace and burner is the ratio of the heat absorbed by the water and steam in the boiler per pound or cubic foot of fuel to the calorific value of 1 lb or cubic foot of fuel respectively.

The following efficiencies apply to current designs of boilers operated under favorable conditions at their gross output ratings. Some older boilers designed primarily for hand firing may have lower efficiencies when automatically fired.

Anthracite, hand fired	60 to 75 per cent
Bituminous Coal, hand fired	50 to 65 per cent
Stoker fired	60 to 75 per cent
Oil and Gas fired	70 to 80 per cent

Higher efficiencies for hand fired bituminous coal may be obtained by careful firing of either a regular or a smokeless boiler.

RATING OF BOILERS

In referring to boiler rating it is necessary to know the basis on which the rating has been established in order to understand the exact meaning of the term. The following example will illustrate the meaning of three ratings which might be established for the same boiler.

Assume that an installation has the following loads determined in accordance with the section *Selection of Boilers:*

Net Load	1000 sq ft of steam radiation
Piping Tax	200 sq ft of steam radiation
Design Load	1200 sq ft of steam radiation
Pickup Allowance	240 sq ft of steam radiation
Maximum or Gross Load	1440 sq ft of steam radiation

A boiler that is just large enough to carry this system might be said to have a *net load rating* of 1000 sq ft, a *design load* rating of 1200 sq ft, or a *gross load* rating of 1440 sq ft, depending on the basis on which the boiler is rated.

On a *net load* basis the boiler would be rated 1000 sq ft of steam radiation and would have sufficient excess capacity to supply the *normal piping* and *pickup load.* Net $I=B=R$ Ratings, *SBI* Net Ratings, and Net Load Ratings of the *Heating, Piping and Air Conditioning Contractors National Association* are established on this basis.

On a *design load* basis the boiler would be rated 1200 sq ft of steam radiation and would have sufficient excess capacity to supply the *pickup load.* It would be of adequate size for a system in which the *sum* of the *net load* and the *piping heat loss* did not exceed 1200 sq ft of steam radiation. The *SBI* Ratings shown in columns 1, 2, 3, 10, 11 and 12 of Table 2 (not to be confused with *SBI* Net Rating) are established on a *design load* basis.

On a *gross output* basis of rating the boiler would be rated 1440 sq ft of steam radiation and would be of adequate size for a system in which the sum of the *net load, piping load,* and *pickup load* did not exceed 1440 sq ft of steam radiation. Gross $I=B=R$ Output and *A.G.A.* Ratings are established on a *gross output* basis.

In the determination of boiler ratings, the *Gross Output* is the quantity of heat available at the boiler nozzle with the boiler normally insulated

and when operating under limitations stipulated in the code or method by which the boiler is rated. The boiler may be capable of producing a greater nozzle output but in doing so would exceed some of these limitations.

SELECTION OF BOILERS

Factors Involved in Boiler Selection

The *Maximum Load* or *Gross Load* on the boiler is the sum of the four following items.

The *Design Load* is the sum of items 1, 2, and 3.

The *Net Load* is the sum of items 1 and 2.

1. *Radiation Load.* The estimated heat emission in Btu per hour of the connected radiation (direct, indirect, or forced convection coils) to be installed.

The connected radiation is determined by calculating the heat losses for each room in accordance with data given in Chapters 6, 8, and 14. The sum of the calculated heat losses for all the rooms represents the total required heat emission of the connected radiation expressed in Btu per hour. As practically all boilers are now rated on a Btu basis, it is unnecessary to convert the radiation load to equivalent square feet of equivalent radiation.

2. *Hot Water Supply Load.* The estimated maximum heat in Btu per hour required to heat water for domestic use.

When the hot water supply is heated by the building heating boiler, this load must be taken into consideration in sizing the boiler. A common practice is to add 240 Btu per hour to the radiation load for each gallon of storage tank capacity. For more specific information see Chapter 50.

3. *Piping Tax.* The estimated heat emission in Btu per hour of the piping connecting the radiation and other apparatus to the boiler.

As the heating industry as a whole is not entirely agreed upon piping tax allowances for different sizes of installations it is better to compute the heat emission from both bare and covered pipe surface in accordance with data in Chapter 28. In average house heating systems, it is common practice to consider the piping tax to be equal to 25 per cent of the Net Load. In determining Net $I=B=R$ Ratings from Gross $I=B=R$ Output, the piping factor allowed varies from 30 per cent for small boilers to 12 per cent for larger boilers.

4. *Warming-Up or Pick-Up Allowance.* The estimated increase in the normal load in Btu per hour caused by the heating up of the cold system.

The warming-up allowance represents the load due to heating the boiler and contents to operating temperature, and heating up cold radiation and piping. The factors to be used for determining the allowance to be made should be selected from Table 4.

Other items to be considered in boiler selection are:

(*a*) Efficiency with hard or soft coal, gas, or oil firing, as the case may be.

(*b*) Grate area with hand fired coal, or fuel burning rate with stokers, oil, or gas.

(*c*) Combustion space in the furnace.

(*d*) Type of heat liberation, whether continuous or intermittent, or a combination of both.

(*e*) Convenience in firing and cleaning.

(*f*) Adaptability to changes in fuel and kind of attention.

(*g*) Height of water line.

(*h*) Miscellaneous items such as draft available, possibility of future extension, possibility of break-down, and head room in the boiler room.

(*i*) The most economical size of boiler is usually one that is just the right size for the load. Either larger or smaller boilers may be less economical.

Selection of Cast-Iron Boilers

Net load ratings of cast-iron boilers are usually available from manufacturers' catalogs. They may also be obtained conveniently from

published tables of $I=B=R$ ratings [6], or from recommendations of the *Heating, Piping and Air Conditioning Contractors National Association* [7] and can be used in selection of boilers, unless the heating system contains an unusual amount of bare pipe, or the nature of the connected load is such that the normal allowances for pipe loss and pickup do not apply. In such a case, the selection must be based on the gross output.

Selection of Steel Heating Boilers

SBI catalog ratings in accordance with the previously mentioned *Steel Boiler Institute, Inc.* code are intended to correspond with the estimated *design load.* When the heat emission of the piping is not known, the net load to be considered for the boiler may be determined from Tables 1 and 2. The difference between design load and net load represents an amount which is considered normal for piping loss of the ordinary heating system.

Boilers with less than 177 sq ft of heating surface and having *SBI* net ratings (steam) of not more than 3,000 sq ft if mechanically fired and 2,480 sq ft if hand fired, are classified as residence size. An insulated residence boiler for oil, gas, or stoker firing may carry a *net load* expressed in square feet of steam radiation of not more than 17 times the square feet of heating surface in the boiler, provided the boiler has been tested in accordance with the *SBI* Code for Testing Oil-Fired Steel Boilers at output rates of 125, 150, and 175 per cent of the *SBI* Net Rating. The *SBI* Net Rating (square feet steam) for hand-fired residence boilers is not greater than 14 times the heating surface. If the heat loss from the piping system exceeds 20 per cent of the installed radiation, the excess is to be considered as a part of the *net load.*

Selection Based on Heating Surface and Grate Area

Where neither the *net load* nor *gross output* ratings based upon performance tests are available, a good general rule for conventionally designed boilers is to provide 1 sq ft of boiler heating surface for each 14 sq ft of equivalent radiation (240 Btu per square foot) represented by the design load. This is equivalent to allowing 10 sq ft of boiler heating surface per boiler horsepower. In this case it is assumed that the *maximum load* including the warming-up allowance will be provided for by

TABLE 4. WARMING-UP ALLOWANCES FOR HAND-FIRED LOW-PRESSURE STEAM AND HOT WATER HEATING BOILERS [a,b,c]

DESIGN LOAD (REPRESENTING SUMMATION OF ITEMS 1, 2, AND 3)		PERCENTAGE CAPACITY TO ADD FOR WARMING-UP[c]
Btu per Hour	Equivalent Square Feet of Radiation[d]	
Up to 100,000	Up to 420	65
100,000 to 200,000	420 to 840	60
200,000 to 600,000	840 to 2500	55
600,000 to 1,200,000	2500 to 5000	50
1,200,000 to 1,800,000	5000 to 7500	45
Above 1,800,000	Above 7500	40

[a] This table is taken from the A.S.H.V.E. Code of Minimum Requirements for the Heating and Ventilation of Buildings, except that the second column has been added for convenience in interpreting the design load in terms of equivalent square feet of radiation.

[b] See also Time Analysis in Starting Heating Apparatus, by Ralph C. Taggart (A.S.H.V.E. TRANSACTIONS, Vol. 19, 1913, p. 292); Report of A.S.H.V.E. Continuing Committee on Codes for Testing and Rating Steam Heating Solid Fuel Boilers (A.S.H.V.E. TRANSACTIONS, Vol. 36, 1930, p. 35); Selecting the Right Size Heating Boiler, by Sabin Crocker (*Heating, Piping and Air Conditioning*, March, 1932).

[c] This table refers to *hand-fired, solid fuel boilers.* A factor of 20 per cent over design load is adequate when *automatically-fired fuels* are used.

[d] 240 Btu per square foot.

operating the boiler in excess of the *design load*, that is, in excess of the 100 per cent rating on a boiler-horsepower basis. *SBI* ratings for hand firing are based on 10 sq ft of heating surface per boiler horsepower.

Due to the wide variation which may be encountered in manufacturers' ratings for boilers of approximately the same capacity, it is advisable to check the grate area required for heating boilers burning solid fuel by means of the following formula:

$$G = \frac{H}{C \times F \times E} \tag{1}$$

where

G = grate area, square feet.
H = required *gross output* of the boiler, Btu per hour (see Selection of Boilers).
C = desirable combustion rate for fuel selected, pounds of dry coal per square foot of grate per hour (see Table 5).
F = calorific value of fuel, Btu per pound.
E = efficiency of boiler, usually taken as 0.60.

Example 1. Determine the grate area for a required *gross output* of the boiler of 500,000 Btu per hour, a combustion rate of 6 lb per hour, a calorific value of 13,000 Btu per pound, and an efficiency of 60 per cent.

$$G = \frac{500{,}000}{6 \times 13{,}000 \times 0.60} = 10.7 \text{ sq ft}$$

The boiler selected should have a grate area not less than that determined by Equation 1. With small boilers, where it is desired to provide sufficient coal capacity for approximately an eight-hour firing period plus a 20 per cent reserve for igniting a new charge, more grate area may be required depending upon the depth of the fuel pot.

TABLE 5. PRACTICAL COMBUSTION RATES FOR COAL-FIRED HEATING BOILERS OPERATING AT MAXIMUM LOAD ON NATURAL DRAFT OF FROM ⅛ IN. TO ½ IN. WATER[a]

KIND OF COAL	SQ FT GRATE	LB OF COAL PER SQ FT GRATE PER HOUR
No. 1 Buckwheat Anthracite	Up to 4	3
	5 to 9	3½
	10 to 14	4
	15 to 19	4½
	20 to 25	5
Anthracite Pea	Up to 9	5
	10 to 19	5½
	20 to 25	6
Anthracite Nut and Larger	Up to 4	8
	5 to 9	9
	10 to 14	10
	15 to 19	11
	20 to 25	13
Bituminous	Up to 4	9.5
	5 to 14	12
	15 and above	15.5

[a]Steel boilers usually have higher combustion rates for grate areas exceeding 15 sq ft than those indicated in this table.

Selection of Gas-Fired Boilers

After determining the *net load* for the installation, gas designed boilers can usually be selected from manufacturers' tables of *net load ratings* which are based on piping and pickup allowances varying from 56 per cent for boilers of 200 sq ft and less to 35 per cent for boilers of 4000 sq ft and larger. If the piping and pickup load or other factors create an unusual load, a boiler should be selected which has an *A.G.A. output rating* equal to the maximum output required. Detailed recommendations for selection of gas designed boilers are given in the *A.G.A.* publication, Comfort Heating[8].

SPACE LIMITATIONS

Boiler rooms should, if possible, be situated at a central point with respect to the building and should be designed for a maximum of natural light. The space in front of the boilers should be sufficient for firing, stoking, ash removal and cleaning or renewal of flue tubes, and should be at least 3 ft greater than the length of the tubes.

A space of at least 3 ft should be allowed on at least one side of every boiler for convenience of erection and for accessibility to the various dampers, cleanouts, and trimmings. The space at the rear of the boiler should be ample for the chimney connection and for cleanouts. With large boilers the rear clearance should be at least 3 ft in width.

The boiler room height should be sufficient for the location of boiler accessories and for proper installation of piping. In general the ceiling height for small steam boilers should be at least 3 ft above the normal boiler water line. With vapor heating, especially, the height above the boiler water line is of vital importance.

When steel boilers are used, space should be provided for the removal and replacement of tubes.

CONNECTIONS AND FITTINGS

Steam outlet connections should be the full size of the manufacturers' tappings in order to keep the velocity of flow through the outlet reasonably low and to avoid fluctuation of the water line and undue entrainment of moisture, and should extend vertically to the maximum height available above the boiler. A steam velocity in boiler outlets not exceeding 25 to 30 fps at maximum load is recommended unless data are available to show that a higher velocity is satisfactory.

Particular attention should be given to *fitting connections* to secure conformity with the *ASME* Boiler Construction Code for Low Pressure Heating Boilers. Attention is called in particular to pressure gage piping, water gage connections, and safety valve capacity.

Where a *return header* is used on a cast-iron sectional boiler to distribute the returns to both rear tappings, it is advisable to provide full size plugged tees instead of elbows where the branch connections enter the return tappings. This facilitates cleaning sludge from the bottom of the boiler sections through the large plugged openings. An equivalent cleanout plug should be provided in the case of a single return connection.

Blow-off or drain connections should be made near the boiler and so arranged that the entire system may be drained of water by opening the

drain cock. In the case of two or more boilers separate blow-off connections must be provided for each boiler on the boiler side of the stop valve on the main return connection.

Water service connections must be provided for both steam and water boilers, for refilling and for the addition of make-up water to boilers. This connection is usually of galvanized steel pipe, and is made to the return main near the boiler or boilers.

For further data on pipe connections for steam and hot water heating systems, see Chapter 23 and 24 and the *ASME* Boiler Construction Code for Low Pressure Heating Boilers.

Smoke Breeching and Chimney Connections. The breeching or smoke pipe from the boiler outlet to the chimney should be air-tight and as short and direct as possible, preference being given to long radius and 45-deg instead of 90-deg bends. The breeching entering a brick chimney should not project beyond the flue lining and where practicable it should be grouted from the inside of the chimney. A thimble or sleeve usually is provided where the breeching enters a brick chimney.

Where a battery of boilers is connected into a breeching each boiler should be provided with a tight damper. The breeching for a battery of boilers should not be reduced in size as it goes to the more remote boilers. Good connections made to a good chimney will usually result in a rapid response by the boilers to demands for heat.

ERECTION, OPERATION, AND MAINTENANCE

The directions of the boiler manufacturer should always be read before the assembly or installation of any boiler is started, even though the contractor may be familiar with the boiler. All joints requiring boiler putty or cement which cannot be reached after assembly is complete must be finished as the assembly progresses.

Five precautions that should be taken in all installations to prevent damage to the boiler are:

1. There should be provided proper and convenient drainage connections for use if the boiler is not in operation during freezing weather.

2. Strains on the boiler due to movement of piping during expansion should be prevented by suitable anchoring of piping and by proper provision for pipe expansion and contraction.

3. Direct impingement of too intense local heat upon any part of the boiler surface, as with oil burners, should be avoided by protecting the surface with firebrick or other refractory material.

4. Condensation in steam systems must flow back to the boiler as rapidly and uniformly as possible. Return connections should prevent the water from backing out of the boiler.

5. Automatic boiler feeders and low water cut-off devices which shut off the source of heat if the water in the boiler falls below a safe level are recommended for mechanically fired boilers.

Boiler Troubles

A complaint regarding boiler operation generally will be found to be due to one of the following:

1. *The boiler fails to deliver enough heat.* The cause of this condition may be: (*a*) poor draft; (*b*) poor fuel; (*c*) inferior attention or firing; (*d*) boiler too small; (*e*) improper piping; (*f*) improper arrangement of sections; (*g*) heating surfaces covered with soot;

(*h*) insufficient radiation installed; and (*i*) with mechanical firing, fuel burning equipment too small.

2. *The water line is unsteady.* The cause of this condition may be: (*a*) grease and dirt in boiler; (*b*) water column connected to a very active section and, therefore, not showing actual water level in boiler; and (*c*) boiler operating at excessive output.

3. *Water disappears from gage glass.* This may be caused by: (*a*) priming due to grease and dirt in boiler; (*b*) too great pressure difference between supply and return piping preventing return of condensation; (*c*) valve closed in return line; (*d*) connection of bottom of water column into a very active section or thin waterway; and (*e*) improper connections between boilers in battery permitting boiler with excess pressure to push returning condensation into boiler with lower pressure.

4. *Water is carried over into steam main.* This may be caused by: (*a*) grease and dirt in boiler; (*b*) insufficient steam dome or too small steam liberating area; (*c*) outlet connections of too small area; (*d*) excessive rate of output; and (*e*) water level carried higher than specified.

5. *Boiler is slow in response to operation of dampers.* This may be due to: (*a*) poor draft resulting from air leaks into chimney or breeching; (*b*) inferior fuel; (*c*) inferior attention; (*d*) accumulation of clinker on grate; and (*e*) boiler too small for the load.

6. *Boiler requires too frequent cleaning of flues.* This may be due to: (*a*) poor draft; (*b*) smoky combustion; (*c*) too low a rate of combustion; and (*d*) too much excess air in firebox causing chilling of gases.

7. *Boiler smokes through fire door.* This may be due to: (*a*) defective draft in chimney or incorrect setting of dampers; (*b*) air leaks into boiler or breeching; (*c*) gas outlet from firebox plugged with fuel; (*d*) dirty or clogged flues; and (*e*) improper reduction in breeching size.

8. *Low carbon dioxide.* This may be due on oil burning boilers to: (*a*) improper adjustment of the burner; (*b*) leakage through the boiler setting; (*c*) improper fire caused by a fouled nozzle; or (*d*) to an insufficient quantity of oil being burned.

Cleaning Boilers

All boilers are provided with flue clean-out openings through which the heating surface can be reached by means of brushes or scrapers. Flues of solid fuel boilers should be cleaned often to keep the surfaces free of soot or ash. Gas boiler flues and burners should be cleaned at least once a year. Oil burning boiler flues should be examined periodically to determine when cleaning is necessary.

The grease used to lubricate the cutting tools during erection of new piping systems serves as a carrier for sand and dirt, with the result that a scum of fine particles and grease accumulates on the surface of the water in all new boilers, while heavier particles may settle to the bottom of the boiler and form sludge. These impurities tend to cause foaming, preventing the generation of steam and causing an unsteady water line.

This unavoidable accumulation of oil and grease should be removed by blowing off the boiler as follows: If not already provided, install a surface blow connection of at least 1¼ in. nominal pipe size with outlet extended to within 18 in. of the floor or to sewer, inserting a valve in line close to boiler. Bring the water line to center of outlet, raise steam pressure, and while fire is burning briskly open valve in blow-off line. When pressure recedes, close valve and repeat process adding water at intervals to maintain proper level. As a final operation bring the pressure in the boiler to about 10 lb, close blow-off, draw the fire or stop burner, and open drain valve. After boiler has cooled partly, fill and flush out several times before filling it to proper water level for normal service. The use of soda, or any alkali, vinegar or any acid is not recommended for cleaning heating boilers because of the difficulty of complete removal and the possibility of subsequent injury, after the cleaning process has been completed.

Insoluble compounds have been developed which are effective, but special instructions on the proper cleaning compound and directions for its use, as given by the boiler manufacturer, should be carefully followed.

Care of Idle Heating Boilers

Heating boilers are often seriously damaged during summer months due chiefly to corrosion resulting from the combination of sulfur in the soot with the moisture in the cellar air. At the end of the heating season the following precautions should be taken:

1. All heating surfaces should be cleaned thoroughly of soot, ash and residue, and the heating surfaces of steel boilers should be given a coating of lubricating oil on the fire side.

2. All machined surfaces should be coated with oil or grease.

3. Connections to the chimney should be cleaned and in case of small boilers the pipe should be placed in a dry place after cleaning.

4. If there is much moisture in the boiler room, it is desirable to drain the boiler to prevent atmospheric condensation on the heating surfaces of the boiler when they are below the dew-point temperature. Due to the hazard that some one may inadvertently build a fire in a dry boiler, however, it is safer to keep the boiler filled with water, particularly in residential installations. Air can be excluded from a steam boiler by raising the water level into the steam outlets. A hot water system usually is left filled to the expansion tank.

5. The grates and ashpit should be cleaned.

6. Clean and repack the gage glass if necessary.

7. Remove any rust or other deposit from exposed surfaces by scraping with a wire brush or sandpaper. After boiler is thoroughly cleaned, apply a coat of preservative paint where required to external parts normally painted.

8. Inspect all accessories of the boiler carefully to see that they are in good working order. In this connection, oil all door hinges, damper bearings, and regulator parts.

WARM AIR FURNACES

Warm air heating furnaces of a number of types and a wide range of sizes are listed and illustrated in the *Catalog Data Section.*

TYPES OF FURNACES

Warm air furnaces may be classified in several different ways:

a. According to method of heat distribution—these are either gravity or mechanical (blower) furnaces.

b. According to fuels for which the furnaces are designed—these are coal hand-fired or stoker-fired, oil, gas, or wood.

c. According to materials of construction—they are cast-iron, low carbon steel, and occasionally high temperature steel alloys.

d. According to design or construction, such as drum and radiator, tubular, horizontal, etc.

Gravity Warm Air Furnaces

A gravity furnace is one in which the motive head producing air flow depends upon the difference in density between the heated air leaving the top of the casing and the cooled air entering the bottom of the casing. Since this gravity head is relatively low, the furnace must have low internal resistance to the flow of air and relatively large areas must be available for free circulation within the furnace casing. It is common practice to provide approximately 50 per cent free air area through gravity type furnaces.

Furnaces for gravity type systems are available in designs suitable for central heating, pipeless furnace, or unit floor furnace installations. Booster fans are sometimes used in conjunction with gravity design

systems, to increase air circulation. Where a fan is to be used with a furnace casing sized for gravity air flow, some form of baffling must be employed to restrict the free area within the casing and to force impingement of the air against the heating surfaces. Where square casings are used, the corners must be baffled.

Mechanical Warm Air Furnaces

Mechanical or forced warm air furnaces include fans or blowers as integral parts for the purpose of circulating the air and usually include air filters.

Fans and Motors

Centrifugal fans with either backward or forward curved blades are the type most commonly used. Motors may be mounted on the fan shaft or connected to the fan by a belt drive. Adjustable pulleys are desirable to provide means of regulating the quantity of air distributed to the heated spaces. Either the motor load or the noise may limit the maximum operating fan speed. Two-speed motors have given successful operating results and are recommended. Motors and mountings must be carefully selected for quiet operation. Electrical conduit and water piping must not be fastened to, nor make contact with the fan housing.

Filters

Several types of filters are available for mechanical warm air furnace applications and are discussed in Chapter 33. For maximum efficiency and life under operating conditions, filters should not be subjected to a temperature in excess of 150 F. Filters should have at least 80 per cent average efficiency on an 8-hr test at a maximum resistance of 0.25 in. of water. Filter resistance rises rapidly with the accumulation of dirt, and may reduce the air circulation over heating surfaces. In domestic furnaces, the maximum velocity, based on nominal filter area, should not exceed 300 fpm.

Fuel Utilization

A combustion rate of from 5 to 8 lb of coal per (square foot of grate) (hour) is recommended for residential furnaces. A higher combustion rate is permissible with larger furnaces for buildings other than residences, depending upon the ratio of grate surface to heating surface, firing period, and available draft.

In residential furnaces for coal burning, the ratio of heating surface to grate area will average about 20 to 1; in commercial sizes the ratio may be as high as 50 to 1, depending on fuel and draft. Furnaces may be installed singly, each furnace with its own fan, or in batteries of a number of furnaces, using one or more fans.

Where oil fuel is used, care must be exercised in selecting the proper size and type of burner for the particular size and type of furnace used. Furnaces for burning oil fuel are usually designed for blow-through installations so that the pressure in the air space is higher than that in the combustion chamber or flues. The *National Warm Air Heating and Air Conditioning Association* has prepared a Tentative Code for Testing and Rating of Oil-Fired Furnaces. Compact fan-furnace-burner units are available, suitable for basement, closet, or even attic installations.

Gas-fired forced air furnaces should conform in construction and performance to *A.G.A.* Approval Requirements.

Heavy Duty Fan Furnaces

Fan furnaces for large commercial and industrial buildings, churches, schools, etc., are available in sizes ranging from 300,000 to 6,000,000 Btu per (hour) (unit). Heavy duty furnace heaters may be arranged in battery combinations of one or more units.

Most manufacturers of heavy duty furnaces rate their furnaces in Btu per hour and also in the number of square feet of heating surface. Conservative practice indicates that at no time in the heating-up period should the furnace surface be required to emit more than an average of 3500 Btu per square foot. A higher rate of heat emission tends to increase the heat loss up the chimney, and raise fuel consumption, to shorten the life of the furnace, and to overheat the air. The ratio of heating surface to grate area of furnaces for this type of work should never be less than 30 to 1 and as indicated previously may run as high as 50 to 1.

Control of temperature is secured through (1) controlling the quantity of heated air entering the room, (2) using mixing dampers, or (3) regulating the fuel supply.

The design of heavy duty fan furnace heating systems is in many respects similar to that of the central fan heating systems described in Chapter 43. Ducts are designed by the method outlined in Chapter 41.

MATERIALS AND CONSTRUCTION

Cast-Iron Furnaces

Cast-iron furnaces are made in a multiplicity of designs or shapes. For solid fuels they are generally of round sectional construction, the sections being cemented or bolted together. Various types of radiators for secondary convection heat transfer are employed. Such radiators are of the circular, doughnut type, or tubular type.

Cast-iron is frequently used in the construction of gas or oil-fired furnaces, designs varying considerably with two general types in common use: multi-sectional type and those with single combustion chambers having auxiliary secondary surface.

Cast-iron furnaces are made in capacities ranging from those for small insulated residence application with inputs of 40,000 Btu per hour or less, to capacities as large as 600,000 Btu per hour.

Cast-iron furnaces are usually constructed with a minimum sectional thickness of ¼ in. and effectively resist high temperatures and corrosion. They usually have a fairly large heat capacity because of their mass, which provides a distinct *fly wheel* or carry-over heating effect.

Steel Furnaces

Formed sheet steel construction is frequently used in furnace design. Welding, riveting, or both are used to join the formed metal. The use of steel castings, however, is rare, because of the cost, and because high stresses are not encountered in normal furnace construction. Types of design employed vary greatly, although perhaps the most common type consists of a drum and circumferential or rear radiator. Steel gas furnaces may also be sectional in design or may be combinations of common combustion chambers and sectional or tubular radiation surfaces connected to a flue gas collector.

Steel furnaces are made in capacities ranging from those for small insulated residence application with inputs of 40,000 Btu per hour to

capacities as large as 600,000 Btu. Steel furnaces have low heat capacities as a result of their relatively low mass and, therefore, deliver heat rapidly on demand.

RATING OF FURNACES—TESTING AND RATING CODES

Warm air furnaces are generally rated in Btu per hour output at the bonnet (point of heat generation) or at the register (point of heat delivery).

Rating Equations for Gravity Warm Air Furnaces[9]

Until a method of testing and rating gravity warm air furnaces has been developed, the following empirical rating equations are recommended by the *National Warm Air Heating and Air Conditioning Association.*

Gravity warm-air furnaces of conventional design, having ratios (of heating surface to grate area) of 15 to 1 or greater, and having a ratio of casing area to face area not less than 0.4, are rated by the following equations:

a. *Hand-fired furnaces Converted to Stoker, Gas, or Oil Firing.*

$$\text{Bonnet Capacity in Btu per hour} = 1785 \times S \times 1.333 \qquad (2)$$

b. *Hand-fired furnaces, with ratios of heating surface to grate area greater than 15 to 1 and less than 25 to 1.*

$$\text{Bonnet Capacity in Btu per hour} = 1785 \times S \times 1.333 \qquad (3)$$

c. *Hand-fired furnaces with ratios of heating surface to grate area in excess of 25 to 1.*

$$\text{Bonnet Capacity in Btu per hour} = 1785 \times 25 \times G \times 1.333 \qquad (4)$$

where

S = heating surface, in square feet.

G = actual grate area, in square feet.

The *Register Delivery Rating* is equal to 0.75 x (*Bonnet Capacity*). The *Leader Pipe Rating* in square inches, formerly used as a rating unit, may be found by dividing the *Register Delivery Rating* by 136.

Heating Surface of Furnace

Prime heating surface is defined as surface above the top of the grate having *hot gases or live fuel on one side and circulating air over the other*, and in all cases is measured on the exterior or air side. The areas of the outer casing, the inner liner, and any radiation shields shall not be considered as heating surface.

In determining the amount of heating surface, extended surfaces are considered to be prime heating surface subject to the following limitations:

a. Extended heating surface may consist of fins, ribs, webs, lugs, or other projections from the prime heating surface. Projections less than ¼ in. thick at the base and extending more than 1 in. from the prime surface are classified as fins.

b. Integral fins are continuously welded to, or cast as a part of, the prime heating surface. Both sides are included as heating surface, subject to the following allowances:

Distance from Prime Surface	1st inch	2nd inch	3rd inch	Over 3 in.
Ratio of Effective Area to Total Area	0.40	0.30	0.20	None

c. Non-integral fins are spot welded to, or otherwise held in line contact with the prime heating surface. Both sides are included as heating surface, subject to the following allowances:

Distance from Prime Surface	1st inch	2nd inch	3rd inch	Over 3 in.
Ratio of Effective Area to Total Area	0.30	0.20	0.15	None

d. In the case of ribs, webs, or lugs more than ¼ in. thick at the base and extending less than 1 in. from the prime surface, the entire surface in contact with circulating air is included as heating surface.

e. In the case of ribs, webs, or lugs more than ¼ in. thick at the base and extending more than 1 in. from the prime heating surface the areas of both sides of the first inch are included as prime heating surface. The portions projecting beyond 1 in. are treated as integral fins.

Grate Area

Grate area is defined and treated for purpose of rating as follows:

a. The *nominal grate area* is defined as the total cross-sectional area of the bottom of the firepot. In steel furnaces the nominal grate area is the cross-sectional area inside the firebrick lining.

b. The *actual grate area*, used for calculating the ratios of heating surface to grate area, is the nominal grate area minus certain areas that cannot be considered as part of the grate itself. The following rules govern these deductions: (1) If a solid, continuous ledge extends around the grate and inside the firepot, any area of this ledge extending inside of a circle, the diameter of which is 1 in. less than the diameter of the bottom of the firepot, shall be deducted. (2) If separate, solid projections extend from the firepot towards the grate, the areas of any portions of these projections extending inside of a circle, the diameter of which is 3 in. less than the diameter of the bottom of the firepot, shall be deducted. (3) In the case of grates which are inclined, or are conical, the projected area is the same as the nominal grate area. The latter should, therefore, be used after making any necessary deductions.

Ratings for Forced Air Furnaces

For solid fuel burning, forced air furnaces having bonnet capacities between 80,000 and 250,000 Btu per hour, no standard method of test has been accepted, although eventually such codes will be developed. The *National Warm Air Heating and Air Conditioning Association* recommends empirical equations similar to Equations 2, 3, and 4 for gravity furnaces, except that a constant of 2265 is used in place of the 1785.

The following testing and rating codes have been generally accepted in the industry:

Commercial Standards CS-109-44 for rating solid fuel-burning, forced-air furnaces having bonnet outputs of 80,000 Btu per hour or less. This provides a method of rating small coal-fired forced-air furnaces by test.

A Tentative Code for Testing Oil-Fired Furnaces. This code has been adopted by the *National Warm Air Heating and Air Conditioning Association* for rating oil-fired furnaces by test.

The American Gas Association method of rating gas-fired furnaces based upon performance under tests. This is described in the Approval Requirements for Central Heating Gas Appliances.

Commercial Standards 113-44 is a method of rating oil-burning floor furnaces by test.

Commercial Standard CS 104-43 is a method of rating warm air furnaces equipped with pot-type oil burners by test.

Various codes covering the construction and performance of appliances as related to fire hazards have been developed by Underwriter Laboratories, Inc. In addition, there

are many municipal codes [10] which regulate construction and installation of furnace equipment.

The Yardstick of the *National Warm Air Heating and Air Conditioning Association* provides criteria for evaluating a furnace design and installation against industry accepted standards.

FURNACE EFFICIENCY

Rating formulae of the *National Warm Air Heating and Air Conditioning Association* are based on 55 per cent efficiency for gravity coal furnaces and 65 per cent efficiency for forced air coal furnaces. In the tentative Oil Testing Code the contemplated minimum efficiency is 70 per cent for oil fired forced air furnaces. Gravity gas furnaces approved by the *American Gas Association* are assigned a rating based on 75 per cent efficiency. All *forced air gas-fired furnaces* approved by *American Gas Association* are assigned a rating based on 80 per cent efficiency.

DESIGN CONSIDERATIONS

Considerations of prime importance in the design of warm air furnaces and some general suggestions to be observed in connection with each are as follows:

1. *Adequate heat transfer surface.*

   a. Heat transfer rates of 2,000 to 4,500 Btu per (hour) (square foot) of heating surface may be obtained without unduly high metal temperatures.

   b. Fins, pins and bosses are frequently used to add surface and to break down superficial gas films, both on gas-to-metal and metal-to-air surfaces.

   c. Surface and stack (flue gas) temperatures are good indications of the amount and effectiveness of the heating surfaces.

2. *Safe and efficient combustion of fuel.*

   a. Proper mixture of fuel and air is necessary for efficient combustion. This necessitates careful attention to the design of grates, nozzles, burners, air inlet areas and location, and combustion chamber baffling.

   b. Regulation of the quantity and the distribution of the air for combustion should be provided by use of check dampers, draft regulators, draft hoods, air shutters and air orifices.

   c. Total draft loss through appliances should not exceed that available from chimneys which would normally be obtainable in the size of building which the appliance will supply with heat.

   d. The use of ignition safety devices such as safety pilots, hold-fire controls, and the like is recommended.

3. *Fuel Capacity of Appliance.*

   a. With solid fuels adequate coal capacity should be provided for at least 5 hr of operation at the maximum rated combustion rate.

4. *Adequate circulation of air over heating surface.*

   a. In gravity furnaces, free air space between casing and heat exchanger should be great enough to permit free flow over all surfaces.

   b. Forced air furnace design must include fans having proper capacity and suitable performance characteristics. Internal static pressures must be minimized without losing the advantages of high velocity circulation over the heat exchanger surfaces.

   c. The air flow over the heating surface must be directed to obtain maximum efficiency and to eliminate hot spots and air noises.

   d. Air velocities at bonnet should not be much in excess of 1,000 fpm and air temperature distribution at the furnace outlet should be uniform within approximately ± 30 deg.

5. *Durability.*

a. A minimum metal weight for gas-fired heat exchangers is established as No. 20 U. S. Gage for plain carbon steel by the *A.G.A.* Approval Requirements for Central Heating Gas Appliances with some municipal codes specifying 18 gage. Cast-iron sectional thicknesses of ¼ in. to ⅜ in. are recommended.

b. Added strength and reinforced designs may be required to preclude damage in shipment, burning out from overfiring, or corrosion from condensation.

c. Maximum heat exchanger surface temperatures which may be used vary with the metal. The *American Gas Association* Approval Requirements for Central Heating Gas Appliances specify a maximum of 875 F for cast-iron or steel gas furnaces, and the Bureau of Standards CS 109-44 Code for Forced Air Solid Fuel-Burning Furnaces specifies 1000 F as a maximum surface temperature. These temperatures define the range in which oxidation of non-alloy ferrous metal begins. The use of proper alloy additions increases the temperature resistance properties of metals.

d. Casing temperatures should be controlled so that they do not become hazards to burn those who touch them, or to create fires.

6. *Serviceability.*

a. Those parts of the furnace which may be subject to soot, fly-ash, or condensation deposits should be accessible for cleaning.

b. Parts which may require adjustments or replacements, such as grates, baffles, liners, controls, should be removable.

c. Furnaces should be so designed that they can be installed with a minimum of difficulty.

7. *Control.*

a. Thermostatic controls of various types should be used to correlate space temperatures with unit operation.

b. Controls should be provided wherever possible, to prevent the occurrence of excessive temperatures or other conditions in any part of the unit which might cause unsafe operation.

8. *General design considerations.*

a. Furnace casings are normally constructed of formed and painted sheet steel or of galvanized iron. The casing should be protection from excessive radiation losses and temperatures by use of insulation or sheet steel air space liners. Liners should extend from the grate level to the top of the furnace and should be spaced from 1 in. to 1½ in. from the outer casing.

b. The hood or bonnet of the casing above the furnace should be as high as basement conditions will allow, to form a plenum chamber over the top of the furnace. This tends to equalize the pressure and temperature of the air leaving the bonnet through the various openings. It is generally considered advisable to take off the warm air pipes from the side of the bonnet near the top, as this method of take-off allows the use of a higher bonnet and thus provides a larger plenum chamber.

c. Warm air outlet and return air connections should be designed so that the ductwork may be easily attached. A ⅞ in. flange is normally used for this purpose.

d. Suitable provision shall be made in appliances so that the controls and humidifiers may be installed in the proper location. When these auxiliary units are installed in the ductwork, detailed instructions should be provided to insure their proper location.

e. The flue connection should be of integral flue pipe size and provision should be made to attach the flue pipe to the flue outlet of the furnace.

HUMIDIFICATION EQUIPMENT FOR FURNACES

Water evaporating pans are usually located in air which has been heated by contact with the heating surfaces. To change water into vapor capable of being carried in an air stream as part of the mixture, about

1000 Btu per pound are required. There is a trend in present practice toward heating the water in addition to heating the air. Equipment for doing this may make use of sprays, or it may take the form of water circulating coils placed within the combustion chamber and connected by pipes to the humidifier pans where a constant water level is maintained by some separate float device.

Sprays are usually controlled by solenoid valves wired in parallel with the fan motor. The water supply may, in turn, be controlled by a humidity-controlling device located in one of the living rooms, so that the washer will operate at all times when the fan is in operation, unless the relative humidity should rise beyond a desirable percentage. Sprays used in connection with commercial or heavy duty plants should be a regulation type of commercial spray. In all cases provision must be made to flush out accumulation of lime and dirt.

REFERENCES

[1]—See A.S.H.V.E. TRANSACTIONS, Vol. 35, 1929, pp. 322 and 332.

[2]—See A.S.H.V.E. TRANSACTIONS, Vol. 36, 1930, p. 42.

[3]—See A.S.H.V.E. TRANSACTIONS, Vol. 37, 1931, p. 23.

[4]—See A.S.H.V.E. TRANSACTIONS, Vol. 44, 1938, p. 366.

[5]—*I=B=R* Testing and Rating Code for Low Pressure Heating Boilers (*Institute of Boiler and Radiator Manufacturers*).

[6]—*I=B=R* Ratings for Cast-Iron Boilers (*Institute of Boiler and Radiator Manufacturers*).

[7]—Engineering Standards, Part II, Net Square Feet Radiation Loads in 70 Deg Fahr., Recommended for Low Pressure Heating Boilers, 1943 (*Heating, Piping and Air Conditioning Contractors National Association*).

[8]—Comfort Heating, 1938, pp. 35 to 39 (*American Gas Association*).

[9]—For definition of Heating Surfaces and Ratings of Wood-Burning Furnaces see Gravity Code and Manual for the Design and Installation of Gravity Warm Air Heating Systems, (*National Warm Air Heating and Air Conditioning Association*).

[10]—Recommended forms for municipal installation and fire codes are included in Volume 7—Code and Manual for the Design and Installation of Warm Air Winter Air Conditioning Systems (*National Warm Air Heating and Air Conditioning Association*).

Chapter 19

CHIMNEYS AND DRAFT CALCULATIONS

Theoretical and Available Draft, Determining Chimney Sizes, Factors Affecting Required Draft, Domestic Chimneys, Observed Test Performance, Draft Requirements of Domestic Appliances, Chimneys for Gas Heating, Construction Details, General Considerations

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A DRAFT, in the older sense, is a current of air and the draft of a furnace or boiler is that air current which flows through the fire-box and furnishes the oxygen for combustion. In engineering, however, the word *draft* has come to mean that pressure difference which causes this air current to flow and the word will be used in this sense in this chapter.

Draft is usually measured in inches of water and it is proper to speak of the draft in the fire-box or in the smoke breeching, etc., meaning the difference in pressure between the gases within and the air without those parts of a system. Draft is called positive when the pressure within such a part is less than that outside.

Draft is classified as natural and mechanical, depending on whether it is produced by a chimney or by a blower, and mechanical draft is further classified as induced or forced, depending on whether the air is drawn through or forced through the combustion chamber.

Chimneys can serve both to create a draft and to dispose of combustion products at a desirable height. For the latter purpose, chimneys, stacks, or, in the case of ships, funnels, are used in conjunction with mechanical-draft systems.

THEORETICAL DRAFT

If the air in one of two equal chimneys is heated while that in the other is not, the air in the heated chimney will be less heavy than that in the other chimney and a manometer or other pressure gage connecting the two at the bottom will indicate a pressure difference, called natural draft. The pressure of the air at the tops of the two chimneys will be equal, so that the pressure difference between them at the bottom will depend only on their height and the difference in density of the air they contain. The density of the air in either chimney is inversely proportional to its absolute temperature, so that the difference in pressure between them at the bottom will be proportional to their height and to the difference between the reciprocals of the absolute temperatures within them.

The pressure at the bottom of an unheated (and uncooled) chimney will be the same as that of the air outside, so that the unheated chimney can be dropped from the foregoing illustration. The manometer reading will be the same if its free connection is left open to the atmosphere.

These considerations in conjunction with those of barometric pressure and the difference in density of flue gases from that of air lead to the following formula:

$$D_t = 2.96\, H B_o \left(\frac{W_o}{T_o} - \frac{W_c}{T_c} \right) \qquad (1)$$

where

H = height of chimney, feet.

B_o = existing barometric pressure, inches of mercury.

W_o = density of air at 0 F and 1 atmosphere pressure, pounds per cubic foot.

W_c = density of flue gas at 0 F and 1 atmosphere pressure, pounds per cubic foot.

T_o = temperature of air surrounding the chimney, Fahrenheit degrees absolute.
T_c = average or effective temperature of the gases in the chimney, Fahrenheit degrees absolute.

The quantity D_t, yielded by the formula, is the pressure difference between the gas inside and air outside of the chimney, in inches of water, when no flow occurs in the chimney. The quantity is variously known as the theoretical draft, the static draft or the computed draft. It is very useful in predicting and analyzing chimney performance, but it is seldom if ever attained in an actual chimney because of the friction incident to gas flow, wind effects, etc.

AVAILABLE DRAFT

The available draft, D_a, *for large chimneys and stacks* has been estimated with apparent satisfaction in the past by means of formulas which in effect deduct an estimated friction loss from a theoretical draft determined as in Equation 1. The friction loss can be estimated by means of one of the formulas available for ducts, such as the Fanning equation. This procedure results in formulas for the available draft as follows:

For a *cylindrical* stack:

$$D_a = 2.96\,HB_o\left(\frac{W_o}{T_o} - \frac{W_c}{T_c}\right) - \frac{0.00126\,W^2 T_c f L}{D^5 B_o W_c} \qquad (2)$$

and for a *rectangular* stack:

$$D_a = 2.96\,HB_o\left(\frac{W_o}{T_o} - \frac{W_c}{T_c}\right) - \frac{0.000388\,W^2\,T_c f L\,(x+y)}{\overline{xy}^2\,B_o\,W_c} \qquad (3)$$

where

D_a = available draft, inches water gage.
H = height of chimney above grate, feet.
B_o = existing barometric pressure, inches of mercury.
W_o = density of air at 0 F, 1 atmosphere pressure.
W_c = density of flue gas at 0 F, 1 atmosphere pressure.
T_o = temperature of atmosphere, Fahrenheit degrees absolute.
T_c = temperature of flue gas, Fahrenheit degrees absolute.
W = flue gas flow rate, pounds per second.
f = coefficient of friction.
L = length of friction duct (= H approximately), feet.
D = minimum diameter of round chimney, feet.
x and y = length and width of cross-section of rectangular chimney, feet.

The following notes facilitate the use of Equations 2 and 3.

1. The *barometric pressure*, represented by B_o, is the actual pressure at the site of the chimney and not the pressure reduced to sea level datum.

In general, the barometric pressure decreases approximately 0.1 in. Hg per 100 ft increase in elevation.

2. The *unit weight of a cubic foot* of chimney gases at 0 F and sea level barometric pressure is given by the equation:

$$W_c = 0.131CO_2 + 0.095O_2 + 0.083N_2 \qquad (4)$$

In this equation CO_2, O_2 and N_2 represent the percentages of the parts by volume of the carbon dioxide, oxygen and nitrogen content, respectively, of the gas analysis. For ordinary operating conditions, the value of W_c may be assumed at 0.09.

The density effect on the chimney gases due to superheated water vapor resulting from moisture and hydrogen in the fuel, or due to any air infiltrations in the chimney proper is disregarded. Though water vapor content is not disclosed by Orsat analysis, its presence tends to reduce the actual weight per cubic foot of chimney gases.

3. The *atmospheric temperature* is the actual observed temperature of the outside air

at the time the analysis of the operating chimney is made. The mean atmospheric temperature in the temperate zone is approximately 62 F.

4. The *chimney gas temperature* decreases from the breeching connection to the top of the stack. This drop in temperature depends upon the material and construction of the stack, its tightness or freedom from leaks, its area, its height, and the velocity of the gases through it. The same chimney will suffer different temperature losses depending upon the capacity under which it is working and the variable atmospheric conditions. No general equation covering all these variables has been suggested, but from observations on chimneys varying in diameter from 3 to 16 ft and in height from 100 to 250 ft Equation 5 was deduced [1]:

$$T_c = \frac{3.13\, T_i \left[\left(\frac{H_b}{3} \right)^{0.96} - 1 \right]}{H_b - 3} \tag{5}$$

where

T_i = absolute temperature at the center of the connection from the breeching, Fahrenheit degrees.

H_b = the height of the stack above center line connection to breeching, feet.

5. The *coefficient of friction* between the chimney gases and a sooted surface has been taken by many workers in this field as a constant value of 0.016 for the conditions involved. This value, of course, would be less for a new unlined steel stack than for a brick or brick-lined chimney, but in time the inside surface of all chimneys regardless of the materials of construction becomes covered with a layer of soot, and thus the coefficient of friction has been taken the same for all types of chimneys and in general constant for all conditions of operation. For reasons of simplicity and convenience to the reader, this constant value of 0.016 has been employed in the development of the various special equations and charts shown in this chapter.

In important chimney design, especially when the construction or the materials are unusual, it is recommended that use be made of the Reynolds number [2] in determining the friction factor, f.

The following problem illustrates the use of Equation 2:

Example 1. Determine the available draft of a natural draft chimney 200 ft in height and 10 ft in diameter operating under the following conditions: atmospheric temperature, 62 F; chimney gas temperature, 500 F; sea level atmospheric pressure, B_o = 29.92 in. Hg; atmospheric and chimney gas density, 0.0863 and 0.09, respectively; coefficient of friction, 0.016; length of friction duct, 200 ft. The chimney discharges 100 lb of gases per second.

Substituting these values in Equation 2 and reducing:

$$D_a = 2.96 \times 200 \times 29.92 \times \left(\frac{0.0863}{522} - \frac{0.09}{960} \right) - \frac{0.00126 \times 100^2 \times 960 \times 0.016 \times 200}{10^5 \times 29.92 \times 0.09}$$

$$= 1.27 - 0.14 = 1.13 \text{ in.}$$

Fig. 1 shows the variation in the available draft of a typical 200 ft by 10 ft chimney operating under the general conditions noted in Example 1. When the chimney is under static conditions and no gases are flowing, the available draft is equal to 1.27 in. of water, the theoretical intensity. As the amount of gases flowing increases, the available draft decreases until it becomes zero at a gas flow of 297 lb per second, at which point the draft loss due to friction is equal to the theoretical intensity. The point of maximum draft and zero capacity is called shut-off draft, or point of impending delivery, and corresponds to the point of shut-off head of a centrifugal pump. The point of zero draft and maximum capacity is called the wide open point and corresponds to the wide open point of a centrifugal pump. A set of operating characteristics may be developed for any size chimney operating under any set of conditions by substituting the proper values in Equation 2 and then plotting the results in the manner shown in Fig. 1.

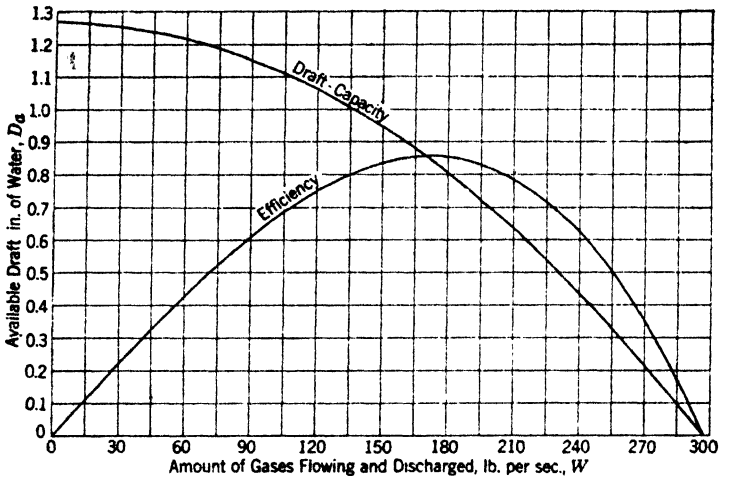


FIG. 1. TYPICAL SET OF OPERATING CHARACTERISTICS OF A NATURAL DRAFT CHIMNEY

Fig. 2 is a typical chimney performance chart giving the available draft for various gas flow rates and sizes of chimney. This chart is based on an atmospheric temperature of 62 F, a chimney gas temperature of 500 F, a unit chimney gas weight of 0.09 lb per cubic foot, sea level atmospheric pressure, a coefficient of friction of 0.016, and a friction duct length equal to the height of the chimney above the grate level. These curves may be used for general operating conditions. For specific conditions, a new chart may be prepared from Equation 2 or 3.

DETERMINING CHIMNEY SIZES

If the required performance for a proposed chimney is known and *if a chimney-gas velocity is assumed*, Equation 2 can be transposed to yield the necessary height and an equation can be developed for the required diameter. These operations result in the following equations:

$$H = \frac{D_T}{2.96B_o\left(\frac{W_o}{T_o} - \frac{W_c}{T_c}\right) - \frac{0.184fW_cB_oV^2}{T_cD}} \tag{6}$$

The weight of gas per second, $W = 12.075\,\frac{D^2\,VB_o\,W_c}{T_c}$ from which

$$D = 0.288\sqrt{\frac{WT_c}{B_oW_cV}} \tag{7}$$

where

H = required height of chimney above grate, feet.
D = required minimum diameter of chimney, feet.
V = chimney gas velocity, feet per second.
D_T = total required draft, inches of water.

For large chimneys, it is usual to assume that total construction cost is least when the product HD (height × diameter) is minimum. On this assumption, the product of Equations 6 and 7 can be differentiated and

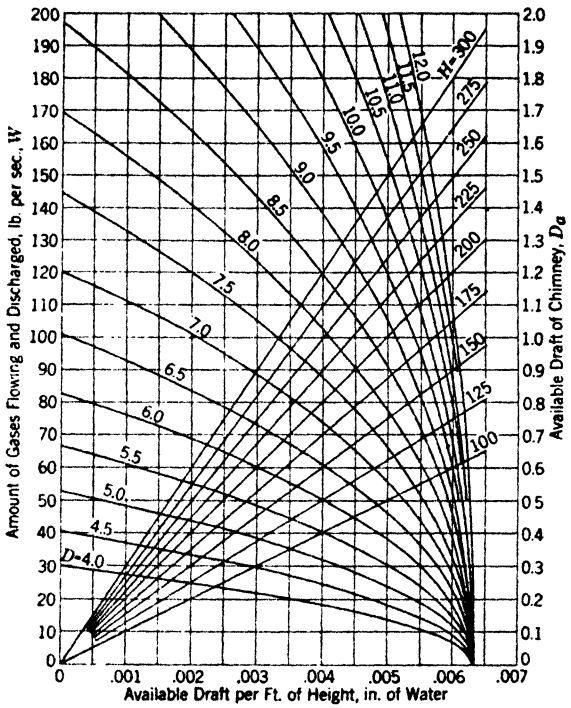


FIG. 2. CHIMNEY PERFORMANCE CHART

To solve a typical example: Proceed horizontally from a Weight Flow Rate point to intersection with diameter line; from this intersection follow vertically to chimney height line; from this intersection follow horizontally to the right to Available Draft scale. Starting from a point of Available Draft, take steps in reverse order.

the differential set equal to zero to find the minimum. Solution for velocity then yields the following equation:

$$V_e = \left(\frac{0.772 T_c \left(\frac{W_o}{T_o} - \frac{W_c}{T_c} \right) \sqrt{\frac{W T_c}{B_o W_c}}}{f W_c} \right)^{2/5} \qquad (8)$$

where V_e = economical chimney gas velocity, feet per second.

Equations 6, 7 and 8 can of course be simplified if values are assumed for some of the factors in it. Some typical figures for boiler plants are:

Average chimney gas temperature 500 F..... T_c = 960 F absolute
Average atmospheric temperature 62 F..... T_o = 522 F absolute
Average coefficient of friction 0.016..... f = 0.016
Average chimney, gas density, 0 F, 1 Atmosphere..... W_c = 0.09 lb per cubic foot
Barometer reading, sea level..... B_o = 29.92 in. Hg

When these values are substituted in Equations 8, 7 and 6 respectively, the results are:

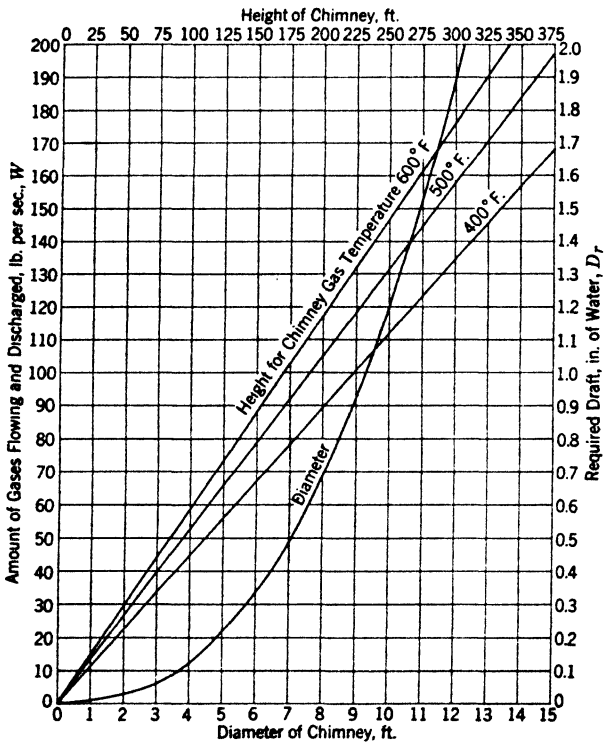
$V_e = 13.7 W^{1/5}$ (9) $\qquad D = 1.5 W^{2/5}$ (10) $\qquad H = 190 D_r$ (11)

Fig. 3 gives the economical chimney sizes for various amounts of gases flowing and for required draft intensities computed from Equations 9, 10 and 11. They are based on the operating factors used in reducing Equations 6, 7 and 8 to their simpler form. The sizes shown by the curves in the chart should be used for general operating conditions only,

or where the required data necessary for an exact determination are difficult or impossible to secure. Whenever it is possible to secure accurate data, or the anticipated operating conditions are fairly well known, the required size should be determined from Equations 6, 7 and 8.

FACTORS AFFECTING REQUIRED DRAFT

The foregoing considerations deal with chimney size selection when the required draft and flue gas volume and temperature are known. The



Diameter values also for gas temperatures of 400, 500 and 600 F.

FIG. 3, ECONOMICAL CHIMNEY SIZES

required draft is, of course, equal to the sum of all the resistances to gas flow from the ash pit door to and including the chimney connection.

Fig. 4 presents information on the fuel-bed draft loss for various kinds of coal burned at different rates and rough generalizations can be given for the losses in the flue passages of boiler or furnace, but, on account of the great differences in such devices, more reliable data on their flue gas volume temperature and flue resistance should be obtained for design purposes from their respective manufacturers.

Flue gases encounter resistance to flow in breechings or smoke pipes and this can probably be treated with sufficient accuracy by means of the method used for air ducts. (See Chapter 41.) The friction in straight ducts can be estimated by means of the last terms of Equations 2 and 3.

Also, the temperature of flue gases falls during passage through breechings or flue pipes. For uninsulated surfaces this probably can be adequately estimated by assuming a loss of heat from the flue gas of 3 Btu per

hour per square foot for each Fahrenheit degree temperature difference between the gases and surrounding air.

DOMESTIC CHIMNEYS

The height of a chimney for a residence or apartment is generally limited by the height of the building since it is desirable to have the chimney architecturally congruous with the building. The height desirable from an architectural viewpoint and the location of the chimney may be disadvantageous to the operation of the boiler or furnace and it is therefore important that the manufacturer of the fuel burning appliance to be installed be consulted in regard to the adequacy of the chimney.

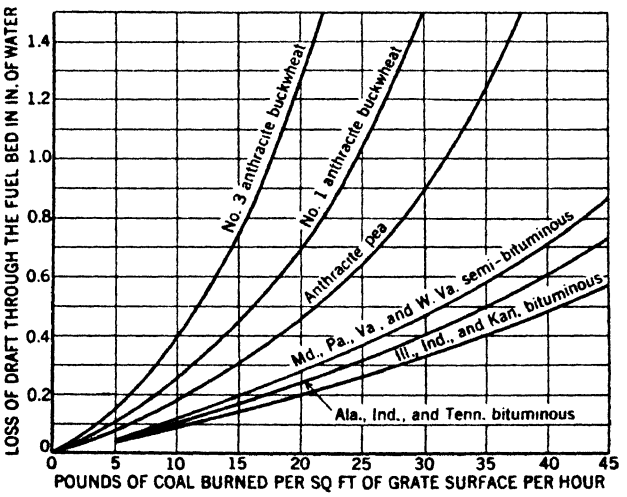


FIG. 4. DRAFT REQUIRED AT DIFFERENT RATES OF COMBUSTION FOR VARIOUS KINDS OF COAL

A chimney in order to provide satisfactory performance must have adequate *height* and *area*, be of permanently tight construction and should be as smooth internally as practicable.

It should be remembered that mechanically fired devices, oil burners and stokers, are equipped with blowers so that, with these devices, the chimney is not required to overcome the resistance of a fuel bed. Nevertheless, a draft in the fire box, of about 0.03 in. of water is considered desirable so that any small openings in the fire box or flue passages will result in leakage of air inward, and not leakage of combustion products outward. This is not to be taken to condone leaks in fire boxes. Such leaks adversely affect plant efficiency.

OBSERVED TEST PERFORMANCE

The observed performances of some brick chimneys[3] are given in Tables 1 and 2.

The tests on which these data are based were made at various outside temperatures as shown and, to make them comparable among themselves, the observed drafts were corrected to 32 F, 1 atmosphere pressure, by the formula:

TABLE 1. TEMPERATURE AND DRAFT IN 9 IN. BY 9 IN. MASONRY CHIMNEY[a]

CHIMNEY HEIGHT, FT		FUEL OIL EQUIVALENT[c] OF CHIMNEY GASES		FLUE GAS TEMP. AT INLET, F	AVERAGE CHIMNEY GAS TEMP. F	OUTSIDE TEMP. F	OBSERVED DRAFT INCH WATER	COMPUTED STATIC DRAFT INCH WATER	CORRECTED DRAFT[b]		INDICATED FRICTION LOSS INCH WATER
Nominal	Height Above Thimble	Fuel Oil Gal/Hr	CO_2 Per Cent						Observed Inch Water	Computed Static Inch Water	
35	31.5	0.5	10	236	142	68	0.040	0.053	0.076	0.089	+0.013
35	31.5	1.5	8	200	158	81	0.043	0.055	0.086	0.098	+0.012
35	31.5	0.5	10	400	224	77	0.081	0.095	0.128	0.142	+0.014
35	31.5	1.5	8	400	278	80	0.092	0.117	0.139	0.164	+0.025
35	31.5	0.5	10	1000	488	77	0.163	0.191	0.206	0.234	+0.028
35	31.5	1.5	8	1000	601	78	0.169	0.214	0.216	0.261	+0.045
30	27.5	0.5	10	250	160	83	0.043	0.049	0.070	0.076	+0.006
30	27.5	1.5	8	250	195	84	0.055	0.064	0.097	0.106	+0.009
30	27.5	0.5	10	400	213	68	0.075	0.084	0.107	0.116	+0.009
30	27.5	1.5	8	400	269	72	0.094	0.108	0.125	0.139	+0.014
30	27.5	0.5	10	1000	460	64	0.146	0.169	0.174	0.197	+0.023
30	27.5	1.5	8	1000	608	72	0.168	0.193	0.204	0.228	+0.025
25	22.3	0.5	10	250	171	92	0.034	0.037	0.072	0.076	+0.003
25	22.3	1.5	8	200	171	94	0.034	0.036	0.074	0.076	+0.002
25	22.3	0.5	10	400	243	78	0.066	0.073	0.097	0.105	+0.006
25	22.3	1.5	8	400	301	79	0.085	0.091	0.116	0.123	+0.006
25	22.3	0.5	10	1000	504	79	0.124	0.137	0.154	0.167	+0.013
25	22.3	1.5	8	1000	642	80	0.146	0.159	0.177	0.190	+0.013
20	17.2	0.5	10	250	179	94	0.029	0.032	0.059	0.062	+0.003
20	17.2	1.5	8	200	188	94	0.031	0.032	0.059	0.060	+0.001
20	17.2	0.5	10	400	270	81	0.058	0.062	0.082	0.086	+0.004
20	17.2	1.5	8	400	297	55	0.075	0.081	0.087	0.093	+0.006
20	17.2	0.5	10	600	330	50	0.086	0.091	0.095	0.100	+0.005
20	17.2	1.5	8	600	425	55	0.104	0.106	0.116	0.118	+0.002
20	17.2	0.5	10	1000	526	37	0.120	0.130	0.123	0.134	+0.010
20	17.2	1.5	8	915	588	44	0.129	0.134	0.135	0.141	+0.005
15	11.3	0.5	10	250	182	87	0.023	0.023	0.041	0.041	+0.000
15	11.3	1.5	8	200	180	84	0.025	0.024	0.042	0.041	−0.001
15	11.3	0.5	10	400	258	32	0.053	0.055	0.054	0.056	+0.002
15	11.3	1.5	8	400	293	43	0.056	0.057	0.060	0.061	+0.001
15	11.3	0.5	10	600	369	34	0.068	0.071	0.069	0.071	+0.003
15	11.3	1.5	8	600	428	40	0.072	0.076	0.075	0.078	+0.004
15	11.3	0.5	10	1000	577	32	0.094	0.092	0.094	0.092	−0.002
15	11.3	1.5	8	1000	654	55	0.092	0.090	0.100	0.098	−0.002

[a] Actual inside dimensions of flue lining 7¼ × 7¼ in.
[b] Corrected for outside temperature 32 F. Barometer 29.92 in. Hg.
[c] ½ gal per hour of fuel oil burned with 10 per cent CO_2 produces 18.4 cfm or 1.38 lb per minute of flue gases (corrected to 70 F, 1 atmosphere pressure); 1½ gal per hour of fuel oil burned with 8 per cent CO_2 produces 67.5 cfm or 5.06 lb per minute of flue gas (corrected to 70 F, 1 atmosphere pressure).

TABLE 2. TEMPERATURE AND DRAFT IN 9 IN. BY 13 IN. MASONRY CHIMNEY[a]

CHIMNEY HEIGHT, FT		FUEL OIL EQUIVALENT[c] OF CHIMNEY GASES		FLUE GAS TEMP. AT INLET, F	AVERAGE CHIMNEY GAS TEMP. F	OUTSIDE TEMP. F	OBSERVED DRAFT INCH WATER	COMPUTED STATIC DRAFT INCH WATER	CORRECTED DRAFT[b]		INDICATED FRICTION LOSS INCH WATER
Nominal	Height Above Thimble	Fuel Oil Gal/Hr	CO_2 Per Cent						Observed Inch Water	Computed Static Inch Water	
35	31.5	0.5	10	204	125	78	0.035	0.034	0.078	0.077	−0.001
35	31.5	1.5	8	206	155	82	0.047	0.052	0.093	0.098	+0.006
35	31.5	1.5	8	600	355	84	0.140	0.141	0.193	0.194	+0.001
35	31.5	0.5	10	600	272	78	0.104	0.117	0.152	0.165	+0.013
35	31.5	0.5	10	1000	438	77	0.163	0.178	0.205	0.221	+0.015
35	31.5	1.5	8	1000	542	84	0.189	0.201	0.236	0.247	+0.012
30	27.5	0.5	10	260	155	83	0.040	0.045	0.081	0.086	+0.005
30	27.5	1.5	8	202	159	83	0.048	0.047	0.089	0.088	−0.001
30	27.5	0.5	10	605	278	80	0.089	0.103	0.129	0.144	+0.014
30	27.5	1.5	8	595	378	72	0.130	0.144	0.161	0.175	+0.014
30	27.5	0.5	10	1007	438	91	0.135	0.148	0.179	0.191	+0.013
30	27.5	1.5	8	995	609	89	0.166	0.168	0.225	0.227	+0.002
25	22.3	0.5	10	258	155	86	0.034	0.034	0.069	0.069	0.000
25	22.3	1.5	8	200	160	86	0.039	0.037	0.074	0.072	−0.002
25	22.3	0.5	10	600	312	86	0.086	0.090	0.122	0.126	+0.004
25	22.3	1.5	8	592	382	83	0.106	0.110	0.140	0.144	+0.004
25	22.3	0.5	10	1007	462	85	0.120	0.127	0.154	0.161	+0.007
25	22.3	1.5	8	1007	607	84	0.151	0.153	0.184	0.185	+0.002
20	17.2	0.5	10	280	175	79	0.030	0.028	0.062	0.060	−0.002
20	17.2	1.5	8	250	192	81	0.044	0.041	0.069	0.066	−0.003
20	17.2	0.5	10	598	324	74	0.069	0.079	0.089	0.099	+0.010
20	17.2	1.5	8	604	410	74	0.090	0.094	0.111	0.115	+0.004
20	17.2	0.5	10	1015	496	79	0.094	0.107	0.115	0.128	+0.013
20	17.2	1.5	8	1000	645	74	0.122	0.127	0.140	0.147	+0.005
15	11.3	0.5	10	270	172	88	0.022	0.021	0.041	0.040	−0.001
15	11.3	1.5	8	200	166	85	0.022	0.020	0.040	0.038	−0.002
15	11.3	0.5	10	604	356	86	0.055	0.052	0.073	0.070	−0.003
15	11.3	1.5	8	599	431	84	0.066	0.062	0.082	0.078	−0.004
15	11.3	0.5	10	1000	560	82	0.066	0.074	0.082	0.091	+0.008
15	11.3	1.5	8	1000	682	85	0.083	0.082	0.101	0.100	−0.001

[a] Actual inside dimensions of flue lining 6½ × 11 in.

[b] Corrected for outside temperature 32 F. Barometer 29.92 in. Hg.

[c] ½ gal per hour of fuel oil burned with 10 per cent CO_2 produces 18.4 cfm or 1.38 lb per minute of flue gases (corrected to 70 F, 1 atmosphere pressure); 1½ gal per hour of fuel oil burned with 8 per cent CO_2 produces 67.5 cfm or 5.06 lb per minute of flue gas (corrected to 70 F, 1 atmosphere pressure).

$$O_2 = O_1 + S_2 - S_1 \quad (12)$$

where

S_1 = computed static (theoretical) draft, experimental conditions.
S_2 = computed static (theoretical) draft, standard conditions.
O_1 = observed draft, experimental conditions.
O_2 = observed draft corrected to standard conditions.

It will be noted that the observed draft exceeded the computed static draft during some observations on the shorter chimneys. This is mainly attributed to the draft producing effect of the hot gases immediately above the chimney. By means of a manometer it was found that a measurable draft existed in this gas column for some distance above the chimney top. However, the temperatures in the chimney were measured with unshielded thermocouples and the actual gas temperatures may have been higher for this reason than the observed temperatures on which the computations of draft were based. The tests were made in calm weather.

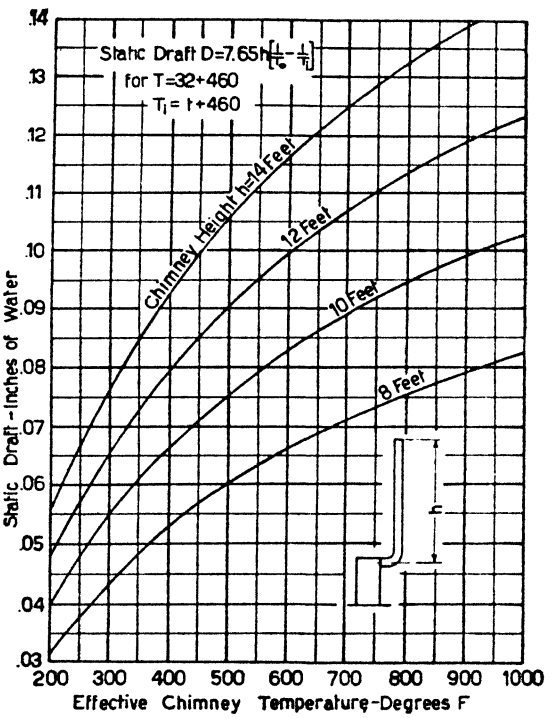


FIG. 5. COMPUTED STATIC DRAFT FOR SHORT CHIMNEYS

Tests were made at the *National Bureau of Standards* to find the draft produced by round, metal smoke pipe set in vertical position to act as chimneys. Curves are presented in Fig. 5 showing the computed static or theoretical draft for short chimneys for various heights and temperatures. For this purpose, the density of chimney gases was assumed to be the same as that of air at the same condition, since the error thus introduced was not considered important in this case. The results of the tests showed that the following procedures would yield the available draft for 6-in. flue pipe used as a chimney within 10 per cent for the range shown and for fuel burning rates from about one-quarter to three-quarters of a gallon of oil per hour.

Using the temperature at the smoke collar of the heater, find the static draft corresponding to the available chimney height. Then:

1. If the chimney is bare, multiply the static draft by 0.76 to find the available draft.
2. If the chimney is insulated with 1 in. of air-cell material with a ¼-in. air space, multiply the static draft by 0.85 to find the available draft.
3. If the chimney is insulated with 1 in. of air-cell material with a 1-in. air space, open

at top and bottom for ventilation, multiply the static draft by 0.81 to find the available draft.

4. If the chimney is insulated with 1 in. of air-cell material and has a 1-in. air space closed at top and bottom to prevent ventilation, multiply the static draft by 0.85 to find the available draft.

The use of the 1-in. air-cell asbestos insulation in the tests discussed is not to be construed as an approval of such insulation in all cases in regard to fire resistance. Several laboratories are working on the fire resistance aspects of the problem but definite rules are not yet available. For coal- or oil-burning devices, a bare smoke pipe is probably safe if kept 2 ft or more from any woodwork and the better the pipe is insulated, or the lower its temperature, the nearer it can be placed to combustible materials.

DRAFT REQUIREMENTS OF DOMESTIC APPLIANCES

Typical flue-gas temperatures and drafts required at rated output for several kinds of domestic heating appliances[4] are contained in Table 3.

TABLE 3. DRAFTS REQUIRED BY TYPICAL DOMESTIC HEATING DEVICES OR APPLIANCES

DEVICE	DRAFT, INCHES WATER	STACK TEMPERATURE F DEG
Space Heater, Oil Burning, Pot Burner	0.06 to 0.08	1000
Warm Air Furnace, Oil Burning, Pot Burner	0.06	860
Warm Air Furnace, Hand Fired	0.06[b]	900
Floor Furnace, Oil Burning, Pot Burner	0.06	860
Mechanical Oil Burner, Less than 5 gph	0.03[a]	.....
Mechanical Oil Burner, More than 5 gph	0.05[a] or less	.....
Cooking Stove, Solid Fuel	0.04[b]	400
Space Heater, Coal Burning	0.06[b]	900

[a]Draft in fire-box. [b]For chestnut sized anthracite.

CHIMNEYS FOR GAS HEATING

Heating appliances designed to burn gas as well as appliances converted to gas burning, except those equipped with power type burners and excepting conversion burner installations in excess of 400,000 Btu per hour input in large steel boilers, are always equipped with a draft hood attached to the flue outlet of the appliance. This draft hood is required if the appliance is to meet the approval requirements of the *American Gas Association* and the *American Standards Association* and is essential for safe operation. It is designed to prevent excessive chimney draft which would lower appliance efficiency, to prevent a blocked flue or a down draft in the chimney from impairing combustion, to provide a relief opening for the products of combustion during down draft or blocked flue conditions, and to prevent spillage of the products of combustion to the space surrounding the appliance if there is a chimney draft equivalent to that provided by a 3-ft chimney. As the draft hood is designed without moving parts, the relief opening is always open and consequently some air is drawn into the chimney. While the air drawn in lowers the gas temperature in the chimney, it also lowers the dew-point of the gases and tends to prevent condensation.

The installation of conversion burner equipment in large boilers is usually made in accordance with regulations of the local gas company. In such installations a definite chimney draft may be required for proper

combustion and consequently the foregoing reference to the use of draft hoods would not apply.

The products of complete combustion of gas are water vapor (H_2O) and carbon dioxide (CO_2). In the case of manufactured gas, the presence of organic sulfur compounds, generally between 3 and 15 grains per hundred cubic feet, gives rise to minute percentages of sulfur dioxide and sulfur tri-oxide.

The volume of water vapor in the flue products from natural or coke oven gas is about twice the volume of carbon dioxide. It is extremely important that the chimney be tight and resistant to corrosion not only of moisture, but also of dilute sulfur trioxide.

Vitreous tile linings with joints which prevent retention of moisture and linings made of non-corrosive materials are advantageous. The protection of unlined chimneys has been investigated and the results indicate that after the loose material has been removed, the spraying with a water emulsion of asphalt chromate will provide excellent protection.

Advice regarding recommended practice and materials for flue connections and chimney linings can usually be obtained from the local gas company and should be given careful consideration.

Since a gas designed appliance must be able to operate at rated input (plus 10 or 15 per cent) without chimney connection, and without producing carbon monoxide, the only function of the chimney is to remove the products of combustion from the room. The chimney provides draft to overcome the friction in the flue pipe and chimney, but does not draw air into the appliance.

Chimneys for venting appliances designed for burning gas can therefore be low in height, but must have adequate area. The height is usually established by the building height. Chimney sizes are usually selected on the basis of Btu input of the appliance. One chart[5] designed to facilitate selection is shown in Fig. 6. The assumptions made in preparing the chart as well as its limitations should be noted carefully.

Since Fig. 6 has been prepared for circular flues, relative capacities for rectangular and semi-elliptical flues[6] are shown in Fig. 7.

When a flue is connected to several appliances, the number of horizontal runs of various sizes which may be substituted for the single run having a diameter equal to that of the flue may be obtained from Table 4.

CONSTRUCTION DETAILS

For general data on the construction of chimneys reference should be made to the Building Code recommended by the *National Board of Fire Underwriters*, Article XI, Sections 1101 to 1105, in which the following are some of the important provisions listed in the 1943 edition:

(*a*) Chimneys erected within or attached to a structure shall be constructed of brick, of solid block masonry, or of reinforced concrete.

(*b*) Chimneys shall extend at least 3 ft above the highest point where they pass through the roof of the building and at least 2 ft higher than any ridge within 10 ft of such chimney.

(*c*) Every such chimney shall be properly capped with brick, terra cotta, stone, cast-iron, concrete or other approved non-combustible, weatherproof material.

(*d*) Chimneys shall be wholly supported on approved masonry or self-supporting fireproof construction.

(*e*) No such chimney shall be corbeled from a wall more than 6 in.; nor shall such chimney be corbeled from a wall which is less than 12 in. in thickness unless it projects equally on each side of the wall; provided that in the second story of two-story dwellings

corbeling of chimneys on the exterior of the enclosing walls may equal the wall thickness. In every case the corbeling shall not exceed 1 in. projection for each course of brick projected.

(*f*) No change in the size or shape of a chimney, where the chimney passes through the roof, shall be made within a distance of 6 in. above or below the roof joists or rafters.

(*g*) Smoke flues for warm air, hot water and low pressure steam heating furnaces shall have walls not less than 8 in. thick; the walls may be of solid masonry using brick, stone or concrete, or of solid moulded or solid cast chimney units of concrete, or of burned clay, or of suitably reinforced solid concrete cast in place; provided that for stone masonry, other than sawed or dressed stone in courses, the thickness shall be not less

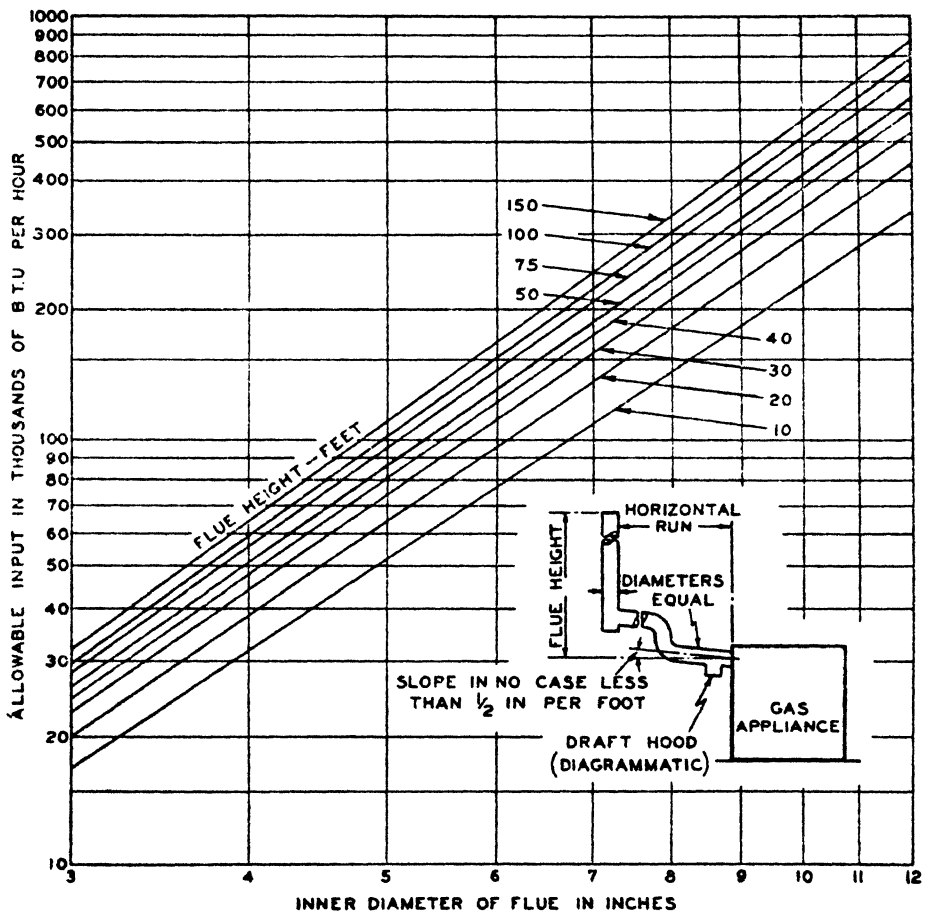


FIG. 6. ALLOWABLE BTU INPUT TO CIRCULAR FLUES FOR DOMESTIC GAS APPLIANCES WITH DRAFT HOODS

Notes Applying to Fig. 6:

1. Chart is based on: average flue temperature of 150 F, outside temperature of 60 F, barometric pressure of 30 in. Hg, 100 per cent excess air and 100 per cent dilution at draft hood.
2. Based on terra-cotta lined flues. With rough brick flues, capacities are 15 per cent less.
3. Based on condition that horizontal run is not greater than 20 ft except for a flue height less than 20 ft, in which case the horizontal run is not to have greater length than the height of the flue.
4. Two long radius elbows are included in the horizontal run, the diameter of which is equal to that of the flue.
5. Each additional elbow reduces the allowable horizontal run by a length in feet equal to the diameter in inches.
6. When the horizontal run has an effective length in excess of that given (or additional elbows) the next larger size of flue should be chosen. It is desirable that long horizontal runs be insulated to reduce heat loss of flue products and to conserve draft.
7. Capacities should be reduced 3.5 per cent for each 1000 ft above sea level.

than 12 in. The walls shall be properly bonded, or tied with non-corrosive metal anchors. In dwellings and buildings of like heating requirements the thickness of the chimney walls may be reduced to not less than 3¾ in. when lined with a flue lining conforming to the Code requirements.

(*h*) Required flue linings shall be made of fire clay or other refractory clay to withstand the action of flue gases and to resist, without softening or cracking, the temperatures to which they will be subjected, but not less than 2,000 F, or of cast-iron of approved quality, form and construction. Approved corrosion resistant linings may be used in flues for gas appliances.

(*i*) Required clay flue linings shall be not less than ⅝ in. thick for the smaller flues and increasing in thickness for the larger flues.

(*j*) Flue linings shall be built ahead of the construction of the chimney as it is carried up, carefully bedded one on the other in mortar as hereinafter specified with close fitting joints left smooth on the inside.

(*k*) Flue linings shall start from a point not less than 8 in. below the intake. They

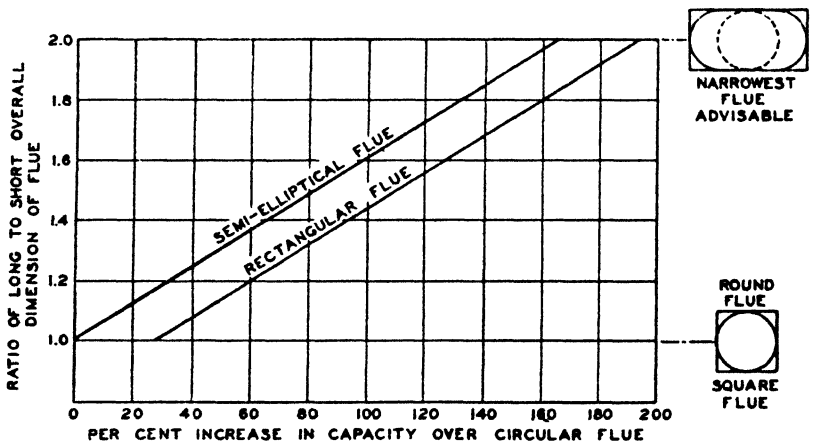


FIG. 7. CAPACITY OF A RECTANGULAR FLUE OR A SEMI-ELLIPTICAL FLUE, WITH SEMI-CIRCULAR ENDS HAVING ITS MINIMUM WIDTH EQUAL TO THE DIAMETER OF A CIRCULAR FLUE, COMPARED WITH THE CAPACITY OF THE CIRCULAR FLUE

shall extend, as nearly vertically as possible, for the entire height of the chimney. It is recommended that flue linings be extended 4 in. above the top or cap of the chimney.

(*l*) Only Portland cement mortar, cement lime mortar or fire clay mortar shall be used in setting flue linings.

For *gas appliances* the Building Code specifies lined chimneys and metal smoke stacks for all appliances which may be converted readily to the use of solid or liquid fuel and also for all boilers and furnaces except those having a flue gas temperature not exceeding 550 F at the outlet of the draft hood when burning gas at the manufacturer's rating and which may therefore be connected to *Type B* vent piping. Approved *Type B* vent piping is non-combustible, corrosion resistant piping of adequate strength and heat insulating value, and having bell and spigot or other acceptable joints. Fig. 6 may be used for selection of vent pipe size.

Important points to be considered in the use of *Type B* vent piping are:

1. *Type B* flues must be plainly and permanently marked, at the point where the vent connection enters the flue: *For use of gas appliances only.*

2. *Type B* vent material should not be used for external chimney flues and external runs of it should not exceed 3 ft outside the building roof. When this requirement makes it necessary to cross over through attic space, the piping should be pitched not less than 45 deg.

3. Because of the small size and low temperature, *Type B* vents should be provided with a vent cap with wire screening to prevent building of birds' nests.

4. Each appliance should have the equivalent of a 4 in. diameter *Type B* vent, even though the appliance may have a 3 in. flue collar. A typical minimum vertical flue size for a frame dwelling is 6 in. in diameter or equivalent.

5. When several floor furnaces are to be vented, it is acceptable practice to connect each of these by means of 4 in. vents to a common 6 in. vertical vent. Lateral piping must have adequate pitch, ½ in. per foot, and should not exceed 20 ft in horizontal length.

6. An alternate method of connecting several appliances is to run separate *Type B* vents to the attic and then to connect them by means of cross-over piping and Y fittings to a common vertical vent passing through the roof. This reduces the number of holes in the roof.

All flue mortar for flues or vent pipes from gas burning appliances shall be acid resisting.

GENERAL CONSIDERATIONS FOR CHIMNEYS

The draft of domestic chimneys may be subject to a variety of influences not usually encountered in power chimneys[7]. Horizontal winds have an aspirating effect as they cross the chimney and are an aid to draft. However, surrounding objects, such as trees or other buildings, may

TABLE 4. EQUIVALENT FLUE PIPE SIZES[a]

DIAMETER OF HORIZONTAL RUNS	SIZE OF FLUE						
	3	4	5	6	8	10	12
3	1	2	3	5	9	12	22
4		1	2	3	5	7	11
5			1	2	3	4	7
6				1	2	3	5
8					1	2	3

[a]Comfort Heating (*American Gas Association*).

affect the direction of the wind at the chimney top and may even direct it down the chimney, tending to reduce the draft or even to cause it to be negative. Although the chimney should extend well above the highest part of the roof, it is impracticable to carry it much beyond this point.

It is also important to consider the source of the air supply for proper combustion. Usually the boiler or furnace is located in the basement. When the furnace room has windows or doors opening to the outside on two or more sides of the house, the leakage of air will be sufficient for combustion, even though the windows and doors may be shut. If, however, the leakage is not sufficient to prevent an appreciable drop of pressure in the furnace room below that of the air outside, the chimney draft will be reduced by the difference between the atmospheric pressure outside and that inside the boiler room. In case the boiler room is fairly tight and is open to the outside on only one side of the house, then the draft will be affected in windy weather even with windows or doors open. If the wind is blowing toward the boiler room the draft will be increased, but if blowing in the opposite direction the draft may be decreased.

It is not to be assumed that increasing the cross-section area of a chimney will always effect a cure for poor draft. The opposite result may be experienced because of the cooling effect of the larger area. This reduces the theoretical draft and the velocity of the gases, and affords a greater opportunity for counter currents in the chimney. Sometimes the only practical remedy for a chimney with bad draft, when the chimney is of the proper size and is affected by conditions beyond control, is to resort to mechanical draft. This can often be done at small expense and the arrangement can be such that the fan or blower need be operated only when conditions are bad.

Two or more chimneys, either large or small, should never be connected together. If connected at the bottom, hot gases in the inverted U-tube thus formed would be in unstable equilibrium. Cold air would descend through one such chimney, from the top, and drive the hot gases out of the other and thus annul the draft.

More than one device can be served by one chimney. Batteries of boilers are commonly connected to a single chimney in power plants. However, if two or more chimneys are used, each chimney should be used separately for part of the boilers, and not connected in manifold with another chimney, in order to avoid the difficulty described previously.

In domestic installations it is sometimes necessary to serve a space heater or cooking stove and a water heater with the same chimney flue. This is not desirable, especially for low chimneys, since doors left open on one device while it is un-fired will tend to annul the draft on another device. Gas burning devices, with their draft hoods and lack of draft dampers, are especially bad in this respect. The traditional method of avoiding this with brick chimneys has been to construct multiple-flue chimneys, so that each fuel-burning device could be served by a separate opening. If two devices must be served by one flue-opening in a chimney, their connections to the chimneys should not be located opposite each other. The connection from the larger device should be reasonably low down and that from the smaller, up near the ceiling, so that each device can be serviced as well as possible, regardless of the treatment of the other.

Excessive height in a chimney does no harm but means for controlling the draft are more than ordinarily essential if the chimney is too large in capacity. Coal-burning devices often have air leaks around the fire-box and the draft doors sometimes fit poorly so that the fire cannot be controlled at a low rate. Perhaps the simplest remedy for such cases is the barometric damper which admits air into the flue pipe and thus reduces the draft.

Directions for building chimneys for fireplaces are contained in Department of Agriculture Farmers' Bulletin No. 1889.

It is considered bad practice to connect any heating device to a fireplace flue unless the fireplace is effectively sealed.

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[1]—Notes on Power Plant Design, by E. F. Miller and James Holt (*Massachusetts Institute of Technology*, 1930).

[2]—A.S.H.V.E. RESEARCH REPORT No. 1105—Frictional Resistance to the Flow of Air in Straight Ducts, by F. C. Houghten, J. B. Schmieler, J. A. Zalovcik and N. Ivanovic (A.S.H.V.E. TRANSACTIONS, Vol. 45, 1939, p. 35) and for more complete discussion see Flow of Fluids in Closed Conduits, by R. J. S. Pigott (*Mechanical Engineering*, August, 1933).

[3]—Observed Performance of Some Experimental Chimneys, by R. S. Dill, P. R. Achenbach and J. T. Duck (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 351).

[4]—*National Bureau of Standards Commercial Standards:* CS101-43 Oil-Burning Space Heaters Equipped With Vaporizing Pot-Type Burners, CS75-42 Automatic Mechanical Oil Burners Designed for Domestic Installations, CS(E)104-43 Warm Air Furnaces Equipped With Vaporizing Pot-Type Burners; and *Trade Standards:* TS3536a Solid-Fuel Burning Forced Air Furnaces, TS3518 Oil-Burning Floor Furnaces Equipped With Vaporizing Pot-Type Burners.

[5]—Comfort Heating, 1938, p. 71 (*American Gas Association*).

[6]—Comfort Heating, 1938, p. 74 (*American Gas Association*).

[7]—Chimneys and Draft (Chapter 32 in Winter Air Conditioning, by S. Konzo, published by *National Warm Air Heating and Air Conditioning Association*, 1939).

Chapter 20

ESTIMATING FUEL CONSUMPTION FOR SPACE HEATING

Fuel Consumption Records, Calculated Heat Loss Method, Degree-Day Method, Estimating Fuel Consumption, Degree-Day as an Operating Unit, Maximum Demands and Load Factors, Seasonal Efficiency

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MANY methods are in use for estimating in advance of actual operation the anticipated heat or fuel consumption of heating plants over long or short periods. With suitable modification in procedure these same general methods are frequently useful in checking the degree of effectiveness with which heat or fuel is utilized during plant operation.

In applying any of these estimating methods to the consumption of a particular building plant it should be noted that (*a*) reliable records of past heat or fuel consumptions of the building under consideration will usually produce more trustworthy estimates of future consumptions than will any data obtained by averages or from other similar buildings; (*b*) where no past records exist useful data can sometimes be obtained from records of similar types of buildings with similar plants *in the same locality;* (*c*) records of consumption, which are averages from many types of plants in many types of buildings in various localities, can produce no better than an average estimate which may be far from accurate; (*d*) estimates based on computed heat losses without the benefit of operating data are wholly dependent on how well the computation represents the actual facts.

Estimates based on computed heat losses alone are especially necessary where unusual operating conditions are encountered such as excessive ventilation, abnormal inside temperatures, heat gains from external sources, etc., or where no information is available as to former consumption as in the case of proposed buildings of unusual design.

In interpreting and evaluating heat or fuel consumption estimates as well as in their preparation, it is well to realize that any estimating method used will produce a more reliable result over a long period operation than over a short period. Nearly all of the methods in common use will give trustworthy results over a full *annual* heating season, and in some cases such estimates will prove consistent within themselves for monthly periods. As the period of the estimate is shortened there is more chance that some factor not allowed for in the estimating method will become controlling and thus give discrepant and even ridiculous results.

Of the various estimating methods in use attention is directed in this discussion to but two as they are illustrative of all, viz: (1) calculated heat loss method, and (2) degree-day method.

CALCULATED HEAT LOSS METHOD

This method is theoretical and assumes constant temperatures for very definite hours each day throughout the entire heating season. It does not take into account factors which are difficult to evaluate such as opening of windows, abnormal heating of the building, poor heating systems, winter heat gains, such as sun effect, and many others. In order to apply this method the hourly heat loss from the building under maximum load,

or design condition, is computed following the principles discussed in Chapters 6 and 8 and the method described and illustrated in Chapter 14.

In predicting fuel consumption for heating a building by the Calculated Heat Loss Method, the general equation is:

$$F = \frac{H\,(t - t_a)\,N}{E\,(t_d - t_o)\,C} \qquad (1)$$

where

F = quantity of fuel or energy required (in the units in which C is expressed).

H = calculated heat loss, Btu per hour, during the design hour, based on t_o and t_d $\left(\text{generally } H = H_t + H_i \text{ but may on occasion equal } H_t + \frac{H_i}{2}\right)$.

t = average inside temperature maintained during heating period, Fahrenheit degrees.

t_a = average outside temperature through estimate period, Fahrenheit degrees (for cities with an Oct. 1-May 1 heating season, see Table 1, Chapter 14).

t_d = inside design temperature, Fahrenheit degrees (usually 70 F).

t_o = outside design temperature, Fahrenheit degrees (see Table 1 in Chapter 14).

N = number of heating hours in estimate period (for an Oct. 1—May 1 heating season, 212 days × 24 hr = 5088).

E = efficiency of utilization of the fuel over the period, expressed as a decimal; not the efficiency at peak or rated load condition.

C = heating value of one unit of fuel or energy.

Although the assumption of an Oct. 1-May 1 heating season is reasonably accurate in the well-populated New York-Chicago zone, it is not valid as far north as Minneapolis nor farther south than Washington, D. C. and St. Louis. Consequently, it is suggested that allowance be made for this variation, especially in the far north or southern cities.

Example 1. A residence building is to be heated to 70 F from 6 A.M. to 10 P.M and 55 F from 10 P.M. to 6 A.M. The calculated hourly heat loss is 120,000 Btu per hour based on 70 F inside at −10 F outside. If the building is to be heated by metered steam, how many pounds would be required during an average heating season?

Solution. The heating value of steam may be taken as 1000 Btu per pound, and since it is purchased steam, the efficiency can be assumed as 100 per cent. Assume average outside temperature as 36.4 F. The average inside temperature is:

$$\frac{(16 \times 70) + (8 \times 55)}{24} = 65 \text{ F.}$$

Substituting in Equation 1:

$$F = \frac{120{,}000\,(65 - 36.4)\,5088}{1.00\,[70 - (-10)]\,1000} = 218{,}275 \text{ lb.}$$

Example 2. How much would the fuel cost to heat the building in Example 1 during an average heating season with coal at $8 per ton and with a calorific value of 11,000 Btu per pound, assuming that the seasonal efficiency of the plant was 55 per cent?

Solution. Substituting in Equation 1: $F = \frac{120{,}000\,(65 - 36.4)\,5088}{0.55\,[70 - (-10)]\,11{,}000} = 36{,}079$ lb = 18 tons, which, at $8 per ton, costs $144.

Example 3. What will be the estimated fuel cost per year of heating a building with gas, assuming that the calculated hourly heat loss is 92,000 Btu based on 0 F, which includes 26,000 Btu for infiltration? The design temperatures are 0 F and 72 F. The normal heating season is 210 days, and the average outside temperature during the heating season is 36.4 F. The seasonal efficiency will be 75 per cent. The heating plant will be thermostatically controlled, and a temperature of 55 F will be maintained from 11 P.M. to 7 A.M. Assume that the price of gas is 7 cents per 100,000 Btu of fuel consumption, and disregard the loss of heat through open windows and doors.

Solution. The average hourly temperature is:

$$t_a = \frac{(72 \times 16) + (55 \times 8)}{24} = 66.3 \text{ F.}$$

The maximum hourly heat loss will be:

$$H = 92{,}000 - \frac{26{,}000}{2} = 79{,}000 \text{ Btu.}$$

$$M = \frac{79{,}000\ (66.3 - 36.4) \times 24 \times 210}{100{,}000 \times 0.75 \times (72 - 0)} = 2204.6 \text{ hundred thousand Btu.}$$

$2204.6 \times \$0.07 = \$154.32$ = estimated fuel cost per year of heating building.

Several time-saving procedures have been devised for quickly estimating the hourly Btu loss of one and two-story residences in order that fuel estimates can be predicted more quickly from Equation 1. A graphical method of calculating heat losses has been developed [1] which makes possible a quick solution if the gross wall, ceiling, or floor areas and respective transmission coefficients are known.

The Federal Housing Administration has originated a short-cut formula for residential heat loss determinations which makes use of the floor area and three selected transmission coefficients. The formula was developed to apply to detached houses approximately rectangular in shape with total exterior door and window areas equal to about 25 per cent of the floor area and with a floor area not greater than about 1500 sq ft. Equation 2 is for a one-story residence and Equation 3 is intended for two-story structures.

$$H_1 = A\ (G + U_w + U_c + U_f)\ (t_d - t_o) \tag{2}$$

$$H_2 = A\ (G + 1.2\ U_w + 0.5\ U_c + 0.5\ U_f)\ (t_d - t_o) \tag{3}$$

where

H_1 = heat loss from one-story residence, Btu per hour.

H_2 = heat loss from two-story residence, Btu per hour.

A = floor area, square feet, measured to the inside faces of enclosing walls and is the sum of the following areas: (1) all the area on each principal floor level; (2) the area of all finished habitable attic rooms, including bathrooms, toilet compartments, closets, and halls; (3) all other areas intended to be heated and not located in the basement.

G = glass and infiltration factor for ordinary construction: (0.45 for no weatherstripping or storm windows), (0.40 for weatherstripping), (0.30 for storm windows with or without weatherstripping).

U_w = coefficient of transmission for outside wall.

U_c = coefficient transmission for ceiling.

U_f = coefficient of transmission for floor.

t_d = inside design temperature, Fahrenheit degrees.

t_o = outside design temperature, Fahrenheit degrees.

Notes for application of Equations 2 and 3.

1. The calculation of heat loss from heated spaces into adjacent spaces such as attics, basementless areas, and heated or unheated garages shall be based on the assumption that the temperature of such adjacent spaces is the same as the outside design temperature.

2. For all floors over basements or other warmed spaces assume $U_f = 0$.

3. For structures having concrete slab floors laid on the ground a modified application of the formula may be made. Assume $U_f = 0$ and calculate the heat loss in accordance with the check formula. Then add the slab loss determined in accordance with the procedure developed by the National Bureau of Standards and described in BMS Report 103.

4. No basement area is to be included in the formula calculation. If finished habitable rooms in the basement are to be heated, the additional heat loss should be calculated separately and added to the amount obtained by the formula.

Both the graphical method and short-cut formulas, when used within the limitations established, have been found to give reasonably accurate

results for the average residence, but if precise estimates are required, the procedure outlined in Chapter 14 should be used.

In the case of gravity warm air heating installations, the load was formerly expressed in square inches of leader pipe which can be converted into Btu per hour by multiplying the square inches of leader area by 111, 167, and 200 for first, second, and third floor respectively.

Example 4. What would be the total gas consumption over a full heating season of a gas-fired gravity warm air furnace designed according to the Code[2], and with four 12 in. and two 8 in. round leaders to the first floor and six 10 in. leaders to the second floor, if the gas has a heating value of 500 Btu per cubic foot, the plant operates at a 70 per cent seasonal efficiency and is designed to maintain an average inside temperature of 65 F when it is 10 F outside in a city where the average outside temperature is 45 F and the heating season is 5088 hr long?

Solution. The area of the round leaders is: 12 in., 113 sq in.; 10 in., 79 sq in.; and 8 in., 50 sq in. The total Btu transmitted is:

First Floor:	$[(4 \times 113) + (2 \times 50)] \times 111$	= 61,272 Btu per hour.
Second Floor:	$(6 \times 79) \times 167$	= 79,158 Btu per hour.
	Total	140,430 Btu per hour.

Substituting this total heat loss value as H in Equation 1 gives:

$$F = \frac{140{,}430\ (65 - 45)\ 5088}{0.70\ (70 - 10)\ 500} = 680{,}483 \text{ cu ft gas.}$$

DEGREE-DAY METHOD

This method is based on consumption data which have been taken from buildings in operation, and the results computed on a degree-day basis. While this method may not be as theoretically correct as the Calculated Heat Loss Method, it is considered by many to be of more value for practical use.

The amount of heat required by a building depends upon the outdoor temperature, if other variables are eliminated. Theoretically it is proportional to the difference between the outdoor and indoor temperatures. The *American Gas Association*[3] determined from experiment in the heating of residences that the gas consumption varied directly as the difference between 65 F and the mean outside temperature. In other words, on a day when the mean temperature was 20 deg below 65 F, twice as much gas was consumed as on a day when the temperature was 10 deg below 65 F. For any one day, when the mean temperature is less than 65 F, there are as many degree-days as there are degrees difference in temperature between the mean temperature for the day and 65 F. Degree-days may be calculated on other than the 65 F base but are seldom used and are of little value except where the inside temperature to be maintained as, for example, in warehouses, differs greatly from the usual inside temperature range of 68 F to 72 F.

Table 1 lists the average number of degree-days, which have occurred over a long period of years, by months and the yearly totals for various cities in the United States, Canada and Newfoundland. The values for United States cities were calculated by taking the difference between 65F and the daily mean temperature computed as ½ the total of the daily maximum and the daily minimum temperatures. The monthly averages were obtained by adding daily degree-days for each month each year and dividing by the number of days in the month; then totaling the respective calendar monthly averages for the number of years indicated and dividing by the number of years. The total or long term yearly average degree-day

value is the summation of the 12 monthly averages. Degree days for Canadian cities were supplied by the Canadian Meteorological Division of the Department of Transport and were computed from the mean temperature normals on record for the various stations.

Any attempt to apply the degree-day method of calculating fuel consumption for less than one month would be of very little value. It should be noted that this method of calculation is based on a long term average and cannot be expected to coincide with any single year in calculating fuel requirement as individual yearly degree-day calculations will vary as much as 20 per cent above and below the long term average.

If the degree-days occurring each day are totaled for a reasonably long period, the fuel consumption during that period as compared with another period will be in direct proportion to the number of degree-days in the two periods. Consequently, for a given installation, the fuel consumption can be calculated in terms of fuel used per degree-day for any sufficiently long period and compared with similar ratios for other periods to determine the relative operating efficiencies with the outside temperature variable eliminated.

Studies made by the *National District Heating Association*[4] of the metered steam consumption of 163 buildings located in 22 different cities and served with steam from a district heating company substantiate the fact that the 65 F base originally chosen by the gas industry is approximately correct.

Formula for Degree-Day Method

The general equation for calculating the probable fuel consumption by the degree-day method is:

$$F = U \times N \times D \tag{4}$$

where

F = fuel consumption for the estimate period.
U = unit fuel consumption, or quantity of fuel used per (degree-day) (*building load unit*).
N = number of *building load units* (when available use calculated hourly heat loss instead of actual amount of radiation installed).
D = number of degree-days for the estimate period.

Values of N depend on the particular building for which the estimate is being prepared and must be found by surveying plans, by observation, or by measurement of the building. Values of U for use in this equation are the unit fuel consumptions per degree-day and are obtained as a result of the collection of operating information. Certain of this information is presented later but before referring to these data attention is directed to the nature of the unit.

Unit Fuel Consumptions per Degree-Day

The quantity of fuel used per degree-day in a given heating plant can be reduced to a unit basis in terms of quantity of fuel or steam per degree-day per square foot of radiation, per cubic foot of heated building space, or per thousand Btu hourly heat loss at design conditions. A less frequently used basis is quantity of fuel per (degree-day) (square foot of floor area). In fact any convenient unit can be used to relate the consumption to the degree-day and to the building.

TABLE 1. AVERAGE MONTHLY AND YEARLY DEGREE-DAYS FOR CITIES IN THE UNITED STATES, CANADA AND NEWFOUNDLAND [a, b] (BASE 65F)

State	Station	Years	No. of Seasons	July	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.	May	June	Yearly Total
Ala.	Anniston	05/06-40/41	36	0	0	10	135	388	600	609	513	361	152	37	1	2806
	Birmingham A	98/99-45/46	48	0	1	10	111	348	586	591	497	313	130	23	1	2611
	Mobile	98/99-45/46	48	0	0	1	44	203	377	397	314	175	52	3	0	1566
	Montgomery	98/99-45/46	48	0	0	4	71	279	484	494	405	239	85	10	0	2071
Ariz.	Flagstaff	98/99-40/41	43	43	70	244	573	847	1111	1167	970	889	668	469	190	7241
	Phoenix	98/99-45/46	48	0	0	0	18	166	384	402	263	154	47	7	0	1441
	Yuma	98/99-40/41 45/46	44	0	0	0	9	113	306	318	182	85	22	1	0	1036
Ark.	Bentonville	06/07-40/41	35	1	1	38	216	516	810	879	716	519	247	86	7	4036
	Fort Smith A	98/99-45/46	48	0	0	12	128	410	717	763	615	390	154	36	1	3226
	Little Rock A	98/99-45/46	48	0	0	11	120	383	668	704	579	367	145	31	1	3009
Calif.	Eureka	98/99-45/46	48	281	269	274	344	411	518	541	478	504	440	391	307	4758
	Fresno A	98/99-45/46	48	0	0	5	77	309	562	573	380	289	152	52	4	2403
	Independence	98/99-40/41	43	0	0	28	216	512	778	799	619	477	267	120	18	3834
	Los Angeles	98/99-45/46	48	1	0	5	43	110	225	272	235	212	158	103	27	1391
	Needles	17/18-38/39	22	0	0	0	19	217	416	447	243	124	26	3	0	1495
	Point Reyes	98/99-40/41	43	350	336	263	282	317	425	467	406	437	413	415	363	4474
	Red Bluff A	98/99-33/34 38/39-40/41 44/45-45/46	41	0	0	12	97	345	592	601	419	328	178	72	9	2653
	Sacramento	98/99-45/46	48	2	1	15	98	332	582	595	405	326	202	101	21	2680
	San Diego A	98/99-45/46	48	5	1	9	60	143	252	300	257	230	172	118	49	1596
	San Francisco	98/99-45/46	48	196	179	121	139	241	420	460	340	317	272	255	197	3137
	San Jose	06/07-40/41	35	21	21	52	151	329	512	527	383	339	249	167	72	2823
Colo.	Denver	98/99-45/46	48	8	8	126	411	716	1005	1023	897	790	516	275	64	5839
	Durango	04/05-40/41	37	25	37	201	535	861	1204	1271	1002	859	615	394	139	7143
	Grand Junction	98/99-45/46	48	1	1	59	347	743	1138	1218	883	671	377	152	23	5613
	Leadville	07/08-40/41	34	280	332	509	841	1139	1413	1470	1285	1245	990	740	434	10678
	Pueblo A	98/99-45/46	48	3	4	91	377	730	1042	1042	875	724	446	195	29	5558
Conn.	Hartford A	04/05-45/46	42	3	16	105	370	692	1065	1157	1062	859	524	213	47	6113
	New Haven A	98/99-45/46	48	3	11	88	341	658	1017	1109	1023	840	522	221	47	5880
D.C.	Washington	98/99-45/46	48	0	2	42	251	553	872	928	834	624	340	101	14	4561
Fla.	Apalachicola	13/14-45/46	33	0	0	1	23	154	300	323	252	159	38	2	0	1252
	Jacksonville	98/99-45/46	48	0	0	0	25	144	294	302	244	131	42	3	0	1185
	Key West	98/99-45/46	48	0	0	0	0	2	14	21	15	7	0	0	0	59
	Miami	11/12-45/46	35	0	0	0	0	15	41	53	45	28	3	0	0	185
	Pensacola	13/14-45/46	33	0	0	0	25	159	305	332	255	162	39	4	0	1281
	Tampa A	98/99-45/46	48	0	0	0	6	60	149	157	126	62	11	0	0	571
Ga.	Atlanta	98/99-45/46	48	0	0	12	128	392	644	660	563	382	169	33	2	2985
	Augusta	98/99-45/46	48	0	0	4	85	312	529	533	448	274	107	13	1	2306
	Macon	99/00-45/46	47	0	0	5	91	322	532	538	449	278	108	14	1	2338
	Savannah A	98/99-45/46	48	0	0	1	45	206	390	395	332	194	66	6	0	1635
	Thomasville	05/06-40/41	36	0	0	2	48	208	361	359	299	178	52	5	1	1513
Idaho	Boise A	98/99-45/46	48	9	17	136	385	717	1025	1077	840	688	440	252	92	5678
	Lewistown	00/01-32/33	33	5	9	107	378	688	932	992	779	603	371	193	52	5109
	Pocatello	98/99-45/46	48	12	21	176	475	821	1159	1224	1004	845	550	330	124	6741
Ill.	Cairo	98/99-45/46	48	0	0	26	181	493	823	878	748	512	232	60	4	3957
	Chicago	98/99-45/46	48	6	7	88	337	712	1116	1218	1080	861	531	259	67	6282
	Peoria A	05/06-45/46	41	4	8	88	350	730	1126	1231	1035	790	436	178	28	6004
	Springfield	98/99-45/46	48	0	3	65	286	664	1056	1151	977	719	377	152	16	5446
Ind.	Evansville A	98/99-45/46	48	0	1	35	211	544	888	948	822	582	288	85	6	4410
	Fort Wayne A	11/12-45/46	35	6	13	106	374	737	1107	1211	1052	864	504	217	41	6232
	Indianapolis	98/99-45/46	48	1	4	66	297	660	1032	1102	973	737	410	154	22	5458
	Royal Center	18/19-31/32	14	11	19	116	373	740	1104	1239	976	860	502	245	54	6239
	Terre Haute	12/13-45/46	34	0	3	62	270	627	993	1072	897	687	358	133	15	5117
Iowa	Charles City	04/05-45/46	42	8	24	164	480	906	1362	1535	1281	995	552	255	62	7624
	Davenport	98/99-45/46	48	2	6	91	344	748	1176	1291	1111	835	448	171	29	6252
	Des Moines	98/99-45/46	48	1	6	102	354	767	1204	1320	1132	843	446	171	29	6375
	Dubuque	98/99-45/46	48	3	12	123	402	808	1249	1380	1190	915	493	204	41	6820
	Koekuk	98/99-41/42	44	1	3	71	303	680	1077	1191	1025	761	397	136	18	5663
	Sioux City A	98/99-45/46	48	3	11	128	402	844	1273	1402	1206	909	485	202	40	6905
Kan.	Concordia	98/99-45/46	48	1	3	68	288	670	1060	1144	954	712	365	142	18	5425
	Dodge City A	98/99-45/46	48	1	3	59	275	641	998	1046	868	668	351	139	20	5069
	Iola	05/06-40/41	36	0	1	40	236	579	930	1026	817	599	282	98	8	4616
	Topeka	98/99-45/46	48	0	2	56	254	623	1013	1096	917	659	326	116	13	5075
	Wichita A	98/99-45/46	48	0	1	41	221	576	947	1016	836	604	290	103	9	4644
Ky.	Louisville	98/99-45/46	48	0	1	35	217	549	881	931	816	588	298	93	8	4417
	Lexington	98/99-40/41	43	1	3	48	258	601	916	964	862	650	352	123	14	4792
La.	New Orleans	98/99-45/46	48	0	0	0	23	145	304	323	247	129	31	1	0	1203
	Shreveport A	98/99-45/46	48	0	0	4	71	275	506	531	415	241	79	10	0	2132
Me.	Eastport	98/99-45/46	48	158	146	271	528	827	1224	1364	1238	1080	778	530	301	8445
	Greenville	07/08-40/41 42/43-45/46	38	69	113	315	643	1012	1464	1625	1443	1251	842	468	194	9439
	Portland A	98/99-45/46	48	28	48	182	466	794	1182	1309	1188	997	671	376	136	7377
Md.	Baltimore	98/99-45/46	48	0	1	33	227	526	855	921	837	637	343	95	12	4487

[a]Computed from daily temperatures recorded by United States Weather Bureau stations in cities over a varied number of seasons as indicated in the 3rd and 4th column of the table. Degree-day data for airport stations are not included in this table. The data for United States cities were computed by the United States Weather Bureau in 1946 and 1947 in accordance with the requirements of the National Joint Committee on Weather Statistics. The data for a number of the cities listed are based on readings taken at more than one official city weather station during the periods of analysis but the slight difference in the readings would not appreciably affect the resultant. Degree-days for cities in Canada and Newfoundland were supplied by the Canadian Meteorological Division, Department of Transport and were computed from mean temperature normals. * Indicates actual degree days for 1947.

[b]Letter A after station indicates city office and airport records combined.

TABLE 1. AVERAGE MONTHLY AND YEARLY DEGREE-DAYS FOR CITIES IN THE UNITED STATES, CANADA AND NEWFOUNDLAND [a] (CONTINUED)

State	Station	Years	No. of Seasons	July	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	Apr.	May	June	Yearly Total
Mass..	Boston....A	98/99-45/46	48	7	15	98	338	647	1008	1108	1025	841	538	245	66	5936
	Fitchburg	98/99-40/41	43	12	29	144	432	774	1139	1240	1137	940	572	254	70	6743
	Nantucket	98/99-45/46	48	15	15	87	315	590	904	1010	967	866	619	366	121	5875
Mich .	Alpena	98/99-45/46	48	53	79	235	548	874	1238	1388	1321	1162	764	448	168	8278
	Detroit....A	98/99-45/46	48	7	15	111	388	749	1124	1230	1134	927	566	253	56	6560
	Escanaba	98/99-45/46	48	54	84	256	572	927	1329	1499	1382	1219	808	477	170	8777
	Grand Rapids	03/04-45/46	43	8	20	128	422	764	1136	1248	1143	944	569	263	57	6702
	Houghton	00/01-40/41														
		42/43-45/46	45	70	94	268	582	965	1355	1535	1421	1251	820	474	195	9030
	Lansing	10/11-45/46	36	18	36	167	467	818	1190	1306	1178	995	600	294	80	7149
	Ludington	12/13-40/41	29	41	55	182	472	794	1135	1271	1183	1056	698	418	153	7458
	Marquette	98/99-45/46	48	86	99	258	555	926	1306	1465	1349	1193	794	494	220	8745
	Sault Ste. Marie .A	98/99-45/46	48	91	110	285	616	965	1379	1572	1470	1291	826	487	215	9307
Minn..	Duluth	98/99-45/46	48	80	97	292	631	1066	1539	1714	1497	1254	804	515	234	9723
	Minneapolis	98/99-45/46	48	8	23	167	481	942	1415	1587	1372	1072	577	260	62	7966
	Morehead	98/99-40/41	43	20	47	240	607	1105	1609	1815	1555	1225	679	327	98	9327
	St. Paul	98/99-32/33														
		37/38-40/41	39	11	24	169	488	942	1412	1589	1371	1078	573	258	60	7975
Miss..	Corinth	09/10-40/41	32	0	1	13	142	418	669	696	570	396	149	32	1	3087
	Meridian	00/01-45/46	46	0	0	6	99	322	525	539	440	274	107	17	1	2330
	Vicksburg	98/99-45/46	48	0	0	5	76	267	483	503	407	236	82	10	0	2069
Mo.	Columbia	98/99-45/46	48	0	3	62	266	621	1000	1076	916	655	337	120	14	5070
	Hannibal	98/99-40/41	43	1	3	66	288	652	1037	1139	980	710	374	128	15	5393
	Kansas City ....A	98/99-45/46	48	0	2	51	239	598	993	1077	909	651	322	108	12	4962
	Saint Louis	98/99-45/46	48	0	1	38	215	558	925	998	855	607	300	91	8	4596
	Springfield....A	98/99-45/46	48	1	2	48	232	561	908	971	827	596	302	109	12	4569
Mont.	Billings ....A	09/10-45/46	37	14	31	223	530	889	1215	1310	1102	923	555	315	106	7213
	Havre	98/99-45/46	48	27	54	275	592	1012	1376	1532	1358	1102	614	341	133	8416
	Helena ....A	98/99-45/46	48	43	66	291	596	944	1252	1347	1157	990	639	413	192	7930
	Kalispell	99/00-45/46	47	66	102	332	636	968	1235	1339	1135	956	630	413	220	8032
	Miles City....A	98/99-45/46	48	7	20	188	510	918	1322	1461	1267	997	545	275	81	7591
	Missoula	92/93-45/46	54	37	56	275	606	951	1235	1331	1072	903	590	369	179	7604
Neb..	Drexel	15/16-25/26	11	4	6	95	405	788	1271	1353	1096	843	493	219	38	6611
	Lincoln	98/99-45/46	48	1	5	85	325	732	1144	1242	1056	792	407	166	25	5980
	North Platte	98/99-45/46	48	4	9	131	410	799	1163	1227	1039	846	480	227	49	6384
	Omaha....A	98/99-45/46	48	1	4	84	324	744	1169	1280	1088	810	410	157	24	6095
	Valentine	98/99-45/46	48	8	19	167	479	877	1246	1349	1166	962	563	287	74	7197
Nev	Reno ....A	05/06-45/46	41	8	18	140	407	697	959	1007	791	702	498	301	93	5621
	Tonopah	14/15-40/41	27	5	7	105	388	713	1010	1075	870	749	522	286	82	5812
	Winnemucca	98/99-45/46	48	10	23	188	494	801	1090	1128	884	768	536	321	114	6357
N. H.	Concord ...A	03/04-45/46	43	18	49	189	497	823	1228	1345	1213	993	637	308	100	7400
N. J..	Atlantic City	98/99-45/46	48	1	2	39	247	546	867	946	887	750	485	208	37	5015
	Cape May	98/99-31/32	34	1	2	38	221	527	852	936	876	737	459	188	33	4870
	Newark....A	98/99-23/24														
		35/36-40/41	32	1	6	65	295	635	980	1083	1002	794	448	162	29	5500
	Sandy Hook	15/16-40/41	26	1	2	40	268	579	921	1016	973	833	499	206	31	5369
	Trenton	14/15-45/46	32	1	6	63	301	604	957	1033	923	748	441	154	25	5256
N. M.	Albuquerque ..A	19/20-45/46	27	0	0	27	258	646	913	955	708	592	322	91	5	4517
	Roswell	05/06-45/46	41	0	0	26	191	512	781	773	585	459	199	50	2	3578
	Santa Fe	98/99-45/46	43	12	15	129	451	772	1071	1094	892	786	544	297	60	6123
N. Y.	Albany	98/99-45/46	48	4	15	117	411	753	1143	1271	1169	948	551	220	46	6648
	Binghamton	98/99-45/46	48	15	37	148	448	767	1137	1236	1155	950	584	267	74	6818
	Buffalo....A	98/99-45/46	48	15	24	126	413	745	1110	1226	1165	995	668	348	90	6925
	Canton	06/07-45/46	40	27	61	219	550	898	1368	1516	1385	1139	695	340	107	8305
	Ithaca	99/00-42/43	44	17	40	156	451	770	1129	1236	1156	978	606	292	83	6914
	New York	98/99-45/46	48	1	4	50	272	594	940	1028	953	771	465	172	30	5280
	Oswego	98/99-45/46	48	20	33	147	440	762	1151	1275	1188	1015	665	366	124	7186
	Rochester ....A	98/99-45/46	48	10	26	132	423	751	1123	1227	1155	967	605	282	71	6772
	Syracuse ....A	03/04-45/46	43	13	32	146	437	760	1147	1255	1167	972	611	283	76	6899
N.C..	Ashville	02/03-45/46	44	2	3	49	279	565	800	817	719	558	315	114	15	4236
	Charlotte	98/99-45/46	48	0	1	17	148	420	684	700	600	413	198	39	4	3224
	Hatteras	98/99-45/46	48	0	0	1	61	273	500	570	530	391	193	34	1	2554
	Manteo	04/05-28/29	25	0	0	7	113	358	595	642	594	469	249	75	7	3109
	Raleigh	98/99-45/46	48	0	1	17	153	415	681	702	615	429	210	46	6	3275
	Wilmington	98/99-45/46	48	0	0	5	90	306	520	531	479	320	144	24	1	2420
N. D.	Bismarck	98/99-45/46	48	21	44	244	595	1057	1520	1704	1479	1181	643	340	109	8937
	Devils Lake	04/05-45/46	42	42	76	295	687	1186	1676	1906	1615	1313	752	411	145	10104
	Grand Forks	12/13-40/41														
		42/43-45/46	33	32	60	274	663	1160	1681	1895	1608	1298	718	359	123	9871
	Williston	98/99-45/46	48	28	61	285	637	1104	1545	1733	1513	1226	671	368	130	9301
Ohio...	Cincinnati	98/99-45/46	48	1	3	53	273	611	960	1008	898	668	369	130	16	4990
	Cleveland	98/99-45/46	48	7	14	93	354	684	1045	1143	1067	876	553	252	56	6144
	Columbus	98/99-45/46	48	2	6	68	314	670	1019	1081	975	749	432	165	25	5506
	Dayton	11/12-42/43														
		45/46	33	2	6	71	309	660	992	1079	939	752	416	163	23	5412
	Sandusky	98/99-45/46	48	3	8	82	347	695	1067	1155	1066	862	536	232	42	6095
	Toledo	98/99-45/46	48	5	13	100	370	718	1097	1189	1083	887	533	227	47	6269
Okla...	Broken Arrow	18/19-30/31	13	0	0	28	169	513	805	881	646	506	212	61	5	3826
	Oklahoma City	98/99-45/46	48	0	0	22	153	455	792	846	684	457	200	58	3	3670
Ore....	Baker	98/99-45/46	48	54	72	259	534	848	1161	1222	984	827	601	418	217	7197
	Medford....A	11/12-40/41														
		45/46	31	7	10	99	345	632	837	844	636	556	387	223	74	4650
	Portland	98/99-45/46	48	27	28	106	292	538	725	775	616	533	368	237	108	4353
	Roseburg	98/99-45/46	48	23	26	116	316	541	714	730	582	530	386	257	111	4332

TABLE 1. AVERAGE MONTHLY AND YEARLY DEGREE-DAYS FOR CITIES IN THE UNITED STATES, CANADA AND NEWFOUNDLAND [a] (CONCLUDED)

State	Station	Years	No. of Seasons	July	Aug.	Sept.	Oct.	Nov.	Dec	Jan.	Feb.	Mar.	Apr.	May	June	Yearly Total
Pa.	Erie	98/99-45/46	48	8	17	101	367	692	1049	1159	1105	922	591	284	68	6363
	Harrisburg A	98/99-45/46	48	1	6	67	314	637	990	1073	973	757	425	146	23	5412
	Philadelphia	98/99-45/46	48	0	2	36	235	544	884	962	881	685	378	115	17	4739
	Pittsburgh	98/99-45/46	48	3	7	69	322	651	982	1042	964	751	444	166	29	5430
	Reading	12/13-45/46	34	1	5	69	301	606	957	1038	929	736	423	144	23	5232
	Scranton	00/01-45/46	46	6	22	117	400	717	1074	1162	1071	862	523	213	51	6218
R. I.	Block Island	98/99-45/46	48	10	11	79	313	596	919	1030	984	875	618	354	108	5897
	Narragansett Pier	98/99-17/18	20	1	26	121	366	691	1012	1113	1074	916	622	342	113	6397
	Providence	04/05-45/46	42	6	16	101	358	668	1020	1106	1027	847	538	237	60	5984
S. C.	Charleston	98/99-45/46	48	0	0	1	47	225	428	452	384	249	83	7	0	1866
	Columbia	98/99-45/46	48	0	0	6	95	327	560	568	482	305	126	18	1	2488
	Due West	21/22-31/32	11	0	0	9	142	393	594	651	491	411	158	39	2	2890
	Greenville A	17/18-45/46	29	0	1	13	127	410	650	684	551	403	179	40	1	3059
S. D.	Huron	98/99-45/46	48	10	20	159	502	962	1409	1572	1353	1039	573	271	70	7940
	Pierre	98/99-40/41 42/43-45/46	47	4	11	136	438	887	1317	1460	1253	971	516	238	52	7283
	Rapid City	98/99-45/46	48	15	28	192	495	842	1178	1280	1140	981	598	339	109	7197
Tenn.	Chattanooga	98/99-45/46	48	0	0	13	150	432	691	711	604	412	185	39	1	3238
	Knoxville A	98/99-45/46	48	0	0	20	189	498	756	774	666	470	226	56	3	3658
	Memphis A	98/99-45/46	48	0	0	14	126	387	670	716	600	386	157	33	1	3090
	Nashville	98/99-45/46	48	0	0	20	170	469	748	788	675	467	218	55	3	3613
Texas	Abilene A	98/99-45/46	48	0	0	10	96	332	603	619	483	296	110	23	1	2573
	Amarillo A	98/99-45/46	48	1	2	42	221	548	854	861	719	546	284	107	11	4196
	Austin A	26/27-45/46	20	0	0	2	31	227	410	458	315	185	46	5	0	1679
	Brownsville A	08/09-45/46	38	0	0	0	8	65	176	191	111	65	11	1	0	628
	Corpus Christi	98/99-45/46	48	0	0	0	11	102	255	282	204	93	17	1	0	965
	Dallas A	13/14-45/46	33	0	0	6	70	293	574	600	437	281	91	15	0	2367
	Del Rio	05/06-45/46	41	0	0	2	35	203	413	413	262	139	31	3	0	1501
	El Paso A	98/99-45/46	48	0	0	6	88	366	615	615	432	291	104	14	1	2532
	Fort Worth A	98/99-45/46	48	0	0	5	79	285	553	586	463	270	97	16	1	2355
	Galveston	98/99-45/46	48	0	0	0	14	123	290	334	255	130	27	1	0	1174
	Houston	09/10-45/46	37	0	0	1	27	160	331	361	247	150	36	2	0	1315
	Palestine	98/99-45/46	48	0	0	4	67	261	496	512	401	236	80	11	0	2068
	Point Arthur	17/18-45/46	29	0	0	1	27	177	328	375	254	151	37	2	0	1352
	San Antonio A	98/99-45/46	48	0	0	1	31	171	366	390	287	148	37	4	0	1435
	Taylor	01/02-40/41	40	0	0	2	56	234	462	494	375	214	64	8	0	1909
Utah	Modena	00/01-45/46	46	6	11	156	499	832	1142	1190	944	816	567	338	97	6598
	Salt Lake City	98/99-45/46	48	3	5	98	371	712	1033	1093	871	716	446	236	66	5650
Vt.	Burlington	06/07-45/46	40	23	51	209	530	870	1313	1467	1338	1111	694	339	106	8051
	Northfield	98/99-42/43	45	62	112	283	602	947	1389	1524	1384	1176	754	405	166	8804
Va.	Cape Henry	98/99-45/46	48	0	0	7	125	398	676	731	682	526	301	86	6	3538
	Lynchburg A	98/99-45/46	48	1	2	37	230	521	799	829	732	537	287	81	12	4068
	Norfolk	98/99-45/46	48	0	0	9	129	392	668	712	650	483	254	62	5	3364
	Richmond	98/99-45/46	48	0	1	27	196	486	780	814	722	538	278	72	8	3922
	Wytheville	02/03-40/41	39	7	13	82	352	662	916	945	836	677	410	168	35	5103
Wash.	North Head	02/03-45/46	44	251	229	255	350	491	642	697	597	610	505	428	312	5367
	Seattle	98/99-45/46	48	67	69	170	365	554	704	759	637	595	436	299	160	4815
	Spokane A	98/99-45/46	48	20	37	184	480	817	1061	1139	931	756	490	285	118	6318
	Tacoma	98/99-45/46	48	71	75	190	390	581	737	786	658	612	455	313	171	5039
	Tatoosh Island	98/99-45/46	48	301	295	325	421	534	654	716	627	643	537	454	350	5857
	Walla Walla	98/99-45/46	48	5	10	90	315	662	910	981	770	571	354	186	56	4910
	Yakima	09/10-45/46	37	8	17	124	395	778	1050	1125	837	624	374	193	60	5585
W. Va.	Elkins A	98/99-45/46	48	15	23	115	403	722	1003	1033	947	763	489	229	58	5800
	Parkersburg	98/99-45/46	48	1	3	56	286	617	930	977	882	660	369	129	18	4928
Wis.	Green Bay	98/99-40/41	48	17	38	179	494	889	1329	1493	1329	1087	658	327	91	7931
	La Crosse	98/99-45/46	48	7	22	157	454	864	1339	1492	1281	990	531	232	52	7421
	Madison	04/05-45/46	42	8	20	145	452	857	1296	1451	1246	1002	588	274	66	7405
	Milwaukee	98/99-45/46	48	13	17	124	411	786	1203	1329	1177	959	617	341	102	7079
	Wausau	15/16-40/41	26	26	58	216	568	982	1427	1594	1381	1147	680	315	100	8494
Wyo.	Cheyenne A	98/99-45/46	48	40	46	251	587	876	1144	1187	1064	996	720	460	165	7536
	Lander	98/99-45/46	48	27	43	265	623	1021	1400	1427	1197	1006	669	410	155	8243
	Yellowstone Park	04/05-40/41	37	125	173	424	759	1079	1386	1464	1252	1165	841	603	334	9605
Alta.	Calgary			108	167	432	722	1122	1426	1609	1355	1215	750	480	264	9,650
	Edmonton			70	167	441	750	1224	1593	1810	1504	1299	777	428	222	10,285
B. C.	Vancouver			43	65	234	459	657	818	893	736	682	498	326	162	5,573
	Victoria			155	158	264	446	462	738	815	689	651	504	366	237	5,485
	Prince Rupert			282	229	342	546	702	893	933	804	809	645	521	357	7,063
Man.	Churchill			350	391	696	1187	1773	2356	2604	2288	2204	1530	1097	672	17,148
	Winnipeg			27°	34	330	744	1302	1829	2111	1775	1531	822	397	78	10,980
N. B.	Moncton			8°	56	282	595	936	1373	1528	1392	1190	798	474	180	8,812
	Saint John			124	112	270	558	870	1271	1417	1266	1132	792	505	261	8,578
N. S.	Halifax			12	12	189	493	783	1141	1280	1168	1065	768	493	210	7,614
Ont.	Fort William			62	155	354	722	1143	1596	1807	1582	1386	888	567	234	10,496
	Hamilton			3°	9°	108	471	816	1178	1305	1187	1063	651	322	6	7,119
	London			34°	11°	126	588	843	1200	1336	1240	1073	642	307	105	7,425
	Ottawa			29°	22°	204	595	984	1494	1646	1459	1256	726	310	91	8,816
	Toronto			16	35	168	504	817	1155	1304	1206	1072	669	341	87	7,374
	Windsor			19°	5°	54	425	795	1172	1283	1148	995	582	251	73	6,802
P.E.I.	Charlottetown			5°	57°	222	539	858	1246	1463	1338	1203	858	536	213	8,538
P. Q.	Montreal			7°	20°	180	561	948	1407	1587	1392	1209	702	298	88	8,399
	Quebec			17°	43	276	651	1050	1534	1696	1481	1311	849	428	102	9,438
Sask.	Saskatoon			16°	68	396	781	1305	1767	2027	1635	1445	725	397	138	10,700
Y. T.	Dawson			167	322	687	1209	1908	2440	2666	2159	1879	1092	580	246	15,355

The choice of these units requires explanation and some discrimination and judgment. If the volume basis is used, the net heated space is preferable to the gross building cubage since gross cubage includes outer walls and certain portions of attic and basement space which are usually unheated. In the absence of data on net heated volume a figure of 80 per cent of the gross volume may be used to obtain the estimated net heated volume. The volume basis has been rather widely used primarily because of its facility in application. In industrial buildings it is usually easier to obtain the correct volume of a given building than to measure and evaluate the heating capacity of its heating system or calculate its maximum hourly Btu loss. The comparison of buildings on a straight volume basis does not allow for variation in exposure, type of construction, ratio of exposed area to cubical contents, and type of occupancy. It is considered inaccurate for purposes of estimating fuel consumption unless the buildings are of very similar nature.

The calculated heat loss or its equivalent square feet of calculated radiator surface may be used as the unit. The use of the unit equivalent direct radiation is of questionable value when referring to heat transfer surfaces used in warm air furnace or central air conditioning systems. Where steam or hot water radiation is already installed, care should be exercised in using the unit equivalent direct radiation basis for estimating, since actual installed radiation may differ considerably from the exact radiation requirements. In view of all these considerations it is believed that the unit based on *thousands of Btu of hourly calculated heat loss for the design hour* is probably the most desirable, although the one most widely used seems to be *units of fuel per degree-day per square foot of equivalent direct radiator surface.* The equivalent heating load for the hot water supply is not included in the latter unit, but it generally includes the piping load.

Since this unit is the one most widely used at present the unit fuel consumptions given in succeeding paragraphs of this chapter make use of this unit to a considerable extent, although it should be understood that most of these units of consumption can be transposed as desired.

Estimating Gas Consumption

Values of the Unit Fuel Consumption Constant (U) for gas are given in Table 2 for various gas heating values, and different types and sizes of heating plants. They are based on an inside design temperature of 70 F and an outside design temperature of 0 F and apply only to these conditions. For other outside design conditions corrections must be made as given in Table 5.

The factors in Table 2, as corrected if necessary, are satisfactory for regions having 3500 to 6500 degree-days per heating season. In regions with less than 3500 degree-days the unit gas consumption is higher than given; where over 6500, the unit is less than given. Ten per cent addition or deduction in these cases is recommended by *A.G.A.* publications. Estimates for industrial buildings where low inside temperatures are maintained cannot be made from this table.

For gas heating values other than those given in Table 2, simply interpolate or extrapolate. It will also be noted that Table 2 applies only to small installations. In general the larger the installation the smaller the unit gas consumption becomes and the values in the table should be used with care, if at all, in large gas-burning installations.

TABLE 2. UNIT FUEL CONSUMPTION CONSTANTS (*U*) FOR GAS[a]

Based on 0 F Outside Temperature, 70 F Inside Temperature, and 8-Hour Reduction to 60 F.

HEATING VALUE OF GAS BTU PER CU FT	HOT WATER			STEAM			WARM AIR	
	Cu Ft Gas per Degree-Day per Sq Ft Radiator			Cu Ft Gas per Degree-Day per Sq Ft Radiator			Cu Ft Gas per Degree-Day per 1000 Btu Hourly Design Heat Loss	
	Up to 500 Sq Ft	500 to 1200 Sq Ft	Over 1200 Sq Ft	Up to 300 Sq Ft	300 to 700 Sq Ft	Over 700 Sq Ft	Gravity	Fan Systems
500	0.142	0.135	0.128	0.242	0.231	0.220	0.855	0.820
535	0.132	0.126	0.120	0.226	0.215	0.206	0.800	0.766
800	0.089	0.085	0.081	0.151	0.144	0.137	0.534	0.513
1000	0.071	0.068	0.065	0.121	0.115	0.110	0.428	0.410
1 Therm = 100,000 Btu	Gas Consumption in Therms per Degree-Day							
	0.000708	0.000675	0.000642	0.00121	0.00115	0.00110	0.00428	0.00409

[a]Abstracted from Comfort Heating, *American Gas Association*, 1938.

TABLE 3. UNIT FUEL CONSUMPTION[a] CONSTANTS (*U*) FOR OIL[b]

Based on 0 F Outside Temperature, 70 F Inside Temperature, and 8-Hour Reduction to 55 F

UNITS	EFFICIENCY IN PER CENT				
	40	50	60	70	80
Gal Oil per Sq Ft Steam Radiator	0.00172	0.00137	0.00114	0.00098	0.00086
Gal Oil per Sq Ft Hot Water Radiator	0.00108	0.00086	0.00072	0.00062	0.00054
Gal Oil per 1000 Btu per Hour Heat Loss	0.00715	0.00571	0.00476	0.00409	0.00358

[a]Based on a heating value of 140,000 Btu per gallon.

[b]Abstracted by permission from *Degree-Day Handbook* (Second Edition, 1937), by C. Strock and C. H. B. Hotchkiss.

[c]Per degree-day.

TABLE 4. UNIT FUEL CONSUMPTION[a] CONSTANTS (*U*) FOR COAL[b]

Based on 0 F Outside Temperature, 70 F Inside Temperature, and 8-Hour Reduction to 55 F.

UNITS	EFFICIENCY IN PER CENT				
	40	50	60	70	80
Lb Coal per Sq Ft Steam Radiator	0.0200	0.0160	0.0133	0.0114	0.0100
Lb Coal per Sq Ft Hot Water Radiator	0.0125	0.0100	0.0084	0.0072	0.0063
Lb Coal per 1000 Btu per Hour Heat Loss	0.0825	0.0666	0.0550	0.0471	0.0412

[a]Based on a heating value of 12,000 Btu per pound.

[b]Abstracted by permission from *Degree-Day Handbook* (Second Edition, 1937), by C. Strock and C. H. B. Hotchkiss.

[c]Per degree-day.

Example 5. Estimate the gas required to heat a building located in Chicago, Ill., which has 6282 degree-days and a gas heating value of 800 Btu per cubic foot. The calculated heating surface requirements are 1000 sq ft of hot water radiation based on design temperature of −10 F and 70 F.

Solution. From Table 2, the fuel consumption for a design temperature of 0 F with 800 Btu gas is found to be 0.085 cu ft of gas per (degree-day) (square foot of hot water radiation). From Table 5, the correction factor is 0.875 for −10 F outside design temperature, hence 0.875 × 0.085 = 0.07438. By Equation 4,

$$F = 0.07438 \times 1000 \times 6282 = 467{,}255 \text{ cu ft.}$$

Estimating Oil Consumption

Unit fuel consumption factors for oil, similar to those for gas in Table 2, are given in Table 3. The factors in Table 3 apply only to an inside design temperature of 70 F and an outside design temperature of 0 F. For other outside design temperatures, the constants in Table 3 must be multiplied by the values in Table 5 as explained under Estimating Gas Consumption.

Values given in Table 3 assume the use of oil with a heating value of 140,000 Btu per gallon. For other heating values, multiply the values in Table 3 by the ratio of 140,000 divided by the heating value per gallon of fuel being used.

Example 6. Estimate the seasonal oil consumption of an oil-fired boiler in a building located in Minneapolis having a calculated heat loss of 192,000 Btu per hour, burning 144,000 Btu per gallon oil and operating at a seasonal efficiency of 60 per cent. The outside design temperature for Minneapolis is −20 F, and the inside design temperature is 70 F.

Solution. From Table 3, under 60 per cent efficiency and opposite the bottom column, the value of U is found to be 0.00476 gal per 1000 Btu hourly heat loss for 0 F outside temperature.

The correction factor for −20 F outside design temperature from Table 5 is 0.778. Solving, 0.778 × 0.00476 = 0.00370. Making a further correction for the heating value:

$$0.0037 \times \frac{140{,}000}{144{,}000} = 0.0036 \text{ gal per 1000 Btu per hour calculated heat loss per degree-day.}$$

From Table 1, the normal degree-days for Minneapolis are 7966. Since U is expressed in 1000 Btu, N is equal to 192. Substituting in Equation 4:

$$F = 0.0036 \times 7966 \times 192 = 5506 \text{ gal.}$$

Estimating Coal or Coke Consumption

Coal or coke consumption estimates are made in exactly the same procedure as for oil. Values of U are given in Table 4 which only apply to an inside design temperature of 70 F and an outside design temperature of 0 F. A correction must be made for other conditions by use of the multiplying factors in Table 5. Data in Table 4 are based on 12,000 Btu per

TABLE 5. CORRECTION FACTORS FOR OUTSIDE DESIGN TEMPERATURES[a]

OUTSIDE DESIGN TEMP. F DEG.	−20	−10	0	+10	20
Correction Factor	0.778	0.875	1.000	1.167	1.400

[a]The multipliers in Table 5, which are high for mild climates and low for cold regions are not in error as might appear. The unit figures in Tables 2, 3, and 4 are per square foot of radiator or thousand Btu heat loss per degree-day. For equivalent buildings and heating seasons, those in warm climates have lower design heat losses and smaller radiator quantities than those in cold cities. Consequently, the *unit* figure in quantity of fuel per (square foot of radiator) (degree-day), is larger for warm localities than for colder regions. Since the northern cities have more radiator surface per given building and a higher seasonal degree-day total than cities in the south, the total fuel per season will be larger for the northern city.

pound coal and for other heating values of coal they must be multiplied by the ratio of 12,000 divided by the heating value of fuel used.

Example 7. A building in Marquette, Mich., has an hourly heat loss at design conditions of 240,000 Btu per hour. Based on an inside design temperature of 70 F and an outside design temperature of −20 F, what will be the estimated normal seasonal coal consumption for heating if 12,000 Btu per pound fuel is burned at a 50 per cent seasonal efficiency, and what part of the total will be used during November, December, and January?

Solution. From Table 4, U is 0.0666 lb of coal per 1000 Btu per hour heat loss. Correcting for the outside design temperature of −20 F from Table 5, the value of U is $0.778 \times 0.0666 = 0.0518$. From Table 1, D is 8745 and from the problem, N is 240.

Substituting in Equation 4:

$$F = 0.0518 \times 240 \times 8745 = 108{,}718 \text{ lb.}$$

Fuel used over any period is, according to the theory of the degree-day, proportional to the number of degree-days during the period. From Table 1, the average numbers of degree-days for November, December, and January in Marquette are 926, 1306, and 1465, a total of 3697. The yearly total is 8745, so that during these three months the estimated consumption is:

$$\frac{3697}{8745} \times 108{,}718 = 45{,}961 \text{ lb.}$$

Estimating Steam Consumption

In estimating steam consumption the efficiency is generally assumed at 100 per cent. If for low pressure steam an average heating value of 1000 Btu per pound of steam is used no correction is necessary. In comparing values from different cities, correction should be made for design temperature (see Table 5) when the unit figures are in terms of square feet of radiation but not when the values are in terms of building volume or floor space.

Where the heat loss is calculated in Btu per (hour) (*degree difference in temperature*) the simple Equation 5 may be used:

$$F = \frac{H \times 24 \times D}{1000} \tag{5}$$

where

F = pounds of steam required for estimate period.
H = calculated heat loss, Btu per (hour) (degree difference).
D = number of degree days for the period of estimation.
1000 = Btu delivered per pound of steam condensed.

In this method the number of degree-days automatically takes care of average inside and outside temperature difference. When degree days are taken from Table 1, an average inside temperature of approximately 65 F is assumed throughout the period. If an average inside temperature other than approximately 65 F is to be used, the number of degree-days should be obtained for the new base.

Example 8. An eight story building in Pittsburgh maintains daytime temperatures of 70 F but allows night temperature to drop to not lower than 60 F. Its calculated heat loss is 10,500 Btu per (hour) (*degree temperature difference*). What is the estimated average yearly steam consumption for building heating?

Solution. Since the average inside temperature is approximately 65 F, the degree-days from Table 1, based on 65 F may be used. Therefore, from Table 1, Pittsburgh has 5430 degree-days per normal season. Inserting in Equation 5

$$F = \frac{10{,}500 \times 24 \times 5430}{1{,}000} = 136{,}836 \text{ lb of steam.}$$

Consideration has been given to the difference in steam utilization of different types of buildings and Table 6 shows actual average units for these various types. These figures were obtained from operating results in 896 buildings located in all sections of the United States. Being averages, and for small groups in each type, the figures may need considerable modification to allow for local variations. It should be especially noted that the steam used for heating hot water is not included in the values given in Table 6.

Example 9. A store in Philadelphia with a heating system designed to maintain 70 F inside in 0 F weather has 250,000 cu ft of heated space. What would be the estimated average yearly steam consumption of purchased steam for heating?

TABLE 6. STEAM CONSUMPTION OF BUILDINGS WITH VARIOUS TYPES OF OCCUPANCY[a]

TYPE OF BUILDING	NO. BLDGS.	AVERAGE VOLUME HEATED SPACE 1000 CU FT	STEAM FOR HEATING	AVERAGE HOURS OF OCCUPANCY
			Lb per DD per 1000 Cu Ft	
Office	334	2160	0.685	12.1
Office and Bank	49	3000	0.577	13.1
Office and Printing	8	1895	1.230	17.7
Office and Theater	7	4950	0.412	12.9
Office and Stores or Shops	26	1615	0.617	13.2
Bank	16	806	0.786	11.7
Department Store	63	3400	0.385	11.1
Stores	73	310	0.624	10.4
Loft	63	865	0.588	10.0
Warehouse	24	2230	0.459	9.4
Hotel and Club	73	1795	0.990	22.3
Apartment or Residence	51	1425	0.962	21.8
Theater	22	1240	0.482	12.9
Garage	13	1540	0.202	21.4
Manufacturing	19	1350	0.808	9.5
Church	9	656	0.532	7.9
Hospital	4	3306	1.194	22.0
School	8	1115	0.592	11.5
Municipal or Federal	15	3215	0.587	15.6
Lodge, Gym, Hall or Auditorium	12	880	0.390	12.4
Miscellaneous	7	1387	0.479	21.4

[a]Principles of Economical Heating, *National Association of Building Owners and Managers.*

Solution. According to Table 6, a store would use 0.624 lb of steam per degree-day per 1000 cu ft heated space. From Table 1, Philadelphia has 4739 degree-days per normal year. Inserting in Equation 4:

$$F = 0.624 \times 250 \times 4739 = 739{,}284 \text{ lb of steam.}$$

Degree-Day as an Operating Unit

The degree day is also widely used as a means of comparing the efficiency of the fuel consumption of one period with another *for the same building.* Since the fuel consumption is proportional to the weather (degree-days) and since the periods to be compared may not have the same weather conditions, the comparison can be made only after the fuel consumptions have been computed on a comparable weather basis, that is, upon the actual number of degree days occurring for a given month and year in the city under consideration. Since fuel consumption is proportional to the number of degree-days, plant operators frequently compute each month the fuel burned per degree-day by the heating

plant. The resulting unit figure, by eliminating the outside temperature variable, indicates whether the operating efficiency of the plant is above or below the previous month or year.

The figures in Table 7 illustrate a typical example of a method of using the degree-day for making heating comparisons for one building for two consecutive heating seasons. The heat quantity figures inserted are pounds of steam, but a similar comparison could be made using pounds of coal, gallons of oil, or cubic feet of gas.

For such a comparison, a two-year record is often used, as shown in Table 7. The year under consideration may then be compared, month by month, with the previous year. Column 3, Consumption for Heating, would be used if the same fuel is used for heating and process steam.

TABLE 7. HEAT CONSUMPTION RECORD FOR COMPARISON

Heating Season		Col. 1	Col. 2	Col. 3	Col. 4	Col. 5	Col. 6	Col. 7
			Total Consumption	Consumption For Heating	Avg Mean Temp.	Deg Days 65 F Base	Lb/Deg Day	Lb/Deg Day/ M Cu Ft
	1942-43	Sept.	337,500	170,500	65	146	1,170	0.575
		Oct.	834,200	667,200	53	339	1,966	0.970
		Nov.	1,446,600	1,279,600	44	641	1,990	0.982
		Dec.	2,176,400	2,009,400	25	1,233	1,630	0.804
		Jan.	2,332,200	2,165,200	22	1,297	1,670	0.822
		Feb.	2,131,100	1,964,100	28	1,106	1,775	0.888
		Mar.	2,021,900	1,854,900	31	1,032	1,799	0.885
		Apr.	1,241,500	1,074,500	43	647	1,660	0.818
		May	672,500	505,500	55	303	1,670	0.822
		June	258,600	91,600	.....	50	1,830	0.905
		July	188,400	.....	.....	.....	.....	.....
		Aug.	180,100	.....	.....	.....	.....	.....
		Total	13,821,000	.....	.....	.....	.....	.....
	1943-44	Sept.	330,200	146,200	61	167	875	0.431
		Oct.	887,100	703,100	52	410	1,718	0.845
		Nov.	1,525,200	1,341,200	39	812	1,653	0.815
		Dec.	2,045,500	1,861,500	28	1,120	1,660	0.817
		Jan.	1,933,400	1,749,400	30	1,044	1,670	0.825
		Feb.	1,990,200	1,806,200	30	1,111	1,624	0.800
		Mar.	1,984,100	1,800,100	31	1,021	1,760	0.868

If, for example, the heat consumption in March, 1943, is compared with that in March, 1944, it will be found that in the latter the steam consumption is 1799 − 1760 = 39 lb less which is a decrease of 2.2 per cent.

Some reasonable figure must be assumed for the process requirement and should be deducted from the amount shown in column 2. This would leave in column 3 only the fuel chargeable to heating. The degree-day values in column 5 are obtainable from the local Weather Bureau. Figures in column 6 are obtained by dividing corresponding values in column 3 by the degree days in column 5. The heating index in column 6 is, then, a figure of heat consumption, corrected for outdoor temperature, and should be relatively constant month by month. Column 7 in Table 7 may be used if the heat consumption is to be compared on a building volume basis with average values shown in Table 6.

MAXIMUM DEMANDS AND LOAD FACTORS

In one form of district heating rates, a portion of the charge is based upon the maximum demand of the building. The maximum demand may

be measured in several different ways. It may be taken as the instantaneous peak or as the rate of use during any specified interval. One method is to take the average of the three highest hours during the winter. These figures are available for a number of buildings in Detroit, as shown in Table 8[5].

These maximum demands were measured by an attachment on the condensation meter and therefore represent the amounts of condensation passed through the meter in the highest hours, rather than the true rate at which steam is supplied. There might be slight differences in these two quantities due to time lag and to storage of condensate in the system, but wherever this has been investigated it has been found to be negligible.

The load factor of a building is the ratio of the average load to the maximum load and is an index of the utilization. Thus, in Table 8, the theaters, operating for short hours, have a load factor of 0.126 as compared with the figure of 0.318 for clubs and lodges.

TABLE 8. BUILDING LOAD FACTORS AND DEMANDS OF SOME DETROIT BUILDINGS

BUILDING CLASSIFICATION	LOAD FACTOR	LB OF DEMAND PER (HOUR) (SQ FT OF EQUIVALENT INSTALLED RADIATOR SURFACE)
Clubs and Lodges	0.318	0.184
Hotels	0.316	0.207
Printing	0.287	0.217
Offices	0.263	0.209
Apartments	0.255	0.225
Retail Stores	0.238	0.182
Auto Sales and Service	0.223	0.248
Banks	0.203	0.158
Churches	0.158	0.152
Department Stores	0.138	0.145
Theaters	0.126	0.151

SEASONAL EFFICIENCY

The task of predicting fuel consumption within reasonably accurate limits is a simple one where sufficient experience data are available for the fuel in question. Such data can be analyzed to the point where average unit factors can be determined and expressed in such terms as, for example, cubic feet of gas actually burned per (square foot of calculated steam radiator surface) (degree-day). The unit U can be inserted directly in Equation 4 without reference to efficiency. Such experience factors are available for gas (see Table 2) and for district steam (Table 6), but not for coal or oil.

Since values of U are not available for oil or coal, an assumed seasonal efficiency E must be used. Selection of a value for this E must be made with caution, for its use implies a meaning not commonly associated with the word efficiency and consequently is frequently misleading.

The input of heat to a building consists not only of the energy in the fuel but that from occupants, the sun, appliances, processes, and all other sources. In many cases these make up, over a period, an important percentage of the total heat required, and if they are not taken into account a calculation of *efficiency* can show a figure over 100 per cent.

For this and other reasons the actual *seasonal efficiency* is a difficult thing to determine. Published data are widely scattered and insufficient.

From the available published material it is found that the seasonal efficiency varies over a wide range, depending on the fuel used, and it varies widely even for a given fuel. For example, in a recent survey of 30 houses in one locality there was found a variation of from 45 to 75 per cent in the utilization *efficiency* depending on the fuel [6].

REFERENCES

1—Graphical Method of Calculating Heat Losses, by Paul D. Close (A.S.H.V.E. TRANSACTIONS, Vol. 49, 1943, p. 345).

2—Standard Gravity Code for the Design and Installation of Gravity Warm Air Heating Systems (11th edition), and the Technical Code for the Design and Installation of Mechanical Warm Air Heating Systems (*National Warm Air Heating and Air Conditioning Association*).

3—See Industrial Gas Series, House Heating (*third edition*), published by the *American Gas Association.*

4—Report of Commercial Relations Committee, *Proceedings, National District Heating Association*, 1932.

5—The Heat Requirements of Buildings, by J. H. Walker and G. H. Tuttle (A.S.H.V.E. TRANSACTIONS, Vol. 41, 1935, p. 171).

6—Heat Losses and Efficiencies of Fuels in Residential Heating, by R. A. Sherman and R. C. Cross (A.S.H.V.E. TRANSACTIONS, Vol. 43, 1937, p. 185).

Chapter 21

GRAVITY WARM AIR SYSTEMS

Warm Air Leaders, Stacks, and Registers; Return Air Grilles, Ducts, and Shoe Connections; Outline of Design Procedure

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WARM air heating systems of the *gravity* type are described in this chapter [1]. In these systems the motive head producing flow depends upon the difference in weight between the heated air leaving the top of the casing and the cooled air entering the bottom of the casing, while in the mechanical type a fan may supply all or part of the motive head.

A gravity warm-air furnace heating plant consists of a fuel-burning furnace or heater, enclosed in a casing of sheet metal, which is placed in the basement of the building. The heated air, taken from the top or sides near the top of the furnace casing, is distributed to the various rooms of the building through sheet metal warm-air pipes. The warm-air pipes in the basement are known as leaders, and the vertical warm-air pipes which are run in the inside partitions of the building are called stacks. The heated air is finally discharged into the rooms through registers which are set in register boxes placed either in the floor or in the side wall, usually at or near the baseboard. A sectional view of a typical plant showing good installation practice is given in Fig. 1.

The air supply to the furnace is usually taken entirely from inside the building through one or more recirculating ducts, although in some cases an outside air supply duct is provided.

WARM AIR LEADERS, STACKS, AND REGISTERS

In a gravity circulating warm-air furnace system, the size of the leader pipe to a given room depends upon the length of the leader and the temperature of the warm air entering the room at the register. For most successful operation, the furnace should be centrally located with respect to register and stack positions so that the leaders will be of uniform length and as short as possible, in which case the frictional resistance to air flow and the temperature loss from the ducts will be about the same for all runs.

In the Standard Code for Installation of Gravity Warm Air Heating Systems, the design was originally based on the heat carrying capacities per square inch of leader pipe area with register air temperatures of 175 F. In a recent revision of the entire design procedure, as shown in the section entitled *Outline of Design Procedure*, the carrying capacities of leader pipes have been expressed directly in terms of Btu per hour.

In general it is advisable to use two or more leader pipes to rooms requiring more than the capacity of a 12 in. round pipe. The tops of all sizes of leader pipes should be cut into the furnace bonnet at the same elevation, and from this point there should be a uniform upgrade of at least 1 in. per foot of run. Leaders over 12 ft in length, or having a large number of elbow fittings should be avoided if possible. In cases where such leaders are necessary, it is recommended that smooth transition fittings be used, and that duct insulation be applied. Asbestos paper, unless of the corrugated type, should not be considered as insulation. To assist in balancing the air distribution of the system, a damper should be placed in each leader pipe except one, this latter leader preferably being connected to a room heated at all times, such as a living room.

In a gravity circulating system, the ratio of stack to leader area is quite important, although little is gained by providing wall stacks with areas in excess of 75 per cent of their connected leader pipe area. In most cases a 3¼ in. × 12 in. stack is the largest which can be installed in normal wall construction. Hence, any room having a heat loss much in excess of 9000 Btu per hour, will require two or more stacks, or one oversized stack built into a 6 in. studding space, providing the design register temperature is to be retained at the value of 175 F as recommended.

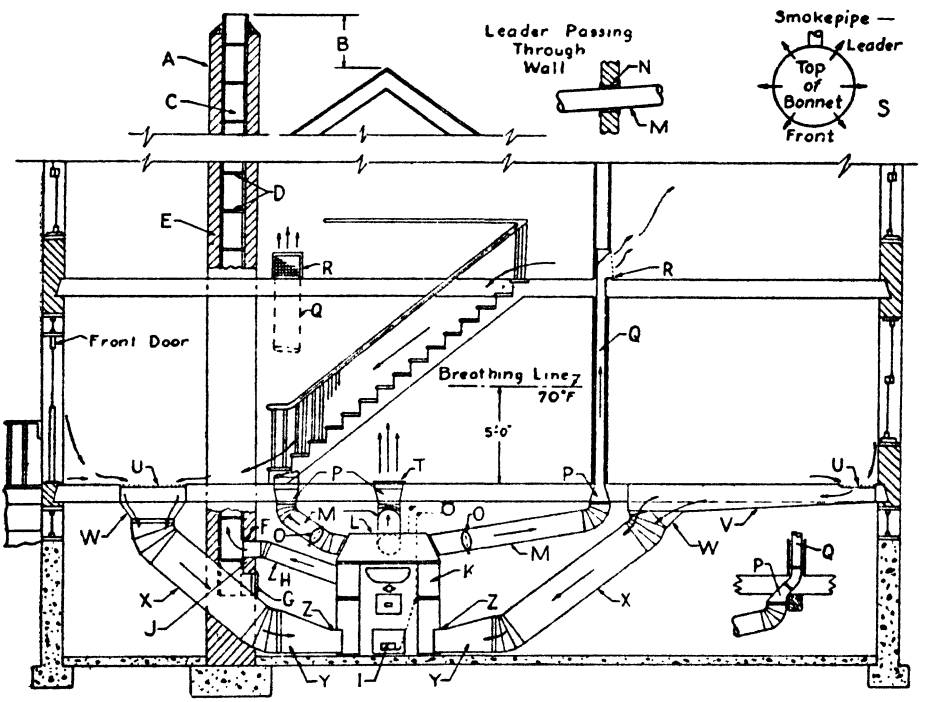


FIG. 1. A SECTIONAL VIEW OF A TYPICAL PLANT SHOWING GOOD INSTALLATION PRACTICE[a]

A. House chimney, no bends nor offsets.
B. Top of chimney at least 2 ft above ridge of roof.
C. Flue lining, fireclay.
D. All joints air tight.
E. At least 8 in. brick.
F. No other connection beside that to furnace.
G. Cleanout frame and door, airtight.
H. Smoke pipe, end flush with inner surface of flue.
I. Draft door.
J. Use flue thimble.
K. Casing body.
L. Casing hood or bonnet, top of all leader collars on same level.
M. Round leader, pitch 1 in. per foot.
N. Sleeve with air space around leader where passing through wall.
O. Dampers in all leaders, except one.
P. Transition fittings.
Q. Rectangular wall stack.
R. Baseboard register.
S. Distribute pipes equally around bonnet.
T. Floor register.
U. Return air face.
V. Panning under joist.
W. Transition collar.
X. Round return pipe.
Y. Transition shoe.
Z. Top of shoe at casing not above grate level.

[a]From *N.W.A.H.&A.C. Assn.* Standard Code Application Manual.

Registers used for discharging warm air into rooms should have a net area not less than the area of the leader pipe to which the register is attached. First story registers should be connected through boot and register box extensions having areas at least equal to leader areas. Upper story registers should be of the same width as the wall stack, and should be placed either in the baseboard or sidewall, preferably without offsets.

First story registers may be of the baseboard or floor type, with the former location preferred. High sidewall registers in gravity systems deliver more warm air into the room than do baseboard registers, but most of the additional air merely results in high temperatures at the ceiling.

RETURN AIR GRILLES, DUCTS, AND SHOE CONNECTIONS

The placement and number of return grilles will depend upon the size, details, and exposure of the house. Small compactly built houses may be adequately served by a single return grille effectively placed in the central hall. It is usually desirable to have two or more returns, provided that in two-story residences one return is placed to effectively receive the return air at the foot of the stairs. A return air connection must be carried to any room whose floor level is below that of adjacent rooms.

The return air grilles should have free areas at least equal to the ducts to which they connect and should be installed in the floor, or in the baseboard with the top edge of the grille not more than about 14 in. above the floor line. Frictional resistance in the return air system is as detrimental as is resistance in the warm-air system, so that care should be exercised in locating return air grilles which require long return ducts.

Where a divided system of two or more returns is used, the grilles must be placed to serve the maximum area of cold wall or windows. Thus, in rooms having only small windows the grille can be brought as close to the furnace as possible, but if the room has large window exposure the grille should be located near the exposure. The frictional resistance of the long ducts used in parallel with short return ducts must be reduced to compensate for the length. Return ducts from upstairs rooms may be necessary in spaces which are closed off from the rest of the house or which have much outdoor exposure. Return grilles on different floor levels should not be connected to the same vertical return duct.

The ducts through which air is returned to the furnace should be designed to minimize resistance to air flow. They should be of ample area, in excess of the total area of warm-air pipes, and should be streamlined. Horizontal ducts should pitch at least ½ in. per foot downward toward the furnace, avoiding fittings which would require lifting of the return air after the duct has passed under some obstacle.

Ducts returning air to the furnace should avoid heat sources which tend to reheat the return air. If the duct must be run over the top of the furnace, or above the vent pipe from the furnace, insulation should be interposed between the heat source and the duct.

Circulation of air is facilitated if the air can slide down a pipe inclined at approximately 45 deg and into a furnace shoe connection having a cross-sectional area equal to that of the pipe. The top of the return shoe should enter the casing below the level of the grate in the case of a coal furnace, and not more than 14 in. above the floor in the case of oil or gas furnaces. In order to accomplish this the shoe is made wide.

OUTLINE OF DESIGN PROCEDURE

The data underlying the design procedure are given in detail in a circular[2] issued by the University of Illinois. In this procedure the design of the warm-air duct system is considered as an entire unit, so that for a given heat loss the sizes of leaders, stacks, boots, stackheads, and registers are

all correlated. Similarly in the case of return ducts, the selection specifies a complete unit consisting of return grille, return duct, and shoe connection.

Recommended Standard Sizes

For the purpose of simplification and standardization, selected combinations of commercial sizes of warm air pipes, return air pipes, ducts, grilles, fittings, and registers are designated as Combination Numbers. The numbers assigned and the combinations selected as standard are listed in the following tables [3].

Table 1—Combination Numbers 1 to 5—First Story Warm Air Ducts and Registers.

Table 2—Combination Numbers 11 to 16—Second Story Warm Air Ducts, Single Wall Stacks, Fittings, and Registers.

Table 3—Combination Numbers 21 to 24—Second Story Warm Air Ducts, Double Wall Stacks, Fittings, and Registers.

Table 4—Combination Numbers 31 to 38—Return Air Ducts, Fittings, and Grilles.

TABLE 1. FIRST STORY WARM-AIR DUCTS[a]

COMBINATION NO.	LEADER PIPE DIAMETER, IN.	REGISTER SIZE, IN.		
		Floor	Baseboard	
			Size	Extension
1	8	8 x 10	10 x 8	2¼
2	9	9 x 12	12 x 8	2¼
3	10	10 x 12	12 x 9	3¼
4	12	12 x 14	13 x 11	5¼
5	14	14 x 16	.....	.....

[a]When the calculations indicate a requirement for a given room greater than Combination No. 4, two or more smaller units totalling the required capacity are recommended.

TABLE 2. SECOND STORY WARM-AIR DUCTS—SINGLE WALL STACKS AND FITTINGS

COMBINATION NO.	LEADER PIPE DIAMETER, IN.	STACK [b] SIZE IN.	REGISTER SIZE, IN.			
			Floor	Baseboard		Sidewall
				Size	Extension	
11	8	10 x 3¼	8 x 10	10 x 8	2¼	10 x 8
12	9	12 x 3¼	9 x 12	12 x 8	2¼	12 x 8
14	10	14 x 3¼	10 x 12	12 x 8	2¼	12 x 8
15	12	12 x 5¼	.....	12 x 9	3¼	.....
16	12	14 x 5¼	.....	13 x 11	5¼	.....

[b]Recommended stack sizes. Tables may also be applied to 3 in. and 3½ in. stack depths.

TABLE 3. SECOND STORY WARM-AIR DUCTS—DOUBLE WALL STACKS AND FITTINGS

COMBINATION NO.	LEADER PIPE DIAMETER, IN.	STACK SIZE, IN.		REGISTER SIZE, IN.			
		Internal	External	Floor	Baseboard		Sidewall
					Size	Extension	
21	8	2½[c] x 10	3⅛[c] x 10⅝	8 x 10	10 x 8	2¼	10 x 8
22	8	3 x 10	3⅝ x 10⅝	8 x 10	10 x 8	2¼	10 x 8
23	9	2½[c] x 12	3⅛[c] x 12⅝	9 x 12	12 x 8	2¼	12 x 8
24	9	3 x 12	3⅝ x 12⅝	9 x 12	12 x 8	2¼	12 x 8

[c]Commercial sizes vary ⅛ in. from values shown.

TABLE 4. RETURN AIR DUCTS

COMBINATION NO.	DUCT DIA. IN.	AREA AT SHOE CONNECTION, SQ IN.	METAL GRILLE SIZES Choose One A	B	C	WHEN JOIST LINING IS USED[d] No. of Joists Lined	Minimum[e] Depth, In.	WHEN DUCT IS USED Choose One	
31	10			8 x 14	10 x 12	1	7	14 x 6	12 x 8
32	12		6 x 30	8 x 24	12 x 14	1	9	22 x 6	16 x 8
33	14	170	8 x 30	10 x 24	14 x 16	1	12	28 x 6	22 x 8
34	16	220	10 x 30	12 x 24		2	8	28 x 8	22 x 10
35	18	280	12 x 30	14 x 24		2	10	36 x 8	28 x 10
36	20	340	14 x 30	18 x 24		2	12.5	36 x 10	30 x 12
37	22	420	18 x 30			2	15.0	42 x 10	36 x 12
38	24	500	20 x 30			2	18.0	42 x 12	36 x 14

[d]Based on 14 in. space between joists.

[e]Use full depth of joist except when joist depth is less than minimum depth required, *when pan must be used.*

The selected types of boots are shown in Fig. 2 and their resistances expressed in equivalent elbows are shown in Table 5. It is essential that free areas be maintained throughout fittings.

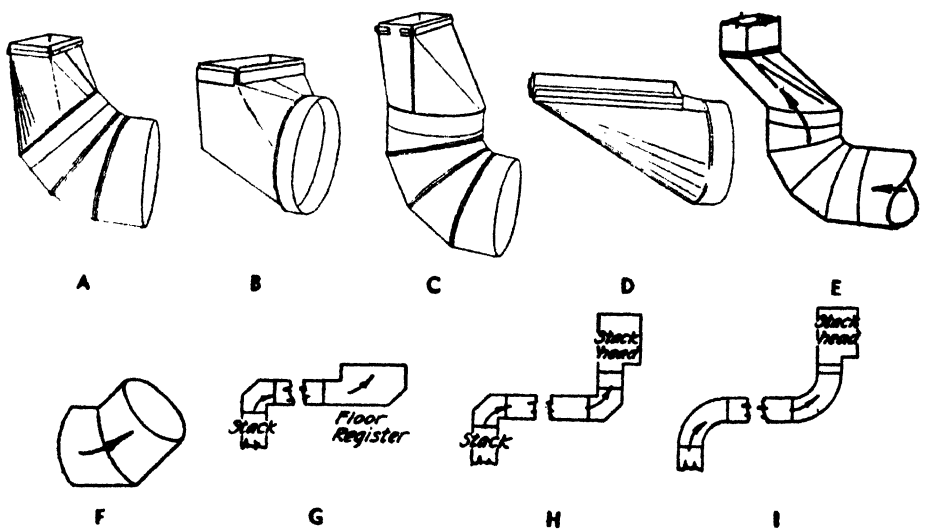


FIG. 2. TYPICAL WARM AIR BOOTS

TABLE 5. RESISTANCES OF WARM AIR BOOT COMBINATIONS EXPRESSED IN ELBOW EQUIVALENTS

WARM AIR BOOT	NAME OF COMBINATION	EQUIVALENT NO. OF 90-DEG ELBOWS
A	45-Deg Angle Boot and 45-Deg Elbow	1
B	90-Deg Angle Boot	1
C	Universal Boot and 90-Deg Elbow	1
D	End Boot	2
E	Offset Boot	2½
F	45-Deg Angle	½
G	Floor Register—Second Story	3
H	Offset	3
I	Offset	2

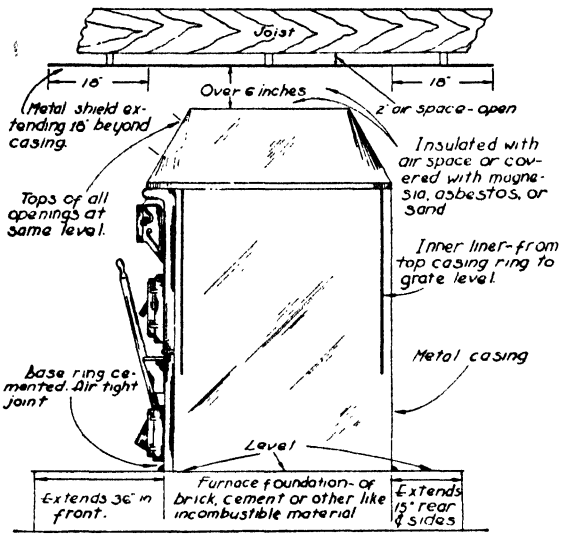


FIG. 3. DETAILS OF FURNACE BONNET, CASING, AND FOUNDATION (FROM GRAVITY CODE AND MANUAL)

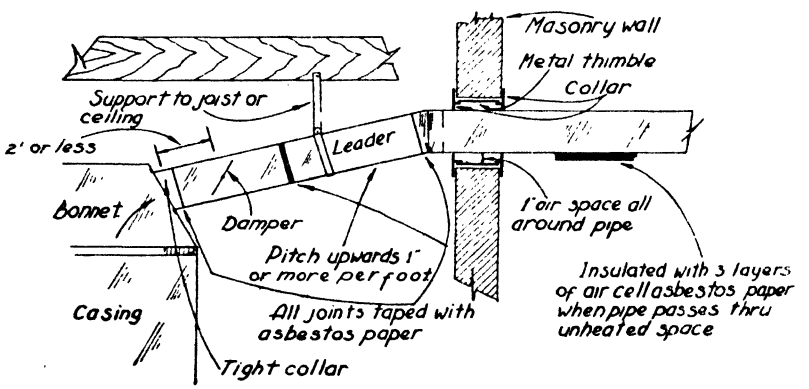


FIG. 4. DETAILS OF BONNET AND LEADER OF GRAVITY WARM-AIR FURNACE (FROM GRAVITY CODE AND MANUAL)

Figs. 3 and 4 show recommended practice as given in the *N.W.A.H. &A.C. Assn.* Gravity Code and Manual. For construction, design features, and ratings of gravity furnaces see Chapter 18.

Carrying Capacity

The Btu carrying capacities of the selected warm air and return air combinations are shown in Tables 6, 7 and 8:

Table 6—Combination Numbers 1 to 5—Warm Air Carrying Capacities to first story registers with 1 to 5 elbows and with leaders 4 to 24 ft long.

Table 7—Combination Numbers 11 to 16 and 21 to 24—Warm Air Carrying Capacities to second story registers with 1 to 5 elbows with leaders 4 to 24 ft long.

Table 8—Combination Numbers 31 to 38—Return Air Carrying Capacities for types *A*, *B*, *C*, *D*, *E*, and *F* return combinations.

TABLE 6. WARM AIR CARRYING CAPACITY, BTU DELIVERED, FIRST STORY REGISTERS[a]

Length of Leader Pipe—in Feet

COMBINATION NO.	NO. OF ELBOWS	4 FT	6 FT	8 FT	10 FT	12 FT	14 FT	16 FT	18 FT	20 FT	22 FT	24 FT
1		6,020	5,850	5,680	5,510	5,340	5,170	5,000	4,830	4,660	4,490	4,320
2		7,620	7,400	7,180	6,970	6,760	6,540	6,320	6,110	5,890	5,680	5,460
3	1	9,400	9,140	8,870	8,600	8,340	8,070	7,810	7,540	7,270	7,010	6,740
4		13,350	12,970	12,590	12,210	11,830	11,450	11,080	10,700	10,320	9,950	9,560
5		17,520	17,020	16,530	16,040	15,550	15,050	14,550	14,050	13,560	13,060	12,560
1		5,850	5,660	5,490	5,330	5,160	5,000	4,840	4,670	4,510	4,340	4,180
2		7,360	7,150	6,940	6,730	6,520	6,320	6,110	5,910	5,700	5,500	5,290
3	2	9,090	8,840	8,580	8,320	8,060	7,800	7,550	7,290	7,040	6,780	6,520
4		12,910	12,540	12,170	11,800	11,430	11,060	10,690	10,320	9,950	9,580	9,210
5		16,940	16,450	15,990	15,500	15,040	14,550	14,080	13,600	13,120	12,650	12,150
1		5,620	5,460	5,310	5,150	4,990	4,830	4,670	4,510	4,350	4,190	4,030
2		7,120	6,910	6,710	6,510	6,310	6,110	5,900	5,700	5,500	5,300	5,100
3	3	8,780	8,530	8,280	8,030	7,780	7,530	7,290	7,040	6,800	6,550	6,300
4		12,450	12,100	11,750	11,400	11,050	10,700	10,350	10,000	9,650	9,300	8,950
5		16,360	15,900	15,440	14,970	14,510	14,050	13,600	13,130	12,660	12,200	11,750
1		5,420	5,260	5,110	4,960	4,800	4,650	4,500	4,350	4,190	4,040	3,890
2		6,860	6,660	6,460	6,270	6,080	5,890	5,690	5,500	5,300	5,110	4,910
3	4	8,460	8,200	7,980	7,740	7,500	7,260	7,020	6,780	6,550	6,310	6,070
4		12,010	11,670	11,330	10,990	10,650	10,310	9,970	9,630	9,290	8,950	8,610
5		15,770	15,320	14,880	14,420	13,990	13,540	13,100	12,650	12,200	11,750	11,310
1		5,240	5,090	4,940	4,790	4,640	4,500	4,350	4,200	4,050	3,910	3,760
2		6,630	6,440	6,250	6,060	5,880	5,690	5,500	5,320	5,130	4,940	4,750
3	5	8,180	7,950	7,720	7,490	7,260	7,030	6,800	6,560	6,330	6,100	5,860
4		11,610	11,290	10,950	10,620	10,300	9,970	9,640	9,320	8,990	8,660	8,320
5		15,250	14,800	14,380	13,950	13,520	13,090	12,650	12,230	11,800	11,370	10,940

[a]Additional values for 6 and 7 elbows are given in original Manual.

TABLE 7. WARM AIR CARRYING CAPACITY, BTU DELIVERED, SECOND STORY REGISTERS[a]

Length of Leader Pipe—in Feet

COMBINATION NO. [b,c]	NO. OF ELBOWS	4 FT	6 FT	8 FT	10 FT	12 FT	14 FT	16 FT	18 FT	20 FT	22 FT	24 FT
11-22		8,370	8,140	7,900	7,670	7,430	7,190	6,950	6,710	6,470	6,240	6,000
12-24		10,040	9,760	9,470	9,190	8,900	8,620	8,330	8,050	7,770	7,480	7,200
14	1	11,710	11,380	11,050	10,720	10,390	10,060	9,720	9,390	9,060	8,730	8,400
15		16,200	15,750	15,300	14,840	14,380	13,920	13,460	13,000	12,550	12,100	11,640
16		18,920	18,390	17,850	17,310	16,780	16,240	15,710	15,180	14,640	14,100	13,570
11-22		7,940	7,720	7,500	7,280	7,050	6,830	6,600	6,370	6,150	5,930	5,700
12-24		9,540	9,270	9,000	8,730	8,460	8,190	7,920	7,650	7,380	7,110	6,840
14	2	11,120	10,810	10,500	10,180	9,870	9,550	9,230	8,920	8,610	8,290	7,980
15		15,400	14,970	14,530	14,100	13,670	13,230	12,800	12,360	11,930	11,500	11,070
16		17,980	17,470	16,960	16,450	15,950	15,430	14,830	14,420	13,910	13,400	12,890
11-22		7,530	7,320	7,110	6,900	6,680	6,470	6,250	6,040	5,830	5,620	5,400
12-24		9,030	8,780	8,520	8,270	8,010	7,750	7,500	7,240	6,990	6,730	6,470
14	3	10,530	10,240	9,940	9,650	9,350	9,050	8,750	8,450	8,160	7,860	7,560
15		14,580	14,180	13,780	13,370	12,950	12,530	12,120	11,710	11,300	10,890	10,480
16		17,040	16,550	16,070	15,580	15,110	14,620	14,140	13,660	13,180	12,700	12,210
11-22		7,120	6,920	6,720	6,520	6,310	6,110	5,900	5,700	5,500	5,300	5,100
12-24		8,530	8,290	8,050	7,810	7,570	7,330	7,080	6,840	6,600	6,360	6,120
14	4	9,950	9,670	9,390	9,110	8,830	8,550	8,260	7,980	7,700	7,420	7,140
15		13,780	13,390	13,000	12,610	12,220	11,830	11,440	11,050	10,670	10,280	9,890
16		16,080	15,620	15,170	14,710	14,260	13,810	13,350	12,900	12,440	11,980	11,530
11-22		6,700	6,510	6,320	6,130	5,940	5,750	5,560	5,370	5,180	4,990	4,800
12-24		8,040	7,810	7,580	7,350	7,130	6,900	6,670	6,440	6,220	5,990	5,760
14	5	9,370	9,110	8,850	8,580	8,310	8,050	7,780	7,510	7,250	6,980	6,720
15		12,970	12,600	12,240	11,870	11,500	11,140	10,770	10,400	10,040	9,680	9,310
16		15,140	14,710	14,280	13,850	13,420	13,000	12,570	12,140	11,710	11,280	10,850

[a]When floor registers are used, see Fig. 2.

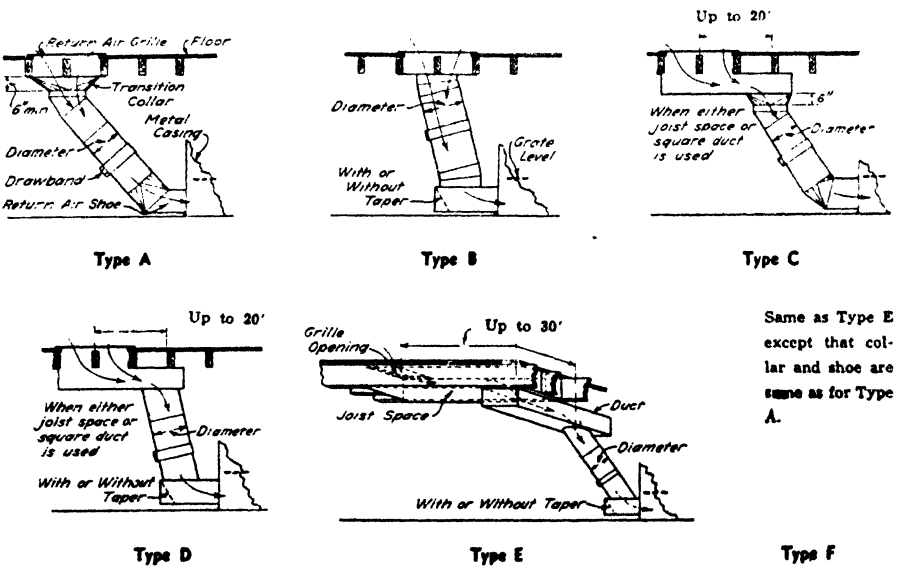
[b]No. 21 for Btu values multiply 11-22 values by 0.83.

[c]No. 23 for Btu values multiply 12-24 values by 0.83.

TABLE 8. RETURN AIR—CARRYING CAPACITY—BTU SERVICED

RETURN AIR COMBINATION NO.	DUCT DIA IN.	TYPE A BTU PER HR	TYPES B AND C BTU PER HR	TYPE D BTU PER HR	TYPE E BTU PER HR	TYPE F BTU PER HR	RETURN AIR COMBINATION NO.
31	10	11,300	9,500	7,800	5,000	7,800	31
32	12	16,300	13,700	11,300	7,200	11,300	32
33	14	22,200	18,700	15,300	9,800	15,300	33
34	16	29,000	24,400	20,000	12,800	20,000	34
35	18	36,700	30,800	25,300	16,200	25,300	35
36	20	45,300	38,000	31,300	20,000	31,300	36
37	22	54,800	46,000	37,800	24,100	37,800	37
38	24	65,200	54,800	45,000	28,700	45,000	38

The selected types of return air ducts and fittings are shown in Fig. 5.



Note: For Types C, D, E, and F return-air duct systems, reduce the carrying capacities shown in Table 8 by 1 per cent for each 4 ft additional length in the horizontal run.

FIG. 5. TYPICAL ARRANGEMENTS OF RETURN-AIR DUCT SYSTEMS

Design Procedure

The steps to be taken in designing a gravity warm air duct system are:

1. Calculate the heat loss from each room as explained in Chapters 6, 8 and 14.

2. Prepare a layout showing (*a*) furnace, (*b*) chimney connection, (*c*) warm air registers (whether floor, baseboard or wall), (*d*) return air grilles.

3. Indicate on each warm air run (using symbols shown in Fig. 6): (*a*) whether the room to be heated is on the first or second story, (*b*) the approximate length of leader pipe in the basement, (*c*) the number of right angle elbows required, including the elbow at the boot connection (see Fig. 2), (*d*) whether the register is to be located in the floor, in the baseboard, or in the wall.

4. Show the number and proposed locations of return air grilles and the type of return air system (see Fig. 5).

5. From Table 6, for first story, or from Table 7 for second story, select the combination number for the warm air system which will supply the heat required to each room, with the number of elbows and length of leader pipe previously determined. Then, using the combination number as found, read directly in Tables 1, 2, or 3 the leader, stack, and register sizes required.

6. From Table 8 select the combination number for the return air system to correspond with the Btu serviced and the type of return air system. Then from Table 4 select the duct and grille sizes, etc., corresponding to the same combination number.

7. Select a furnace having a register delivery, in Btu per hour, equal to the total heat loss from the structure.

Design Examples

Examples 1 and 2 will illustrate the use of the tables in selecting warm air and return system sizes.

Example 1. For a room which has a heat loss of 22,500 Btu per hour select the size of first story warm air system. There are three elbows and the leader is approximately 10 ft long.

Solution: Since 22,500 Btu is beyond the capacities shown in Table 6, it is necessary to select two units of 11,250 each. From Table 6 in 10 ft leader column and in section for three elbows find 11,400 as nearest capacity which corresponds to Combination Number 4 in first column. Refer to Combination Number 4 in Table 1 and find that the leader should be 12 in. in diameter and should be used with a 12 x 14 in. floor register or a 13 x 11 in. baseboard register with a 5¼ in. extension.

Example 2. What is the size of a return system of Type D which is to service 35,000 Btu per hour?

Solution: From Table 8 find Combination Number 37 which will service 37,800 Btu per hour. Refer to Table 4 to find that Combination Number 37 will require a 22-in. diameter duct, a shoe area of 420 sq in., a metal grille 18 x 30 in., a duct 42 x 10 in. or 36 x 12 in. If joist lining is used the minimum depth should be 15 in. for two 2-joist spaces 14 in. wide, or 10 in. for three joist spaces.

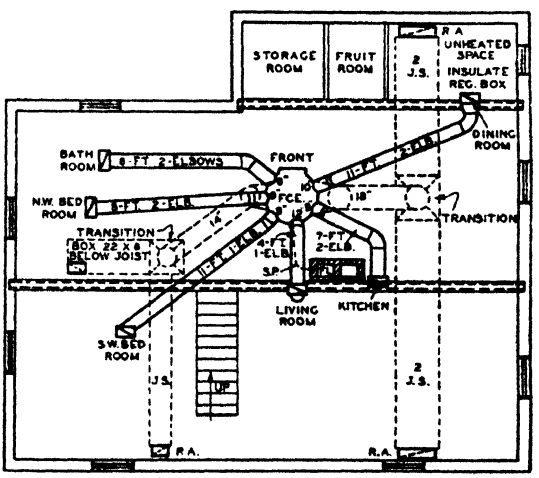


FIG. 6. TYPICAL BASEMENT LINE DRAWING

REFERENCES

[1]—The engineering data were obtained from University of Illinois, *Engineering Experiment Station Bulletins* Nos. 141, 188, 189 and 246; Warm Air Furnaces and Heating Systems, by A. C. Willard, A. P. Kratz, V. S. Day, and S. Konso. See also Gravity Code and Manual for Gravity Warm Air Heating Systems, published by the *National Warm Air Heating and Air Conditioning Association.*

[2]—Simplified Procedure for Selecting Capacities of Duct Systems for Gravity Warm-Air Heating Plants, by A. P. Kratz and S. Konso (*University of Illinois, Engineering Experiment Station Circular* 45, Dec., 1942).

[3]—Gravity Code and Manual for Gravity Warm Air Heating Systems, Second Edition, 1945, *National Warm Air Heating and Air Conditioning Association.*

Chapter 22

MECHANICAL WARM AIR SYSTEMS

Air Distribution, Standard Combinations of Parts, Simplified Design of Heating System, Automatic Controls, Cooling Methods, Procedure for Larger Systems

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IN mechanical warm air or fan furnace heating systems [1], the air circulation is effected by motor-driven fans instead of by the difference in weight between the heated air leaving the top of the casing and the cooled air entering the bottom, as in gravity systems described in Chapter 21. The advantages of mechanical systems, as compared with gravity systems, are:

1. The furnace need not be centrally located but may be placed in any part of the basement.

2. Basement distribution piping can be made smaller and can be so installed as to give full head room in all parts of the average basement, or be completely concealed from view where desired.

3. Circulation of air is positive, and in a properly designed system can be balanced in such a way as to give a greater uniformity of temperature distribution.

4. Humidity control is more readily attained.

5. The air may be cleaned by sprays or filters, or both.

6. The fan and duct equipment may be utilized for a complete cooling and dehumidifying system for summer, using either ice, mechanical refrigeration, or low temperature water for cooling and dehumidifying, or adsorbers for dehumidifying.

7. The use of the fan increases the volume of air which can be handled, thereby increasing the rate of heat extraction from a given amount of heating surface and insuring sufficient air volume to obtain proper distribution in a large room.

8. Ventilation air may be positively introduced and heated.

The construction features of mechanical warm air furnace units and discussions of the function and selection of the various parts, such as the furnace, casings, motors, filters and controls are included in Chapter 18.

AIR DISTRIBUTION

The conditions of comfort obtained in a room are greatly influenced by the type of register used and the locations of the supply registers and return grilles. In general it has been found that changes in the type, air velocity, and location of the supply register affect the room conditions much more than the changes in the location of the return grilles. One method is to locate the supply register near the floor so that the warm air from the register *blankets* a cold wall, and mixes with the cold air dropping off from the exposed walls and glass. Another method is to locate the supply openings near the floor on the inside wall and the return openings near the greatest outside exposure. In any case the warm air registers should be located so that the air stream never discharges directly into space that will normally be occupied by people at rest. Tests in the Warm Air Research Residence [2] have indicated that continuous fan operation provided better results than intermittent fan operation.

Register and Grille Openings

Supply registers located in the floor require attention to keep them clean and are usually avoided. Tests conducted in the Warm Air Research

Residence have indicated that comparable results are obtainable with either high side wall or baseboard registers, if proper registers and air velocities are selected. Baseboard registers should be of a deflecting-diffuser type which throw the air downward toward the floor and diffuse it at the same time. For baseboard registers air temperatures under 125 F and air velocities over 500 fpm should be avoided as they may cause drafts.

High side wall registers must be of such type that the air is delivered horizontally or in a slightly downward direction, and must be so located as to avoid impingement of air on ceiling or wall. Directional flow diffusing type should be used to insure best results. Register air velocities

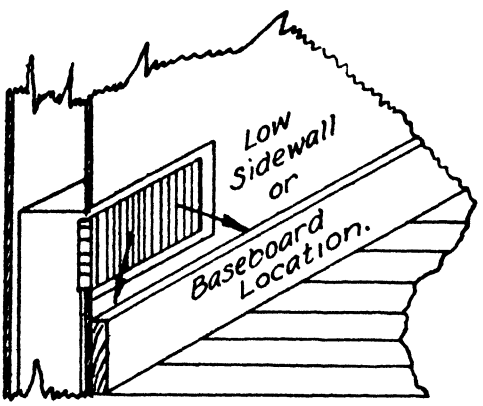

FIG. 1. RECOMMENDED TYPE OF BASEBOARD AND LOW SIDEWALL REGISTERS[a]

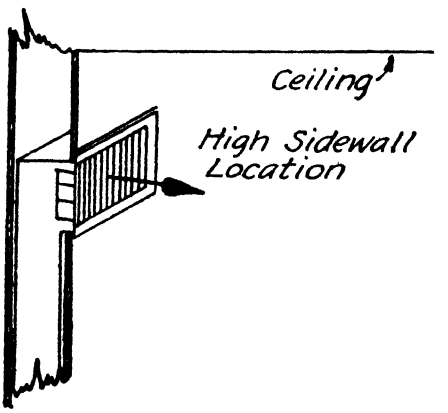

FIG. 2. RECOMMENDED TYPE OF HIGH SIDEWALL REGISTERS[b]

[a]Vertical bars with adjustable deflection, or fixed vertical bars with deflections to right and left not exceeding about 22 deg. For low sidewall location, the deflection for horizontal, multiple valve, registers should not exceed 22 deg. For baseboard locations, the deflection for horizontal, multiple valve, registers should not exceed about 10 deg.

[b]Horizontal valves, in back or front, to give downward deflections not to exceed from 15 to 22 deg.

should be such that the air stream carries to the opposite exposure. Velocities under 500 fpm are not recommended. Basic rules for the location and selection of registers are given in Section C of the Code and Manual (Textbook Section 7) of the *National Warm Air Heating and Air Conditioning Association.*

Registers should be well proportioned and decorated to harmonize with the trim. Air supply registers should be equipped with dampers and all registers should be sealed against leakage around edges. The register types shown in Figs. 1 and 2 have been recommended as standard by the *National Warm Air Heating and Air Conditioning Association.*

Velocities through registers may be reduced by the use of registers larger than the connecting ducts. Diffusers should be used to spread the air uniformly over the register face.

Return air grilles may be located in hallways, near entrance doors, under windows, in exposed corners, or inside walls, depending on location of supply registers. Baseboard returns are preferable to floor grilles.

Dampers

Suitable dampers for air direction or volume control are essential to any trunk or individual duct system. Special care must be used in the design

TABLE 1. WARM AIR DUCT SYSTEM COMBINATIONS OF PARTS SELECTED AS STANDARD

COMBINATION NO.	STACK SIZE IN.	BRANCH PIPE SIZE, IN.		REGISTER SIZE, IN. (SEE FIGS. 1 AND 2)				REQUIRED INCREASE IN WIDTH OF TRUNK DUCT, IN.
		ROUND	RECTANGULAR	BASEBOARD OR LOW SIDEWALL	HIGH SIDEWALL		FLOOR REGISTERS[a]	
					For throws less than 13 ft	For throws more than 13 ft		
1	2	3	4	5	6	7	8	9
41	10 x 3¼	6	4 x 8	10 x 6	10 x 6	10 x 4	8 x 10[a]	1
42	10 x 3¼	6	4 x 8	10 x 6	10 x 6	10 x 4	8 x 10[a]	2
43	12 x 3¼	7	5 x 8	12 x 6	12 x 6	12 x 4	9 x 12[a]	3
44	14 x 3¼	8	6 x 8	14 x 6	14 x 6	14 x 4	9 x 12[a] or longer	4
45	10 x 3¼ (2-Stacks)	9	8 x 8	(2) 10 x 6 or (1) 24 x 6	(2) 10 x 6 or (1) 24 x 6	(2) 10 x 4 or (1) 24 x 4	10 x 12[a]	6
46	12 x 3¼ (2-Stacks)	10	10 x 8	(2) 12 x 6 or (1) 30 x 6	(2) 12 x 6 or (1) 30 x 6	(2) 12 x 4 or (1) 30 x 4	12 x 14[a]	7

[a]Use these items only when the building construction or capacity requirements necessitate the use of floor registers. The sizes listed for floor registers correspond to the standard sizes for gravity warm-air systems, except for the sizes of the floor box collars. The use of standard blind boxes is suggested.

of any system to avoid turbulence and to minimize resistance. Sharp elbows, angles, and offsets should be avoided. Three types of dampers are commonly used. *Volume dampers* are used to completely cut off or reduce the flow through pipes. *Splitter dampers* are used where a branch is taken off from a main trunk. *Squeeze dampers* are used for adjusting the volume of air flow and resistance through a given duct. It is essential that a damper with positive locking device be provided for each main or duct branch. Labels placed on ducts should indicate the room being served. Damper positions should be marked for summer and winter operation, and to avoid tampering.

Ducts

The ducts may be either round or rectangular in cross section. The radii of elbows should preferably be not less than one and one-half times the pipe diameter for round pipes, or the equivalent round pipe size in the case of rectangular ducts. Warm air ducts passing through cold spaces, or where located in exposed walls, should have ½ to 2 in. of insulation.

Special attention should be given to the problem of noise elimination. The metal duct connection to and from the furnace casing and fan housing should be broken by strips of canvas. Motors and mountings must be carefully selected for quiet operation. Electrical conduit and water piping must not be fastened to, nor make contact with fan housing. Installation of a fan directly under a cold air grille is usually not recommended.

STANDARD COMBINATIONS OF PARTS

The combinations of parts selected as standard by the *National Warm Air Heating and Air Conditioning Association* are shown in Tables 1 and 2. A method for selecting these combinations is indicated in the following section *Simplified Method of Designing Domestic Forced-Air Systems.*

TABLE 2. RETURN-AIR DUCT SYSTEM COMBINATIONS OF PARTS SELECTED AS STANDARD

COMBINATION NO.	RETURN-AIR INTAKE SIZE, IN.		RISER SIZE, IN. WHERE STACK IS USED IN STUD SPACE	BRANCH PIPE SIZE, IN.		WHEN JOIST LINING IS USED[b] NUMBER OF JOIST SPACES LINED AND MINIMUM DEPTH OF SPACE REQUIRED	REQUIRED INCREASE IN WIDTH OF TRUNK DUCT (FOR 8 IN. DEPTH OF DUCT), IN.
	BASEBOARD	FLOOR[a]		ROUND	RECTANGULAR		
1	2	3	4	5	6	7	8
51	10 x 6	6 x 10 or 4 x 14	10 x 3¼[c]	6	4 x 8	1 space of 3 in. depth	1
52	10 x 6	6 x 10 or 4 x 14	10 x 3¼[c]	6	4 x 8	1 space of 3 in. depth	2
53	12 x 6	6 x 12 or 6 x 14	12 x 3¼[d]	7	5 x 8	1 space of 4 in. depth	3
54	14 x 6	6 x 14	14 x 3¼[d]	8	6 x 8	1 space of 5 in. depth	4
55	24 x 6 or 30 x 6	6 x 30	Two stacks each 10 x 3¼[c]	9	8 x 8	1 space of 6 in. depth or 2 spaces of 3 in. depth	6
56	30 x 6	6 x 30	Two stacks 12 x 3¼[d]	10	10 x 8	1 space of 7 in. depth or 2 spaces of 4 in. depth	7
57	.....	8 x 30	.....	12	15 x 8	1 space of 9 in. depth or 2 spaces of 5 in. depth	11

[a] Use these items only when building construction, or capacities, require the use of floor intakes. The sizes listed correspond to standard sizes for gravity installations, except floor box collars. The use of standard blind boxes is suggested.

[b] Based on 14 in. space between joists. Use full depth of joist, except when joist depth is less than minimum depth required, in which case a drop pan must be used. This may occur when two or more return ducts are connected to the same joist space.

[c] If it is desired to use 14 in. x 3½ in. stud space, it makes no difference whether this space has protruding keys or not.

[d] If it is desired to use 14 in. x 3½ in. stud space, the plaster base must be smooth, without any protruding plaster keys to interfere with the flow of air.

SIMPLIFIED METHOD OF DESIGNING DOMESTIC FORCED-AIR SYSTEMS

A simplified method for selecting the combinations of branches, boots, stacks, and registers, is given in the Code and Manual (Textbook section No. 7) of the *National Warm Air Heating and Air Conditioning Association*. In this method the sizes of the branch ducts are obtained from two tables giving their Btu capacities. The proper combination of parts for each branch can be determined if the following information is available.

a. Location of room, that is, whether on first or second story.

b. Actual length of basement duct from bonnet to boot, in feet.

c. Btu loss from room to be heated.

d. Equivalent lengths in feet of all fittings and of the register. Fig. 3 shows the values of equivalent lengths of fittings commonly used for domestic systems.

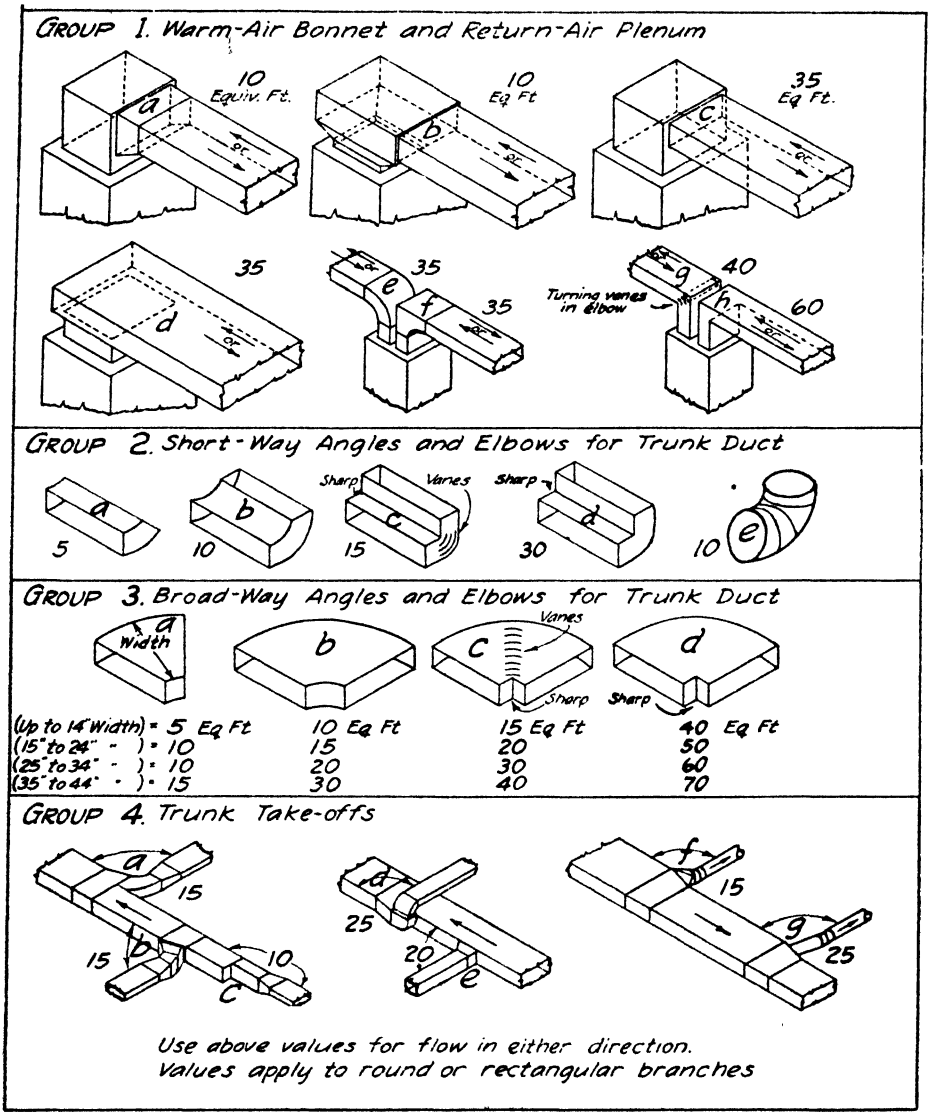

FIG. 3. EQUIVALENT LENGTH OF FITTINGS

This simplified method is applicable to structures having heat losses not in excess of approximately 150,000 Btu per hour. The capacities shown in Tables 3 and 4 are based upon the most reliable data pertaining to friction losses and temperature drops in ducts. They are also based upon a 100 deg temperature rise of the air, and a static pressure available for overcoming friction losses in the external duct system alone of 0.20 in. water gage. The use of this method assumes that the fan in the fan-furnace assembly will be capable not only of overcoming the resistance of the external duct system alone, but also the resistances imposed by the blower inlet, the filter, and the furnace casing. The combination numbers shown in the right hand column of Tables 3 and 4 correspond to those given in Tables 1 and 2. Tables 3 and 4 are also applicable for the selection of the return air branches. A depth of 8 in. has been adopted as

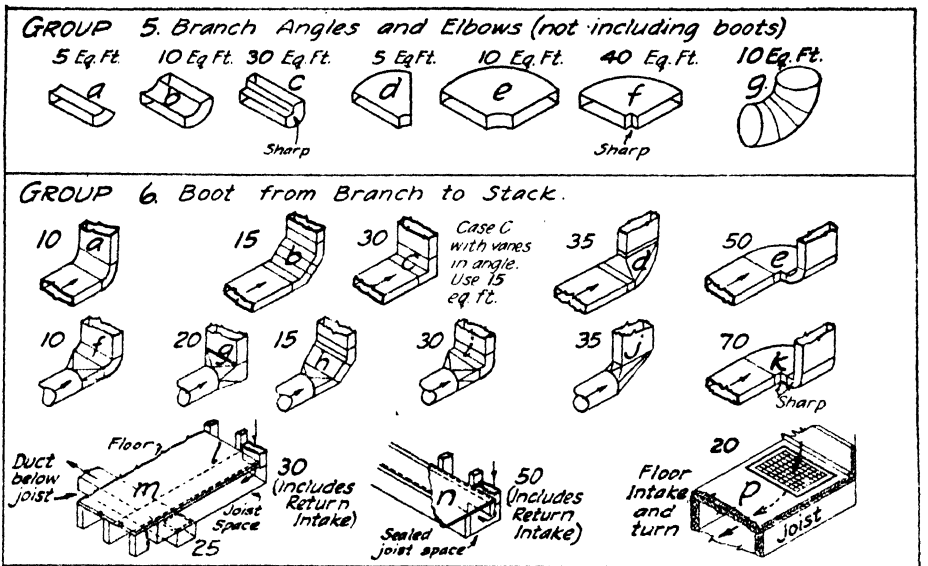

TABLE 7.
Equivalent Length for Registers.
(See diagrams at right)

Deflection Angle a	Baseboard or Low Sidewall Register	High Sidewall Register For throw of air of: less than 13 feet	over 13 feet
0°	35 Eq Ft	35 Eq. Ft.	70 Eq Ft
15°	40 " "	40 " "	80 " "
22°	45 " "	45 " "	90 " "
30°	60 " "	60 " "	115 " "
45°	115 " "	115 " "	230 " "

Notes for Table 7

a) When turning vanes are used in stackhead use 0.7 of values in columns 2 to 4

b) Values shown in 2nd and 3rd columns in Table are for 6 in height registers (Standard height). and those in 4th column are for 4 in height registers. For 5 in height registers, multiply values in Col 2 and 3 by 1.3 For 8 in. height registers, multiply values in Col. 2 and 3 by 0.8

For 2-way deflection registers, add the vertical and horizontal deflection angles together and multiply by 0.7. Select closest angle "a" in Col. 1 of Table 7

FIG. 3. EQUIVALENT LENGTH OF FITTINGS (Continued)

the standard for the trunk ducts. The width of a trunk duct serving two branches is determined by adding to the width of the remote branch the value shown in column 9 of Table 1, or column 8 of Table 2.

AUTOMATIC CONTROLS

Air stratification, high bonnet temperatures, excessive flue gas temperatures, and heat overrun or lag in a properly designed system can be largely eliminated through proper care in the planning and installation of the control system [8]; desirable controls usually employed are:

1. A *thermostat* located in a living room where maximum fluctuation in temperature can be expected, in order to secure frequent operation of fans, drafts, and burners. The thermostat location should not be on an outside wall, in a bed room, bath room or

TABLE 3. CAPACITY TABLES FOR WARM-AIR AND RETURN-AIR BRANCHES[a,b]

FIRST STORY

FOR UNINSULATED METAL DUCTS	ACTUAL LENGTH (FROM BONNET TO BOOT) OR, (FROM RETURN PLENUM TO BOOT) IN FEET								WARM AIR COMBINATION NO.	RETURN AIR COMBINATION NO.
	1 TO 7 FT	8 TO 12 FT	13 TO 17 FT	18 TO 24 FT	25 TO 34 FT	35 TO 44 FT	45 TO 54 FT	55 TO 64 FT		
	COL. A	COL. B	COL. C	COL. D	COL. E	COL. F	COL. G	COL. H		
Section A.	7200	6700	6100	5600	4800	4100	3500	3000	41	51
	12500	11700	10800	9900	8500	7400	6400	5500	42	52
40 to 69	16000	15000	14000	13000	11300	9900	8700	7700	43	53
Equivalent	19100	18000	17000	16000	14200	12500	11000	9600	44	54
Ft for										
Fittings	25000	23400	21600	19800	17000	14800	12800	11000	45[c]	55
and	32000	30000	28000	26000	22600	19800	17400	15400	46[c]	56
Register	80000	75000	70000	65000	56500	49500	43500	38500	....	57[c]
Section B.	5500	5100	4800	4500	3900	3400	3000	2600	41	51
	9900	9200	8600	8100	7100	6200	5400	4600	42	52
70 to 99	13100	12300	11600	10900	9700	8500	7500	6500	43	53
Equivalent	16300	15400	14500	13700	12200	10800	9500	8300	44	54
Ft										
	19800	18400	17200	16200	14200	12400	10800	9200	45[c]	55
	26200	24600	23200	21800	19400	17000	15000	13000	46[c]	56
	65500	61500	58000	54500	48500	42500	37500	32500	....	57[c]
Section C.	4400	4200	3900	3700	3200	2900	2600	2300	41	51
	8100	7600	7100	6600	5800	5100	4500	4000	42	52
100 to 139	10800	10100	9600	9000	8000	7100	6200	5400	43	53
Equivalent	13700	12900	12100	11300	10000	8900	7900	7000	44	54
Ft										
	16200	15200	14200	13200	11600	10200	9000	8000	45[c]	55
	21600	20200	19200	18000	16000	14200	12400	10800	46[c]	56
	54000	50500	48000	45000	40000	35500	31000	27000	....	57[c]
Section D.	3900	3700	3500	3300	2900	2500	2200	2000	41	51
	6900	6500	6100	5700	5100	4500	4000	3600	42	52
140 to 189	9300	8700	8100	7600	6800	6000	5300	4700	43	53
Equivalent	11600	11000	10400	9800	8700	7700	6800	6000	44	54
Ft										
	13800	13000	12200	11400	10200	9000	8000	7200	45[c]	55
	18600	17400	16200	15200	13600	12000	10600	9400	46[c]	56
	46500	43500	40500	38000	34000	30000	26500	23500	....	57[c]
Section E.	3300	3100	2900	2700	2500	2200	1900	1700	41	51
	5700	5400	5100	4800	4300	3800	3400	3000	42	52
190 to 250	7800	7300	6900	6500	5700	5000	4400	3900	43	53
Equivalent	9700	9100	8600	8100	7300	6500	5800	5100	44	54
Ft										
	11400	10800	10200	9600	8600	7600	6800	6000	45[c]	55
	15600	14600	13800	13000	11400	10000	8800	7800	46[c]	56
	39000	36500	34500	32500	28500	25000	22000	19500	....	57[c]

FOR INSULATED DUCTS	COL. A	COL. B	COL. C	COL. D	COL. E	COL. F	FOR DUCTS THAT ARE COMPLETELY INSULATED WITH ½ IN. THICK INSULATION FROM BONNET TO BOOT, USE THESE COLUMN HEADINGS.
	1 TO 9 FT	10 TO 17 FT	18 TO 24 FT	25 TO 34 FT	35 TO 54 FT	55 TO 74 FT	

[a]These tables are for use in sizing both the warm air and the return air branches.

[b]Frictional resistances and temperature drops in ducts have both been accounted for in these tables.

[c]Use these items only when the building construction, or capacity requirements, necessitate the use of two adjoining stacks or floor registers.

TABLE 4. CAPACITY TABLES FOR WARM-AIR AND RETURN AIR BRANCHES[a,b]

SECOND STORY

FOR UNINSULATED METAL DUCTS	ACTUAL LENGTH (FROM BONNET TO BOOT) OR, (FROM RETURN PLENUM TO BOOT) IN FEET								WARM AIR COMBINATION No.	RETURN AIR COMBINATION No.
	1 TO 7 FT	8 TO 12 FT	13 TO 17 FT	18 TO 24 FT	25 TO 34 FT	35 TO 44 FT	45 TO 54 FT	55 TO 64 FT		
	COL. A	COL. B	COL. C	COL. D	COL. E	COL. F	COL. G	COL. H		
Section A.	6300	5700	5200	4800	4100	3500	3100	2800	41	51
	10900	10000	9200	8500	7300	6400	5600	5000	42	52
40 to 69	14000	13000	12100	11400	10000	8800	7800	6800	43	53
Equivalent	17000	15900	14900	13900	12400	11100	9900	9000	44	54
Ft for										
Fittings	21800	20000	18400	17000	14600	12800	11200	10000	45[c]	55
and	28000	26000	24200	22400	20000	17600	15600	13600	46[c]	56
Register	70000	65000	60500	57000	50000	44000	39000	34000	....	57[c]
Section B.	5000	4600	4300	4000	3400	3000	2700	2300	41	51
	9000	8200	7600	7100	6200	5400	4700	4200	42	52
70 to 99	11900	11000	10300	9600	8400	7500	6700	6000	43	53
Equivalent	14800	13900	13000	12200	10800	9600	8500	7500	44	54
Ft										
	18000	16400	15200	14200	12400	10800	9400	8400	45[c]	55
	23900	22000	20600	19200	16800	15000	13400	12000	46[c]	56
	59500	55000	51500	48000	42000	37500	33500	30000	....	57[c]
Section C.	4100	3800	3600	3400	2900	2600	2300	2000	41	51
	7400	6900	6400	6000	5200	4600	4000	3600	42	52
100 to 139	10000	9300	8700	8100	7100	6200	5500	4800	43	53
Equivalent	12500	11600	10800	10100	9000	8000	7200	6500	44	54
Ft										
	14800	13800	12800	12000	10400	9200	8000	7200	45[c]	55
	20000	18600	17400	16200	14200	12400	11000	9600	46[c]	56
	50000	46500	43500	40500	35500	31000	27500	24000	....	57[c]
Section D.	3700	3400	3100	2900	2600	2200	2000	1800	41	51
	6500	6000	5600	5300	4700	4100	3700	3300	42	52
140 to 189	8600	8000	7500	7000	6100	5400	4800	4300	43	53
Equivalent	10900	10100	9400	8800	7800	6900	6100	5400	44	54
Ft										
	13000	12000	11200	10600	9400	8200	7400	6600	45[c]	55
	17200	16000	15000	14000	12200	10800	9600	8600	46[c]	56
	43000	40000	37500	35000	30500	27000	24000	21500	....	57[c]
Section E.	3200	2900	2700	2500	2200	1900	1700	1500	41	51
	5500	5200	4800	4400	3900	3400	3100	2800	42	52
190 to 250	7300	6800	6300	5900	5100	4500	3900	3500	43	53
Equivalent	9100	8500	7900	7500	6600	5900	5200	4700	44	54
Ft										
	11000	10400	9600	8800	7800	6800	6200	5600	45[c]	55
	14600	13600	12600	11800	10200	9000	7800	7000	46[c]	56
	36500	34000	31500	29500	25500	22500	19500	17500	....	57[c]

FOR INSULATED DUCTS	COL. A	COL. B	COL. C	COL. D	COL. E	COL. F	COL. G	FOR DUCTS THAT ARE COMPLETELY INSULATED WITH ½ IN. THICK INSULATION FROM BONNET TO BOOT USE THESE COLUMN HEADINGS.
	1 TO 8 FT	9 TO 14 FT	15 TO 20 FT	21 TO 27 FT	28 TO 42 FT	43 TO 54 FT	55 TO 70 FT	

[a] These tables are for use in sizing both the warm air and the return air branches.

[b] Frictional resistance and temperature drops in ducts have both been accounted for in these tables.

[c] Use these items only when the building construction, or capacity requirements, necessitate the use of two adjoining stacks or floor registers.

sun room, or in a location where it will be affected by direct radiant heat from the sun or from a fireplace, or by direct heat from any warm air duct, register or chimney.

2. A *fan switch* control located in the bonnet to start blower operations at temperatures between 110 and 130 F, and to stop the blower at about 25 to 30 deg below the cut-in point. The lower settings are used for high side wall register installations, and the higher settings for baseboard register installations. For most satisfactory results these settings should be as low as is feasible.

3. A *protective high limit switch* located in the bonnet to stop the system independently of the thermostat if the bonnet temperature exceeds 175 F.

4. On oil and gas burner installations, a protective control should be included which will stop the system if the fire is extinguished or if there is a failure of the ignition system.

5. On automatic stoker installations, a control is usually included which will start the operation regardless of thermostat settings whenever the bonnet temperature indicates that the fire is dying, or a time interval contactor is used that will start the stoker to run a few minutes out of each hour.

6. A *humidistat* to regulate the moisture supplied to the rooms, located either in one of the rooms or in the main return duct near the furnace.

COOLING METHODS

A slight cooling effect may be obtained under certain conditions by the use of the cooler basement air. A more positive cooling effect may be obtained by the use of an air washer where the temperature of the city or well water is sufficiently low (55 F or lower), and where a sufficient volume of water can be provided. Unless the temperature of the leaving water is below the dew-point temperature of the indoor air at the time the washer is started, both the relative and absolute humidities will be somewhat increased.

Coils of copper finned tubing through which cold water is pumped are available for cooling. They require less space than air washers and have the advantage that no moisture is added to the air when the temperature of the water rises above the dew-point. Ample coil surface and fan capacity are necessary with this type of cooling.

It is thoroughly feasible to use ice or mechanical refrigeration in connection with a warm air system and to cool the building by this method, provided the building is reasonably well constructed and insulated. Windows and doors should be tight, and awnings should be supplied on the sunny side of the building. (See also Chapters 38, 39 and 43.)

Conclusions drawn from studies [4] conducted in the University of Illinois Research Residence, subject to the limitations of the test are:

1. An uninsulated building of ordinary residential type may require the equivalent of three tons of ice in 24 hr on days when the maximum outdoor temperature reaches 100 F if an effective temperature of approximately 72 deg is maintained indoors.

2. The use of awnings at all windows in east, south, and west exposures may result in savings of from 20 to 30 per cent in the required cooling load.

3. The cooling load per degree difference in temperature is not constant but increases as the outdoor temperature increases.

4. The heat lag of the building complicates the estimation of the cooling load under any specified conditions and makes such estimates, based on the usual methods of computation, of doubtful value.

5. The seasonal cooling requirements are extremely variable from year to year, and the ratio between the degree-hours of any two seasons occurring within a 10-year period may be as high as 7.5 to 1. Hence an average value of the degree-hours cooling per season is comparatively meaningless.

6. The duct system in a forced-air heating installation can be successfully converted to a system for conveying cool air for the purpose of cooling the structure. No condensation of moisture was observed when the duct temperatures were not less than 65 F.

7. Cooling by means of water at a temperature of 60 F is not satisfactory unless an indoor temperature of less than 80 F is maintained.

8. In the selection of cooling coils, the additional frictional resistance of the coil to flow of air must be given consideration.

9. Cooling the structure by introducing large quantities of air from outdoors at night tended to reduce the amount of cooling required on the following day and was a practical means of providing more comfortable conditions in those homes where cooling systems were not available.

DESIGN PROCEDURE FOR LARGER SYSTEMS[5]

For buildings having a heat loss in excess of 150,000 Btu per hour the design procedure given in Manual No. 9, Technical Code, of the *National Warm Air Heating and Air Conditioning Association*, may be used. This procedure follows a general outline given below:

1. Calculation of design heat losses from individual spaces in the structure. (See Chapter 14.)

2. Location of registers and return intakes on floor plan, types of registers, with throws and deflections of registers desired.

3. Laying out a proposed duct system for both warm air and return air sides of the system including details of types of fittings and the actual and equivalent lengths of each branch line from bonnet to register, without sizes.

The following items are determined from tables in Manual No. 9:

4. Determination of bonnet temperature.

5. Determination of air volume to be delivered through each register and the respective register air temperatures.

6. Selection of register sizes and pressure losses to produce necessary throw, for the air volumes handled.

7. Design of duct system.
   a. Warm air branches.
   b. Return air branches.
   c. Trunk ducts for warm air and return air sides of system.

8. Selection of blower and furnace.

REFERENCES

1—Specifications for the furnace unit and the installed duct system are shown in The Yardstick (Textbook Section 8) and the Code and Manual (Textbook Section 7) published by *National Warm Air Heating and Air Conditioning Association*.

2—Performance of a Forced Warm-Air Heating System as Affected by Changes in Volume and Temperature of Air Recirculated, by A. P. Kratz and S. Konzo (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 393).

3—Automatic Controls for Forced-Air Heating Systems, by S. Konzo and A. F. Hubbard (A.S.H.V.E. TRANSACTIONS, Vol. 40, 1934, p. 37).

4—Summer Cooling in the Research Residence, by A. P. Kratz, S. Konzo, M. K. Fahnestock and E. L. Broderick (University of Illinois *Engineering Experiment Station Bulletins* Nos. 290, 305 and 321). A.S.H.V.E. RESEARCH REPORT No. 1177—Summer Cooling in the Research Residence with a Gas-Fired Dehydration Cooling Unit, by A. P. Kratz, S. Konzo and E. L. Broderick (A.S.H.V.E. TRANSACTIONS, Vol. 47, 1941, p. 203).

5—Proposed Design Procedure for Large Mechanical Warm Air Heating Systems, by S. Konzo, R. J. Martin, D. S. Levinson, and R. W. Roose, A.S.H.V.E. Journal Section, *Heating, Piping and Air Conditioning*, May, 1947, p. 108.

Chapter 23

STEAM HEATING SYSTEMS AND PIPING

Classification of Steam Heating Systems by Types; One-pipe; Two-pipe, Sub-atmospheric and Orifice Systems; Sizing Piping for Steam Heating Systems; Pressure Reducing Valves; Boiler Connections; Condensate Return Pumps; Vacuum Heating Pumps; Traps; Drips; Connections to Heating Units; Control Valves

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STEAM heating systems may be classified according to any one of, or combination of, the following features: (1) by the piping arrangement, (2) by the pressure or vacuum conditions obtained in operation, (3) by the method of returning condensate to the boiler.

1. *By Piping Arrangement.* A steam heating system is known as a *one-pipe system* when a single main serves the dual purpose of supplying steam to the heating unit and conveying condensate from it. Ordinarily to each heating unit there is but one connection which must serve as both the supply and the return, although separate supply and return connections may be used.

A steam heating system is known as a *two-pipe system* when each heating unit is provided with two piping connections and when steam and condensate flow in separate mains and branches.

Heating systems may also be described as *up-flow* or *down-flow* depending on the direction of steam flow in the risers; and as a *dry-return* or a *wet-return* depending on whether the condensate mains are above or below the water line of the boiler or condensate receiver.

2. *By Pressure or Vacuum Conditions.* Steam heating systems may also be classified as *high pressure, low pressure, vapor,* and *vacuum* systems, depending on the pressure conditions under which the system is designed to operate.

A system is known as a *high pressure system* when the operating pressures employed are above 15 psi; as a *low pressure system* when pressures vary from 0 to 15 psi; as a *vapor system* when the system operates under both vacuum and low pressure conditions without the use of a vacuum pump; and as a *vacuum system* when the system operates under vacuum and low pressure conditions with the use of vacuum pump.

When automatic controls are employed to vary the pressure conditions in the system in accordance with outside weather conditions, the system may be known as a *sub-atmospheric, differential,* or *synchronized* system. These latter classifications are proprietary designations.

When orifices are employed on the inlets to the heating units the system may be known as an *orifice system.*

3. *By Method of Returning Condensate.* When condensate is returned to the boiler by gravity, the system is known as a *gravity return system.* In this system all heating units must be elevated sufficiently above the water line of the boiler, so that the condensate can flow freely to the boiler. Elevation of the heating units above the water line must therefore be sufficient to overcome pressure drops due to flow as well as pressure differences due to operation.

Referring to Fig. 1 it will be noted that the boiler and wet return form a U-shaped container, with the boiler steam pressure on the top of the water at one end and the steam main pressure on the top of the water at the other end. The difference between these two pressures is the *pressure drop* in the system, *i.e.,* the friction and resistance to the flow of steam in passing from the boiler to the far end of the main and the pressure reduction in consequence of the condensation occurring in the system. The water in the far end will rise sufficiently to overcome this difference in order to balance the pressures, and it will rise far enough to produce a flow through the return pipe and overcome the resistance of check valves if installed. .

If a one-pipe steam system is designed, for example, for a total pressure drop of ⅛ psi, and utilizes a Hartford return connection instead of a check valve on the return, the rise in the water level at the far end of the return due to the difference in steam pressure would be ⅛ of 28 in. (28 in. head being equal to one pound per square inch), or 3½ in. Adding 3 in. to overcome the resistance of the return main and 6 in. as a factor of safety

for heating up gives 12½ in. as the distance the bottom of the lowest part of the steam main and all heating units must be above the boiler water line. The same system, however, installed and sized for a total pressure drop of ½ psi, and with a check in the return, would require ½ of 28 in., or 14 in. for the difference in steam pressure, 3 in. for the flow through the return, 4 in. to operate the check, and 6 in. for a factor of safety, making a total of 27 in. as the required distance. Higher pressure drops would increase the distance accordingly.

When conditions are such that condensate cannot be returned to the boiler by the action of gravity, and either traps or pumps must be employed, the system is known as a *mechanical return system.* There are three general types of mechanical condensate return devices in common use: (*a*) the alternating return trap (*b*) the condensate return pump, and (*c*) the vacuum return pump.

In systems where pressure conditions in the system vary between that of a gravity return and a forced return system, a boiler return trap or alternating receiver is employed and the system may be known as an *alternating return system.*

When condensate is pumped to the boiler under pressures of the atmosphere or above, the system is known as a *condensate pump return system.*

When condensate is pumped to the boiler under vacuum conditions, the system is known as a *vacuum pump return system.*

In either the *condensate* or *vacuum pump systems* it is highly desirable to arrange for gravity flow to a receiver and to the pump. The pump then forces condensate into the boiler against its pressure.

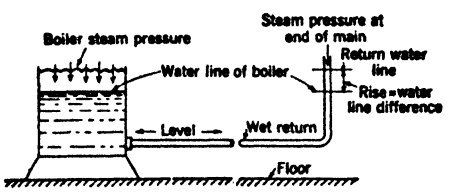


FIG. 1. DIFFERENCE IN STEAM PRESSURE ON WATER IN BOILER AND AT END OF STEAM MAIN

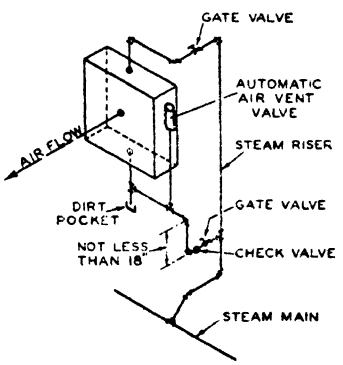


FIG. 2. TYPICAL TWO-PIPE CONNECTIONS TO UNIT HEATERS IN ONE-PIPE AIR VENT SYSTEMS

ONE-PIPE SYSTEMS

One-pipe systems, as previously defined, are systems in which steam and condensate flow in the same pipe. Radiators and other heating units, in general, have only one piping connection from main to unit, although it is possible to employ two connections to the same main as indicated in Fig. 2. Unit heaters in one-pipe systems may also have separate connections to the wet return as shown in Fig. 5 Chapter 26.

There are several variations in the piping arrangement of a one-pipe system as follows:

1. Up-feed one-pipe systems where the radiators and other heating units are located above the supply mains. The mains in this instance convey both steam and condensate. Such a system is illustrated in Fig. 3. Typical connections to radiator or risers are illustrated in Fig. 4 and method of changing sizes of mains in Fig. 5.

2. Up-feed one-pipe systems where the radiators and other heating units are located above the mains and the mains are dripped at each radiator connection to a wet return, so that the steam main carries a minimum of the condensate. This system is illustrated

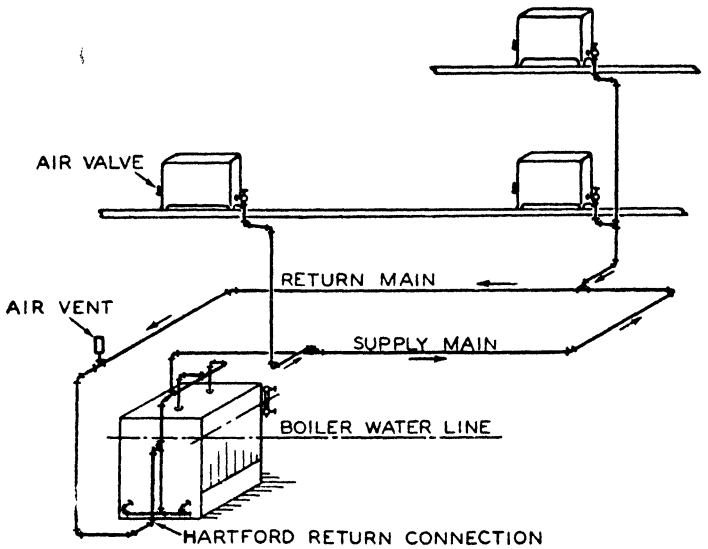


FIG. 3. TYPICAL UP-FEED GRAVITY ONE-PIPE AIR-VENT SYSTEM

in Fig. 6. Typical connections to radiators and risers are illustrated in Fig. 7. Up-feed systems are not recommended for systems higher than four stories.

3. Down-feed one-pipe systems, where the radiators and other heating units are located below the supply main. In this arrangement only risers and connections to heating units convey both steam and condensate, and both are flowing in the same direction. The steam main is kept relatively free of condensate by dripping through the drop risers.

Each radiator or heating unit in a one-pipe system must be supplied with a thermostatic air valve which functions to relieve air from the heating unit under pressure, and to close when steam itself heats the thermostatic element of the valve.

To improve steam circulation in one-pipe systems quick vent air valves should be provided at the ends and at intermediate points where the steam main is brought to a higher elevation or where dropped below the water line. It is desirable to install the air-vent valves about a foot ahead of the drips, as indicated in Fig. 6, to prevent possible damage to their mechanisms by water.

Air valves are of two general types, the pressure and the vacuum types. The pressure type permits the inflow of atmospheric air to the system when the steam pressure in the system falls below atmospheric pressure. The vacuum type, which contains a small check valve, prevents the air from flowing back to the system and thereby maintains vacuum condi-

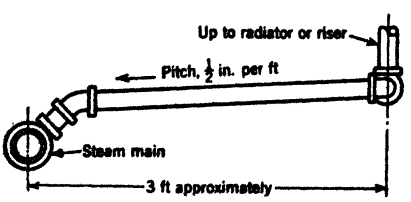


FIG. 4. TYPICAL STEAM RUNOUT WHERE RISERS ARE NOT DRIPPED

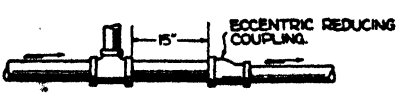


FIG. 5. METHOD OF CHANGING SIZE OF STEAM MAIN WHEN RUNOUTS ARE TAKEN FROM TOP

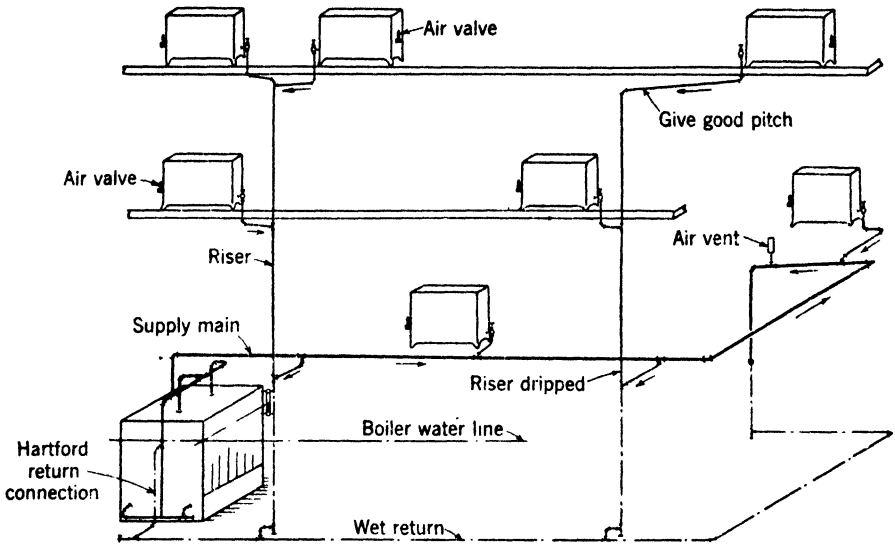


FIG. 6. TYPICAL UP-FEED GRAVITY ONE-PIPE AIR-VENT SYSTEM

tions in the system, and a consequent evaporation or generation of steam or vapor at sub-atmospheric pressures, and at consequent lower temperatures. Systems which use vacuum valves are known as *vapor* or *vacuum one-pipe systems*. The vapor or vacuum systems will maintain a more uniform temperature condition than the pressure systems.

Each heating unit in a one-pipe system may also be provided with a valve on the connection to the unit, although this is not essential except to shut the unit off in case it is not desired for heating. Valves on one-pipe systems must be either fully opened or fully closed. No throttling or modulating position can be maintained, since if a valve is partially closed condensate will not drain from the unit. This condition is dangerous because it may create a low water condition in the boiler with consequent burning or cracking of the boiler, or of creating a hazard due to the freezing of the water logged heating unit itself.

TWO-PIPE SYSTEMS

Two-pipe systems, as previously defined, are systems in which steam and condensate flow in separate pipes. Two-pipe systems operate under

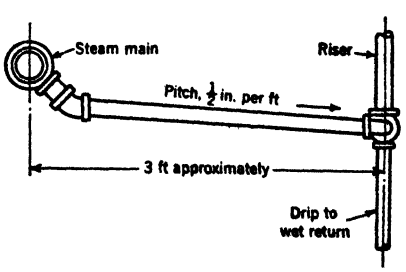


FIG. 7. TYPICAL STEAM RUNOUT WHERE RISERS ARE DRIPPED

either high pressure, low pressure, vapor, or vacuum conditions. Either the up-flow or the down-flow arrangement of mains may be employed.

Two-Pipe High Pressure Systems

Two-pipe high pressure systems operate at pressures above 15 psi, usually from 30 to 150 psi. Large industrial type buildings, which are equipped with unit heaters or large built up fan units, usually use high pressure steam systems.

Fig. 8 illustrates a typical high pressure system. Because of the high pressures and the great differential between steam and return mains, it is possible to locate returns above the heating units and lift the condensate to these returns.

The condensate can be flashed into steam in low pressure mains if any are available or passed through an economizer heater before being dis-

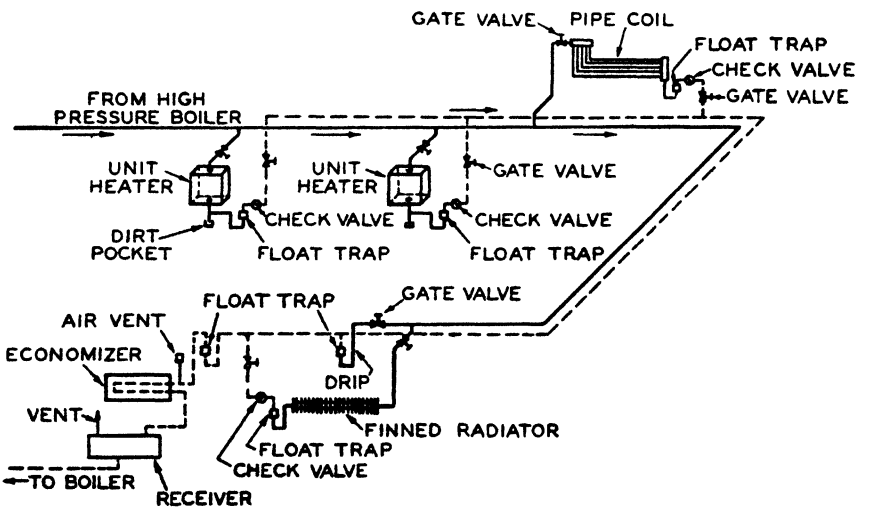


FIG. 8. TYPICAL HIGH PRESSURE HEATING SYSTEM

charged to a vented receiver. It is of course necessary to provide for the elimination of air from high pressure systems, the same as in low pressure systems.

Return traps used on high pressure systems are usually of the bucket, inverted bucket, float or impulse type.

Two-Pipe Low Pressure Systems

Low pressure systems operate at pressures of 0 to 15 psi. The piping arrangement of both up-feed and down-feed low pressure systems is identical with these of two-pipe vapor systems described in the following section. The only difference between the two systems is in the type of air valve used. The air valves used in low pressure systems do not contain the check discs and hence the system cannot operate under vacuum conditions. The low pressure systems are not as popular as the vapor systems, because they have the disadvantage of not holding heat when the rate of steam generation is diminishing. They also have the disadvantage of

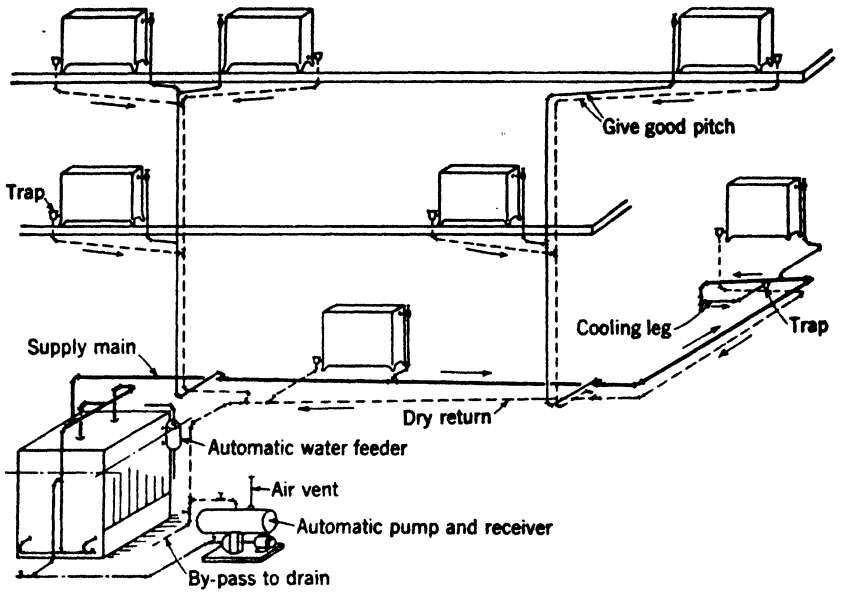


FIG. 9. TYPICAL INSTALLATION USING CONDENSATE PUMP

corroding to a greater extent than vapor systems due to the continued presence of new air in the system.

Low pressure systems have the advantage however of returning condensate to the boiler readily and not retaining it in the piping as may be possible in vapor systems.

Fig. 9 illustrates a typical low pressure system with condensate pump.

Two-Pipe Vapor Systems

Two-pipe vapor systems operate at pressures varying from 30 in. vacuum to 15 psi without the use of a vacuum pump. A typical two-

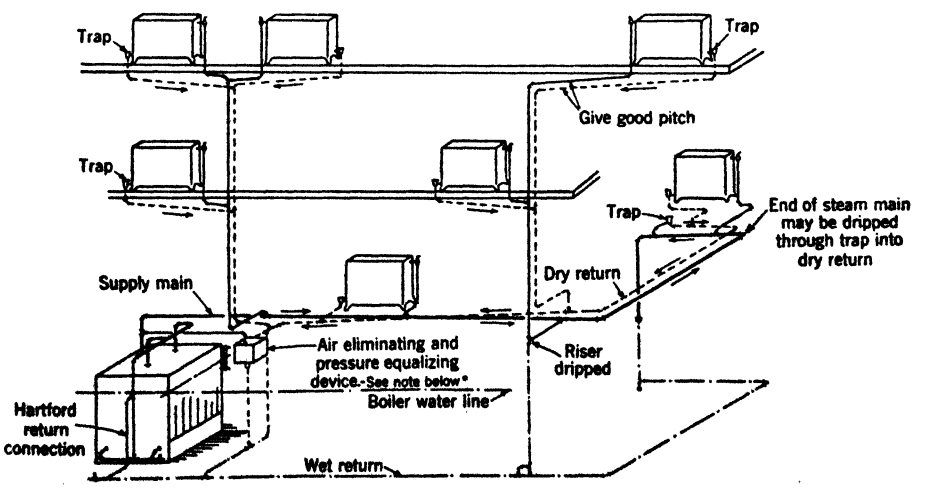


FIG. 10. TYPICAL UP-FEED TWO-PIPE SYSTEM WITH AUTOMATIC RETURN TRAP*

*Proper piping connections are essential with special appliances for pressure equalizing and air elimination.

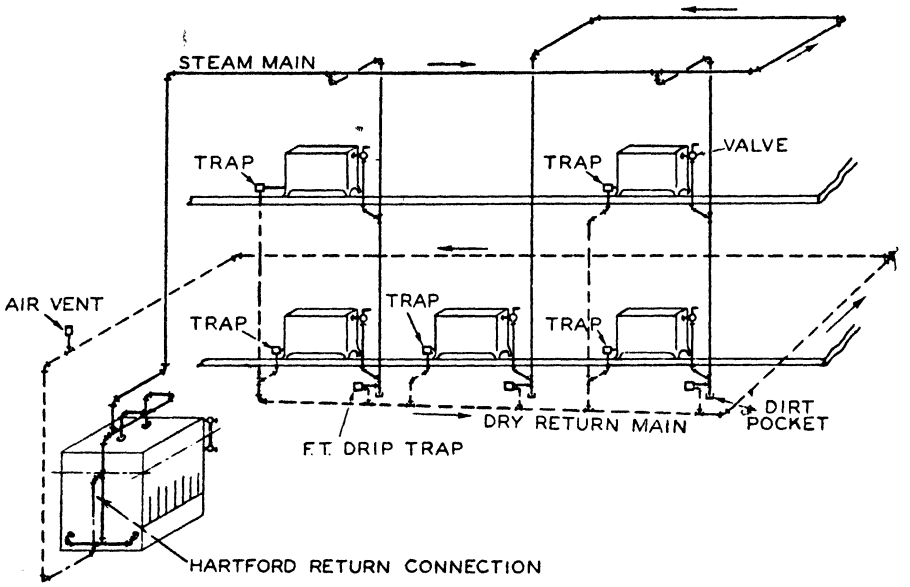


FIG. 11. TYPICAL DOWN-FEED TWO-PIPE SYSTEM

pipe up-feed vapor system is shown in Fig. 10, and a typical two-pipe down-feed system is illustrated in Fig. 11. The method of dripping drop risers in a down-feed system is illustrated in Fig. 12. Radiators discharge their condensate and air through thermostatic traps to the dry return main. Air is eliminated, when the system is under pressure, at the ends of the supply and return mains just before they drop to the wet return. The air valves are of the float and thermostatic type which opens when cool air contracts the thermostatic element and closes when steam expands the element. The float element of the valve closes the valve when, due to pressure differences, water rises to the point of overflow in the main. The air valves are also provided with a small check

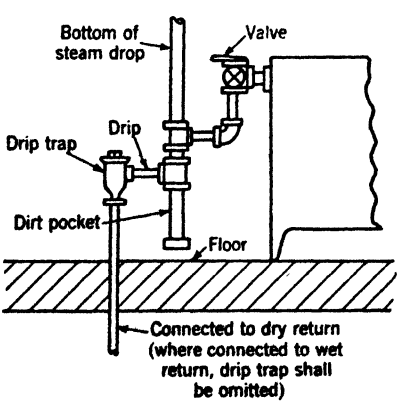


FIG. 12. DETAIL OF DRIP CONNECTIONS AT BOTTOM OF DOWN-FEED STEAM DROP

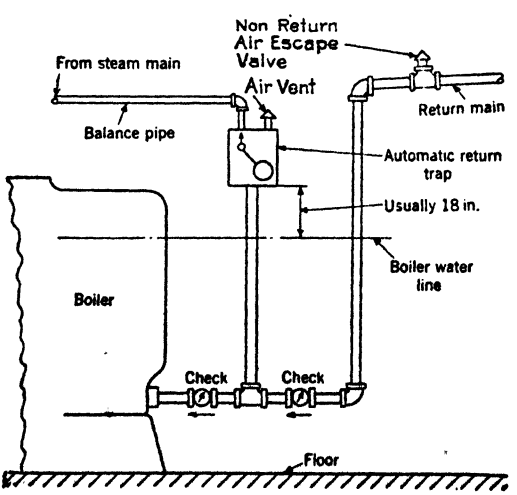


FIG. 13. TYPICAL CONNECTIONS FOR AUTOMATIC RETURN TRAP

disc which closes to prevent the inflow of air to the system when the pressure drops below atmospheric pressure. This enables the system to operate under vacuum conditions at lower steam temperatures for a period of four to eight hours depending on the tightness of the system.

Vapor systems may also be provided with an automatic return trap or alternating receiver which automatically returns condensate to the boiler when the boiler is steaming under pressure conditions which would prevent the return of condensate by gravity. The typical connections for an automatic return trap are illustrated in Fig. 13.

Each heating unit in a vapor system, as in all two-pipe systems, is provided with a graduated or modulating valve which permits the control of heat in the radiator by varying the opening of the valve.

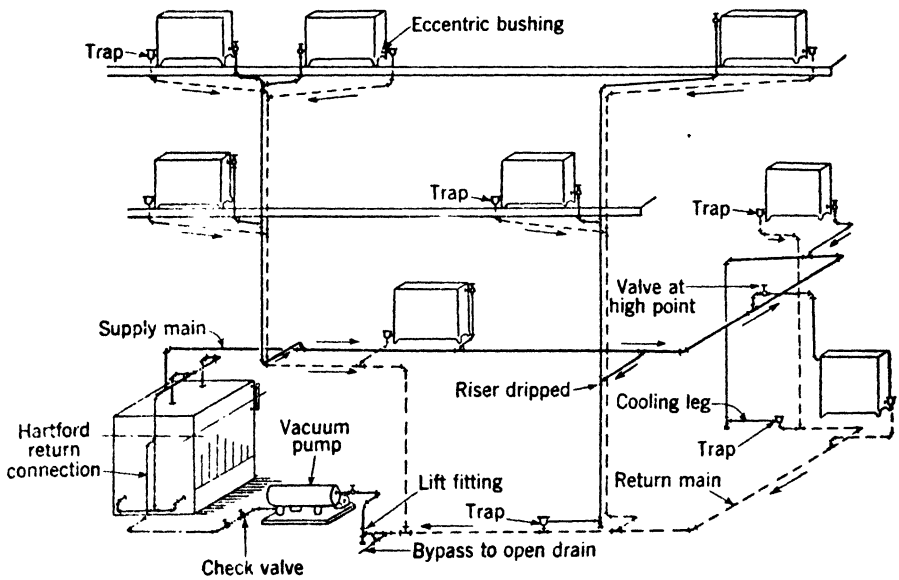


FIG. 14. TYPICAL UP-FEED VACUUM PUMP SYSTEM

Two-Pipe Vacuum Systems

Vacuum systems operate under conditions of both low pressure and vacuum, but employ the use of a vacuum pump to insure maintenance of sub-atmospheric pressures.

A typical two-pipe up-feed vacuum system is illustrated in Fig. 14, and a down-feed arrangement in Fig. 15.

The return risers are connected in the basement into a common return main which slopes downward toward the vacuum pump. The vacuum pump withdraws the air and water from the system, separates the air from the water and expels it to atmosphere and pumps the water back to the boiler, or other receiver, which may be a feed-water heater or hot well. It is essential that no connection be made from the supply side to the return side at any point except through a trap. The desirable practice demands a return flowing to the vacuum pump by an uninterrupted downward slope. In some instances local conditions make it necessary to drop the return below the level of the vacuum pump inlet, before the pump can

be reached. In such an event one of the advantages of the vacuum system is the ability to raise the condensate to a considerable height by the suction of the vacuum pump by means of a lift connection or fitting inserted in the return. The height the condensate can be raised depends on the amount of vacuum maintained. It is preferable to limit lift connections to a single lift at the vacuum pump. A still more preferable arrangement is the use of an accumulator tank, or receiver tank, with a float control for the pump, at the low point of the return main located adjacent to the vacuum pump.

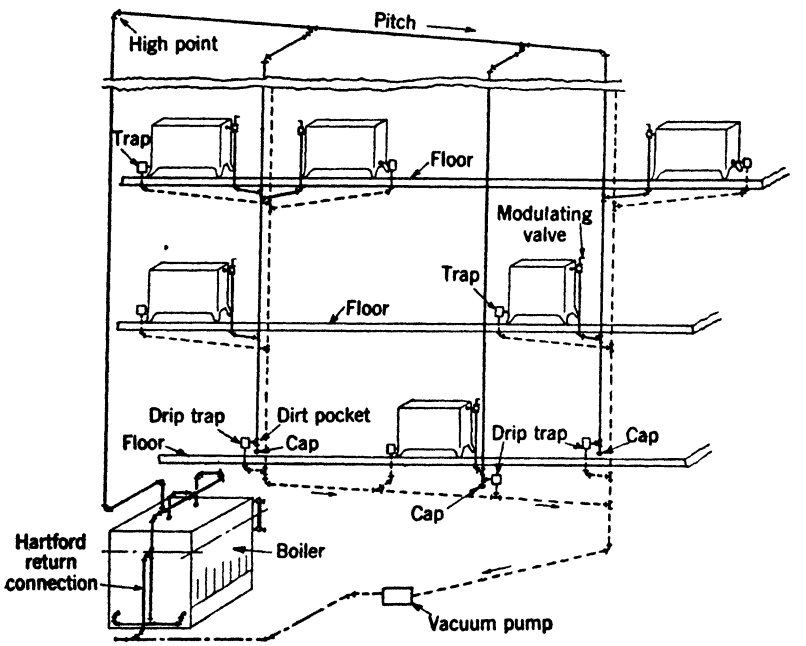


FIG. 15. TYPICAL DOWN-FEED VACUUM SYSTEM

When the vertical lift is considerable, several lift fittings should be used in steps as shown in Fig. 16. This permits a given lift to be secured with a somewhat lower vacuum than where the vertical distance is served by a single lift. Where several lifts are present in a given system at different locations, the lifting cannot occur until the entire system is filled with steam. A lift connection for location close to the pump, where the size may be above the commercial stock sizes, is shown in Fig. 17. It is desirable that means be provided for manually draining the low point of the lift fittings to eliminate danger of freezing.

TWO-PIPE SUB-ATMOSPHERIC SYSTEMS

Sub-atmospheric systems are similar to vacuum systems but, in contrast, provide control of building temperature by variation of the heat output from the radiators. The radiator heat emission is controlled by varying the pressure, temperature and specific volume of steam in circulation. These systems differ from the ordinary vacuum system in that they maintain a controllable partial vacuum on both the supply and return sides of the system, instead of only on the return side. In the

vacuum system, steam pressure above that of the atmosphere exists in the supply mains and radiators practically at all times. In the sub-atmospheric system, atmospheric pressure or higher exists in the steam supply piping and radiators only during severe weather. Under average winter temperature the steam is under partial vacuum which in mild weather may reach as high as 25 in. Hg, after which further reduction in heat output is obtained by restricting the quantity of steam.

The rate of steam supply is controled by a valve in the steam main or by thermostatically controlling the rate of steam production in the boiler. The control valve may be of the automatic *modulating* or *floating* type governed thermostatically from selected control points in the building, or it may be a special pressure reducing valve which will maintain the desired sub-atmospheric pressures by continuous flow into the heating main. In some systems radiator supply valves include adjustable orifices

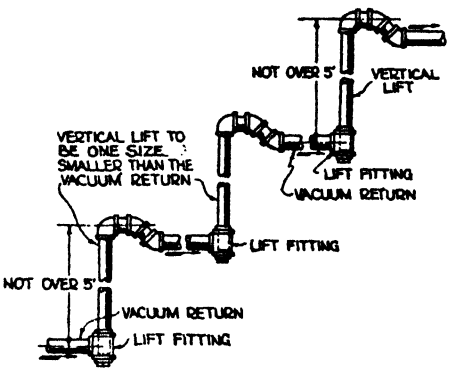


FIG. 16. METHOD OF MAKING LIFTS ON VACUUM SYSTEMS WHEN DISTANCE IS OVER 5 FT

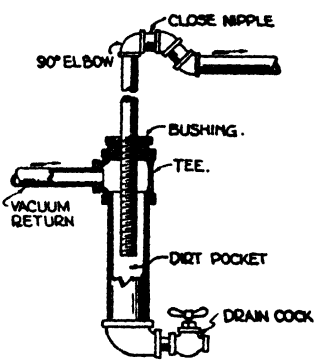


FIG. 17. DETAIL OF MAIN RETURN LIFT AT VACUUM PUMP

or are equipped with regulating orifice plates. The sizes of orifices used are larger than for other types of orifice systems because for equal radiator sizes the volume flowing is larger. Orifices are omitted on some systems. Radiator traps and drips are designed to operate at any pressure from 15 lb gage to 26 in. Hg. A vacuum pump capable of operating at high vacuum is preferable to promote accuracy in the distribution of steam throughout the system, particularly in mild weather. This vacuum is partially self-induced by the condensation of the steam in the system under conditions of restricted supply for reduction of the radiator heat emission.

The returns must grade downward constantly and uninterruptedly from the radiator return outlets to the inlet of the receiver of the vacuum pump. One radical difference between this and the ordinary vacuum system is that no lifts should be made in the return line, except at the vacuum pump. The receivers are placed at a lower level than the pump and equipped with float control so that the pump may operate as a return pump under night conditions. The system may be operated in the same manner as the ordinary vacuum system when desired.

Steam for heating domestic hot water should be taken from the boiler header back of the control valve so that pressures sufficiently high for heating the water may be maintained on the heater. The sub-atmospheric method of heating can be used for the heating coils of ventilating

and air conditioning systems. The flexible control of heat output secured by this method materially reduces the required size of by-pass around the heaters. Some applications of sub-atmospheric systems are proprietary.

TWO-PIPE ORIFICE SYSTEMS

Orifice steam heating systems may have piping arrangements identical with vacuum systems. Some of these omit the radiator thermostatic traps but use thermostatic or combination float and thermostatic traps on all drip points. A return condensate pump with receiver vented to atmosphere, a return line vacuum pump, or a return trap, is generally used to return the condensate to the boiler or place of similar disposition, such as a feed-water heater or hot well. The heat emission from the radiators is controlled by varying the pressure differential maintained.

The principle on which these systems operate is based on the fact that the steam flow through an orifice will vary when the ratio of the absolute pressures on the two sides of the orifice exceeds 58 per cent. If the absolute pressure on the outlet side is less than 58 per cent of the absolute pressure on the inlet side, no further increase in flow will be obtained as a result of the increased pressure difference. If an orifice is so designed in size as to exactly fill a radiator with 2 psi gage on one side and ¼ psi gage on the other, the absolute pressure relation is:

$$\frac{14.7 + 0.25}{14.7 + 2.0} = 0.90 \text{ or } 90 \text{ per cent.}$$

Should the steam pressure be dropped to ¼ lb on the supply pipe, the pressure on each side of the orifice would be balanced and no steam flow would take place. From this it will be apparent that if an orifice of a given diameter will fill a given radiator with steam when there is a given pressure on the main, reducing this steam main pressure will permit filling various desired portions of the radiator down to the point where the main pressure equals the back pressure in the radiator provided the supply pipe pressures may be controlled sufficiently close. If orifices are designed on a similar basis for a given system and proportioned to the heating capacity of the radiators they serve, all radiators will heat proportionately to the steam pressure. The range of pressure variation is limited by the permissible noise level of the steam flowing under the pressure difference required for maximum heat output. The control of the steam supply is obtained by a valve placed in the steam main, which maintains a determined pressure by varying the vacuum in the return lines, or by varying the pressure in the supply lines and the vacuum in the returns. The valves are frequently manually set from a remote location, guided by temperature indicating stations in the building; or thermostatically controlled from a thermostat on the roof, which automatically measures the differential of outside and inside temperatures. Since the range through which the pressures may be varied is usually from 0 to 4 psi gage, the control should be capable of maintaining close regulation to maintain the desired space temperatures, particularly in mild weather.

A recommended orifice schedule is shown in Table 1. Some systems use orifices not only in radiator inlets but also at different points in the steam supply piping for the purpose of balancing the system to a greater extent. In this manner the difference between the initial and terminal pressure in the steam main may be compensated to a great extent. For example, if the initial pressure was 3 psi gage and the pressure at the end of the main was 2 psi, an orifice could be used in each branch for the purpose

TABLE 1. ORIFICE CAPACITIES FOR LOW PRESSURE STEAM SYSTEMS

This table is based on data from actual tests[a]

ORIFICE DIAMETER 64THS OF AN INCH	6 IN. HG DIFFERENTIAL	5 IN. HG DIFFERENTIAL	4 IN. HG DIFFERENTIAL	2 IN. HG DIFFERENTIAL	1 IN. HG DIFFERENTIAL
	Capacity Expressed in Square Feet E D R				
7	18–23	16–21	15–19	10–13	
8	23–29	21–27	19–25	13–17	8–11
9	29–36	27–33	25–30	17–21	11–14
10	36–44	33–40	30–37	21–26	14–17
11	44–52	40–48	37–44	26–31	17–20
12	52–62	48–57	44–51	31–37	20–24
13	62–72	57–66	51–59	37–43	24–28
14	72–83	66–76	59–67	43–49	28–32
15	83–94	76–86	67–76	49–56	32–37
16	94–106	86–97	76–86	56–64	37–42
17	106–119	97–109	86–97	64–72	42–47
18	119–133	109–122	97–108	72–80	47–52
19	133–148	122–135	108–120	80–88	52–58
20	148–163	135–149	120–133	88–98	58–64
21	163–179	149–164	133–145	98–107	64–71
	Capacity Expressed in Pounds per Hour				
7	4.5–5.8	4.0–5.3	3.8–4.8	2.5–3.3	
8	5.8–7.3	5.3–6.8	4.8–6.3	3.3–4.3	2.0–2.8
9	7.3–9.0	6.8–8.3	6.3–7.5	4.3–5.3	2.8–3.5
10	9.0–11.0	8.3–10.0	7.5–9.3	5.3–6.5	3.5–4.3
11	11.0–13.0	10.0–12.0	9.3–11.0	6.5–7.8	4.3–5.0
12	13.0–15.5	12.0–14.3	11.0–12.8	7.8–9.3	5.0–6.0
13	15.5–18.0	14.3–16.5	12.8–14.8	9.3–10.8	6.0–7.0
14	18.0–20.8	16.5–19.0	14.8–16.8	10.8–12.3	7.0–8.0
15	20.8–23.5	19.0–21.5	16.8–19.0	12.3–14.0	8.0–9.3
16	23.5–26.5	21.5–24.3	19.0–21.5	14.0–16.0	9.3–10.5
17	26.5–29.8	24.3–27.3	21.5–24.3	16.0–18.0	10.5–11.8
18	29.8–33.3	27.3–30.5	24.3–27.0	18.0–20.0	11.8–13.0
19	33.3–37.0	30.5–33.8	27.0–30.0	20.0–22.0	13.0–14.5
20	37.0–40.8	33.8–37.3	30.0–33.3	22.0–24.5	14.5–16.0
21	40.8–44.8	37.3–41.0	33.3 36.3	24.5–26.8	16.0–17.8

Note.—The radiator orifice plates recommended in this table are made of brass stampings 0.023 in. thick cup-shaped to be inserted in radiator valve unions.

[a]Flow of Steam Through Orifices into Radiators, by S. S. Sanford and C. B. Sprenger (A.S.H.V.E. TRANSACTIONS, Vol. 37, 1931, p. 371).

of obtaining a more uniform pressure throughout the system. Such a provision may be particularly useful in this system for branches close to the boiler where the drop in the main has not yet been produced. Some orifice systems are proprietary.

SIZING PIPING FOR STEAM HEATING SYSTEMS

The functions of the piping system are the distribution of the steam, the return of the condensate and, in systems where no local air vents are provided, the removal of the air. The distribution of the steam should be rapid, uniform and without noise, and the release of air should be facilitated as much as possible, as an air bound system will not heat readily nor properly. In designing the piping arrangement it is desirable to maintain equivalent resistances in the supply and return piping to and from a radiator. Arranging the piping so the total distance from the

boiler to the radiation is the same as the return piping distance from the heating unit back to the boiler tends to obtain such a result. The condensate which occurs in steam piping as well as in radiators must be drained to prevent impeding the ready flow of the steam and air. The effect of back pressure in the returns and excessive revaporization, such as occurs where condensate is released from pressures considerably higher than the vacuum or pressure in the return, must be avoided.

It is important that steam piping systems distribute steam not only at full *design* load but during excess and partial loads. Usually the average winter steam demand is less than half of the demand at the *design* outside temperature. Moreover, in rapidly warming up a system even in moderate weather, the load on the steam main and returns may exceed the maximum operating load for severe weather due to the necessity of raising the temperature of the metal in the system to the steam temperature and the building to the *design* indoor temperature. Investigations of the

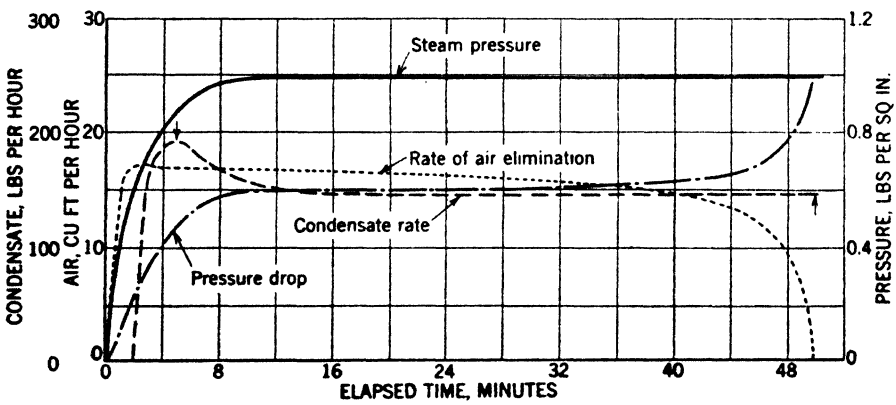


FIG. 18. RELATION BETWEEN ELASPED TIME, STEAM PRESSURE, CONDENSATE AND AIR ELIMINATION RATES

return of condensate have revealed that as high as 143 per cent of the design condensation rate may exist under conditions of actual operation.

The piping design of a heating system is greatly influenced by its operating characteristics. Heating systems do not operate under constant conditions as they are continually changing due to variation in load. As the system is being filled with steam the pressures existing in various locations may be different from those which exist for appreciable periods at other locations although at equilibrium conditions the pressures are approximately the same. In designing piping it is of especial importance to arrange the system to preclude trouble caused by such pressure differences. The systems which readily release the air permit uniform pressures to be attained in much shorter time intervals than those which are sluggish. Results are given in Fig. 18 from investigations [1] to determine the rate of condensate and air return from a two-pipe gravity heating system. Variations in the steam pressure during the warming-up period when the rate of air elimination and condensation is high are clearly indicated in these curves.

It is evident that the condensate flow during the initial warming-up period reaches a peak which is greater than the constant condensing rate eventually reached when the pressure becomes uniform. Moreover, the peak condensing rate is obtained when the system steam pressure is

lower than that existing during a period of constant condensing rate. It will also be noted that the peak rate of air elimination does not coincide with the higher condensing rate.

Steam Flow

The rate of flow of dry steam or steam with a small amount of water flowing in the same direction is in accordance with the general laws of gas flow and is a function of the length and diameter of the pipe, the density of the steam, and the pressure drop through the pipe. This relationship has been established by Babcock in the formula given at the top of Table 2. In Columns 1, 2, 3, and 4 of this table, the numerical values of the factors for different pressure losses, pipe diameters, steam densities and lengths of pipe have been worked out in convenient form so that the steam flowing in any pipe may be calculated by multiplying together the proper factors in each column as shown in the example at the bottom of the table.

Pipe Sizes

The determination of pipe sizes for a given load in steam heating depends on the following principal factors:

1. The initial pressure and the total pressure drop which may be allowed between the source of supply and the end of the return system.
2. The maximum velocity of steam allowable for quiet and dependable operation of the system, taking into consideration the direction of condensate flow.
3. The equivalent length of the run from the boiler or source of steam supply to the farthest heating unit.
4. The direction of flow of the condensate, whether against or with the steam.

Initial Pressure and Pressure Drop

Theoretically there are several factors to be considered, such as initial pressure and pressure required at the end of the line, but it is most important that: (1) the total pressure drop does not exceed the initial gage pressure of the system and in actual practice it should never exceed one-half of the initial gage pressure; (2) the pressure drop is not so great as to cause excessive velocities; (3) there is a constant initial pressure, except on systems specially designed for varying initial pressures, such as the sub-atmospheric, which normally operate under controlled partial vacua, and orifice and vapor systems which at times operate under such partial vacua as may be obtained due to the condition of the fire; and (4) the rise in water due to pressure drop does not exceed the difference in level, for gravity return systems, between the lowest point on the steam main, the heating units, or the dry return, and the boiler water line.

All systems should be designed for a low initial pressure and a reasonably small pressure drop for two reasons: *first*, the present tendency in steam heating unmistakably points toward a constant lowering of pressures even to those below atmospheric; *second*, a system designed in this manner will operate under higher pressures without difficulty. When a system designed for a relatively high initial pressure and a relatively high pressure drop is operated at a lower pressure, it is likely to be noisy and have poor circulation.

The total pressure drop should never exceed one-half of the initial gage pressure when condensate is flowing in the same direction as the steam. Where the condensate must flow counter to the steam, the governing factor is the velocity permissible without interfering with the condensate flow. A.S.H.V.E. Research Laboratory experiments limit this to the capacities given in Table 3 for horizontal pipes at varying grades.

TABLE 2. FLOW OF STEAM IN PIPES

P = loss in pressure in pounds per square inch.
D = inside diameter of pipe in inches.
L = length of pipe in feet.
d = weight of 1 cu ft of steam.
W = pounds of steam per hour.

$$W = 5220\sqrt{\frac{PdD^5}{\left(1+\frac{3.6}{D}\right)L}}$$

$$P = 0.0000000367\left(1+\frac{3.6}{D}\right)\frac{W^2L}{dD^5}$$

Pressure Loss in Ounces	Col. 1 $5220\sqrt{\frac{P}{100}}$	Pipe Size Nominal	Pipe Size Actual Internal Diameter	Internal Area of Pipe Sq Inches	Col. 2 $\sqrt{\frac{D^5}{1+\frac{3.6}{D}}}$	Avg Steam Press. psig	Col. 3 $\sqrt{d}$	Length of Pipe in Feet	Col. 4 $\sqrt{\frac{100}{L}}$
0.25	65.28	1	1.049	0.864	0.536	−1.0[a]	0.187	20	2.240
0.50	92.28	1¼	1.380	1.496	1.178	−0.5[a]	0.190	40	1.580
1.00	130.5	1½	1.610	2.036	1.828	0.0	0.193	60	1.290
2	184.6	2	2.067	3.356	3.710	0.3	0.195	80	1.120
3	226.0	2½	2.469	4.788	6.109	1.3	0.201	100	1.000
4	261.0	3	3.068	7.393	11.183	2.3	0.207	120	0.912
5	291.8	3½	3.548	9.887	16.705	5.3	0.223	140	0.841
6	319.7	4	4.026	12.730	23.631	10.3	0.248	160	0.793
7	345.3	4½	4.506	15.947	32.134	15.3	0.270	180	0.741
8	369.1	5	5.047	20.006	43.719	20.3	0.290	200	0.710
10	412.7	6	6.065	28.886	71.762	30.3	0.326	250	0.632
12	452.0	7	7.023	38.743	106.278	40.3	0.358	300	0.578
14	488.3	8	7.981	50.027	149.382	50.3	0.388	350	0.538
16	522.0	9	8.941	62.786	201.833	60.3	0.415	400	0.500
20	583.6	10	10.020	78.854	272.592	75.3	0.452	450	0.477
24	639.3	12	12.000	113.098	437.503	100.3	0.507	500	0.447
28	690.5	14	13.250	137.880	566.693	125.3	0.557	600	0.407
32	738.2	16	15.250	182.655	816.872	150.3	0.603	700	0.378
40	825.4					175.3	0.645	800	0.354
48	904.1					200.3	0.685	900	0.333
80	1167.2							1000	0.316
160	1650.7							1200	0.289
320	2334.5							1500	0.258
480	2859.1							2000	0.224

Column 1 × 2 × 3 × 4 = lb of steam per hour that will flow through a straight pipe for a given condition.

Example 1: 1 oz drop — 2 in. pipe — 1.3 lb press. — 100 ft equivalent length:

130.5 × 3.710 × 0.201 × 1 = 97.2 lb per hour.
97.2 × 4[b] = 388.8 sq ft equivalent radiation.

Table 1 does not allow for entrained water in low-pressure steam, condensation in covered pipe and roughness in commercial pipe as found in practice.

[a] Pounds per square inch gage = 2.04 in. Vacuum, Mercury Column.
[b] The factor 4 is the approximate equivalent in square feet of steam radiation of 1 lb of steam per hour.

Maximum Velocity

The capacity of a steam pipe in any part of a steam system depends upon the quantity of condensate present, the direction in which the condensate is flowing, and the pressure drop in the pipe. Where the quantity of condensate is limited and is flowing in the same direction as the steam, only the pressure drop need be considered. When the condensate must flow against the steam, even in limited quantity, the velocity of the steam must not exceed limits above which the disturbance between the steam and the counter-flowing water may produce objectionable sounds, such as water hammer, or may result in the retention of water in certain parts of the system until the steam flow is reduced sufficiently to permit the water to pass. The velocity at which such disturbances take place is a function of (1) the pipe size, whether the pipe

TABLE 3. COMPARATIVE CAPACITY OF STEAM LINES AT VARIOUS PITCHES FOR STEAM AND CONDENSATE FLOWING IN OPPOSITE DIRECTIONS[a]

Pitch of Pipe in Inches per 10 Ft. Velocity in Ft per Sec.

PITCH OF PIPE	¼ IN.		½ IN.		1 IN.		1¼ IN.		2 IN.		3 IN.		4 IN.		5 IN.	
Pipe Size Inches	Capacity	Max. Vel.	Capacity	Max. Vel.	Capacity	Max. Vel.	Capacity	Max. Vel.	Capacity	Max. Vel.	Capacity	Max. Vel.	Capacity	Max. Vel.	Capacity	Max. Vel.
	Capacity Expressed in Square Feet E D R															
¾	25.0	12	30.3	14	37.3	18	40.4	19	42.5	20	46.1	21	47.5	22	49.3	23
1	45.8	12	52.6	15	63.0	17	70.0	20	75.2	22	83.0	23	87.9	25	90.2	26
1¼	104.9	18	117.2	20	133.0	23	144.5	25	154.0	27	165.0	28	172.6	29	178.2	31
1½	142.6	18	159.0	21	181.0	23	196.5	25	209.3	27	224.0	28	234.8	30	242.6	31
2	236.0	19	263.5	20	299.5	23	325.5	25	346.5	27	371.5	28	388.4	29	401.1	30
	Capacity Expressed in Pounds per Hour															
¾	6.3	12	7.6	14	9.3	18	10.1	19	10.6	20	11.5	21	11.9	22	12.3	23
1	11.5	12	13.2	15	15.8	17	17.5	20	18.8	22	20.8	23	22.0	25	22.6	26
1¼	26.2	18	29.3	20	33.3	23	36.1	25	38.5	27	41.3	28	43.2	29	44.6	31
1½	35.7	18	39.8	21	45.3	23	49.1	25	52.3	27	56.0	28	58.7	30	60.7	31
2	59.0	19	65.9	20	74.9	23	81.4	25	86.6	27	92.4	28	97.1	29	100.3	30

[a]Data from AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS Research Laboratory.

runs horizontally or vertically, (2) the pitch of the pipe if it runs horizontally, (3) the quantity of condensate flowing against the steam, and (4) freedom of the piping from water pockets which under certain conditions act as a restriction in pipe size.

Reaming Important

Three factors of uncertainty always exist in determining the capacity of any steam pipe. The first is variation in manufacture, which apparently cannot be avoided. The second is the care used in reaming the ends of the pipe after cutting. The effect of both of these factors increases as the pipe size decreases. According to A.S.H.V.E. Research Laboratory tests, either of these factors may affect the capacity of a 1-in. pipe as much as 20 per cent. The third factor is the uniformity in grading the pipe line. All of the capacity tables given in this chapter include a factor of safety. However, the factor of safety referred to does not cover abnormal defects or constrictions *nor does it cover pipe not properly reamed.*

Equivalent Length of Run

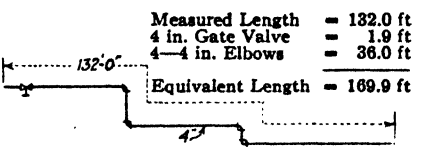
All tables for the flow of steam in pipes, based on pressure drop, must allow for the friction offered by the pipe as well as for the additional resistance of the fittings and valves. These resistances generally are stated in terms of straight pipe; in other words, a certain fitting will produce a drop in pressure equivalent to so many feet of straight run of the same size of pipe. Table 4 gives the number of feet of straight pipe usually allowed for the more common types of fittings and valves. In all pipe sizing tables in this chapter the *length of run* refers to the *equivalent length of run* as distinguished from the *actual length* of pipe in feet. The

TABLE 4. LENGTH IN FEET OF PIPE TO BE ADDED TO ACTUAL LENGTH OF RUN—OWING TO FITTINGS—TO OBTAIN EQUIVALENT LENGTH

SIZE OF PIPE INCHES	LENGTH IN FEET TO BE ADDED TO RUN				
	Standard Elbow	Side Outlet Tee	Gate Valve[a]	Globe Valve[a]	Angle Valve[a]
½	1.3	3	0.3	14	7
¾	1.8	4	0.4	18	10
1	2.2	5	0.5	23	12
1¼	3.0	6	0.6	29	15
1½	3.5	7	0.8	34	18
2	4.3	8	1.0	46	22
2½	5.0	11	1.1	54	27
3	6.5	13	1.4	66	34
3½	8	15	1.6	80	40
4	9	18	1.9	92	45
5	11	22	2.2	112	56
6	13	27	2.8	136	67
8	17	35	3.7	180	92
10	21	45	4.6	230	112
12	27	53	5.5	270	132
14	30	63	6.4	310	152

[a]Valve in full open position.

Example of length in feet of pipe to be added to actual length of run.



length of run is not usually known at the outset; hence it may be necessary to assume some pipe size at the start. Such an assumption frequently is considerably in error and a more common and practical method is to assume the length of run and to check this assumption after the pipes are sized. For this purpose the length of run usually is taken as double the actual length of pipe.

TABLES FOR PIPE SIZING FOR LOW PRESSURE SYSTEMS[2]

Tables 5, 6, and 7 are based on the actual inside diameters of the pipe and the condensation of ¼ lb (4 oz) of steam per square foot of equivalent direct radiation (*abbreviated EDR*) per hour. The drops indicated are drops in pressure per 100 ft of equivalent length of run. The pipe is assumed to be well reamed and without unusual or noticeable defects.

Table 5. Steam Pipe Capacities for Low Pressure Systems

(Reference to this table will be by column letter *A* through *L*)

This table is based on pipe size data developed through the research investigations of the American Society of Heating and Ventilating Engineers.

Pipe Size In.	Capacities of Steam Mains and Risers — Direction of Condensate Flow in Pipe Line: With the Steam in One-Pipe and Two-Pipe Systems: ⅛ psi or ½ Oz Drop	1/16 psi or ¼ Oz Drop	⅛ psi or 1 Oz Drop	⅛ psi or 2 Oz Drop	¼ psi or 4 Oz Drop	½ psi or 8 Oz Drop	Against the Steam Two-Pipe Only: Vertical	Horizontal	Special Capacities for One-Pipe Systems Only: Supply Risers Up-Feed	Radiator Valves and Vertical Connections	Radiator and Riser Runouts
A	*B*	*C*	*D*	*E*	*F*	*G*	*H*[a]	*I*[a]	*J*[b]	*K*	*L*[c]
	Capacity Expressed in Square Feet E D R										
¾	.....	.....	30	.....	.....	.....	30	.....	25	.....	.....
1	39	46	56	79	111	157	56	34	45	28	28
1¼	87	100	122	173	245	346	122	75	98	62	62
1½	134	155	190	269	380	538	190	108	152	93	93
2	273	315	386	546	771	1,091	386	195	288	169	169
2½	449	518	635	898	1,270	1,800	635	395	464	.....	260
3	822	948	1,160	1,650	2,330	3,290	1,130	700	800	.....	475
3½	1,230	1,420	1,740	2,460	3,470	4,910	1,550	1,150	1,140	.....	745
4	1,740	2,010	2,460	3,480	4,910	6,950	2,040	1,700	1,520	.....	1,110
5	3,210	3,710	4,550	6,430	9,090	12,900	.....	3,150	.....	.....	2,180
6	5,280	6,100	7,460	10,550	14,900	21,100	.....	.....	.....	.....	.....
8	11,000	12,700	15,500	21,970	31,070	43,900	.....	.....	.....	.....	.....
10	20,000	23,100	28,300	40,100	56,700	80,200	.....	.....	.....	.....	.....
12	32,000	37,100	45,500	64,300	91,000	129,000	.....	.....	.....	.....	.....
16	61,000	69,700	84,800	121,000	170,000	242,000	.....	.....	.....	.....	.....
	Capacity Expressed in Pounds per Hour										
¾	.....	.....	8	.....	.....	.....	8	.....	6	.....	7
1	10	12	14	20	28	40	14	9	11	7	7
1¼	22	25	31	43	61	87	31	19	20	16	16
1½	34	39	48	67	95	135	48	27	38	23	23
2	68	79	97	137	193	273	97	49	72	42	42
2½	112	130	159	225	318	449	159	99	116	.....	65
3	206	237	291	411	581	822	282	175	200	.....	119
3½	307	355	434	614	869	1,230	387	288	286	.....	186
4	435	503	614	869	1,230	1,740	511	425	380	.....	278
5	806	928	1,140	1,610	2,270	3,210	.....	788	.....	.....	545
6	1,320	1,520	1,870	2,640	3,730	5,280	.....	.....	.....	.....	.....
8	2,750	3,170	3,880	5,490	7,770	11,000	.....	.....	.....	.....	.....
10	5,010	5,790	7,090	10,000	14,200	20,000	.....	.....	.....	.....	.....
12	8,040	9,290	11,400	16,100	22,700	32,200	.....	.....	.....	.....	.....
16	15,100	17,400	21,200	30,300	42,400	60,500	.....	.....	.....	.....	.....
	All Horizontal Mains and Down-Feed Risers						Up-Feed Risers	Mains and Undripped Runouts	Up-Feed Risers	Radiator Connections	Runouts Not Dripped

Note.—Steam at an average pressure of 1 psi is used as a basis for calculating capacities. All drops shown are in psi per 100 ft of equivalent run—based on pipe properly reamed.

[a] Do not use Column *H* for drops of 1/16 or 1/32 psi; substitute Column *C* or Column *B* as required.

[b] Do not use Column *J* for drop of 1/32 psi except on sizes 3 in. and over; below 3 in. substitute Column *B*.

[c] On radiator runouts over 8 ft long increase one pipe size over that shown in Table 4.

TABLE 6. RETURN PIPE CAPACITIES FOR LOW PRESSURE SYSTEMS

Capacity Expressed in Square Feet of Equivalent Direct Radiation

(Reference to this table will be by column letter *M* through *EE*)

This table is based on pipe size data developed through the research investigations of the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS.

Pipe Size Inches	CAPACITY OF RETURN MAINS AND RISERS																	
	MAINS																	
	1/32 Psi or 1/2 Oz Drop per 100 Ft			1/24 Psi or 3/8 Oz Drop per 100 Ft			1/16 Psi or 1 Oz Drop per 100 Ft			1/8 Psi or 2 Oz Drop per 100 Ft			1/4 Psi or 4 Oz Drop per 100 Ft			1/2 Psi or 8 Oz Drop per 100 Ft		
	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.
M	*N*	*O*	*P*	*Q*	*R*	*S*	*T*	*U*	*V*	*W*	*X*	*Y*	*Z*	*AA*	*BB*	*CC*	*DD*	*EE*
3/4	.....	.....	.....	.....	.....	326	.....	.....	400	.....	.....	568	.....	.....	800	.....	.....	1,130
1	500	248	.....	580	285	570	700	320	700	1,000	412	994	1,400	460	1,400	.....	.....	1,980
1 1/4	850	520	.....	990	595	976	1,200	670	1,200	1,700	868	1,700	2,400	962	2,400	.....	.....	3,390
1 1/2	1,350	822	.....	1,570	943	1,550	1,900	1,060	1,900	2,700	1,360	2,700	3,800	1,510	3,800	.....	.....	5,370
2	2,800	1,880	.....	3,240	2,140	3,260	4,000	2,300	4,000	5,600	2,960	5,680	8,000	3,300	8,000	.....	.....	11,300
2 1/2*	4,700	3,040	.....	5,300	3,470	5,450	6,700	3,800	6,700	9,400	4,900	9,510	13,400	5,450	13,400	.....	.....	18,900
3	7,500	5,840	.....	8,500	6,250	8,710	10,700	7,000	10,700	15,000	9,000	15,200	21,400	10,000	21,400	.....	.....	30,200
3 1/2	11,000	7,880	.....	13,200	8,800	13,000	16,000	10,000	16,000	22,000	12,900	22,700	32,000	14,300	32,000	.....	.....	45,200
4	15,500	11,700	.....	18,300	13,400	18,000	22,000	15,000	22,000	31,000	19,300	31,200	44,000	21,500	44,000	.....	.....	62,190
5	.....	.....	.....	.....	.....	31,500	.....	.....	38,700	.....	.....	54,900	.....	.....	77,400	.....	.....	109,000
6	.....	.....	.....	.....	.....	50,450	.....	.....	62,000	.....	.....	88,000	.....	.....	124,000	.....	.....	175,000
	RISERS																	
3/4	.....	190	.....	.....	190	570	.....	190	700	.....	190	994	.....	190	1,400	.....	.....	1,980
1	.....	450	.....	.....	450	976	.....	450	1,200	.....	450	1,700	.....	450	2,400	.....	.....	3,390
1 1/4	.....	990	.....	.....	990	1,550	.....	990	1,900	.....	990	2,700	.....	990	3,800	.....	.....	5,370
1 1/2	.....	1,500	.....	.....	1,500	3,260	.....	1,500	4,000	.....	1,500	5,680	.....	1,500	8,000	.....	.....	11,300
2	.....	3,000	.....	.....	3,000	5,450	.....	3,000	6,700	.....	3,000	9,510	.....	3,000	13,400	.....	.....	18,900
2 1/2	.....	.....	.....	.....	.....	8,710	.....	.....	10,700	.....	.....	15,200	.....	.....	21,400	.....	.....	30,200
3	.....	.....	.....	.....	.....	13,000	.....	.....	16,000	.....	.....	22,700	.....	.....	32,000	.....	.....	45,200
3 1/2	.....	.....	.....	.....	.....	17,900	.....	.....	22,000	.....	.....	31,200	.....	.....	44,000	.....	.....	62,200
4	.....	.....	.....	.....	.....	31,500	.....	.....	38,700	.....	.....	54,900	.....	.....	77,400	.....	.....	109,000
5	.....	.....	.....	.....	.....	50,500	.....	.....	62,000	.....	.....	88,000	.....	.....	124,000	.....	.....	175,000

TABLE 7. RETURN PIPE CAPACITIES FOR LOW PRESSURE SYSTEMS

Capacity Expressed in Pounds per Hour

(Reference to this table will be made by column letter *M* through *EE*)

This table is based on pipe size data developed through the research investigations of the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS.

PIPE SIZE INCHES	CAPACITY OF RETURN MAINS AND RISERS																	
	MAINS																	
	1/16 Psi or 1/2 Oz Drop per 100 Ft			1/24 Psi or 3/8 Oz Drop per 100 Ft			1/16 Psi or 1 Oz Drop per 100 Ft			1/8 Psi or 2 Oz Drop per 100 Ft			1/4 Psi or 4 Oz Drop per 100 Ft			1/2 Psi or 8 Oz Drop per 100 Ft		
	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.	Wet	Dry	Vac.
M	*N*	*O*	*P*	*Q*	*R*	*S*	*T*	*U*	*V*	*W*	*X*	*Y*	*Z*	*AA*	*BB*	*CC*	*DD*	*EE*
3/4	.....	.....	.....	.....	.....	42	.....	.....	100	.....	.....	142	.....	.....	200	.....	.....	283
1	125	62	.....	145	71	143	175	80	175	250	103	249	350	115	350	.....	.....	494
1 1/4	213	130	.....	248	149	244	300	168	300	425	217	426	600	241	600	.....	.....	848
1 1/2	338	206	.....	393	236	388	475	265	475	675	340	674	950	378	950	.....	.....	1,340
2	700	470	.....	810	535	815	1,000	575	1,000	1,400	740	1,420	2,000	825	2,000	.....	.....	2,830
2 1/2	1,180	760	.....	1,580	868	1,360	1,680	950	1,680	2,350	1,230	2,380	3,350	1,360	3,350	.....	.....	4,730
3	1,880	1,460	.....	2,130	1,560	2,180	2,680	1,750	2,680	3,750	2,250	3,800	5,350	2,500	5,350	.....	.....	7,560
3 1/2	2,750	1,970	.....	3,300	2,200	3,250	4,000	2,500	4,000	5,500	3,230	5,680	8,000	3,580	8,000	.....	.....	11,300
4	3,880	2,930	.....	4,580	3,350	4,500	5,500	3,750	5,500	7,750	4,830	7,810	11,000	5,380	11,000	.....	.....	15,500
5	.....	.....	.....	.....	.....	7,880	.....	.....	9,680	.....	.....	13,700	.....	.....	19,400	.....	.....	27,300
6	.....	.....	.....	.....	.....	12,600	.....	.....	15,500	.....	.....	22,000	.....	.....	31,000	.....	.....	43,800
	RISERS																	
3/4	.....	48	.....	.....	48	143	.....	48	175	.....	48	249	.....	48	350	.....	.....	494
1	.....	113	.....	.....	113	244	.....	113	300	.....	113	426	.....	113	600	.....	.....	848
1 1/4	.....	248	.....	.....	248	388	.....	248	475	.....	248	674	.....	248	950	.....	.....	1,340
1 1/2	.....	375	.....	.....	375	815	.....	375	1,000	.....	375	1,420	.....	375	2,000	.....	.....	2,830
2	.....	750	.....	.....	750	1,360	.....	750	1,680	.....	750	2,380	.....	750	3,350	.....	.....	4,730
2 1/2	.....	.....	.....	.....	.....	2,180	.....	.....	2,680	.....	.....	3,800	.....	.....	5,350	.....	.....	7,560
3	.....	.....	.....	.....	.....	3,250	.....	.....	4,000	.....	.....	5,680	.....	.....	8,000	.....	.....	11,300
3 1/2	.....	.....	.....	.....	.....	4,480	.....	.....	5,500	.....	.....	7,810	.....	.....	11,000	.....	.....	15,500
4	.....	.....	.....	.....	.....	7,880	.....	.....	9,680	.....	.....	13,700	.....	.....	19,400	.....	.....	27,300
5	.....	.....	.....	.....	.....	12,600	.....	.....	15,500	.....	.....	22,000	.....	.....	31,000	.....	.....	43,800

Table 5 may be used for sizing piping for steam heating systems by pre-determining the allowable or desired pressure drop per 100 equivalent feet of run and reading from the column for that particular pressure drop. This applies to all steam mains on both one-pipe and two-pipe systems, vapor systems, and vacuum systems. Columns *B* to *G*, inclusive, are used where the steam and condensate flow in the same direction, while Columns *H* and *I* are for cases where the steam and condensate flow in opposite directions, as in risers and runouts that are not dripped. Columns *J*, *K*, and *L* are for one-pipe systems and cover riser, radiator valve and vertical connection sizes, and radiator and runout sizes, all of which are based on the critical velocities of the steam to permit the counter flow of condensate without noise.

Return piping may be sized with the aid of Tables 6 and 7 where pipe capacities for wet, dry, and vacuum return lines are shown for the pressure drops per 100 ft corresponding to the drops in Table 5. *It is customary to use the same pressure drop on both the steam and return sides of a system.*

Example 2. What pressure drop should be used for the steam piping of a system if the measured length of the longest run is 500 ft and the initial pressure is not to be over 2-psi gage?

Solution. It will be assumed, if the measured length of the longest run is 500 ft, that when the allowance for fittings is added the equivalent length of run will not exceed 1,000 ft. Then, with the pressure drop not over one half of the initial pressure, the drop could be 1 psi or less. With a pressure drop of 1 psi and a length of run of 1,000 ft, the drop per 100 ft would be $\frac{1}{10}$ psi, while if the total drop were $\frac{1}{2}$ psi, the drop per 100 ft would be $\frac{1}{20}$ psi. In the first instance the pipe could be sized according to Column *D* for $\frac{1}{16}$ psi per 100 ft, and in the second case, the pipe could be sized according to Column *C* for $\frac{1}{24}$ psi. On completion of the sizing, the drop could be checked by taking the longest line and actually calculating the equivalent length of run from the pipe sizes determined. If the calculated drop is less than that assumed, the pipe size is all right; if it is more, it is probable that there are an unusual number of fittings involved, and either the lines must be straightened or the column for the next lower drop must be used and the lines resized. Ordinarily resizing will be unnecessary.

TABLES FOR PIPE SIZING FOR HIGH PRESSURE SYSTEMS

Many of the recent installations of heating systems for large industrial type buildings have been designed for the use of high pressure steam, that is, without the use of pressure reducing valves. Such systems usually involve the use of unit heaters or large built-up fan units with blast heating coils. Pressures on these systems vary from 30 to 150 psi. Temperatures are controlled by a modulating or throttling type thermostatic valve controlled by the air temperature in the room, fan inlet or outlet.

Tables 8 to 11 may be used for the sizing of steam and return piping for systems of 30 and 150 psi pressure at various pressure drops. These tables are based on Babcock's formula, and have been used as the basis of design for a number of years.

SIZING PIPING FOR ONE-PIPE GRAVITY SYSTEMS

Gravity one-pipe air-vent systems in which the equivalent length of run does not exceed 200 ft should be sized by means of Tables 5, 6 and 7 as follows:

1. *For the steam main and dripped runouts to risers* where the steam and condensate flow in the same direction, use $\frac{1}{16}$-psi drop (Column *D*).

2. *Where the riser runouts are not dripped* and the steam and condensate flow in opposite directions, and *also in the radiator runouts* where the same condition occurs, use Column *L*.

TABLE 8. STEAM PIPE CAPACITIES FOR 30 PSI STEAM SYSTEMS[a]

Capacity Expressed in Pounds per Hour

(Steam and Condensate Flowing in Same Direction)

PIPE SIZE INCHES	DROP IN PRESSURE—POUNDS PER 100 FT IN LENGTH					
	⅛	¼	½	¾	1	2
¾	15	22	31	38	45	63
1	31	46	63	77	89	125
1¼	69	100	141	172	199	281
1½	107	154	219	267	309	437
2	217	313	444	543	627	886
2½	358	516	730	924	1,030	1,460
3	651	940	1,330	1,630	1,880	2,660
3½	979	1,410	2,000	2,450	2,830	4,000
4	1,390	2,000	2,830	3,460	4,000	5,660
5	2,560	3,640	5,230	6,400	7,390	10,500
6	4,210	6,030	8,590	10,400	12,100	17,200
8	8,750	12,600	17,900	21,900	25,300	35,100
10	16,300	23,500	33,200	40,600	46,900	66,400
12	25,600	36,900	52,300	64,000	74,000	104,500

[a]Note: Steam at an average pressure of 30 psi is used as the basis for calculating the above table.

3. *For up-feed steam risers* carrying condensate back from the radiators, use Column *J*.

4. *For down-feed systems the main risers* of which do not carry any radiator condensate use Column *H*.

5. *For the radiator valve size and the stub connection*, use Column *K*.

6. For the *dry return main*, use Column *U*.

7. For the *wet return main* use Column *T*.

On systems exceeding an equivalent length of 200 ft, it is suggested that the total drop be not over ¼ psi. The return piping sizes should correspond with the drop used on the steam side of the system. Thus, where ¼-psi drop is being used, the steam main and dripped runouts would be sized from Column *C*; radiator runouts and undripped riser runouts from Column *L*; up-feed risers from Column *J*; the main riser on a down-feed system from Column *C* (it will be noted that if Column *H* is used the drop would exceed the limit of ¼ psi); the dry return from Column *R*; and the wet return from Column *Q*.

With a ⅛-psi drop the sizing would be the same as for ¼ psi except that the steam main and dripped runouts would be sized from Column *B*,

TABLE 9. STEAM PIPE CAPACITIES FOR 150 PSI STEAM SYSTEMS[a]

Capacity Expressed in Pounds per Hour

(Steam and Condensate Flowing in Same Direction)

PIPE SIZE INCHES	DROP IN PRESSURE—PSI PER 100 FT IN LENGTH						
	⅛	¼	½	¾	1	2	5
¾	29	41	58	71	82	116	184
1	58	82	117	143	165	233	369
1¼	130	185	262	320	370	523	827
1½	203	287	407	497	575	813	1,290
2	412	583	825	1,010	1,170	1,650	2,600
2½	683	959	1,360	1,650	1,920	2,710	4,290
3	1,240	1,750	2,480	3,020	3,500	4,940	7,820
3½	1,860	2,630	3,720	4,550	5,250	7,420	11,700
4	2,630	3,720	5,260	6,430	7,430	10,500	16,600
5	4,860	6,880	9,730	11,900	13,800	19,500	30,800
6	7,960	11,300	16,000	19,500	22,600	31,900	50,400
8	16,600	23,500	33,200	40,600	47,000	66,400	105,000
10	30,800	43,400	61,700	75,600	87,300	123,000	195,000
12	48,600	68,800	97,300	119,000	138,000	194,000	307,500

[a]Note: Steam at an average pressure of 150 psi is used as the basis for calculating the above table.

TABLE 10. RETURN PIPE CAPACITIES FOR 30 PSI STEAM SYSTEMS[a]

Capacity Expressed in Pounds per Hour

PIPE SIZE INCHES	DROP IN PRESSURE—POUNDS PER 100 FT IN LENGTH				
	⅛	¼	½	¾	1
¾	115	170	245	308	365
1	230	340	490	615	730
1¼	485	710	1,025	1,290	1,530
1½	790	1,160	1,670	2,100	2,500
2	1,580	2,360	3,400	4,300	5,050
2½	2,650	3,900	5,600	7,100	8,400
3	4,850	7,100	10,300	12,900	15,300
3½	7,200	10,600	15,300	19,200	22,800
4	10,200	15,000	21,600	27,000	32,300
5	19,000	27,800	40,300	55,500	60,000
6	31,000	45,500	65,500	83,000	98,000

[a]Note: The above table is based on steam at pressures of 0 to 4 psi.

the main riser on a down-feed system from Column *B*, the dry return from Column *O*, and the wet return from Column *N*.

Notes on Gravity One-Pipe Air-Vent Systems

1. Pitch of mains should not be less than ¼ in. in 10 ft.

2. Pitch of horizontal runouts to risers and radiators should not be less than ½ in. per foot. Where this pitch cannot be obtained runouts over 8 ft in length should be one size larger than called for in the table.

3. In general, it is not desirable to have a main less than 2 in. The diameter of the far end of the supply main should not be less than half its diameter at its largest part.

4. Supply mains, runouts to risers, or risers, should be dripped where necessary.

5. Where supply mains are decreased in size they should be dripped, or be provided with eccentric couplings, flush on bottom.

Example 4. Size the one-pipe gravity steam system shown in Fig. 19 assuming that this is all there is to the system or that the riser and main shown involve the longest run on the system.

Solution. The total length of run actually shown is 215 ft. If the equivalent length of run is taken at double this, it will amount to 430 ft, and with a total drop of ¼ psi the drop per 100 ft will be slightly less than 1/16 psi. It would be well in this case to use 1/24 psi, and this would result in the theoretical sizes indicated in Table 12. These theo-

TABLE 11. RETURN PIPE CAPACITIES FOR 150 PSI STEAM SYSTEMS[a]

Capacity Expressed in Pounds per Hour

PIPE SIZE INCHES	DROP IN PRESSURE—PSI PER 100 FT IN LENGTH					
	⅛	¼	⅓	½	1	2
¾	156	232	360	465	560	890
1	313	462	690	910	1,120	1,780
1¼	650	960	1,500	1,950	2,330	3,700
1½	1,070	1,580	2,460	3,160	3,800	6,100
2	2,160	3,300	4,950	6,400	7,700	12,300
2½	3,600	5,350	8,200	10,700	12,800	20,400
3	6,500	9,600	15,000	19,500	23,300	37,200
3½	9,600	14,400	22,300	28,700	34,500	55,000
4	13,700	20,500	31,600	40,500	49,200	78,500
5	25,600	38,100	58,500	76,000	91,500	146,000
6	42,000	62,500	96,000	125,000	150,000	238,000

[a]Note: The above table is based on steam at pressures of 1 to 20 psi.

TABLE 12. PIPE SIZES FOR ONE-PIPE UP-FEED SYSTEM SHOWN IN FIG. 19

PART OF SYSTEM	SECTION OF PIPE	RADIATION SUPPLIED EDR SQ FT	THEORETICAL PIPE SIZE (INCHES)	PRACTICAL PIPE SIZE (INCHES)
Branches to radiators..	.....	100	2	2
Branches to radiators..	.....	50	1¼	1¼
Riser.....	*a* to *b*	200	2	2
Riser.....	*b* to *c*	300	2½	2½
Riser.....	*c* to *d*	400	2½	2½
Riser.....	*d* to *e*	500	3	3
Riser.....	*e* to *f*	600	3	3
Runout to riser.....	*f* to *g*	600	3½	3½
Supply main.....	*g* to *h*	600	3	3
Branch to supply main	*h* to *j*	600	2½	3
Dry return main.....	*f* to *k*	600	1¼	2
Wet return main.....	*k* to *m*	600	1	2
Wet return main.....	*m* to *n*	600	1	2
Wet return main.....	*n* to *p*	600	1	2

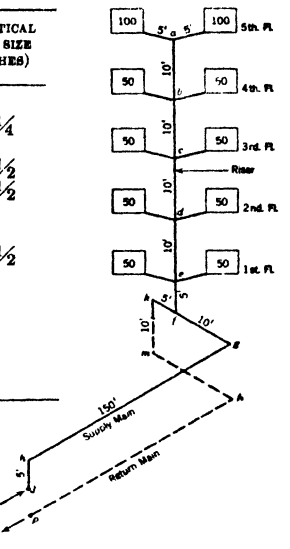


FIG. 19. RISER, SUPPLY MAIN AND RETURN MAIN OF ONE-PIPE SYSTEM

retical sizes, however, should be modified by not using a wet return less than 2 in. while the main supply, *g-h*, if from the uptake of a boiler, should be made the full size of the main, or 3 in. Also the portion of the main *k-m* should be made 2 in. if the wet return is made 2 in.

SIZING PIPING FOR ONE-PIPE VAPOR SYSTEMS

Piping for one-pipe vapor systems is sized so as to permit only a few ounces pressure drop in the system. Otherwise, the method follows that outlined for sizing one-pipe gravity systems.

SIZING PIPING FOR TWO-PIPE HIGH PRESSURE SYSTEMS

Steam piping for two-pipe high pressure can be sized for greater pressure drops than that of the return piping. For a system using steam at 30 psi, the total pressure drop can be 5 to 10 psi and for 150 psi systems, 25 to 30 psi.

It has been observed that the maximum total pressure in the returns of a 30-psi system is about 5 psi, and that of a 150-psi system is about 20 psi. The pressure in the return mains is, of course, caused by the discharge of traps, or by leaky traps and by flashing of condensate into steam due to the lower pressure in the return line. The usual practice in the sizing of high pressure returns has been to size on the basis of ½ psi per 100 ft of pipe for 30-psi systems, and 1 psi per 100 ft for 150-psi systems. This is an average figure which corresponds generally to several of the previously published tables for the design of high pressure return piping.

Notes on Two-Pipe High Pressure Systems

Pitch of mains should not be less than ¼ inch in 10 feet.

Pitch of horizontal runouts to risers and heating units should be not less than ½ inch per foot.

SIZING PIPING FOR TWO-PIPE LOW PRESSURE SYSTEMS

Piping for two-pipe low pressure systems is sized in the same manner as for two-pipe vapor systems, except that the pressure drop throughout the system can be based on ½ psi to 1 psi drop.

SIZING PIPING FOR TWO-PIPE VAPOR SYSTEMS

While many manufacturers of patented vapor heating accessories have their own schedules for pipe sizing, an inspection of these sizing tables indicates that in general as small a drop as possible is recommended. The reasons for this are: (1) to have the condensate return to the boiler by gravity, (2) to obtain a more uniform distribution of steam throughout the system, especially when it is desirable to carry a moderate or low fire, and (3) because with large variations in pressure the value of graduated valves on radiators is destroyed.

For small vapor systems where the equivalent length of run does not exceed 200 ft, it is recommended that the main and any runouts to risers that may be dripped should be sized from Column *D*, Table 5, while riser runouts not dripped and radiator runouts should employ Column *I*. The up-feed steam risers should be taken from Column *H*. On the returns, the risers should be sized from Tables 6 and 7, Column *U*, (lower portion) and the mains from Column *U* (upper portion). It should again be noted that the pressure drop in the steam side of the system is kept the same as on the return side except where the flow in the riser is concerned.

On a down-feed system the main vertical riser should be sized from Column *H*, but the down-feed risers can be taken from Column *D* although it so happens that the values in Columns *D* and *H* for small systems correspond. This will not hold true in larger systems.

For vapor systems over 200 ft of equivalent length, the drop should not exceed ⅛ psi to ¼ psi, if possible. Thus, for a 400 ft equivalent run the drop per 100 ft should be not over ⅛ psi divided by 4, or 1/32 psi. In this case the steam mains would be sized from Column *B*, the radiator and undripped riser runouts from Column *I*; the risers from Column *B*, because Column *H* gives a drop in excess of 1/32 psi. On a down-feed system, Column *B* would have to be used for both the main riser and the smaller risers feeding the radiators in order not to increase the drop over 1/32 psi. The return risers would be sized from the lower portion of Column *O* and the dry return main from the upper portion of the same column, while any wet returns would be sized from Column *N*. The same pressure drop is applied on both the steam and the return sides of the system.

Notes on Vapor Systems

1. Pitch of mains should not be less than ¼ in. in 10 ft.
2. Pitch of horizontal runouts to risers and radiators should not be less than ½ in. per foot. Where this pitch cannot be obtained runouts over 8 ft in length should be one size larger than called for in the table.
3. In general it is not desirable to have a supply main smaller than 2 in.
4. When necessary, supply main, supply risers, or runouts to supply risers should be dripped separately into a wet return, or may be connected into the dry return through a thermostatic drip trap.

SIZING PIPING FOR TWO-PIPE VACUUM SYSTEMS

Vacuum, atmospheric, sub-atmospheric and orifice systems are usually employed in large installations and have total drops varying from ¼ to

½ psi. Systems in which the maximum equivalent length does not exceed 200 ft preferably employ the smaller pressure drop, while systems over 200 ft equivalent length of run more frequently are designed for the higher drop, owing to the relatively greater saving in pipe sizes. For example, a system with 1200 ft longest equivalent length of run would employ a drop per 100 ft of ½ psi divided by 12, or 1/24 psi. In this case, the steam main would be sized from Column *C*, Table 5, and the risers also from Column *C* (Column *H* could be used as far as critical velocity is concerned but the drop would exceed the limit of 1/24 psi). Riser runouts, if dripped, would use Column *C* but if undripped would use Column *I*; radiator runouts, Column *I*; return risers, lower part of Column *S*, Tables 6 and 7; return runouts to radiators, one pipe size larger than the radiator trap connections.

Notes on Vacuum Systems

1. It is not generally considered good practice to exceed ⅛ psi drop per 100 ft of equivalent run nor to exceed 1 psi total pressure drop in any system.

2. Pitch of mains should not be less than ¼ in. in 10 ft.

3. Pitch of horizontal runouts to risers and radiators should not be less than ½ in. per foot. Where this pitch cannot be obtained runouts over 8 ft in length should be one size larger than called for in the table.

4. In general it is not considered desirable to have a supply main smaller than 2 in.

5. When necessary, the supply main, supply riser, or runout to a supply riser should be dripped separately through a trap into the vacuum return. A connection should not be made between the steam and return sides of a vacuum system without interposing a trap to prevent the steam from entering the return line.

6. Lifts should be avoided if possible, but when they cannot be eliminated they should be made in the manner described in this chapter.

7. No lifts can be used in orifice and atmospheric systems. In sub-atmospheric systems the lift must be at the vacuum pump.

SIZING PIPING FOR INDIRECT HEATING UNITS

Pipe connections and mains for indirect heating units are sized in a manner similar to radiators, but the equivalent direct radiation must be ascertained for each row of heating unit stacks and then must be divided into the number of stacks constituting that row and into the number of connections to each stack.

$$EDR = \frac{Q \times 60 \times (t_1 - t_e)}{55.2 \times 240} = \frac{Q \times (t_1 - t_e)}{220.8} \qquad (1)$$

where

EDR = equivalent direct radiation, square feet.

Q = volume of air, cubic feet per minute.

t_e = the temperature of the air entering the row of heating units under consideration, Fahrenheit degrees.

t_1 = the temperature of the air leaving the row of heating units under consideration, Fahrenheit degrees.

60 = the number of minutes in one hour.

55.2 = the number of cubic feet of air heated 1 Fahrenheit degree by 1 Btu.

240 = Btu equivalent of 1 sq ft of EDR.

Example 3. **Assume that a 3-row heating unit shown in this chapter in Fig. 38 is handling 50,000 cfm of air and that the rise in the first row is from 0 to 40 F, in the second row from 40 to 65 F, and in the third row from 65 to 80 F. What is the load in EDR on each supply and return connection?**

Solution. For row 1,

$$R = \frac{50{,}000 \times (40 - 0)}{220.8} = 9058 \text{ sq ft.}$$

For row 2,

$$R = \frac{50{,}000 \times (65 - 40)}{220.8} = 5661 \text{ sq ft.}$$

For row 3,

$$R = \frac{50{,}000 \times (80 - 65)}{220.8} = 3397 \text{ sq ft.}$$

Each row of heating units consists of four stacks and each stack has two connections so that the load on each stack and each connection of the stack is as follows:

Row	Total Load (EDR)	Stack Load[a] (EDR)	Connection Load[b] (EDR)
1	9058	2265	2265 or 1132
2	5661	1415	1415 or 708
3	3397	849	849 or 425

[a]One quarter of total row load.

[b]One half of stack load if two steam connections are made; otherwise, same as stack load.

The pipe sizes would then be based on the length of the run and the pressure drop desired, as in the case of radiators. It generally is considered desirable to place the indirect heating units on a separate system and not on supply or return lines connected to the general heating system.

Most manufacturers of heating coils now publish condensing capacities of their coils for all common operating conditions in pounds of steam per hour per square foot of face area (or free area for some designs). These rates may be used in connection with Tables 5 to 7 to size the piping.

PRESSURE REDUCING VALVES

While the illustrations given in Figs. 2 to 17 inclusive indicate the various systems to be supplied by separate boiler plants, it is also possible to have steam supplied at high pressure by a boiler plant remotely located. In this case steam is supplied directly to the system or through a pressure reducing valve. Condensate can either be returned to the boiler plant or wasted to the sewer. The general arrangement of the systems fed through a pressure reducing valve will not vary from those illustrated with a boiler supply.

When high pressure steam is being supplied and lower steam pressures are required for heating, for domestic hot water, for utility services, etc., one or more pressure reducing valves (pressure regulators) are required.

These are used in two classes of service, one where the steam must be shut off tight to prevent the low pressure building up at time of no load, and the other where the low pressure lines will condense enough steam to offset normal leaking through the valve. In the latter case, double seated valves may be used in a manner that reduces the work required of the diaphragm in closing the valve and consequently the size of the diaphragm. These valves also control the low pressures more closely under conditions of varying high pressures.

Valves that shut off all steam are called *dead end* type. They are single seated, and some of them have pilot operation that provides close control of the reduced pressure. If a thermostatically controlled valve is installed

after, and near, a reducing valve in such a manner as to cut off the passage of steam, the dead end type should be used.

It is common practice when the initial steam pressure is 100 psi or higher to install two-stage reduction. If the radiation served is cast-iron, the *A.S.M.E.* code requires two reducing valves when the inlet pressure exceeds 50 psi. This makes a quieter condition of steam flow, as it is apparent that with one reduction, as for example from 150 to 2 psi, there is a smaller opening with greater velocity across the reducing valve and, consequently, more noise. A two-stage reduction also introduces a source of safety, since if one reducing valve were to build up its discharge pressure, this excess pressure would not be so great as the case might be in a one-stage reduction.

If an installation requires single seated valves and the pilot type cannot be used, it is necessary to use two-stage reduction, as single seated valves require sufficient diaphragm area to overcome the unbalanced pressure underneath the single valve. In many cases the large diameter of diaphragm required would make it impractical in construction. With a two-stage reduction the diaphragm diameter required would be reduced. If a one-stage reduction is desired, it is necessary to use a pilot controlled pressure reducing valve, where low pressures are to be maintained closely.

In making a two-stage reduction, allowance for expansion of steam on the low pressure side of the valve should be made by increasing the pipe size. This also allows steam flow to be at a more nearly uniform velocity. Separating the valves by a distance up to 20 ft is recommended to reduce excessive hunting action of the first valve.

When the reduced pressure is approximately 15 psi or lower, the weight and lever diaphragm valve gives the best results with minimum maintenance. Above 15 psi, spring loaded diaphragm valves should be used, because of the extra weights required on weight and lever type. Pressure equalizing lines should not be connected too close to the valve. They should be connected into the bottom of the reduced pressure steam main, to allow maximum condensate to exist in the equalizing lines, or the connection can be made into the top of the main if a water accumulator is used to reduce the variation of the head of water on the diaphragm.

Care should be exercised in selecting the size of a reducing valve. The safest method is to consult the manufacturer. It is essential that sizes of piping to and from the reducing valve be such that they will pass the desired amount of steam with the maximum velocity desired. A common error is to make the size of the reducing valve the same size as that of the service, or outlet pipe size. Generally, this will make the reducing valve oversized, and bring about wire-drawing of valve and seat, due to small lift of the valve seat.

On installations where the steam requirements are relatively large and variable in mild weather or reduced demand periods, wire-drawing may occur. To overcome this condition, two reducing valves are installed in parallel, with the sizes selected on a 70 and 30 per cent proportion of maximum flow. For example, if 50,000 lb of steam per hour are required, the size of one valve is on the basis of $0.7 \times 50{,}000$ lb, or 35,000 lb, and the other on the basis of $0.3 \times 50{,}000$ lb, or 15,000 lb. During the mild or reduced demand periods, steam will flow through the smaller valve only. During the remainder of the season, the larger valve is set to control at whatever low pressure is desired, and the smaller one at a somewhat lower pressure. Thus, when steam flow is not at its maximum, the smaller valve is closed, but it opens automatically when the maximum

steam demand occurs, because this maximum demand creates a slight pressure drop in the service line.

The installation of reducing valves in pipe lines requires detailed planning. They should be installed to give ease of access for inspection and repair, and wherever possible with diaphragm downward, except in cases of pilot operated valves.

There should be a by-pass around each reducing valve of size equal to one-half the size of reducing valve. The globe valve in by-pass line should be of a better type of construction, and must shut off absolutely tight. A steam pressure gage, graduated up to the initial pressure, should be installed on the low pressure side. Safety valves located on the low pressure side should be set 5 psi higher than the final pressure but may be 10 psi higher than the reduced pressure if this reduced pressure is that of the first stage reduction of a double reduction. Strainers are sometimes installed on the inlet to the reducing valve but are not required before a second-stage reduction. If a two-stage reduction is made, it is well to install a pressure gage immediately before the reducing valve of the second-stage reduction also. In sizes 3 in. and above, it is advisable to install a drip trap between the two reducing valves.

BOILER CONNECTIONS

Steam

Cast-iron, sectional heating boilers usually have several outlets in the top. Two or more outlets should be used whenever possible to reduce the velocity of the steam in the vertical uptakes from the boiler and thus to prevent water being carried over into the steam main.

Return

Cast-iron boilers are generally provided with return tappings on both sides, while steel boilers are generally equipped with only one return tapping. Where two tappings are provided, both should be used to effect proper circulation through the boiler. The return connection should include either a Hartford return connection or a check valve to prevent the accidental loss of boiler water to the returns with consequent danger of boiler damage. The Hartford return connection is to be preferred over the check valve because the latter is apt to stick or not close tightly and, furthermore, because the check valve offers additional resistance to the condensate coming back to the boiler, which in gravity systems would raise the water line in the far end of the wet return several inches.

In order to prevent the boiler from losing its water under any circumstances, the use of the Hartford return connection is recommended. This connection for a one- or two-boiler installation is shown in Fig. 20. The essential features of construction of a Hartford return connection are: (1) a direct connection (made without valves) between the steam side of the boiler and the return side of the boiler, and (2) a close nipple, or preferably an inverted Y-fitting connection about 2 in. below the normal boiler water line from the return main to the boiler steam and return pressure balance connection. Equalizing pipe connections between the steam and return are given in Fig. 20, based on grate areas, but in no case shall this pipe size be less than the main return piping from the system.

Sizing Boiler Connections

Little information is available on the sizing of boiler runouts and steam headers. Although some engineers prefer an enlarged steam header to

serve as additional steam storage space, there ordinarily is no sudden demand for steam in a steam heating system except during the heating-up period, at which time a large steam header is a disadvantage rather than an advantage. The boiler header may be sized by first computing the maximum load that must be carried by any portion of the header under any conceivable method of operation, and then applying the same schedule of pipe sizing to the header as is used on the steam mains for the building. The horizontal runouts from the boiler, or boilers, may be sized by calculating the heaviest load that will be placed on the boiler at any time, and sizing the runout on the same basis as the building mains. The difference in size between the vertical uptakes from the boiler, which should be of same size as the boiler outlet tapping, and the horizontal main or runout is compensated for by the use of reducing ells.

Return connections to boilers in gravity systems are made the same size as the return main itself. Where the return is split and connected to

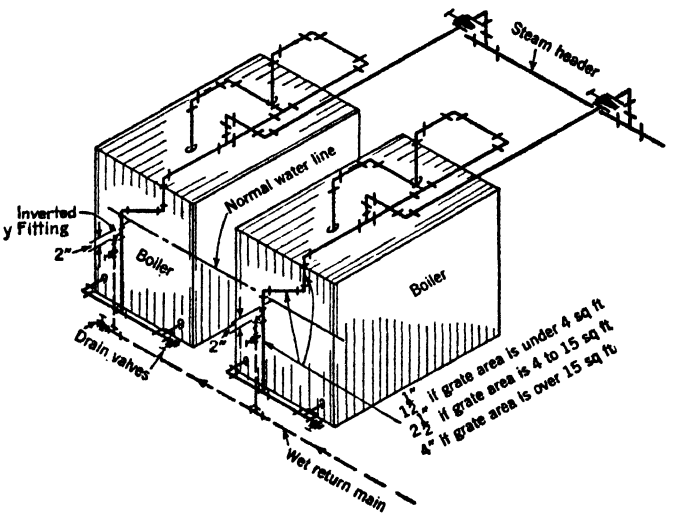


FIG. 20. THE HARTFORD RETURN CONNECTION

two tappings on the same boiler, both connections are made the full size of the return line. Where two or more boilers are in use, the return to each may be sized to carry the full amount of return for the maximum load which that boiler will be required to carry. Where two boilers are used, one of them being a spare, the full size of the return main would be carried to each boiler, but if three boilers are installed, with one spare, the return line to each boiler would require only half of the capacity of the entire system, or, if the boiler capacity were more than one-half the entire system load, the return would be sized on the basis of the maximum boiler capacity. As the return piping around the boiler is usually small and short, it should not be sized to the minimum.

With returns pumped from a vacuum or receiver return pump, the size of the line may be calculated from the water rate on the pump discharge when it is operating, and the line sized for a very small pressure drop. The relative boiler loads should be considered, as in the case of gravity return connections. Boiler header and piping sizes should be based on the total load.

CONDENSATE RETURN PUMPS

Condensate return pumps are used for gravity systems when the local conditions do not permit the condensate to return to the boiler under the existing static head. The return of the condensate permits the water to repeatedly go through the cycle of vaporization, with subsequent condensation and return to the boiler. During such repeated cycles any incrustants or other substances in solution are precipitated and the water de-activated to a considerable extent so that corrosion of a serious nature is seldom ever encountered where the condensate is repeatedly used. Serious corrosion is more frequently found in systems in which the condensate is wasted and fresh make-up water is continually being introduced.

The most generally accepted condensate pump unit for low pressure heating systems consists of a motor-driven centrifugal pump with receiver and automatic float control. Other types in use include rotary, screw, turbine and reciprocating pumps with steam turbine or motor drive, and direct-acting steam reciprocating pumps.

The receiver capacities of these automatic units should be sized so as not to cause too great a fluctuation of the boiler water line if fed directly to the boiler and at the same time not so small as to cause too frequent operation of the unit. The usual unit provides storage capacity between stops in the receiver of approximately 1.5 times the amount of condensate returned per minute and the pump generally has a delivery rate of 3 to 4 times the normal flow. This relation of receiver and pump size to heating system condensing capacity takes account of the peak condensation rate.

A typical installation of a motor driven automatic condensate unit is illustrated in Fig. 9.

VACUUM HEATING PUMPS

On vacuum systems, where the returns are under a vacuum, and sub-atmospheric systems, where the supply piping, radiation and the returns are under a vacuum, it is necessary to use a vacuum pump to discharge the air and non-condensable gases to atmosphere and to dispose of the condensate. Direct-acting steam-driven reciprocating vacuum pumps are sometimes used where high pressure steam is available or where the exhaust steam from the pump can be utilized. In general, however, these have been replaced by the automatic motor-driven return line heating pump especially developed for this service. Steam turbine drive is also frequently used where steam at suitable pressures is available, the steam being used afterward for building heating. The usual vacuum pump unit consists of a compact assembly of exhausting unit for withdrawing the air-vapor mixture and discharging the air to atmosphere and a water removal unit which discharges the condensate to the boiler. They are furnished complete with receiver, separating tank and automatic controls mounted as an integrated unit on one base. There are also special steam turbine driven units which are operated by passing the steam to be used in heating the building through the turbine with only a 2 to 3 psi drop across the turbine required for its operation. Under special conditions such as installations where it is necessary to return the condensate to a high pressure boiler, auxiliary water pumps may be supplied. In some instances separate air and water pumps may be used.

For rating purposes[3] vacuum pumps are classified as *low vacuum* and *high vacuum*. Low vacuum pumps are those rated for maintaining 5½ in.

Hg vacuum on the system, and high vacuum pumps are those rated to maintain vacuums above 5½ in.

Manufacturers of vacuum pumps specify that the standard capacity of pumps shall be 0.3 to 0.5 cfm of air removal and 0.5 gpm of water per 1000 *EDR* served. This capacity is at 5½ in. of vacuum and with condensate at 160 F. The larger air capacity is for smaller systems and the smaller capacity for the larger systems.

Some manufacturers, however, specify more air capacity than standard where higher vacuums are desired and where air leakage is suspected.

The vacuum that can be maintained on a system depends upon the relationship of the air leakage rate into the system to the operating air capacity of the hydraulic evacuator when operating at any given return line temperature. The hotter the returns, the lower will be the possible vacuum for a given air leakage rate into the system. It is particularly essential on high vacuum installations to see that the entire system is tight in order to reduce the amount of inward air leakage and, further-

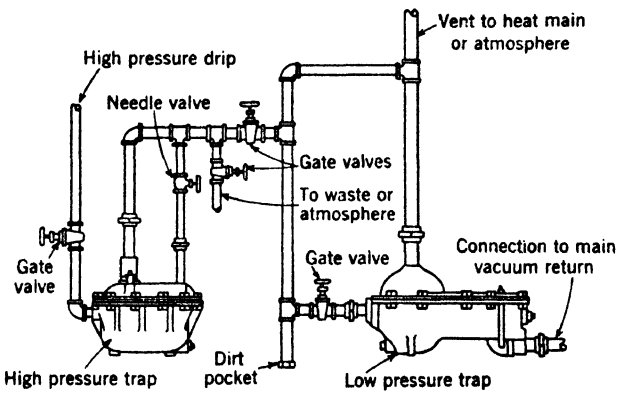


FIG. 21. METHOD OF DISCHARGING HIGH-PRESSURE APPARATUS INTO LOW-PRESSURE HEATING MAINS AND VACUUM RETURN MAINS THROUGH A LOW-PRESSURE TRAP

more, to see that relatively higher temperature steam is prevented from entering the vacuum return lines through leaky traps, high pressure drips, etc. It is for this reason that the condensate from equipment using steam at high pressures should not be connected directly to a vacuum return line, but should drain to a receiver through a high pressure trap. The receiver should have an equalizing connection to a low pressure steam main and drain through a low pressure trap to the vacuum return main as indicated in Fig. 21.

Vacuum Pump Controls

In the ordinary vacuum system, the vacuum pump is controlled by a vacuum regulator which cuts in when the vacuum drops to the lowest point desired and cuts out when it has been increased to the highest point, these points being varied to suit the particular system or operating conditions. In addition to this vacuum control, a float control is included which will start the pump whenever sufficient condensate accumulates in the receiver, regardless of the vacuum on the system. A selector switch is usually provided to allow operation at night as a condensate pump only, also to give manual or continuous operation when desired.

There are several variations in the control of the vacuum maintained on the system by the pump. In some sub-atmospheric systems where orifices are used, the vacuum pump control maintains a pressure difference between the supply and the return piping, which is held within relatively close limits. There are other sub-atmospheric systems which utilize special temperature-pressure actuated controls for maintaining the desired conditions in the return lines. Where various zones are connected to the same return main, the return vacuum must be controlled to meet the requirements of the zone operating at the lowest steam supply pressure.

Piston Displacement Vacuum Pumps

Piston displacement return vacuum heating pumps may be either electric or steam driven. Their piston speed in feet per minute should not exceed 20 times the square root of the number of inches in their stroke. They are usually supplied with an air separating tank, open to atmosphere, placed on the discharge side of the pump and at an elevation sufficiently high to allow gravity flow of the condensate to the boiler. If the boiler pressure is too high for such gravity feed, then an additional steam pump for feeding the boiler is desirable. The extra pump is sometimes avoided by using a closed separating tank with a float controlled vent. In both arrangements, the air taken from the system must be discharged against the full discharge pressure of the vacuum pump. In the case of high or medium pressure boilers, it is better to use the atmospheric separator and the second pump.

In figuring the required displacement for such pumps, a value of from 6 to 10 times the volumetric flow of condensate is used for average vacuums and systems.

TRAPS

The fundamental principle upon which the operation of practically all traps depends is that the pressure within the trap at the time of discharge shall be equal to, or slightly in excess of, the pressure against which the trap must discharge, including the friction head, velocity head and static head on the discharge side of the trap.

Traps are generally classified as to function as (*a*) separating traps, (*b*) return, lifting or vacuum traps, and (*c*) air traps.

Separating traps may be either float operated, thermostatically operated, or float and thermostatically operated. Separating traps are used to release water of condensation but to retain steam. The thermostatic, and float and thermostatic types release both condensate and air but retain steam. Separating traps are used for draining condensate from radiators, indirect air heaters, steam piping systems, kitchen equipment, laundry equipment, hospital equipment, drying equipment and many other kinds of apparatus.

Return traps are used for returning condensate either by gravity, by steam pressure, or by both, to a boiler or other point of disposal, and for lifting condensate from a lower to a higher elevation, or for handling condensate from a lower to a higher pressure. Return traps for low pressure service are referred to later as *alternating receivers* in this chapter. Return traps may also operate to receive condensate under a vacuum and return it to atmosphere or a higher pressure.

Automatic return traps, sometimes called *alternating receivers*, may be of the counterbalanced, tilting type, or spring actuated. These consist of a small receiver with an internal float, and when the condensate will not flow into the boiler under pressure, it will feed into the receiver of the trap, and in so doing, raise or tilt the float or mechanism which actuates a steam valve automatically. This admits steam to the receiver, at boiler pressure, and the equalizing of the pressures which follows allows the water to flow into the boiler.

In the general heating plant, where thermostatic traps are installed on the heating units, it becomes necessary to provide a means for returning the water of condensation to the boiler, if a condensate or vacuum pump is not used. When the return main can be kept sufficiently high above the boiler water line for all operating conditions, the water

of condensation will flow back by gravity, and no mechanical device is required. But actually this does not work out in practice. It follows, therefore, that a direct-return trap is needed for the handling of the condensate even though it may not be called into action except under some operating condition where the pressure differential exceeds the static head provided. The installation of a direct-return trap assures safety for such systems, and guarantees the operation of the plant under varying conditions.

Air traps release air but retain water. Devices known as air vents are, in principle, traps which allow the passage of air but prevent the passage of either water or steam. Air traps are generally float operated.

Traps may also be classified according to the principle of operating device which supplies the power to cause them to function as (1) float, (2) bucket, (3) thermostatic, (4) float and thermostatic, (5) impulse, or (6) tilting traps.

Float Traps. A discharge valve is operated by the rise and fall of a float due to the change of water level in the trap. When the trap is empty the float is in its lowest position, and the discharge valve is closed. A gage glass may be used to indicate the height of water in the chamber.

Unless float traps are well made and proportioned there is danger of considerable steam leakage through the discharge valve due to unequal expansion of the valve and seat and the sticking of moving parts. The discharge from a float trap is usually continuous since the height of the float, and consequently the area of the outlet, is proportional to the amount of water present.

Bucket Traps. Bucket traps are of two types, the upright and inverted, and although they are both of the open float construction, their operating principle is entirely different. In the *upright bucket* trap, the water of condensation enters the trap and fills the space between the bucket and the walls of the trap. This causes the bucket to float and forces the valve against its seat, the valve and its stem usually being fastened to the bucket. When the water rises above the edges of the bucket it flows into it and causes it to sink, thereby withdrawing the valve from its seat. This permits the steam pressure acting on the surface of the water in the bucket to force the water to a discharge opening. When the bucket is emptied it rises and closes the valve and another cycle begins. The discharge from this type of trap is intermittent.

In the *inverted bucket* trap, steam floats the inverted submerged bucket and closes the valve. Water entering the trap fills the bucket, which sinks and through compound leverage opens the valve, and the trap discharges. It is impossible to install a water gage glass on an inverted bucket trap, but if visual inspection is necessary, a gage glass can be placed on the line leading to the trap. No air relief cocks can be used, but they are unnecessary, as the elimination of air is automatically taken care of by air passing through the vent in the top of the inverted bucket regardless of temperature.

Thermostatic Traps. Thermostatic traps are of two types, those in which the discharge valve is operated by the relative expansion of metals, and those in which the action of a volatile liquid is utilized for this purpose. Thermostatic traps of large capacity for draining blast coils or very large radiators are called *blast* traps.

Float and thermostatic traps have both a thermostatic element to release air and a float element to release the water.

Impulse traps operate with a moving valve actuated by a control cylinder. When the trap is handling condensate, the pressure required to lift the valve is greater than the reduced pressure in the control cylinder and consequently the valve opens allowing a free discharge of condensate. As the remaining condensate approaches steam temperature, flashing into steam results, flow through the valve orifice is choked and the pressure builds up in the control chamber closing the valve.

Tilting Traps. With this type of trap, water enters a bowl and rises until its weight overbalances that of a counter-weight, and the bowl sinks to the bottom. As the bowl sinks, a valve is opened, thus admitting live steam pressure on the surface of the water, and the trap then discharges. After the water is discharged, the counter-weight sinks and raises the bowl, which in turn closes the valve and the cycle begins again. Tilting traps are necessarily intermittent in operation. They are not ordinarily equipped with glass water gages, as the action of the trap shows when it is filling or emptying. The air relief of tilting traps is taken care of by the valves of the trap.

DRIPS

A steam main in any type of steam heating system may be dropped to a lower level without dripping if the pitch is downward with the direction of

steam flow. Any steam main in any heating system can be elevated if dripped. Fig. 22 shows a connection where the steam main is raised and the drain is to a wet return. If the elevation of the low point is above a dry return, it may be drained through a trap to the dry return in two-pipe vapor, vacuum and sub-atmospheric systems. Horizontal steam pipes may also be run over obstructions without a change in level if a small pipe is carried below the obstruction to care for the condensate (Fig. 23). Horizontal return pipes may be carried past doorways and other ob-

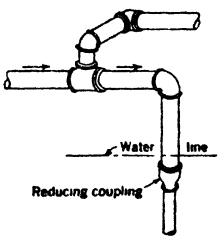


FIG. 22. DRIPPING MAIN WHERE IT RISES TO HIGHER LEVEL

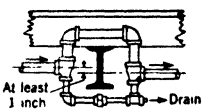


FIG. 23. LOOPING MAIN AROUND BEAM

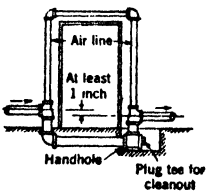


FIG. 24. LOOPING DRY RETURN MAIN AROUND OPENING

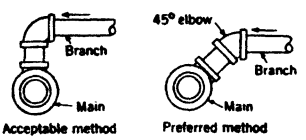
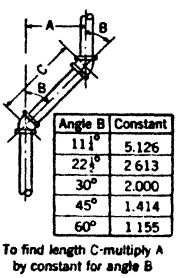


FIG. 25. METHODS OF TAKING BRANCH FROM MAIN



Angle B	Constant
11½°	5.126
22½°	2.613
30°	2.000
45°	1.414
60°	1.155

To find length C-multiply A by constant for angle B

FIG. 26. CONSTANTS FOR DETERMINING LENGTH OF OFFSET PIPE

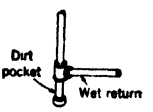


FIG. 27. DIRT POCKET CONNECTION

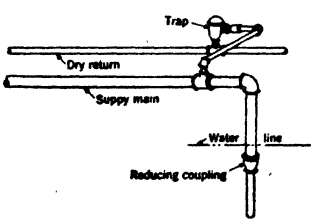


FIG. 28. DRIPPING END OF MAIN INTO WET RETURN

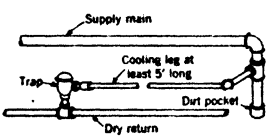


FIG. 29. DRIPPING END OF MAIN INTO DRY RETURN

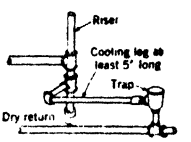


FIG. 30. DRIPPING HEEL OF RISER INTO DRY RETURN

structions by using the scheme illustrated in Fig. 24. It will be noted that the large pipe, in this case, runs below the obstruction and the smaller one over it.

Branches from steam mains in one-pipe gravity steam systems should use the *preferred connection* shown in Fig. 25, but where radiator condensate does not flow back into the main the *acceptable* method shown in the same figure may be used. This acceptable method has the advantage of giving a perfect swing joint when connected to the vertical riser or radiator connection, whereas the preferred connection does not give this swing

without distorting the angle of the pipe. Runouts are usually made about 5 ft long to provide flexibility for movement in the main.

Offsets in steam and return piping should preferably be made with 90-deg ells but occasionally fittings of other angles are used, and in such cases the length of the diagonal offset will be found as shown in Fig. 26.

Dirt pockets, desirable on all systems employing thermostatic traps, should be so located as to protect the traps from scale and muck which will interfere with their operation. Dirt pockets are usually made 8 in. to 12 in. deep and serve as receivers for foreign matter which otherwise would be carried into the trap. They are constructed as shown in Fig. 27.

On vapor systems where the end of the steam main is dripped down into the wet return, the air venting at the end of the main is accomplished

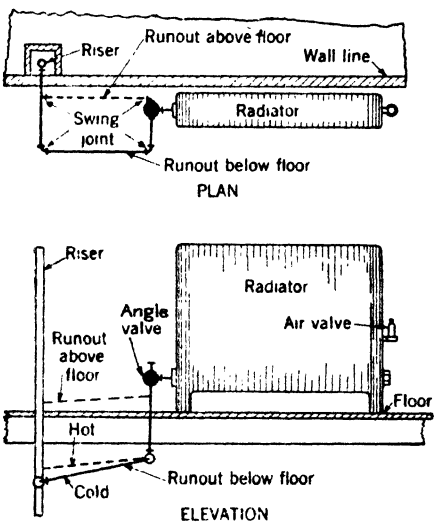


FIG. 31. ONE-PIPE RADIATOR CONNECTIONS

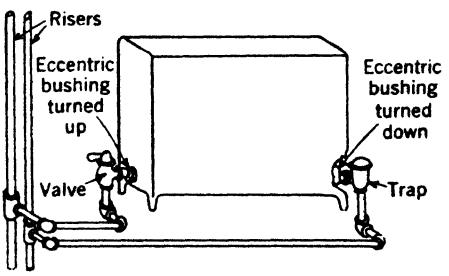


FIG. 32. TYPICAL CONNECTIONS FOR TWO-PIPE SYSTEM

by an air vent passing through a thermostatic trap into the dry return line as shown in Fig. 28. On vacuum systems the ends of the steam mains are dripped and vented into the return through drip traps opening into the return line. The same method may be used in atmospheric systems. A float type trap is preferable to a thermostatic trap for dripping steam mains and large risers. If thermostatic traps are used, a cooling leg (Fig. 29) should always be provided. The cooling leg is for cooling the condensate sufficiently before it reaches the trap, so the trap will not be held shut by too high a temperature. On down-feed systems of atmospheric, vapor, and vacuum types, the bottoms of the steam risers are dripped in the manner shown in Fig. 30. On large systems it is desirable to install a gate valve in the cooling leg ahead of the trap.

CONNECTIONS TO HEATING UNITS

Riser, radiator and convector connections must not only be properly pitched at the time they are installed but must be arranged so that the pitch will be maintained under the strains of expansion and contraction. These connections may be made by swing joints which permit the expansion or contraction to occur under heating and cooling without bending

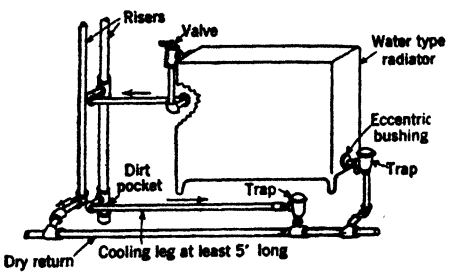


FIG. 33. TOP AND BOTTOM OPPOSITE END RADIATOR CONNECTIONS

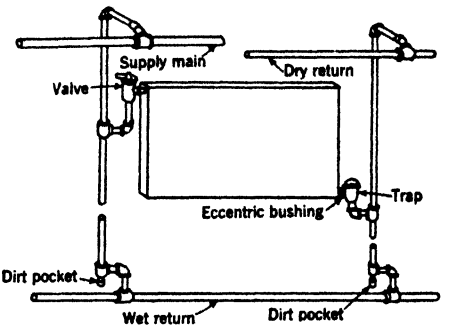


FIG. 34. CONNECTIONS TO RADIATOR HUNG ON WALL

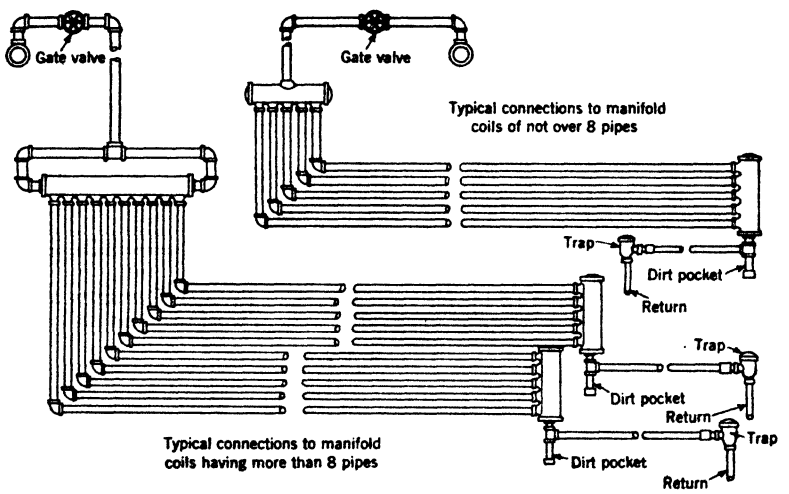


FIG. 35. TYPICAL PIPE COIL CONNECTIONS

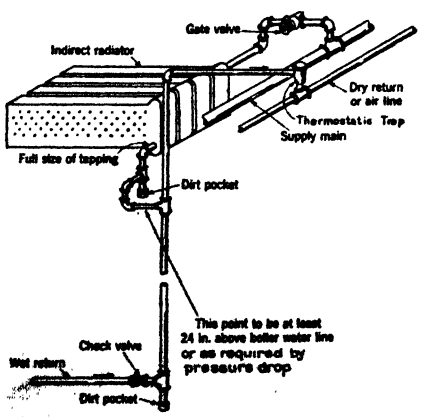


FIG. 36. TYPICAL PIPING CONNECTIONS TO INDIRECT RADIATORS WITH WET RETURNS

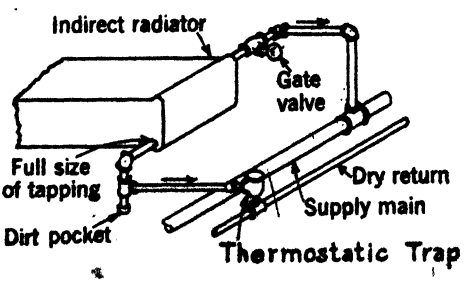


FIG. 37. TYPICAL PIPING CONNECTIONS TO INDIRECT RADIATORS WITH DRY RETURNS

of pipes. To take care of expansion in long risers, either expansion joints of commercial construction or pipe swing joints are used. Anchoring of pipes between expansion joints is desirable.

Two satisfactory methods of making runouts for one-pipe systems for either the up-feed or the down-feed type are shown in Fig. 31. Where the vertical distance is limited and the runouts must run above the floor, the radiator may be set on pedestals or raised by means of high legs. Two methods of connecting a unit heater to a one-pipe steam heating system are illustrated in Fig. 2 and also in Fig. 5 of Chapter 26.

Typical two-pipe radiator or convector connections are shown in Figs. 32, 33 and 34. While the top is the preferred location for the control valve, it may be located at the bottom. Short radiators may be top supply and bottom return on same end. With convectors the control

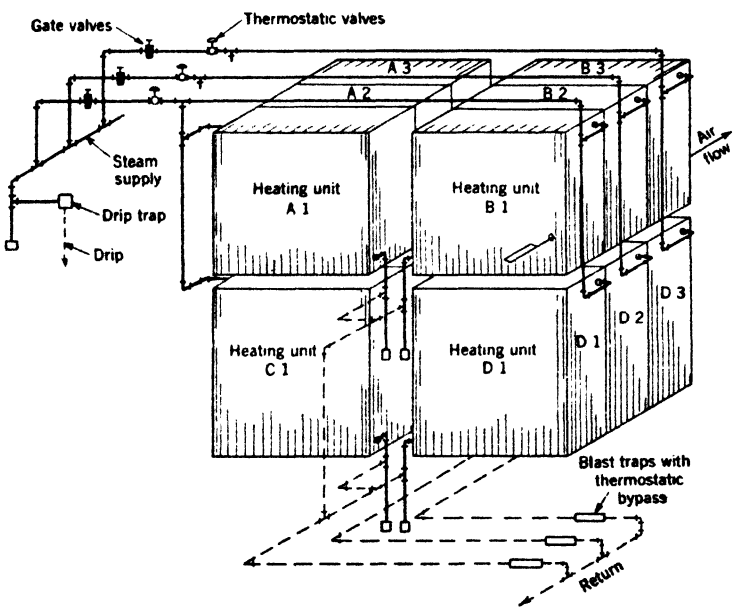


FIG. 38. TYPICAL PIPING FOR ATMOSPHERIC AND VACUUM SYSTEMS WITH THERMOSTATIC CONTROL (CENTRAL FAN SYSTEM)

valve is sometimes omitted and a damper in outlet grille used for heat control. The typical method of connecting pipe coils is shown in Fig. 35 and is suitable for atmospheric, vapor, vacuum, sub-atmospheric, and orifice systems.

Typical pipe connections for indirect radiators and tempering or heating stacks are shown in Figs. 36, 37, 38, 39, 40, 41, and 42.

Where a building is served by a vacuum system or a sub-atmospheric system the stacks should be piped in the usual manner and traps of large capacity, preferably of the combination float and thermostatic type, should be used. In the orifice and *closed* two-pipe systems, traps should be used on the returns so that a pressure above that of the atmosphere may be secured on the heaters.

Each stack should have a separate steam and return connection and trap. Wide stacks are more evenly heated if divided and supplied with two steam connections, one at each end, and a return connection for each

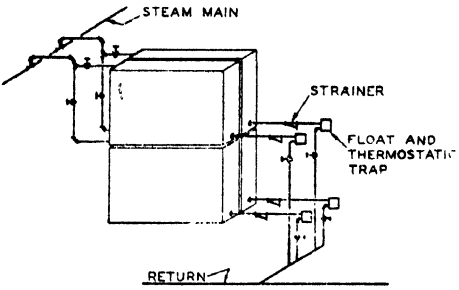


FIG. 39. TYPICAL CONNECTIONS TO CAST IRON BLAST HEATERS LESS THAN 12 SECTIONS LONG

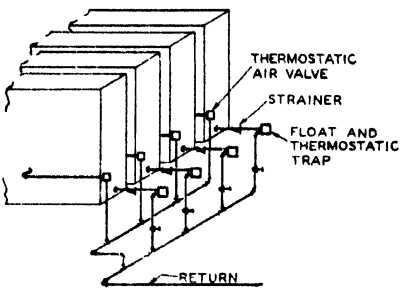


FIG. 40. TYPICAL CONNECTIONS TO CAST IRON BLAST HEATERS MORE THAN 12 SECTIONS LONG

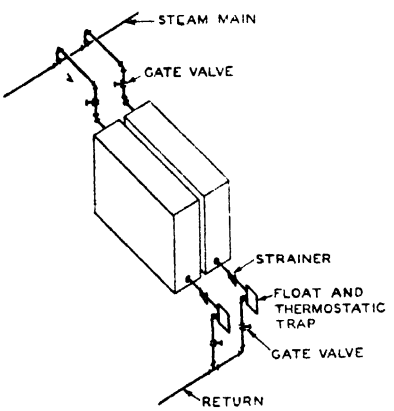


FIG. 41. TYPICAL CONNECTIONS TO FINNED TUBE BLAST HEATERS WITH LOW PRESSURE STEAM

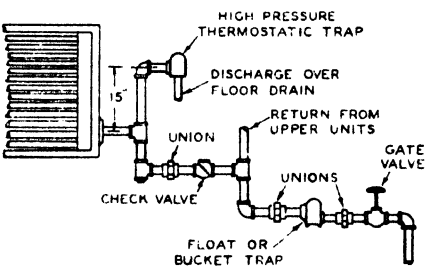


FIG. 42. TYPICAL RETURN CONNECTION FROM FINNED TUBE BLAST HEATERS WITH HIGH PRESSURE STEAM

steam connection. For stacks of large capacity it is sometimes desirable to run a separate steam main direct from the boiler to the stacks.

CONTROL VALVES

Gate valves are recommended in all cases where service demands that the valve be either entirely open or entirely closed, but they should never be used for throttling. Angle globe valves and straight globe valves should be used for throttling, as done on by-passes around pressure reducing valves or on by-passes around traps.

REFERENCES

1—A.S.H.V.E. RESEARCH REPORT NO. 954—Condensate and Air Return in Steam Heating Systems, by F. C. Houghten and J. L. Blackshaw (A.S.H.V.E. TRANSACTIONS, Vol. 39, 1933, p. 199).

2—Pipe size tables in this chapter have been compiled in simplified and condensed form for the convenience of the user; at the same time all of the information contained in previous editions of THE GUIDE has been retained. Values of pressure drops, formerly expressed in ounces, are now expressed in fractions of a pound.

3—A.S.H.V.E. Standard Code for Testing and Rating Return Line Low Vacuum Heating Pumps (A.S.H.V.E. TRANSACTIONS, Vol. 40, 1934, p. 33).

Chapter 24

HOT WATER HEATING SYSTEMS AND PIPING

Available Head; Friction Loss; Classification; System Design; Examples of Piping Design; One-Pipe Gravity, One-Pipe Forced Circulation, Two-Pipe Gravity, and Two-Pipe Forced Circulation Systems, Expansion Tanks, Installation Details, Zoning Systems

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A HEATING system is called a hot water system if water is used to convey heat by flowing through pipes connecting a boiler or water heater with radiators, convectors or other suitable heat dispensing means. There are two types: the gravity system in which the water flows by virtue of thermo-syphon action, and the forced system in which a pump, usually driven by an electric motor, sometimes by a steam turbine or other means, maintains the necessary flow. Most panel heating systems (see Chapter 31) fall into the category of forced hot water systems, and the design procedures pertaining to pipe sizing and friction contained in this chapter are largely applicable to such systems.

Historically, the gravity system is much the older, and many such systems have been in satisfactory operation for several decades. Operation depends on the difference in density of the water due to difference in temperature in the flow and return pipes. The available head is therefore limited and the pipes must be ample in size to permit adequate flow of water. In the forced system, the pipes, valves and fittings can be much smaller, with a resultant saving in the cost of installation, since the available head is limited only by consideration of economy in pumping the water. With the forced system, higher boiler temperatures and automatic control of the pump or circulator make possible the use of indirect water heaters with hot water systems when that is desirable. (See Chapter 50).

AVAILABLE CIRCULATION HEAD

The available head in a gravity circulation system may be found from the equation:

$$h_a = \frac{\rho_1 - \rho_2}{144} \times 2.31 \times 12{,}000 \qquad (1)$$

where

h_a = available head per foot of height, milinches (1 milinch = 1/1000 of 1 in. of water).

ρ_1 = average density of flow water, pounds per cubic foot.

ρ_2 = average density of return, pounds per cubic foot.

144 = square inches per square foot.

2.31 = height of water column equivalent to 1 psi, feet.

12,000 = milinches equivalent of 1 ft of water column.

The available head may also be found from Fig. 1. For example, at a flow temperature of 200 F and a 35 deg drop, and with the mains located 4 ft above the top of the boiler, a head of 600 milinches is obtained. This is found by following the 200 F flow riser line in Fig. 1 to where it intersects the 165 F return riser line and reading horizontally a head of 150 milinches per foot or 600 milinches for 4 ft. If the first floor radiators are located 3 ft above the mains, second floor radiators 12 ft above the mains, third floor 21 ft, and fourth floor 30 ft, the heads are 450, 1800, 3150, and 4500 milinches respectively.

In *forced circulation* systems flow is produced mechanically by means of a pump driven by electricity, steam, or other source of energy. As forced circulation velocities are higher than those in gravity systems, and as the friction in a heating system varies almost as the square of the velocity, a given error in the calculation or assumption of the velocity is less important in a forced circulation system than in a gravity circu-

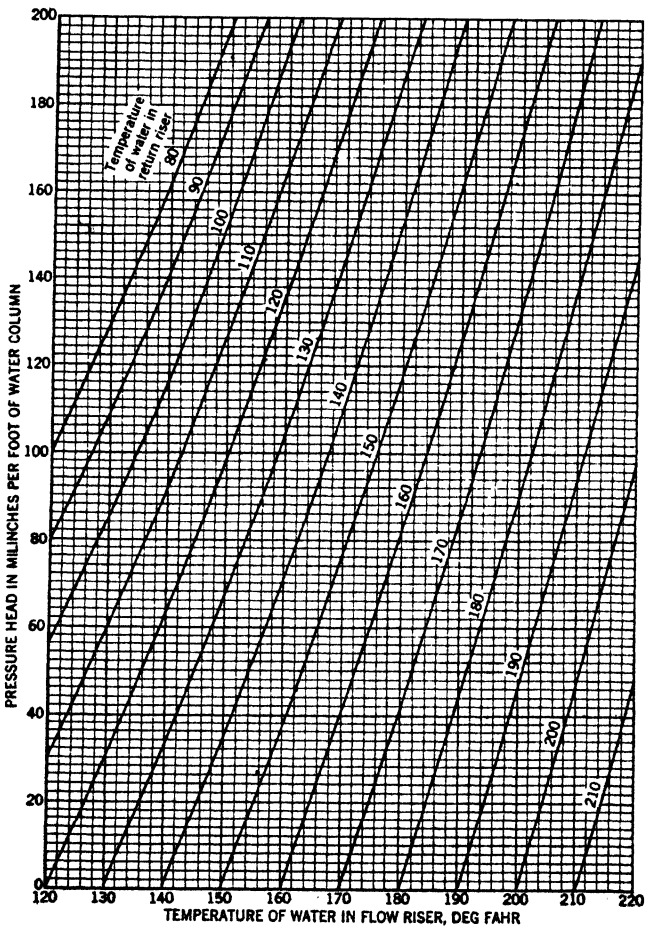

FIG. 1. HEADS RESULTING FROM TEMPERATURE DIFFERENCE (GRAVITY SYSTEMS)

lation system, and, consequently, it is easier to design a satisfactory forced circulation system than a satisfactory gravity circulation system.

FRICTION LOSS

Values of friction loss due to flow of water in the various parts of a heating system must be known in order to design either gravity or forced circulation systems.

The friction loss of fittings is customarily expressed in equivalent number of elbows of the same pipe size which would have the same

TABLE 1. IRON AND COPPER ELBOW EQUIVALENTS[a]

FITTING	IRON PIPE	COPPER TUBING	FITTING	IRON PIPE	COPPER TUBING
Elbow, 90-deg	1.0	1.0	Angle radiator valve	2.0	3.0
Elbow, 45-deg	0.7	0.7	Radiator or convector	3.0	4.0
Elbow, 90-deg long turn	0.5	0.5	Boiler or heater	3.0	4.0
Elbow, welded, 90-deg	0.5	0.5			
Reduced coupling	0.4	0.4	Tee, per cent flowing		
Open return band	1.0	1.0	through branch:		
Open gate valve	0.5	0.7	100	1.8	1.2
Open globe valve	12.0	17.0	50	4.0	4.0
			25	16.0	20.0

[a]The friction in one 90 deg standard elbow is approximately equal to the friction of a length of straight pipe of the same nominal size and 25 diam long. Hence one elbow equivalent in feet of pipe equals 25 diam (in inches) divided by 12.

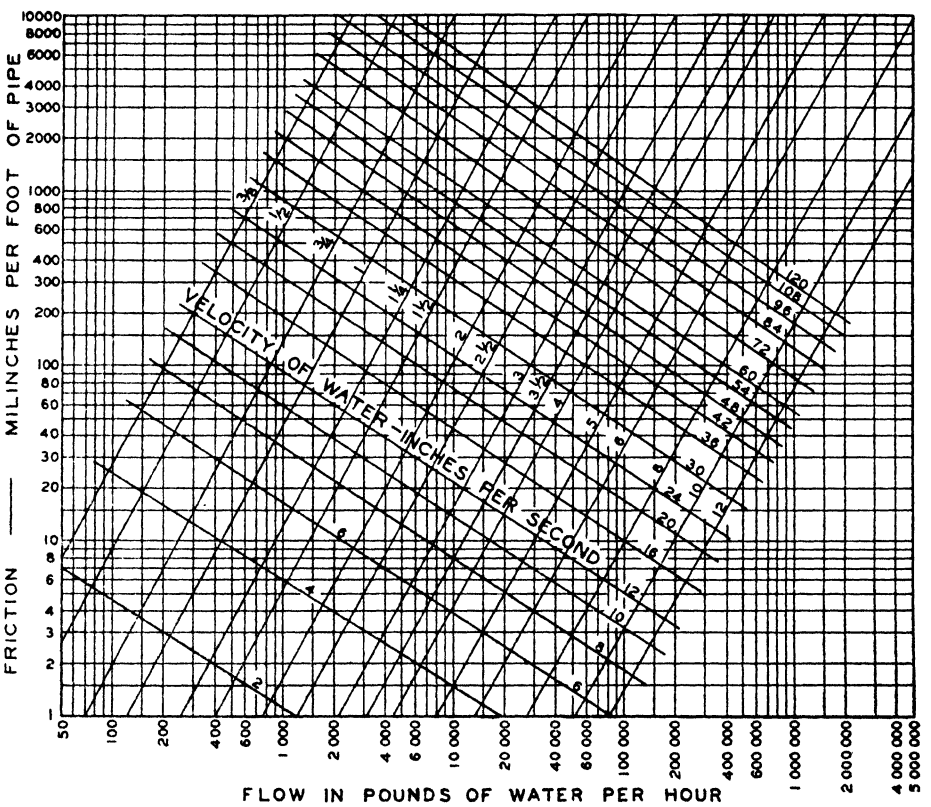

FIG. 2. FRICTION IN BLACK IRON PIPES BASED ON FLOW IN POUNDS PER HOUR

friction loss. An elbow is assumed to have the same friction loss as a straight pipe having a length equal to 25 diameters (nominal) of the elbow.

The resistance of various types of fittings expressed in equivalent elbow resistance is shown in Table 1.

The friction loss in black iron pipes for a determined weight of water may be obtained from Fig. 2. For the frequently used temperature drop of 20 deg the friction loss may be determined directly from the heat

TABLE 2. HEAT-CARRYING CAPACITY OF STANDARD BLACK PIPES WITH TEMPERATURE DROP OF 20 DEG[a]

Nominal Pipe Sizes ⅜ in. to 12 in., and Friction 4 to 800 milinches per foot (A = Capacity, Mbh. B = Velocity, inches per second) (One milinch equals 0.001 in.)

Milinch Friction Loss per Foot of Pipe		Nominal Pipe Size, Inches															
		⅜	½	¾	1	1¼	1½	2	2½	3	3½	4	5	6	8	10	12
4	A	0.75	1.35	2.85	5.4	11.3	17.0	33.0	53.1	95	141	197	363	596	1250	2320	3730
	B	1.5	1.7	2.1	2.4	2.9	3 2	3.8	4.3	5.0	5.5	6.0	7.0	7.9	9.6	11	12
6	A	0.9	1.7	3.6	6.75	14.0	21.2	41.3	66.4	119	176	248	456	748	1570	2920	4690
	B	1.8	2.1	2.6	3.0	3.6	4.0	4.7	5.3	6.2	6.9	7.5	8.8	10	12	14	16
8	A	1.05	2.0	4.2	7.9	16.4	24.8	48.4	77.9	140	207	291	535	879	1850	3440	5520
	B	2.1	2.5	3.0	3.5	4.2	4.7	5.6	6.3	7.3	8.0	8.8	10	12	14	17	19
10	A	1.2	2.2	4.7	8.9	18.6	28.0	54.7	88.1	158	234	329	605	997	2100	3910	6270
	B	2.4	2.8	3.4	4.0	4.8	5.3	6.3	7.1	8.2	9.1	9.9	12	13	16	19	27
12	A	1.35	2.45	5.2	9.8	20.5	31.0	60.4	97.4	175	259	364	671	1100	2320	4330	6950
	B	2.7	3.1	3.7	4.4	5.3	5.9	6.9	7.8	9.1	10	11	13	15	18	21	24
14	A	1.45	2.65	5.65	10.7	22.3	33.7	65.8	106	190	282	397	731	1200	2530	4730	7590
	B	2.9	3.4	4.1	4.8	5.7	6.4	7.6	8.5	9.9	11	12	14	16	20	23	26
16	A	1.55	2.85	6.05	11.5	24.0	36.3	70.8	114	205	303	428	787	1300	2730	5100	8190
	B	3.1	3.6	4.4	5.1	6.2	6.9	8.1	9.7	11	12	13	15	17	21	25	28
20	A	1.75	3.25	6.85	13.0	27.1	41.0	80.0	129	232	344	484	892	1470	3100	5790	9300
	B	3.5	4.1	4.9	5.8	7.0	7.7	9.2	10	12	13	15	17	20	24	28	32
25	A	2.0	3.65	7.75	14.7	30.6	46.3	90.5	146	263	389	548	1010	1670	3510	6570	10560
	B	4.0	4.6	5.6	6.5	7.9	8.8	10	12	14	15	17	19	22	27	32	36
30	A	2.2	4.0	8.55	16.2	33.8	51.2	100	162	290	430	607	1120	1850	3900	7280	11710
	B	4.4	5.1	6.1	7.2	8.7	9.7	11	13	15	17	18	22	25	30	35	40
35	A	2.35	4.4	9.3	17.6	36.8	55.7	109	176	316	469	661	1220	2010	4250	7940	12780
	B	4.7	5.5	6.7	7.9	9.5	11	13	14	16	18	20	23	27	33	39	44
40	A	2.55	4.7	10.0	18.9	39.6	59.9	117	189	341	505	712	1320	2170	4580	8570	13780
	B	5.1	5.9	7.2	8.4	10	11	13	15	18	20	22	25	29	35	42	47
50	A	2.85	5.3	11.3	21.4	44.7	67.7	133	214	386	572	807	1490	2460	5190	9720	15650
	B	5.7	6.7	8.1	9.5	12	13	15	17	20	22	24	29	33	40	47	54
60	A	3.15	5.85	12.4	23.6	49.4	74.9	147	238	427	633	893	1650	2730	5760	10780	17360
	B	6.3	7 4	8.9	11	13	14	17	19	22	25	27	32	36	44	52	60
70	A	3.45	6.35	13.5	25.7	53.8	81.4	160	258	465	690	973	1800	2970	6280	11760	18950
	B	6.9	8.0	9.7	11	14	15	18	21	24	27	29	35	40	48	57	65
80	A	3.7	6.8	14.5	27.6	57.9	87.6	172	278	500	743	1050	1940	3200	6770	12690	20440
	B	7.4	8.6	10	12	15	17	20	22	26	29	32	37	43	52	62	70
100	A	4.15	7.7	16.4	31.1	65.4	99.0	194	314	566	840	1190	2200	3630	7680	14400	23200
	B	8.3	9.7	12	14	17	19	22	25	30	33	36	42	48	59	70	80
150	A	5.2	9.6	20.4	38.8	81.6	124	243	393	709	1050	1490	2760	4560	9650	18120	29220
	B	10	12	15	17	21	23	28	32	37	41	45	53	61	74	88	101
200	A	6.05	11.2	23.9	45.4	95.5	145	285	461	832	1240	1750	3240	5360	11350	21320	34400
	B	12	14	17	20	25	27	33	37	43	48	53	62	71	87	104	118
300	A	7.5	13.9	29.7	56.6	119	181	356	577	1040	1550	2190	4060	6730	14270	26830	43300
	B	15	18	21	25	31	34	41	46	54	60	66	78	90	110	131	149
400	A	8.75	16.2	34.7	66.2	140	212	417	676	1220	1820	2570	4780	7910	16790	31580	51000
	B	18	21	26	30	36	40	48	54	64	71	78	92	105	129	154	175
500	A	9.85	18.3	39.2	74.8	158	239	471	765	1380	2060	2910	5410	8970	19040	35840	57880
	B	20	23	29	33	41	45	54	62	72	80	88	104	119	147	174	199
600	A	10.9	20.2	43.2	82.5	174	264	521	846	1530	2280	3220	5990	9930	21100	39740	64210
	B	22	26	32	37	45	50	60	68	80	89	97	115	132	163	193	221
800	A	12.7	23.6	50.5	96.5	204	310	610	992	1790	2670	3780	7030	11670	24820	46780	75620
	B	25	30	37	43	52	59	70	80	94	104	114	135	155	191	228	260

[a]For other temperature drops the pipe capacities may be changed correspondingly. For example, with a temperature drop of 30 deg the capacities shown in this table are to be multiplied by 1.5.

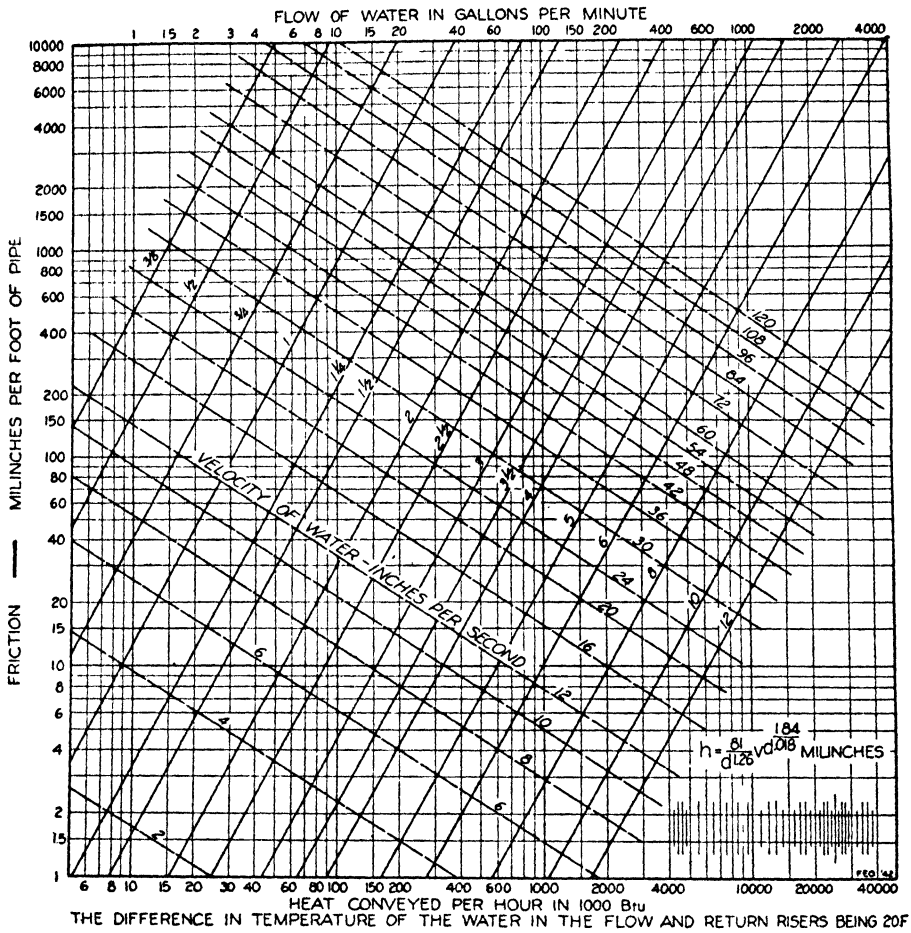

FIG. 3. FRICTION IN BLACK IRON PIPES

To find friction when temperature drop is other than 20 deg, multiply the actual heat conveyed by $\left(\frac{20}{\text{actual temp drop}}\right)$ and read the corresponding friction.

requirement by means of Table 2 or Fig. 3 for black iron pipes, or by means of Table 3 for copper tubing.

Orifices drilled in plates inserted in pipe unions are convenient means for introducing friction, where required to balance various circuits. The friction losses caused by various sizes of orifices are given in Table 4.

CLASSIFICATION OF SYSTEMS

Gravity or *forced* systems of piping may be classified according to piping arrangement and type of circulation as shown in Table 5. Flow and return main piping (gravity systems) for one-pipe, two-pipe direct return, and two-pipe reversed return systems are shown in Figs. 4, 5, and 6 respectively. These Figures would also illustrate forced circulation if a pump or circulator were shown in the return line at the boiler.

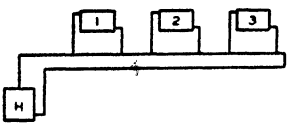

FIG. 4. ONE-PIPE SYSTEM

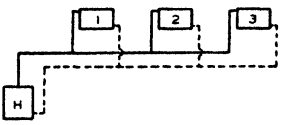

FIG. 5. A TWO-PIPE DIRECT RETURN SYSTEM

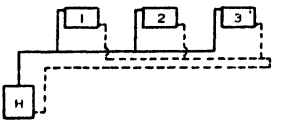

FIG. 6. A TWO-PIPE REVERSED RETURN SYSTEM

One-pipe gravity systems require very precise design owing to the small circulating head available. Also, circulation in them is slow, and temperature drop is large toward the end of the main, and consequently these systems are usually considered impractical.

One-pipe forced systems compared with gravity systems provide more rapid circulation with consequent smaller temperature drop in mains and more uniform water temperature in all radiators and are therefore preferred. Special flow and return fittings are available for improving the circulation to risers.

Two-pipe systems have separate flow and return mains. If the return main is *direct* as shown in Fig. 5 the radiator at the end of the system has the longest supply and longest return piping. The lengths of circuits to the various radiators may be equalized by using a *reversed return* main, (see Fig. 6). In some cases *reversed return* mains require no more piping than *direct return* systems.

TABLE 3. HEAT-CARRYING CAPACITY OF TYPE L COPPER TUBING WITH TEMPERATURE DROP OF 20 DEG[a]

Nominal Tube Sizes ⅜ in. to 4 in., and Friction 60 to 720 milinches per foot. (A = Capacity, Mbh. B = Velocity, inches per second) (One milinch equals 0.001 in.)

NOMINAL TUBE SIZE, IN.		MILINCH FRICTION LOSS PER FOOT OF TUBE											
		720	600	480	360	300	240	180	150	120	90	75	60
⅜	A	10	9	8	6.8	6.2	5.4	4.6	4	3.6	3	2.8	2.4
	B	27	24	21	18	16.5	14	13	11	10	8.5	8	7
½	A	20	18	16	13.5	12	10.8	9	8	7	6	5.4	4.7
	B	35	30	25	21	19	17	15	13	12	10	9	8
⅝	A	36	30	26	22.1	20	17.8	15	13.1	11.8	9.9	9	7.9
	B	37	34	30	24	21	19	17	15	13	11	10	9
¾	A	51	46	40	34	31	28	23.2	20.5	18.1	15.3	13.9	12.1
	B	42	38	33	27	24	21	19	17	14	12	11.5	10
1	A	104	94	82	70	63	56	47	42	37	32	28	25
	B	48	45	39	34	30	25	22	19	17	14.5	13	12
1¼	A	185	169	149	125	112	100	84	75	66	56	50	44
	B	55	51	45	39	35	30	25	22	19	17	15	13
1½	A	300	270	235	200	180	160	134	120	105	90	81	71
	B	62	57	51	43	39	35	30	25	22	19	17	15
2	A	625	560	495	420	375	335	280	250	200	188	170	150
	B	76	68	59	51	47	42	36	32	27	22	20	18
2½	A	1130	1010	890	750	680	600	500	450	395	335	305	270
	B	90	80	69	58	49	47	42	37	33	26	23	21
3	A	1840	1650	1450	1210	1100	980	820	740	650	550	490	420
	B	98	90	80	66	59	52	47	42	36	30	27	23
3½	A	2750	2480	2170	1840	1650	1450	1210	1100	980	820	740	650
	B	110	100	89	75	66	57	51	45	40	35	30	26
4	A	3900	3505	3100	2600	2350	2090	1760	1580	1390	1180	1060	950
	B	120	108	96	83	73	63	55	49	44	37	34	29

[a]For other temperature drops the pipe capacities may be changed correspondingly. For example, with temperature drop of 30 deg the capacities shown in this table are to be multiplied by 1.5.

TABLE 4. FRICTION (IN MILINCHES) OF CENTRAL CIRCULAR DIAPHRAGM ORIFICES IN UNIONS

(One milinch equals 0.001 in.)

Diameter of Orifices (Inches)	Velocity of Water in Pipe in Inches per Second									
	2	3	4	6	8	10	12	18	24	36
					¾-in. Pipe					
0.25	1300	2900	5000	11,300	20,800	32,000	45,000			
0.30	650	1450	2500	5700	10,400	16,000	23,000	57,000		
0.35	330	740	1300	2900	5200	8000	12,000	26,000	47,000	
0.40	170	380	660	1500	2600	4000	6800	13,000	24,000	53,000
0.45		185	330	740	1300	2000	2900	6500	12,000	27,000
0.50			155	350	620	970	1400	3200	5700	13,000
0.55			75	170	300	480	700	1600	2800	6400
					1-in. Pipe					
0.35	900	2000	3500	7800	14,000	22,000	32,000			
0.40	460	1000	1800	4000	7200	12,000	17,000	37,000	65,000	
0.45	270	570	1000	2300	4100	6400	9300	21,000	37,000	
0.50	160	330	580	1400	2300	3700	5400	12,000	22,000	50,000
0.55		190	330	750	1300	2200	3000	7000	13,000	28,000
0.60			200	440	800	1300	1800	4200	7400	17,000
0.65			120	260	460	720	1100	2400	4300	10,000
					1¼-in. Pipe					
0.45	1000	2250	4000	8900	16,000	25,000	36,000			
0.50	660	1450	2600	5800	10,400	16,400	23,000	53,000		
0.55	430	950	1700	3800	6800	10,500	15,000	34,000	60,000	
0.60	280	630	1100	2500	4400	6900	10,000	22,000	40,000	
0.65	190	420	750	1700	3000	4700	6700	15,000	27,000	60,000
0.70		285	510	1150	2000	3100	4500	10,000	18,000	40,000
0.75		190	330	750	1300	2100	3000	6700	12,000	26,000
					1½-in. Pipe					
0.55	850	1900	3300	7400	13,000	21,000	30,000			
0.60	600	1300	2300	5400	8600	16,800	21,000	50,000		
0.65	400	850	1500	3600	7200	10,400	14,000	30,000	53,000	
0.70	260	600	1100	2600	4400	7000	10,000	21,000	39,000	
0.75	180	400	760	1800	3000	5000	7000	14,000	28,000	
0.80		300	540	1200	2200	3200	5000	10,200	19,000	45,000
0.85		200	380	860	1600	2300	3000	7800	13,000	30,000
					2-in. Pipe					
0.70	890	1850	3500	7400	14,000	22,300	33,000			
0.80	470	975	1800	3900	7400	11,700	17,000	37,000		
0.90	255	560	1000	2200	4200	6500	9500	20,500	38,000	
1.00	160	340	610	1320	2520	4000	5800	12,500	23,000	49,000
1.10		214	375	850	1600	2500	3700	7900	14,000	30,000
1.20			195	460	950	1360	1910	4200	8100	16,800
1.30				275	525	980	1375	3100	4400	8850

Note.—The losses of head for the orifices in the 1½-in. and 2-in. pipe were calculated from those in the smaller pipes, the calculations being based on the assumption that, for any given velocity, the loss of head is a function of the ratio of the diameter of the pipe to that of the orifice. This had been found to be practically true in the tests to determine the losses of head in orifices in ¾-in., 1-in., and 1¼-in. pipe, conducted by the Texas Engineering Experiment Station, and also in the tests to determine the losses of head in orifices in 4-in., 6-in., and 12-in. pipe, conducted by the Engineering Experiment Station of the University of Illinois. (*Bulletin* 109, Table 6, p. 38, Davis and Jordan).

TABLE 5. CLASSIFICATION OF HOT WATER HEATING SYSTEMS

PIPING ARRANGEMENT	TYPE OF CIRCULATION	EXPANSION TANK	
One-Pipe	Gravity	Open	Closed
	Forced	Open	Closed
Two-Pipe Direct Return	Gravity	Open	Closed
	Forced	Open	Closed
Two-Pipe Reversed Return	Gravity	Open	Closed
	Forced	Open	Closed

With *gravity* circulation and *direct* return piping it is necessary to design the longest circuit for the available circulating head and to obtain the same resistance in all other circuits by proper selection of pipe sizes, by addition of fittings, or by use of orifices. When a *reversed return* system is used, it is usually found that but little adjustment is required to attain uniform distribution to all radiators.

Forced circulation in two-pipe systems, because of increased available circulating head, permits design for higher velocities with a consequent reduction in pipe sizes. The increased velocity also shortens the heating-up period and facilitates control of circulation. Reversed return mains are also advantageous in forced circulation systems in equalizing piping resistance to all heating units.

PIPING SYSTEM DESIGN

In designing hot water heating systems certain assumptions are usually made for the purpose of simplification as follows:

1. Water temperature drop is assumed to be 30 to 35 deg for gravity systems and 20 deg for forced circulation systems. These values usually result in economical design but, particularly in large forced circulation systems, it is necessary to take into account the cost of pumping the water required at various velocities in relation to the annual charges in the capital cost of the system.

2. Water velocities in forced systems in excess of 4 fps are likely to cause disturbing noises in buildings other than factories.

3. Design outlet water temperatures in gravity systems are generally selected between 140 and 200 F (with the average approximately 180 F); while forced circulation design temperatures vary from 170 to 220 F, although higher temperatures can be used if the pressure in the system corresponds.

4. For forced circulation systems, the allowable friction loss, which is based upon the available circulating head, is determined partially by the characteristics of the pumps available.

5. Forced hot water system friction should usually be held between 600 and 250 milinches per foot. Above 600 milinches high velocities would be encountered and below 250 milinches circulation would become too slow so that much of the rapid response expected from forced circulation would be lost.

The water to be circulated is

$$W = H/(C\,\Delta\,t) \qquad (2)$$

where W = weight of water, pounds per hour [gallons per hour = $W/(8 \times 60)$].
H = heat required, Btu per hour.
C = specific heat of water (= 1).
Δt = drop in temperature between supply and return, Fahrenheit degrees.

The following graded series of examples of the design of hot water piping systems will illustrate the fundamental principles and methods. The differences between reversed return and direct return systems are

shown, and the methods of balancing the several radiators or circuits are illustrated. A simple gravity system is shown in Fig. 7 and an elementary forced circulation system is diagrammed in Fig. 8.

Elementary Gravity System

Example 1. A simple gravity-circulation system is illustrated in Fig. 7 with one radiator that is giving off heat at the rate of 20,000 Btu per hour or 20 Mbh. The boiler imparts heat to the water at the same rate, and the water circulates at a uniform velocity. This uniform velocity is such that the friction of the circuit is equal to the head developed by the difference in density between the supply and return water and the height of the system. The circuit consists of 1 boiler, 1 radiator, 2 ells, 1 radiator valve and a total of 24 ft of pipe.

Solution. With the average water temperatures of 200 and 180 F in the supply and return risers, respectively, the head will be 90 milinches per foot of water column. This head may be found from Fig. 1. Since the center of the radiator is 10 ft above the center of the boiler, the total head of the circuit is 10 x 90, or 900 milinches, or 0.9 inches of 190 F water. The friction of the circuit must then also be 900 milinches. The friction of 1 ft of 1 in. pipe is found from Fig. 3 to be about 46 milinches at 20 Mbh, and the

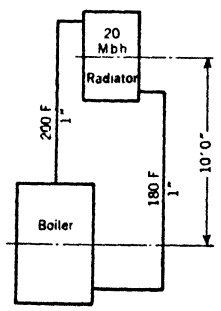

FIG. 7. GRAVITY SYSTEM

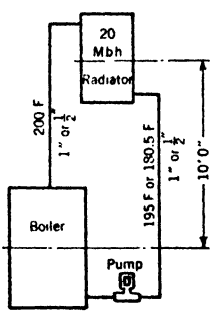

FIG. 8. FORCED CIRCULATION SYSTEM

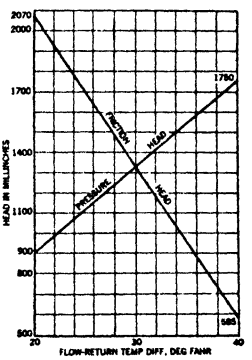

FIG. 9. DETERMINATION OF REQUIRED TEMPERATURE DIFFERENCE

corresponding velocity 9 in. per second. (Note that all values in Fig. 3 are based on a temperature difference of 20 deg).

Similarly, if a 1¼ in. pipe were to be used, the friction head would be about 12 milinches per foot and the corresponding velocity about 5 in. per second, from Fig. 3.

To find the friction in the elbows, boiler, radiator, and valve, Table 1 is used, and the entire circuit is found to be equal to 10 elbow-equivalents plus 24 ft of pipe. Each elbow-equivalent is equal to a pipe length of 25 times the nominal diameter. Then the equivalent lengths of straight pipe are 45 ft of 1 in. pipe or 50 ft of 1¼ in. pipe. In many cases, it is sufficiently accurate to add 50 per cent to the total pipe length to correct for resistance of fittings.

Hence, if 1 in. pipe is used, the friction of the circuit will be 45 x 46, or 2070 milinches, and if 1¼ in. pipe is used, the friction will be 50 x 12, or 600 milinches. A 1 in. pipe would, therefore, be too small and a 1¼ in. pipe too large to permit the desired circulation with a flow-return temperature difference of 20 deg.

If the circuit is of 1 in. pipe, the circulation will take place with a temperature difference greater than 20 deg, and if the circuit is of 1¼ in. pipe, the circulation will take place with a temperature difference smaller than 20 deg. To find, for example, the temperature difference at which a circuit of 1 in. pipe would transmit the required 20 Mbh, assume the difference to be 40 deg.

From Fig. 1, the head available for producing circulation would be 175 milinches per foot or 1750 for the system for a temperature drop from 200 to 160 F. The friction of the system may be found from Fig. 3; the chart of this figure is based on a temperature

difference of 20 deg; if the temperature difference were 40 deg, the heat conveyed would be twice that shown in the chart. Hence, find 10 Mbh on the lower scale, proceed vertically upward to the intersection with the 1 in. line, and from there to the left scale read 13 milinches per foot. Note that the velocity would then be only about 5 in. per second. The total friction would then be 45 x 13 or 585 milinches. Since the head would be 1750, circulation would take place with a temperature difference less than 40 deg. The required temperature difference may be determined by constructing the diagram of Fig. 9, from which it appears that the temperature difference with which the 1 in. pipe circuit would function is about 30 deg. Hence, if the flow riser temperature is 200, the return riser temperature will be 170, and the average water temperature in the radiator about 185 F.

Elementary Forced Circulation System

Example 2. Design a system for the piping arrangement shown in Fig. 8, according to one of the outlined procedures. The procedure may be as follows: Assume the head developed by the circulating pump and the pipe size and find the flow-return temperature difference; or, assume the head developed by the pump and the flow-return temperature difference and find the pipe size; or, assume the pipe size and the flow-return temperature difference and find the head which the circulating pump must develop.

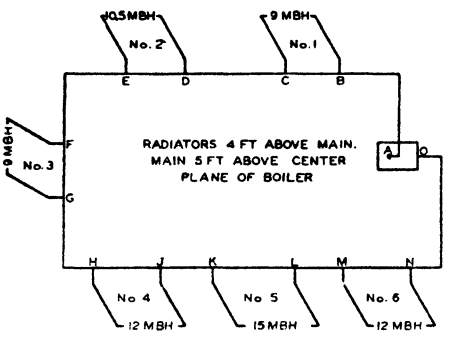

FIG. 10. ONE-PIPE GRAVITY CIRCULATION SYSTEM (EXAMPLE 3)

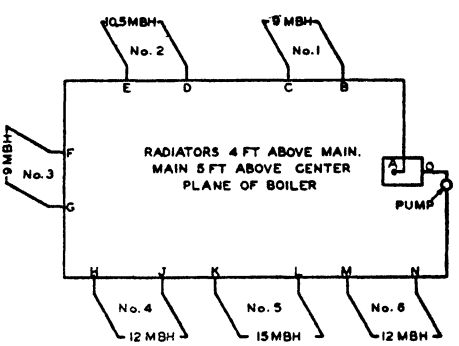

FIG. 11. ONE-PIPE FORCED CIRCULATION SYSTEM (EXAMPLE 4)

Solution. Assume that the circulating pump will develop a head of 2 ft or 24,000 milinches and that a 1 in. pipe is to be used. The equivalent length of the circuit will then be 45 ft, as in Fig. 7, and the available head will be 24,000/45, or 533 milinches per foot. In Fig. 3, find 533 on the left scale, move horizontally to the intersection with the 1 in. pipe line, and read about 77 Mbh delivered by the pipe (with a velocity of about 35 in. per second) for a temperature difference of 20 deg. Since the circuit is to deliver only 20 Mbh, the temperature difference will be 20 divided by 77 and multiplied by 20, or 5.2 deg. Hence, if the flow riser temperature is 200, the return riser temperature will be about 195, and the average water temperature in the radiator about 197.5 F.

If a ½ in. pipe were used instead of a 1 in., the equivalent length of circuit would be 35 ft instead of 45; the unit head, 686 milinches instead of 533; the velocity, 27 in. per second instead of 35; the temperature difference, 19.5 instead of 5.2; and the average water temperature in the radiator, about 190.5 instead of 197.5 F.

If the 1 in. pipe is used for the circuit, the gravity head will be 22 milinches per foot, or 220 for the circuit (Fig. 1, 200 to 195). Since this is only 1 per cent of the pump head (24,000 milinches), it may be neglected in the calculation, as was done previously. However, there are cases in which the gravity head is so large compared with the pump head that it should be included in the calculation.

The methods just described for the design of the two elementary systems are fundamental and apply to the design of all hot water heating systems. In every system, however large and complicated, the pipe system must be such that the head forcing the water from the boiler to any one radiator is equal to the friction in that radiator's circuit when the

radiator is receiving its proper quantity of hot water and the system is functioning at a steady rate.

Other examples illustrating design of various systems follow.

One-Pipe Gravity Circulation System

Example 3. Select pipe sizes for the one-pipe gravity system having a total load of 67,500 Btu, shown in Fig. 10. Assume: flow temperature 190 F, return temperature 160 F, mains 5 ft above datum plane of boiler, center plane of radiators 4 ft above the mains, length of main 100 ft.

Solution: From Fig. 1 the available circulating head for 190 F flow and 160 F return temperature is 126 milinches per foot of height. The available circulating head for design of the main is therefore 5 x 126 = 630 milinches. The measured length of main plus 50 per cent added for resistance of fittings equals 150 ft equivalent length.

The main can then be designed for a friction loss of 630 ÷ 150 = 4 milinches per foot. From Table 2 at 4 milinch friction loss, a 2 in. pipe will supply 33 Mbh and a 2½ in. pipe will supply 53.1 Mbh at 20 deg drop. This is equivalent at 30 deg drop to 49.5 Mbh for 2 in. and 79.6 Mbh for 2½ in. pipe. A 2½ in. main will therefore be selected and the pressure drop will be somewhat less than 4 milinches per foot.

The piping from main to radiators is sized in a similar manner. Assume that water reaches point B, Fig. 10, at 190 F and has a 30 deg drop in the radiator circuit. From Fig. 1 the available head is 126 milinches per foot of height or a total of 4 × 126 = 504 milinches for the circuit (with the radiator 4 ft above the main).

The measured length of piping is 11 ft and the fittings add 14 elbow equivalents (which would be equivalent to 22 ft if the pipe size is assumed to be ¾ in.); the equivalent length is therefore 33 ft. The circuit can therefore be designed for a friction loss of 504 ÷ 33 = 15 milinches per foot.

From Table 2 by interpolation a ¾ in. pipe would supply 5.85 Mbh at 20 deg drop or 8.78 Mbh at 30 deg drop. Since the load is 9 Mbh the ¾ in. size will be satisfactory.

The remaining radiator circuits may be sized in a similar manner. Allowance should be made in one-pipe gravity systems for the drop in temperature which occurs in the supply main as the cooler water returns from the radiators. The drop will be in the same proportion to the total drop of 30 deg which the load supplied to any point in the main bears to the total system load; *e.g.* the temperature at D will be $190 - \left(\frac{9000}{67{,}500} \times 30\right) = 186$ F. At point F the temperature will be $190 - \left(\frac{9000 + 10{,}500}{67{,}400} \times 30\right) = 181$ F.

One-Pipe Forced Circulation System

Example 4. Select pipe sizes for the one-pipe forced circulation system having a load of 67,500 Btu shown in Fig. 11. Assume a water temperature drop of 20 deg. The water temperature does not affect the size of piping but does affect the radiator sizes required.

Solution: The water to be circulated at 20 deg drop will be 67,500 ÷ 20 = 3375 lb per hour or $\frac{3375}{8 \times 60} = 7$ gpm.

By reference to manufacturers' pump capacity charts, such as illustrated in Fig. 12, it will be found that a 1 in. pump will deliver 7 gpm against a head of 4½ ft (54,000 milinches).

Since the main from A to O has an equivalent length of 150 ft (100 ft actual length plus 50 per cent added for friction loss in fittings), the main may be sized for 54,000/150 = 360 milinches per foot.

From Table 2 by interpolation at 360 milinches friction loss and at 20 deg drop a 1 in. pipe would supply 62,600 Btu per hour and a 1¼ in. pipe would supply 131,600. Since the 1 in. pipe is too small, a 1¼ in. pipe will be used.

Since the 1¼ in. pipe offers less than 360 milinches resistance per foot, the velocity of water will increase until the output of the pump and the friction loss are in equilibrium at some point on the pump performance curve, for instance, at 10 gpm and a head of 4 ft or 48,000 ÷ 150 = 320 milinches per foot of pipe. The friction loss in the main between flow and return connections to radiators will be assumed to be 320 milinches per foot.

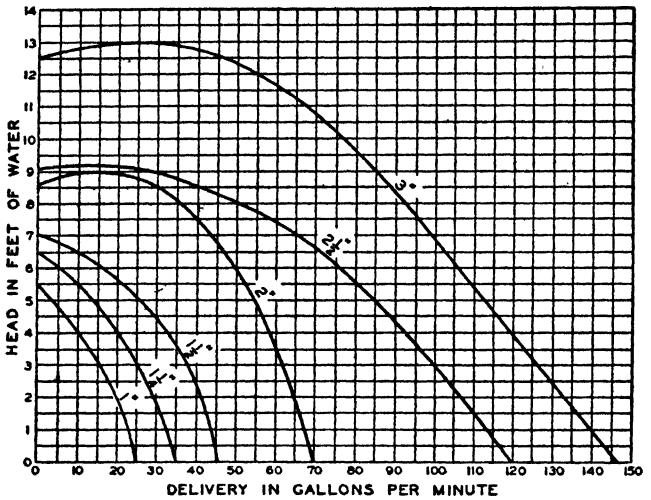

FIG. 12. PERFORMANCE CHART FOR CIRCULATING PUMP

In determining sizes for the piping from the main to any radiator, the resistance in the radiator circuit such as B-C (which has a load of 9 Mbh) is made equal to the resistance in the main from B to C which, if there are 3 ft of main between connections, is 3 x 320 = 960 milinches. If the total equivalent length of the radiator circuit determined by use of Table 1 is 32 ft, the radiator circuit B-C will be sized for a friction loss of 960 ÷ 32 = 30 milinches per foot, for which in Table 2 a ¾ in. pipe is found to supply 8550 Btu per hour and will be considered ample.

Other radiator circuits such as D-E, F-G etc. can be sized in a similar manner.

Two-Pipe Gravity System (with Reversed Return)

Example 5. Select pipe sizes for the two-pipe gravity system shown in Fig. 13. The center plane of the highest radiator is 8 ft above the center plane of the boiler. Assume a 180 F flow temperature and a 150 F return temperature.

Solution. The piping should be sized so that the frictional resistance at the desired rate of flow is equal to the available circulating head.

From Fig. 1 at 180 F flow and 150 F return temperature the available head is 118 milinches per foot of height or 8 × 118 = 944 milinches total for the highest radiator. The longest circuit from boiler to radiator and back to boiler must therefore have a resistance of 944 milinches. The longest circuit (see Fig. 13) is A-D + D-H + H-N containing 38 ft of pipe and, if 50 per cent is added for equivalent length of fittings, the equivalent length is 57 ft.

The circuit should then be designed for a friction loss of 944 ÷ 57 = 16 milinches per foot (approximately).

The pipe size may be found from Table 2 at 16 milinches per foot as follows:

SECTION	LOAD MBH	SIZE OF PIPE FOR 16 MILINCHES PER FOOT	SECTION	LOAD MBH	SIZE OF PIPE FOR 16 MILINCHES PER FOOT
A-B	58	2	G-H	11	1
B-C	31	1½	H-K	19	1¼
C-D	20	1¼	K-L	25	1¼
D-E	16	1¼	L-M	31	1½
E-F	6	¾	M-N	58	2

Pipe sizes to the radiators may be sized for the same resistance per foot. From Table 2 at 16 milinch per foot the sizes will be selected as follows:

Radiator	#1	#2	#3	#4	#5	#6
Load, Mbh	11	8	6	6	24	8
Pipe size, In.	1	1	¾	¾	1¼	¾

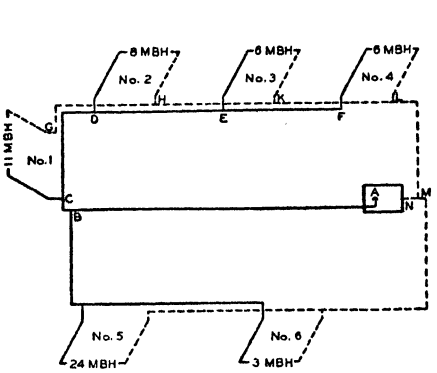

FIG. 13. TWO-PIPE REVERSED RETURN GRAVITY SYSTEM (EXAMPLE 5)

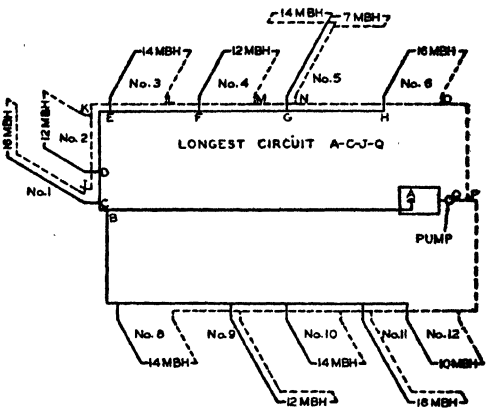

FIG. 14. FORCED CIRCULATION TWO-PIPE REVERSED RETURN SYSTEM

A hot water heating system will adjust its rate of flow until the friction loss balances the available head. It is therefore self-correcting in regard to small errors made in selection of pipe sizes.

Two-Pipe Forced Circulation System

Example 6. Select pipe sizes for the two-pipe forced circulation reversed return system having a total load of 159 Mbh shown in Fig. 14. Assume a difference of 20 deg in supply and return water temperature. The total equivalent length of the longest circuit is 180 ft. The gravity circulating head due to difference in temperature may be disregarded in design.

Solution. The water to be circulated is 159,000 ÷ 20 = 79,500 lb per hour or $\frac{7950}{60 \times 8}$ = 16.5 gpm. From a pump performance chart such as Fig. 12 it is found that 16.5 gpm will be delivered by a 1 in. pump against a 3 ft head (36,000 milinches) or a 1¼ in. pump against a 4.5 head (54,000 milinches).

The longest circuit including the supply and return main and the longest radiator circuit is 120 ft and, if 50 per cent is added for friction loss in fittings, the equivalent length is 180 ft. If the 1 in. pump is used, the piping will be sized for 36,000/180 =200 milinches per foot, resulting in selection from Table 2 of a 2 in. main for the Section A-B which supplies 159 Mbh. The large difference in pump and main size, as well as the low velocity resulting from the 200 milinch per foot friction loss, indicates that the 1¼ in. pump should be considered. The design friction loss, if the 1¼ in. pump is used, can be 54,000/180 = 300 milinches per foot and at this friction loss Table 2 will indicate the pipe sizes for the various sections in Fig. 14 as follows:

SUPPLY			RETURN		
Section	Mbh	Pipe Size, In.	Section	Mbh	Pipe Size, In.
A-B	159	1½	J-K	16	¾
B-C	91	1¼	K-L	28	¾
C-D	75	1¼	L-M	42	1
D-E	63	1¼	M-N	54	1
E-F	49	1	N-O	75	1¼
F-G	37	1	O-P	91	1¼
G-H	16	¾	P-Q	159	1½

The radiator circuits may also be sized for the same friction loss, 300 milinches per foot, using Table 2 as follows:

Radiator	#1	#2	#3	#4	#5 and #6	#7
Load, Mbh	16	12	14	12	21	16
Pipe size, In.	¾	½	½	½	¾[a]	¾

[a]Where circuit divides, use ¾ in. branch to #5 and ½ in. to #6 radiator.

EXPANSION TANKS

Water heated from 40 F to 200 F expands about 0.04 of the original volume. The expansion tank permits the change in volume of the water in the heating system to take place without producing undesirable stresses due to pressure in any part of the system. Expansion tanks may be open, as illustrated in Fig. 15, or closed as shown in Fig. 16. An open expansion tank has free vent to the atmosphere and consequently the pressure on the surface of the water is always that of one atmosphere. The minimum contents of an open tank should be 0.06 of the volume of the water in the system including that in the boiler, heat transmitters, pipes, etc. This capacity is 50 per cent in excess of the actual increase in volume of water

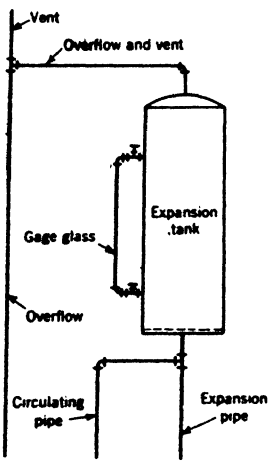

FIG. 15. AN OPEN EXPANSION TANK

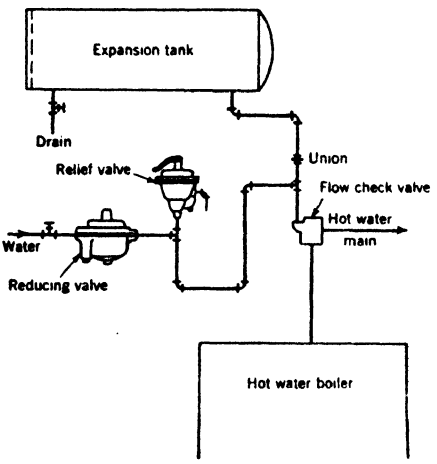

FIG. 16. A CLOSED EXPANSION TANK

due to increase in temperature from 40 F to 200 F. The tank should be located at least 3 ft above the highest radiator. Provision must be made to prevent freezing of the water in the tank as well as in the pipe leading to the tank.

When the vent from an open expansion tank is extended through the roof, it should be not less than 4 in. in diameter from a point below the roof, through and beyond the roof line. This will prevent vapor, which sometimes rises from an expansion tank, from closing the vent during outside freezing temperatures.

In a gravity circulation system, the pipe to the open expansion tank should be connected to the supply riser from the boiler, so that the air liberated from the water in the boiler will enter the expansion tank.

In a forced circulation system, the pipe to an open expansion tank should be connected on the suction side of the circulating pump.

A closed expansion tank is sealed against free venting to the atmosphere. The tank may be above the highest radiator or heat transmitter, or may be below the lowest one. The minimum contents of a closed expansion tank must be such that the expansion of the water due to increase in temperature will be cushioned against a reservoir of compressed air above the water level in the expansion tank. The tank must provide

space not only for the change in water volume, but also for variations in air volume within the tank due to changes in air pressure. If the closed expansion tank is below the heat transmitters, the tank should be larger than if it is above them, and the higher the building, under such circumstances, the larger should be the air capacity in excess of that required for increase in water volume due to temperature rise.

The size of an expansion tank for installation in a closed system may be determined by the following formula:

$$V = \frac{E}{\frac{P_1}{P_1 + 0.434\,H} - \frac{P_1}{P_2}} \tag{3}$$

where

V = required tank capacity, gallons.
E = expansion of water from cold system to flow riser temperature, gallons.
P_1 = atmospheric pressure, psia.
P_2 = maximum tank pressure specified for heated system, psia.
H = height of top of filled system above tank, feet. (NOTE: Top of system open to atmosphere when system is filled.)

Example 7. Select a closed expansion tank for basement installation on a system containing 5000 gal and operating at 200 F flow temperature. The static head due to the height of the system is 70 ft. The maximum pressure should not exceed 100 psig.

Solution. Assume that the system is filled at 40 F. Then

$$E = 0.04 \times 5000 = 200 \text{ gal}$$
$$P_1 = 14.7 \text{ psia}$$
$$P_2 = 100 + 14.7 = 114.7 \text{ psia.}$$

Substituting these values in Equation 3:

$$V = \frac{200}{\frac{14.7}{14.7 + 0.434\,(70)} - \frac{14.7}{114.7}} = \frac{200}{0.327 - 0.128} = 1000 \text{ gal.}$$

The size of a basement-located closed expansion tank should be at least equal to the following:

One story buildings:	$x = 0.10\ V$	Three story buildings:	$x = 0.17\ V$
Two story buildings:	$x = 0.13\ V$	Four story buildings:	$x = 0.23\ V$

where x = expansion tank size in gallons.
V = water volume in heating system in gallons.

This condition favors, especially in tall buildings, the placing of the closed expansion tank above the highest heat transmitter.

It is common practice to make multiple tank installations on large systems in lieu of having a tank made where the capacity required is beyond commercially manufactured sizes.

Any closed expansion tank located above the heat transmitters of a hot water heating system should be connected by a direct pipe with the flow main leaving the boiler, in order to enable the air to pass easily to the expansion tank. In a closed hot water heating system the water under pressure tends to absorb air at a rate increasing with pressure increase and decreasing with temperature increase.

Means must be provided to adjust and to observe the proportion of air within any closed expansion tank. This involves the provision of an air

inlet valve, a water gage, and a relief valve. A source of supply of compressed air for renewing the air cushion is highly desirable, especially in large, high pressure, hot water heating systems where it is inconvenient, if not impracticable, to drain down the water in the system so as to permit introduction of atmospheric pressure air.

For every hot water heating system the designer should calculate the volume of water contained in the radiators, piping system, boiler, etc., in order to select the proper size of expansion tank. The water content of the piping can be obtained from Table 6. For a rough selection of size, however, it is sometimes assumed that 50 per cent of the volume of water is contained in the radiators, and that the water content per square foot of radiator heating surface is 0.2 gal for column radiators and 0.13 gal for tube type radiators.

Another rough method for determining the size of an expansion tank to be located above the highest radiator is to divide the square feet of radiation by the factor 40 to obtain the required capacity in gallons of the expansion tank.

TABLE 6. VOLUME OF WATER IN STANDARD PIPE

PIPE SIZE, IN.	LINEAL FT OF PIPE CONTAINING 1 GAL	PIPE SIZE, IN.	LINEAL FT OF PIPE CONTAINING 1 GAL
½	63.1	2	5.75
¾	36.1	2½	4.02
1	22.2	3	2.60
1¼	12.8	4	1.52
1½	9.47	5	0.96
		6	0.67

INSTALLATION DETAILS

Items that should be considered in the design of this type of system are:

All piping must be so pitched that all air in the system can be vented either through an open expansion tank, radiators or automatic relief valves. When piping must be run around an obstacle such as a beam, it is advisable to drop the piping below the beam. If looped over the beam, it becomes necessary to provide for venting of air from the high point of the pipe.

When changing the size of horizontal runs of pipe, eccentric fittings should be used to keep the tops of the pipes in line to permit free passage of air along the pipe.

All piping must be arranged so that the entire system can be drained. Sections of piping individually valved shall have corresponding drain valves.

In large buildings, the piping may be zoned according to exposure of building, usage of building, or method of control.

All piping must be installed so that it is free to expand and contract with changes of temperature without producing undue stresses in the pipes or connections. For this purpose it is generally sufficient to allow for a variation in length of 1 in. for 100 ft of pipe.

The pipe system should be designed so that each circuit has its correct friction for balanced water distribution. This may be done by change of pipe size or change in piping detail.

The connections from the boiler to the mains should be short and direct, to reduce the friction and should allow for expansion.

The mains and branches should pitch up and away from the heater, generally not less than 1 in. in 10 ft.

The connections from mains to branches and to risers should be such that circulation through the risers will start in the right direction. Hence, in a one-pipe system the flow connection must be nearer the heater than the return connection. In a correctly-designed two-pipe system, the pressure in the flow main is higher than that in the return

main, and a slight variation in the distances of the flow and return connections from the heater is not material; but it is generally best to have the two connections about equally distant from the heater.

Generally, connections to risers or radiators are taken out of the top of mains either 45 or 90 deg.

Supply connections are usually made at the bottom of radiators so that circulation will not be stopped by accumulation of air, as would be the case with a top supply connection. Short radiators are sometimes connected for top supply and bottom return on the same end. When so connected, attention must be given to venting of air from the top of the radiator somewhat oftener than when bottom connections are used.

Unless used as heating surface, all piping, both flow and return, should be insulated.

All large systems should be provided with extra stop and drain valves, suitably located so that parts of the system may be isolated for repairs without making it necessary to drain the water from the entire system.

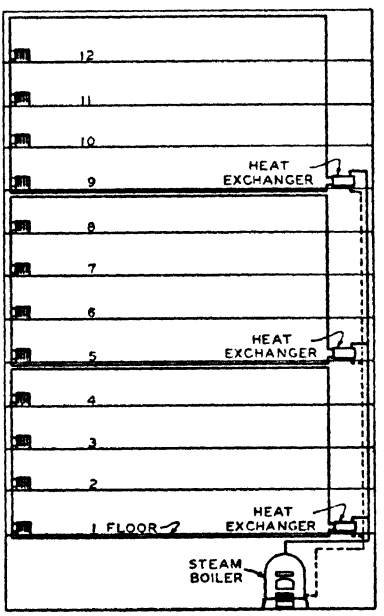

FIG. 17. ILLUSTRATION OF VERTICAL ZONING IN HOT WATER HEATING SYSTEM IN A 12-STORY BUILDING

ZONING

In large hot water systems improved control and economy can be achieved by separating the systems into sections or zones (vertical or horizontal) which can be operated independently of each other. Variations in heat requirement of the different zones as influenced by the exposure of the building, solar heat, weather conditions, heat from processes, type of occupancy, building chimney effect, etc. can readily be compensated for when heat can be supplied only where needed.

In tall buildings, vertical zoning such as shown in Fig. 17 not only provides the advantages of control and economy, but also reduces the water pressure in the system to that caused only by the number of floors served by each section. As shown in Fig. 17 a steam boiler can conveniently be used to supply steam to the heat exchangers supplying heated water to each zone.

Chapter 25

RADIATORS, CONVECTORS, COILS

Heat Emission of Radiators and Convectors, Types of Radiators, Convectors, Radiator and Convector Ratings, Effect of Operating Conditions, Heating Effect, Heating Up the Radiator and Convector, Enclosed Radiators, Coils, Coil Construction and Arrangement, Steam Coils, Water Coils, Direct-Expansion Coils, Flow Arrangement, Applications, Heat Transfer and Air Flow Resistance, Coil Selection

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RADIATORS and convectors are primarily used for heating and, since their performance is affected by many of the same conditions, they will be considered together, while coils will be treated separately in the latter part of the chapter.

HEAT EMISSION OF RADIATORS AND CONVECTORS

Most heating units emit heat by *radiation* and *convection*. An exposed *radiator* emits roughly half of its heat by radiation, the amount depending upon the size and number of sections. When the radiator is enclosed or shielded, the proportion of radiation is further reduced. The balance of the emission occurs by conduction to the air in contact with the heating surface, and the resulting circulation of the air warms by convection. A *convector* emits practically all of its heat by conduction to the air surrounding it and this heated air is in turn transmitted by convection to the rooms or spaces to be warmed, the heat emitted by radiation being negligible.

The output of a radiator can be measured only by the heat it emits and is generally expressed in units of: Btu per hr; *Mbh* (1000 Btu per hour); or in equivalent direct radiation (240 Btu per hour for steam or 150 for water radiation).

TYPES OF RADIATORS

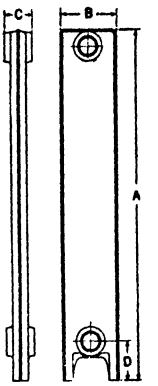
Present day radiators may be classified as tubular, wall, or window type and are generally made of cast-iron. Only the small-tube type of tubular radiators with a spacing of $1\frac{3}{4}$ in. per section are now available. Small-tube radiators occupy less space and are particularly suited for installation in recesses.

Baseboard radiation consists of long, low units which are made to resemble conventional baseboards and are installed along the outside walls of rooms in place of the usual wooden baseboard. Units are made either of hollow cast-iron panels (with, or without fins on the back) or of ferrous or non-ferrous finned tubing installed behind a metal enclosure. They are suited for use on hot water systems, but may also be used on two-pipe steam systems. Ratings are expressed in Btu per (hour) (linear foot) and must be obtained from the manufacturer as there is not yet a standardization of outputs for radiation of this type.

Among the advantages claimed for baseboard radiation are that it is inconspicuous; clean in operation; offers a minimum of interference with furniture placement; distributes the heat near the floor, thus preventing cold floors sometimes experienced—especially in basementless houses; and blankets exposed walls with a film of warmed air. This reduces floor to ceiling temperature gradient to about 2 F and tends to produce uniform temperatures throughout the room.

TABLE 1. SMALL-TUBE CAST-IRON RADIATORS

Number of Tubes per Section	Catalog Rating per Section[a]	Section Dimensions				
		A Height[c]	*B* Width		*C* Spacing[b]	*D* Leg Height[c]
			Minimum	Maximum		
	Sq Ft	In.	In.	In.	In.	In.
3[d]	1.6	25	3¼	3½	1¾	2½
4[d]	1.6	19	4 7/16	4 13/16	1¾	2½
	1.8	22	4 7/16	4 13/16	1¾	2½
	2.0	25	4 7/16	4 13/16	1¾	2½
5[d]	2.1	22	5⅝	6 5/16	1¾	2½
	2.4	25	5⅝	6 5/16	1¾	2½
6[d]	1.6	14	6 13/16	8	1¾	2½
	2.3	19	6 13/16	8	1¾	2½
	3.0	25	6 13/16	8	1¾	2½
	3.7	32	6 13/16	8	1¾	2½



[a]The square foot of equivalent direct steam radiation is defined as the ability to emit 240 Btu per hour, with steam at 215 F, in air of 70 F. These ratings apply only to installed radiators exposed in a normal manner; not to radiators installed behind enclosures, grilles, etc. (See A.S.H.V.E. Code for Testing Radiators adopted January, 1927.)

[b]Length equals number of sections times 1¾ in.

[c]Over-all height and leg height, as produced by some manufacturers, are one inch (1 in.) greater than shown in Columns *A* and *D*. Radiators may be furnished without legs. Where greater than standard leg heights are required this dimension shall be 4½ in.

[d]Or equal.

After a study of the demand for various sizes of radiators, the *Institute of Boiler and Radiator Manufacturers*, in cooperation with the Division of Simplified Practice, *National Bureau of Standards*, established Simplified Practice Recommendation R174-43 for small-tube cast-iron radiators. Table 1 shows the size and dimensions now being manufactured.

Wall radiators are now rated in terms of equivalent square feet, the same as small-tube radiators. Tests have shown that the heat emitted from a wall-type radiator may be reduced from 5 to 10 per cent if the radiator is placed near the ceiling with the bars horizontal and in an air temperature exceeding 70 F. When radiators are placed near the ceiling, there is usually such a large difference in the temperature between the floor level and the ceiling that it becomes difficult to heat the living zone of the room satisfactorily.

Pipe coils are assemblies of standard pipe or tubing (1 in. to 2 in.) which are used as radiators. In older practice these coils were commonly used

TABLE 2. HEAT EMISSION OF PIPE COILS PLACED VERTICALLY ON A WALL (PIPES HORIZONTAL) CONTAINING STEAM AT 215 F AND SURROUNDED WITH AIR AT 70 F

Btu per linear foot of coil per hour (not linear feet of pipe)

Size of Pipe	1 In.	1¼ In.	1½ In.
Single row	132	162	185
Two	252	312	348
Four	440	545	616
Six	567	702	793
Eight	651	796	907
Ten	732	907	1020
Twelve	812	1005	1135

in factory buildings, but now wall-type radiators are most frequently used for this service. When coils are used, the miter type assembly is preferable as it readily permits expansion in the pipe. Cast manifolds or headers, known as branch tees, are available for this construction.

The heat emission of pipe coils placed vertically on a wall with the pipes horizontal is given in Table 2 which has been developed from available data and does not represent definite results of tests. For such coils the heat emission varies as the height of the coil. The heat emission of each pipe of ceiling coils, placed horizontally, is about 126 Btu, 156 Btu, and 175 Btu per linear foot of pipe, respectively, for 1-in., 1¼-in., and 1½-in. coils.

CONVECTORS

Cast-iron radiators may be concealed in a cabinet or other enclosure for appearance. In such cases a greater percentage of heat is conveyed to

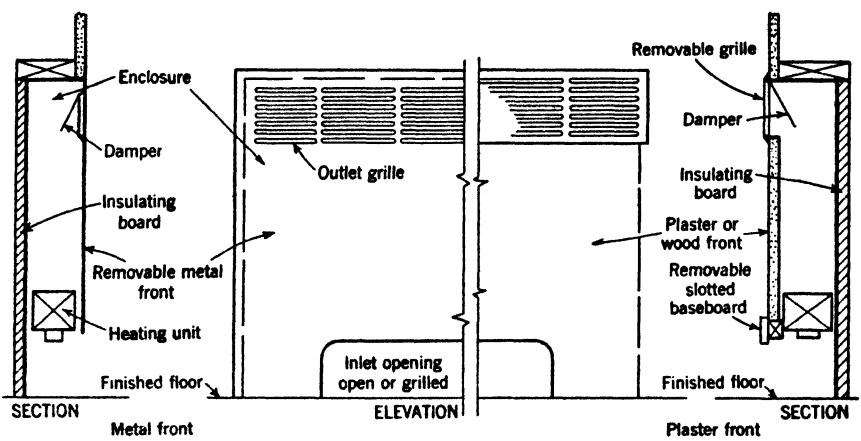


FIG. 1. TYPICAL RECESSED CONVECTOR

the room by convection thereby resulting in a form of gravity convector. A typical recessed convector is shown in Fig. 1. The heating element consisting of a large percentage of fin surface is usually shallow in depth and placed low in the enclosure in order to produce maximum chimney effect in the enclosure. The air enters the enclosure near the floor line just below the heating element, is moderately heated in passing through the core and is delivered to the room through an opening near the top of the enclosure. This air movement accomplishes a reduction in temperature differentials and assures maximum comfort in the living zone.

Concealed heaters or convectors are generally available as completely built-in units. Combinations are available in several styles for installations, such as the wall-hung type, free-standing floor type, recess type set flush with wall or offset, and the completely concealed type. Most of these types may be arranged with a top outlet grille in a plane parallel with the floor, although the front outlet is practically standard. In cases where enclosures are to be used but are not furnished by the heater manufacturer, it is important that the proportions of the cabinet and the grilles be so designed that they will not impair the performance of the assembled convector. It is desirable that the enclosure or housing for the

convector fit as snugly as possible so that the air to be heated cannot by-pass the heating element in passing through the enclosure.

The output of a convector, for any given length and depth, is a function of the height. Published ratings are generally given in terms of equivalent square feet, corrected for heating effect. However, an extended surface heating unit is entirely different structurally and physically from a direct radiator and, since it has no area measurement corresponding to the heating surface of a radiator, many engineers believe that the performance of convectors should be stated in Btu. For steam convectors, as for radiators, 240 Btu per hour may be taken as an equivalent square foot of radiation. When more than one heating unit is used, one mounted above the other in the same cabinet, the output of the upper unit or units will be materially less than that of the bottom unit.

RADIATOR AND CONVECTOR RATINGS

A standard method of testing radiators was adopted by the A.S.H.V.E. in 1927 [1]. This Code provides for a standard test room, the temperature of which is to be maintained at 70 F, measured in the center of the room at an elevation of 5 ft above the floor. The steam temperature in the radiator is to be 215 F, which corresponds to 15.6 lb per square inch absolute. The weight of condensate per hour, under these standard conditions, multiplied by the difference in the enthalpy of the steam entering the radiator and that of the condensate leaving the radiator, gives the radiator output in Btu per hour. This output divided by 240 gives the steam rating of the radiator in equivalent square feet.

Similar test methods for convectors are the A.S.H.V.E. Codes for Testing and Rating Concealed Gravity Type Radiation [2], (Steam Code 1932 and Hot Water Code 1933). These Codes recognize a different type of test booth, and the air temperature used is that of the air entering the convector casing instead of the temperature in the center of the room. The entering air temperature for standard test conditions is 65 F. For hot water the standard test conditions call for a mean temperature of the water in the convector of 170 F.

The *Convector Manufacturers Association* has adopted the A.S.H.V.E. standard in the formulation of its ratings and has compiled a tentative standard of heating effect allowances for various enclosure heights to be included in the ratings by its members.

All published ratings bearing the title *C.M.C. Ratings* (*Convector Manufacturers Certified Ratings*) indicate that the convectors have been tested in accordance with the A.S.H.V.E. Code by an impartial and disinterested laboratory and that the ratings have been approved by the Standardization Committee of the *Convector Manufacturers Association.*

Effect of Operating Conditions

The heat output of a radiator is proportional to the 1.3 power of the temperature difference between the air in the room at the 60 in. level and the heating medium in the radiator. The heat output of a convector is proportional to the 1.5 power of the temperature difference between the air entering the convector and the heating medium, steam or hot water, within the convector [3]. For hot water the arithmetical average between entering and leaving water temperatures is used. These laws may be expressed as correction factors to change from output under standard

TABLE 3. CORRECTION FACTORS FOR DIRECT CAST-IRON RADIATORS AND CONVECTORS[a]

STEAM PRESS. APPROX.		HEATING MEDIUM TEMP F STEAM OR WATER	FACTORS FOR DIRECT CAST-IRON RADIATORS							FACTORS FOR CONVECTORS						
			ROOM TEMPERATURE F							INLET AIR TEMPERATURE F						
Gage Vacuum In. Hg.	Abs. Lb per Sq In.		80	75	70	65	60	55	50	80	75	70	65	60	55	50
22.4	3.7	150	2.58	2.36	2.17	2.00	1.86	1.73	1 62	3.14	2.83	2.57	2.35	2.15	1.98	1.84
20.3	4.7	160	2.17	2.00	1.86	1.73	1.62	1.52	1.44	2.57	2.35	2.15	1.98	1.84	1.71	1.59
17.7	6.0	170	1.86	1.73	1.62	1 52	1.44	1.35	1.28	2.15	1.98	1.84	1.71	1.59	1.49	1.40
14.6	7.5	180	1.62	1.52	1.44	1.35	1.28	1.21	1.15	1.84	1.71	1.59	1.49	1.40	1.32	1.24
10.9	9.3	190	1.44	1.35	1.28	1.21	1.15	1.10	1.05	1.59	1.49	1.40	1.32	1.24	1.17	1.11
6.5	11.5	200	1.28	1.21	1.15	1.10	1.05	1.00	0.96	1.40	1.32	1.24	1.17	1.11	1.05	1.00
LbperSqIn																
1	15.6	215	1.10	1.05	1.00	0.96	0.92	0.88	0.85	1.17	1.11	1.05	1.00	0.95	0.91	0.87
6	21	230	0.96	0.92	0.88	0.85	0.81	0.78	0.76	1.00	0.95	0.91	0.87	0.83	0.79	0.76
15	30	250	0 81	0.78	0.76	0.73	0.70	0.68	0.66	0.83	0 79	0.76	0.73	0.70	0.68	0.65
27	42	270	0.70	0 68	0.66	0.64	0.62	0 60	0.58	0.70	0.68	0.65	0.63	0.60	0.58	0.56
52	67	300	0.58	0.57	0.55	0.53	0.52	0.51	0.49	0 56	0.54	0.53	0.51	0.49	0.48	0.47

[a]To determine the size of a radiator or a convector for a given space, divide the heat loss in Btu per hour by 240 and multiply the result by the proper factor from the above table.

To determine the heating capacity of a radiator or a convector under conditions other than the basic ones with the heating medium at a temperature of 215 F, and the room temperature at 70 F in the case of a radiator, and the inlet air temperature at 65 F in the case of a convector, divide the heating capacities at the basic conditions by the proper factor from the above table.

rating-test conditions to output under other operating conditions. Such factors are given in Table 3.

When it is desired to change the output under any test conditions to the corresponding output under standard Code test conditions, the reciprocal form of correction factor may be derived. The equations for steam units are:

For radiators:

$$C_s = \left(\frac{215 - 70}{t_s - t_r}\right)^{1.3} \qquad (1)$$

For convectors:

$$C_s = \left(\frac{215 - 65}{t_s - t_i}\right)^{1.5} \qquad (2)$$

The output under standard conditions will be:

$$H_s = C_s H_t \qquad (3)$$

where

C_s = correction factor.
t_s = steam temperature during test, Fahrenheit degrees.
t_r = room temperature during test, Fahrenheit degrees.
t_i = inlet air temperature during test, Fahrenheit degrees.
H_s = heat emission rating under standard conditions, Btu per hour.
H_t = heat output under test conditions, Btu per hour.

The relation between the size of the radiator or convector and the size of the test room will affect the results obtained in a capacity-rating test.[4] The height and location of the radiator and the insulation of the test room are other important factors that are not specifically regulated by the Code.

For a radiator, the finish coat of paint affects the heat output. Oil paints of any color will give about the same results as unpainted black or rusty surfaces, but an aluminum or a bronze paint will reduce the heat emitted by radiation. The net effect may be a reduction of 10 per cent or more in the total heat output of the radiator [5,6,7].

Radiator enclosures and convector casings affect the heat distribution within the room as well as the total amount of heat supplied by the steam or hot water [8]

Heating Effect

For several years the term *heating effect* has been used to designate the relation between the *useful output* of a radiator, in the comfort zone of a room, and the total input as measured by steam condensation or water temperatures [9, 10]. The application of such a heating effect factor is a recognition that some radiators and convectors use less steam than others for producing equal comfort heating results in the room.

No standard method for evaluating the heating effect of radiators and convectors and correlating it with comfort has yet been accepted. One method, with test data [11] on radiators and convectors, and making use of the eupatheoscope for evaluating the environment produced, has been suggested by the University of Illinois. The principle underlying the eupatheoscope involves the measurement of the heat loss from a sizable

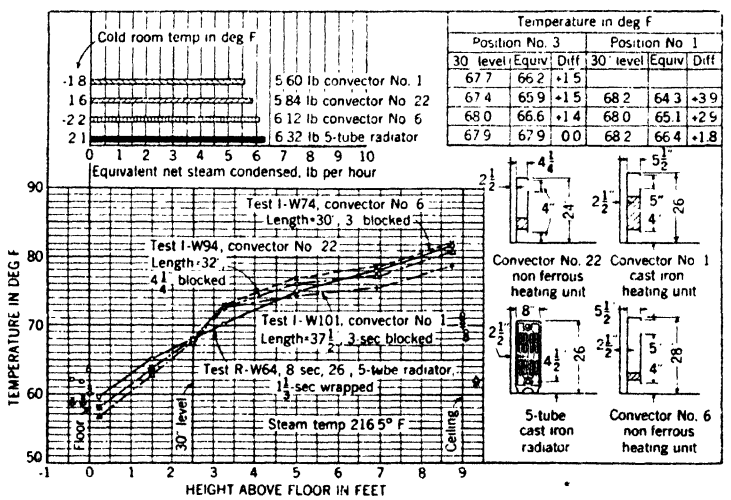


FIG. 2. TEMPERATURE GRADIENTS AND EQUIVALENT TEMPERATURES FOR RADIATOR AND CONVECTORS WITH COMMON 30 IN. LEVEL TEMPERATURE

body by radiation and convection, when the surface is maintained at some constant temperature. Through the use of this instrument and its calibration curve, non-uniform environments may be referred to uniform environments in which the air and all surrounding surfaces are at the same temperature. The temperatures of the uniform environments are referred to as equivalent temperatures.

The Kata thermometer [12], the thermo-integrator [13,14], and the globe [15] thermometer are other instruments which have been used to measure the influence of air temperature, air movement and radiation in an environment.

Data given in Fig. 2 show that while the air temperature at the 30-in. level is the same for the three convectors and the one large-tube cast-iron radiator, in position No. 3 in the test room, the equivalent temperature is 1.5 F lower than the air temperature in the case of the three convectors, and the same as the air temperature in the case of the radiator. The difference between the minimum and the maximum amount of heat

required to maintain the common air temperature at the 30-in. level is of the order of 13 per cent.

In Fig. 3 are shown the results of tests made with the same three convectors and the one large-tube cast-iron radiator, so adjusted in size that each gave approximately the same equivalent temperature in the No. 3 position in the test room. The difference between the minimum and the maximum amount of heat required to maintain the common equivalent temperature is of the order of 7 per cent.

The following statements applying to the use of radiators are based on experience and test results:

1. The heating effect of a radiator cannot be judged solely by the amount of steam condensed within the radiator.

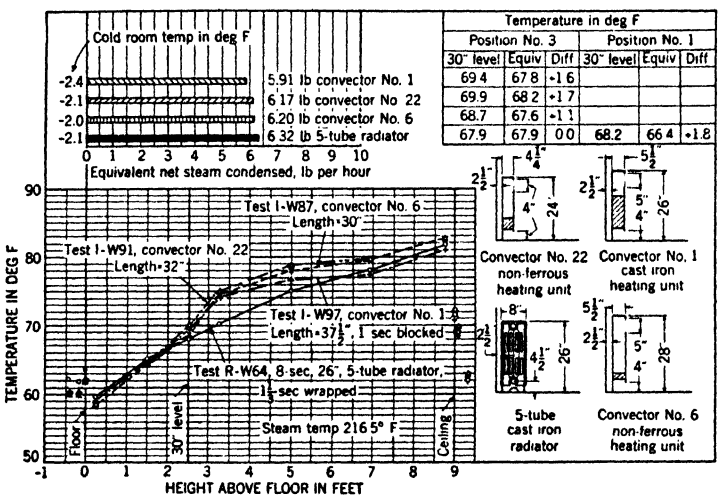


FIG. 3. TEMPERATURE GRADIENTS AND EQUIVALENT TEMPERATURES FOR RADIATOR AND CONVECTORS WITH COMMON EQUIVALENT TEMPERATURE

2. Smaller floor-to-ceiling temperature differentials can be maintained with long, low, thin, direct radiators, than is possible with high, direct radiators.

3. The larger portion of the floor-to-ceiling temperature differential in a room of average ceiling height heated with direct radiators occurs between the floor and the breathing level.

4. The comfort level (approximately 2 ft-6 in. above floor) is below the breathing line level (approximately 5 ft-0 in. above floor), and temperatures taken at the breathing line may not be indicative of the actual heating effect of a radiator in the room. The comfort-indicating temperature should be taken below the breathing line level.

5. High column radiators placed at the sides of window openings do not produce as comfortable heating effects as long, low, direct radiators placed beneath windows.

HEATING UP THE RADIATOR AND CONVECTOR

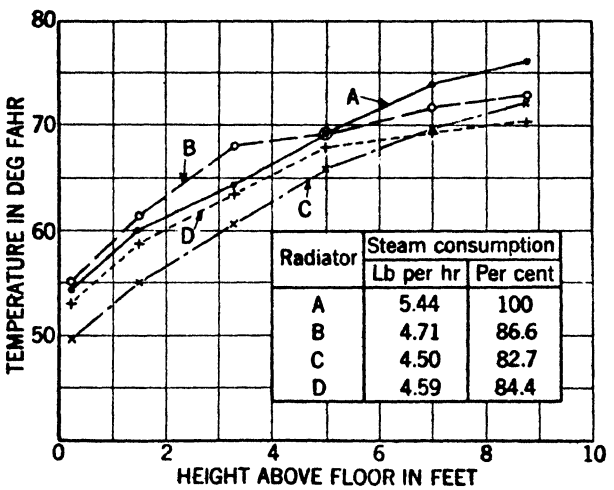
The maximum condensation occurs in a heating unit when the steam is first turned on. Tests [16] on an old-style column-type cast-iron radiator indicated that in the first 10 min the condensation rate reached a peak of 0.95 lb per square foot of radiator per hour and 10 to 15 min later dropped

to a rate of 0.24 lb. In practice the rate of steam supply to the heating unit, while heating up, is frequently retarded by controlled elimination of air through air valves or traps. Automatic control valves may also retard the supply of steam. Vacuum types of air venting valves may be used to reduce the length of the venting periods.

ENCLOSED RADIATORS

The general effect of an enclosure placed about a direct radiator is to restrict the air flow, diminish the radiation and, when properly designed, improve the heating effect. Investigations [10] indicate that in the design of the enclosure three things should be considered:

1. There should be better distribution of the heat below the breathing line level to produce greater heating comfort and lowered ceiling temperatures.



Radiator	Steam consumption	
	Lb per hr	Per cent
A	5.44	100
B	4.71	86.6
C	4.50	82.7
D	4.59	84.4

Fig. 4. Steam Consumption of Exposed and Concealed Radiators

2. The lessened steam consumption may not materially change the radiator heating performance.

3. The enclosed radiator may inadequately heat the space.

A comparison between a bare or exposed radiator (A) and the same radiator with a well-designed enclosure (B), with a poorly-designed enclosure (C), and with a cloth cover (D) will illustrate the relative heating effects. In Fig. 4 the curve (B) reveals that the enclosed radiator used less steam than the exposed radiator, but gave a satisfactory heating performance. A well-designed shield placed over a radiator gives about the same heating effect. Curve (C) shows the unsatisfactory effects produced by improperly-designed enclosures. Curve (D) shows that the effect of a cloth cover extending downward 6 in. from the top of the radiator was to make the performance unsatisfactory and inadequate.

Some commercial enclosures and shields for use on direct radiators are equipped with water pans for the purpose of adding moisture to the air in the room. Tests [17] show that an average evaporative rate of about 0.235 lb per square foot of water surface per hour may be obtained from

such pans, when a radiator is steam heated and the relative humidity in the room is between 25 and 40 per cent. This source of supply of moisture alone is not adequate to maintain a relative humidity above 25 per cent on a zero day.

COILS

Coils described in this chapter are used for heating or cooling an air stream under forced convection. Surface coil equipment may be made up of a number of banks assembled in the field, or the entire assembly may be factory constructed. The applications of each type of coil are limited to the field within which it is rated. Other limitations are imposed by code regulations, by proper choice of materials for the fluids used and the condition of the air handled, or by an economic analysis of the possible alternates on each installation.

For heating service, coils are used as preheaters, reheaters or booster heaters. The function of the coils is air heating only, but the apparatus assembly may include means for humidification and air cleaning. Steam or hot water are the usual heating media, although others are used in special cases, such as reheating by means of discharge gas from a refrigerating system.

Coils are used for air cooling with or without accompanying dehumidification. Examples of cooling applications without dehumidification are precooling coils using well water or other relatively high temperature water to reduce the load on the refrigerating machinery, or water cooled coils to remove sensible heat in connection with chemical moisture-absorption apparatus. By proper coil selection it is possible to handle both sensible cooling and dehumidification together as explained later. The assembly usually includes air cleaning means to protect the coil from accumulation of dirt and to keep dust and foreign matter out of the conditioned space. Although cooling and dehumidification are the usual functions, there are cases of cooling coils purposely wetted to aid in air cleaning and odor absorption.

The usual cooling media used in surface coils are cold water or Group I (*ASA* Classification) refrigerants, but others are used in special cases. Brines are seldom required for the range of applications covered by this chapter, although there are cases where low entering air temperatures with large latent heat loads require a refrigerant temperature so low that water becomes impractical. Sometimes, also, brine from an industrial system already installed is the only convenient source of refrigeration.

For combined cooling and dehumidifying, surface coils present an alternate to spray dehumidifiers. For many applications it is possible, by proper selection of apparatus, choice of air velocities, refrigerant temperatures, etc., to perform the same duty with either. In a few cases both sprays and coils are used. The coils may then be installed within the spray chamber, either in series with the sprays or below them. In making the selection between spray and surface dehumidifiers, certain advantages of each should be considered. The fact that a spray dehumidifier is usually designed to deliver nearly saturated air tends to simplify the control problem. In this case the dry-bulb temperature is also the dew-point, and hence a dew-point control can be arranged by using a simple duct thermostat. Spray dehumidifiers have an advantage over unwetted coils of obtaining some air cleaning and odor absorption. On

the other hand, coils make possible a closed and balanced cooling water circuit, obviating the unbalanced pumping head, the complication of water level control, and danger from possible floods incidental to multiple spray dehumidifiers, especially if located on different levels. The use of coils often makes it possible for the same surface to serve for summer cooling and winter heating by circulating cold water in the one season and hot water in the other, with consequent saving in apparatus and piping. Another advantage is that where the surface coil system can be used with direct expansion of refrigerant, it is comparatively low in initial and operating costs. The safety of the occupant must be kept in mind in comfort conditioning applications. Some localities have refrigeration codes which restrict the use of direct-expansion coils in the air stream, and hence local codes should be consulted by the engineer before a system employing direct expansion methods is designed. The choice between spray dehumidifiers and coils depends upon the necessities and the economic aspects of each case and no general rule can be given. There are many installations in which either may be used.

COIL CONSTRUCTION AND ARRANGEMENT

Coils are basically of two types, those consisting of plain tubes or pipe and those having *extended* surfaces. The former are little used for the applications covered by this chapter, but are often employed where conditions cause frost accumulation, and for cooling within spray dehumidifiers.

The heat transmission from air passing over a tube to a fluid flowing within it is impeded by three resistances. The first resistance is from the air to the surface of the tube, usually called the outside surface resistance or air-film resistance. Second is the resistance to the flow of heat by conduction through the metal itself. Finally there is another surface or film resistance to the flow of heat between the inside surface of the metal and the fluid in the tube. For the applications under consideration both the resistance of the metal wall to heat conduction, and the inside surface or film resistance are usually low as compared with the air-side surface resistance. Economy in space, weight and cost makes it advantageous to decrease the external surface resistance, where it is proportionately large, to approach that of the tube wall, and that from the tube to refrigerant. This may be accomplished by increasing the external surface by means of fins. Sometimes water spray is applied to the same type surface as would have been used without it. The over-all heat transfer is not necessarily increased much by such an arrangement, but the water spray may serve other purposes than to increase the flow of heat, such as air and coil cleaning. (See Chapter 7).

In fin or *extended* surface coils the external surface of the tubes is known as *primary* and the fin surface is called *secondary*. The primary surface consists generally of round tubes or pipes. In some cases these are staggered and in others in line with respect to the air flow. The staggered arrangement gives a somewhat higher heat transfer value but also a higher resistance to air flow and in some cases makes the header and return bend arrangement more complicated. Numerous types of fin arrangement are used, the most common of which are spiral, flat and flat-crinkled or corrugated, all as shown in Fig. 5. While the spiral fin surrounds each tube individually in all cases, the flat types may be continuous (including several rows of tubes), or they may be round or square, with individual fins for each tube. All of these, as well as other less

common types, are in use, the selection for a particular installation being based on economic considerations, space requirements and resistances of individual designs of coils. A most important factor in the performance of extended surface coils is the bond between the fin and the tube. An intimate contact is assured in a number of ways. The assembled coil may be coated with tin, zinc, etc., after fabrication. The spiral type fin may be knurled into a shallow groove on the exterior of the tube. The tube may be expanded after the fins are assembled, or the tube hole flanges of a flat or corrugated fin may be made to override those in the preceding fin and so compress them upon the tube. There are also types of construction where the fin is formed out of the material of the tube itself.

For heating coils the materials most generally used are copper, steel and aluminum. Sometimes aluminum or brass fins are used on copper tubes. Some types of heating coils are made of cast-iron. For equal performance brass and aluminum fins must be of greater thickness than copper fins because of their lower thermal conductivities. Copper coils are frequently

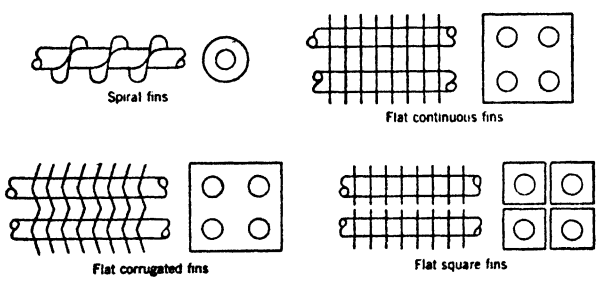


FIG. 5. TYPES OF FIN COIL ARRANGEMENT

tin-dipped and steel coils galvanized to protect them from corrosion and to assure a bond between fin and tube.

Cooling coils for water or for volatile refrigerants most frequently have copper fins and tubes, although aluminum fins on copper tubes are also used. For brines such as sodium or calcium chloride and for ammonia, steel fins and tubes are common.

Although there are many variations for special cases, tube and fin sizes and spacings for air conditioning coils, both heating and cooling, fall within fairly narrow limits. The tubes are usually $\frac{3}{8}$, $\frac{1}{2}$, $\frac{5}{8}$, or $\frac{3}{4}$ in. OD, and the fins spaced from 4 to 8 per inch, 7 per inch being a common design. The tube spacing generally varies from about $1\frac{1}{8}$ to 2 in. on centers. Small tube size and close fin spacing give large capacity with small space demand, but the resistance, both over the surface and through the tubes, is higher than with larger tubes and more widely spaced fins. Moreover, too close a fin spacing may result in trouble from dirt accumulation, especially on dehumidifying coils, and may also cause trouble from water held between the fins, particularly with air flow vertically upward. This condition increases the air resistance and decreases the capacity of the coil. Water hold-up sometimes causes flooding trouble in vertical air flow units by accumulating too much water for the drain to handle all at once when the fan is stopped.

Steam Coils

For proper performance of steam heating coils, condensate and air must be continuously eliminated and the steam must be evenly distributed to the individual tubes. This distribution is usually accomplished by individual orifices in the tubes, by distributing plates and orifices in the steam header, or by perforated internal steam-distributing pipes extending into the individual tubes. The latter arrangement has the advantage of distributing the steam throughout the length of each tube, and is conducive to uniform temperature of delivered air. The tendency of condensate to freeze at the bottom of the coil with cold entering air and light

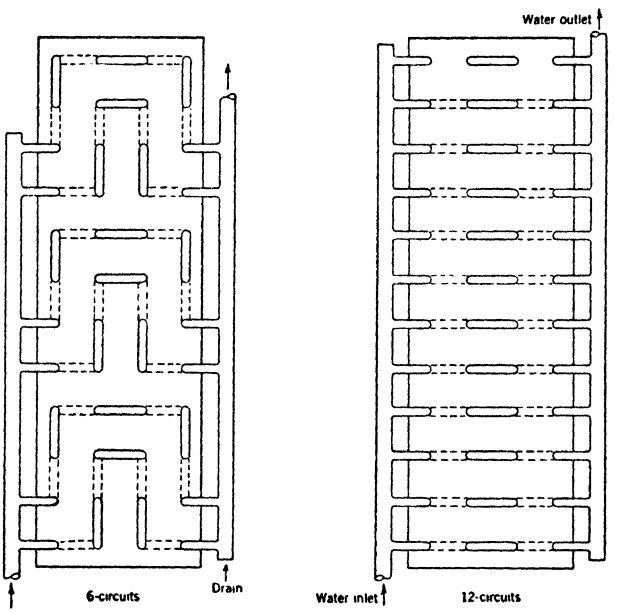


FIG. 6. VARIOUS WATER CIRCUIT ARRANGEMENTS

heating loads is also minimized. This is especially valuable for outside air preheaters. Methods of air and condensate elimination are discussed in Chapters 23 and 26.

Water Coils

The performance of water coils, for heating or cooling, depends on the elimination of air from the system and proper distribution of water. Air elimination is taken care of in the system piping as described in Chapter 24. To assure a pressure drop sufficient for adequate distribution but at the same time to provide against excessive pumping head where large water quantities are handled, water coils are provided with various water circuit arrangements. For instance, a typical coil 18 tubes high and 6 tubes deep in the direction of air flow can be arranged for 6, 9, 18 or 36 parallel water circuits as conditions may require. Orifices in individual tubes are occasionally employed but are usually unnecessary as the resistance of individual water circuits is generally sufficient to effect a satisfactory distribution. In precooling coils using well water where there may be considerable sand and other foreign matter in the water,

provision for cleaning of individual tubes is of advantage. It is important to arrange water coils for complete drainage if located where they will be exposed to freezing. Fig. 6 shows such construction. The drains may be provided in the water piping although they are often arranged in the coil headers.

Direct-Expansion Coils

Coils for volatile refrigerants present more complex problems of fluid distribution than do water, brine or steam. It is desirable that the coil be effectively and uniformly cooled throughout, and necessary that the compressor be protected from entrained, unevaporated refrigerant. There are two types; namely, flooded systems, and thermal expansion valve systems, as shown in Figs. 7 and 8. In a flooded coil, the circulation is similar to that in a water tube boiler. The liquid is maintained at the proper level by the action of a float regulator as shown in Fig. 7. The thermal expansion valve system depends upon the thermal valve auto-

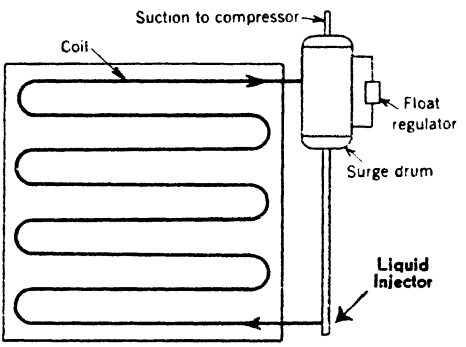


FIG. 7. DIRECT-EXPANSION COIL WITH FLOODED SYSTEM

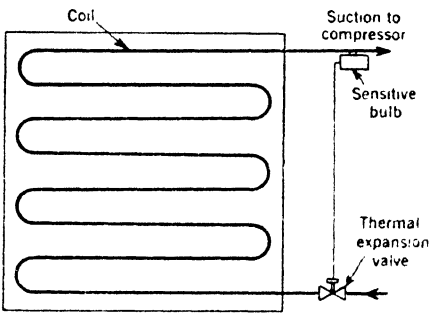


FIG. 8. DIRECT-EXPANSION COIL WITH THERMAL VALVE SYSTEM

matically feeding just as much liquid to the coils as is required to maintain the superheat at the coil suction outlet within predetermined limits which vary from about 6 to 10 deg. The thermal valve arrangement is in common use for the type of coils covered by this chapter, while the flooded system is comparatively rare.

With the flooded system the refrigerant distribution through the tubes depends on properly selecting the length of the feeds and the head of liquid imposed upon the liquid inlets. No auxiliary distributing devices are required. With the thermal valve system there are two factors to consider. There must be, generally, more than one refrigerant feed through the coil per thermal valve to keep the pressure drop through the refrigerant circuit within practical limits and to reduce the corresponding penalty in increased evaporating temperature. At the same time the coil must be so arranged that the required suction superheat can be attained with a minimum sacrifice in the performance of the coil as a whole. It is general practice to attain this superheat within the coil itself and not by the use of external heat exchangers or other auxiliary devices.

With thermal expansion valves it is advantageous to keep the pressure drop through the refrigerant feeds as low as possible. The feeds are laid out to expose each to the same mean temperature difference so that it

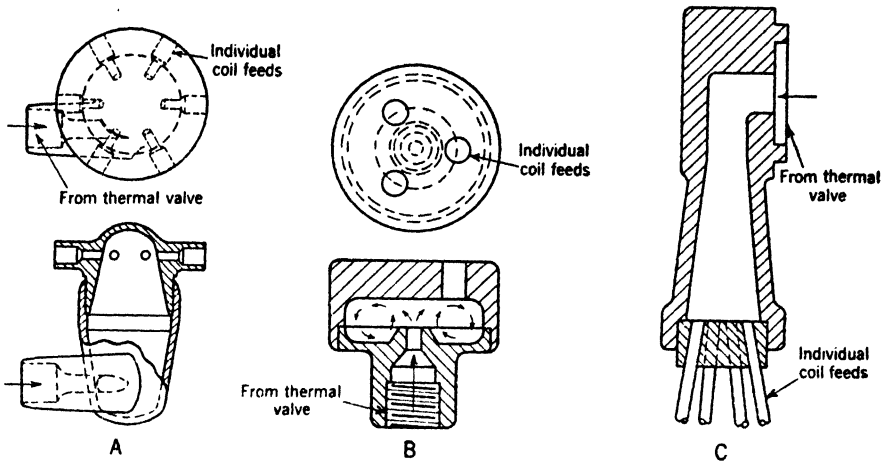


FIG. 9. TYPES OF REFRIGERANT FEED DISTRIBUTING HEADS

handles the same refrigerating load. A distributing means is imposed between valve and coil liquid inlets to divide the refrigerant equally among the feeds. Such a distributor must be effective for distributing both liquid and vapor, because the entering refrigerant is a mixture of the two. Fig. 9 shows three typical types of distributors. In distributor A the liquid and gas mixture from the thermal valve is led tangentially into a chamber. The coil feed connections extend outward radially at the top of this chamber. In distributor B the refrigerant is discharged at a high velocity through a central jet against the end plate, forming a uniform mixture of gas and liquid within the distributor, from which individual

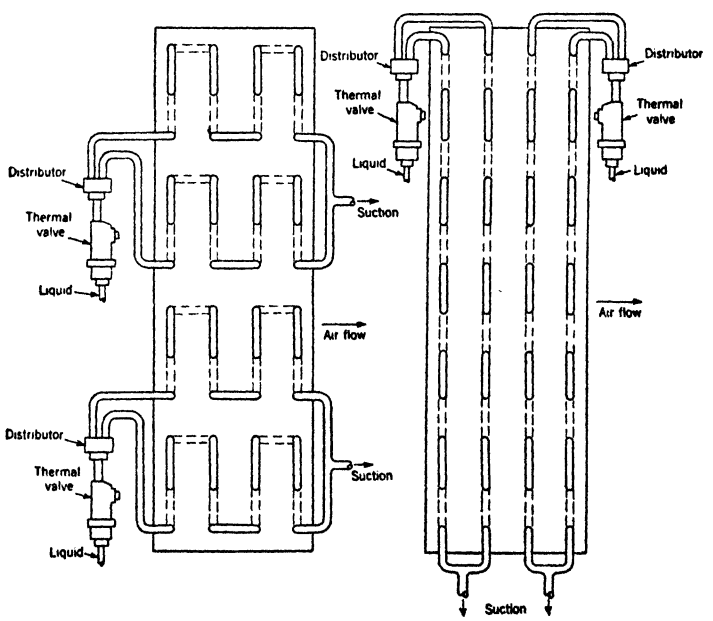


FIG. 10. ARRANGEMENT FOR FACE CONTROL

FIG. 11. ARRANGEMENT FOR DEPTH CONTROL

connections are led as shown. In type C the refrigerant enters at high velocity from the thermal valve and is discharged against the end plug in which the individual liquid feeds are closely arranged. These distributors can be used in either vertical or horizontal position. Although there are other forms of distributors those mentioned are typical examples. The individual liquid connections from the distributor to the coil inlet are commonly made of small diameter tubing and are all of the same length and diameter in order to impose the same friction between the distributor and the coil. Since the thermal valves act in response to the superheat at the coil outlet, this superheat should be produced with the least possible sacrifice of active evaporating surface. Sometimes a single thermal valve is used per coil. In other cases multiple valves are used, with the coil divided across the air flow or parallel to the air flow as shown in Fig.

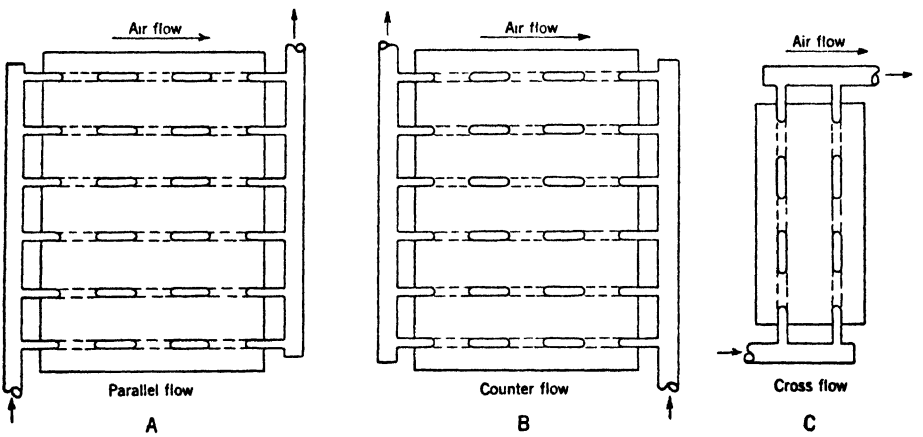


FIG. 12. FLOW OF MEDIA IN TUBES IN RELATION TO AIR FLOW

10. The arrangement of Fig. 11 should be avoided since it offers the disadvantage of unequal load on the two parallel circuits.

Flow Arrangement

The relative direction of flow of the air outside the tubes and the medium within them influence the performance of the surface. There are three types of relative flow in common use. Fig. 12A shows parallel-flow in which the air and the medium in the tubes proceed through the coil in the same direction. Fig. 12B shows counter-flow in which the medium in the tubes proceeds in a direction opposite to the flow of air. Fig. 12C shows cross-flow in which the air and the medium in the tubes pass at right angles to each other. The counter-flow arrangement is almost universally used in brine or water coils to take advantage of the highest possible mean temperature difference for given entering water and air temperatures. It is also commonly used in coils fed with volatile refrigerant to take advantage of the higher air temperature for superheating the leaving gas. In deep coils, however, it is sometimes advantageous to use parallel flow from second row to last row and then to complete the circuit by passing through the first row to take advantage of the higher air temperature for superheating. Complete evaporation and superheating of the refrigerant are essential to proper operation of the thermal expansion valve. Cross-flow is common in steam heating

coils, the temperature within the tubes being substantially uniform and the mean temperature difference the same whatever the direction of flow, relative to the air. Cross-flow is to be avoided in coils with volatile refrigerants on account of unequal loading of parallel circuits and the danger of short circuiting of liquid refrigerant which disturbs proper functioning of the thermal expansion valve.

Applications

Heating coils in field assembled banks are used for a number of purposes as described in Chapter 43. They may be arranged with the air flow vertical or horizontal, although the latter is more common. For steam heating, the coils may be set with the tubes vertical or horizontal. In the latter case the coil should be sloped to provide for condensate drainage. Because of the multi-circuit feed arrangement and the neces-

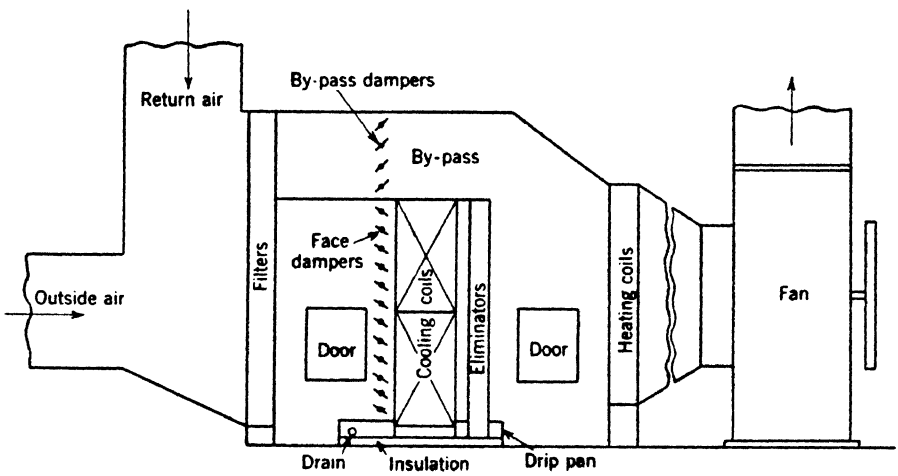


FIG. 13. TYPICAL ARRANGEMENT OF COOLING COILS IN A CENTRAL SYSTEM

sity for avoiding air and water pockets, water heating coils are generally arranged with the tubes horizontal. Certain precautions must be taken against freezing. Where steam coils are used with entering air below freezing temperature, throttling the steam supply may result in freezing the condensate in the bottom of the coil if the tubes are of the variety not provided with internal distributing pipes, or an equivalent arrangement. If these are used, there is little danger of freezing the condensate as long as the leaving air temperature is not allowed to fall below about 40 F. As an added precaution with both steam and water coils the outside air inlet dampers are often closed automatically when the fan is stopped to avoid trouble caused by very cold outside air drifting in during *off* periods.

A typical arrangement of cooling coils is shown in Fig. 13. Some means should be provided to filter all the entering air to keep dirt and foreign matter from accumulating on the coils. The assembly is provided with a drip-pan to catch the condensate during summer dehumidifying duty and to collect the non-evaporated water from the humidifying sprays in winter. The drip connection should be made ample in size and liberally provided with plugged tees and crosses for cleaning. It should not be

exposed to freezing temperatures in winter if the apparatus is used on winter humidifying duty. Access doors should be provided for servicing filters, humidifying nozzles, and fan bearings and for cleaning the coils. With certain designs of coils when used for dehumidifying, eliminators must be used beyond the coil to catch any water which may be blown into the air stream. It is customary to include these eliminators when the air velocity exceeds about 450 fpm with the individual fins and about 600 fpm for the continuous flat fin type. Where a number of coil sections are stacked one upon another, and where the velocities are low, so that eliminators need not be used, occasional trouble results when water splashes down from one coil to the next and blows out into the air stream. In such cases drip troughs as shown in Fig. 14 are used to collect this water and conduct it to the condensate pan.

Sometimes finned surface coils on summer cooling and dehumidifying

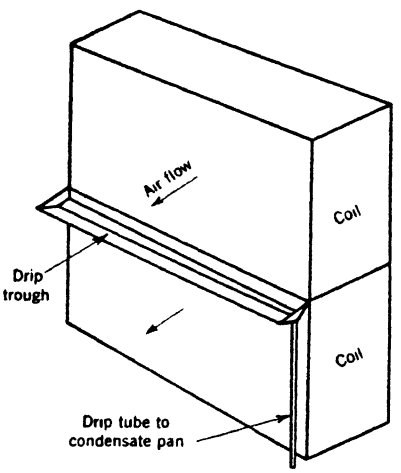


FIG. 14. COIL ARRANGED WITH DRIP TROUGH

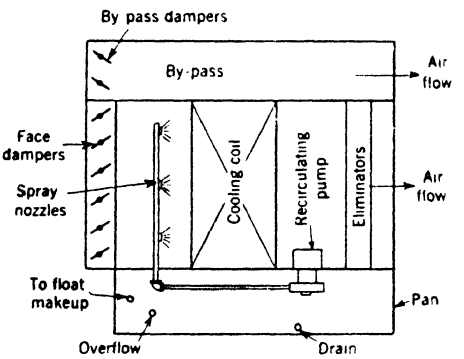


FIG. 15. RECIRCULATING SPRAY SYSTEM FOR CLEANING COILS

duty are provided with water sprays. These sprays are of two types. In the first type a set of spray nozzles is arranged for intermittent cleaning. These sprays are not operative when the system is in use and no recirculating pump is provided. The second arrangement requires a collecting tank and a recirculating pump. The water is in circulation whenever the apparatus is in operation, and assists in keeping the coil clean and in absorbing odors. Fig. 15 illustrates such an arrangement. Wherever air by-passes are used around a coil on summer duty for control purposes, it is advantageous to direct only return air through the by-pass rather than a mixture of return and outside air. The casing should be arranged accordingly. To maintain the air quantity handled by the fan reasonably constant, and to assure the required design quantity of by-passed air when the by-pass damper is open, cooling coil banks are frequently furnished with both face and by-pass dampers as shown in Fig. 13.

Although both heating and cooling coils are made of sufficient strength to take up expansion and contraction arising within themselves, care should be taken to avoid imposing strains from the piping on to the coil connections. (See Chapter 23.)

HEAT TRANSFER AND AIR FLOW RESISTANCE

The transfer of heat between the heating or cooling medium and the air stream is influenced by several variables:

1. The temperature difference.
2. The design and surface arrangement of the coil.
3. The velocity and character of the air stream.
4. The velocity and character of the medium in the tubes.

The driving force is usually taken as the logarithmic mean temperature difference for heating or cooling without dehumidification. For combined cooling and dehumidification, the logarithmic difference does not apply strictly and such problems should be handled as described in Chapter 7. With volatile refrigerants there is often an appreciable pressure drop and corresponding change in evaporating temperature through the refrigerant circuit. The problem is further complicated by the fact that the refrigerant is evaporating in part of the circuit and superheating in the remainder. In spite of this, heat transfer and ratings for coils using volatile refrigerants are usually based on a refrigerant temperature corresponding to the average pressure in the coil.

The design and surface arrangement of the coil include such items as materials, type, thickness, height and spacing of the fins, and the ratio of this surface to that of the tube, the use of the staggered or in-line tube arrangement, and provisions to increase the air turbulence such as the use of corrugated as against flat fins. Staggered tubes increase the total heat transfer as against the in-line arrangement and corrugated fins may be more effective than flat. This design and surface arrangement has a large effect on the air film heat transfer resistance.

The velocity of the air usually considered is the coil face velocity. This bears a *varied relation to the actual velocity* over the surface, depending upon the individual coil design. As long as a fixed design of coil is under consideration face velocities may be used, but they may be unsatisfactory in comparing different designs, as it is the *actual surface velocity that is significant.* The air volume is often based on standard air at 70 F and a barometric pressure of 29.92 in. Hg. The use of air volume in coil *rating* information may be misleading. *The significant value is mass velocity in pounds per (minute) (square foot of face area) and not cubic feet per minute,* because for a fixed volume the corresponding weight may vary widely, depending upon the temperature and barometric pressure.

At the same mass air velocity, varying performance can be obtained depending upon the turbulence of the air flow into the coil and upon the uniformity of distribution of air over the coil face. The latter is very important in obtaining reliable test ratings and in realizing rated performance in practical installations. The resistance through the coils will assist in distributing the air properly, but where the inlet duct connections are brought in at sharp angles to the coil face, the effect is frequently bad and there may even be reverse air currents through the coils. This reduces the capacity, but can be avoided by proper layout or by the use of directing baffles.

Heat transfer depends also upon the velocity of the medium in the tubes and upon its character, whether flowing water, condensing steam or evaporating volatile refrigerant. Heat transfer rates expressed as Btu per (square foot of internal surface) (degree logarithmic mean effective temperature difference between the fluid and tube wall) are, for example:

about 150 to 300 for evaporating dichlorodifluoromethane, about 350 to 1200 for water at 2 and 6 fps and about 1200 for condensing steam. The influence of the medium in the tubes on the over-all heat transfer rate is, therefore, apparent.

Because of these variables, reliable rating and performance information for any design of coil must be based on actual tests on that coil under the expected conditions of operation. A comparison between the performance of two designs, unless based on such tests on each, may lead to entirely erroneous conclusions. For details on coil calculation and performance see Chapter 7.

COIL SELECTION

In the selection of a coil it is necessary to consider several factors:

1. The duty required—heating, cooling, dehumidifying.
2. Temperature of entering air—dry-bulb only if there is no dehumidification, dry- and wet-bulb if moisture is to be removed.
3. Available heating and cooling media.
4. Space and dimensional limitations.
5. Air quantity limitations.
6. Allowable resistances in air circuit and through tubes.
7. Peculiarities of individul designs of coils.
8. Individual installation requirements, such, for example, as type of automatic control to be used.

The duties required may be determined from information in Chapters 6, 8, 14 and 15. There may or may not be a choice of cooling and heating media, as well as temperatures available, depending upon whether the installation is new or is in combination with present sources of heating or cooling. Space limitations are dictated by the requirements of individual cases. The air quantity is influenced by a number of considerations. The air quantity through heating coils is often made the same as that necessary to handle the summer cooling load. The air handled may be fixed by the use of old ventilating ducts as an air distribution system for new air conditioning apparatus, or may be dictated by requirements of satisfactory air distribution or ventilation. The resistance through the air circuit influences the fan horsepower and speed. This resistance may be limited to allow the use of a given size of fan motor, or to keep the operating expense low, or it may be limited by the maximum fan peripheral velocity which requirements of quietness may permit. The friction through the water or brine circuit may be dictated by the head available from a given size of pump and pump motor. As the fan and pump motor inputs represent a refrigerating load on cooling installations, it is economical to keep them low.

Proper performance of a surface heating or cooling coil depends upon correct choice of the original equipment and upon certain other factors. The usual coil ratings are based on a uniform face velocity of air. If the air is brought in at odd angles or if the fan is located so as to block part of the air flow, the performance as given in the manufacturer's ratings cannot usually be obtained. To obtain this performance it is necessary also that the air quantity be adjusted on the job to that used in determining the coil selection, and must also be kept at this value. The most common causes for a reduction of air quantity are the fouling of the filters and collection of dirt in the coils. These difficulties can be avoided by

proper design and proper servicing. There are a number of ways in which coils may be cleaned. A common method is to wash them off with water. They can sometimes be brushed and cleaned with a vacuum cleaner. In bad cases of neglect, especially on restaurant jobs where grease and dirt have accumulated, it is sometimes necessary to remove the coils and wash off the accumulation with steam, compressed air and water, or hot water. The most satisfactory solution, however, is to keep the filters serviced, and thus make the cleaning of the coils unnecessary.

The proper selection of coils requires an understanding of the necessities of each case and should be based on an economic analysis of the plant design as a whole. No general rule can, therefore, be laid down for the selection of heating or cooling coils. It is possible, however, to point out the limits of usual practice and to indicate the influence of the variables involved in the coil selection.

Heating Coils

Steam and *hot water heating coils* are usually *rated* within these limits:

Air Face Velocity—200 to 1200 fpm, sometimes up to 1500 fpm.
Steam Pressure—2 to 200 lb, sometimes up to 350 lb per square inch.
Hot Water Temperature—150 to 225 F.
Water Velocity—2 to 6 fps.

Individual cases may deviate widely, but the tabulation given herewith will serve as a guide to usual *heating installation practice:*

Air Face Velocity—500 to 800 fpm face, 500 being a common figure.
Delivered Air Temperature—varies from about 72 F for ventilation only to about 150 F for complete heating.
Steam Pressure—2 to 10 lb, 5 lb being common.
Hot Water Temperature—150 to 225 F.
Water Velocity—2 to 6 fps.
Water Quantity—Based on about 20 F temperature drop through a hot-water coil.
Air Resistance—The total resistance through heating coils is usually limited to from $\frac{3}{8}$ to $\frac{5}{8}$ in. of water gage for public buildings, to about 1 in. for factories.

The selection of heating coils is relatively simple as it involves dry-bulb temperatures and sensible heat only, without the complication of simultaneous latent heat loads, as in cooling coils. For a given duty, entering air temperature, and steam pressure, it is possible to select several arrangements of the same design of coil depending upon the relative importance of space, cross-sectional area, and air resistance.

Cooling Coils

Cooling and *dehumidifying coils* are usually *rated* within these limits:

Entering Air Dry-Bulb—60 to 100 F.
Entering Air Wet-Bulb—50 to 80 F.
Air Face Velocities—300 to 800 fpm, (sometimes as low as 200 and as high as 1200).
Volatile Refrigerant Temperatures—25 to 55 F, at coil suction outlet.
Water Temperatures—40 to 65 F.
Water Quantities—2 to 6 gpm per ton, or equivalent to a water temperature rise of from 4 to 12 deg.
Water Velocity—2 to 6 fps.

The ratio of total to sensible heat removed varies in practice from 1.00 to about 1.65, *i.e.*, sensible heat is from 60 to 100 per cent of total,

depending on the application. (See Chapter 43.) Since required ratios may demand wide variations in air velocities, refrigerant temperatures, and coil depth, general rules as to their values may be misleading. On usual comfort installations air face velocities between 400 and 600 fpm are frequent, 500 being a common value. Refrigerant temperatures ordinarily vary between 40 and 50 F where cooling is accompanied by dehumidification. Water velocities range from 2 to about 6 fps.

When no dehumidification is desired, for which condition the dew-point of the entering air is equal to or lower than the cooling coil surface temperature, the coil selection is made on the basis of dry-bulb temperatures and sensible heat transfer only, the same as with heating coils. It is possible also to choose various arrangements of face area, depth, air velocity, etc., for the same duty.

Dehumidifying Coils

The selection of coils for combined cooling and dehumidifying duty is more involved than for heating or sensible cooling and requires consideration of both dry- and wet-bulb air temperatures. (See Chapter 7.) It is further complicated by the fact that the proportional amount of dehumidification required is also highly variable. The methods outlined previously under Heat Transfer and Resistance may be used to determine whether it is possible for a coil to perform the duty required. If entering and leaving air conditions are arbitrarily specified, the corresponding duty sometimes cannot be obtained at all without the use of reheat. As with heating and sensible cooling coils, there are combinations of face areas, depth, air velocity and refrigerant temperatures which will give the required performance. This is illustrated in Table 4.

TABLE 4. VARIOUS COOLING COIL ARRANGEMENTS

SELECTION	1	2	3	4
Total cooling capacity, tons	100	100	100	100
Sensible cooling capacity, tons	69	69	69	69
Latent cooling capacity, tons	31	31	31	31
Ratio total to sensible heat	1.45	1.45	1.45	1.45
Air quantity, cfm	47,800	41,700	37,100	46,800
Cfm per total ton	478	417	371	468
Face velocity, fpm	325	423	500	600
Resistance, in. water	0.11	0.27	0.51	0.37
Coil face area, sq ft	147	99.0	74.2	78.1
Coil rows deep	4	6	8	4
Coil evaporator temp. F deg	45	45	45	38

It is possible as shown in Table 4 to perform approximately the same duty at a given refrigerant temperature with small face area and large thickness or vice versa. The large face area coil gives low air velocity and resistance but high air quantities per ton. The coil of small face area and great depth requires small air quantities per ton of refrigeration, high resistance and high air velocities. As shown also in Table 4 the same sensible, latent and total cooling capacity may be obtained with various refrigerant temperatures by proper choice of coil. This makes it possible to keep the evaporating temperature high enough to carry the load with a chosen size of condensing unit. High evaporating temperatures with correspondingly small compressor operating expense can be attained but

at the expense of coil surface, air quantity or both. The choice will be determined by the necessities of individual installations.

For a given quantity and condition of entering air the evaporating temperature of a volatile refrigerant coil is determined by a balance between the condensing unit and the coil. The total, sensible and latent cooling capacity can then be determined from the coil rating information. If the condensing unit and cooling coil have been properly balanced for the required load and, due to miscalculated duct resistance or improper choice of fan speed, the air quantity is reduced, the total cooling capacity will also be reduced. The decrease is generally in the sensible capacity. This is the effect also when the air by-pass or volume control is used.

It is necessary that not only the total capacity but also the sensible and latent cooling requirements both be met. The installation of an excess of coil results in an increase in total capacity, but not a proportional gain in latent heat capacity. On installations controlled from dry-bulb tem-

TABLE 5. CAPACITY BALANCES FOR MAXIMUM AND MINIMUM LOAD CONDITIONS

CONDITIONS	CAPACITY IN TONS			RATIO $\frac{\text{TOTAL}}{\text{SENSIBLE}}$
	Total	Sensible	Latent	
Required at peak load conditions	10.90	7.90	3.00	1.38
Required at minimum load conditions	6.62	3.36	3.26	1.98
Peak load equipment balance	10.90	7.90	3.00	1.38
Same equipment balanced at minimum load conditions	9.85	6.58	3.26	1.50
Same equipment balanced at maximum load conditions with 40 per cent by-pass	8.38	5.05	3.33	1.66
Same equipment balanced at minimum load conditions with 38,800 Btu per hour reheat	6.62	3.36	3.26	1.98

perature the operating time is shortened because of the added sensible cooling capacity. This results in less moisture pick-up and higher relative humidity than calculated. If an oversize condensing unit is installed, the opposite situation occurs. Generally, this is not a disadvantage except that it results in a load from outside air greater than calculated, as well as in increased power consumption. If oversize equipment is furnished, a balance should be made to assure that the ratio of total to sensible capacity is the same as in the estimated load.

Sometimes arbitrary air quantities are specified for ventilation or other reasons independent of the selection of the cooilng coil. As shown in Table 4, the coil selection can be altered to take care of various air quantities for the same duty.

Where coil and condensing unit are selected for the peak load condition, and the sensible load partially disappears due to fall of outside temperature or other cause, the condensing unit and coil rebalance. This may result in more sensible and less latent capacity than required at the light load condition, with an increased relative humidity in the conditioned space. Such a condition is shown in Table 5. If approximately 40 per cent of the total air is by-passed, the condition is improved as indicated. The situation may be entirely avoided by using reheat, where it is possible to handle any ratio of sensible and latent loads and maintain the design temperature and humidity [18].

Care should be taken to avoid freezing at light loads. In general, freezing occurs when the coil surface temperature falls to 32 F. With

usual coils for comfort installations, this does not occur unless the evaporating temperature at the coil outlet is about 20 to 25 F. The exact value depends on the design of the coil and the amount of loading. Although it is not customary to choose coil and condensing units to balance at low temperatures at peak loads, there is danger of this occurring when the load decreases. This is further aggravated if a by-pass is used so that less air is passed through the coil at light loads. It may be even worse if the control is arranged for decrease of inside temperature with fall of that outside. Freezing can be avoided by making the full load balance a high evaporating temperature and checking the balance at the minimum load.

Care should be exercised in the design of humidity control to minimize the cycling of the refrigerating compressor because of re-evaporation of moisture from the fins. It is sometimes necessary to by-pass air around a coil when the compressor is not operating.

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Chapter 26

UNIT HEATERS, UNIT VENTILATORS, UNIT HUMIDIFIERS

Definitions; Unit Heaters: Classification, Application, Outlet Velocities, Ratings for Various Types, Temperature, Automatic Control, Location, Piping Connections; Boiler Capacity for Steam Unit Heaters; Unit Ventilators: Ratings, Applications, Location, Exhaust Vents; Window Ventilators; Unit Humidifiers

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DESCRIPTIONS of heating, cooling, ventilating, humidifying, and dehumidifying systems are given in other chapters. This chapter deals with unit heaters, unit ventilators, and unit humidifiers. Cooling units, unit air conditioners, and attic fans are described in Chapter 36.

Definitions

The generally accepted meaning of the word *unit* in the terms unit heaters, unit ventilators, and unit humidifiers is that of a factory made, encased assembly of the functional elements indicated by its name. Such units can be shipped complete or in sections so that the only field work necessary is the assembling of the sections, providing proper supports and connecting the unit to sources of heat (or fuel), power and water supply, and, if necessary, to vent pipes for combustion gases.

The term *unit heater* denotes an assembly of elements whose principal function is heating. The essential elements of a unit heater are a fan and motor, a heater, a housing, and outlet vanes or diffusers.

The term *unit ventilator* denotes an assembly whose principal function is to ventilate. It may serve to circulate air within the space, or to introduce air from without the space, or may accomplish both purposes. The essential elements of a unit ventilator are a fan and motor, a heater, a set of dampers, a housing and outlet vanes or diffusers.

The term *unit humidifier* denotes an assembly of elements whose principal function is to humidify. The essential element of a unit humidifier is an atomizer or evaporator. To this may be added a fan, a heater, outlet vanes or diffusers, and a housing to enclose the various parts.

UNIT HEATERS

Classification

The various types of unit heaters which are at present available can usually be classified according to one of the three following methods:

1. *By type of heater.* Under this classification there are three types of heating elements to be considered: (*a*) *the steam or hot water type*, (*b*) *the electric type*, and (*c*) *the direct fired type* which may be *gas*, *oil*, or *coal fired*.

2. *By type of fan.* Under this classification there are two types of fans to be considered: (*a*) the *propeller type*[1] which may be equipped with a horizontal or vertical shaft, and (*b*) the *centrifugal type* which may be designed for *horizontal* or *vertical blow*.

3. *By arrangement of elements.* Under this classification there are two types of heaters to be considered: (*a*) the *draw-through type*, in which the

fan draws air through, and (*b*) the *blow-through type*, in which the fan blows air through the heater.

Unit heaters are available in any combination of the three preceding general classifications. For example, the steam or hot water type may be secured with either the propeller or centrifugal type of fans, and in either the draw-through or blow-through type.

Unit heaters also vary in other minor respects. For example, steam and return inlets and outlets may be located on the top and bottom respectively or on the same side of the unit. Some units are supported by the piping and some have independent supports. The heating surface of steam or water type units is generally made up of a non-ferrous tube-and-fin assembly; or it may be fabricated of steel, or cast in steel.

Application of Unit Heaters

Unit heaters are used principally for heating commercial and industrial structures such as garages, factories, laboratories, and stores. They may also be used for heating finished rooms, if properly applied and concealed and if some consideration is given to the problem of noise.

Unit heaters may also be adapted to a number of industrial processes, such as drying and curing, in which the use of heated air in rapid circulation with uniform distribution is of particular advantage. They may be used for moisture absorption, such as fog removal in dye houses, or for the prevention of condensation on ceilings or other cold surfaces of buildings in which process moisture is released. When such conditions are severe, it is necessary that the unit heaters draw air from outside in enough volume to provide a rapid air change and that they operate in conjunction with ventilators or fans for exhausting the moisture-laden air. See discussion of condensation in Chapter 6.

There are three major factors to consider in the application of unit heaters, namely: (1) location of unit, (2) air distribution, and (3) heating medium.

There are a variety of applications which are favorable to the use of *electric unit heaters*. For supplemental heat in residence bath rooms, for the heating of ticket booths, watchmen's offices, factory offices, locker rooms and other isolated rooms scattered over large areas, their use is peculiarly adaptable. They are particularly useful in isolated and untended pumping stations or pits where they may be thermostatically controlled to prevent freezing temperatures.

Gas fired unit heaters find application in industrial plants, offices, stores, garages, in fact in almost every location where steam type units are used. The installation cost of gas fired units is usually less than that of a type requiring that a new boiler be installed.

Oil fired unit heaters are used in industrial plants, garages and commercial buildings.

Coal fired unit heaters are of finned, welded steel, or cast-iron construction and equipped with centrifugal blowers. They are usually stoker-fired to insure proper firing of fuel. They are used principally in large industrial plants such as foundries or assembly plants, and provide a very economical source of heat, both from the installation and the operating standpoint.

Outlet Velocities

Outlet velocities of unit heaters vary from about 400 to 2500 fpm depending upon the type of unit and the distance to which the air is to be

projected. Noise and drafts must be considered in the choice of air velocities, since both increase with increase of air velocity.

Velocities and decibel ratings for the various types of unit heaters illustrated in Figs. 1, 2, 3 and 4 are given in Table 1. (See Chapter 42 for a discussion of decibel ratings).

In the selection of unit heaters it is important to ascertain that the throw is sufficient. The throw is dependent to a marked degree on the temperature of air leaving the heater as well as upon its velocity. See discussion under heading of Inlet, Outlet, and Space Temperatures with Unit Heaters.

Air Outlets

In order to direct the air to points desired and to diffuse the air to avoid

TABLE 1. OUTLET VELOCITIES, DISTANCE OF BLOW AND DECIBEL RATINGS FOR VARIOUS TYPES OF UNIT HEATERS

TYPE OF UNIT HEATER	OUTLET VELOCITIES FPM	DISTANCES OF BLOW—FT[a]	DECIBEL RATING
Centrifugal Fan	1500–2500	20–200	34–90
Horizontal Propeller Fan	400–1000	30–100	26–84
Vertical Propeller Fan	1200–2200	70	50–82

[a]Refer to manufacturers' tables for limits of blow and decibel ratings. Values in this table are maxima and do not apply to all makes of units.

drafts, unit heaters are commonly equipped with directional outlets, adjustable louvers or fixed types of diffusers.

RATINGS OF UNIT HEATERS

It is standard practice to rate unit heaters on the basis of the amount of heat delivered by the air in Btu per hour above an entering air temperature of 60 F. This applies to all types of unit heaters, the steam or hot water type, the electric type and the direct fired type. There are, however, other factors which must be taken into account, especially when an attempt is made to compare one type of heater with another. These are the temperature of the heating element and the velocity of air through it. Consideration is given to these factors in the discussion of ratings for each type of unit heater in the following paragraphs.

Ratings for Steam Type

The rating of steam type unit heaters has been standardized by a code[2] in which the following items are the basis of rating: dry saturated steam at 2 psig pressure (29.92 in. Hg barometric pressure) at the heater coil; air at 60 F entering the heater; and heater operating free of external resistance to air flow.

The capacity of a heater increases as the steam pressure increases, and decreases as the entering air temperature increases. The heating capacity for any condition of steam pressure and entering air temperature other than standard may be calculated approximately from any given rating by the use of factors in Table 2 for the blow-through or draw-through types of units.

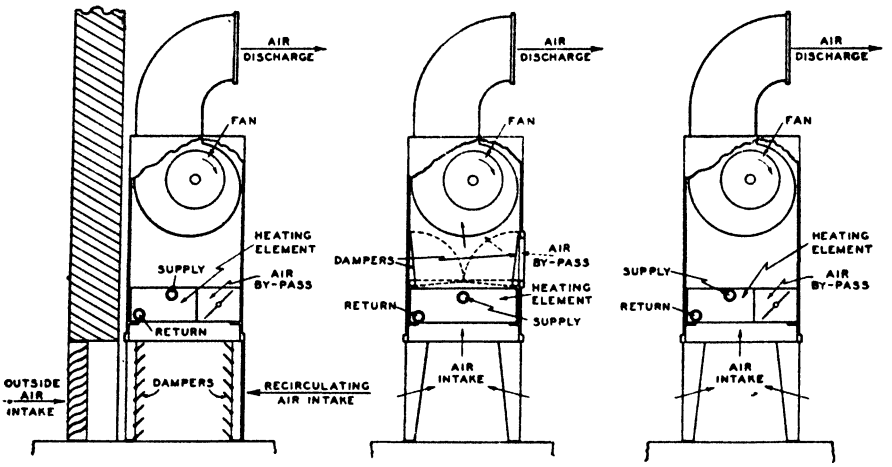


FIG. 1. CENTRIFUGAL FAN TYPE UNIT HEATER—FLOOR MOUNTED

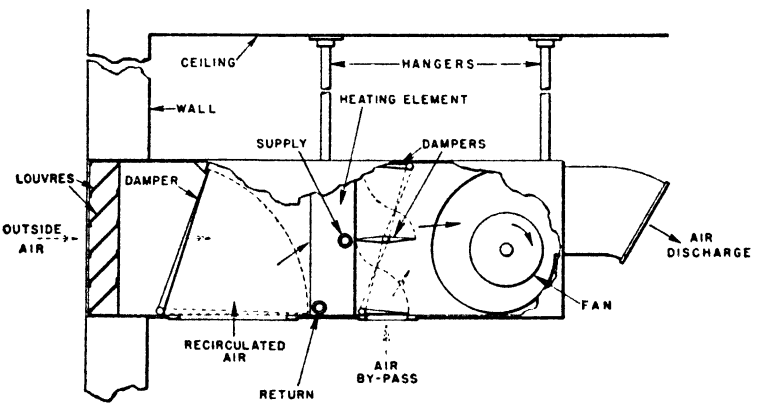


FIG. 2. CENTRIFUGAL FAN TYPE UNIT HEATER—SUSPENDED

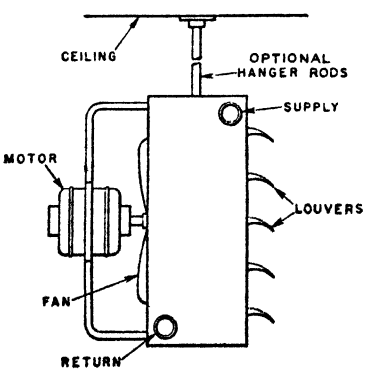


FIG. 3. PROPELLER FAN TYPE UNIT HEATER—HORIZONTAL BLOW

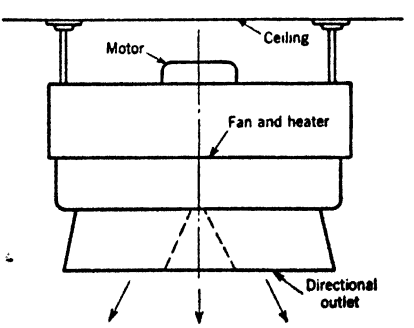


FIG. 4. PROPELLER FAN TYPE UNIT HEATER—VERTICAL BLOW

TABLE 2. CONSTANTS FOR DETERMINING THE CAPACITY OF UNIT HEATERS FOR VARIOUS STEAM PRESSURES AND TEMPERATURES OF ENTERING AIR

(Based on Steam Pressure of 2 psig and Entering Air Temperature of 60 F)

	Steam Pressure psi	Temperature of Entering Air											
		− 10°	0°	10°	20°	30°	40°	50°	60°	70°	80°	90°	100°
Blow Through Type	0	1.51	1.45	1.37	1.27	1.19	1.11	1.03	0.96	0.88	0.81	0.74	0.67
	2	1.59	1.50	1.41	1.32	1.24	1.16	1.08	1.00	0.93	0.85	0.78	0.71
	5	1.64	1.55	1.46	1.37	1.29	1.21	1.13	1.05	0.97	0.90	0.83	0.76
	10	1.73	1.64	1.55	1.46	1.38	1.29	1.21	1.13	1.06	0.98	0.91	0.84
	15	1.80	1.71	1.61	1.53	1.44	1.34	1.28	1.19	1.12	1.04	0.97	0.90
	20	1.86	1.77	1.68	1.58	1.50	1.42	1.33	1.25	1.17	1.10	1.02	0.95
	30	1.97	1.87	1.78	1.68	1.60	1.51	1.43	1.35	1.27	1.19	1.12	1.04
	40	2.06	1.96	1.86	1.77	1.68	1.60	1.51	1.43	1.35	1.27	1.19	1.12
	50	2.13	2.04	1.94	1.85	1.76	1.67	1.58	1.50	1.42	1.34	1.26	1.19
	60	2.20	2.09	2.00	1.90	1.81	1.73	1.64	1.56	1.47	1.39	1.31	1.24
	70	2.26	2.16	2.06	1.96	1.87	1.78	1.70	1.61	1.53	1.45	1.37	1.29
	75	2.28	2.18	2.09	1.99	1.90	1.81	1.72	1.64	1.55	1.47	1.40	1.32
	80	2.31	2.21	2.11	2.02	1.93	1.84	1.75	1.66	1.58	1.50	1.42	1.34
	90	2.36	2.26	2.16	2.06	1.97	1.88	1.79	1.71	1.62	1.54	1.46	1.38
	100	2.41	2.31	2.20	2.11	2.02	1.93	1.84	1.75	1.66	1.58	1.50	1.42
Draw Through Type	0	1.48	1.41	1.33	1.25	1.18	1.11	1.03	0.96	0.89	0.82	0.75	0.69
	2	1.52	1.44	1.36	1.29	1.22	1.14	1.07	1.00	0.93	0.86	0.79	0.73
	5	1.57	1.49	1.41	1.33	1.26	1.19	1.11	1.05	0.98	0.91	0.84	0.77
	10	1.64	1.56	1.48	1.40	1.33	1.25	1.18	1.11	1.04	0.97	0.90	0.84
	15	1.69	1.61	1.53	1.46	1.38	1.31	1.24	1.17	1.10	1.03	0.96	0.90
	20	1.73	1.65	1.57	1.50	1.42	1.35	1.28	1.21	1.14	1.07	1.00	0.94
	30	1.80	1.73	1.65	1.57	1.50	1.42	1.35	1.28	1.21	1.15	1.08	1.01
	40	1.86	1.79	1.71	1.64	1.56	1.49	1.42	1.35	1.28	1.22	1.15	1.08
	50	1.93	1.85	1.77	1.70	1.63	1.55	1.48	1.42	1.35	1.28	1.21	1.15
	60	1.97	1.90	1.82	1.75	1.67	1.60	1.53	1.46	1.40	1.33	1.26	1.19
	70	2.02	1.94	1.87	1.80	1.72	1.65	1.58	1.51	1.44	1.38	1.31	1.24
	75	2.04	1.97	1.90	1.82	1.75	1.68	1.61	1.54	1.47	1.40	1.33	1.27
	80	2.06	1.99	1.91	1.84	1.77	1.70	1.63	1.56	1.49	1.42	1.35	1.29
	90	2.10	2.03	1.95	1.88	1.80	1.73	1.66	1.59	1.52	1.46	1.39	1.32
	100	2.15	2.07	1.99	1.92	1.85	1.77	1.70	1.63	1.56	1.49	1.43	1.36

Note: To determine capacity at any steam pressure and entering temperature, multiply constant from table by rated capacity at 60 F entering air and 2 psi.

When increasing steam pressure it is important to determine whether the heater is suitable for the increased pressure application and whether the resulting increased outlet temperature is satisfactory.

Ratings for Hot Water Type

A standard for the rating of hot water type unit heaters has also been established by code [8] in which the following items are the basis of rating: entering water at 200 F; entering air at 60 F (29.92 in. Hg barometric pressure); and heater operating free of external resistance to air flow. This code also prescribes a method of translating the output in Btu and the temperature rise as obtained under test conditions to standard conditions of air and water temperature.

Ratings for Electric Type

Electric type unit heaters are available in sizes up to at least 60 kw capacity. They consist of resistance type heating elements combined with fan and motor, together with a suitable casing. Electric unit heaters are made in the built-in-wall model, suspension model, and free-standing or portable model.

Electric unit heaters are rated on the energy input to the heater, expressed in terms of kilowatts, Btu or EDR. Quite often all three ratings are given in parallel columns in the catalogs.

Ratings for Gas Fired Type

Gas fired unit heaters are built in both suspended and floor models with either propeller or centrifugal type fans. They are available in a wide range of sizes from about 24,000 to over 4,000,000 Btu per hr capacity and are usually rated in terms of both input and output according to the approval requirements of the *American Standards Association*. Any gas fired unit which is thermostatically controlled and has a pilot must have an element in the pilot flame which will automatically close the gas valve on pilot failure.

Ratings for Oil Fired Type

The oil fired type of unit heater is usually equipped with the centrifugal type of fan only and can be obtained in sizes ranging from 125,000 to 1,650,000 Btu per hour output capacity in standard units. It is furnished in either the floor mounted or in smaller sizes in the suspended type.

Ratings for Coal Fired Type

The stoker fired type of unit heater can be obtained in ranges of from 300,000 to 6,000,000 (or more) Btu per hour output capacity. Ratings are based upon the delivered output at the heater outlet.

Effect of Resistance Upon Capacity

Unit heaters are customarily rated as free delivery type units. If outside air intakes, air filters, or ducts on the discharge side are used with the unit, a reduction in air and heating capacity will result because of this added resistance. The percentage of this reduction in capacity will depend upon the characteristics of the heater and on the type, design and speed of the fans, so that no specific percentage reduction can be assigned for all heaters at a given added resistance. In general, however, propeller fan type units will experience a larger reduction in capacity than housed centrifugal fan units for a given added resistance and a given heater will have a larger reduction in capacity as the fan speed is lowered. The heat output to be expected under other than free delivery conditions should be secured from the manufacturer.

Inlet, Outlet and Space Temperatures with Unit Heaters

In the selection of unit heaters for any particular design, consideration should be given to the temperature of air entering the heaters as well as the temperature to be maintained in the working zone of the space. In general, the temperature differences per foot of elevation, when using unit heaters, are less than corresponding variations when using direct radiation[4]. High velocity units will maintain slightly lower temperature differences than low discharge velocity units. Correspondingly, units with lower discharge air temperature will maintain lower temperature differences than units with higher discharge temperatures. Directional control of the discharged air from a unit heater can be an important factor, added to qualities of reasonably good outlet velocity and outlet temperature, in effecting satisfactory distribution of heat and restraining floor-to-ceiling temperature difference.

When some *outside air* is introduced, the temperature of the mixture of outside and recirculating air must be calculated and used as the entering air temperature at the heater. Unit heaters connected in this manner perform the function of unit ventilators. For a discussion of this function see the section of this chapter entitled *Unit Ventilators.*

For recirculating heaters located *at the floor* or with *intakes at the floor,* the temperature of air entering the heater should be assumed to be the same as that to be maintained in the room itself.

Automatic Control of Unit Heaters

Thermostatic control of unit heaters may be accomplished either by starting and stopping the fan or by controlling the flow of the heating medium to the heating element. If the fan is controlled, it is advisable to provide a temperature-operated switch to prevent the fan from starting until the heating element is heated throughout.

Unit heaters may be used in summer as a means of circulating air to give some measure of comfort due to air motion. In such cases the heating element should be shut off from the source of heat. The thermostat which prevents the fan from starting until the heating element is heated, should be provided with a by-pass switch, which, upon being closed, will permit the fan to be operated independently of the heating element.

Location of Unit Heaters

Care should be taken in the location of unit heaters to insure free air circulation to the intake. The best arrangement is to locate units so that they discharge air nearly parallel to exterior walls, and in a direction which will produce a rotational circulation around the room. This is preferable to directing the discharge against the outside walls.

Various types and makes of unit heaters are illustrated in the *Catalog Data Section* of this edition. As hot blasts of air in working zones are usually objectionable, heaters mounted on the floor should have their discharge outlets above the head line, and suspended heaters should be placed in such manner and turned in such direction that the heated air stream will not be objectionable in the working zone. In the interest of economy, however, the elevation of the heater outlet and the direction of discharge should be so arranged that the heated air shall be brought as close above the head line as possible, yet not into the working zone.

In connection with the use of vertical type unit heaters, care must be exercised in the selection of the heater. It has been found that the higher the unit is placed above the floor, the lower must be the outlet temperature of the air leaving the heater in order that the heated air may be forced into the occupied zone.

Determining Unit Heater Requirements

The formulas given in the section on Unit Ventilators may be used to determine unit heater capacity requirements.

PIPING CONNECTIONS FOR STEAM UNIT HEATERS

Piping connections for steam unit heaters are similar to those for other types of fan blast heaters. The piping of unit heaters must conform

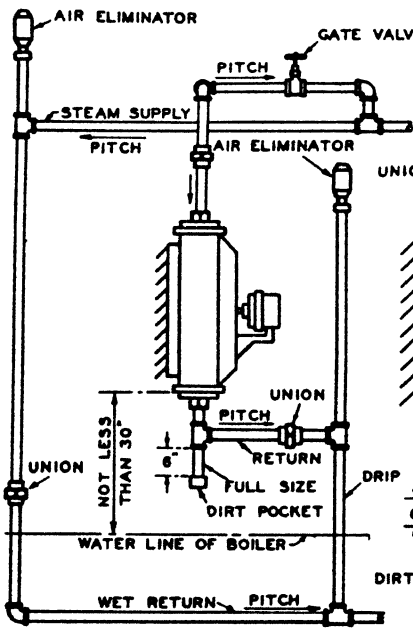


FIG. 5. UNIT HEATER CONNECTION TO ONE-PIPE GRAVITY STEAM SYSTEM

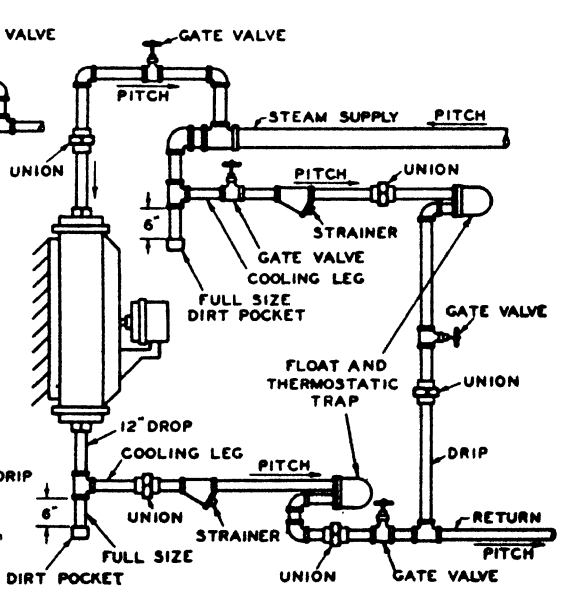


FIG. 6. UNIT HEATER CONNECTION FOR VACUUM OR VAPOR SYSTEM DISCHARGING CONDENSATION INTO DRY RETURN

strictly to the system requirements while at the same time permitting the heaters themselves to function as intended. The basic piping principles for steam systems are discussed in Chapter 23.

Rapid condensation of steam, especially during heating-up periods, is characteristic of this type of equipment. The return piping must be planned to keep the heating coil free of rapid condensation, while the steam piping must be ample to carry a full supply of steam to the unit to take the place of that condensed. Adequate sizes of piping are especially essential where a unit heater fan is operated under start-and-stop control and where all or part of the air is taken from the outside. In such installations the condensation rate may vary rapidly and the necessity for ample pipe capacity is particularly important.

A method of connecting a unit heater to a one-pipe gravity system is illustrated in Fig. 5. In cases where the return main is located above the

boiler water line, an artificial water line must be created by providing an equalizing loop to prevent steam passing into the return and thus into other units.

A piping arrangement where both the air and condensate pass through a common return to a boiler, with vent trap or condensate pump and receiver, is shown in Fig. 6. The traps must pass air and condensate rapidly to keep the return piping partially full of water.

Since unit heaters are often constructed with sufficient strength, the use of high pressure steam in them is a common practice. As shown in Fig. 7 the condensate and air reach the return overhead through traps, and check valves are located in the return piping. It is, however, preferable to locate the high pressure return below the heater.

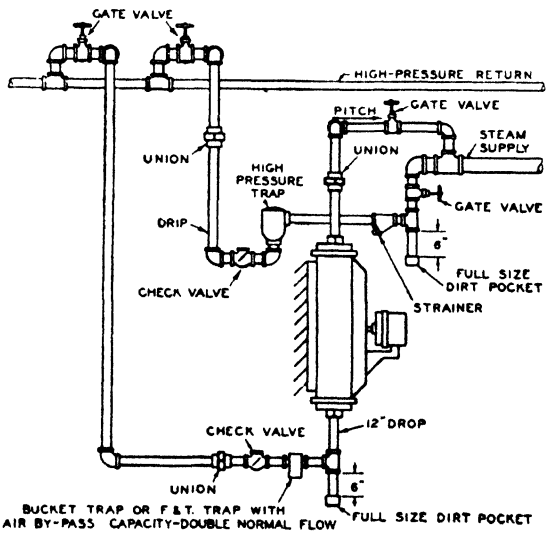


FIG. 7. METHOD OF CONNECTING UNIT HEATER TO HIGH PRESSURE SYSTEM

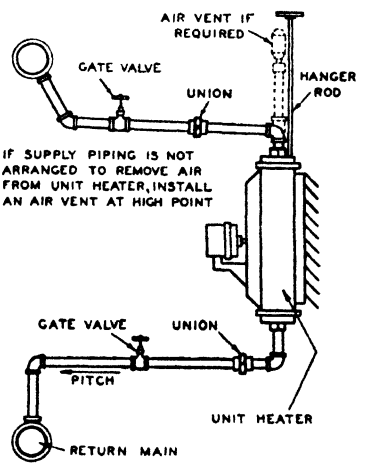


FIG. 8. METHOD OF CONNECTING UNIT HEATER TO HOT WATER SYSTEM

For two-pipe closed gravity return systems, the return from each unit should be fitted with a heavy duty or blast trap, and an automatic air valve should be connected into the return header of each unit heater. Provisions must be made to compensate for the pressure drop by elevating the unit heater above the water line of the boiler or of the receiver.

In pump and receiver systems the air may be eliminated by individual air valves on the heaters, or it may be carried into the returns as in vacuum systems and the entire return system be free-vented to the atmosphere, provided all units, drip points, and radiation are properly trapped to prevent steam entering the returns.

On vacuum or open vent systems the return from each unit should be fitted with a large capacity trap to discharge the water of condensation and with a thermostatic air valve for eliminating the air, or with a heavy-duty trap for handling both the condensation and the air, provided the air finally can be eliminated at some other point in the return system.

For high pressure systems the same kind of traps may be used as with vacuum systems, except that they must be constructed for the pressure

used. If the air is to be eliminated at the return header of the unit, a high pressure air valve can be used; otherwise the air may be passed with the condensate through the high-pressure return trap, and then eliminated at some other point in the system.

Fig. 8 represents the connections to a hot water heating system. The air vent is not required if the main is above the heater and air can be eliminated through the piping system.

BOILER CAPACITY FOR STEAM UNIT HEATERS

The capacity of the boiler should be based on the rated capacity of the unit heaters at the lowest entering air temperature and highest fan speed that will occur, plus an allowance for pipe line losses. It is unwise to install a single unit heater as the sole load on any boiler, particularly if the unit heater motor is started and stopped by thermostatic control. The wide and sudden fluctuations of load that occur under such conditions would require closer attention to the boiler than is usually possible in a small installation. Where oil or gas is used to fire the boiler, it is possible by means of a pressurestat to control the boiler, in response to this rapid fluctuation. In most cases, and particularly where the boiler is coal-fired, it is advisable to use two or more smaller unit heaters instead of one large unit.

Steam pressures below 5 lb can be used with safety for recirculating unit heaters when their heating surfaces are designed for those pressures, and when proper provision is made for returning the condensate. If units admit air that may be at a temperature below freezing, a steam pressure of not less than 5 lb should be maintained on the heating element, or a corresponding differential in pressure between the supply and returns should be maintained by means of a vacuum.

UNIT VENTILATORS

A unit ventilator is essentially a unit heater equipped with dampers for introducing outdoor and recirculating air in varying quantities, and arranged with a system of control that permits the heating effect to be varied with the fans operating continuously. Either steam or forced hot water may be employed as the heating medium, although steam is the more common. Unit ventilators are intended primarily for use in schools, meeting rooms, offices or other applications where the density of occupancy indicates the need for ventilation. In normal operation, the discharge air temperature from a unit ventilator is varied in accordance with the room demands. Where a heating effect is required, the air delivered is above room temperature. Where the heat generated within the room by occupants, sun, etc., is sufficient to cause overheating, then the air delivery temperature must be below that of the rooms. It is cutomary to equip unit ventilators with control devices that prevent the delivery of air at a temperature that will cause cold drafts. Unit ventilators may be of the radiator or damper controlled type constructed on the blow-through or draw-through principle as illustrated in Fig. 9.

Ratings of Unit Ventilators

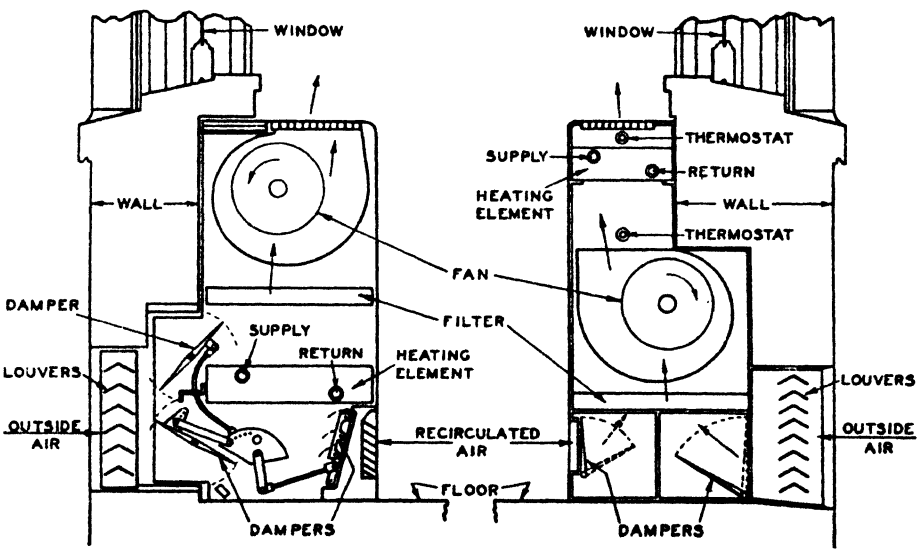
Unit ventilators of the steam type are customarily cataloged with two ratings, one the input and the other the output capacity. The first is the

heat input to the unit which is determined by measuring the temperature and quantity of condensate and the pressure and quality of the steam. The second is the heat output of the unit which is determined by measuring the quantity of air delivered and the temperature of the air to and from the unit. Table 3 shows the air handling capacities by the two methods of rating[5] and also the approximate heating data. In accordance with the A.S.H.V.E. Standard Code for Testing and Rating Steam Unit Ventilators the information to be supplied regarding ratings and the basis of rating is the following:

Rating Factors to Be Specified. The rating of the unit ventilator shall specify the following:

a. Final temperature at different entering air temperatures.

b. Total EDR at different entering air temperatures.



DRAW-THROUGH TYPE BLOW-THROUGH TYPE

FIG. 9. TYPICAL UNIT VENTILATORS SHOWING TWO OF MANY ARRANGEMENTS OF DAMPERS AND HEATING COILS

c. Air delivered by the unit in cubic feet per minute at the *standard basis of rating* with the fans operated at rated speed, with all air being blown through the heating unit and with the standard louver and grille on the outlet.

The Standard Basis of Rating shall be as follows:

a. Dry saturated steam at a temperature at the unit corresponding to an absolute pressure of 16.7 psi (218.5 F).

b. Entering air temperature of zero Fahrenheit degrees.

c. Volume delivered in cubic feet per minute converted to standard air at 70 F.

Rating Tables for unit ventilators shall contain the following data in addition to the standard rating, for entering air temperatures from −30 F to +60 F:

a. Inlet temperature, Fahrenheit degrees.

b. Final temperature, Fahrenheit degrees.

c. Total EDR at the specified entering temperature.

d. Surplus or heating EDR at the specified entering temperature.

Surplus or Heating Equivalent Direct Radiation for the purposes of this code shall be construed to mean difference between the total EDR at a specified inlet temperature and the EDR required to heat the air from that temperature to 70 F.

If no direct heating surface (radiation) is installed to take care of the normal heat transfer losses, and the unit ventilator is to be used for both heating and ventilation, then the combined requirements must be taken care of by the unit ventilator.

TABLE 3. TYPICAL CAPACITIES OF UNIT VENTILATORS FOR AN ENTERING AIR TEMPERATURE OF ZERO

CUBIC FEET OF AIR PER MINUTE		TOTAL CAPACITY IN SQUARE FEET, EQUIVALENT DIRECT RADIATION	CAPACITY AVAILABLE FOR HEATING THE ROOM, SQUARE FEET EQUIVALENT DIRECT RADIATION	FINAL AIR TEMPERATURE F DEG
Anemometer Rating	Condensate Rating			
750	500	214	56	95
1000	750	320	84	95
1260	1000	427	112	95
1560	1250	534	141	95

Heat Required for Ventilating Only

When all of the air handled by the unit is taken from the outside, the total heat to be supplied is obtained by means of Equations 1, 2, 3, and 4.

$$H = 0.24\ W\ (t_y - t) \tag{1}$$

$$H_v = 0.24\ W\ (t - t_o) \tag{2}$$

$$H_t = 0.24\ W\ (t_y - t_o) = H + H_v \tag{3}$$

$$W = d\ 60\ Q \tag{4}$$

From Equations 2, 3, and 4:

$$H_t = H + 0.24\ d\ 60\ Q\ (t - t_o). \tag{5}$$

where

d = density of air, pounds per cubic foot (0.075 lb per cu ft for Standard Air by definition).
H = heat loss of room, Btu per hour.
H_v = heat required to warm air for ventilation, Btu per hour.
H_t = total heat requirements for both heating and ventilation, Btu per hour. $= H + H_v$.
Q = volume of air handled by the ventilating equipment, cubic feet per minute.
t = temperature to be maintained in the room, Fahrenheit degrees.
t_o = outside temperature, Fahrenheit degrees.
t_y = temperature of the air leaving the unit, Fahrenheit degrees.
W = weight of air circulated, pounds per hour.
0.24 = specific heat of air at constant pressure (approximate value).

Example 1. The heat loss of a certain room is 24,000 Btu per hour, and the ventilating requirements are 1000 cfm. If the room temperature is to be 70 F and all air is taken from the outside at zero, what will be the total heat demand on the unit if it is required to provide for both the heating and ventilating requirements (combined system)?

Solution. Substituting in Equation 5:

$$H_t = 24{,}000 + 0.24 \times 0.075 \times 60 \times 1000\ (70 - 0) = 99{,}600 \text{ Btu per hour}$$

$$t_y = \frac{24{,}000}{0.24 \times 0.075 \times 60 \times 1000} + 70 = 92.2 \text{ F.}$$

Heat Required for Ventilating and Recirculating

When part of the air handled by the unit is taken from the room and the remainder from the outside,

$$H_t = 0.24 W_o (t_y - t_o) + 0.24 W_i (t_y - t) \quad (7)$$

$$W_o = d_o 60 Q_o \quad (8)$$

$$W_i = d_i 60 Q_i \quad (9)$$

$$t_y = \frac{H}{0.24 (W_o + W_i)} + t \quad (10)$$

$$H_t = H + 0.24 d_o 60 Q_o (t - t_o) \quad (11)$$

where

W_o = weight of air, pounds per hour taken from out-of-doors.
W_i = weight of air, pounds per hour taken from the room.
d_o = density of air, pounds per cubic foot at temperature t_o.
d_i = density of air, pounds per cubic foot at temperature t.
Q_o = volume of air taken in from the outside, cubic feet per minute.
Q_i = volume of air taken in from the room, cubic feet per minute.

Applications of Unit Ventilators

Items to be considered in the application of unit ventilators are: (1) combination with other means of heating, (2) location of units, and (3) method of venting or exhausting.

In a *split* system the unit is used primarily for ventilation. Air is delivered to the room at or slightly above room temperature, and enough radiation is installed in the room to take care of the normal heat transfer losses. Where the unit ventilator selected has a capacity more than sufficient to warm the air needed to meet the ventilating requirements, a corresponding reduction may be made in the amount of direct radiation installed. The greater the amount of excess capacity of the unit, the more efficient will be the temperature regulation of the room. The split system permits the heating of the room during failure of electric current, since the direct radiators will furnish heat, but it permits a careless operator to avoid operating the ventilating equipment.

The *combined* system employs a unit ventilator with sufficient capacity for both ventilation and the normal heat transfer losses. In such a case no direct radiation is required. The necessary operation of the fan when the room is being heated also gives assurance that some ventilation is being provided, especially if automatic dampers are used in the air intake and in the recirculating intake. These dampers are arranged to provide a certain quantity of outside air, depending upon the weather conditions. The cost of installation of a combined system is usually less than that of a split system and there is less danger of overheating, but if the electric energy fails there will be available only the heating effect of the units acting as convectors.

Location of Unit Ventilator

The location of the unit ventilator in a room is important. Wherever possible it should be placed against an outside wall and on the center line of the room. It is difficult to obtain proper air distribution if the unit is installed either on an inside wall or in a corner of the room. Standard units discharge the air stream upward, but for special cases units may be installed to discharge air horizontally. Units may be set away from the

wall or partially recessed into the wall to save space without materially affecting the results. The air inlet may enter the cabinet at the back at any point from top to bottom.

Air Exhaust Vents and Flues

The size and location of the air exhaust vent[6] outlet is important. In many cases the sizes for public buildings are regulated by law.

In cases where no codes govern, the location and size of vents are left to the discretion of the engineer.

Best results have been obtained with a velocity through the vent openings nearly equal to that at which the air is introduced into the room, thus maintaining a slight pressure in the room. Calculated velocities at the vent openings of from 600 to 800 fpm produce the best diffusion results from this system. Many states, however, have regulations that will not permit velocities as high as 800 fpm. If a vent opening at or near the floor is near a desk or place where a person is seated, a velocity of 800 fpm in the vent opening will produce an objectionable draft. In such a case the velocity in the vent opening should not exceed 400 to 450 fpm, although duct velocities are maintained at 600 to 800 fpm if codes permit.

In school buildings provided with wardrobes or cloakrooms the vents may be so located that the air shall pass through these spaces, ventilating them with air which otherwise would be passed to the outside without being used to the best advantage. Many state codes for ventilation of public buildings make this arrangement mandatory.

WINDOW VENTILATORS

A window ventilator illustrated in Fig. 10 consists of filter and switch controlled motor driven fans enclosed in a cabinet to be mounted on the window sill. Such units accomplish ventilation, air cleaning, and air circulation, but have no means of heating the air. The direction of air discharge is manually adjustable for seasonal operation.

UNIT HUMIDIFIERS

Unit humidifiers fall into four general classifications, depending on the method of causing evaporation. These are as follows: (1) *Nozzle Type*, (2) *Rotary Type*, (3) *Cascade Type*, and (4) *Heater Type*.

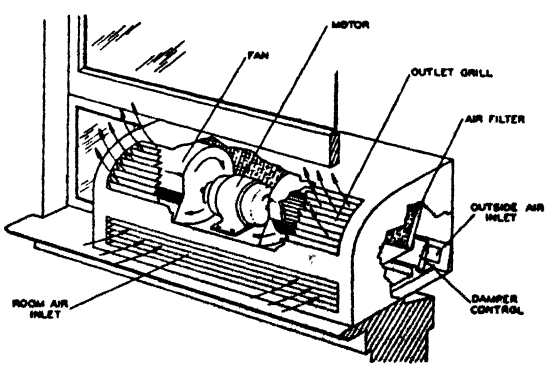


FIG. 10. TYPICAL WINDOW VENTILATOR

In the *nozzle type* of humidifier water is sprayed into the air and evaporation is effected by adiabatic exchange of energy. Units of this type in simplest form spray a fine mist of water directly into the air in a space. They are used to a great extent in the textile industry.

To the simple type of nozzle unit may be added the following accessories: a water heater whose function is to increase the vapor pressure, an air heater to heat the air either before or after humidification takes place, a screen or air filter over which the water is sprayed and through which the air is drawn for intimate contact with the water, a fan to create an air stream and to deliver air to the space to be humidified, and a housing to enclose all the elements. This type of unit has been made in practically all of the variations mentioned. It has the disadvantage of clogging the nozzles and must be serviced continually.

Fig. 11 illustrates a nozzle unit having a humidifying capacity sufficient for a residence or small building. These units usually include air filters and in some cases provide ventilation air by means of an outside air duct connection to the unit. The units are constructed for either floor or ceiling mounting and are usually placed in a central location in the basement with short supply and return duct connections from the first floor. Room air is brought into the unit through the return duct connection, is passed over a tempering coil heated by steam or hot water, and is then humidified by passing through some type of spray humidifier. Surplus moisture is removed by an eliminator and the humidified air is delivered to the room through a duct connection. Since a large percentage of the tempering coil capacity is transformed into latent heat during the humidifying process, the unit does not generally eliminate any existing steam radiation but does tend to improve comfort conditions by supplying heat during the off-period of furnace operation[7].

In the *rotary type* of humidifier the spray is created by rotating vanes or discs which throw the water by centrifugal force and in so doing break it up into a fine mist. In all other respects, this type of humidifier is similar to the nozzle type. It has the advantage over the nozzle type of being less liable to become clogged.

In the *cascade type* the humidification takes place by water falling in sheets over a series of baffles or trays. This type is usually furnished with a fan, air heater, and air filter all enclosed in a housing.

In the *heater type* of humidifier the water is heated either to the boiling point or to a temperature at which the water vapor readily passes into the air stream. There are many variations of this type of humidifier. In the simplest form the heating element using steam, hot water, gas, oil, or electricity is placed in a pan or vessel of water and the vapor passes from the surface of the water to the stream of air.

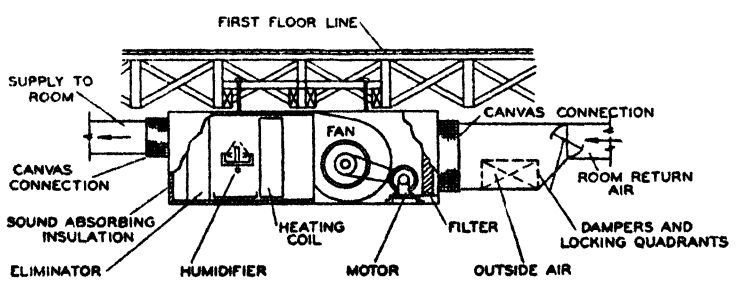


FIG. 11. TYPICAL UNIT HUMIDIFIER OF THE SPRAY TYPE WITH STEAM COIL TO PREHEAT THE AIR FOR RESIDENCES

A modification of this type of humidifier is the combination of spray nozzle and heater type in which the water is sprayed over a hot surface and evaporated. It has the disadvantage of accumulating scale on the surfaces of the vessel or heating surface.

For a discussion of various methods of humidification see Chapter 37.

REFERENCES

[1]—See *National Fan Manufacturers Association* standard definitions in Chapter 32.

[2]—Standard Code for Testing and Rating Steam Unit Heaters (A.S.H.V.E. TRANSACTIONS, Vol. 36, 1930, p. 165), prepared by a Joint Code Committee of the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS and the *Industrial Unit Heater Association* and adopted 1930.

[3]—Standard Code for Testing Hot Water Unit Heaters prepared by Engineering Committee of *Industrial Unit Heater Association*. Adopted by *Industrial Unit Heater Association* August 1942 and published September 1942.

[4]—A.S.H.V.E. RESEARCH REPORT No. 958—Temperature Gradient Observations in a Large Heated Space, by G. L. Larson, D. W. Nelson and O. C. Cromer (A.S.H.V.E. TRANSACTIONS, Vol. 39, 1933, p. 243). A.S.H.V.E. RESEARCH REPORT No. 1011—Tests of Three Heating Systems in an Industrial Type of Building by G. L. Larson, D. W. Nelson and John James (A.S.H.V.E. TRANSACTIONS, Vol. 41, 1935, p. 185).

[5]—A.S.H.V.E. Standard Code for Testing and Rating Steam Unit Ventilators (A.S.H.V.E. TRANSACTIONS, Vol. 38, 1932, p. 25).

[6]—A.S H.V.E. RESEARCH REPORT No. 936—Investigation of Air Outlets in Class Room Ventilation, by G. L. Larson, D. W. Nelson and R. W. Kubasta (A.S.H.V.E. TRANSACTIONS, Vol. 38, 1932, p. 463). A.S.H.V.E. RESEARCH REPORT No. 1017—Air Supply to Classrooms in Relation to Vent Flue Openings, by F. C. Houghten, Carl Gutberlet and M. F. Lichtenfels (A.S.H.V.E. TRANSACTIONS, Vol. 41, 1935, p 279).

[7]—Estimating the Humidification Requirements of Residences, by W. H. Severns (Papers Presented at the First Annual Conference on Air Conditioning, University of Illinois, *Engineering Experiment Station Circular, No. 26*, October, 1936).

Chapter 27

PIPE, FITTINGS, WELDING

Pipe Materials, Types of Pipe, Commercial Pipe Dimensions, Expansion and Flexibility of Pipe, Pipe Threads and Hangers, Types of Fittings, Flange Facings and Gaskets, Welding in Erection of Piping, Valves, Corrosion

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IMPORTANT considerations in the selection and installation of pipe and fittings for heating, ventilating, and air conditioning are dealt with in this chapter.

PIPE MATERIALS

Use of corrosion-resistant materials for pipe, including special alloy steels and irons, wrought-iron, copper, and brass, has increased considerably during the past few years. The recent development of copper, brass, and bronze fittings which can be assembled by soldering or sweating permits the use of thin-wall pipe and thereby has reduced the initial cost of such installations. The following brief discussion indicates the variety of pipe materials and the types of pipe available.

Wrought-Steel Pipe. Because of its low price, the great bulk of wrought pipe used for heating and ventilating work at the present time is of wrought steel. The material used for steel pipe is a mild steel made by the acid-bessemer, the open-hearth, or the electric-furnace process. Ordinary wrought-steel pipe is made either by shaping sheets of metal into cylindrical form and welding the edges together, or by forming or drawing from a solid billet. The former is known as *welded pipe*, the latter as *seamless pipe.*

Many types of welded pipe are available, although the smaller sizes most frequently used in heating and ventilating work are made by the lap-weld, resistance-weld, or butt-weld process. While the lap-weld and resistance-weld processes produce a better weld than the butt type, lap-weld and resistance-weld pipe are seldom manufactured in nominal pipe sizes less than 2 in. Seamless pipe can be obtained in the small sizes at a somewhat higher cost.

Seamless steel pipe is frequently used for high pressure work or where pipe is desired for close coiling, cold bending, or other forming operation. Its advantages are its somewhat greater strength which permits use of a thinner wall and, in the small sizes, its freedom from the occasional tendency of welded pipe to split at the weld when bent.

Wrought-Iron Pipe. Wrought-iron pipe is claimed to be more corrosion-resisting than ordinary steel pipe and therefore its somewhat higher first cost is said to be justified on the basis of longer life expectancy. Wrought-iron pipe may be identified by the spiral line marked into each length, either knurled into the metal or painted on it in red or other bright color. Otherwise, there is little difference in the appearance of wrought iron and steel pipe, although microscopic examination of polished and etched specimens will readily disclose the difference.

Cast-Ferrous Pipe. There are now available several types of cast-ferrous metal pipe made of a good grade of cast-iron with or without additions of nickel, chromium, or other alloy. This pipe is available in sizes from 1½ in. to 6 in., and in standard lengths of 5 or 6 ft with external and internal diameters closely approximating those of extra strong

wrought pipe. Cast-ferrous pipe may be obtained coupled, beveled for welding, or with ends plain or grooved for the several types of couplings. It is easily cut and threaded as well as welded. The fact that it is readily welded enables the manufacturers to supply the pipe in any lengths practicable for handling.

Alloy Metal Pipe. Steel pipe bearing a small alloy of copper or other alloying element and iron pipe bearing a small alloy of copper and molybdenum have been claimed to possess more resistance to corrosion than plain

TABLE 1. DIMENSIONS OF SCHEDULES 30 AND 40 AND STANDARD WEIGHT PIPE[a]

Size	Diameter In.		Thickness[b], In.	Weight per Ft, Lb		Threads per In.	Circumference, In.		Transverse Area, Sq In.			Length of Pipe, Ft per Sq Ft		Length of Pipe, Ft Containing 1 Cu Ft	Weight of Water, Lb per Ft
	External	Internal		Plain Ends	Threads and Couplings		External	Internal	External	Internal	Metal	External Surface	Internal Surface		
1/8	0.405	0.269	**0.068**	0.244	0.245	27	1.272	0.845	0.129	0.057	0.072	9.431	14.199	2533.775	0.025
1/4	0.540	0.364	**0.088**	0.424	0.425	18	1.696	1.144	0.229	0.104	0.125	7.073	10.493	1383.789	0.045
3/8	0.675	0.493	**0.091**	0.567	0.568	18	2.121	1.549	0.358	0.191	0.167	5.658	7.748	754.360	0.083
1/2	0.840	0.622	**0.109**	0.850	0.852	14	2.639	1.954	0.554	0.304	0.250	4.547	6.141	473.906	0.132
3/4	1.050	0.824	**0.113**	1.130	1.134	14	3.299	2.589	0.866	0.533	0.333	3.637	4.635	270.034	0.231
1	1.315	1.049	**0.133**	1.678	1.684	11½	4.131	3.296	1.358	0.864	0.494	2.904	3.641	166.618	0.375
1¼	1.660	1.380	**0.140**	2.272	2.281	11½	5.215	4.335	2.164	1.495	0.669	2.301	2.768	96.275	0.65
1½	1.900	1.610	**0.145**	2.717	2.731	11½	5.969	5.058	2.835	2.036	0.799	2.010	2.372	70.733	0.88
2	2.375	2.067	**0.154**	3.652	3.678	11½	7.461	6.494	4.430	3.355	1.075	1.608	1.847	42.913	1.45
2½	2.875	2.469	**0.203**	5.793	5.819	8	9.032	7.757	6.492	4.788	1.704	1.328	1.547	30.077	2.07
3	3.500	3.068	**0.216**	7.575	7.616	8	10.996	9.638	9.621	7.393	2.228	1.091	1.245	19.479	3.20
3½	4.000	3.548	**0.226**	9.109	9.202	8	12.566	11.146	12.566	9.886	2.680	0.954	1.076	14.565	4.29
4	4.500	4.026	**0.237**	10.790	10.889	8	14.137	12.648	15.904	12.730	3.174	0.848	0.948	11.312	5.50
5	5.563	5.047	**0.258**	14.617	14.810	8	17.477	15.856	24.306	20.006	4.300	0.686	0.756	7.198	8.67
6	6.625	6.065	**0.280**	18.974	19.185	8	20.813	19.054	34.472	28.891	5.581	0.576	0.629	4.984	12.51
8[c]	8.625	8.071	0.277	24.696	25.000	8	27.096	25.356	58.426	51.161	7.265	0.443	0.473	2.815	22.18
8	8.625	7.981	**0.322**	28.554	28.809	8	27.096	25.073	58.426	50.027	8.399	0.443	0.478	2.878	21.70
10[c]	10.750	10.136	0.307	34.240	35.000	8	33.772	31.843	90.763	80.691	10.072	0.355	0.376	1.785	34.95
10	10.750	10.020	**0.365**	40.483	41.132	8	33.772	31.479	90.763	78.855	11.908	0.355	0.381	1.826	34.20
12[c]	12.750	12.090	0.330	43.773	45.000	8	40.055	37.982	127.676	114.800	12.876	0.299	0.315	1.254	49.70
12	12.750	12.000	0.375	49.562	50.706	8	40.055	37.699	127.676	113.097	14.579	0.299	0.318	1.273	49.00

[a]Standard-weight wrought-iron pipe has approximately the same wall thicknesses and weights as contained herein for steel pipe. For exact dimensions, see *American Standard for Wrought-Iron and Wrought-Steel Pipe, A.S.A.* B36.10.

[b]Thicknesses shown in bold face type are identical with thicknesses for Schedule 40 pipe of *A.S.A.* B36.10.

[c]Same as Schedule 30, *A.S.A.* B36.10.

steel pipe and they are advertised and sold under various trade names.

Copper Pipe and Fittings. Owing to its inherent resistance to corrosion, copper and brass pipe have always been used in heating, ventilating, and water supply installations, but the cost with standard dimensions for threaded connections has been high. The recent introduction of fittings which permit erection by soldering or sweating allows the use of pipe with thinner walls than are possible with threaded connections, thereby reducing the cost of installations.

The initial cost of brass and copper pipe installations generally runs higher than the corresponding job with steel pipe and screwed connections in spite of the use of thin wall pipe, but the corrosive nature of the fluid conveyed or the inaccessibility of some of the piping may warrant use of a more expensive material than plain steel. The advantages of corrosion-

resisting pipe and fittings should be weighed against the correspondingly higher initial cost.

COMMERCIAL PIPE DIMENSIONS

The two weights of steel and wrought-iron pipe commonly used are known as *standard weight* and *extra strong*, which correspond to Schedules 40 and 80 respectively of the *American Standard for Wrought-Iron and Wrought-Steel Pipe, A.S.A.* B36.10. The same external diameter is used for both weights of each nominal size for manufacturing reasons as well

TABLE 2. STANDARD WEIGHTS AND DIMENSIONS OF WELDED AND SEAMLESS STEEL PIPE[a]

Size	Outside Diameter, In.	No. of Threads per In.	Standard-Weight Pipe				Extra-Strong Pipe				Double Extra-Strong Pipe[b]	
			Schedule 30		Schedule 40		Schedule 60		Schedule 80			
			Wall Thickness, In.	Weight per Ft, Lb T & C	Wall Thickness, In.	Weight per Ft, Lb T & C	Wall Thickness, In.	Weight per Ft, Lb Plain Ends	Wall Thickness, In.	Weight per Ft, Lb Plain Ends	Wall Thickness In.	Weight per Ft, Lb Plain Ends
⅛	0.405	27	.....	.....	0.068	0.25	.....	.....	0.095	0.31	.....	.....
¼	0.540	18	.....	.....	0.088	0.43	.....	.....	0.119	0.54	.....	.....
⅜	0.675	18	..	..	0 091	0.57	.....	.....	0.126	0.74	.....	.....
½	0.840	14	.....	.. ..	0.109	0.85	.....	.....	0.147	1.09	0.294	1.71
¾	1.050	14	.....	..	0.113	1.13	.....	.....	0 154	1.47	0.308	2.44
1	1.315	11½	.....	.....	0.133	1.68	.....	.....	0.179	2.17	0.358	3.66
1¼	1.660	11½	.....	.....	0.140	2.28	.....	.....	0.191	3.00	0.382	5.21
1½	1.900	11½	.....	.....	0.145	2.73	.....	.....	0.200	3.63	0.400	6.41
2	2.375	11½	.....	.....	0.154	3.68	.....	.....	0.218	5.02	0.436	9.03
2½	2.875	8	.....	.....	0.203	5.82	.....	.....	0.276	7.66	0.552	13.70
3	3.500	8	.....	.....	0.216	7.62	.....	.....	0.300	10.25	0.600	18.58
3½	4.000	8	.....	.....	0.226	9.20	.....	.....	0.318	12.51	0.636	22.85
4	4.500	8	.....	.....	0.237	10.89	.....	.....	0.337	14.98	0.674	27.54
5	5.563	8	.....	.....	0.258	14.81	.....	.....	0.375	20.78	0.750	38.55
6	6.625	8	.....	.....	0.280	19.19	.....	.....	0.432	28.57	0.864	53.16
8	8.625	8	0.277	25.00	0.322	28.81	.....	.....	0.500	43.39	0.875	72.42
10[c]	10.750	8	0.307	35.00	0.365	41.13	0.500	54.74	.....	.....	.....	.....
12[d]	12.750	8	0.330	45.00	0.375	50.71	0.500[d]	65.41	.....	.....	.....	.....

From Standard Specifications for Welded and Seamless Steel Pipe of the *American Society for Testing Materials, A.S.T.M.* Designation A120.

[a]Sizes larger than those shown in the table are measured by their outside diameter, such as 14 in. outside diameter, etc. These larger sizes will be furnished with plain ends, unless otherwise specified. The weights will correspond to the manufacturers' published standards although it is possible to calculate the theoretical weights for any given size and wall thickness on the basis of 1 cu in. of steel weighing 0.2833 lb.

[b]The American Standard for Wrought-Iron and Wrought-Steel Pipe *A.S.A.* B36.10-1939 has assigned no schedule number to *Double Extra-Strong* pipe.

[c]A 10 in. Standard Weight pipe is also available with 0.279 in. wall thickness, but this wall is not covered by a Schedule Number.

[d]Owing to a departure from the *Standard-Weight* and *Extra-Strong* wall thicknesses for the 12 in. nominal size, Schedules 40 and 60, Table 2 of the *A.S.A.* B36.10-1939, Standard for Wrought-Iron and Wrought-Steel Pipe, the regular *Standard* and *Extra-Strong* wall thicknesses (0.375 in. and 0.500 in.) have been substituted.

as to afford interchangeability in threading, and other elements associated with fabrication and erection. Hence the difference in wall thickness is accompanied by a corresponding change in inside diameter. In sizes up to 14 in., pipe is designated by its nominal size which corresponds roughly to the inside diameter of Schedule 40 pipe. In sizes 14 in. and upward, pipe is designated by its outside diameter (O. D.), and the wall thickness is specified.

While the demands for pipe for the heating and ventilating industry are reasonably well served by Schedule 40 (standard weight) pipe, the erection of pipe by welding sometimes warrants using lighter wall thicknesses. The considerations governing pipe wall thickness and its relation to joint design are covered in the *American Standard Code for Pressure Piping, A.S.A.* B31.1-1942, see Section 122. Standard schedules of pipe thick-

nesses are contained in the *American Standard for Wrought-Iron and Wrought-Steel Pipe, A.S.A.* B36.10, which includes standard-weight and extra-strong thicknesses in Schedules 40 and 80, respectively, and eight other schedules of varying wall thickness to provide for different service conditions. Dimensions and other useful data for Schedules 30 and 40 pipe are given in Table 1. Table 2 from *A.S.T.M.* Specifications A53 and

TABLE 3. STANDARD DIMENSIONS AND WEIGHTS, AND TOLERANCES IN DIAMETER AND WALL THICKNESS FOR COPPER WATER TUBES[a]

(All tolerances in this table are plus and minus except as otherwise indicated)

Standard Water Tube Size, In.	Actual Outside Diameter In.	Average Outside Diameter Tolerance, In.		Wall Thickness In. Type K		Type L		Type M		Theoretical Weight, Lb per Ft		
		Annealed	Drawn Temper	Nominal	Tolerance	Nominal	Tolerance	Nominal	Tolerance	Type K	Type L	Type M
⅛	0.250	0.002	0.001	0.032	0.003	0.025	0.0025	0.025	0.0025	0.085	0.068	0.068
¼	0.375	0.002	0.001	0.032	0.004	0.030	0.0035	0.025	0.0025	0.134	0.126	0.107
⅜	0.500	0.0025	0.001	0.049	0.004	0.035	0.0035	0.025	0.0025	0.269	0.198	0.145
½	0.625	0.0025	0.001	0.049	0.004	0.040	0.0035	0.028	0.0025	0.344	0.285	0.204
⅝	0.750	0.0025	0.001	0.049	0.004	0.042	0.0035	0.030	0.0025	0 418	0.362	0.263
¾	0.875	0.003	0.001	0.065	0.0045	0.045	0.004	0.032	0.003	0.641	0.455	0.328
1	1.125	0.0035	0.0015	0.065	0.0045	0.050	0.004	0.035	0.0035	0.839	0.655	0.465
1¼	1.375	0.004	0.0015	0.065	0.0045	0.055	0.0045	0.042	0.0035	1.04	0.884	0.682
1½	1.625	0.0045	0.002	0.072	0.005	0.060	0.0045	0.049	0.004	1.36	1.14	0.940
2	2.125	0.005	0.002	0.083	0.007	0.070	0.006	0.058	0.006	2.06	1.75	1.46
2½	2.625	0.005	0.002	0.095	0.007	0.080	0.006	0.065	0.006	2.93	2.48	2.03
3	3.125	0.005	0.002	0.109	0.007	0.090	0.007	0.072	0.006	4.00	3.33	2.68
3½	3.625	0.005	0.002	0.120	0.008	0.100	0.007	0.083	0.007	5.12	4.29	3.58
4	4.125	0.005	0.002	0.134	0.010	0.110	0.009	0.095	0.009	6.51	5.38	4.66
5	5.125	0.005	0.002	0.160	0.010	0.125	0.010	0.109	0.009	9.67	7.61	6.66
6	6.125	0.005	0.002	0.192	0.012	0.140	0.010	0.122	0.010	13.9	10.2	8.92
8	8.125	0.006	+0.002 −0.004	0.271	0.016	0.200	0.014	0.170	0.014	25.9	19.3	16.5
10	10.125	0.008	+0.002 −0.006	0.338	0.018	0.250	0.016	0.212	0.015	40.3	30.1	25.6
12	12.125	0.008	+0.002 −0.006	0.405	0.020	0.280	0.018	0.254	0.016	57.8	40.4	36.7

[a]From Standard Specifications for Copper Water Tube of the *American Society for Testing Materials, A.S.T.M.* Designation B88-41.

NOTE 1:—For copper gas and oil burner tubes, the tolerances shown above for various wall thicknesses (type K) apply irrespective of diameter.

NOTE 2:—For tubes other than round no standard tolerances are established. These tolerances do not apply to condenser and heat exchanger tubes.

A120 combines the schedule thicknesses of *A.S.A.* B36.10 and the old series designations.

Standard-weight pipe is generally furnished with threaded ends in random lengths of 16 to 22 ft, although when ordered with plain ends, 5 per cent may be in lengths of 12 to 16 ft. Five per cent of the total number of lengths ordered may be *jointers* which are two pieces coupled together. Extra-strong pipe is generally furnished with plain ends in random lengths of 12 to 22 ft, although 5 per cent may be in lengths of 6 to 12 ft.

In addition to *IPS* copper pipe, several varieties of copper tubing are in use with either flared or compression couplings or soldered joints. Dimensions of copper water tubing intended for plumbing, underground water service, fuel-oil lines, gas lines, etc., have been standardized by the U. S.

Government and the *American Society for Testing Materials*. There are three standard wall-thickness schedules of copper water tubing classified in accordance with their principal uses as follows:

Type *K*—Designed for underground services and general plumbing service.
Type *L*—Designed for general plumbing purposes.
Type *M*—Designed for use with soldered fittings only.

In general, Type *K* is used where corrosion conditions are severe, and Types *L* and *M* where such conditions may be considered normal as, for instance, in heating work. Types *K* and *L* are available in both hard and soft tempers; Type *M* is available only in hard temper. Where flexibility is essential as in hidden replacement work, or where as few joints as possible are desired as in fuel-oil lines, the soft temper is commonly used. In new

TABLE 4. THERMAL EXPANSION OF PIPE IN INCHES PER 100 FT[a]

(For superheated steam and other fluids refer to temperature column)

Saturated Steam			Elongation in Inches per 100 ft from −20 F up				Saturated Steam		Elongation in Inches per 100 ft from −20 F up			
Vacuum Inches of Hg.	Pressure Psig	Temperature Fahrenheit Degrees	Cast-Iron Pipe	Steel Pipe	Wrought-Iron Pipe	Copper Pipe	Pressure Psig	Temperature Fahrenheit Degrees	Cast-Iron Pipe	Steel Pipe	Wrought-Iron Pipe	Copper Pipe
		−20	0	0	0	0	2.5	220	1.634	1.852	1.936	2.720
		0	0.127	0.145	0.152	0.204	10.3	240	1.780	2.020	2.110	2.960
		20	0.255	0.293	0.306	0.442	20.7	260	1.931	2.183	2.279	3.189
		40	0.390	0.430	0.465	0.655	34.5	280	2.085	2.350	2.465	3.422
29.39	.....	60	0.518	0.593	0.620	0.888	52.3	300	2.233	2.519	2.630	3.665
28.89	.....	80	0.649	0.725	0.780	1.100	74.9	320	2.395	2.690	2.800	3.900
27.99	.....	100	0.787	0.898	0.939	1.338	103.3	340	2.543	2.862	2.988	4.145
26.48	.....	120	0.926	1.055	1.110	1.570	138.3	360	2.700	3.029	3.175	4.380
24.04	.....	140	1.051	1.209	1.265	1.794	180.9	380	2.859	3.211	3.350	4.628
20.27	.....	160	1.200	1.368	1.427	2.008	232.4	400	3.008	3.375	3.521	4.870
14.63	.....	180	1.345	1.528	1.597	2.255	293.7	420	3.182	3.566	3.720	5.118
6.45	.....	200	1.495	1.691	1.778	2.500	366.1	440	3.345	3.740	3.900	5.358

[a]From *Piping Handbook*, by Walker and Crocker. This table gives the expansion from −20 F to the temperature in question. To obtain the amount of expansion between any two temperatures take the difference between the figures in the table for those temperatures. For example, if a steel pipe is installed at a temperature of 60 F and is to operate at 300 F, the expansion would be 2.519 − 0.593 = 1.926 in.

or exposed work copper pipe of a hard temper is generally used. All three classes are extensively used with soldered fittings.

Standard dimensions, weights, and diameter and wall-thickness tolerances for these classes of copper tubing are given in Table 3. Copper pipe is also available with dimensions of steel pipe.

Refrigeration lines used in connection with air conditioning equipment also employ copper tubing extensively. For refrigeration use where tubing absolutely free from scale and dirt is required, bright annealed copper tubing that has been deoxidized is used. This tubing is available in a variety of sizes and wall thicknesses.

EXPANSION AND FLEXIBILITY

The increase in temperature of a pipe from room temperature to an operating steam or water temperature 100 deg or more above room temperature results in an increase in length of the pipe for which provision must be made. The amount of linear expansion (or contraction in the case of refrigeration lines) per unit length of material per degree change in

temperature is termed the *coefficient of linear expansion*, or commonly, the *coefficient of expansion*. This coefficient varies with the material.

The linear expansion of cast-iron, steel, wrought-iron, and copper pipe, the materials most frequently used in heating and ventilating work, can be determined from Table 4.

The three methods by which the elongation due to thermal expansion may be taken care of are: (1) Expansion joints; (2) Swivel joints; (3) Inherent flexibility of the pipe itself utilized through pipe bends, right-angle turns, or offsets in the line.

Expansion joints of the slip-sleeve, diaphragm, or corrugated types made of copper, rubber, or other gasket material are all used for taking up expansion, but generally only for low pressures or where the inherent flexibility of the pipe cannot readily be used as in underground steam or hot water distribution lines.

Swivel joints are used to some extent in low-pressure steam and hot-

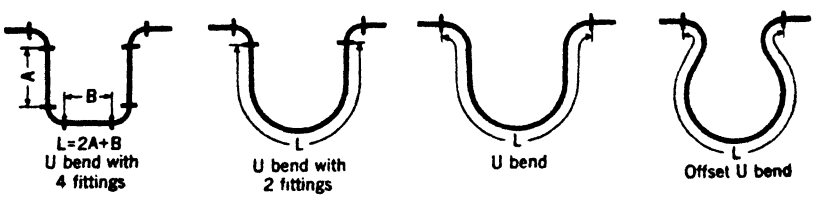


FIG. 1. MEASUREMENT OF L ON VARIOUS PIPE BENDS

water heating systems, and in hot-water supply lines. Since swivel joints permit the expansive movement of the pipe by turning of threaded joints, which may ultimately result in a leak, it is preferable to provide sufficient flexibility without resorting to swiveling in the threads.

Probably the most economical method of providing for expansion of piping in a long run is to take advantage of the directional changes which must necessarily occur in the piping and proportion the offsets so that sufficient flexibility is secured. Ninety-degree bends with long, straight tangents in either a horizontal or a vertical plane are an excellent means for securing adequate flexibility with larger sizes of pipe. When flexibility cannot be obtained in this manner, it is necessary to make use of some type of expansion bend. The exact calculation of the size of expansion bends required to take up a given amount of thermal expansion is relatively complicated[1]. The following approximate method, however, has been found to give reasonably good results and is deemed to be sufficiently accurate for most heating installations.

Fig. 1 shows several types of expansion bends commonly used for taking up thermal expansion. The amount of pipe, L, required in each of these bends may be computed from Equation 1.

$$L = 6.16\sqrt{D\Delta} \qquad (1)$$

where

L = length of pipe, feet.
D = outside diameter of the pipe used, inches.
Δ = the amount of expansion to be taken up, inches.

This formula, based on the use of mild-steel pipe with wall thicknesses not heavier than extra-strong, assumes a maximum safe value of fiber

stress of 16,000 psi. When square type bends are used, the width of the bend should not exceed about twice the height, since for a given total length of pipe in the bend, the height of the bend becomes progressively less with increase in width until the height approaches zero and no flexibility exists. Actually, wide bends utilize to best advantage the inherent flexibility of the line, but such bends cannot be proportioned on the basis of Equation 1. For such applications, more accurate methods [1] should be employed. It is further assumed that the corners are made with screwed or flanged elbows or with arcs of circles having radii five to six times the pipe diameter. Use of welding elbows with radii of 1½ times the pipe diameter will decrease the end thrusts somewhat but will raise the fiber stress correspondingly.

All risers must be anchored and safeguarded so that the difference in length when hot from the length when cold shall not disarrange the normal and orderly provisions for drainage of the branches.

Proper anchoring of piping is especially necessary with light-weight radiators, to allow for freedom of expansion in order that no pipe strain will distort the radiators. When expansion strains from the pipes are permitted to reach these light metal heaters, they usually emit disturbing sounds.

HANGERS AND SUPPORTS

Heating system piping requires careful and substantial support. Where changes in temperature of the line are not large, such simple methods of support may be utilized as hanging the line by means of rods or perforated strip from the building structure, or supporting it by brackets or on piers.

When fluids are conveyed at temperatures of 150 F or above, however, hangers or supporting equipment must be fabricated and assembled to permit free expansion or contraction of the piping. This can be accomplished by the use of long rod hangers, spring hangers, chains, hangers or supports fitted with rollers, machined blocks, elliptical or circular rings of larger diameter than the pipe giving contact only at the bottom, or trolley hangers. In all cases, allowance should be made for rod clearance to permit swinging without setting up severe bending action in the rods.

For pipes of small size, perforated metal strip is often used. For horizontal mains, the rod or strip usually is attached to the joists or steel work of the floor above. For long runs of vertical pipe subject to considerable thermal expansion, either the hangers should be designed to prevent excessive load on the bottom support due to expansion, or the bottom support should be designed to withstand the entire load.

THREADING PRACTICE

In all threaded pipe for heating and ventilating installations the American Standard taper pipe thread, *A.S.A.* B2.1-1942 is used. This thread is cut with a taper of 1 in 16 measured on the diameter of the pipe so as to secure a tight joint. The number of threads per inch varies with the pipe size. Threads for fittings are the same, except that it is regular practice to furnish straight tapped couplings for Schedule 40 pipe 2 in. and smaller. For steam pressures in excess of 25 psi, it is recommended that taper-tapped couplings be used to obtain a tight joint. These may be secured by ordering *line* pipe [2] which is used for oil piping, the couplings of which are provided with taper-tapped threads and may be used with regular mill-threaded standard weight pipe. Thread lengths should be in accordance with *A.S.A.* B2.1. Right-hand threads are used unless

otherwise ordered. To facilitate drainage, some elbows have the thread tapped at an angle to provide a pitch of the connecting pipe of ¼ in. to the foot. These elbows are known to the trade as pitch elbows and are commercially available. All threaded pipe joints should be made up with a thread paste suitable for the service for which the pipe is to be used.

TYPES OF FITTINGS

Fittings for joining the separate lengths of pipe together are made in a variety of forms, and are either screwed or flanged, the former being generally used for the smaller sizes of pipe up to and including 3½ in., and the latter for the larger sizes, 4 in. and above. Screwed fittings of

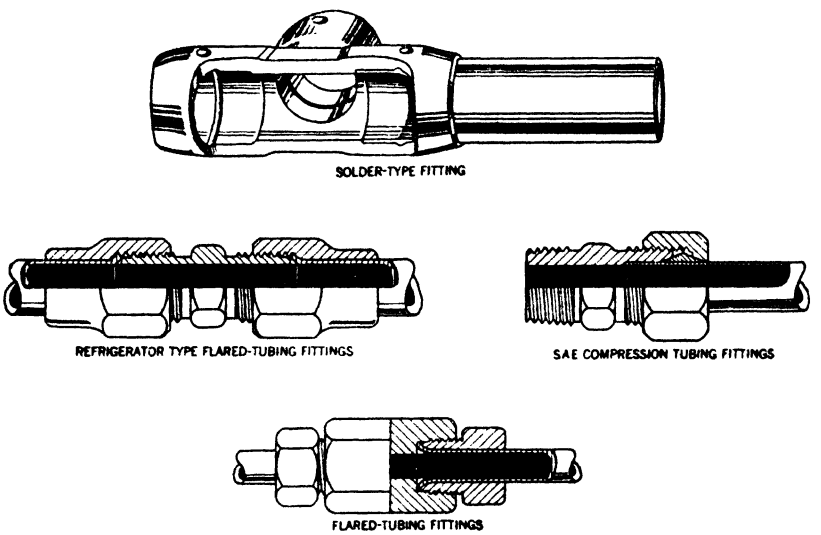


FIG. 2. COPPER OR BRASS TUBING FITTINGS

large size as well as flanged fittings of small size are also made and are used for certain classes of work at the proper pressure.

The material used for fittings is generally cast-iron, but in addition to this, malleable-iron, steel and steel alloys are also used, as well as various grades of brass or bronze. The material to be used depends on the character of the service and the pressure. Malleable iron fittings, like brass fittings, are cast with a round instead of a flat band or bead, or with no bead at all. Fittings are designated as male or female, depending on whether the threads are on the outside or inside, respectively. Screwed galvanized fittings are made according to the 150 lb American Standard.

As in the case of pipe, several weights of fittings are manufactured. Recognized American Standards for the various weights are as follows:

Cast-iron pipe flanges and flanged fittings for 25 lb (sizes 4 in. and larger), 125 lb, and 250 lb maximum saturated steam pressure, *A.S.A.* B16b2, B16a, and B16b respectively.

Malleable iron screwed fittings for 150 lb maximum saturated steam pressure, *A.S.A.* B16c.

Cast-iron screwed fittings for 125 and 250 lb maximum saturated steam pressure, *A.S.A.* B16d.

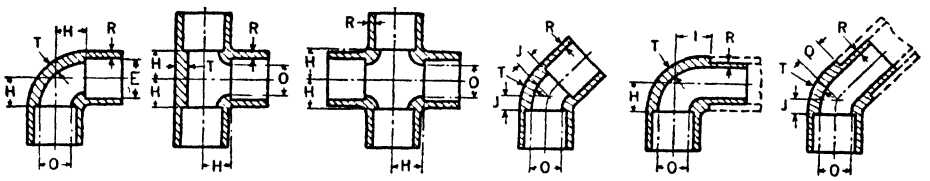
Steel flanged fittings for 150 and 300 lb maximum steam service pressure, *A.S.A.* B16e.

The allowable cold water working pressures for these standards vary from 43 lb for the 25 lb standard to 500 lb for the 300 lb steel standard.

War standard ratings in effect for the duration of the emergency permitted higher ratings for certain sizes of the 125 lb cast-iron flanged fitting standard, and for 300 lb steel flanges and flanged fittings than those shown in the regular American Standards mentioned previously.

Screwed fittings include: nipples or short pieces of pipe of varying lengths; couplings of steel or wrought-iron; elbows for turning angles of either 45 deg or 90 deg; return bends, which may be of either the close

TABLE 5. AMERICAN STANDARD DIMENSIONS OF ELBOWS, TEES, CROSSES, AND 45 DEG ELBOWS, SOLDERED-JOINT FITTINGS, *A.S.A.* A40.3-1941



NOMINAL SIZE[a]	CAST BRASS[b]							WROUGHT METAL	BORE OF FITTINGS
	Laying Length, Tee, Ell, and Cross[b]	Laying Length, Ell With External Shoulder	Laying Length, 45 Deg Ell	Laying Length, 45 Deg Ell External Shoulder	Inside Diameter of Fittings,[c] Min.	Metal Thickness[d]		Metal Thickness[e] Min.[f]	
	H	I	J	Q	O	T	R	T and R	E, Min.
1/4	1/4	3/8	3/16	1/4	0.31	0.08	0.048	0.030	0.378
3/8	5/16	7/16	3/16	5/16	0.43	0.08	0.048	0.035	0.503
1/2	7/16	9/16	3/16	5/16	0.54	0.09	0.054	0.040	0.628
3/4	9/16	11/16	1/4	3/8	0.78	0.10	0.060	0.045	0.878
1	3/4	7/8	5/16	7/16	1.02	0.11	0.066	0.050	1.1285
1 1/4	7/8	1	7/16	9/16	1.26	0.12	0.072	0.055	1.3785
1 1/2	1	1 1/8	1/2	5/8	1.50	0.13	0.078	0.060	1.629
2	1 1/4	1 3/8	9/16	3/4	1.98	0.15	0.090	0.070	2.129
2 1/2	1 1/2	1 5/8	5/8	7/8	2.46	0.17	0.102	0.080	2.629
3	1 3/4	1 7/8	3/4	1	2.94	0.19	0.114	0.090	3.129
3 1/2	2	2 1/8	7/8	1 1/8	3.42	0.20	0.120	0.100	3.629
4	2 1/4	2 3/8	15/16	1 1/4	3.90	0.22	0.132	0.110	4.129
5	3 1/8	.....	1 1/16	.....	4.87	0.28	0.168	0.125	5.129
6	3 5/8	.....	1 5/8	.....	5.84	0.34	0.204	0.140	6.129

All dimensions given in inches.

[a] This size is the nominal bore of the tube.

[b] These dimensions may be used for wrought-metal fittings as well as for cast-brass fittings at manufacturer's option.

[c] This dimension is the same as the inside diameter Class L tubing (American Standard Specifications for Copper Water Tube, *A.S.A.* H23.1-1939 (*A.S.T.M.* B88).

[d] Patterns shall be designed to produce body thicknesses given in the table. Metal thickness at no point shall be less than 90 per cent of the thicknesses given in the table.

[e] This dimension has the same thickness as Type L tubing.

[f] These dimensions are minimum, but in every case the thickness of wrought fittings should be at least as heavy as the tubing with which it is to be used.

NOTE 1:—Wrought fittings, as well as cast fittings, must be provided with a shoulder or stop at the bottom end of socket.

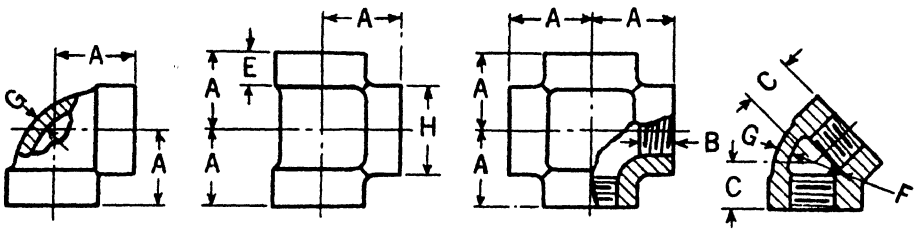
NOTE 2:—Street fittings with male ends are for use in connection with other fittings illustrated.

or open pattern, and may be cast with either a back or side outlet; tees; crosses; laterals or *Y* branches; and a variety of plugs, bushings, caps, lock-nuts, flanges and reducing fittings. Reducing fittings as well as bushings, both of which are used in changing from one pipe size to another, may have the smaller connection tapped eccentrically to permit free drain-

age of the water of condensation in steam lines or free escape of air in water lines.

Fittings for copper tubing are available in the soldered, flared, or compression types. Illustrations of each of these types are shown in Fig. 2. Fittings for copper pipe of *IPS* dimensions are available in screwed or soldered types of connection. Table 5 from *A.S.A.* Standard A40.3-1941

TABLE 6. AMERICAN STANDARD DIMENSIONS OF ELBOWS, 45-DEG ELBOWS, TEES, AND CROSSES (STRAIGHT SIZES) FOR CLASS 125 CAST-IRON SCREWED FITTINGS, *A.S.A.* B16a-1939



Elbow Tee Cross 45 deg elbow

Nominal Pipe Size	*A* Center to End, Elbows, Tees and Crosses	*C* Center to End, 45 Deg Elbows	*B* Length of Thread, Min.	*E* Width of Band, Min.	*F* Inside Diameter of Fitting, Min.	*F* Inside Diameter of Fitting, Max.	*G* Metal Thickness,[a] Min.	*H* Outside Diameter of Band, Min.
¼	0.81	0.73	0.32	0.38	0.540	0.584	0.110	0.93
⅜	0.95	0.80	0.36	0.44	0.675	0.719	0.120	1.12
½	1.12	0.88	0.43	0.50	0.840	0.897	0.130	1.34
¾	1.31	0.98	0.50	0.56	1.050	1.107	0.155	1.63
1	1.50	1.12	0.58	0.62	1.315	1.385	0.170	1.95
1¼	1.75	1.29	0.67	0.69	1.660	1.730	0.185	2.39
1½	1.94	1.43	0.70	0.75	1.900	1.970	0.200	2.68
2	2.25	1.68	0.75	0.84	2.375	2.445	0.220	3.28
2½	2.70	1.95	0.92	0.94	2.875	2.975	0.240	3.86
3	3.08	2.17	0.98	1.00	3.500	3.600	0.260	4.62
3½	3.42	2.39	1.03	1.06	4.000	4.100	0.280	5.20
4	3.79	2.61	1.08	1.12	4.500	4.600	0.310	5.79
5	4.50	3.05	1.18	1.18	5.563	5.663	0.380	7.05
6	5.13	3.46	1.28	1.28	6.625	6.725	0.430	8.28
8	6.56	4.28	1.47	1.47	8.625	8.725	0.550	10.63
10	8.08[b]	5.16	1.68	1.68	10.750	10.850	0.690	13.12
12	9.50[b]	5.97	1.88	1.88	12.750	12.850	0.800	15.47

All dimensions given in inches.

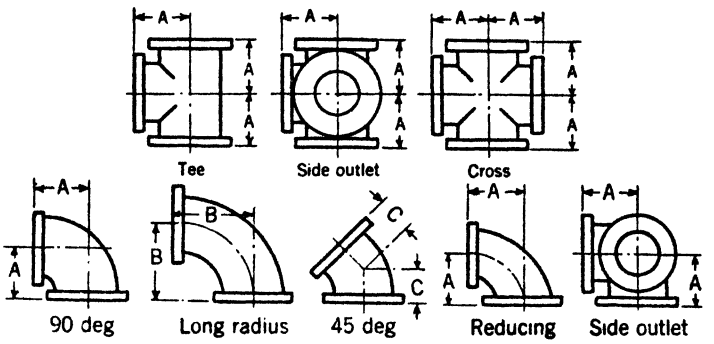
[a]Patterns shall be designed to produce castings of metal thickness given in the table. Metal thickness at no point shall be less than 90 per cent of the thickness given in the table.

[b]Applies to elbows and tees only.

contains dimensions for soldered joint elbows, tees, crosses, and 45 deg elbows.

The compression type fitting is generally limited to smaller size tubing while the flared and soldered types are used in both large and small sizes. An American Standard, *A.S.A.* A40.2-1936 has been prepared to standardize dimensions for brass fittings for flared copper water tubes. Flared tube fittings are widely used in refrigerating work where *S.A.E.* dimensions and a 45-deg flare render most fittings interchangeable, although

TABLE 7. AMERICAN STANDARD DIMENSIONS OF TEES, CROSSES[a] (STRAIGHT SIZES), AND ELBOWS FOR CLASS 125 CAST-IRON FLANGED FITTINGS, *A.S.A.* B16a-1939



Nominal Pipe Size[b-e]	*A* Center to Face Tees, Crosses[c-d] and Elbows	*AA* Face to Face Tees and Crosses[c-d]	*B* Center to Face Long Radius Elbows[e,f,g]	*C* Center to Face 45 Deg Elbows	Diameter of Flange	Thickness of Flange, Min	Metal[h] Thickness of Body
1	3½	7	5	1¾	4¼	7/16	5/16
1¼	3¾	7½	5½	2	4⅝	½	5/16
1½	4	8	6	2¼	5	9/16	5/16
2	4½	9	6½	2½	6	5/8	5/16
2½	5	10	7	3	7	11/16	5/16
3	5½	11	7¾	3	7½	¾	⅜
3½	6	12	8½	3½	8½	13/16	7/16
4	6½	13	9	4	9	15/16	½
5	7½	15	10¼	4½	10	15/16	½
6	8	16	11½	5	11	1	9/16
8	9	18	14	5½	13½	1⅛	⅝
10	11	22	16½	6½	16	1⅜16	¾
12	12	24	19	7½	19	1¼	13/16
14 O.D.	14	28	21½	7½	21	1⅜	⅞
16 O.D.	15	30	24	8	23½	1⅞16	1
18 O.D.	16½	33	26½	8½	25	1⅝16	1 1/16
20 O.D.	18	36	29	9½	27½	1 11/16	1⅛
24 O.D.	22	44	34	11	32	1⅞	1¼
30 O.D.	25	50	41½	15	38¾	2⅛	1⅜16
36 O.D.	28	56	49	18	46	2⅜	1⅝
42 O.D.	31	62	56½	21	53	2⅝	1 13/16
48 O.D.	34	68	64	24	59½	2¾	2

All dimensions given in inches.

[a] Crosses both straight and reducing sizes 18 in. and larger shall be reinforced to compensate for the inherent weakness in the casting design.

[b] Size of all fittings listed indicates nominal inside diameter of port.

[c] Tees, side outlet tees, and crosses, 16 in. and smaller, reducing on the outlet, have the same dimensions center to face, and face to face as straight size fittings corresponding to the size of the larger opening. Sizes 18 in. and larger, reducing on the outlet, are made in two lengths, depending on the size of the outlet.

[d] Tees and crosses, reducing on run only, carry same dimensions center to face and face to face as a straight size fitting of the larger opening.

[e] Reducing elbows and side outlet elbows carry same dimensions center to face as straight size elbows corresponding to the size of the larger opening.

[f] Special degree elbows, ranging from 1 to 45 deg, inclusive, shall have the same center to face dimensions as given for 45-deg elbows and those over 45 deg and up to 90 deg, inclusive, shall have the same center to face dimensions as given for 90-deg elbows. The angle designation of an elbow is its deflection from straight line flow and is the angle between the flange faces.

[g] Side outlet elbows shall have all openings on intersecting center-lines.

[h] Body thickness at no point shall be less than 87½ per cent of the dimensions given in the table.

for refrigeration use, thread fits and tolerances on thread gages must be maintained within close limits. Brass fittings with *S.A.E.* dimensions are not interchangeable with the American Standard fittings for water tubes.

Ammonia pipe fittings made of cast-iron were formerly used extensively in handling refrigerants in large installations. Replacement of ammonia by other refrigerants operating at lower pressures has seriously curtailed the market for these fittings. For this reason formulation of an American Standard for these fittings was abandoned by the *A.S.A.* in 1936.

FLANGE FACINGS AND GASKETS

A number of different flange facings in common use are plain face, raised face, tongue and groove, and male and female. Cast-iron fittings for 125 psi and below are normally furnished with a plain face, while the 250 lb cast-iron fittings are supplied with a 1/16-in. raised face. The standard facing for steel flanged fittings for 150 and 300 psi is a 1/16-in. raised face although these fittings are obtainable with a variety of facings. The gasket surface of the raised face may be finished smooth or may be machined with concentric or spiral grooves often referred to as serrated face or phonograph finish, respectively.

The dimensions of elbows, tees, and crosses for 125 lb cast-iron screwed fittings are given in Table 6, whereas the dimensions for 125 lb cast-iron flanged fittings are given in Table 7.

For low temperature service not to exceed about 220 F, a number of paper or vegetable fiber gasket materials will prove satisfactory; for plain raised face flanges, rubber or rubber inserted gaskets are commonly employed. Asbestos composition gaskets are probably the most widely used, particularly where the temperature exceeds 250 F. Jacketed asbestos and metallic gaskets may be used for any pressure and temperature conditions, but preferably only with a narrow recessed facing.

WELDING

Erection of piping in heating and ventilating installations by means of fusion welding has been commonly accepted in the past few years as an alternate method to the screwed and flanged joint. Since the question of economy of welding as against the use of screwed and flanged fittings is dependent on the individual job, the use of welding is generally recommended on the basis of a greatly reduced cost of maintenance and repair, of less weight resulting from the use of a lighter-weight pipe, and of increased economy in pipe insulation, hangers, and supports rather than on the basis of any economy that might be effected in actual erection by welding on low to medium pressure heating jobs.

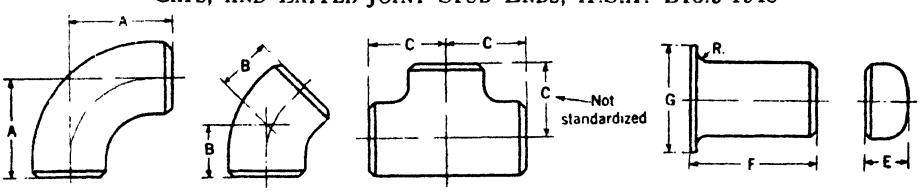
Fusion welding, commonly used in erection of piping, is defined as the process of joining metal parts in the molten, or molten and vapor states, without the application of mechanical pressure or blows. Fusion welding embraces gas welding and electric arc welding, both of which are commonly used to produce acceptable welds. Welding processes and procedure are described in various publications.

Welding application requires the same basic knowledge of design as do the other types of assembly, but, in addition, requires a generous knowledge of the sciences involved, particularly as to welding qualities of metal, their reaction to extremely high temperatures, and the ability to determine and use only the best quality welding rods. This requirement applies equally to employer and employee with the employer accepting

all of the responsibility. Thus the employer should select his welding mechanics with good judgment, provide them with first-class equipment and tools, arrange for their training and use of acceptable workmanship standards, and at regular intervals subject their work to prescribed tests.

Rules for fusion welding of pipe joints, the qualification of welding operators, welding procedures and the testing thereof, are contained in the Standard Manual on Pipe Welding of the Heating, Piping & Air Conditioning Contractors National Association, and other nationally recognized groups[3, 4, 5]. In general, the wall thickness and chemical analysis of the pipe are the governing factors, not the working pressure. There are a number of safety codes which govern the installation of welded piping in many cities and states. Some of the more prominent are listed at the end of this chapter[4, 5, 6].

TABLE 8. AMERICAN STANDARD DIMENSIONS FOR BUTT-WELDING ELBOWS, TEES, CAPS, AND LAPPED-JOINT STUB ENDS, *A.S.A.* B16.9-1940



Nominal Pipe Size	Outside Diameter	Center-to-End			Caps *Eb-c*	Lapped-Joint Stub Ends		
		90-Deg Elbows *A*	45-Deg Elbows *B*	Of Run Tee *Ca*		Length *Fb*	Radius of Fillet *R*	Diam. of Lap *Gd*
1	1.315	1½	⅞	1½	1½	4	⅛	2
1¼	1.660	1⅞	1	1⅞	1½	4	3/16	2½
1½	1.900	2¼	1⅛	2¼	1½	4	¼	2⅞
2	2.375	3	1⅜	2½	1½	6	5/16	3⅝
2½	2.875	3¾	1¾	3	1½	6	5/16	4⅛
3	3.500	4½	2	3⅜	2	6	⅜	5
3½	4.000	5¼	2¼	3¾	2½	6	⅜	5½
4	4.500	6	2½	4⅛	2½	6	7/16	6 3/16
5	5.563	7½	3⅛	4⅞	3	8	7/16	7 5/16
6	6.625	9	3¾	5⅝	3½	8	½	8½
8	8 625	12	5	7	4	8	½	10⅝
10	10.750	15	6¼	8½	5	10	½	12¾
12	12.750	18	7½	10	6	10	½	15

All dimensions given in inches.

[a] The dimensions of welding tees cover those which have side outlets from one size less than half the size of the run-way opening of the tees to full size.

[b] Dimensions *E* and *F* are applicable only to these fittings in schedules up to and including Schedule 80, *A.S.A.* Standard B36.10-1939.

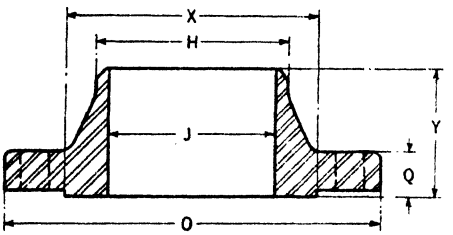
[c] The shape of these caps shall be ellipsoidal and shall conform to the requirements of the *A.S.M.E.* Boiler Construction Code.

[d] This dimension is for standard machined facings in accordance with American Standard for Steel Pipe Flanges and Flanged Fittings (*A.S.A.* B16e-1939). The back face of the lap shall be machined to conform to the surface of the flange on which it seats. Where ring joint facings are to be applied, use dimension *K* as given in *A.S.A.* B16e-1939.

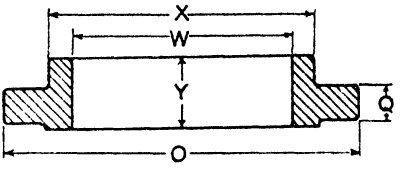
A complete line of manufactured steel welding fittings is now available and a dimensional standard has been prepared under the procedure of the *American Standards Association* to unify heretofore divergent dimensions for the same type welding fittings as produced by different manufacturers. Standard dimensions for steel butt-welding elbows, tees, caps, and lapped-joint stub ends are given in Table 8. Dimensions for eccentric and concentric reducers, and 180-deg return bends are not shown in Table 8 but

are included in the American Standard. Larger sizes also are available in some types of fittings. The welding bevel which is a straight 37½-deg V for wall thickness ¾ in. and below, and a U-bevel for thicknesses heavier than ¾ in., conforms to the recommended practice of *A.S.A.*

TABLE 9. AMERICAN STANDARD DIMENSIONS OF STEEL WELDING NECK AND SLIP-ON WELDING FLANGES FOR STEAM SERVICE PRESSURE RATING OF 150 PSI (GAGE) AT A TEMPERATURE OF 500 F, AND 100 PSI (GAGE) AT 750 F, *A.S.A.* B16e-1939



WELDING NECK



SLIP-ON WELDING

NOMINAL PIPE SIZE	DIAMETER OF FLANGE	THICKNESS OF FLG.[a] MIN.	DIAMETER OF HUB	HUB DIAM. BEGINNING OF CHAMFER[b-c]	LENGTH THRU HUB[a]	INSIDE DIAM. OF PIPE SCHEDULE 40[c]	BORE OF SLIP-ON FLANGES MIN	DIAM OF BOLT CIRCLE	NO. OF BOLTS	SIZE OF BOLTS
	O	*Q*	*X*	*H*	*Y*	*J*	*W*			
½	3½	7/16	1 3/16	0.84	1 7/8	0.62*	0.88	2 3/8	4	½
¾	3 7/8	½	1 ½	1.05	2 1/16	0.82*	1.09	2 3/4	4	½
1	4 1/4	9/16	1 15/16	1.32	2 3/16	1.05*	1.38	3 1/8	4	½
1¼	4 5/8	5/8	2 5/16	1.66	2 1/4	1.38*	1.72	3 ½	4	½
1½	5	11/16	2 9/16	1.90	2 7/16	1.61*	1.97	3 7/8	4	½
2	6	¾	3 1/16	2.38	2 ½	2.07*	2.44	4 ¾	4	5/8
2½	7	7/8	3 9/16	2.88	2 3/4	2.47*	2.94	5 ½	4	5/8
3	7½	15/16	4 1/4	3.50	2 3/4	3.07*	3.56	6	4	5/8
3½	8½	15/16	4 13/16	4.00	2 13/16	3.55*	4.06	7	8	5/8
4	9	15/16	5 5/16	4.50	3	4.03*	4.56	7½	8	5/8
5	10	15/16	6 7/16	5.56	3½	5.05*	5.66	8½	8	¾
6	11	1	7 9/16	6.63	3½	6.07*	6.72	9½	8	¾
8	13½	1 1/8	9 11/16	8.63	4	7.98*	8.72	11 ¾	8	¾
10	16	1 3/16	12	10.75	4	10.02*	10.88	14¼	12	7/8
12	19	1¼	14 3/8	12.75	4½	.....	12.88	17	12	7/8
14 O.D.	21	1 3/8	15 ¾	14.00	5	To Be	14.19	18 ¾	12	1
16 O.D.	23½	1 7/16	18	16.00	5	Specified	16.19	21¼	16	1
18 O.D.	25	1 9/16	19 7/8	18.00	5½	by	18.19	22 ¾	16	1 1/8
20 O.D.	27½	1 11/16	22	20.00	5 11/16	Purchaser	20.19	25	20	1 1/8
24 O.D.	32	1 7/8	26 1/8	24.00	6		24.19	29½	20	1¼

All dimensions given in inches.

[a] A raised face of 1/16 in. is included in *thickness of flange minimum* and in *length through hub.*

[b] The outside surface of the welding end of the hub shall be straight or tapered at not more than 6 deg.

[c] Dimensions *H* and *J* correspond to the outside and inside diameters of pipe as given in *A.S.A.* B36.10-1939, Schedule 40.

*These diameters are identical with the diameters of what was formerly designated as *Standard Weight Pipe* of the corresponding sizes.

Standard B16e-1939, American Standard for Steel Pipe Flanges and Flanged Fittings. The latter also contains dimensions for steel welding neck flanges for pressures up to 2500 psi, and slip-on welding flanges for 150 and 300 psi. Table 9 gives these dimensions for welding-neck and slip-on welding flanges suitable for 150 psi gage pressure.

Socket-welding fittings also are commercially available. These fittings have a machined recess for inserting the pipe which is attached by a fillet weld between the pipe wall and socket end. Use of socket-welding fittings generally is restricted to nominal pipe sizes 3 in. and smaller in

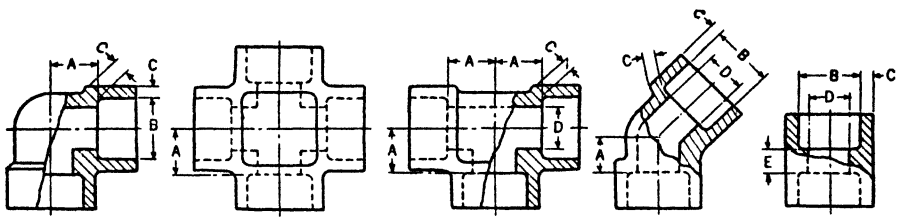
which range commercial fittings are available. This type of fitting has gained rapid acceptance owing to its ease of installation, low cost, and ability to make a pressure tight joint without weakening the pipe as is the case with threading. Dimensions for socket-welding fittings as offered by most manufacturers of the product are given in Table 10.

VALVES

Valves are made with both threaded and flanged ends for screwed and bolted connections just as are pipe fittings.

The material used for valves of small size is generally brass or bronze for low pressures and forged steel for high pressures, while in the larger

TABLE 10. PROPOSED AMERICAN STANDARD DIMENSIONS OF SOCKET-WELDING ELBOWS, TEES, CROSSES, 45-DEG ELBOWS, AND COUPLINGS



Nominal Pipe Size	Minimum Depth of Socket	Center to Bottom of Socket: 90-Deg Ells, Tees, Crosses, Sched. 40 & 80	Center to Bottom of Socket: 90-Deg Ells, Tees, Crosses, Sched. 160	Center to Bottom of Socket: 45-Deg Ells, Sched. 40 & 80	Center to Bottom of Socket: 45-Deg Ells, Sched. 160	Couplings Distance Between Bottom Sockets	Bore Diameter of Socket, Minimum	Minimum Socket Wall Thickness: Sched. 40	Minimum Socket Wall Thickness: Sched. 80	Minimum Socket Wall Thickness: Sched. 160	Bore Diameter of Fittings: Sched. 40	Bore Diameter of Fittings: Sched. 80	Bore Diameter of Fittings: Sched. 160
		A		A		E	B	C[a]			D		
¼	3/8	17/32	.....	5/16	.....	¼	0.555	0.156	0.156	.....	0.364	0.302	.....
3/8	3/8	17/32	.....	5/16	.....	¼	0.690	0.156	0.158	.....	0.493	0.423	.....
½	3/8	5/8	¾	7/16	½	3/8	0.855	0 156	0.184	0.234	0.622	0.546	0.466
¾	½	¾	⅞	½	9/16	3/8	1.065	0.156	0.193	0.273	0.824	0.742	0.614
1	½	⅞	1 1/16	⅝	11/16	½	1.330	0.166	0.224	0.313	1.049	0.957	0.815
1¼	½	1 1/16	1¼	13/16	15/16	½	1.675	0.175	0.239	0.313	1.380	1.278	1.160
1½	½	1¼	1½	15/16	1	½	1.915	0.181	0.250	0.351	1.610	1.500	1.338
2	5/8	1½	1 5/8	1	1 1/16	¾	2.406	0 193	0.273	0.429	2.067	1.939	1.689
2½	5/8	1 5/8	2¼	1 1/16	1¼	¾	2.906	0.254	0.345	0.469	2.469	2.323	2.125
3	5/8	2¼	2½	1¼	1 3/8	¾	3.535	0.270	0.375	0.546	3.068	2.900	2.626

All dimensions are given in inches.

[a]Dimension *C* is 1¼ times the nominal pipe thickness, minimum, but not less than 1/16 in.

Reducing sizes have same center to bottom of socket dimension as the largest size of reducing fitting.

sizes either cast-iron, cast-steel or some of the steel alloys are employed. Practically all iron or steel valves intended for steam or water work are bronze-mounted or trimmed.

Brass, bronze, and iron valves are generally designed for standard or extra heavy service, the former being used up to 125 lb and the latter up to 250 lb saturated steam working pressure, although most manufacturers also make valves for medium pressure up to 175 lb steam working pressure. The more common types are gate valves or straightway valves, globe valves, angle valves, check valves and automatic valves, such as reducing and back-pressure valves.

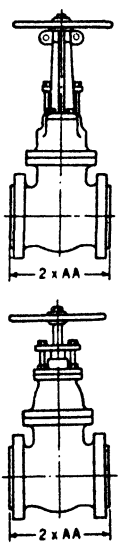
Gate valves are the most frequently used of all valves since in their open position the resistance to flow is a minimum, but they should not be used where it is desired to throttle the flow; globe valves should be used for this purpose. Gate valves may be secured with either a rising or a non-

rising stem, although in the smaller sizes the rising stem is more commonly used. The rising stem valve is desirable because the positions of the handle and stem indicate whether the valve is open or closed, although space limitations may prevent its use. The globe valve is less expensive to manufacture than the gate valve, but its peculiar construction offers a high resistance to flow and may prevent complete drainage of the pipe line. These objections are of particular importance in heating work.

An American Standard, *A.S.A.* B16.10-1939, has been prepared giving the face-to-face dimensions of ferrous flanged and welding-end valves. The following types are covered: wedge gate, double disc gate, globe and angle, and swing check. One purpose of establishing these dimensions is

TABLE 11. AMERICAN STANDARD CONTACT SURFACE TO CONTACT SURFACE DIMENSIONS OF CAST-IRON AND STEEL FLANGED WEDGE GATE VALVES, *A.S.A.* B16.10-1939

NOMINAL PIPE SIZE	CONTACT SURFACE TO CONTACT SURFACE DIMENSIONS, (2 × AA)				
	Cast-Iron[a]			Steel	
	125	175[bc]	250[b]	150[b]	300[b]
1	.....	.....	.....	.....	.....
1¼	.....	.....	.....	.....	.....
1½	.....	.....	.....	.....	7½
2	7	7¼	8½	7	8½
2½	7½	8	9½	7½	9½
3	8	9¼	11⅛	8	11⅛
3½	8½	10	11⅞	8½	11⅞
4	9	10½	12	9	12
5	10	11½	15	10	15
6	10½	13	15⅞	10½	15⅞
8	11½	14¼	16½	11½	16½
10	13	16¾	18	13	18
12	14	17½	19¾	14	19¾
14 O.D.	15	.....	22½	15	30
16 O.D.	16	.....	24	16	33
18 O.D.	17	.....	26	17	36
20 O.D.	18	.....	28	18	39
24 O.D.	20	.....	31	20	45



All dimensions given in inches.

[a]These dimensions are the same for Cast-Iron Double Disc Flanged Gate Valves.

[b]These are pressure designations which refer to the primary service ratings in pounds per square inch of the connecting end flanges.

[c]The connecting end flanges of 175 lb valves are the same as those on 250 lb valves.

NOTE 1:—Where dimensions are not given, the sizes either are not made or there is insufficient demand to warrant the expense of unification.

NOTE 2:—Female and groove joint facings have bottom of groove in same plane as *flange edge*, and center to contact surface dimensions for these facings are reduced by the amount of the raised face.

to insure that gate valves of a given rating and flange dimension of either the wedge or double disc design will be interchangeable in a pipe line. Contact surface to contact surface dimensions of cast-iron and steel flanged wedge-gate valves are given in Table 11. End-to-end dimensions for steel butt-welding valves in sizes up to 8 in., inclusive, are the same as those given in Table 11 for steel valves.

Check valves are automatic in operation and permit flow in only one direction, depending for operation on the difference in pressure between the two sides of the valve. The two principal kinds of check valves are the swing check in which a flapper is hinged to swing back and forth, and the lift check in which a dead weight disc moves vertically from its seat.

Valves commonly used for controlling steam or water supply to radiators constitute a special class since they are manufactured to meet

heating system requirements. These valves are generally of the angle type and are usually made of brass. Graduations on the heads or lever handles are often supplied to indicate the relative opening of the valve.

Automatic control of steam supply to individual radiators can be effected by use of direct-acting radiator valves having a thermostatic element at the valve, or near to it. The direct-acting valve is usually an angle-type valve containing a thermostatic element which permits the flow of steam in accordance with room temperature requirements. These valves usually are capable of adjustment to permit variation in room temperature to suit individual taste.

Ordinary steam valves may be used for hot water service by drilling a 1/16-in. hole through the web forming the seat to insure sufficient circulation to prevent freezing when the valve is closed. Valves made for use in hot water heating systems are of simpler design, one type consisting of a simple butterfly valve, and another of a quick opening type in which a part in the valve mechanism matches up with an opening in the valve body.

In one-pipe steam-heating systems, automatic air valves are required at the radiators. Two common types of air valves available are the vacuum type and the straight-pressure type. Vacuum valves permit the expulsion of air from the radiators when the steam pressure rises and, in addition, act as checks to prevent the return of air into the radiator when a vacuum is formed by the condensation of steam after the supply pressure has dropped. Ordinary air valves permit the expulsion of air from the radiator when steam is supplied under pressure, but when a vacuum tends to be formed the air is drawn back into the radiator.

REFERENCES

[1]—See (1) Piping Handbook, by Walker and Crocker (McGraw-Hill Co.); (2) A Manual for The Design of Piping for Flexibility by the Use of Graphs, by E. A. Wert, S. Smith, E. T. Cope, (The Detroit Edison Company).

[2]—See *API Specification 5L for Line Pipe, American Petroleum Institute.*

[3]—Standard Manual on Pipe Welding, *Heating, Piping and Air Conditioning Contractors National Association.* Welding Handbook, *American Welding Society,* 1942.

[4]—ASME Power Boiler Code, *American Society of Mechanical Engineers.*

[5]—American Standard Code for Pressure Piping, A.S.A. B-31.1—1942, *American Standards Association.*

[6]—Marine Engineering Regulations of the Coast Guard, *American Bureau of Shipping.*

General Specifications for Inspection of Material, Appendix VII, Welding, *U. S. Navy.* Specifications for Welding, Appendix 5, Part 1—General—for vessels of the *U. S. Navy, Bureau of Ships,* April, 1940.

Chapter 28

PIPE INSULATION

Heat Losses from Bare and Insulated Pipes, Low Temperature Pipe Insulation, Insulation of Pipes to Prevent Freezing, Economical Thickness of Pipe Insulation, Underground Pipe Insulation

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THE heat loss from uninsulated pipes may be of considerable magnitude if the temperature of the surrounding medium differs appreciably from that of the fluid conveyed. Losses are increased by rapid motion of the surrounding air or by contact of the pipe with bodies of high conductivity. Careful consideration must, therefore, be given to this factor in a properly designed system and adequate insulation provided, if necessary.

HEAT LOSSES FROM BARE PIPES

Heat losses from horizontal bare steel pipes, based on tests at *Mellon Institute* and calculated from the fundamental radiation and convection equations (Chapter 5), are given in Table 1. Heat losses from horizontal copper tubes and pipes with tarnished surfaces, are given in Table 2 [1].

Heat losses from bare pipe of materials having lower emissivities may be calculated from data appearing in Chapter 5.

The area in square feet per linear foot of pipe is given in Table 3 for various standard pipe sizes, and Table 4 for copper tubing, while Table 5 gives the area in square feet of flanges and fittings for various standard pipe sizes. These tables can be used to advantage in estimating the amount of insulation required.

Very often, when pipes are insulated, flanges and fittings are left bare so as to allow for easy access to the fittings in case of repairs. The fact that a pair of 8-in. standard flanges having an area of 2.41 sq ft would lose, at 100 lb steam pressure, an amount of heat equivalent to more than a ton of coal per year shows the necessity for insulating such surfaces.

Examples 1 and *2* show how the annual heat loss from uncovered pipe and its dollar value may be computed from the data in Table 1.

Example 1. Compute the total annual heat loss from 165 ft of 2 in. bare pipe in service 4000 hr per year. The pipe is carrying steam at 10 lb pressure and is exposed to an average air temperature of 70 F.

Solution. The pipe temperature is taken as the steam temperature, which is 239.4 F, obtained by interpolation from Steam Tables. The temperature difference between the pipe and air = 239.4 − 70 = 169.4 F. By interpolation of Table 1 between temperature differences of 157.1 and 227.7 F, the heat loss from a 2-in. pipe at a temperature difference of 169.4 F is found to be 1.624 Btu per (hour) (linear foot) (Fahrenheit degree). The total annual heat loss from the entire line = 1.624 × 169.4 × 165 (linear feet) × 4000 (hours) = 181,600 Mb. (Mb = 1000 Btu.)

Example 2. Coal costing $11.50 per ton and having a calorific value of 13,000 Btu per pound is being burned in the furnace supplying steam to the pipe line given in the previous example. If the system is operating at an over-all efficiency of 55 per cent, determine the monetary value of the annual heat loss from the line.

Solution. The cost of heat per 1000 Mb supplied to the system = 1,000,000 × 11.5 (dollars) ÷ [13,000 (Btu) × 2000 (lb) × 0.55 (efficiency)] = $0.804. The total cost of heat lost per year = 0.804 × 181.6 (thousand Mb) = $146.00.

PIPE INSULATIONS

Pipe insulations are of several general forms and are made of various types of material. The most common form is the rigid sectional covering either split longitudinally into halves or cut through on one side and scored on the other, to facilitate assembling on pipes. Preformed ma-

TABLE 1. HEAT LOSSES FROM HORIZONTAL BARE STEEL PIPES

Expressed in Btu per (hour) (linear foot) (Fahrenheit degree difference between the pipe and surrounding still air at 70 F)

Nominal Pipe Size (Inches)	Hot Water				Steam		
	120 F	150 F	180 F	210 F	227.1 F (5 Lb)	299.7 F (50 Lb)	337.9 F (100 Lb)
	Temperature Difference						
	50 F	80 F	110 F	140 F	157.1 F	227.7 F	267.9 F
½	0.455	0.495	0.546	0.584	0.612	0.706	0.760
¾	0.555	0.605	0.666	0.715	0.748	0.866	0.933
1	0.684	0.743	0.819	0.877	0.919	1.065	1.147
1¼	0.847	0.919	1.014	1.086	1.138	1.324	1.425
1½	0.958	1.041	1.148	1.230	1.288	1.492	1.633
2	1.180	1.281	1.412	1.512	1.578	1.840	1.987
2½	1.400	1.532	1.683	1.796	1.883	2.190	2.363
3	1.680	1.825	2.010	2.153	2.260	2.630	2.840
3½	1.900	2.064	2.221	2.433	2.552	2.974	3.215
4	2.118	2.302	2.534	2.717	2.850	3.320	3.590
5	2.580	2.804	3.084	3.303	3.470	4.050	4.385
6	3.036	3.294	3.626	3.886	4.074	4.765	5.160
8	3.880	4.215	4.638	4.960	5.210	6.100	6.610
10	4.760	5.180	5.680	6.090	6.410	7.490	8.115
12	5.590	6.070	6.670	7.145	7.500	8.800	9.530

TABLE 2. HEAT LOSS FROM HORIZONTAL TARNISHED COPPER PIPE

Expressed in Btu per (hour) (linear foot) (Fahrenheit degree difference between the pipe and surrounding still air at 70 F)

Nominal Pipe Size (Inches)	Hot Water (Type K Copper Tube)				Steam (Standard Pipe Size Pipe)		
	120 F	150 F	180 F	210 F	227.1 F (5 Lb)	297.7 F (50 Lb)	337.9 F (100 Lb)
	Temperature Difference						
	50 F	80 F	110 F	140 F	157.1 F	227.7 F	267.9 F
½	0.250	0.287	0.300	0.321	0.433	0.500	0.530
¾	0.340	0.381	0.409	0.429	0.533	0.543	0.654
1	0.440	0.475	0.509	0.536	0.636	0.746	0.803
1¼	0.500	0.559	0.618	0.622	0.764	0.878	0.934
1½	0.580	0.656	0.710	0.750	0.904	1.053	1.120
2	0.730	0.825	0.890	0.957	1.101	1.273	1.364
2½	0.880	1.000	1.091	1.143	1.305	1.490	1.605
3	1.040	1.175	1.272	1.343	1.560	1.800	1.940
3½	1.180	1.350	1.454	1.535	1.750	2.020	2.170
4	1.460	1.500	1.635	1.715	1.941	2.240	2.430
4½	.....	.....	.....	.....	2.131	2.465	2.650
5	1.600	1.812	1.980	2.071	2.387	2.770	2.990
6	1.840	2.125	2.270	2.430	2.740	3.210	3.440
8	2.400	2.685	2.910	3.110	3.310	4.050	4.370

terials are supplied in segments for assembly on large pipes. The sectional coverings are generally supplied with a pasted on canvas jacket. Blanket insulations are sometimes used for wrapping large pipes, particularly where removal for frequent servicing of the pipe is necessary. Fittings and bends are commonly covered with portions of standard preformed

TABLE 3. EXTERNAL SURFACE PER LINEAR FOOT OF PIPE

NOMINAL PIPE SIZE (INCHES)	SURFACE AREA (SQ FT)	NOMINAL PIPE SIZE (INCHES)	SURFACE AREA (SQ FT)	NOMINAL PIPE SIZE (INCHES)	SURFACE AREA (SQ FT)
½	0.22	2	0.622	5	1.456
¾	0.275	2½	0.753	6	1.734
1	0.344	3	0.917	8	2.257
1¼	0.435	3½	1.047	10	2.817
1½	0.498	4	1.178	12	3.338

insulation or, when irregular in contour, with plastic materials known as insulating cements. Insulation is secured to pipes with staples which are used to bridge the joint between half sections, and with metal pipe covering bands or rings of wire which secure individual sections and effect a junction between abutting sections. Surface finishes used over pipe insulation depend upon the service encountered and appearance desired. Canvas jackets are most common although asbestos paper or asbestos finishing cements are sometimes employed. Insulation outdoors should be waterproof and is generally protected with an asphalt felt for piping and asphaltic cements for fittings. Insulation on lines carrying cold water, brine, or other cold fluids is carefully finished to obtain adequate sealing against the penetration of water vapor.

The selection of pipe insulation for a particular service condition must be made with full consideration of a number of properties in addition to thermal conductivity. Factors which may be of more importance than the thermal conductivity are: ease of application, fire resistance, heat stability, weathering stability, resistance to damage by physical abuse, and others which may apply to a particular installation. A complete evaluation of pipe insulation cannot be included here. Insulation manufacturers should be consulted in regard to the selection of insulation which is to meet specific requirements.

HEAT LOSSES FROM INSULATED PIPES

The conductivities of various materials used for insulating steam and hot water systems are given in Table 6. They are given as functions of the mean temperatures or the arithmetic mean of the inner and outer surface temperatures of the insulations. It should be emphasized that they are the average values obtained from a number of tests made on each type of material, also, that in the use of *conductivity* all variables due to differences in thickness, pipe sizes, and air conditions are eliminated. Individual manufacturer's materials will, of course, vary in conductivity to some extent from these values.

The heat losses through 1, 1½, and 2-in. thick 85 per cent magnesia type of insulation for temperature differences between the pipe and the

TABLE 4. EXTERNAL SURFACE PER LINEAR FOOT OF COPPER TUBING

Outside diameter ⅛ in. greater than nominal size

TUBE SIZE (INCHES)	SURFACE AREA (SQ FT)	TUBE SIZE (INCHES)	SURFACE AREA (SQ FT)	TUBE SIZE (INCHES)	SURFACE AREA (SQ FT)
½	0.164	2	0.556	5	1.342
¾	0.229	2½	0.687	6	1.604
1	0.295	3	0.818	8	2.128
1¼	0.360	3½	0.949	....	.....
1½	0.426	4	1.080	....	.....

TABLE 5. AREA OF FLANGED FITTINGS, SQUARE FEET[a]

NOMINAL PIPE SIZE (INCHES)	FLANGED COUPLING		90 DEG ELL		LONG RADIUS ELL		TEE		CROSS	
	Standard	Extra Heavy	Standard	Extra Heavy	Standard	Extra Heavy	Standard	Extra Heavy	Standard	Extra Heavy
1	0.320	0.438	0.795	1.015	0.892	1.083	1.235	1.575	1.622	2.07
1¼	0.383	0.510	0.957	1.098	1.084	1.340	1.481	1.925	1.943	2.53
1½	0.477	0.727	1.174	1.332	1.337	1.874	1.815	2.68	2.38	3.54
2	0.672	0.848	1.65	2.01	1.84	2.16	2.54	3.09	3.32	4.06
2½	0.841	1.107	2.09	2.57	2.32	2.76	3.21	4.05	4.19	5.17
3	0.945	1.484	2.38	3.49	2.68	3.74	3.66	5.33	4.77	6.95
3½	1.122	1.644	2.98	3.96	3.28	4.28	4.48	6.04	5.83	7.89
4	1.344	1.914	3.53	4.64	3.96	4.99	5.41	7.07	7.03	9.24
4½	1.474	2.04	3.95	5.02	4.43	5.46	6.07	7.72	7.87	10.07
5	1.622	2.18	4.44	5.47	5.00	6.02	6.81	8.52	8.82	10.97
6	1.82	2.78	5.13	6.99	5.99	7.76	7.84	10.64	10.08	13.75
8	2.41	3.77	6.98	9.76	8.56	11.09	10.55	14.74	13.44	18.97
10	3.43	5.20	10.18	13.58	12.35	15.60	15.41	20.41	19.58	26.26
12	4.41	6.71	13.08	17.73	16.35	18.76	19.67	26.65	24.87	34.11

[a]Including areas of accompanying flanges bolted to the fitting.

surrounding atmosphere up to 280 F are shown in Figs. 1, 2, and 3. Standard thicknesses of 85 per cent magnesia pipe covering are not exactly 1 in. However, the loss through any given thickness of insulation can be obtained by interpolation. Also, the losses through any of the insulations given in Table 6 can be obtained by multiplying the losses obtained from Figs. 1, 2, or 3 by the factors given in Table 7.

TABLE 6. THERMAL CONDUCTIVITY (*k*) OF VARIOUS TYPE PIPE INSULATIONS FOR MEDIUM AND HIGH TEMPERATURE PIPE[a]

Expressed in Btu per (hour) (square foot) (Fahrenheit degree temperature difference per inch)

TYPES OF INSULATING MATERIALS	DENSITY LB/CU FT	TEMP. RANGE OF ACCEPTED USE	MEAN TEMPERATURE, F DEG				
			100	200	300	400	500
85% Magnesia—Type	13–15	Up to 600 F	0.41	0.45	0.48	0.52	.....
Corrugated Asbestos—Type							
4 Ply per 1 in.	11–13	Up to 300 F	0.57	0.68	0.80		.....
6 Ply per 1 in.	15–17	Up to 300 F	0.51	0.59	0.69		.....
8 Ply per 1 in.	18–20	Up to 300 F	0.49	0.57	0.65	.....	.....
Laminated Asbestos—Type (35–40 laminations per 1 in.)	30–35	Up to 700 F	0.39	0.44	0.49	0.54	.....
Mineral Wool—Type	10–15	Up to 800 F	0.40	0.45	0.50	0.55	.....
Diatomaceous Silica—Type	25–30	Up to 1900 F	0.63	0.66	0.69	0.72	0.75
Brown Asbestos Fiber—Type	13–15	Up to 1200 F	0.34	0.39	0.44	0.49	0.54

[a]Average values from various laboratories for insulating materials of various manufacturers.

TABLE 7. PIPE COVERING FACTORS

TYPES OF INSUALTING MATERIALS	TEMPERATURE DIFFERENCE, PIPE TO AIR, F DEG				
	100	200	300	400	500
Corrugated Asbestos—Type					
4 Ply per 1 in.	1.30	1.36	1.42	.....	.....
6 Ply per 1 in.	1.19	1.23	1.27	.....	.....
8 Ply per 1 in.	1.15	1.19	1.23	.....	.....
Laminated Asbestos—Type	0.96	0.98	1.00	1.02	1.04
Mineral Wool—Type	0.98	1.00	1.02	1.05	1.07
Diatomaceous Silica—Type	1.37	1.36	1.35	1.35	1.34
Brown Asbestos Fiber—Type	0.86	0.88	0.91	0.93	0.96

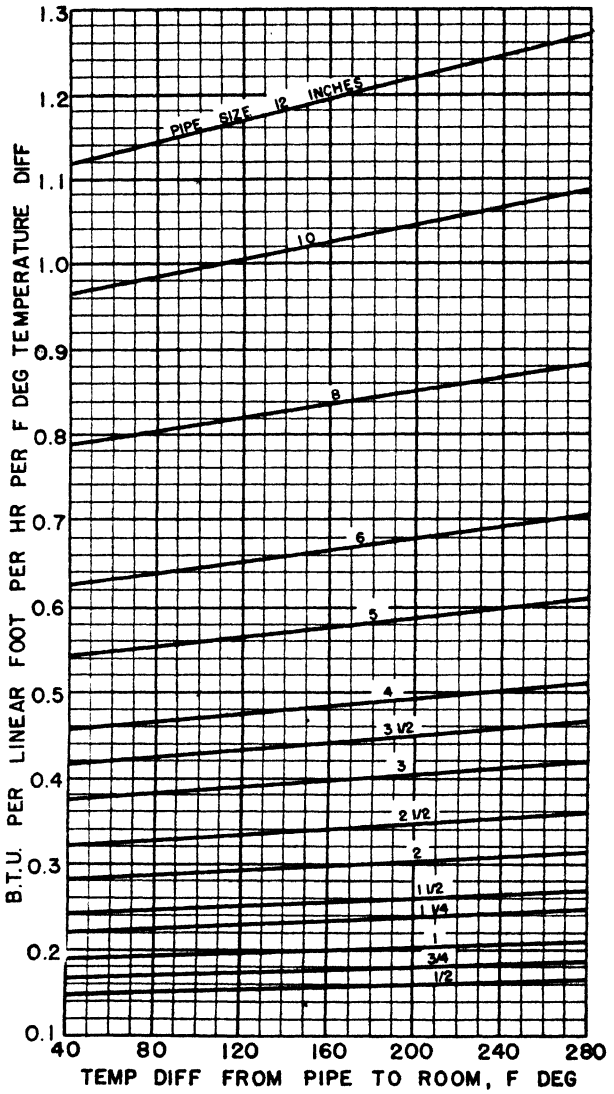


FIG. 1. HEAT LOSS THROUGH 1 IN. THICK 85 PER CENT MAGNESIA TYPE COVERING

Pipes operating at high temperatures are frequently insulated to the best advantage by combining a high temperature insulation near the pipe with a moderate or low temperature insulation around it as an outer layer. By this method an efficient material may be used for each of the two temperature ranges encountered. In calculating the heat loss through such a combination the mean temperature of each layer must be determined along with the thickness of each. This is readily done in three or four calculations performed as a series of approximations in which assumptions of thickness and mean temperature are adjusted as indicated in the discussion which follows.

In the case of a single thickness of pipe covering, the quantity of heat

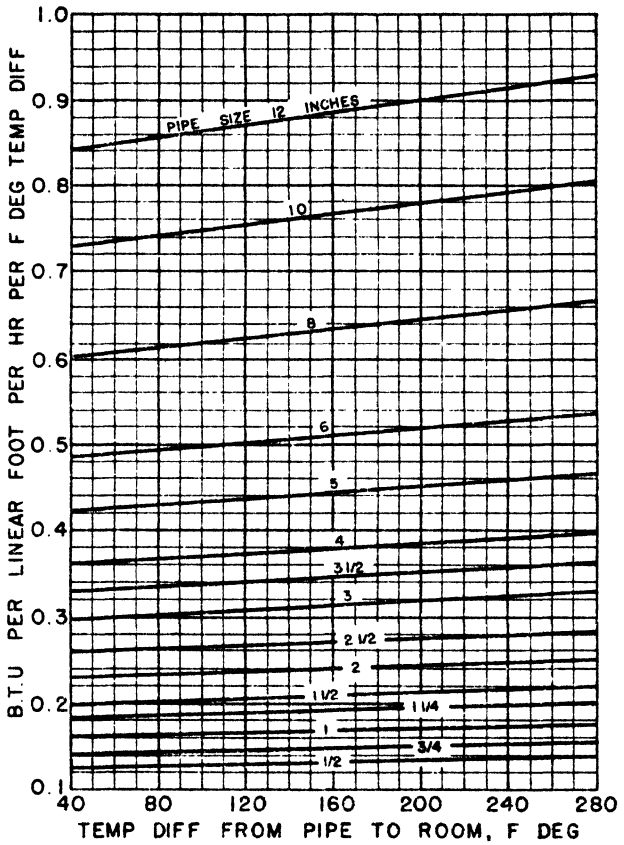


FIG. 2. HEAT LOSS THROUGH 1½ IN. THICK 85 PER CENT MAGNESIA TYPE COVERING

transferred per square foot of outer surface of the insulation is given by the equation:

$$q_o = \frac{k\,(t_1 - t_2)}{r_2 \log_e \frac{r_2}{r_1}} \qquad (1)$$

where

q_o = Btu per (hour) (square foot of outer surface of insulation).

r_1 = outer radius of pipe or inner radius of insulation, inches.

r_2 = outer radius of insulation, inches.

k = thermal conductivity of insulation, Btu per (hour) (square foot) (Fahrenheit degree per inch).

t_1 = temperature of inner surface of insulation, Fahrenheit degrees.

t_2 = temperature of outer surface of insulation, Fahrenheit degrees.

It is convenient to work from the outer surface of the insulation, since the loss through the covering must be determined from the outer surface loss by means of surface loss curves such as given in Fig. 4.

After the true heat loss is obtained, the loss per square foot of pipe surface can be calculated from the relationship:

$$q_i = q_o (r_2/r_1).$$

where

q_i = Btu per (hour) (square foot outer surface of pipe).

The heat loss through two or more thicknesses of insulation applied to a pipe can be calculated by means of the equation:

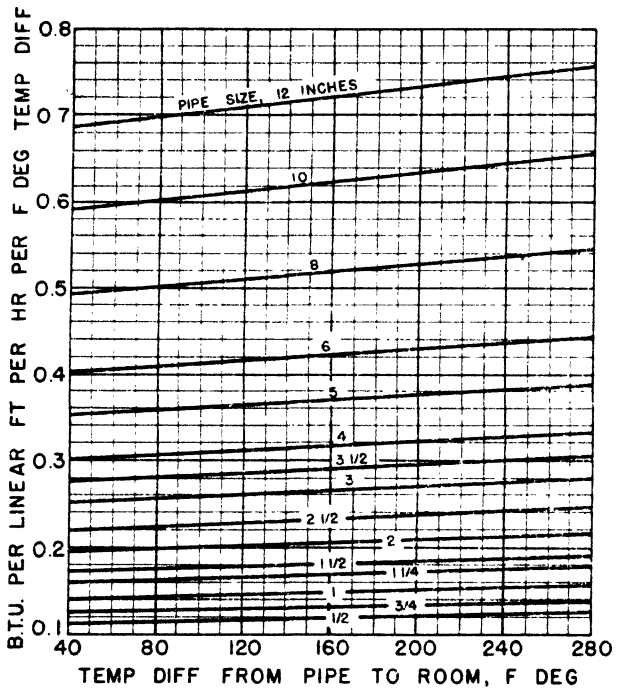


FIG. 3. HEAT LOSS THROUGH 2 IN. THICK 85 PER CENT MAGNESIA TYPE COVERING

$$q_o = \frac{t_1 - t_2}{\frac{r_s \log_e \frac{r_2}{r_1}}{k_1} + \frac{r_s \log_e \frac{r_3}{r_2}}{k_2} + \ldots} \qquad (2)$$

where

r_s = outer radius of second layer of insulation, inches.

r_s = outer radius of last layer of insulation, inches.

The method of solving Equation 2, which is the most difficult of the two, is given in Example 3.

Example 3. Compute the heat loss per linear foot of pipe surface per hour from a 6-in. pipe, insulated with a 3-in. thickness of diatomaceous silica, and a 2-in. thickness of 85 per cent magnesia. The pipe is operating at a temperature of 1200 F and is exposed to a room temperature of 80 F.

Solution. In figuring the heat loss from Equation 2, it is necessary to first make an assumption for the outer surface temperature t_2 and the temperature between the diatomaceous silica and 85 per cent magnesia insulation, so that the mean temperature of each material can be obtained and the thermal conductivity corresponding to the mean temperature of each material substituted in the formula. First assume an outer surface temperature of 140 F and a temperature of 570 F between the two materials corresponding to a mean temperature of (1200 + 570) ÷ 2 or 885 F for the diatomaceous silica and (570 + 140) ÷ 2 or 355 F for the 85 per cent magnesia insulation. The conductivities of these two materials at mean temperatures of 885 and 355 F interpolated from Table 6 are 0.865 and 0.5 Btu respectively.

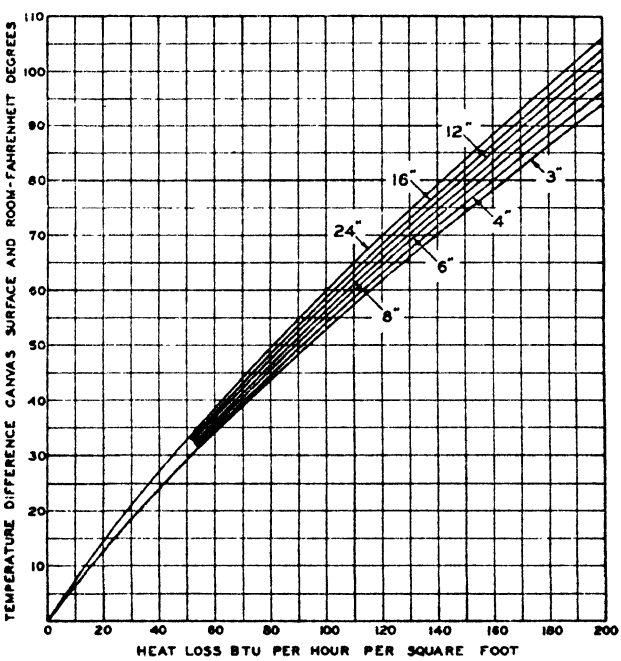


FIG. 4. HEAT LOSS FROM CANVAS-COVERED CYLINDRICAL SURFACES OF VARIOUS DIAMETERS

These values are substituted in Equation 2 and a trial calculation made. For a nominal 6-in. steel pipe $r_1 = 3.312$, $r_2 = 6.312$ and $r_3 = 8.312$ then,

$$q_o = \frac{1200 - 140}{\dfrac{8.312 \log_e \dfrac{6.312}{3.312}}{0.865} + \dfrac{8.312 \log_e \dfrac{8.312}{6.312}}{0.5}} = \frac{1060}{6.2 + 4.58} = 98.3 \text{ Btu.}$$

The temperature drop from the outer surface of the insulation to the surrounding air for a heat loss of 98.3 Btu is found from Fig. 4 to be 57 F for a 16-in. O.D. cylindrical surface, or 57 + 80 F room temperature = 137 F surface temperature. Since a surface temperature of 140 F was assumed, it is evident that a temperature closer to 137 F, or, for instance, 138 F should be used for recalculation:

$$q_o = \frac{1200 - 138}{6.2 + 4.58} = 98.4 \text{ Btu.}$$

Since the temperature drop through each material is equal to the heat flow times the actual resistance of each material the temperature drop through the diatomaceous silica is 98.4 × 6.2 = 610 F or the temperature between the two insulating materials is

(1200 − 610) = 590 F. Since a temperature of 570 F between the two materials was assumed, it is obvious that a temperature closer to 590, or for instance 586 F may be selected. The mean temperatures of the two insulations corresponding to the new assumptions are (1200 + 586) ÷ 2 = 893 and (586 + 138) ÷ 2 = 362 and the interpolated conductivities corresponding to the new mean temperatures are 0.87 and 0.505 for the diatomaceous silica and 85 per cent magnesia respectively. By substituting in Equation 2:

$$q_o = \frac{1200 - 138}{\frac{5.36}{0.87} + \frac{2.29}{0.505}} = \frac{1062}{6.16 + 4.53} = 99.3 \text{ Btu}$$

Again referring to Fig. 4, it is seen that the temperature drop from the outer surface of the insulation to the surrounding air for a heat loss of 99.3 Btu = 38 F which corresponds to the surface temperature of 138 F last assumed. The temperature drop through the diatomaceous silica is 99.3 × 6.16 = 612 F, corresponding to a temperature of 588 F between the two materials which checks very closely with the temperature of 585 F last assumed. The heat loss is therefore 99.3 × 8.312 ÷ 3.312 or 249 Btu per square foot of pipe surface. Since the surface area per linear foot of 6-in. pipe is 1 734 sq ft (Table 5), the heat loss per linear foot of pipe will be 249 × 1.734 = 432 Btu per hour.

The rate of heat loss from a surface maintained at constant temperature is greatly increased by air circulation over the surface. In the case of well-insulated surfaces, the increases in losses due to air velocity are very small as compared with increases from bare surfaces, because of the fact that air flowing over the surface of the insulation can increase only the conductance of heat from surface to air, and cannot change the internal conductance of the insulation itself. The maximum increase in heat loss due to air velocity ranges from about 15 per cent in the case of 1-in. thick insulation, to about 5 per cent in the case of 3-in. thick insulation, provided that the insulation is thoroughly sealed so that air can flow only over the surface. If the conditions are such that the air may circulate through cracks and crevices in the insulation, the increases may be far greater than those given. Therefore, it is essential that insulation be applied in such a manner that air circulation within it or between it and the pipe is avoided.

Fig. 4 shows the loss of heat from canvas-covered, cylindrical surfaces of various outside diameters when the surface to air temperature difference is low. The data are from tests made at Mellon Institute.

The frequent practice of omitting insulation on that portion of a pipe which passes through a masonry wall or which may be in contact with other metals should be avoided. Physical contact between the pipe surface and other structural materials of high thermal conductivity will result in heat transfer much greater than that shown in Tables 1 and 2 for transfer from bare pipe to air.

The saving due to use of insulation on piping is illustrated in *Example 4*.

Example 4. If the steam line given in *Examples 1* and *2* is covered with 1 in. thick 85 per cent magnesia, determine the resulting total annual loss through the insulation. Also compute the monetary value of the annual saving and the percentage of saving over the heat loss from the bare pipe.

Solution. By referring to Fig. 1, the coefficient for 1 in. magnesia on a 2-in. pipe is found to be 0.300 Btu per (hour) (linear foot of pipe) (degree temperature difference) at a temperature difference of 169.4 F. The total hourly loss per linear foot of pipe will then be 0.300 × 169.4 = 50.8 Btu. The total annual loss through the insulation = 50.8 × 165 (linear feet) × 4000 (hours) = 33,500 Mb. The annual bare pipe loss as determined in the solution of *Example 1* was found to be 181,600 Mb. The saving due to insulation is then 181,600 − 33,500 = 148,100 Mb per year.

From the solution of *Example 2*, it was found that the heat supplied to the system cost $0.804 per thousand Mb. Therefore, the monetary value of the saving = 0.804 (dollars) × 148.1 (thousand Mb) = $119.07, or 81.5 per cent of the cost when using uninsulated pipe.

LOW TEMPERATURE PIPE INSULATION

Surfaces maintained at temperatures lower than the surrounding air are insulated to reduce the flow of heat and to prevent condensation. The insulating material should absorb a minimum amount of moisture, because the absorption of moisture substantially increases the conductivity of the material. This property is particularly important in the

TABLE 8. HEAT GAINS FOR INSULATED COLD PIPES

Rates of heat transmission given in Btu per (hour) (Fahrenheit degree temperature difference between fluid in pipe and surrounding still air)

Based on materials having conductivity, k = 0.30

Nominal Pipe Size (Inches)	Ice Water Thickness			Brine Thickness			Heavy Brine Thickness		
	Thickness of Insulation (Inches)	Btu Per Linear Foot	Btu Per Sq Ft Pipe Surface	Thickness of Insulation (Inches)	Btu Per Linear Foot	Btu Per Sq Ft Pipe Surface	Thickness of Insulation (Inches)	Btu Per Linear Foot	Btu Per Sq Ft Pipe Surface
½	1.5	0.110	0.502	2.0	0.098	0.446	2.8	0.087	0.394
¾	1.6	0.119	0.431	2.0	0.111	0.405	2.9	0.094	0.340
1	1.6	0.139	0.403	2.0	0.124	0.352	3.0	0.104	0.294
1¼	1.6	0.155	0.357	2.4	0.131	0.300	3.1	0.113	0.260
1½	1.5	0.174	0.351	2.5	0.134	0.270	3.2	0.118	0.238
2	1.5	0.200	0.322	2.5	0.151	0.244	3.3	0.134	0.214
2½	1.5	0.228	0.303	2.6	0.170	0.226	3.3	0.147	0.197
3	1.5	0.269	0.293	2.7	0.186	0.202	3.4	0.162	0.176
3½	1.5	0.295	0.282	2.9	0 191	0.183	3.5	0.176	0.167
4	1.7	0.294	0.248	2.9	0.209	0.176	3.7	0.182	0.154
5	1.7	0.349	0.239	3.0	0.241	0.165	3.9	0.202	0.138
6	1.7	0.404	0.233	3.0	0.259	0.150	4.0	0.228	0.130
8	1.9	0.455	0.201	3.0	0.318	0.140	4.0	0.263	0.116
10	1.9	0.559	0.198	3.0	0 383	0.135	4.0	0.309	0.110
12	1.9	0.648	0.194	3.0	0.438	0.131	4.0	0.364	0.108

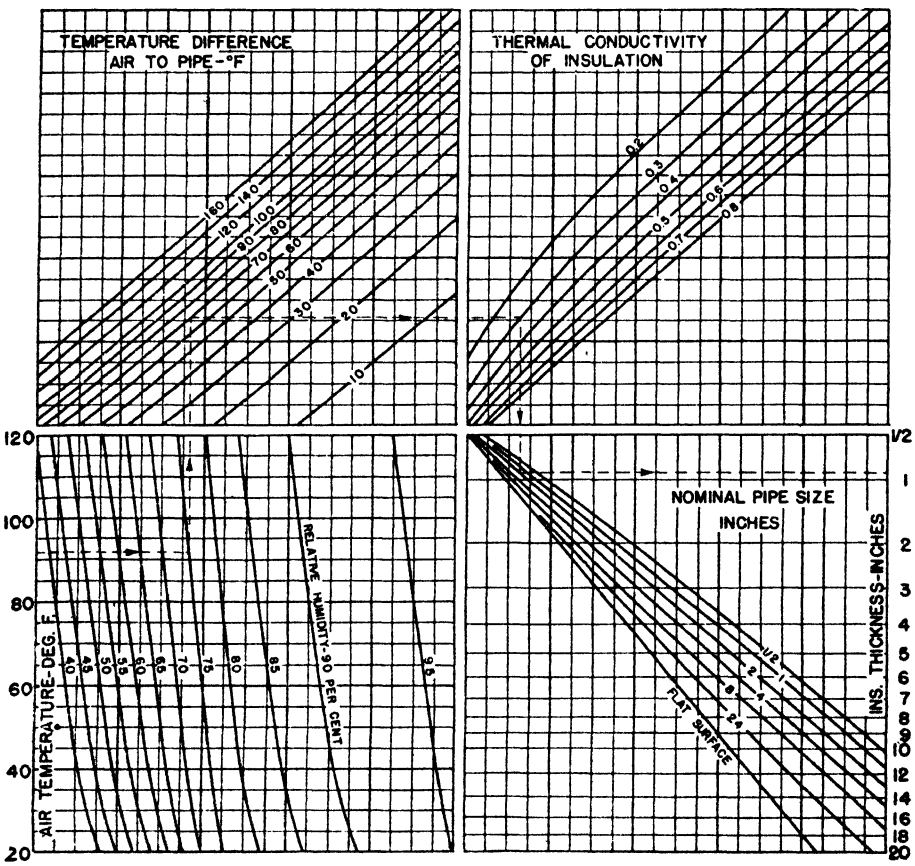
insulation of surfaces that are below the dew-point of the surrounding air. In such cases, due to vapor pressure difference, it is necessary to seal the surface of the insulating material against the penetration of water vapor which would condense within the material, causing a serious increase in heat flow, possible breakdown of the material, and corrosion of metal surfaces: An insulating material with a high degree of moisture absorption might pick up moisture before application and then, when the seal is in place and the temperature of the insulated surface reduced, release that moisture to the cold surface. There are a number of methods of producing vapor seals, some of which have been worked out by insulation manufacturers to suit their products and others by applicators and users. Unless time proven methods are known, specifications of insulation manufacturers should be obtained and followed carefully.

The thickness of insulation required to prevent condensation on the outer surface is that thickness which will raise the temperature of the outer surface of the insulation to a point slightly higher than the dew-point of the surrounding vapor. The dew-point for various humidities can be readily ascertained from a psychrometric chart.

The approximate required thickness of insulation to prevent condensation on pipes and flat metallic surfaces may be obtained from Fig. 5 in which a surface resistance of 0.606 corresponding to a film conductance of

1.65, was used in calculating the curves. This value provides a slight factor of safety and its use is known to give satisfactory field results. In using the chart it is advisable to specify the next thicker, rather than the next thinner, commercial insulation in cases where an intermediate thickness is indicated.

Heat gains for pipes insulated with a material having an installed conductivity of 0.30 Btu per (square foot) (hour) (Fahrenheit degree per inch) are given in Table 8. This table may be used for any of the com-



[a] Solve problems as indicated by dotted line, entering chart at lower left-hand scale.

FIG. 5. THICKNESS OF PIPE INSULATION TO PREVENT CONDENSATION ON OUTER SURFACE[a]

mercial insulations offered for this purpose since they have conductivities very near the 0.3 value used.

INSULATION OF PIPES TO PREVENT FREEZING

If the surrounding air temperature remains sufficiently low for an ample period of time, insulation cannot prevent the freezing of still water, or of water flowing at such a velocity that the quantity of heat carried in the water is not sufficient to take care of the heat losses which will result and cause the temperature of the water to be lowered to the freezing point.

Insulation can materially prolong the time required for the water to give up its heat, and if the velocity of the water flowing in the pipe is maintained at a sufficiently high rate, freezing may be prevented.

Table 9 may be used for making estimates of the thickness of insulation necessary to take care of still water in pipes at various water and surrounding air temperature conditions. Because of the damage and service interruptions which may result from frozen water in pipes, it is essential that an efficient insulation be utilized. This table is based on the use of a material having a conductivity of 0.30. The initial water temperature is assumed to be 10 F above, and the surrounding air temperature 50 F below the freezing point of water (temperature difference, 60 F).

The last column of Table 9 gives the minimum quantity of water at initial temperature of 42 F which should be supplied every hour for each

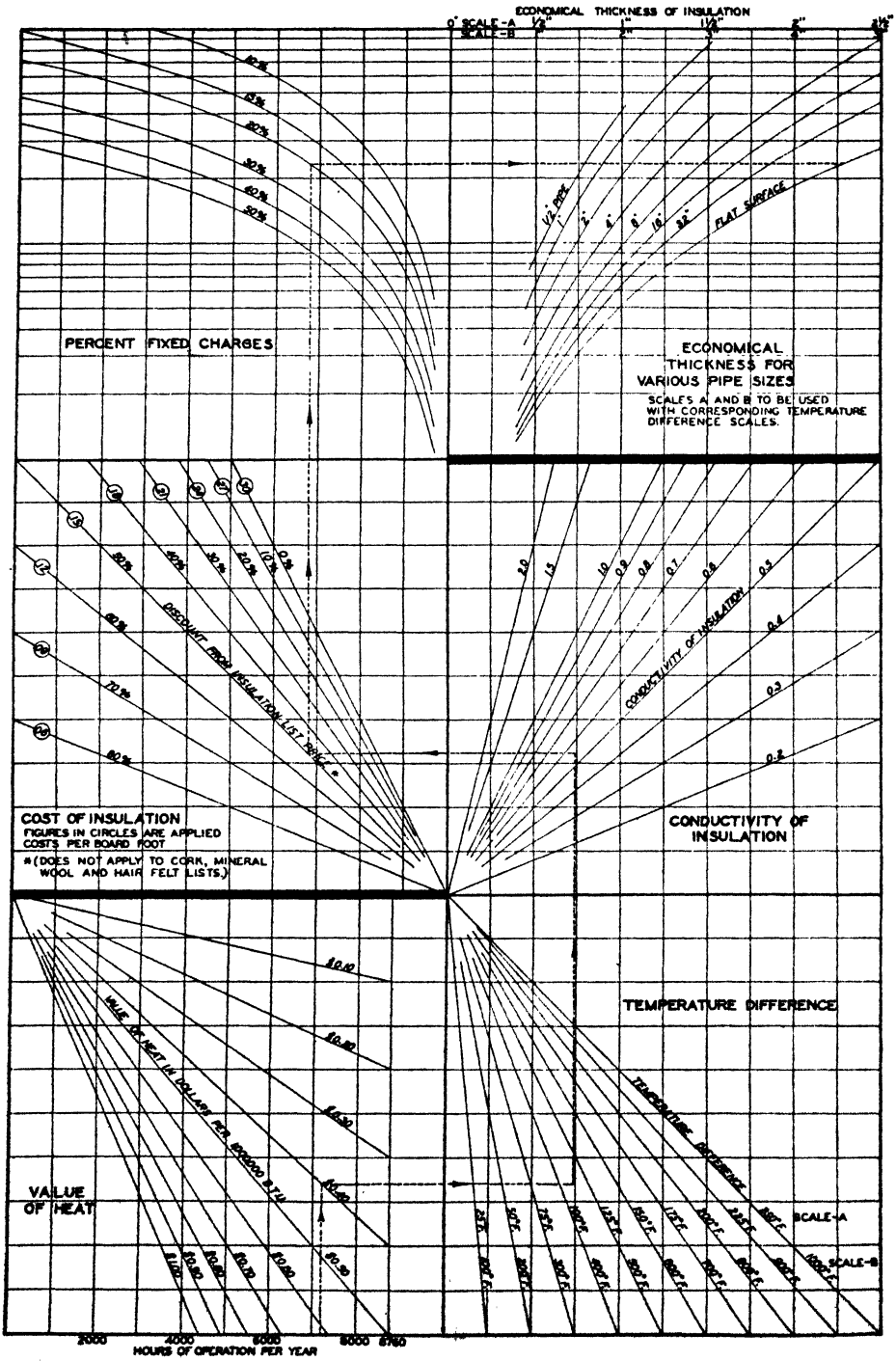
TABLE 9. DATA FOR ESTIMATING REQUIREMENTS TO PREVENT FREEZING OF WATER IN PIPES WITH SURROUNDING AIR AT −18 F

NOMINAL PIPE SIZE (INCHES)	NUMBER OF HOURS TO COOL 42 F WATER TO FREEZING POINT			WATER FLOW REQUIRED AT 42 F TO PREVENT FREEZING, POUNDS PER LINEAR FOOT OF PIPE PER HOUR		
	Thickness of Insulation in Inches (Conductivity, k = 0.30)					
	2	3	4	2	3	4
½	0.42	0.50	0.57	0.54	0.45	0.40
1	0.83	1.02	1.16	0.68	0.55	0.48
1½	1.40	1.74	2.02	0.84	0.68	0.58
2	1.94	2.48	2.90	0.95	0.75	0.64
3	3.25	4.27	5.08	1.24	0.94	0.79
4	4.55	6.02	7.20	1.47	1.11	0.93
5	5.92	7.96	9.69	1.73	1.29	1.06
6	7.35	9.88	12.20	1.98	1.46	1.19
8	10.05	13.90	17.25	2.46	1.78	1.43
10	13.00	18.10	22.70	2.96	2.12	1.70
12	15.80	22.20	28.10	3.43	2.45	1.93

linear foot of pipe, in order to prevent the temperature of the water from being lowered to the freezing point. The weights given in this column should be multiplied by the total length of the exposed pipe line expressed in feet. As an additional factor of safety, and in order to provide against temporary reductions in flow occasioned by reduced pressure, it is advisable to double the rates of flow listed in the table. It must be emphasized that the flow rates and periods of time designated apply only for the conditions stated. To estimate for other service conditions the following method of procedure may be used.

If water enters the pipe at 52 F instead of 42 F, the time required to cool it to the freezing point will be prolonged to twice that given in the table, or the rate of flow of water may be reduced so that the quantity required will be one-half that shown in the last column of Table 9. However, if the water enters the pipe at 34 F it will be cooled to 32 F in one-fifth of the time given in the table. It will then be necessary to increase the rate of flow so that five times the specified quantity of water will have to be supplied in order to prevent freezing.

If the minimum air temperature is −38 F (temperature difference 80 F) instead of −18 F, the time required to cool the water to the freezing point will be 60/80 of the time given in the table, or the necessary quantity of water to be supplied will be 80/60 of that given.



(L. B. McMillan, *Proc. National District Heating Association*, Vol. 18, p. 136).

FIG. 6. CHART FOR DETERMINING ECONOMICAL THICKNESS OF PIPE INSULATION

In making calculations to arrive at the values given in Table 9, the loss of heat stored in the insulation, the effect of a varying temperature difference due to the cooling of pipe and water, and the resistance of the outer surface of the insulation to the transfer of heat to the air have all been neglected. When these factors enter into the computations it is necessary to enlarge the factor of safety. Also as stated, the time shown in the table is that required to lower the water to the freezing point. A longer period would be required to freeze the water but the danger point is reached when freezing starts. The flow of water will stop and the entire line will be in danger as soon as the water freezes across the section of the pipe at any point.

When water must remain stationary longer than the times designated in Table 9, the only safe way to insure against freezing is to install a steam or hot water line or to place an electric resistance heater along the side of the exposed water line. The heating system and the water line are then insulated so that the heat losses from the heating system are not excessive, and the heating effect is concentrated against the water pipe where it is needed. For this form of protection 2 in. of an efficient insulation may be applied.

TABLE 10. THICKNESS OF PIPE INSULATION ORDINARILY USED INDOORS[a]

STEAM PRESSURE PSIG OR CONDITION	STEAM TEMPERATURE FAHRENHEIT DEGREES	THICKNESS OF INSULATION		
		Pipes Larger Than 4 In.	Pipes 2 In. to 4 In.	Pipes ½ In. to 1½ In.
0 to 25	212 to 267	1 in.	1 in.	1 in.
25 to 100	267 to 338	1½ in.	1 in.	1 in.
100 to 200	338 to 388	2 in.	1½ in.	1 in.
Low Superheat	388 to 500	2½ in.	2 in.	1½ in.
Medium Superheat	500 to 600	3 in.	2½ in.	2 in.
High Superheat	600 to 700	3½ in.	3 in.	2 in.

[a]All piping located outdoors or exposed to weather is ordinarily insulated to a thickness ½ in. greater than shown in this table, and covered with a waterproof jacket.

ECONOMICAL THICKNESS OF PIPE INSULATION

The thicknesses of insulation which ordinarily are used for various temperature conditions are given in Table 10. Where a thorough analysis of economic thickness is desired this may be accomplished through the use of the chart, Fig. 6.

The dotted line on the chart illustrates its use in solving a typical example. In using the chart, start with the scale at the left bottom margin representing the given number of hours of operation per year; then proceed vertically to the line representing the given value of heat; thence horizontally to the right, to the line representing the given temperature difference; thence vertically to the line representing the conductivity of the given material; thence horizontally, to the left, to the line representing the given discount on that material; thence vertically to the curve representing the required per cent return on the investment; thence horizontally to the right, to the curve representing the given pipe size; thence vertically to the scale at the top right margin where the economical thickness may be read off directly.

UNDERGROUND PIPE INSULATION

Underground steam distribution lines are carried in protective structures of various types, sizes and shapes (See Chapter 29). Detailed data

TABLE 11. THICKNESS OF LOOSE INSULATION FOR USE AS FILL IN UNDERGROUND CONDUIT SYSTEMS

STEAM PRESSURE PSIG OR CONDITION	STEAM TEMPERATURE FAHRENHEIT DEGREES	MINIMUM THICKNESS OF INSULATION IN INCHES					MINIMUM DISTANCE BETWEEN STEAM AND RETURN
		STEAM LINES			RETURN LINES		
		Pipes Less than 4 In.	Pipes 4 In. to 10 In.	Pipes Larger than 12 In.	Pipes Less than 4 In.	Pipes 4 In. and Larger	
Hot Water, or 0 to 25	212 to 267	1½	2	2½	1¼	1½	1
25 to 125	267 to 352	2	2½	3	1¼	1½	1¼
Above 125, or superheat	352 to 500	2½	3	3½	1¼	1½	1½

on commonly used forms of tunnels and conduit systems have been published by the *National District Heating Association* [2].

Pipes in tunnels are covered with sectional insulation to provide maximum thermal efficiency and are also finished with good mechanical protection in the form of metal or waterproofing membrane outer jackets. In some instances, where actual submersion of hot lines may occur it has been found good practice to firmly secure the covering with corrosion resistant wire, then sew on a wire-inserted asbestos fabric jacket with wire. This jacket is porous. The principle of withstanding submersion is that water may enter as water, then actually boil at the pipe surfaces and escape as steam without rupturing the insulation or jacket. Conduit systems are in more general use than tunnels. Pipes carried in conduits may be insulated with sectional insulation; however, the more usual practice is to fill the entire section of the conduit around the pipes with high quality, loose insulating material. The insulation must be kept dry at all times, and for this purpose effective waterproofing membranes enclose the insulation. A drainage system is also provided to divert water which may tend to enter the conduit.

The economical thickness of insulation for underground work is difficult to determine accurately due to the many variables which have to be considered. As a result of theories [3] previously developed, together with other experimental data which have been presented, the usual endeavor is to secure not less than 90 per cent efficiency for underground piping. Table 11 can be used as a guide in arriving at the minimum thickness of loose insulation fills to use for laying out conduit systems. Other factors such as the number of pipes and their combination of sizes, as well as the standard conduit sizes, are primary controlling factors in the amount and thickness of insulation for use.

When sectional insulation is applied to lines in tunnels or conduits, usual practice is to apply the most efficient materials ½ in. less in thickness than that determined by the use of Fig. 6. The data in Fig. 6 are based on conditions of insulation exposed to the air, whereas normal ground temperature is substituted for air temperature in determining the temperature difference for use with the chart when applying it for underground pipe line estimates.

REFERENCES

1—Heat Loss from Copper Piping, by R. H. Heilman (*Heating, Piping and Air Conditioning*, September, 1933, p. 458).

2—Handbook of the *National District Heating Association*, Second Edition, 1932.

3—Theory of Heat Losses from Pipes Buried in the Ground, by J. R. Allen (A.S.H.V.E. TRANSACTIONS Vol. 26, 1920, p. 335).

Chapter 29

DISTRICT HEATING

Steam Distribution Piping, Selection of Pipe Sizes, Conduits for Piping, Pipe Tunnels, Overhead Distribution, Inside Piping, Metering, Steam Requirements, Rates, Utilization, Automatic Temperature Control

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THE term *district heating* refers to the heating of several buildings from a central plant as in the heating of portions of cities, and is also used in connection with the heating of groups of buildings as in institutions and factories. It is usually preferable, in a group of industrial or institutional buildings, that they be heated from a central plant rather than by individual plants. Fuel can generally be burned more efficiently, less labor is required, and often a central plant is cheaper to install. Those phases of district heating which frequently fall within the province of the heating engineer are outlined here with data and information for solving incidental problems in connection with institutions and factories. Some data are included to cover the piping peculiar to heating systems which are to be supplied with purchased steam. A complete district heating installation should not be attempted without a thorough study of the entire problem by men competent and experienced in that industry.

STEAM DISTRIBUTION PIPING

The methods used in district heating work for the distribution of steam are applicable to any problem involving the supply of steam to a group of buildings. The first step is to establish the route of the pipes, and in this matter since the local conditions control the layout little can be said regarding it.

Having established the route of the pipes, the next step is to calculate the pipe sizes. In district heating work it is common practice to design the piping system on the basis of pressure drop. The initial pressure and the minimum permissible terminal pressure are specified and the pipe sizes are so chosen that the required amount of steam, with suitable allowances for future increases, will be transmitted without exceeding this pressure drop. The steam velocity is therefore almost disregarded and may reach a very high figure. Velocities of 35,000 fpm are not considered high. By the use of this method the pipe sizes are kept to a minimum with consequent savings in investment.

The steam flowing through any section of the piping can be computed from a study of the requirements of the several buildings served. In general a condensation rate of 0.25 lb per (hour) (square foot of equivalent direct radiation) is a safe figure. This allows for line condensation which, however, is a small part of the total at times of maximum load. Miscellaneous steam requirements such as laundry, cooking, or process should be individually calculated. The steam requirements for water heating should be taken into account, but in most types of buildings this load will be relatively small compared with the heating load and will seldom occur at the time of the heating peak. Unusual features such as large heaters for swimming pools should not be overlooked.

The pressure at which the steam is to be distributed will depend upon (1) boiler pressure, (2) whether exhaust or live steam, (3) pressure requirements of apparatus to be served. If steam has been passed through

electrical generating units, the pressure will be considerably lower than if live steam, direct from the boilers, is used.

The advantages of low pressure distribution (2 to 30 psi) are (1) smaller heat loss per square foot of pipe surface, (2) less trouble with traps and valves, (3) simpler problems in pressure reduction at the buildings, and (4) general reduction in maintenance costs. With distribution pressures not exceeding 40 psi there is little danger even if the full distribution pressure should build up in the radiators through the faulty operation of

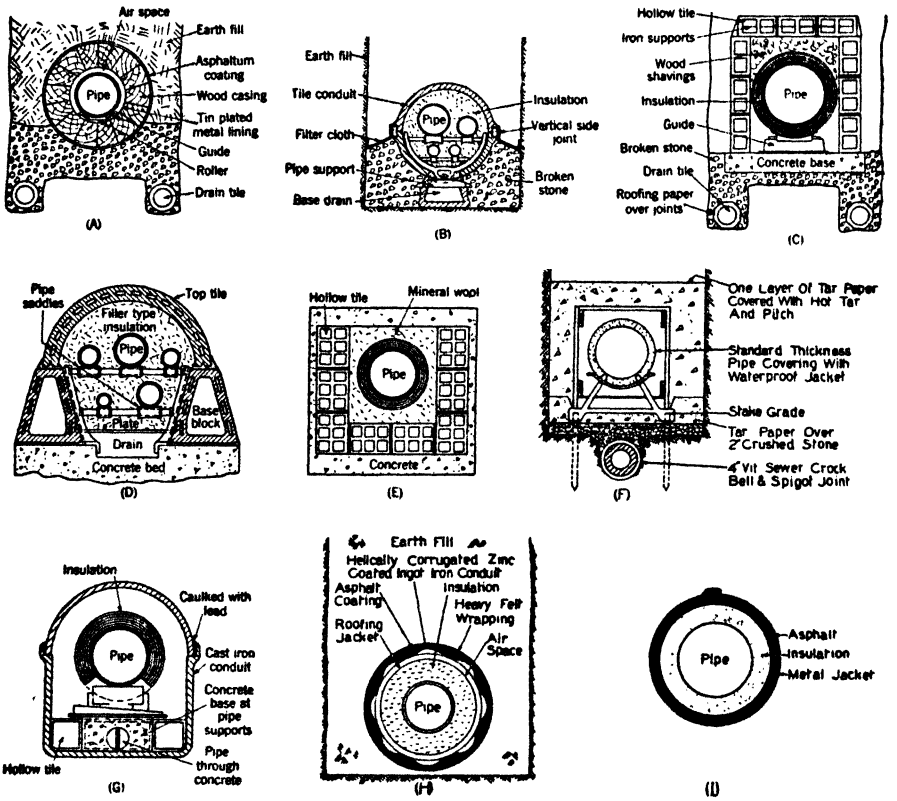


FIG. 1. CONSTRUCTION DETAILS OF CONDUITS COMMONLY USED

a reducing valve; but with pressures higher than 50 psi a second reducing valve or some form of emergency relief is usually desirable to prevent excessive pressures in the radiators.

The advantages of high pressure distribution are (1) smaller pipe sizes and (2) greater adaptability of the steam to various operations other than building heating, (3) wider flexibility as to allowance for maximum pressure drop and ability to serve equipment requiring higher pressures.

Frequently the different kinds of apparatus which must be served require various minimum pressures. Kitchen equipment requires from 5 to 15 psi, the higher pressures being necessary for apparatus in which water is boiled, such as stock kettles and coffee urns. An increased amount of heating surface, which is easily obtained in some kinds of apparatus, results in quicker and more satisfactory operation at low pressures. For laundry equipment, particularly the mangle, a pressure

of 75 psi is usually demanded although 30 psi is sufficient if the flat work ironer is equipped with a large number of rolls and if a slower rate of operation is permissible. Pressing machines and hospital sterilizers require about 50 psi. Where pressures are not as high as desired higher pressures can be obtained by a steam compressor.

PIPE SIZES

The lengths of pipe, steam quantities, and initial and terminal pressures having been chosen, the pipe sizes can readily be calculated by means of Babcock's pressure drop formula:

$$P = 0.0000000367 \left(1 + \frac{3.6}{D}\right) \frac{W^2 L}{d D^5}$$

$$W = 5220 \sqrt{\frac{P d D^5}{\left(1 + \frac{3.6}{D}\right) L}}$$

Numerical values of the various factors are given in Table 2, Chapter 23.

CONDUITS FOR PIPING

Conduits for steam pipes buried underground should be reasonably waterproof, able to withstand earth loads and to take care of the expansion and contraction of the piping without strain or stress on the couplings, or without affecting the insulation or conduit. Expansion of the piping must be carefully controlled by means of anchors and expansion joints or bends so that the pipes can never come in contact with the conduit. Anchors can be anchor fittings or U-shaped steel straps which partially encircle the pipes and are firmly bolted to a short length of structural or cast steel set in concrete. In general, cast steel is preferable to structural steel.

Important points in laying out underground conduits are:

1. The depth of the buried conduit should be kept at a minimum. Excavation costs are a large factor in the total cost.

2. An expansion joint, offset, or bend should be placed between each two anchors. Advantage should be taken of the flexibility of piping to absorb expansion wherever possible. Information on provisions for expansion will be found in Chapter 27.

3. A proper hydrostatic test should be made on the assembled line before the insulation and the top of the conduit are applied. The hydrostatic test pressure should be one and one-half times the maximum service pressure and it should be held for a period of at least two hours without evidence of leakage.

There are many types of conduits, some of which are manufactured products and some of which are built in the field. Some of the more common forms are illustrated in Fig. 1.

The conduit (A) is of a wood casing construction which has been widely used in the past. The wood casing is segmented, lined with tin, and bound with wire. The outside of the conduit is coated with asphaltum. It is not suitable for high temperatures or poorly drained soils.

In Fig. 1 (B), (C), (D), (H) and (I) are patented forms of conduits. The insulation is sometimes a loose filler packed into the conduit. Conduits (H) and (I) are prefabricated. Both of these conduits are enclosed in metal jackets.

At (C) and (E) are shown two tile conduits using sectional insulation. In these particular designs the space surrounding the pipe is filled partially or wholly with a loose insulating material. The addition of this

loose insulating material to the sectional insulation is, of course, optional and is justified only where high pressure steam is used.

(E) and (F) are conduits used by two district heating companies, and have the advantage of being constructed of common materials.

Conduit (G) is of cast-iron construction, assembled with lead joints and is water-tight, if properly laid. It is obviously expensive and is justified only in exceptional cases.

Since it is difficult to make a concrete or masonry conduit absolutely water-tight, provision should be made for some seepage. The pipe should be protected by a waterproof jacket over the insulation and the seepage drained from the inside of the conduit. Underdrainage of the conduit is

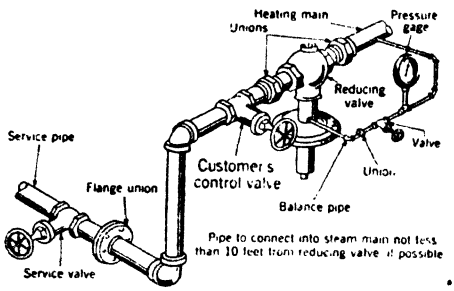


FIG. 2. CONNECTIONS FOR REDUCING VALVE WITHOUT BYPASS

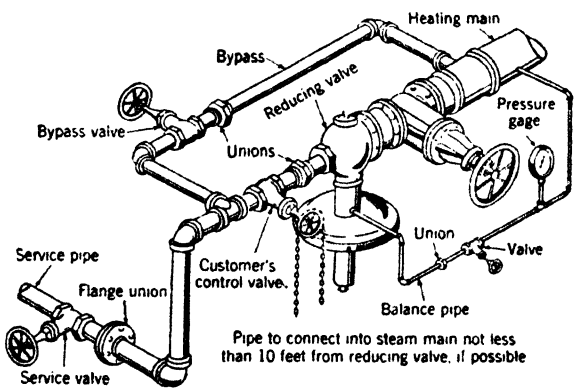


FIG. 3. CONNECTIONS FOR REDUCING VALVE WITH BYPASS

generally provided for by a tile drain laid in crushed stone or gravel underneath the conduit. The tile underdrain should be carried to the sewer or some other drainage point. Manholes are required at intervals for access to valves, traps, and some types of expansion joints.

Where steam and return piping are installed in the same conduit, the return piping usually follows the same grade as the steam piping. In general, the condensation is pumped back under pressure.

Where it is possible to use basement or sub-sidewalk space for the distribution piping the cost of installation and maintenance is greatly reduced.

PIPE TUNNELS

Where steam heating lines are installed in tunnels large enough to provide walking space, the pipes are supported by means of hangers or

roller frames on brackets or frame racks at the side or sides of the tunnel. The pipes are insulated with sectional pipe insulation over which is placed a sewed-on, painted canvas jacket or a jacket of asphalt-saturated asbestos water-proofing felt. The tunnel itself is usually built of concrete or brick and water-proofed on the outside with membrane water-proofing.

Because of their relatively high first cost as compared with smaller conduits, walking tunnels are sometimes omitted along heating lines unless they are required to accommodate miscellaneous other services or provide underground passage between buildings.

OVERHEAD DISTRIBUTION

In some industrial and institutional applications, the distribution piping may be installed, entirely or in part, above ground. This method

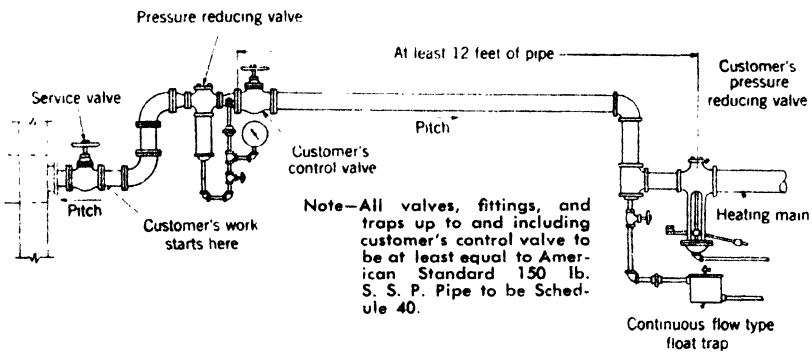


FIG. 4. STEAM SUPPLY CONNECTION WHEN USING TWO REDUCING VALVES

of construction has the advantage of requiring no excavation and being easily maintained.

INSIDE PIPING

Figs. 2 and 3 show typical service connections used for low pressure steam service.

Fig. 2 shows installation of a reducing valve without a bypass, which is usually omitted in the case of smaller size valves.

Fig. 3 illustrates the use of a reducing valve, with a bypass which is generally provided for larger installations. This latter construction permits the operation of the line in case of failure in the reducing valve. In the smaller sizes, the reducing valve can be removed, a filler installed, and the house valve used to throttle the flow of steam until repairs are made.

Fig. 4 shows a typical installation used for high pressure steam service[1]. The first reducing valve effects the initial pressure reduction. The second reducing valve reduces the steam pressure to that required.

In a heating system the pipes carrying condensate are more subject to corrosion than other parts of the system. Care must be taken to give proper pitch to the pipes and provide proper venting of non-condensable gases. (See Chapter 51, Corrosion).

Most district heating companies enforce certain regulations regarding the consumer's installation, partly to safeguard their own interests but principally to insure satisfactory and economical service to the consumer.

There are certain fundamental principles that should be followed in the design of a building heating system which is to be supplied from street mains. Although some of these apply to any building, they have been demonstrated to be especially important when steam is purchased.

1. Provision should be made for conveniently shutting off the steam supply at night and at other times when heat is not needed.

It has been thoroughly demonstrated that a considerable amount of heat can be saved by shutting off steam at night. Although there is, in some cases, an increased consumption of heat when steam is again turned on in the morning, there is a large net saving which may be explained by the fact that the lower inside temperature maintained during the night obviously results in lower heat loss from the building, and less heat need therefore be supplied.

Steam can be entirely shut off at night in most buildings even in very cold weather without endangering plumbing. It is necessary, however, to have an ample amount of heating surface so that the building can be quickly warmed in the morning. Where the

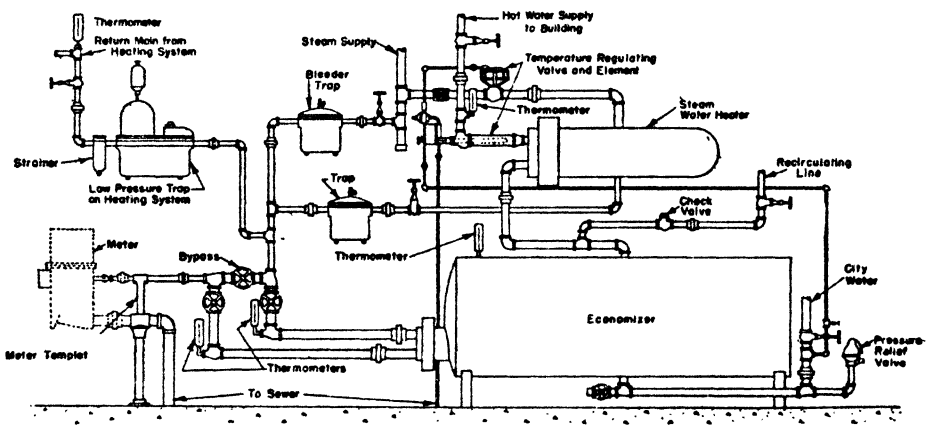


FIG. 5. METHOD OF INSTALLING A WATER HEATER AND ECONOMIZER IN A GRAVITY HEATING SYSTEM

hours of occupancy differ in various parts of the building, it is good practice to install separate supply pipes to the different parts. For example, in an office building with stores or restaurants on the first floor which are open in the evening, a separate main supplying the first floor will permit the steam to be shut off from the remainder of the building in the late afternoon. The division of the building into zones each with a separately controlled heat supply is sometimes desirable, as it permits the heat to be adjusted according to variations in sunshine and wind.

2. Residual heat in the condensate should be salvaged.

This heat may be salvaged by means of a cooling coil, or as is more frequently done, by a water heating economizer (see Fig. 5) which preheats the hot water supply to the building.

The condensate from the heating system, after leaving the trap, passes through the economizer. The supply to the hot water heater passes through the economizer, absorbing heat from the condensate. If the hot water system in the building is of the recirculating type, the recirculating connection should be tied in *between* the economizer and the water heater proper, not at the economizer inlet, because the recirculated hot water is itself at a high temperature.

Because of the lack of coincidence between the heating system load and the hot water demand, a greater amount of heat can be extracted from the condensate if storage capacity is provided for the preheated water. Frequently a type of economizer is used in which the coils are submerged in a storage tank.

3. Heat supply should be graduated according to variations in the outside temperature.

The maximum in economical operation and satisfactory heating can only be obtained by the use of some automatic temperature control system.

METERING

The perfection of fluid meters has contributed as much to the advancement of district heating as any other one thing. Meters are classified into two groups: *Condensate Meters* and *Rate of Flow Meters.*

Condensate Meters

The one type of quantity meter used is the condensate meter, which may be of the *tilting bucket* or *revolving drum* type.

The condensate meter is a popular type for use on small and medium sized installations, where all the condensate can be brought to a common point for metering purposes. Its simplicity of design, ease in testing, accuracy at all loads, low cost, and adaptability to low pressure distribution has made it standard equipment with many heating companies.

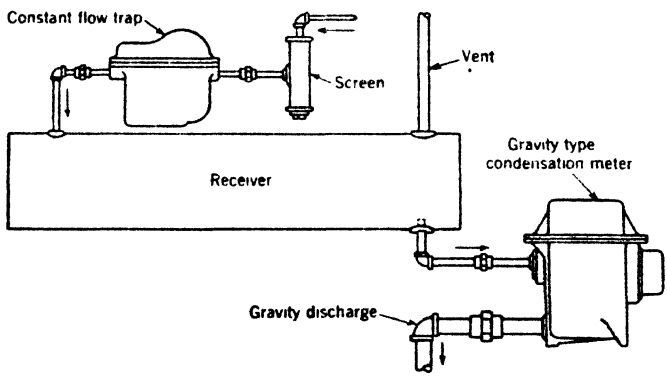


FIG. 6. GRAVITY INSTALLATION FOR CONDENSATION METER USING VENTED RECEIVERS

Condensate meters should not be operated under pressure; they are made for either gravity or vacuum installations. Where bucket traps are used, a vented receiver is essential ahead of the meter. Where continuous flow traps are used, a vented receiver is not necessary, but is desirable. Fig. 6 illustrates a gravity condensate meter installation using a vented receiver.

Rate of Flow or Flow Meters

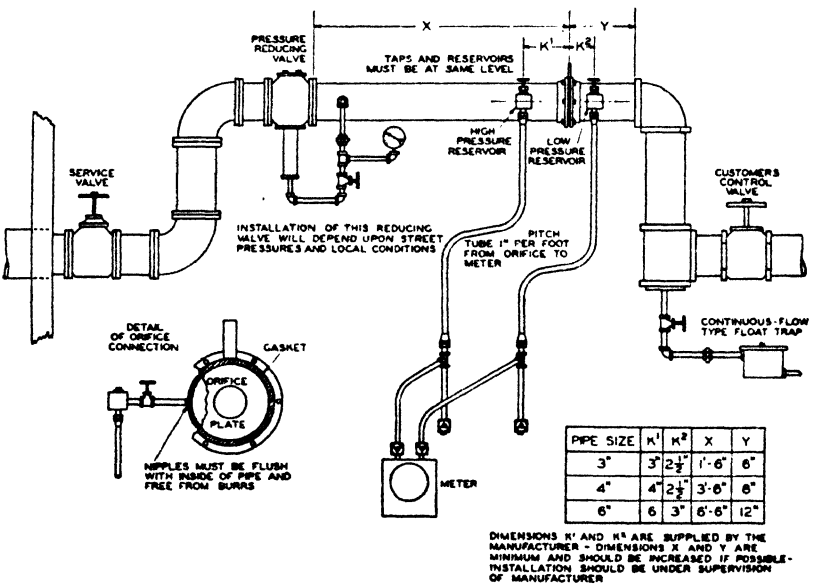
Flow meters used for district heating work are of three types: *Area Meters, Head Meters* and *Velocity Meters.* (See Chapter 4, Fluid Flow).

Area meters are those, in the operation of which, a variation in the cross-section of stream under constant head is used as an indication of the rate of flow. A tapered plug is suspended in an orifice and moves axially with the flow, which is vertically upward. The weight of the plug provides a definite pressure differential and the plug floats at such a height as will provide enough orifice area to pass the flow at the pressure difference. The position of the plug is transmitted by means of a lever and pencil and records the flow on a graduated strip chart.

Head meters are those in which the stream of fluid creates a difference of pressure, or differential head. This head is created by an orifice,

Venturi tube, flow nozzle, or Pitot tube and will depend upon the velocity and density of the fluid. The secondary element must contain a differential pressure gage, which will translate the pressure difference into rate of flow or total flow. This mechanism may be either mechanical or electrical. The electric flow meter has the advantage of being able to locate the instruments at some distance from the primary element.

Fig. 7 is a typical example of an orifice-type meter installation. A few general points to be considered in installing a meter of this type are: (1) It is desirable to place the differential medium in a horizontal pipe in preference to a vertical one, where either location is available. (2) Reservoirs should always be on the same level and installed in accordance with the instructions of the meter company. (3) The meter body should be placed at a lower level than that of the pressure differential



PIPE SIZE	K¹	K²	X	Y
3"	3"	2½"	1'-6"	6"
4"	4"	2½"	3'-6"	6"
6"	6	3"	6'-6"	12"

FIG. 7. ORIFICE METER STEAM SUPPLY CONNECTION

medium. Special instructions are furnished where the meter body is above. (4) Meter piping should be kept free from leaks. (5) Sludge should not be permitted to collect in the meter body. (6) The meter body and meter piping should be kept above freezing temperatures. (7) It is best not to connect a meter body to more than one service. (8) Special instructions are furnished for metering a turbulent or pulsating flow.

Velocity meters are those in which the primary element is some device that is kept in continual rotation by the linear motion of the stream. The secondary element is, essentially, a revolution counter. The primary and secondary elements are combined into one unit.

For steam metering, the shunt meter is an example of the velocity type. This unit is connected directly in 2, 3 and 4 in. pipe lines. Larger size mains are metered by installing a 2 in. meter in a bypass with a restricting orifice in the main line.

Selection of Meter

In selecting a meter for a particular installation, the number of different makes and types of meters suitable for the job is usually limited by one

or more of the following considerations: (1) Its use in a new or an old installation. (2) Method to be used in charging for the service. (3) Location of the meter. (4) Large or small quantity to be measured. (5) Temporary or permanent installation. (6) Cleanliness of the fluid to be measured. (7) Temperature of the fluid to be measured. (8) Accuracy expected. (9) Nature of flow: turbulent, pulsating, or steady. (10) Cost. *a.* purchase price, *b.* installation cost, *c.* calibration cost, *d.* maintenance cost. (11) Servicing facilities of the manufacturer. (12) Pressure at which fluid is to be metered. (13) Type of record desired as to indicating, recording or totalizing. (14) Stocking of repair parts. (15) Use of open jets where steam is to be metered. (16) Metering to be done by one meter or by a combination of meters. (17) Use as a check meter. (18) Its facilities for determining or recording information other than flow. (19) Whether or not the condensate can be returned to a central point.

STEAM REQUIREMENTS

Methods of estimating steam requirements for heating various types of buildings are given in Chapter 20.

Table 6 in Chapter 20 represents information obtained from all sections of the United States, and the group of buildings from which the information was taken represents a cross-section of all types of heating systems.

Steam requirements for water heating can be satisfactorily estimated by using a consumption of 0.0025 lb per (day) (cubic foot of heated space) for office buildings, without restaurants, and 0.0065 lb per (day) (cubic foot of heated space) for apartment buildings.

Complete information on water heating requirements is given in Chapter 50.

Additional data on steam requirements of various types of buildings in a number of cities may be found in the Handbook of the *National District Heating Association.*

RATES

Fundamentally, district heating rates are based upon the same principles as those recognized in the electric light and power industry, the main object being a reasonable return on the investment. However, there are other requirements to be met; the rate for each class of service should be based upon the cost to the utility company of the service supplied and upon the value of the service to the consumer, and it must be between these two limits. District heating rates should be designed to produce a sufficient return on the investment regardless of weather conditions, although existing rate schedules do not always conform to this principle. Lastly, the rate schedule must be reasonably simple and understandable.

Glossary of Rate Terms

Load Factor. The ratio, in per cent, of the average hourly load to the maximum hourly load. This is usually based on a one year period but may be applied to any specified period.

Demand Factor. The relation between the connected radiator surface or required radiator surface and the demand of the particular installation. It varies from 0.25 to 0.3 lb per (hour) (square foot of surface).

Diversity Factor. The ratio of the sum of the individual demands of a number of buildings to the actual composite demand of the group.

Types of Rates

The various types of rates to be found in use in district heating systems are:

1. Straight-Line Meter Rate. The price charged per unit is constant, and the consumer pays in direct proportion to his consumption without regard to the difference in costs of supplying the individual customers.

2. Block Meter Rate. The pounds of steam consumed by a customer are divided into blocks of thousands of pounds each, and lower rates are charged for each successive block consumed. This type of charge predominates in steam heating rate schedules for it has the advantage of proportioning the bill according to the consumption and the cost of service. It has the disadvantage of not discriminating between customers having a high load factor (relatively low demand) and those having a low load factor (relatively high demand). The utility company must maintain sufficient capacity to serve the high demand customers and the cost of the increased plant investment is divided equally among the users, so the high demand customers are benefited at the expense of the others.

3. Demand Rates. These refer to any method of charge based on a measured maximum load during a specified period of time.

The *flat demand rate* is usually expressed in dollars per thousand pounds of demand per month or per annum. It is based on the size of a customer's installation, and is seldom used except where a meter is not practicable.

The *Wright demand rate* is similar in calculation to the block rate except that it is expressed in terms of hours' use of the maximum demand. It is seldom used but forms the basis for other forms of rates.

The *Hopkinson demand rate* is divided into two elements:

(*a*) A charge based upon the demand, either estimated or measured.

(*b*) A charge based upon the amount of steam consumed.

This rate may be modified by dividing the quantities of steam demanded and consumed into blocks charged for at different rates.

The *Doherty rate* is divided into three elements:

(*a*) A charge based upon demand.

(*b*) A charge based upon steam consumed.

(*c*) A customer charge.

In the *Hopkinson rate*, the last two elements are combined into one element.

Demand rates are comparatively new and are not yet widely used; though they are equitable and competitive they are difficult for the average layman to understand. They are of benefit to utility companies and to consumers because the investment and operating costs can be divided to suit the particular circumstances into demand, customer, and consumption groups through the use of some modification of the Hopkinson rate. Demand rates are an advantage to the customer in that the use of such a rate reduces the rate per thousand pounds to the long-hour user.

Fuel Price Surcharge. It is usually desirable to establish a rate upon a specified basic cost of fuel to the utility company. Where there are wide variations in the price of fuel, it is also desirable to add a definite charge per thousand pounds of steam sold for each increment of increase in the price of fuel. This surcharge automatically compensates for the variations without necessitating frequent changing of the whole rate structure.

Some utility companies include a labor surcharge as well as a coal surcharge.

UTILIZATION

Considerable savings can be made by the proper and intelligent operation of heating systems. It should be borne in mind that a heating system is designed to heat a building to 70 F inside when the outside temperature is at its lowest point for that particular locality. There is a tendency to overheat the building at any time the outside temperature is above the design temperature unless some method of regulation is used, either automatic or manual.

The general rules for economical operation[2] are as follows:

1. *Reduce the heat losses from the building to a minimum.*
   - *a.* Weatherstrip all windows, and caulk all window frames.
   - *b.* Provide revolving or vestibule doors on all entrances. Separate shipping and receiving rooms from the remainder of the building by partitions so that the large doors will not ventilate the entire building.
   - *c.* Eliminate all unnecessary ventilation. Ventilating equipment is usually sized to meet extreme requirements. In a theater or auditorium, do not supply enough ventilation for an audience of 2000 when there are only 200 present.
2. *Limit the hours of heating to those in which the required temperature is necessary.*
   - *a.* Determine the hours that heating is required and see that steam is shut off for the maximum time when not required, such as nights, Sundays, and holidays.
   - *b.* Shut steam off entirely in unoccupied sections of the building, taking care to avoid freezing plumbing.
   - *c.* Install separate lines for those parts of the building that require long-hour or 24-hour heating. This is much cheaper than heating the entire building.
   - *d.* Control the heat supplied to water storage tanks located on or above the roof. Such tanks require heat to prevent freezing when the outdoor temperature is below 32 F.
3. *Regulate the amount of heat so as to prevent overheating and to maintain uniform temperatures during the hours of occupancy.*
   - *a.* Determine the temperature required for the occupancy of a building. Do not heat a storage garage or a furniture warehouse to the temperature required in a hospital ward.
   - *b.* Shut off steam during the day whenever possible. An automatic control will do this, but it can be done by hand, with good results.
   - *c.* Provide some good means of temperature control.
4. *See that the heat input is properly balanced throughout the building.*
   - *a.* See that the entire heating system responds rapidly when steam is turned on. Locate and eliminate the cause of any sluggish circulation. Balance the radiation, provide adequate air elimination, and correct any trapped run-outs to provide quick system drainage.
   - *b.* Place the radiation near the outside walls under the windows or where the exposure occurs, if possible.
   - *c.* Do not obstruct radiators or prevent the free circulation of air around them; to do so seriously reduces the heating capacity of a radiator.
5. *Keep all heating equipment in first class condition.*
   - *a.* Keep the system in good repair. This applies to all traps, valves, vents, steam and return piping, vacuum pumps, and temperature control apparatus.
   - *b.* In a vacuum system, maintain the degree of vacuum recommended by the control manufacturer. If this is not possible, locate and eliminate all leaks.
   - *c.* Insulate all steam pipes not used as heating surface.
6. *Arrange the heating system to obtain from it the highest possible efficiency.*
   - *a.* Locate all valves and controls so as to be convenient and accessible. It is only human nature to delay or avoid doing that which is unnecessarily inconvenient.
   - *b.* Investigate every complaint of "No Heat;" find the cause and correct it. Do not overheat an entire building to correct a local condition.
   - *c.* Extract the heat in the condensate for heating water or for some other useful purpose.

7. *Make a study of the heating system and heating requirements.*
   a. Provide thermometers and recording pressure gages so that the heating system may be operated with full knowledge of what is being accomplished.
   b. Keep daily consumption records and check against the theoretical requirements.
   c. Study the system and understand its functions and its operations.

AUTOMATIC TEMPERATURE CONTROL

As stated in Chapter 34, Automatic Control, properly applied to heating, ventilating and air conditioning systems, makes possible the maintenance of desired conditions with maximum operating economy. The use of adequate temperature control provides more healthful, comfortable, and efficient working conditions in buildings.

There are three general means of obtaining centralized control of heat output of radiators.

1. *Controlling the rate of steam flow* into the radiators. This is accomplished by equipping the radiator inlets with orifices and controlling the flow of steam through them into the radiator by controlling the difference in pressure between the supply and return.

2. *Controlling the temperature of steam* in the radiators by varying its pressure. This involves the use of high vacuums to obtain low steam temperatures. This must be supplemented by some other type of control for low heat output.

3. *Controlling the length of time steam flows* into the radiators by admitting steam to a heating system intermittently and varying the length of the *on* and *off* periods. Two types of controls are used. (1) A clock control providing *on* and *off* settings of various lengths, which can be changed in accordance with outside temperatures. In most cases these changes are made automatically by means of a thermostatic bulb, placed outdoors. (2) A control, having an outdoor bulb and a bulb attached to the radiator, which varies the length and frequency of the *on* intervals in such a way that the radiator temperature is varied according to the outside temperature. In some cases heat supply is controlled by combinations of the three methods described.

Before installing any type of modern temperature control equipment, it is necessary to see that the heating system is put in good operating condition. In general, the heating system in a building is not given the attention that other mechanical equipment is given because it will continue to function, after a fashion, even though changes in piping, location of radiation, settlement of piping, and the normal wear and tear or other changes have taken place. Because of this depreciation of the system, operation becomes more and more costly and parts of the building have to be greatly overheated in order to prevent underheating in other parts. Vents, traps, vacuum pumps, and valves should be given a careful inspection and replaced or repaired if required. The piping should be of adequate size and graded properly. The return piping should be inspected, and any pockets or lifts removed and properly vented. These inspections and repairs are not costly and may prevent a much greater outlay in future years. In most cities district heating companies will be willing to make a survey of heating systems and offer recommendations in regard to operation and changes in piping layout.

The selection of control equipment depends upon the type and size of building and the degree of saving which may be obtainable.

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Chapter 30

ELECTRIC HEATING

Resistors, Heating Elements, Electric Heaters, Unit Heaters, Central Fan Heating, Electric Boilers, Electric Hot Water Heating, Heating Domestic Water Supply, Control, Calculating Capacities, Radiant Drying, Induction and Electrostatic Heating, Power Problems

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ELECTRIC heating deals with the conversion of electrical energy into heat and the distribution and practical use of the heat so produced. In certain regions, where the cost of electricity is favorable, electric heating is used extensively. Its use is also frequently dictated by special conditions.

DEFINITIONS

Definitions of general terms used in fuel heating are given in Chapter 1. Terms which apply particularly to electric heating are as follows:

Electric Resistor: A material used to produce heat by passing an electric current through it.

Electric Heating Element: A unit assembly consisting of a resistor, insulated supports, and terminals for connecting the resistor to electric power.

Electric Heater: A complete assembly of heating elements with their enclosure, ready for installation in service.

RESISTORS AND HEATING ELEMENTS

Solids, liquids, and gases may be used as resistors, but most commercial electric heating elements have solid resistors, such as metal alloys, and non-metallic compounds containing carbon. In some types of electric boilers, water forms the resistor which is heated by an alternating current of electricity passing through it. One of the more common resistors is nickel-chromium wire or ribbon which, in order to avoid oxidation, contains practically no iron.

Commercial electric heating elements are made in many types. Some have resistors exposed to the air being heated. The resistors may be coils of wire or metal ribbon, supported by refractory insulation, or they may be non-metallic rods, mounted on insulators. This type of element is used extensively for operation at high temperatures when radiant heat is desired, also at low temperatures for convection and fan circulation heating, especially in large installations.

Some elements have metallic resistors embedded in a refractory insulating material, encased in a protective sheath of metal. Fins or extended surfaces may be used to add heat-dissipating area. Elements are made in many forms, such as strips, rings, plates and tubes. Strip elements are used for clamping to surfaces requiring heat by conduction, and in some types of convection air heaters. Ring and plate elements are used in electric ranges, waffle irons, and in many small air heaters. Tubular elements may be immersed in liquids, cast into metal, and, when formed into coils, used in electric ranges and air heaters. Cloth fabrics woven from flexible resistor wires and asbestos thread are used for many low temperature purposes such as heating pads, aviators' clothing and radiant panel heating installations.

Special incandescent lamps are used as heating elements in certain applications where radiant heat is desired. These use carbon or tungsten

filaments as resistors, and are designed to produce maximum energy in the infra-red portion of the spectrum.

ELECTRIC HEATERS

Electric heaters may be divided into four groups: conduction, radiant, convection, and induction.

Conduction electric heaters, which deliver most of their heat by actual contact with the object to be heated, are used in such applications as aviators' clothing, hot pads, soil heaters, ice melters, and water heaters. Conduction heaters are useful in conserving and localizing heat delivery at definite points. They are not suitable for general air heating.

Radiant electric heaters, which deliver most of their heat by radiation, have high temperature heating elements and reflectors to concentrate the heat rays in the desired directions. The immediate and pleasant sensation of warmth which is caused by radiant heat makes this type desirable for temporary use where the heat rays can fall directly upon the body. They are not satisfactory for general air heating, as radiant heat rays do not warm the air through which they pass. They must first be absorbed by walls, furniture, or other solid objects which then give up the heat to the air. For a discussion of electrically heated panels as applied to radiant heating, see Chapter 31.

Gravity convection electric heaters, designed to induce thermal air circulation, deliver heat largely by convection, and should be located and used in much the same manner as steam and hot water radiators or convectors. They generally have heating elements of large area, with moderate surface temperature, enclosed to give proper stack effect to draw cold air from the floor line. The flexibility possible with electric heating elements should discourage the use of secondary mediums for heat transfer. Water and steam add nothing to the efficiency of an electric heater and entail expensive construction and maintenance.

Induction Heaters are described in the section on Electronic Heating by Induction and Electronic Means.

UNIT HEATERS

Electric unit heaters include a built-in fan unit which circulates room air over the heating elements. They are adapted to the same uses as other types of unit heaters where conditions are favorable to electric heating. They are very adaptable for heating of small offices, locker rooms, etc., in otherwise unheated buildings. In small unattended equipment rooms, thermostatically controlled electric unit heaters are frequently used to maintain a temperature above freezing.

The best location for electric unit heaters depends upon local conditions. Various designs and arrangements are available, as with steam unit heaters. See Chapter 26.

The arrangement of the wiring circuits is very important for electric unit heaters. In principle they are all the same and include as essential elements an automatic control panel, a thermostat, and a master hand switch. All heaters should be designed with a safety thermal trip wired in series with the magnet coil of the control panel and with the hand switch and thermostat. A typical wiring diagram is shown in Fig. 1. This applies to a single phase power supply, but for 3-phase the only difference is to have a 3-pole panel and a heater arrangement for 3-phase connection.

CENTRAL FAN HEATING

Electric heating elements can be used for the prime source of heat in a central fan electric heating system or in the heating phase of a complete air conditioning system. They can be used in the same manner as steam heating units for tempering, preheating or reheating the air at the main supply fan location and as booster heaters at the delivery terminals of the duct system. In the humidification phase of air conditioning electric heating elements can be used to provide moisture by the evaporation of water, or for controlling air washer dew-point temperatures when mounted as preheating units on the intake side of the air washer. (See Chapter 43.)

In coordinating the input of heat energy and the volume of air circulation, a basic difference between electric heating and steam heating enters into the problem. Steam is approximately a constant-temperature source of heat for any given pressure and a change in air volume flowing

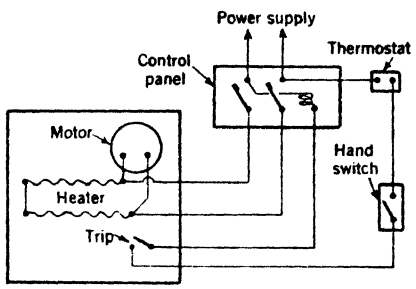

FIG. 1. WIRING DIAGRAM FOR UNIT HEATER

over steam coils does not greatly affect the temperatures of the delivered air. The amount of steam condensed (heat input) varies in proportion to the air volume, but the surface temperature of the steam coils remains about the same. Electric heat is quite different, having a constant input of energy. If the volume of air flow over electric heating elements is changed, and no change is made in the electrical power connections, there will be a corresponding change in the temperature of the air delivered. This occurs because the electrical energy input remains constant and the surface temperature of the heating elements will vary as is necessary to force the air to accept all the heat. With electric heat the total heat is constant unless some compensating action is performed by control. Automatic variation of the electrical heat input synchronized properly with the air flow can be successfully accomplished by various special methods of control. By-pass dampers as used in steam units will not control electric heat.

Electric heaters are useful in balancing the heat distribution in central fan heating systems. Even in those instances where steam is the principal heat source, the temperature of individual rooms can be controlled locally by separate electric booster heaters. These heaters can be installed in branch ducts or behind the air outlet grilles in each room. With this arrangement, the central heating unit distributes air at an average temperature, controlled from a thermostat centrally located, such as in the main return duct. The electric booster heaters may be controlled by thermostats mounted in each individual room which permit the occupant to maintain any desired temperature independent of the rest of the building.

ELECTRIC BOILERS

Steam or hot water generating boilers using electric energy are entirely automatic and are well adapted to intermittent operation. Small electric boilers usually have heating elements of the enclosed metal resistor type immersed in the water. Boilers of this construction may be used either with direct or alternating current since the heat is delivered to the water by contact with the hot surfaces. To lessen the likelihood of the heating elements burning out, they should be of substantial construction, with a low heat density per unit of surface area and provision should be made for cleaning off deposits of scale which restrict the heat flow. A typical resistance type of steam or hot water boiler is shown in Fig. 2.

Large electric boilers are usually of the type employing water as the resistor, using immersed electrodes. With this type only alternating current can be used, as direct current would cause electrolytic deterioration. Such a type of electrode boiler is shown in Fig. 3.

Electric steam boilers are useful in industrial plants which require limited amounts of steam for local processes, and also for sterilizers,

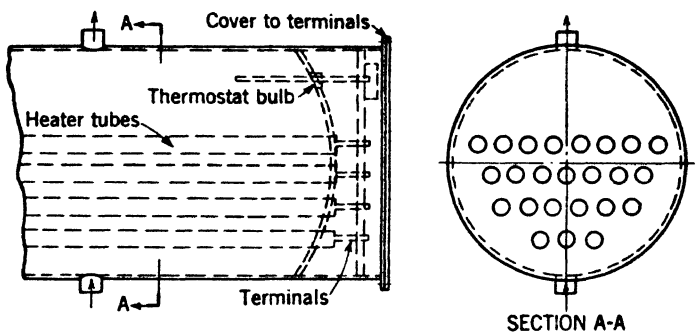

FIG. 2. RESISTANCE TYPE BOILER FOR STEAM OR HOT WATER

jacketed vessels and pressing machines which need a ready supply of steam. It sometimes is economical to shut down the main plant fuel burning boilers when the heating season ends, and to supply steam for summer needs with small electric steam boilers located close to the operation.

ELECTRIC HOT WATER HEATING

Electric water heating, using an electric boiler in place of a fuel burning boiler, like electric steam heating, is generally confined to auxiliary or other limited applications. The use of insulated water storage tanks, in which to store heat generated by electricity during off-peak hours at extremely low rates, is a development which has some special applications.

In this system of heating, the primary storage tank is simply a large, well-insulated, pressure type steel tank, equipped with electric heating elements and automatic time switches, which also have automatic limit controls for temperature and pressure. The heating system installed in the building may be of any standard design. A system of this kind requires very careful design to avoid excessive over-all radiation losses during periods of low heat demand. It is also important to provide for

sudden changes in heat demand. A typical hot water heating boiler is illustrated in Fig. 2.

HEATING DOMESTIC WATER BY ELECTRICITY [1]

Electric water heaters of the automatic storage type for domestic hot water supply are simple and reliable. In many sections of the country low electric rates have been established by the electric utilities to secure this load. In many localities, electric rate schedules divide the current used for water heating into two classifications, regular and off-peak. A time switch automatically limits use of the off-peak heating element to the hours of off-peak load, while the regular heating element is a stand-by at all times. Storage of this two-element type of water heater is larger than average to carry over the periods when the off-peak element is timed out, without too frequent demands on the regular heating element which takes the higher domestic lighting service rate. Some utilities now offer

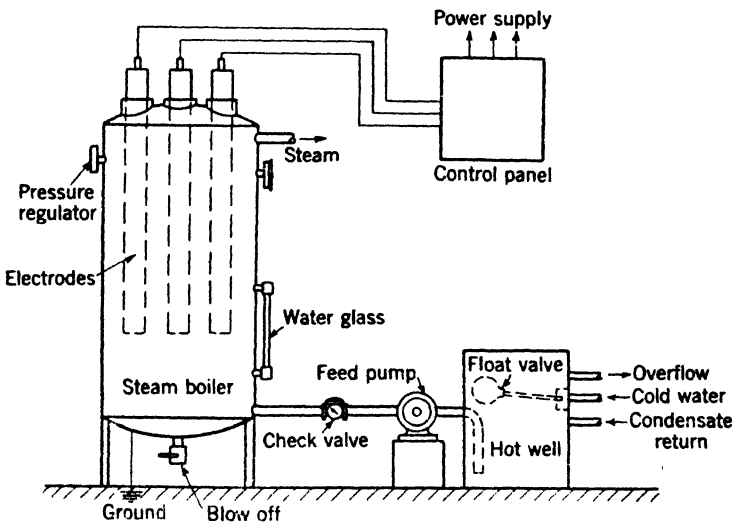

FIG. 3. DIAGRAMMATIC ARRANGEMENT OF AN ELECTRODE BOILER

a schedule which, beyond a stipulated minimum, lowers the rate for all electric service if an electric water heater is installed.

Competition with other fuels, especially gas, seems to be the major controlling factor in the use of electricity. The first cost of electric storage heaters is greater than for gas, owing to the need for larger tank storage due to off-peak service and slower recuperating capacity.

In residential work, to effect a saving in the cost of operation, it is sometimes desirable to use a furnace coil or indirect heater in connection with an electric water heater. In this case it is important to make the proper connections in order to benefit by any heat obtained from the furnace and at the same time to prevent dangerous overheating. The proper piping connections are shown in Fig. 4, and in this case the electric heater will only furnish heat when insufficient heat is supplied from the furnace. This arrangement has a further advantage in the summertime in that the bare tank through which the cold water passes on its way to the electric heater serves as a tempering tank, absorbing heat from the basement air and requiring the use of less energy in the electric heater.

A typical domestic hot water heater as shown in Fig. 5 is arranged with upper and lower heating elements for the usual type of off-peak heating service. The lower heating element is under the control of the off-peak time switch. However, the upper heating element is usually connected to the line so that, in case the supply of hot water in the tank becomes exhausted, the top thermostat can turn on the top heater and heat a small supply of water. The top heater will not heat the water in the tank below its location, but when the off-peak period arrives the lower heater is turned on and the entire tank becomes heated.

HEATING BY REVERSED CYCLE REFRIGERATION

Reversed refrigeration is frequently referred to as a *heat pump* since the electric motor driving the refrigerating compressor furnishes the motive power to transfer heat from one temperature to a higher temperature

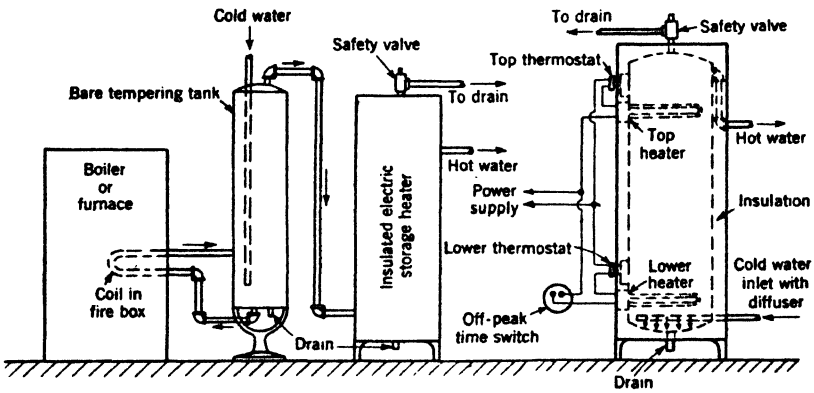

FIG. 4. PIPING ARRANGEMENT FOR CONNECTING ELECTRIC WATER HEATER TO FIRE-BOX COIL

FIG. 5. DOMESTIC HOT WATER HEATER FOR OFF-PEAK SERVICE

level. The compressor acts as a reversible refrigerating unit to extract heat from the outdoor air in winter and deliver it indoors for heating purposes, and, by a reversal, to extract heat from the indoor air in summer and discharge it outdoors. For details see Chapter 39.

CALCULATING CAPACITIES

In calculating electric heating capacity one kilowatt is equal to 3413 Btu per hour or 14.2 sq ft equivalent direct steam radiation.

All of the energy applied to an electric resistor is transformed into heat. The output of an electric heater is a fixed constant, unaffected by the temperature of the surrounding air and the total load on an electric heating system is the total wattage of the connected electric heaters.

RADIANT DRYING

Lacquers and similar surface films can be very effectively dried by radiation. Special electric lamp bulbs have been developed which give off a high percentage of infra-red and similar heat rays [2]. These are mounted in very efficient reflectors. For continuous manufacturing processes these reflectors are mounted in tunnels through which conveyors pass. For

local applications, as for example paint drying in automobile repair shops, they may be mounted on portable racks. Objects of relatively large surface area in proportion to their weight, and fabricated materials having a rather high heat absorption, may be satisfactorily heated by such a source.

In the application of this type of drying the composition of the paint or lacquer is important. In general, lacquers and those enamels using synthetic resins react most favorably. Other applications include the drying of ink, glue, and water, the softening of celluloid and bakelite for punching or shearing, and a wide variety of other uses [3].

ELECTRONIC HEATING BY INDUCTION AND ELECTROSTATIC MEANS

These methods differ radically from resistance heating as they employ high frequency radio waves to apply the energy which produces heat. High frequency heating has many important industrial uses and opens up a whole new field of special applications where extreme accuracy and speed are vital.

Metals can be heated by induction. When the work is placed in a magnetic field within a high frequency coil, eddy currents immediately produce heat in the body of the metallic piece. The speed and intensity of this heating can be regulated by controlling the high frequency currents producing the magnetic field and the location of the spot heated by the position of the work piece within the coil. Induction heating is very useful in special processes such as melting metals, brazing, forging, heat treating, etc. It is possible to apply localized heat so rapidly that conduction cannot draw the heat away before it has time to accomplish the desired purpose at a particular spot. One example is the rapid hardening of a tool edge or tip too quickly for scale to form.

Dielectric materials can be heated internally by introducing them into an electrostatic field between high frequency electrode plates. Foods can be sterilized, plywoods bonded, plastics heated, granular or crystalline materials dehydrated, and countless other products heated quickly and uniformly, although they are poor thermal conductors and resist heat applied to their exteriors. Electrostatic heating is ideally suited for continuous production processes as the materials can pass through the heating field quickly with very short exposures to the high frequency radio waves.

POWER PROBLEMS

The cost of electric energy varies because of several factors. Distribution costs differ for large and small users. The fact that electricity cannot be economically stored, but must be used as fast as it is generated, makes it impossible to operate electric plants at uniform loads; hence, even the time of use may affect the cost of electricity. Special low rates are sometimes available during certain prescribed hours of use.

Since the cost of production and distribution depends not only upon the quantity of energy used but also upon the maximum rate at which it is used, electric energy is often sold on a demand rate basis. In some cases, the demand charge is based upon the rated connected load, in other cases, upon the maximum demand as indicated by a demand meter.

Homes are almost universally supplied with lighting current of 115 volts, which can only be used economically for small heaters. Usually

the service lines will not permit more than plug-in devices. The Underwriters permit approved heaters of 1320 watts or less to be plugged into approved baseboard receptacles, but such heaters cannot be served on a circuit supplying much other load without overloading the fuses. There is an increasing trend toward supplying homes with three wire 115-230 volt service. Where homes have such service, larger heaters can be installed. For industrial purposes, heaters should be designed to use polyphase power, which is usually supplied at 208, 220, 440 or 550 volts. All polyphase heaters should be balanced between phases. In ordering electric heaters the proper voltage must be specified as the heat produced will vary as the square of any variation in voltage.

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Chapter 31

PANEL HEATING AND RADIANT HEATING

Influence of Heat Radiation on Human Comfort, Objectives of Radiant Heating, Practical Problems of Radiant Heating from a Physiological Standpoint, Fundamental Computations, Application Methods, Calculation Principles, Measurement and Control

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IT has been pointed out in Chapter 12 that the human body loses heat to its environment in three ways; by convection, radiation, and evaporation. The Effective Temperature Chart takes account of convection and evaporation, but does not provide for such radiative effects as occur when room air and its surrounding surfaces differ widely in temperature.

INFLUENCE OF HEAT RADIATION ON HUMAN COMFORT

When, however, the body is exposed to radiation from a hot surface or is radiating to a cold surface, the factor of radiative heat gain or heat loss may be important. This phenomenon is most marked in the case of exposure to the sun's radiative heat. On a cold day, with no wind blowing, while standing in the sunshine, one may feel perfectly comfortable but, when a cloud passes over the sun, one may instantly feel much cooler. The cloud acts as a shield to interrupt the radiant heat from the sun. The change in feeling of comfort is due to the instant change in rate of heat loss from the body caused by the shielding effect of the cloud. A shielded thermometer under the same condition would register no change in temperature.

The rate of heat loss by convection depends upon the average temperature difference between the surface of the body and the surrounding air, the shape and size of the body, and the rate of air motion over the body.

The rate of heat loss by radiation depends upon the exposed surface area of the body, and upon the difference between the mean surface temperature of the body and the mean surface temperature of the surrounding walls or other objects. This latter temperature is called the Mean Radiant Temperature (MRT).

Because these two types of heat loss supplement each other, a required rate of total heat loss can result either from a relatively low air temperature and a relatively high MRT, or vice versa.

At the temperature which produces comfort (and at all lower temperatures) the production of sweat is low and the heat loss by evaporation is relatively low and relatively constant, irrespective of the relative humidity of the atmosphere. Under such conditions the heat loss from the body is chiefly related to the combined effect of convection and radiation. For unclothed subjects in a reclining posture the heat demand of the environment, so far as these two factors of radiation and convection are concerned, may be measured by Operative Temperature, which is defined by the following formula, modified from that of Gagge [1] by the expression of air velocity in feet per minute and temperature in Fahrenheit degrees,

$$t_o = 0.81\, t_w + 0.135 \left[\sqrt{V}\, t_A - \left(\sqrt{V} - 1.40 \right) t_s \right],$$

where

t_o = operative temperature, Fahrenheit degrees.
t_w = mean radiant temperature, Fahrenheit degrees.
t_A = air temperature, Fahrenheit degrees.
t_s = mean skin temperature, Fahrenheit degrees.
V = air velocity in feet per minute.

Under comfortable still air conditions during the heating season, the mean skin temperature of persons normally clothed is between 90 and 93 F (with lower values for the extremities), and the mean clothing surface temperature is between 82 and 86 F.

The normal rate of heat production in an average sized sedentary individual is about 400 Btu per hour. The heat production for persons subjected to various rates of activity is given in Chapter 12. The human body is of complicated shape, and radiation takes place freely only from the exposed outer surfaces; there are considerable portions of the body such as the legs, arms, lower part of the head, etc., which radiate most of their heat to other portions.

It is necessary to determine the equivalent surface of the body from which heat is radiated and a similar value for convection. The total may be assumed to be about 19.5 sq ft for convection and 15.5 sq ft for radiation, in an average sized individual.

The loss by respiration and by evaporation from the nose and throat depends on the temperature and area of the moist surfaces (respiratory) of the body, the air temperature, air movement, and humidity. In air at a temperature of 70 F, this loss, for a sedentary individual of average size, will be approximately 90 Btu per hour; and at 60 F about 70 Btu per hour. These values are relative, because the total will vary materially with change of position, bodily activity, age, sex, race, etc.

The balance of the heat generated in the average human body, approximately 300 to 320 Btu per hour at about 70 F room temperature, is the approximate amount of heat given off by radiation and by convection from the external body surfaces. Under normal conditions (in still air), the radiation loss will be about 190 Btu per hour; and the convection loss about 120 Btu per hour. With an air velocity of 520 fpm, comfort will require an increase in Operative Temperature of nearly 12 deg; under such conditions the convection loss will rise to 250 Btu per hour but comfort may be attained if the subject is surrounded by heated walls which keep the radiation loss at about 50 Btu[2].

It is neither feasible nor desirable to change the relationships of convection and radiation very greatly in actual heating practice. In the laboratory, where the laws of radiative heat loss have been deduced, it is necessary to produce wide differences between radiative and convective heat loss. This can only be accomplished, however, by elaborate and powerful conditioning apparatus which simultaneously heats walls and cools air, or vice versa. Such a process would be very costly in practice and would not be justified unless marked improvement in comfort resulted from such a condition—an assumption which has not been demonstrated. In practice, where radiant heat is introduced into a room,

that heat is absorbed by surfaces, furniture, and the like, and then transformed into convective heat so that air and surfaces tend to attain a generally uniform temperature.

OBJECTIVES OF RADIANT HEATING

Under ordinary circumstances the human being, indoors, is not subjected to marked variations between the factors affecting convection and radiation. Air and walls are not commonly very far apart in temperature; air movement and relative humidity are usually low. Where such conditions obtain, the ordinary air thermometer is a good measure of comfort —which is the reason why it has enjoyed such universal use. Where considerable window surfaces create heavy radiation loss, or where stoves or open fires, or very hot ceilings contribute to large radiation gain, the picture is changed and the air temperature productive of comfort must be correspondingly modified.

In general, however, radiant heating of occupied spaces is not a procedure designed to create differences between air and walls, but is merely one method of introducing heat into that space. The engineering factors used in determining desirable heat input will be essentially the same as if the heat were introduced by convection, or in any other way.

PRACTICAL PROBLEMS OF RADIANT HEATING FROM A PHYSIOLOGICAL STANDPOINT

It is convenient to distinguish two different methods of introducing radiant heat into an enclosed space. The first, which may be called High-Temperature Radiation, involves direct exposure of the occupied parts of the room to radiation emitted from relatively small heating units of very high temperatures (perhaps 1,000 F); the second, Panel Heating, involves exposure to relatively large surfaces at not over 130 F.

High-Temperature Radiant Heating may be useful for temporary purposes, as in the use of a bathroom heater. It is, however, generally an undesirable process (except in rooms of great height) on account of the marked unevenness of the effect produced on the human body. Studies at the John B. Pierce Laboratory of Hygiene have shown that this type of heating produces uncomfortable differences in the temperature of different parts of the body (an over-heated head, for example, if the heat comes from the ceiling).

Panel Heating, on the other hand, is advantageous from the standpoint of temperature differentials. In actual practice, a well-designed system of this sort produces very uniform conditions, the air throughout the room differing at various points by only 5 deg. This is desirable from the comfort standpoint and may also be a factor in heat economy, since high temperatures in the upper part of the room favor excessive heat loss. The esthetic value of such a system is also considerable, since it avoids the presence of registers or free-standing radiators in the room.

In the design of Panel Heating, however, careful thought must be given to the location of the panels from the standpoint of comfort. The English commonly use the ceiling for their panels, but their rooms are generally high-studded, and outdoor winter temperatures moderate. With low ceilings even panels may produce an excessive directional heating effect if all the heat necessary in a cold climate is introduced from above. Similarly, if the floor alone is used, it may—in very cold weather—be necessary to make the floor too hot for comfort. Wall panels, or a combination of ceiling and floor panels, will perhaps produce the best results.

FUNDAMENTAL COMPUTATIONS

The mean surface temperature of an inert body, which will cause given rates of heat loss by radiation and by convection in a uniform environment, having a given air temperature and a given mean wall temperature, may be calculated from fundamental equations [3] for radiation and natural convection, with substitution of comparable cylinders for the irregular human body.

$$q_r = 0.1730\, e \left[\left(\frac{T_s}{100}\right)^4 - \left(\frac{T_w}{100}\right)^4 \right] \quad (1)$$

$$q_c = 1.235 \left(\frac{1}{D}\right)^{0.2} \times \left(\frac{1}{T_m}\right)^{0.181} \times \left(T_s - T_a\right)^{1.266} \quad (2)$$

where

q_r = heat loss by radiation, Btu per (square foot) (hour.)

q_c = heat loss by convection, Btu per (square foot) (hour.)

T_s = absolute temperature of the body surface, Fahrenheit degrees

T_w = absolute temperature of the walls, Fahrenheit degrees.

T_a = absolute temperature of the air, Fahrenheit degrees.

$T_m = \dfrac{T_s + T_a}{2}$

D = diameter of cylinder, inches.

e = the ratio of actual emission to black body emission.

If it is assumed that an average adult has a height of 5 ft 8 in., a body surface of 19.5 sq ft for convection, and 15.5 sq ft for radiation, an equivalent effect can be worked out for two cylinders, 5 ft 8 in. high by 13.15 in. diameter and 10.45 in. diameter, respectively. However, while the effects on a cylinder, of a particular size and shape may be used to estimate average similar effects on the human body, it should be remembered that the heat loss from the body varies greatly. Every movement alters not only its shape, but also the heat generated by the body, the velocity of the air passing over it and the surface exposed to radiation. This fact renders the results of any such computation only approximate.

APPLICATION METHODS

The several methods of applying panel and radiant heating to a structure are:

1. *By warming the interior wall and ceiling surface of the building.* Pipe coils are imbedded in the concrete or plaster of the walls or ceilings, the heating medium being hot water circulating through the pipe coils. These coils are generally constructed of small pipe ½ or ¾ in. I.D. and spaced about 6 to 9 in. apart. See Fig. 1. This has the effect of warming the entire concrete or plaster surface in which the pipes are imbedded. Since the temperature of the heating medium should never exceed about 130 F, due to the possibility of cracking the plaster the area of the warmed surface must be sufficient to supply the requisite quantity of heat at this low temperature. Normally the hot water circulation is maintained by means of a circulating pump and facilities have to be provided to eliminate all air at the top of the system. All coils and circulating pipes are welded together and tested after erection to a hydraulic pressure of 300 psi.

2. *By circulating warm air through shallow ducts under the floor.* In this design the entire floor surface of a room is heated as in Fig. 2. This method was used 2000 years ago in many parts of the Roman Empire. While this method is more expensive in construction, it is effective and quite suitable for cathedrals and large public buildings. To provide a uniform floor temperature, one should give special consideration to the design of the air ducts so that equal heat distribution is obtained.

3. *By placing hot water pipes in or under the floor.* With this arrangement the whole floor surface of a room is raised to a temperature sufficient to give comfortable conditions. Floor heating is recommended for schools and hospitals where large quantities of outside air are desirable. The floor surface may be of concrete, wood blocks, marble or any other material unaffected by heat, and while it is true that heat will be conducted through all materials used in floor construction, it is important that due consideration be given to the emissivity of the floor. In some cases where pipe coils are installed in the air space

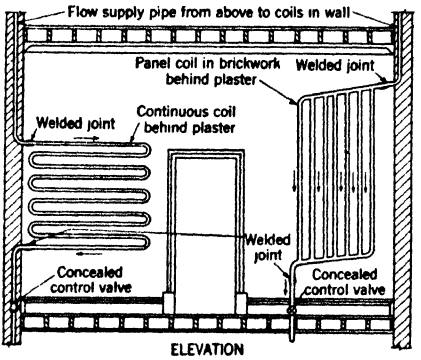

FIG. 1. COILS IN WALL SURFACES

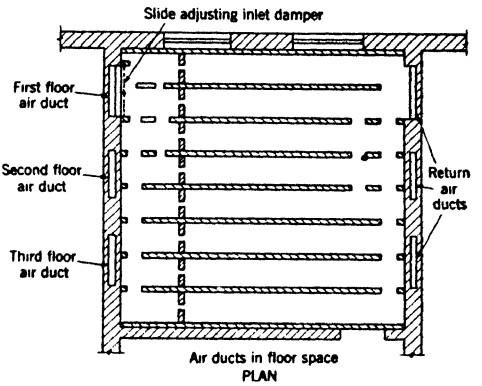

FIG. 2. AIR DUCTS FOR FLOOR HEATING

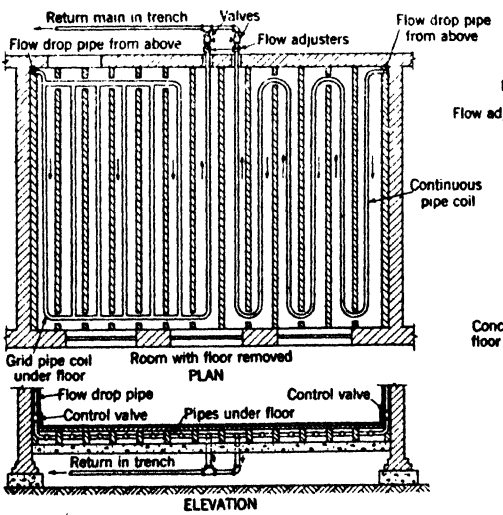

FIG. 3. CONTINUOUS COIL IN FLOOR

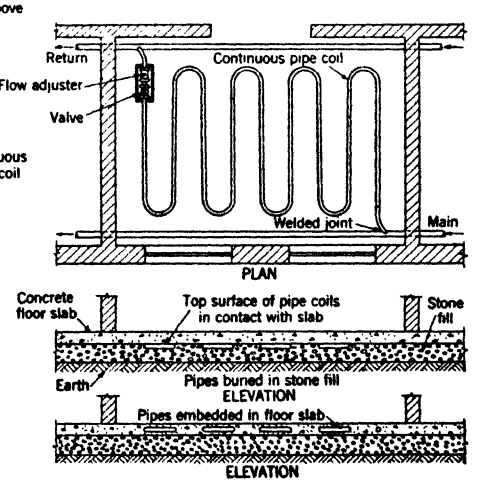

FIG. 4. COILS EMBEDDED IN FLOORS

under the floor, special floors are constructed in sections so that the whole floor can be lifted to examine the coils. See Fig. 3. Pipes supported thus may be larger and the heating medium maintained at a higher temperature than when pipes are actually imbedded in the floor. Pipes may be 1½ or 2 in. in the former, but for the latter ¾ or 1 in. pipes are recommended. See Fig. 4. Where the heat losses from a room are exceptionally high it may be necessary to supplement the warm floor by either adding some coils in the ceiling or forming heated panels in the side walls.

4. *By attaching separate heated metal plates or panels to the interior surfaces.* These plates or panels are placed either in an insulated recess so that the surface of the panel is flush with the surface of the walls or ceilings, or they may be secured to the face of the wall. They may be covered with wood veneers and decorated to harmonize with other

parts of the room, or they may be cast into panels to imitate oak or other wood designs. With flat plate panels it is common practice to use a frame of plaster, wood, metal or composition to allow for expansion. These plates may be heated with either hot water or steam and connected as in an ordinary radiator system. See Figs. 5 and 6.

5. *By electric heated metal plates or panels.* These plates or panels are either placed in insulated recesses of walls or ceilings or fastened to the construction, as found desirable. They should not have a surface temperature much above 200 F. Some have a much higher surface temperature but a lower temperature gives a more comfortable condition and is more efficient.

6. *By electrically heated tapestry mounted on screens and on the wall.* For this purpose the screen is woven with an electric continuous conductor. Such screens are useful to plug in at any position for emergency local heating without taking care of a large room or office.

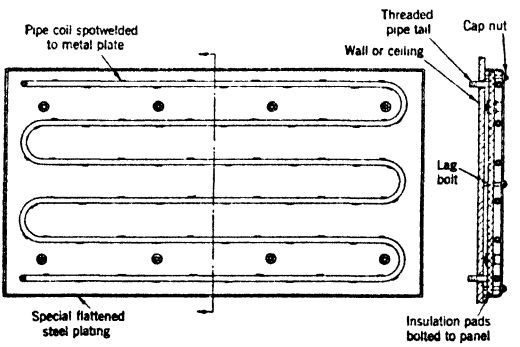

FIG. 5. PILLAR TYPE RADIANT HEAT PANEL

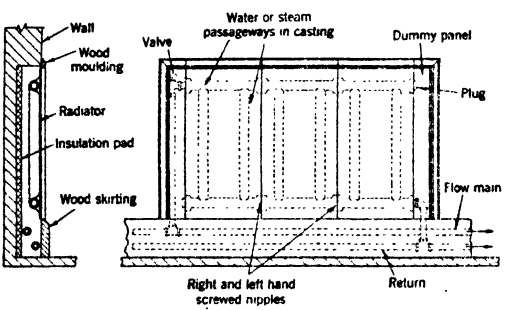

FIG. 6. FLAT TYPE PANEL INSTALLED IN WALL RECESS

Note. If all of a heating panel is installed at one end of a large room there may be a marked difference between the equivalent temperature on the two sides of the body. It is usually desirable, therefore, that the heat be distributed at different parts of the walls and ceilings so that no uncomfortable effect will be felt from unequal heating.

CALCULATION PRINCIPLES

Part I—Panel Heating

The term *panel heating*, involving both radiation and convection, is applied in this chapter to a system in which the heat is transmitted from panel surfaces to both air and surrounding surfaces, as is the case under indoor conditions.

Panel heating systems for buildings may be designed as illustrated and described in the following design of a panel heating system for the room shown in Fig. 7. The design is based on continuous heating. Panel

heating systems should, in general, be operated continuously since the panels have large thermal capacities. Where panels are heated by high temperature radiation from a heat source directed toward them, this qualification does not apply.

1. *Assume the location and the approximate size of the heating panel.*

Heating panels may be located in ceilings or floors or walls. Ceiling panels have the advantage that their heat emission is not affected by tapestry or furniture and that they can be used, to a limited extent, as cooling panels during the summer months. If used in low rooms, however, they may produce an undesirable heating effect upon the head. Floor panels have the advantage that they can be easily installed and that much of the radiated heat is delivered to the lower portions of the walls; they have the disadvantage that their heat emission is rather uncertain, since it may be affected by rugs, carpets, furniture, machinery, etc.

It is best to make the panels as large as practicable; for example, if the floor or ceiling is used as the heating panel, it is best to use the entire floor or the entire ceiling, or both. Heating a room by means of panels is very similar to lighting a room. Heat radiation is exactly like light radiation, except that it has a longer wave length. If a room is lighted

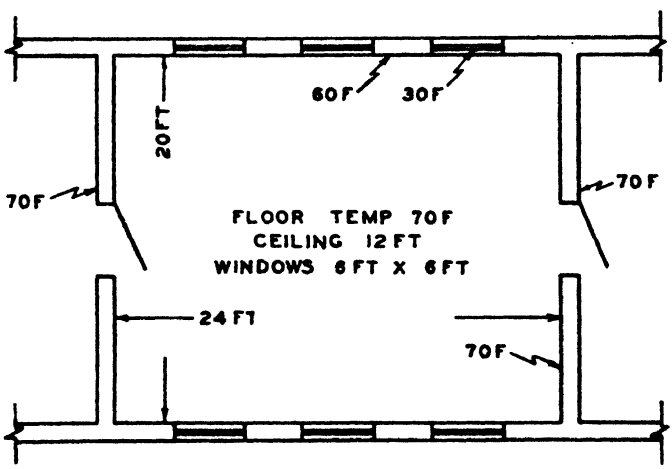

FIG. 7. ROOM PLAN USED FOR ILLUSTRATION OF METHOD OF DESIGNING A PANEL HEATING SYSTEM

by means of a large number of small units distributed uniformly over the ceiling, the room is lighted more uniformly than if it is lighted by means of a single unit of equal capacity. Similarly, if the entire ceiling is the heating panel, the room is heated more uniformly than if only a fractional part of the ceiling is used as the heating panel.

In the following example, *the entire ceiling will be used as the heating panel.*

2. *Select the desired mean temperature of the air in the room.*

In a panel-heated room, the mean air temperature is a few degrees lower than the mean temperature of the surfaces of the enclosing walls, floor, and ceiling. In a room heated by introduction of warm air or by means of radiators, convectors, or other similar heating appliances, located within the room, the mean temperature of the air is a few degrees higher than the mean temperature of the surfaces of the enclosing walls, floor, and ceiling. Under ordinary conditions, in a panel-heated room, the mean temperature of the air ranges from approximately 65 F to 72 F.

In the following example, *68 F is selected as the mean air temperature.*

3. *Determine as accurately as practicable, the mean temperature of the inside surfaces of the enclosing walls, floor, and ceiling.*

The two inside walls are assumed to separate rooms, which are filled with 68 F air, so that both surfaces of each wall are in close contact with 68 F air. The surface tem-

peratures of these walls, therefore, cannot be lower than 68 F and must actually be higher than 68 F because, in addition to their contact with 68 F air and their contact with the heated ceiling, they are exposed to the heat radiation from the ceiling.

In the following example, *70 F will be selected as the mean surface temperature of the inside walls.*

For the two outside walls, the mean inside surface temperature can be calculated with fair accuracy. For a heat transmission coefficient of 0.25 and a temperature difference of 68 deg, heat flows through the wall at the rate of 17 Btuh per square foot. If the indoor film coefficient is 1.65, the temperature difference, indoor air to inside wall surface, is 17/1.65 or 10 deg and the wall surface temperature is 68 − 10, or 58 F. This value may be taken directly from Fig. 8. However, the film coefficient 1.65 was deter-

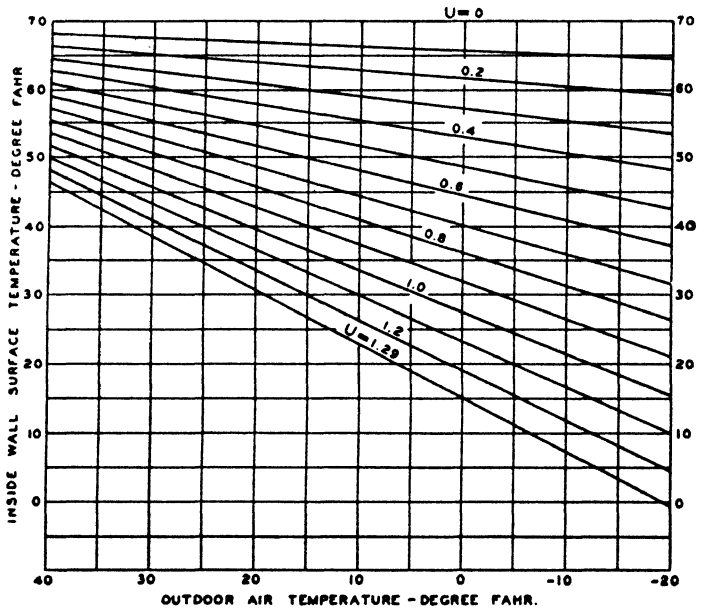

FIG. 8. CHART FOR ESTIMATING INSIDE SURFACE TEMPERATURES OF OUTSIDE WALLS[a]

[a]NOTE: The value of U, the over-all coefficient of heat transmission, cannot exceed 1.29 if the inside and outside film coefficients are 1.65 and 6.0 respectively (*e.g.* $\frac{1}{U} = \frac{1}{1.65} + \frac{1}{6} = \frac{1}{0.773}$. Therefore $U = 1.29$ maximum).

mined to represent the sum of the heat flow into the wall, by conduction from the air in contact with the wall, and by radiation from the warmer surfaces *seen* by the wall surface. In a panel-heated room, the rate of heat flow into the outside wall by radiation is greater than it is in a radiator-heated room; consequently, the film coefficient is higher, and the temperature difference, air to wall surface, is smaller, and therefore, the wall surface temperature is higher than the calculated 58 F. It is impossible to determine accurately how much higher than 58 F the temperature of the wall surface will be until the corresponding indoor air film coefficient has been determined accurately.

In the following example, *60 F will be selected as the probable mean inside surface temperature of the outside walls.*

The probable mean inside surface temperatures of the floor and the glass may be determined by calculations and by reasoning similar to that employed to determine the inside surface temperature of the outside walls.

In the following example, *30 F and 70 F will be selected as the probable inside surface temperatures of the glass and floor*, respectively.

TABLE 1. CALCULATED HEAT LOSS OF ROOM

SURFACE	AREA SQ FT	*U*	CALCULATION	HEAT LOSS BTUH
Outside Walls	360	0.25	360 x 0.25 x 68	6,120
Glass	216	1.13	216 x 1.13 x 68	16,597
Inside Walls	480	.....	No heat loss	.....
Ceiling	480	.....	Heating Panel	.....
Floor	480	0.10	480 x 0.10 x 38	1,824
Infiltration	.....	.....	5,760 cu ft x 1.50 x 68 x 0.018	10,576
			Total	35,117

4. *Determine the heat loss of the room.*

In the following example, the heat loss calculation will be based on an outdoor air temperature of 0 F. Since the functioning of a panel-heating system differs very little from that of a radiator-type heating system, the heat loss shown in Table 1 may be calculated according to Chapter 14.

The heat loss through the outside walls and through the glass is probably a little greater than calculated because the calculation is based on an indoor air film coefficient of 1.65 Btuh, whereas, for a panel-heated room, this coefficient is a little higher, but the difference is probably not sufficiently large to be considered in design calculations for a heating system.

5. *Estimate the Mean Radiant Temperature.*

The Mean Radiant Temperature of the surfaces enclosing the room but not including the heating panels may be estimated as follows:

SURFACE	AREA	FAHR DEG	PRODUCT
Interior Walls	480	70	33,600
Exterior Walls	360	60	21,600
Glass	216	30	6,480
Floor	480	70	33,600
	1,536		95,280

The sum of these products divided by the sum of the surface areas is: 95,280/1,536 or 62.03 F, the required mean surface temperature.

In the following example, *62 F will be selected as the MRT of walls, glass and floors.*

6. *Determine the temperature of the ceiling panel.*

Determine the temperature of the ceiling so that the ceiling panel will deliver heat to the room at a rate equal to the rate at which the room is calculated to lose heat, namely, 35,117 Btuh.

When a room is heated by means of a panel, air convection currents are developed in the room similar to those which are developed when the room is heated by means of a free-standing radiator. Consequently, the heating panel delivers heat to the room partly by radiation and partly by convection. The proportion of the total heat flow delivered by convection varies with the location of the heating panel, with the height of the ceiling, and with the size, number, and location of pieces of furniture and other articles which interfere with the free flow of air along the floor and along the walls. It is generally sufficiently accurate to assume that a ceiling panel will deliver 70 per cent of its heat by radiation and 30 per cent by convection; a floor panel 55 per cent by radiation and 45 per cent by convection; and a wall panel 65 per cent by radiation and 35 per cent by convection.

In the following example, ***it will be assumed that the ceiling panel must deliver 70 per cent of its heat or 24,582 Btuh by radiation***, since the total calculated heat loss is 35,117.

When two plane surfaces of infinite size are parallel to each other and their surfaces are at different temperatures, the exchange of heat between the two is proportional to the difference between the fourth powers of their absolute temperatures. This is also true when one surface is completely surrounded by another surface; for example, if one sphere is placed within another sphere, the flow of heat between the outer surface of the smaller sphere and the inner surface of the larger sphere is proportional to the fourth power of the absolute temperatures of the two surfaces.

In a panel-heated room, the heated panel may be considered to be completely enclosed by the remaining surfaces, because all heat radiated by the heated panel is intercepted by those surfaces. Consequently, the flow of heat from the heated ceiling to the room, by radiation, is proportional to the difference between the fourth powers of the absolute temperature of the ceiling and the absolute mean radiant temperature of the remaining surfaces.

The rate at which a surface emits heat varies with the temperature of the surface and with other characteristics of the surface. For ordinary heat flow calculations it is

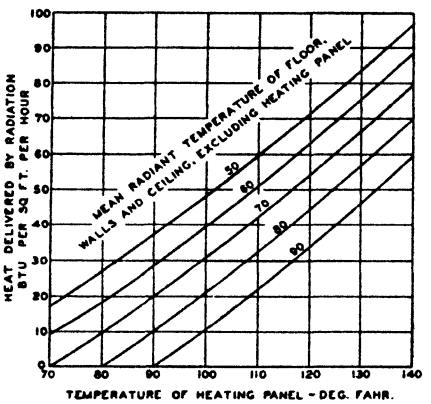

FIG. 9. HEAT DELIVERED TO ROOM BY RADIATION FROM PANEL

sufficiently accurate to assume that the materials which are commonly used in building construction emit heat at a rate of:

$$0.156 \left(\frac{T}{100}\right)^4 \text{ Btuh per square foot}$$

where

T is the absolute temperature of the surface in Fahrenheit degrees.

On this basis the flow of heat from the ceiling to its surrounding surfaces is at the rate of:

$$480 \times 0.156 \left[\left(\frac{T}{100}\right)^4 - \left(\frac{522}{100}\right)^4\right] \text{ Btuh.}$$

In order that this rate may be equal to 24,582 Btuh, T must be 572 and the ceiling temperature about 112 F.

Instead of calculating this temperature it may be taken from Fig. 9, as follows: The ceiling must deliver heat to the room, by radiation, at the rate of 24,582/480 or 51 Btuh per square foot. Find 51 on the left margin and move horizontally to the intersection with a 62 MRT line, and from the point of intersection to the lower margin and read about 112 F.

With a ceiling temperature of 112 F, the MRT of the room will be 480 × 112 + 1,586 × 62; the sum divided by 2,016, or 74 F.

If an air temperature of 68 F and an MRT of 74 F should not produce satisfactory conditions, the ceiling temperature can easily be changed as necessary by changing the temperature of the circulating water.

Calculations like the preceding may also be made with the aid of Table 2. The rate at which the ceiling must radiate heat exceeds by 51 Btuh per square foot the rate at

TABLE 2. TOTAL HEAT EMISSION BY RADIATION[a]

Body or Mean Radiant Temperature F Deg	Radiation in Btu per (square foot) (hour) emitted to surroundings with a temperature of absolute zero by bodies at various temperatures and with emissivity factor e				Body or Mean Radiant Temperature F Deg	Radiation in Btu per (square foot) (hour) emitted to surroundings with a temperature of absolute zero by bodies at various temperatures and with emissivity factor e			
	e 1.00	e 0.95	e 0.90	e 0.80		e 1.00	e 0.95	e 0.90	e 0.80
30	99.7	94.7	89.8	79.7	71	137.0	130.1	123.3	109.7
35	103.9	98.7	93.6	83.1	72	137.9	131.0	124.0	110.3
40	108.0	102.8	97.2	86.4	73	138.9	132.0	124.9	111.0
45	112.5	106.9	101.3	89.0	74	140.2	133.1	126.1	112.1
46	113.3	107.7	102.0	90.8	75	141.6	134.4	127.4	113.2
47	114.3	108.6	102.9	91.5	80	147.2	140.0	132.5	117.9
48	115.2	109.5	103.8	92.3	85	152.9	145.2	137.6	122.4
49	116.0	110.3	104.5	92.8	90	158.5	150.5	142.7	126.9
50	116.9	111.0	105.3	93.6	100	170.3	161.7	153.2	136.2
51	117.9	112.0	106.4	94.4	110	182.3	173.2	164.2	146.0
52	118.8	112.9	106.9	95.1	120	195.6	185.7	176.1	156.5
53	119.8	113.8	107.8	95.9	130	210.9	200.4	189.8	168.8
54	120.6	114.6	108.6	96.6	140	224.1	212.9	201.8	179.2
55	121.7	115.5	109.4	97.3	150	238.0	226.1	214.4	190.5
56	122.6	116.4	110.3	98.1	160	252.1	239.8	226.9	201.8
57	123.5	117.4	111.3	98.9	170	271.6	258.0	244.5	217.2
58	124.4	118.2	112.0	99.6	180	289.1	274.9	260.1	231.3
59	125.3	119.0	112.8	100.3	190	307.7	292.1	276.9	246.1
60	126.3	119.9	113.8	101.1	200	326.5	310.2	293.9	261.3
61	127.1	120.7	114.4	101.8	210	349.3	331.9	314.3	279.5
62	128.2	121.8	115.3	102.6	220	373.0	354.4	335.7	298.2
63	129.1	122.6	116.2	103.3	250	439.5	417.6	395.6	351.6
64	130.1	123.5	117.1	104.1	300	577.3	548.2	519.6	461.8
65	131.0	124.4	117.9	104.8	350	743.0	705.8	668.6	594.3
66	132.1	125.5	118.8	105.8	400	945.8	898.5	850.8	756.5
67	133.0	126.4	119.7	106.4	450	1181.0	1121.0	1063.0	944.0
68	134.0	127.3	120.5	107.2	500	1470.0	1396.0	1323.0	1176.0
69	135.0	128.3	121.5	108.0	550	1798.0	1708.0	1619.0	1439.0
70	136.0	129.3	122.3	108.8	600	2181.0	2072.0	1962.0	1745.0

[a]These factors are calculated from the formula

$$q_r = e\left(\frac{0.173 \times T^4}{100{,}000{,}000}\right)$$

where

q_r = total radiation, Btu per (sq ft) (hr)
e = emissivity.
T = absolute temperature, Fahrenheit degrees.

which the ceiling receives radiant heat from its surroundings. Assuming the emissivity of the walls, floor, and ceiling to be 90 per cent of that of a *black* body, the heat radiated to the ceiling, from the surfaces whose MRT is 62 F, is (Table 2) at the rate of 115.3 Btuh per square foot; the ceiling must therefore radiate heat at the rate of 115.3 plus 51, or 166.3; its temperature must be (Table 2) between 110 F and 120 F, and, by interpolation, 112 F, as calculated.

7. *Select the medium for heating the ceiling panel.*

The medium may be electricity, steam, air, or water, but usually is air or water. If air is used it is generally heated in the basement, passed up through hollow inside walls or through ducts in those walls, allowed to flow between the ceiling and the floor above, and returned to the basement through hollow outside walls or through ducts in those walls.

If the walls and floors are constructed of hollow tile, the cells in the tile can be placed so that they will form continuous ducts through which the warm air can flow up the inside walls, then between the ceiling and the floor above, and down the outside walls. In this way the walls and ceiling become heating panels.

If water is used as the medium, the pipes through which the water circulates—almost always under forced circulation—are placed in the floor, walls, or ceiling in such a manner that as much as possible of the heat emitted by the pipes will be delivered to the space to be heated.

TABLE 3. HIGHEST SAFE SURFACE TEMPERATURES FOR HEATING PANEL

TYPE OF PANEL	SURFACE TEMPERATURE F DEG
Plastered Ceiling (Pipes Imbedded)	115
Plastered Walls (Pipes Imbedded)	120
Floor, Any Method	85
Floor, Border and Aisles	120
Iron, Hot Water Medium[a]	160
Iron, Steam Vapor[a]	180
Electrically Heated Panels[a]	200

[a]Low surface temperature radiation is recommended regardless of the heating medium employed.

Practical limits for surface temperatures of heating panels are given in Table 3.

In this example water will be selected as the medium.

8. *Determine the size, length, and location of the pipe coils in the panels.*

When hot-water pipes are imbedded in concrete slabs or attached to plastered surfaces, their rate of heat emission varies with many factors. If the pipes are imbedded in dense concrete slabs, it may be assumed that the rate of heat emission of ½-in. pipe, spaced 6 in. on centers; ¾-in. pipe, spaced 9 in. on centers; and 1-in. pipe spaced 12 in on centers; per foot of length of pipe and per degree difference between the temperature of the water in the pipe and that of the air in the space to be heated, is 0.8, 1.0, and 1.2 Btuh, respectively. If the distance between the pipes is increased, the rate of heat emission, per foot of pipe, is also increased; if the distance is doubled, the rate of heat emission is increased about 15 per cent. If the pipes are attached to plastered ceilings, the rate of heat emission is slightly less, probably about 10 per cent less, than when the pipes are imbedded in concrete slabs. The data given regarding heat emission of panels are intended as general guides for the designer. Additional experience and research are needed to develop definite and complete data. However, after a heating panel has been designed and installed, any small error can easily be corrected by modifying the temperature of the water circulating through the coils.

When the heating pipes are attached to a plastered ceiling, a portion of the heat emitted by the pipes is delivered to the space below the ceiling and a portion to the space above the ceiling. The relative quantities depend on the degree of insulation applied above the heating coils.

When the heating pipes are imbedded in a concrete floor slab a portion of the heat emitted by the pipes will flow upward into the space to be heated, and the remainder will flow downward into the ground.

When the heating pipes are placed below the concrete floor slab instead of being imbedded in the slab, a larger portion of the heat will flow into the ground, and a smaller portion into the space to be heated.

In the following example *it is assumed that the insulation above the pipe coils is such that 90 per cent of the heat emitted by the pipe coils will flow into the room and 10 per cent into the space above.*

Since the room is to receive 35,117 Btuh, and since the room is assumed to receive only 90 per cent of the heat emitted by the coils attached to the plastered ceiling, the coils must emit 35,117/0.9 or 39,000 Btuh. If ¾-in. pipe and a mean water temperature of 140 F are selected, the heat emitted, per foot of pipe, will be 0.9 (140 − 68) or 65 Btuh. The quantity of pipe required will therefore be 39,000/65 = 600 lineal feet.

The pipe coils can be arranged in any convenient manner, but should be arranged so that the temperature of the water in the pipe will vary only slightly; otherwise, the temperature distribution over the ceiling will not be uniform. Generally, it is best to arrange the pipes so as to form two-pipe reversed-return systems, as suggested by the two sketches in Fig. 10. By using 33 runs of ¾-in. pipe, welded to two 1¼ in. mains, sufficient pipe surface is secured; the ¾-in. pipes will then be spaced about 8½ in. on centers, which is satisfactory.

While coils can be designed with pipe and fitting resistances which will insure proper distribution to each coil it is advantageous to provide adjustable flow control valves or resistances for final regulation of the water temperature or flow to the various coils. It

is desirable to divide large heating systems into sections and to install valves so that individual sections can be disconnected without interfering with the operation of the system as a whole.

Part II—Radiant Heating

The term *radiant heating* is applied in this chapter to a system in which only the heat radiated from the panel is effective as in outdoor and semi-outdoor conditions.

The outstanding example of radiant heating is the transfer of heat from the sun to the earth. The sun radiates large quantities of energy of which a very small portion is intercepted by the earth. A part of the intercepted radiation is transformed into heat when it strikes the earth's

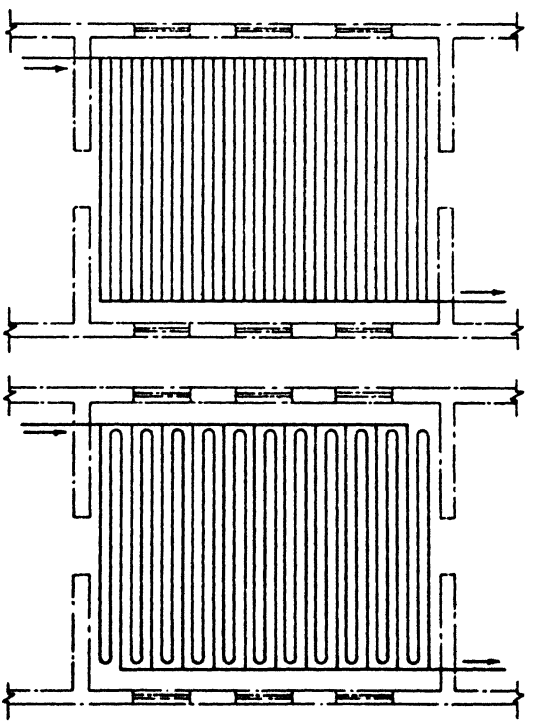

FIG. 10. ARRANGEMENT OF PIPE COIL FOR EVEN DISTRIBUTION OF PANEL TEMPERATURE

surface. In this manner *heat* is received by the earth from the sun by *radiation.*

In industry, radiant heating is employed in manufacturing processes, particularly in drying, baking, and dehydrating operations; in agriculture, it is employed to improve living and growing conditions for young plants and young animals.

The heating engineer employs radiant heat primarily in the heating of open-air schools and open-air hospitals. When a surface radiates heat, and every surface does unless its temperature is absolute zero, every point of the surface radiates heat in all directions. The total quantity of heat radiated by a point or by an elementary area is π times the quantity of heat radiated at right angles to the surface.

Thus, if in an elementary cube the upper face is the heating panel, the lower face would receive only about 32 per cent of the radiated energy and the four sides would receive each about 17 per cent.

For larger surfaces the conditions are different. If two parallel plane surfaces of considerable size are near each other, the rate of heat exchange between the two can be determined fairly accurately by means of the chart of Fig. 9. This is possible because the larger part of the heat radiated by one of the surfaces is intercepted by the other surface and only a small portion is radiated in such directions that it will not impinge upon the opposite surface.

As the distance between the two surfaces is increased, the proportion of the heat radiated by one of the parallel plane surfaces and intercepted by the other decreases almost as the square of the distance between the surfaces increases, because the intensity of heat radiation, like the intensity of light radiation, varies inversely as the square of the distance from the source of radiation.

For the purpose of designing radiant heating systems in which the heating panel is practically square and is radiating heat toward a parallel surface of equal size and shape, as shown in Fig. 11, the rate of heat exchange between the two surfaces will be equal to that shown in Fig. 9, multiplied by a factor, p, which depends upon the ratio of h to s (Fig. 11) as shown in the following table:

h/s =	1	2	3	4	5
p =	0.200	0.070	0.034	0.020	0.013

For example, if a panel 3 ft square is located parallel to, and 9 ft above, a bed in an open-air hospital, and if the temperature of the panel is 112 F and that of the bed is 70 F, the rate of heat transfer from the panel to a 9 sq ft section of the bed directly beneath the panel, will be 3.4 per cent of the rate shown in Fig. 9, or $0.034 \times 9 \times 44$, or 14 Btuh, approximately. The rate of heat transfer from the panel to a section of the bed other than the 9 sq ft directly beneath the panel will be lower than 14/9 Btuh per square foot.

This is a crude way of designing a radiant heating system for an open-air hospital, but it is sufficiently accurate, because the required temperature of the bed and the required rate of heat flow into it will vary with the temperature of the outdoor air, with the air movement over the bed, with the thickness and the character of the bedding, and with the physical condition of the patient.

A radiant heating system for an open-air school may be designed as described for the open-air hospital. The heating panel in such a case should be almost as large as the ceiling and, in order to keep the heat loss by radiation at a minimum, should be placed so that a maximum portion of the heat radiated by the panel will be directed toward the pupils and a minimum toward the outside walls and particularly the windows.

MEASUREMENT OF RADIANT HEATING

Radiant heating is intended to control the rate of radiant heat loss from the human body and should be measured by calorimetric methods.

The apparatus for this purpose consists essentially of a cylinder, maintained at the accepted mean surface temperature of the human body, together with an accurate (usually electrical) measuring of the varying rate of heat supply required to maintain this exact temperature. This instrument, the *eupatheoscope*, is readily adapted to function like a thermostat so as to turn heat on or off, when the desired temperature of 80 F, or any other predetermined surface temperature of the cylinder,

decreases or increases as a result of changes in the Operative Temperature.

For testing work, the *globe thermometer* is a useful instrument. It consists of an ordinary mercury thermometer, with its bulb placed in the center of a sphere from 6 to 9 in. in diameter, usually made of thin copper and painted black and sometimes covered with cloth. The temperature recorded by thermometer with its bulb in the center of the sphere is termed the *radiation-convection temperature.* See Chapter 11.

CONTROL OF PANEL AND RADIANT HEATING

The effectiveness of any type of control will depend largely on the time lag of the system. With warm air passing through floor ducts the time lag is usually too long for any kind of room thermostat, in fact a thermo-

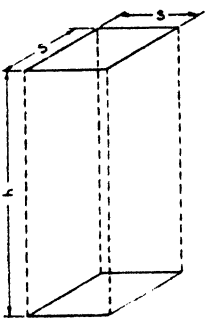

FIG. 11. EFFECT OF HEIGHT UPON RADIATION RECEIVED FROM A PANEL

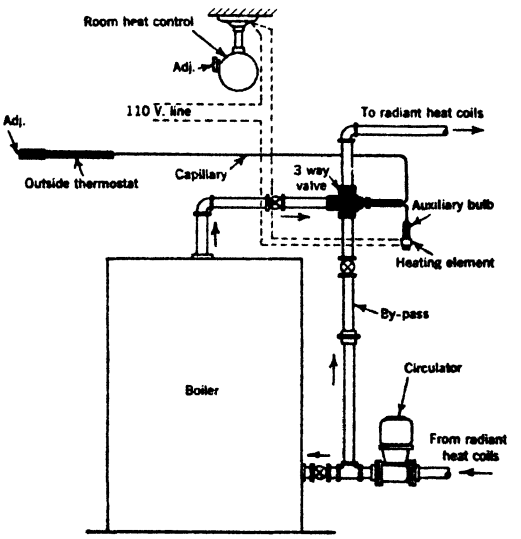

FIG. 12. TYPICAL PANEL AND RADIANT HEAT CONTROL SYSTEM

stat will not prove suitable with any system if the building is constructed with massive brickwork and masonry, unless it operates in conjunction with a time control responsive to changes in outside conditions.

The heat emitted by hot water pipes imbedded in the plaster of the ceiling and walls or in the concrete base of a floor can be effectively controlled by an instrument designed to modulate the temperature of the water circulating in the system according to the outside conditions. Metal panels which can be installed in the ceiling or side walls may be either controlled by an instrument responsive to outside weather conditions or by a specially designed instrument responsive to both air temperature and radiation. Any purely *on or off* control system is not recommended for panel heating.

A typical control system operated from an outside thermostat and supplemented with a room heat control instrument is illustrated in Fig. 12. The outside thermostat modulates the temperature of the circulating water in the coils by mixing some of the hot water leaving the boiler with a proportionate amount of return water which is diverted to the three-way valve.

One type of room instrument consists of a blackened copper sphere of 6 or 8 in. in diameter, in which a cylindrical sump contains a volatile liquid. A small electric heating coil creates in the sphere a vapor pressure which remains constant as long as the total heat loss from the sphere is at the desired rate. If the Operative Temperature becomes too high for comfort, a greater vapor pressure results from the smaller heat loss from the sphere. This acts on a diaphragm and reduces the supply of heat to the room. With too low an Operative Temperature the reverse action occurs. A similar instrument which has an electric heating element for warming the air inside the sphere and the thermostat operated switch is also used for controlling room conditions.

In addition to a thermostatically controlled device for modulating the temperature of the circulating water, it is advantageous to insert in each coil a locked flow control or adjustable resistance to give uniform conditions throughout all rooms. Owing to unforeseen difficulties with varying frictional losses in pipes, emission factor, and exposures, it is an advantage to be able to regulate permanently the flow through each circuit by means of a key operated valve as indicated in Fig. 4.

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Chapter 32

FANS

Classification, Performance, Fan Efficiency, Characteristic Curves, System Characteristics, Selection of Fans, Fan Designations, Control, Motive Power, Attic Fans

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IN heating, ventilating, and air conditioning practice, fans and blowers are used to produce air flow. All fans or blowers are classified according to the direction of air flow through the fan with relation to the axis of rotation and are either of the (1) *axial flow* or *propeller* type, in which the flow is parallel to the axis, or (2) *radial flow* or *centrifugal* type, in which the flow is at right angles to the axis.

Axial flow fans are made in various designs and sizes. The form and number of blades may vary for impellers of the same or different diameters. The blades may be of uniform thickness and made of cast or sheet metal, and either flat or cambered or of screw form; or they may vary in thickness, in the latter case usually being designed to conform to so-called *airfoil* sections of known characteristics, similar to those which have been developed for airplane propellers. Likewise, blade angle, or the angular relation of the blades to the plane of rotation, varies over a wide range. For operation against comparatively high pressures, it is customary to resort to enlarged hubs in proportion to fan diameter (large hub ratio) and correspondingly short blade length. The term *disc fan* has sometimes been loosely applied to such large hub fans, though it has long been generally used in connection with any propeller fan of comparatively short axial length whose blades are relatively flat; in other words, for fan wheels which occupy a space which is more or less disc-shaped. Single stage air foil axial flow fans can operate at pressures up to 4 in. at a quite low noise level and, at considerably higher pressures, they are comparable in regard to noise to the centrifugal fan type.

Radial flow or *centrifugal fans* used in heating, ventilating, and air conditioning practice, are in general of two types; one with forward-sloped blades, and the other with backward-sloped blades. Many modifications may be made in the proportions, the curvature, and the slope or angularity of the blades. The slope or angularity of the blades determines the operating characteristics of a fan; a forward-curved or sloped blade is found in a fan having low speed operating characteristics, while a backward-curved or sloped blade is found in a fan having higher speed operating characteristics.

A wide variety of heating, ventilating, and air conditioning systems creates a wide variety in the demands that have to be met by the fan or blower. The requirement may be to move small or large quantities of air against little or no resistance, or to move small or large quantities of air against higher resistance. Between the two limits innumerable specific requirements must be met. Although fans of any class in either of the two general types can in general be made to perform the same duty, mechanical difficulties, space and noise limitations, efficiency and power limitations usually determine the selection.

FAN PERFORMANCE

Fans of all types follow certain laws of performance which are useful in predicting the effect upon performance of changes in the conditions of operation, the duty required of the installation, or the size of the equip-

ment due to the space, power, or speed limitations. The following laws in which Q = air volume and P = static, velocity or total pressure, apply to all types of fans:

1. Variation in Fan Speed:
   Constant Air Density—Constant System
   (*a*) Q: Varies as fan speed.
   (*b*) P: Varies as square of fan speed.
   (*c*) Power: Varies as cube of fan speed.

2. Variation in Fan Size:
   Constant Tip Speed—Constant Air Density
   Constant Fan Proportions—Fixed Point of Rating
   (*a*) Q: Varies as square of wheel diameter.
   (*b*) P: Remains constant.
   (*c*) RPM: Varies inversely as wheel diameter.
   (*d*) Power: Varies as square of wheel diameter.

3. Variation in Fan Size:
   At Constant RPM—Constant Air Density
   Constant Fan Proportions—Fixed Point of Rating
   (*a*) Q: Varies as cube of wheel diameter.
   (*b*) P: Varies as square of wheel diameter.
   (*c*) Tip Speed: Varies as wheel diameter.
   (*d*) Power: Varies as fifth power of diameter.

4. Variation in Air Density:
   Constant Volume—Constant System
   Fixed Fan Size—Constant Fan Speed
   (*a*) Q: Constant.
   (*b*) P: Varies as density.
   (*c*) Power: Varies as density.

5. Variation in Air Density:
   Constant Pressure—Constant System
   Fixed Fan Size—Variable Fan Speed
   (*a*) Q: Varies inversely as square root of density.
   (*b*) P: Constant.
   (*c*) RPM: Varies inversely as square root of density.
   (*d*) Power: Varies inversely as square root of density.

6. Variation in Air Density:
   Constant Weight of Air—Constant System
   Fixed Fan Size—Variable Fan Speed
   (*a*) Q: Varies inversely as density.
   (*b*) P: Varies inversely as density.
   (*c*) RPM: Varies inversely as density.
   (*d*) Power: Varies inversely as square of density.

Examples 1 to 4 illustrate the application of the preceding fan laws.

Example 1. **A certain fan delivers 12,000 cfm at a static pressure of 1 in. of water when operating at a speed of 400 rpm and requires an input of 4 hp. If in the same installation 15,000 cfm are desired, what will be the speed, static pressure, and power?**

$$\text{Speed} = 400 \times \frac{15{,}000}{12{,}000} = 500 \text{ rpm}$$

$$\text{Static pressure} = 1 \times \left(\frac{500}{400}\right)^2 = 1.56 \text{ in.}$$

$$\text{Power} = 4 \times \left(\frac{500}{400}\right)^3 = 7.81 \text{ hp.}$$

Example 2. **A certain fan delivers 12,000 cfm at 70 F and normal barometric pressure (density 0.075 lb per cubic foot) at a static pressure of 1 in. of water when operating at**

400 rpm, and requires 4 hp. If the air temperature is increased to 200 F (density 0.0602 lb) and the speed of the fan remains the same, what will be the static pressure and power?

$$\text{Static pressure} = 1 \times \frac{0.0602}{0.075} = 0.80 \text{ in.}$$

$$\text{Power} = 4 \times \frac{0.0602}{0.075} = 3.20 \text{ hp}$$

Example 3. If the speed of the fan of *Example 2* is increased so as to produce a static pressure of 1 in. of water at the 200 F temperature, what will be the speed, capacity, and power?

$$\text{Speed} = 400 \times \sqrt{\frac{0.075}{0.0602}} = 446 \text{ rpm}$$

$$\text{Capacity} = 12{,}000 \times \sqrt{\frac{0.075}{0.0602}} = 13{,}392 \text{ cfm (measured at 200 F)}$$

$$\text{Power} = 4 \times \sqrt{\frac{0.075}{0.0602}} = 4.46 \text{ hp.}$$

Example 4. If the speed of the fan of the previous examples is increased so as to deliver the same weight of air at 200 F as at 70 F, what will be the speed, capacity, static pressure, and power?

$$\text{Speed} = 400 \times \frac{0.075}{0.0602} = 498 \text{ rpm}$$

$$\text{Capacity} = 12{,}000 \times \frac{0.075}{0.0602} = 14{,}945 \text{ cfm (measured at 200 F)}$$

$$\text{Static pressure} = 1 \times \frac{0.075}{0.0602} = 1.25 \text{ in.}$$

$$\text{Power} = 4 \times \left(\frac{0.075}{0.0602}\right)^2 = 6.20 \text{ hp.}$$

Law of Homologous Fans

The laws applying to different sizes of homologous fans are as follows:

Capacity varies as the ratio of size cubed, times the ratio of the rpm.

Pressure varies as the ratio of size squared, times the ratio of the rpm squared.

Horsepower varies as the ratio of the size to fifth power, times the ratio of the rpm cubed.

Example 5. Assuming that a fan with a 36 in. diameter blast wheel will deliver 12,000 cfm at 70 F at 1 in. static pressure, requiring 4.0 brake hp when operating at 400 rpm, what is the capacity, pressure and horsepower of a homologous fan having a 45 in. wheel at the same speed?

$$\text{Capacity} = \left(\frac{45}{36}\right)^3 \times \left(\frac{400}{400}\right) \times 12{,}000 = 23{,}400 \text{ cfm}$$

$$\text{Static Pressure} = \left(\frac{45}{36}\right)^2 \times \left(\frac{400}{400}\right)^2 \times 1 = 1.56 \text{ in.}$$

$$\text{Horsepower} = \left(\frac{45}{36}\right)^5 \times \left(\frac{400}{400}\right)^3 \times 4 = 12.2 \text{ hp}$$

FAN EFFICIENCY

The efficiency of a fan may be defined as the ratio of the horsepower output to the horsepower input.

The horsepower output is expressed by the formula:

$$\text{Air Horsepower}^1 = \frac{\text{cfm} \times \text{total pressure in inches of water}}{6356} \quad (1)$$

When the static pressure is used in the computation in place of total pressure it is assumed that this represents the useful pressure and that the velocity pressure is lost in the piping system and in the air which leaves the system. Since in most installations a higher velocity exists at the fan outlet than at the point of delivery into the atmosphere, some of the velocity pressure at the fan outlet may be utilized by conversion to static pressure within the system, but, owing to the uncertainty of friction losses which occur at the places where changes in velocity take place, the amount of velocity pressure which is actually utilized is seldom known, and the static pressure alone may best represent the useful pressure. In the standards for published capacity tables as adopted by the *National Association of Fan Manufacturers*, the term *static pressure* refers to the true resistance to air flow. Such tables charge both the inlet and outlet velocity of the fan to the fan performance, and may be used directly where the static pressure of the system as calculated represents only the actual resistance to flow of the air.

The efficiency based upon static pressure is known as the static efficiency and may be expressed as follows:

$$\text{Static Efficiency}^1 = \frac{\text{cfm} \times \text{static pressure in inches of water}}{6356 \times \text{Horsepower input}} \quad (2)$$

Different fans may develop the same capacity against the same static pressure and with the same power input, and therefore operate at the same static efficiency, while maintaining different outlet velocities. Where a high outlet velocity is desirable or can be utilized effectively, the static efficiency fails to be a satisfactory measurement of the performance. In many applications of propeller fans, air is circulated without encountering resistance and no static pressure is developed. The static efficiency is zero and its calculation is meaningless. Because of such situations where the static efficiency fails to indicate the true performance, many engineers prefer to base the calculation of efficiency upon the total pressure. This efficiency is variously known as the total, or mechanical efficiency, and may be expressed as follows:

$$\text{Mechanical or Total Efficiency}^1 = \frac{\text{cfm} \times \text{total pressure in inches of water}}{6356 \times \text{Horsepower input}} \quad (3)$$

CHARACTERISTIC CURVES

In the operation of a fan at a fixed speed the static and total efficiencies vary with any change in the resistance which is imposed. With different designs the peak of efficiency occurs when the fans deliver different percentages of their wide-open capacity. Variations in efficiency accompany variations in pressures and power consumption which are characteristic of the individual designs and which are influenced particularly by the shape and angularity of the blades. Such variations in pressure, power, and efficiency are shown by characteristic curves.

Characteristic curves of fans based upon tests performed in accordance with the Standard Test Code for Centrifugal and Axial Fans[1] prepared jointly by the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS and the *National Association of Fan Manufacturers* are generally plotted to show total and static pressure, mechanical and static efficiency, and horsepower in relation to air delivery as a basis. Results may also

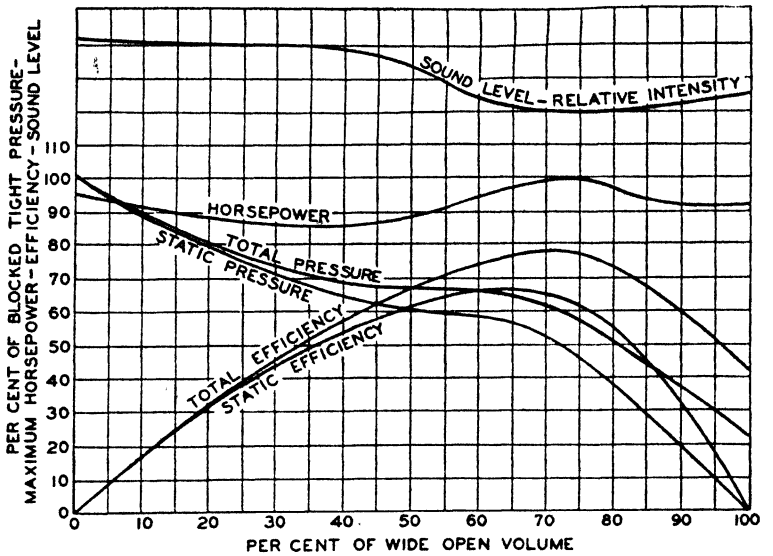


FIG. 1. OPERATING CHARACTERISTICS OF AXIAL FLOW AIRFOIL TYPE FAN

be plotted against per cent of wide open volume or discharge. Examples of fan performance curves are shown in Figs. 1, 2 and 3.

In the selection of all but very small fans, power consumption is usually a major consideration. It must be borne in mind that the horsepower at peak efficiency alone may be misleading, as actual operation is apt to occur at some point on the pressure-volume curve varying considerably from that specified, due to inaccuracies of the estimated system resistance

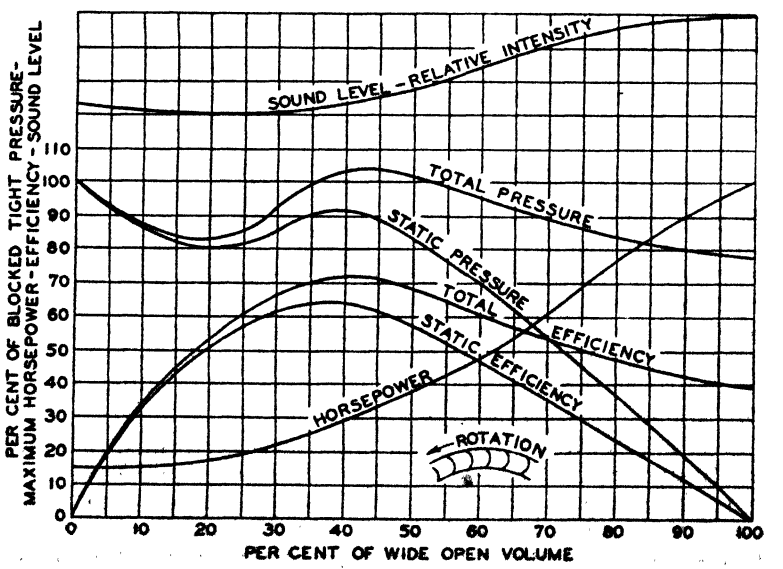


FIG. 2. OPERATING CHARACTERISTICS OF A FAN WITH BLADES CURVED FORWARD

or to fluctuating resistance caused by damper or louver adjustments. To cope with such variations a fan should be selected having a high efficiency over a wide range, that is, a *flat* or broad efficiency curve is more desirable than a sharp or narrow curve which, though reaching a high peak, falls off rapidly to either side of a narrow range. When the point of operation varies only within narrow limits and both volume and pressure requirements are accurately known in advance, the designer can select a fan operating at maximum efficiency, irrespective of performance over the entire range.

Generally, fans are selected either at the peak of the static efficiency or to the right of the peak depending on the requirements of the particular installation. Fans selected to the right of the peak will be smaller but will require more power, run at higher speeds and may have a higher sound rating. Where first cost is important and added horsepower and noise are

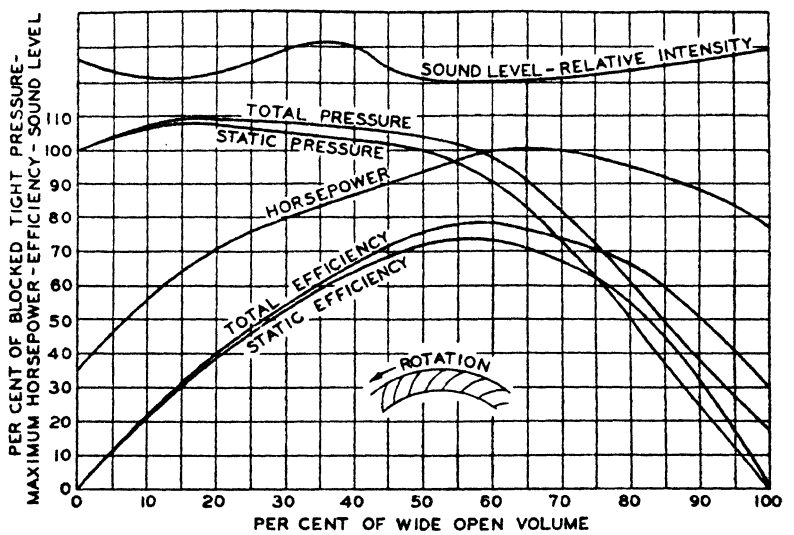


FIG. 3. OPERATING CHARACTERISTICS OF A FAN WITH BLADES CURVED BACKWARD

not important, smaller fans may be used. Where efficient and quiet operations are most important, fans are selected at or near the peak of the static efficiency curve. Fans are not ordinarily selected to the left of the peak of the static efficiency curve as this results in larger, more costly fans, requiring more power and in some cases producing objectionable noise.

The curves in Figs. 1, 2, and 3 show operating characteristics for axial flow and two classes of centrifugal fans, namely, forward-curved multiple blade and backward-inclined blade design, for comparison purposes. These curves are not applicable for rigid comparison or actual selection, but are shown to indicate variations in operating characteristics.

The curves in Fig. 1 of a *typical axial flow* fan show characteristics of non-overloading horsepower and high efficiency. These results are obtained by producing a more uniform pressure throughout the blade annulus, so that back flow does not occur except at high pressures. This avoidance in turbulence has a tendency to reduce noise. Fans of this type are operating against static pressures as high as 4 in. water. The

capacity and efficiency of axial flow fans when operating above the low pressure range can be improved by the use of either inlet or outlet guide vanes or both. The effect of such vanes is to increase the level of the pressure volume curve, and properly designed vanes on the discharge side of the fan have the advantage of eliminating the rotational component of the air stream, thus restoring uniform axial flow. As high pressures usually require large hubs in proportion to the fan diameter, performance is improved by the use of round-nosed or conical forms mounted coaxially with the direct-connected fan (sometimes partly or wholly enclosing the motor) so as to make the changes in velocity to and from the fan blade annulus as uniform as space conditions permit. When axial flow fans are installed in ducts, provisions may be made to install the driving motor outside by employing slots in the duct to permit a belt drive from motor to fan sheave, or by extending the shaft for a direct-connected motor placed outside of a Y fitting or elbow in the duct system.

The *forward-curved multiblade* fan and the *backward-curved* type are used extensively in heating, ventilating, and air conditioning work. The forward-curved type has a low peripheral speed and a large capacity. (See Fig. 2.) The point of maximum efficiency for this fan occurs near the point of maximum pressure. The static pressure drops consistently from the point of maximum efficiency to full open operation. The power curve rises continuously from low to peak capacity and, if reasonable care is exercised in calculating resistance, a moderate reserve in power in the motor selection will prevent overloading.

The *backward-sloped type* includes the full backward-curved blade and the double-curved blade having a forward-curved heel and a backward-curved tip. This type has steep pressure curves, non-overloading power characteristics, and relatively high speed (see Fig. 3). This fan operates at a peripheral speed approximately 175 to 200 per cent of that of the forward-curved multiblade fan for like performance. Pressure curves for this type begin to drop at very low capacity, with the most rapid drop beginning at about 60 per cent of wide open volume. The steep portions of the pressure curves tend to produce nearly constant capacity under changing pressures. Where wide fluctuations in demand occur, especially where the regulation is obtained by damper control and particularly through by-passes, this type of fan is desirable to prevent overloading of motor. The maximum power requirement occurs at about the maximum efficiency. Consequently a motor selected to carry the load at this point will be of sufficient capacity to drive the fan over its full range of capacities at a given speed. The high speed of this type makes it adaptable for direct connected electric motor drives.

Between the extremes of the forward and backward curved blade type centrifugal fans there exists a number of modified designs differing in angularity and in the shape of the blades. Characteristic curves of these types show varying degrees of similarity to the curves in Figs. 2 and 3.

SYSTEM CHARACTERISTICS

Any ventilating system consisting of duct work, heaters, air washers, filters, etc., has a system characteristic which is individual to that system and is independent of any fan which may be applied to the system. This characteristic may be expressed in curve form in exactly the same manner that fan characteristics may be shown. Typical system characteristic curves are shown as A, B and C in Fig. 4. These curves are drawn to

follow the simple parabolic law in which the static pressure or resistance to flow of air varies as the square of the volume flowing through the system. Heating and ventilating systems follow this law very closely and no serious error is introduced by its use.

When a constant speed fan curve for a given size fan is super-imposed upon a system characteristic curve, the relation between the two is at once apparent. The only point common to the two curves is the point at the intersection of the system characteristic curve and the fan characteristic curve, and it is at this point that the combination will operate. In Fig. 4, system characteristic curves A, B and C cross the fan characteristic curve at points X, Y and Z. The fan whose curve is shown, when applied to systems having characteristic curves A, B and C, will deliver 10,000, 13,000 or 16,400 cfm respectively.

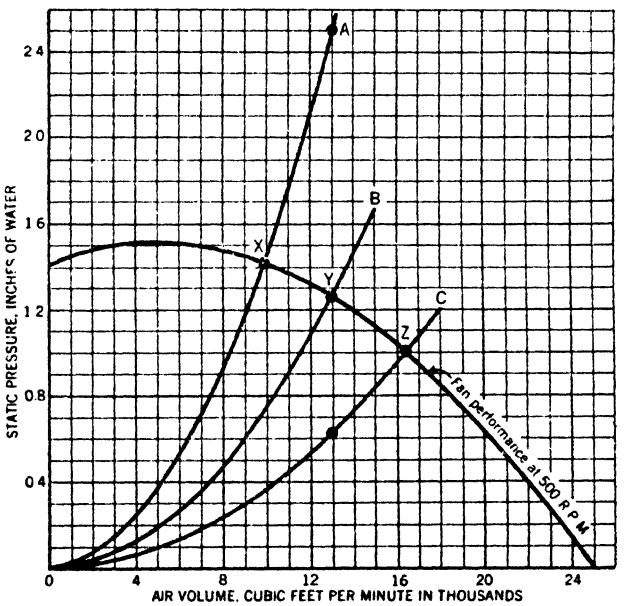


FIG. 4. PARABOLIC SYSTEM CHARACTERISTIC CURVES

The curves in Fig. 4 also illustrate the effect of errors which may be made in calculating the resistance of a ventilating system. For instance, if a given system requires 13,000 cfm and the resistance to flow of the system has been computed as 1.25 in. static pressure, such a system would be represented by system characteristic curve B in Fig. 4. If a 100 per cent error had been made and the resistance were 2.5 in. instead of 1.25 in., then the system characteristic would be as shown in curve A and would cross the fan curve at 10,000 cfm. Such an error would cause the flow of air to be decreased from a design volume of 13,000 cfm to 10,000 cfm. If the resistance to flow had been over estimated and the resistance actually were 0.625 in., the system characteristic curve would be as shown in curve C and the fan would deliver 16,400 cfm to the system instead of the design volume of 13,000 cfm.

In this example extreme errors have been selected to emphasize the effect the square function of the system characteristic has in maintaining the fan performance within comparatively narrow limits. In the first

example a system estimated at half what it should have been, resulted in a drop of 23 per cent in volume; and in the second example, a system estimated at twice what it should have been resulted in an increase of 26 per cent in volume.

In some instances fans may be applied to variable flow systems. In such cases the limiting systems may be plotted and the effect on fan performance examined. For instance, a system might have a characteristic curve between A, shown in Fig. 4, as one limit, and B as the other limit. The fan performance will then fall between points X and Y on the fan curve at a point determined by the system characteristics at that particular time. If A and B are the limiting characteristic curves of the systems, the fan performance will never be outside the points X or Y.

SELECTION OF FANS

The following information is required to select the proper type of fan:

1. Cubic feet of air per minute to be moved.
2. Static pressure required to move the air through the system.
3. Density of air to be moved.
4. Type of motive power available.
5. Whether fans are to operate singly or in parallel on any one duct.
6. What degree of noise is permissible.
7. Nature of the load, such as variable air quantities or pressures.

In order to facilitate the choice of apparatus, the various fan manufacturers supply fan tables or curves which usually show the following factors for each size of fan operating against a wide range of static pressures: (1) volume of air in cubic feet per minute (68 F, 50 per cent relative humidity, 0.075 lb per cubic foot), (2) outlet velocity, (3) revolutions per minute, (4) brake horsepower, (5) tip or peripheral speed, and (6) static pressure. The most efficient operating point is usually shown by either bold-face or italicized figures in the capacity tables.

Other important factors to be considered in selecting fans are: (1) efficiency, (2) space occupied, (3) sound emission, (4) first cost, and

TABLE 1. GOOD OPERATING VELOCITIES AND TIP SPEEDS FOR MULTIBLADE VENTILATING FANS

Static Pressure Inches of Water	Forward Curved Blade Fans		Backward Tipped and Double Curved Blade Fans	
	Outlet Velocity Feet per Minute	Tip Speed Feet per Minute	Outlet Velocity Feet per Minute	Tip Speed Feet per Minute
¼	1000–1100	1520–1700	800–1100	2600–3100
⅜	1000–1100	1760–1900	800–1150	3000–3500
½	1000–1200	1970–2150	900–1300	3400–4000
⅝	1200–1400	2225–2450	1000–1500	3800–4500
¾	1300–1500	2480–2700	1100–1650	4200–5000
⅞	1400–1700	2660–2910	1200–1750	4500–5300
1	1500–1800	2820–3120	1200–1900	4800–5750
1¼	1600–1900	3162–3450	1300–2100	5300–6350
1½	1800–2100	3480–3810	1400–2300	5750–6950
1¾	1900–2200	3760–4205	1500–2500	6200–7550
2	2000–2400	4000–4500	1600–2700	6650–8050
2¼	2200–2600	4250–4740	1700–2800	7050–8550
2½	2300–2600	4475–4970	1800–2950	7450–9000
3	2500–2800	4900–5365	2000–3200	8200–9850

(5) speed (both peripheral and revolutions per minute). These factors are not necessarily shown in the order of importance. In some installations space occupied may be of first importance. In others lowest power consumption is desirable. In many cases quietness of operation of the entire system is essential. Practically all fans operate at their lowest sound level when selected at or near the peak of the static efficiency so that in selecting a fan for highest static efficiency the quietest operating range of the fan will also be obtained. Table 1 shows desirable outlet velocities and tip speeds, or peripheral velocities, for various static pressures. Fans selected accordingly will operate at or near the peak of the static efficiency with resulting low power consumption and noise levels. Smaller fans with higher outlet velocities may be used if the conditions are such as to warrant the additional power and increased sound level. When space for duct expansion from a fan outlet is not available there may be advantages in selecting a larger fan for reducing duct noises, although lower outlet velocities generally result in lower fan efficiencies which cannot always be justified on the basis of increased cost and space. Fans for schools, churches, residences, and all public buildings should be selected for lower outlet velocities and tip speeds than would be required for other types of installations.

Having selected a fan for its quietest operating point consistent with the requirements of the installation (note sound level curves on Figs. 1, 2 and 3), it must be recognized that ventilating fans, even so selected, emit noise and precautions must be taken in the installation of the fans to prevent this noise from being transmitted to occupied portions of the building. Fans operating against high static pressures produce more noise than fans operating against low static pressures. Consequently, from a noise standpoint, the system should be designed to operate against the lowest static pressure possible. In many modern air conditioning systems it is necessary to introduce devices into the air stream for conditioning the air in various ways, the result of which is to set up a rather high static pressure against which the fan must operate. In such cases the sound level at the fan may be too high to be neglected and special sound treatment of the installation must be considered. When a fan is operating against higher pressures it should be located in a room either removed from the occupied areas, or in a room which has been acoustically treated to prevent sound being carried through the walls to adjoining spaces. The fan should be mounted on a resilient base along with its driving motor to absorb any noise or vibration which might be transmitted to the floor and thence to the building structure. All ducts should be connected to fans with unpainted canvas, or other flexible material, to prevent any vibrations being transmitted to the duct work. Ducts leading into the fan room or from the fan should be acoustically treated on the interior and in special cases should be provided with sound traps or filters. Many ventilating systems encounter noises which are connected with the fan in no way. Noises due to high duct velocities, abrupt turns, grilles, etc., may be present. Treatment of such problems is covered in Chapter 42.

If double width, double inlet fans are selected, care must be taken that both inlets have the same free area. If one inlet of a fan is obstructed more than the other, the fan will not operate properly, as one half of the wheel will deliver more air than the other half. Proper installation and location are as important as the selection of the size of fan for that particular installation. All fans will work according to their characteristic curves if properly selected and properly installed and operated.

FAN DESIGNATIONS

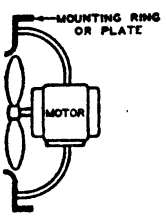
Fig. 5 shows the names and definitions of types of fans recently distributed by the *National Association of Fan Manufacturers* [2].

In order to prevent misunderstandings, which may cause delays and losses, the arrangements and designations adopted by the *National Association of Fan Manufacturers* [3] and indicated in Figs. 6 and 7 should be used.

FAN CONTROL

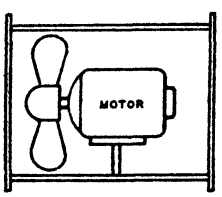
In some heating and ventilating systems it is desirable to vary the volume of air handled by the fan, and this may be accomplished by a number of methods. Where the change is made infrequently, the pulley or sheave on the driving motor, or fan, may be changed to vary the speed of the fan and alter the air volume. Dampers may be placed in the duct system to vary the volume. Variable speed pulleys or transmissions, such as fan belt change boxes, electric or hydraulic couplings, may be used to vary the fan speed. Variable speed motors and variable fan inlet vanes may also be used to adjust the fan volume. All of these methods will give control. From a power consumption standpoint, a reduction of the fan speed is most efficient. Inlet vanes save some power and dampers save the least. From the standpoint of first cost, dampers usually are the lowest in cost. In some installations adjustments of volume are desirable

FIG. 5. NAMES AND DEFINITIONS OF TYPES OF FANS



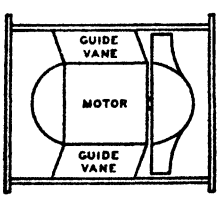
Propeller Fan

A propeller fan consists of a propeller or disc type wheel within a mounting ring or plate and including driving mechanism supports either for belt drive or direct connection.



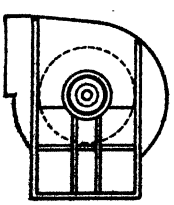
Tubeaxial Fan

A tubeaxial fan consists of a propeller or disc type wheel within a cylinder and including driving mechanism supports either for belt drive or direct connection.



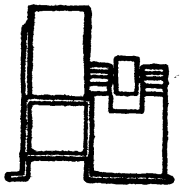
Vaneaxial Fan

A vaneaxial fan consists of a disc type wheel within a cylinder, a set of air guide vanes located either before or after the wheel and including driving mechanism supports either for belt drive or direct connection.



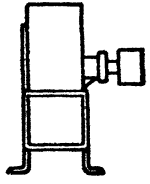
Centrifugal Fan

A centrifugal fan consists of a fan rotor or wheel within a scroll type of housing and including driving mechanism supports either for belt drive or direct connection.



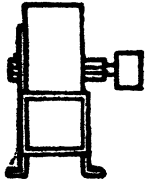
Arr. 1.
For belt drive.

Wheel overhung. Bearings on pedestal.



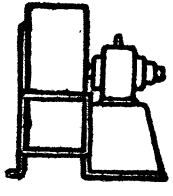
Arr. 2.
For belt drive.

Pulley and wheel overhung. Bearings in bracket on fan housing. Made only in smaller sizes for reversible discharge



Arr. 3.
For belt drive.

Pulley overhung. Bearings supported on fan housing.

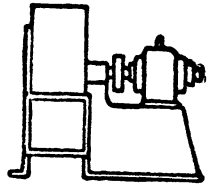


Arr. 4.
For direct drive.

Wheel overhung. No bearings on fan. Wheel mounted on motor or engine shaft. Pedestal for motor or engine.

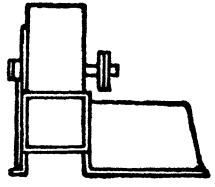
Arr. 5.
For direct drive.

Wheel overhung. Includes housing, wheel, shaft, one intermediate bearing, flanged coupling and pedestal only for motor or engine.



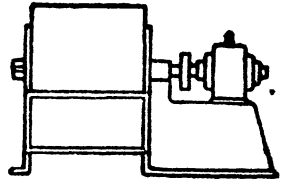
Arr. 6.
For direct drive.

Three-bearing arrangement with fan bearing at inlet side. Includes housing, wheel, shaft, one bearing (in inlet), rigid coupling, and pedestal only for motor or engine.



Arr. 7.
For direct drive.

Similar to Arr. 6, but with two bearings on fan, and flexible instead of rigid coupling.



Arr. 8.
Similar to Arr. 5.

But with two bearings on pedestal with motor, and flexible instead of rigid coupling.

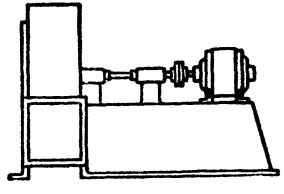


FIG. 6. ARRANGEMENT OF FAN DRIVES

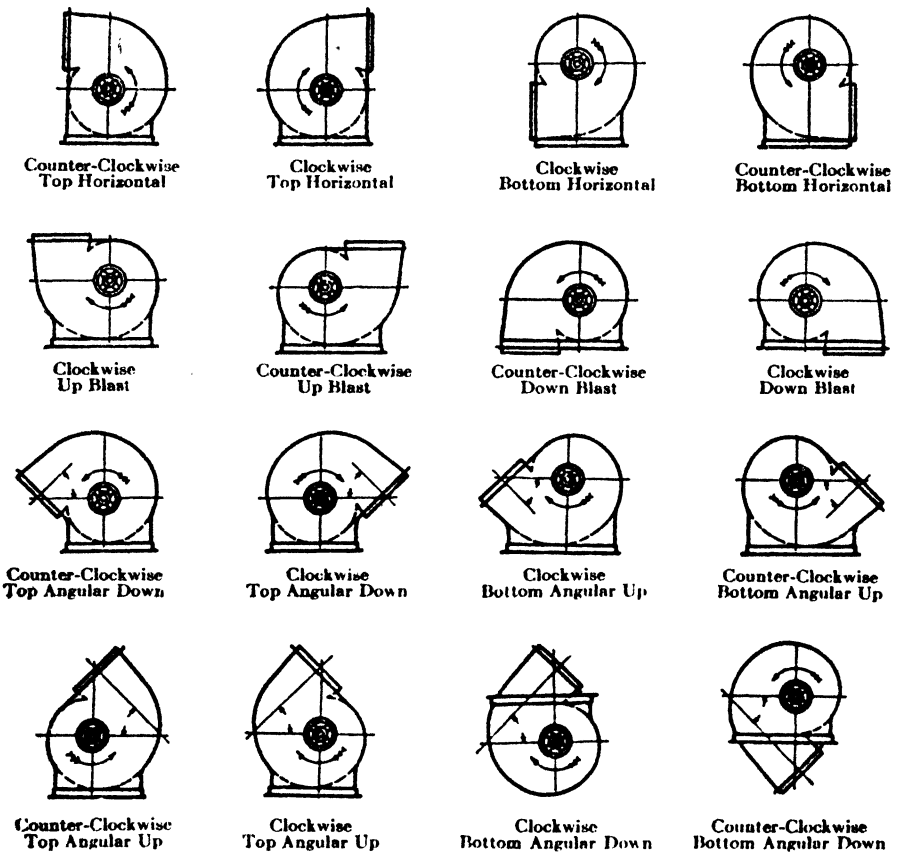


FIG. 7. DESIGNATION OF DIRECTION OF ROTATION AND DISCHARGE

Note: Direction of Rotation is determined from the drive side for either single or double width or single or double inlet fans. (The driving side of a single inlet fan is considered to be the side opposite the inlet regardless of the actual location of the drive.)

at various times during the day or continuously. In others an increased supply of air in summer over that needed in winter is demanded. The demands of each case will dictate which type of control is most desirable. Where noise is a factor, lowering the fan speed if possible is preferred as a control means, because of the resulting reduction in sound level.

MOTIVE POWER

Heating, ventilating and air conditioning fans are usually driven by electric motors, although other prime movers may be used. The small sizes of fans, and especially those operating in the higher speed range, are equipped with direct-connected motors. For larger size fans and those operating at lower speed V-belt drives are generally used.

In selecting the size of motor for operating a fan, it is advisable to select at least the standard size next larger than the fan requirements. Direct-connected motors do not require so great a safety factor as belted units. Justification for liberal power provision exists only in systems where it is possible that larger volumes of air may be required at intervals

and made available by use of by-pass dampers, thus greatly reducing the system resistance. If such a system includes a fan with forward-curved blades, it would be necessary that the motor be sized for the maximum volume and duty. If such a system includes fans with backward-curved blades, the volume peak would not make it necessary to provide additional motor power. In selecting fans for such a system, sound ratings should be given careful consideration.

Where a system is constant, and has no provision for volume change that would materially reduce the resistance, and when the resistance calculations are reasonably accurate, there is no necessity for too liberal a motor allowance, even where fans with forward-curved blades are used, if the fan has been properly selected. Fig. 4 shows that the system resistance varies as the square of the volume and the fan static pressure varies approximately inversely as the volume, thus greatly offsetting the trend toward both increase in air delivery and motor load. Reference to Fig. 4 indicates that there is no justification for allowing large spare motor capacity, and it is generally more economical to operate motors well loaded.

ATTIC FANS

Attic fans are used during the warm months of the year to draw large volumes of outside air through a house and offer a means of using the comparative coolness of outside evening and night air to lower the inside temperature.

Because the low static pressures involved are usually less than $\frac{1}{8}$ in. of water, disc or propeller fans are generally used instead of the blower types. The fans should have quiet operating characteristics, and they should be capable of giving 20 to 30 room air changes per hour in northern areas. In the South the usual specification requires one air change per minute which provides appreciable air movement in addition to lowering the inside air temperatures [4].

Types

Open attic fans are units in which the fan is installed in a gable or dormer of the attic and one or more grilles are provided in the floor of the attic, permitting air to flow from the hall below. Outdoor air, which enters the house through open windows, is drawn into the attic through the grilles, and is discharged outside by the fan. An attic stairway may be used in place of the grilles. It is essential that the roof and the attic walls be free from air leaks.

Boxed-in fans are units in which the fan is installed within the attic in a box or housing directly over a central ceiling grille, or in a bulkhead enclosing an attic stair. The fan may be connected by a duct system to the grilles in individual rooms. Outdoor air entering through the windows of the rooms below is discharged into the attic space and escapes to the outside through louvers, dormer windows, or screened openings.

Another version of the attic fan is the *window fan* for use when attic application is not feasible or no attic is available. Supplied with a perforated or expanded metal enclosure and mounted in either the upper or lower window section, this fan is easy to install or transfer.

The locations of the fan, the outlet openings, and grilles should be selected after consideration of the room and attic arrangements in order to give uniform air distribution in the individual rooms served. If the outlet for the air is not on the side away from the direction of the pre-

vailing wind as in the case of the boxed-in fan, openings should be provided on all sides. Kitchens should be separately ventilated because of the fire hazard, and to prevent the spread of cooking odors.

The window fan may be located in a hall or an unused bedroom. Noise of operation is more of a problem with the window fan than with the attic type, although care should be taken to locate either type of fan so that occupants are not disturbed.

These fans range in capacity from 3,000 to 30,000 cfm. The window type usually does not exceed 8000 cfm, while the most generally used attic type ranges from 8000 to 16,000 cfm. Power consumption is under 50 watts an hour per 1000 cfm of rated output for the 8000 cfm fan and larger, while the watts input for smaller fans is greater than this figure. Improved results can be secured with the window fan by closing off parts of the house where ventilation is not desired.

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[2]—Recommendations adopted by the *National Association of Fan Manufacturers.*

[3]—Supplement No. B to Form X-12, *National Association of Fan Manufacturers.*

[4]—Comfort Cooling with Attic Ventilating Fans, by G. B. Helmrich and G. H. Tuttle (A.S.H.V.E. TRANSACTIONS, Vol. 40, 1934, p. 155). A.S.H.V.E. RESEARCH REPORT No. 979—Study of Summer Cooling in the Research Residence for the Summer of 1933, by A. P. Kratz and S. Konzo (A.S.H.V.E. TRANSACTIONS, Vol. 40, 1934, p. 167). A.S.H.V.E. RESEARCH REPORT No. 1198—The Effect of Attic Fan Operation on the Cooling of a Structure, by W. A. Hinton and A. F. Poor (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 145). The Installation and Use of Attic Fans, by W. H. Badgett (Agricultural and Mechanical College of Texas, *Bulletin* No. 52, 1940).

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Chapter 33

AIR CLEANING DEVICES

Dust and Lint, Classification of Air Cleaning Media, Viscous Impingement Type Cleaners, Automatic Viscous Filters, Dry Air Filters, Electric Precipitators, Performance and Testing, Selection and Maintenance, Methods of Installation, Safety Requirements, Adsorption of Vapors

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AN air cleaner is a device for removing solid matter from a stream of air. This solid matter includes fibrous material such as lint, hair, dust, fumes, smoke, cinders, etc. The character of these airborne solids varies with the locality, as wind direction and velocity, industrial activity, etc. Information on air pollution and purification will be found in Chapters 10 and 12 and air sterilization in Chapter 13. In general, air cleaners are installed in ventilating systems to remove the airborne dusts which tend to settle out in the still air of the ventilated space and become a nuisance. Such dust comes under the classification of temporary atmospheric impurities listed in Fig. 1, Chapter 10, and includes most of the pollens, house dust, and similar allergens which motivate attacks upon persons of allergic sensitivity [1].

The air filters classified as viscous impingement types are widely used in general ventilating systems and will usually justify their cost through a reduction in housekeeping costs in the ventilated space.

For industrial applications and in locations where the larger part of the atmospheric impurities are of fine particle size such as smoke and fumes, more effective dry filters and electric precipitators are proving economical. By use of combinations of filters advantage may be taken of specific characteristics of the various types of filters. In at least one industrial application the air is passed through a series of filters, consisting of a bank of viscous impingement filters followed by an electric precipitator, which in turn is followed by a dry type filter using wool felt as a filter medium and, for absorbing certain gases, an activated carbon filter. Installations of this type which have been in operation for several years have proved to be economical on the basis of a reduction in cost of maintenance of the electrical equipment housed in the ventilated space.

There is at the present time no recognized standard test guide or method for measuring the cleaning efficiency of an air filter and expressing the efficiency in terms of the economic value which would result from the use of the filter. Air filters are usually selected on the basis of experience or judgment guided by the results of various test procedures.

A description of various types of air cleaners available commercially will be found under air filters in the catalog section of THE GUIDE.

DUST AND LINT

Airborne solid matter from the viewpoint of air cleaning is considered as lint and dust. Some lint originates outdoors, as animal hair, vegetable fibers, etc., but much is generated within buildings by the wear and brushing of fabrics in the form of clothes, draperies, carpets, etc. Lint is comparatively easy to capture in an air filter because of its comparatively great length. So far as air filter performance and testing are concerned, lint is chiefly important because of its tendency to impede or stop the flow of air through the filter. In general, lint, if not captured, will accumulate in corners and under furniture in a building in areas of slight air motion

and in some cases may seriously obstruct heating and cooling coils. Dust settles, or is precipitated by heat or air motion, upon furniture, fixtures and walls and the only satisfactory treatment is washing or re-painting. Dust is more difficult to capture than lint, and, obviously, small particles are more difficult to capture than large ones. The air cleaning problem is complicated by the vast difference in size of dust particles, the range of which is shown in Fig. 1, Chapter 10.

Even if the discussion is limited to the range from 0.1 micron to 50 microns, that is, between the smallest particle observable in the microscope and the smallest particle distinguishable to the naked eye, this range is so far outside the usual experience that it is difficult to visualize. If particles could be examined through a super microscope having a magnification of 250,000 diameters, a tobacco smoke particle of 0.1 micron would appear to be 1 in. in diameter, or approximately the size of a golf ball; a soft coal smoke particle 0.3 micron in diameter would appear like a baseball; a ragweed pollen grain 20 microns in diameter would appear 16.5 ft in diameter, while the 50 micron particle, just visible to the naked eye and able to pass through a 270 mesh screen, would appear to be 50 ft in diameter. Picturing this range in particle size from a golf ball to a sphere 50 ft in diameter will emphasize the difficulty of cleaning air or of devising any single test to adequately measure the performance of air cleaning devices under all conditions of service.

As a general rule, the removal of the coarser dust particles and lint from the ventilating air produces tangible results in so far as cleanliness in a house or building is concerned, because much of the finer dust remains suspended in the air and is removed from the building by the circulating air. However, since some of the fine dusts are undoubtedly deposited by means other than settling, such as electrical or thermal precipitation [2,3] and by contact, the ability to remove small particles is desirable in an air cleaner if it can be obtained at not too great a cost.

CLASSIFICATION OF AIR CLEANING MEDIA

Considering the wide diversification of materials and particle sizes to be removed and the varying requirements which have to be met in the field, it is obvious that many kinds of air cleaning devices used cannot be shown satisfactorily in a simple outline. Classifications on three different bases are enumerated as follows:

(A) Principle of air cleaning; 1. Viscous-impingement filters, 2. Dry filters, 3. Washers, 4. Centrifugal devices, 5. Electrical precipitators, (B) Methods of servicing; 1. Automatic, 2. Non-automatic, (a) Throw-away (replaceable elements). (b) Manually cleaned in place (including one type of electrostatic). (c) Removable for cleaning. (C) Classification according to applications; 1. General air conditioning—(a) Central cleaning system, (b) Unit ventilator, (c) Window installation, (d) Warm air furnace, 2. Removal of smoke and fumes from stack gases, 3. Collection of dusts from exhaust systems.

VISCOUS IMPINGEMENT TYPE CLEANERS

The medium in a viscous impingement type filter is usually a fiber pack for non-automatic types or a series of metal plates for automatic self-cleaning types. In either case, the medium is treated with a viscous substance, often an oil or grease, called the *adhesive* or the *saturant*, intended to retain dust particles which come in contact with it. Also, in

either case, the arrangement is such that the air stream is broken up into many small air streams and these are caused to change direction abruptly a number of times in order to throw the dust particles, by momentum, against the adhesive. Several desirable characteristics of an adhesive for air cleaners of this type are: (1) Its surface tension should be such as to produce a homogeneous film or coating on the filter medium, (2) The viscosity should vary only slightly with normal changes of temperature, (3) It should prevent the development of mold spores and bacteria on the filter medium, (4) The liquid should have high capillarity, or ability to wet and retain the dust at all operating temperatures, (5) Evaporation should be slight, (6) It should be fire resistant, (7) It should be odorless.

Various fibrous materials have been used as filtering media in unit filters of the viscous impingement type. These include glass fiber, steel wool, similar *wool* of non-ferrous metals, wire screen, animal hair, hemp fibers, and other materials. In such filters, the medium is often packed more densely on the discharge than on the approach-side in order to increase the dust holding capacity. This results in a selective arrestance of dust with the larger particles nearer the approach face. The arrangement also permits some penetration of lint into (but not through) the filter, so that the amount of lint which can be tolerated on the filter is also increased. Due to plane surface area the viscous impingement type filter, however, may be inferior to some dry types if the air carries a high percentage of lint.

The resistance of air filters obviously increases with the air flow through them. Face velocities of about 300 fpm and resistances in the range from 0.1 to 0.2 in. water, when the device is new and clean, are usual for ventilation system filters. Special filters with low resistances are available for use with gravity warm air furnaces and for other applications where only low pressure is available.

The resistance of these filters increases with dust or lint loading and it is the resistance due to this cause which ordinarily necessitates servicing. The rate of loading obviously depends upon the amount as well as the kind of dust in the air and for this reason periods between servicing cannot be predicted. Manometers are often installed to indicate the pressure drop across filter banks and they serve to indicate when the filter requires cleaning. The pressure drop tolerated differs between operators and system designs. The resistance of a filter bank can be kept desirably low by periodically servicing some but not all of the units in the bank at one time, providing the difference in resistance between the clean and dirty filters is small.

The method of cleaning viscous impingement unit filters differs for different types of filters and kinds of dust. Much dry dust or lint can often be removed by rapping the filter.

Throw-away filters are constructed of inexpensive materials and are designed to be discarded after one use. The frame is frequently a combination of cardboard and wire.

Cleanable types usually have metal frames. Various cleaning methods have been recommended including: air jet, water jet, steam jet, washing in kerosene, and dipping in an oil. The latter may serve both to clean the filter and add the necessary adhesive.

Automatic Viscous Filters

In an automatic air filter, means are provided to remove the dust from the medium mechanically. Automatic filters with moving cloth media

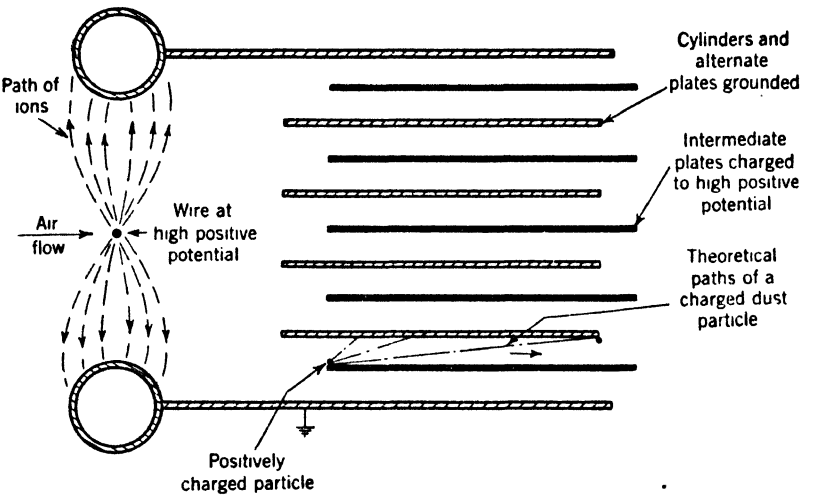

FIG. 1. DIAGRAMMATIC CROSS-SECTION OF ELECTROSTATIC PRECIPITATOR

have been constructed. The media are supported on rollers and move slowly and continuously across the air stream and then through some cleaning mechanism, such as a beater, a vacuum cleaner, or a brushing arrangement. Such filters, however, are not now in wide use, possibly because of mechanical difficulties and the rapid and sometimes permanent increase of resistance caused by oily matter present in the air.

The medium in a typical automatic filter at present consists of a series of specially formed metal plates mounted on a pair of chains. The chains are mounted on sprockets located at the top and bottom of the filter housing, so that the filter medium can be moved as a continuous curtain up one side and down the other side of the sprockets. The arrangement is such that, at the bottom, the medium passes through a bath of special oil which both serves to remove the dirt from the plates and acts as an adhesive when the cleaned plates next pass through the air stream. The plates forming the filtering medium or curtain usually overlap each other and due to their special shape many small air passages are formed between them. These air passages turn abruptly one or more times in order to give the impingement effect.

An electrically driven rotating device is usually supplied with an automatic filter. The device may be set to move the curtain periodically, or a special switch, actuated by pressure drop, may be used to govern its motion. Such a switch will cause the gear to move the curtain when the resistance of the filter to air flow becomes excessive and will stop it when the resistance becomes sufficiently low.

In operation, the resistance of an automatic filter will remain approximately constant as long as proper operation is obtained. A resistance of $\frac{3}{8}$ in. water at a face velocity of 500 fpm is typical of this class.

DRY AIR FILTERS

As the name implies, adhesives are not used on dry air filters. The media in such filters are usually fabrics or fabric-like materials. Media of wool felt, cotton batting (both glazed and unglazed), cellulose fiber and other materials have been used commercially. The medium in a filter of

this class is usually supported by a wire frame in the form of pockets or V-shaped pleats in order to increase the area exposed to the passage of air. A 2 ft square unit may contain from 15 to 30 sq ft of medium.

Dry air filters are likely to have a comparatively high lint-holding capacity on account of the large area of medium used. Wool felt media are troublesome to clean when impregnated with greasy dust and they are too expensive to discard frequently. Both vacuum cleaning and dry cleaning have been used for reconditioning wool felt filters.

ELECTRIC PRECIPITATORS

The fact that a particle exposed to an electric field will assume a charge and migrate toward one of the electrodes has been utilized for some years in boiler plants as a means of smoke abatement. The same principle has been used in equipment developed for air cleaning in air conditioning without generating ozone in intolerable quantities. The air stream in a precipitator passes first through a relatively high-tension electric field, known as the ionizing field, and then through a secondary field where the precipitation of the dust occurs. The arrangement is as shown in Fig. 1.

In a typical case, a potential of 12,000 volts may be used to create the ionizing field, and some 5000 volts between the plates upon which the precipitation of dust occurs. These voltages, which are capable of shock to personnel similar to that of a spark plug, necessitate some safety measures. A typical arrangement provides means for automatically making the unit inoperative when a door to the precipitator is opened. To resume operation the procedure necessitates closing the door and turning an electric switch, the latter of which should be located at a reasonable distance from the equipment. The voltages necessary for the operation of the precipitator are usually obtained from an alternating current building service line by means of a step-up transformer. Precipitation with alternating current is possible but is not nearly so effective; so the current is usually rectified by means of vacuum tubes. The transformer and tubes are collectively termed the power pack.

Only a very small amount of electric energy is necessary to operate an electric precipitator and the resistance to air flow through the device is practically negligible. Some care is necessary in arranging the duct approaches on the entering and leaving sides of precipitators to assure that the air flow is distributed uniformly over the cross-sectional area. The efficiency of the precipitator is sensitive to air velocity and the device itself has much less tendency to rectify the air stream than filters, which have much higher resistances.

Electric precipitators are available in both automatic and non-automatic types. The plates of non-automatic precipitators are commonly coated with a light oil as an adhesive. Cleaning is accomplished with a water hose and, for this reason, the bottom of the equipment is made water tight and provided with a drain. In one automatic type, precipitation units are mounted on chains and are alternately dipped in oil and exposed to the air stream with an action similar to that of an automatic impingement filter. An arrangement of sliding contacts maintains the necessary electric circuits.

PERFORMANCE AND TESTING

The rating of an air cleaner is the air flow for which it is designed expressed in cubic feet per minute. Face velocity is defined as the average

velocity of the air entering the cleaner, and it is determined by taking the air flow and dividing it by the area of the duct connection to the cleaner in square feet. Cleaners are often rated at a face velocity in the range of 250 to 500 fpm. The resistance of an air cleaner to air flow is usually measured in inches water. The resistances of filters when new and clean and when operated at rated capacity are generally available from the manufacturer (see *Catalog Data Section*).

The ability of air cleaners to clean air is called the efficiency or the arrestance, and may be denoted by the symbol E. The efficiency of an air cleaner differs with the size and nature of the dust on which the cleaner operates. Obviously, large particles and lint are more easily captured than minute particles which are small in all dimensions. The efficiency of an air cleaner, algebraically expressed, is:

$$E = \frac{D_1 - D_2}{D_1} \tag{1}$$

where

D_1 = amount of dust per unit volume in uncleaned air.

D_2 = amount of dust per unit volume in cleaned air.

Several methods have been investigated for evaluating D_1 and D_2. The particle count method is not used for efficiency evaluation except in investigation of filter performance on specific particles such as pollen or on certain industrial dusts harmful to health. Dust particles can be captured on microscope slides by means of one of the various kinds of impingement devices. The process is useful if an inspection and analysis of dust is desired, but particle counting is not sufficiently precise for evaluating the efficiency of a cleaner operating on a heterogeneous dust.

The weight method of evaluating efficiency has found wide utility and was recognized by the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS and incorporated in a code [4]. For this test, a known weight of a prepared dust is injected into air supplied to the filter and the quantity of dust in the cleaned air is determined by extracting and weighing the dust from a known volume of the cleaned air. Dust extraction from the air is accomplished by drawing the air through a porous crucible or thimble by means of a high vacuum.

The *dust-spot* or *blackness* test for cleaner efficiency was developed at the *National Bureau of Standards* [5]. The test consists of drawing samples of cleaned air and of uncleaned air through filter papers simultaneously. The ratio of the areas of paper through which the air samples are drawn and the ratio of the amount of air drawn through the papers are adjusted during successive trials to yield spots of approximately equal blackness on the papers. The ratios of the areas and of the volumes of the air samples are then indicators of the filter effectiveness. A special photometer is provided for comparing the blackness or opacity of the papers by transmitted light. For tests of ordinary air filters by this method, a dust is injected into the air stream. The dust consists of precipitated smoke particles from a Cottrell precipitator used in a local power plant for smoke abatement. For tests of electrostatic air cleaners, no dust is added to the air. Tests are commonly made with the dust existing in the air at the location of the installation on a clear day. Some specifications for this type cleaner have required that in dust spots of equal area the downstream spot shall not be any dirtier than the upstream spot when 10 times as much air is drawn through it as is drawn through the upstream

spot. When this condition is met the cleaner is said to have an efficiency or arrestance of 90 per cent or better on atmospheric air.

Dust-holding capacity is defined as the amount of dust which a filter can retain and have a resistance less than some arbitrary value. The term applies only to non-automatic air cleaners. Determination of dust-holding capacity is an objective of each test under the A.S.H.V.E. Standard Code [4]. Curves are obtained during such tests to show the relation between dust load and resistance. Typical curves are shown in Fig. 2. Type A is a dense pack used in bacterium control; Type B is a medium pack used for general ventilation work; and Type C is a low resistance unit, for use where low resistance is the important factor and maximum cleaning efficiencies are not essential.

At the *National Bureau of Standards* two injectors are provided on the air cleaner testing apparatus. One injector is used to contaminate the air stream with Cottrell precipitate, previously described. This dust is used to make both efficiency determination and dust-holding capacity tests. The other injector contaminates the air stream with cotton linters with which lint-holding capacity tests are made. The curves in Fig. 3

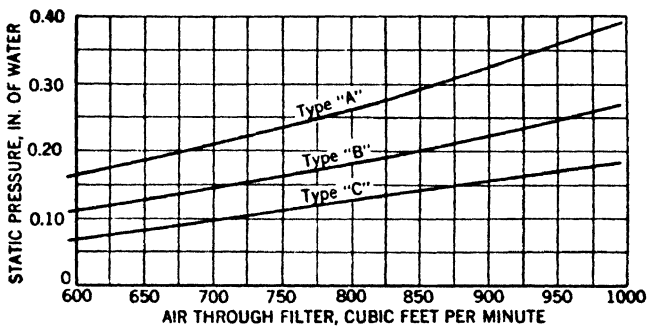

FIG. 2. RESISTANCE TO AIR FLOW OF TYPICAL UNIT AIR FILTERS

illustrate the difference in the characteristics of two filters, one a viscous-impingement type and the other a dry filter with a cellulose fiber medium. The two injectors can be operated either separately or simultaneously. A total dust deposit of 4 per cent cotton linters and 96 per cent Cottrell precipitate gives a deposit on a filter closely resembling those that occur in Washington, D. C.

SELECTION AND MAINTENANCE

For removing fine dust or liquid particles which show no gravitational settling tendency electrical precipitators are highly effective in air cleaning applications. The electrostatic equipment is comparatively expensive to install and maintain. However, in many applications where the cleanest air possible is needed, this expense is justified by the results obtained with properly installed and operated electrostatic air filters.

The advantage of the automatic impingement type filter consists in the small amount of attention which it requires. Such devices are therefore to be recommended where labor is scarce or where reliable and frequent attention to filters cannot be assumed. This type of equipment is not any better in dust arrestance than some unit filters, and it ranks next to precipitators in first cost.

Unit filters constitute the majority of air cleaners now in use, and some choice is possible between the types available. Where lint in an eminently dry state predominates, a dry filter obviously may be preferable to other types on account of its lint-holding capacity. If the lint is greasy or if oil vapor exists in the air, the dry filter, if it is of the cleanable type, may be troublesome, since grease tends to make it difficult to clean. The cleaning difficulty is avoided if a throw-away type of medium is used. Some dry filters are capable of high efficiencies, compared to other unit filters on fine particles, but their dust-holding capacity for such dust may be inferior to that of the viscous impingement type.

Viscous impingement unit filters represent the general type of air cleaner now in use. They have approached standards in size and their over-all dimensions are small when compared with their ratings.

Throw-away units are often installed in series so that the one in front, which usually becomes plugged with lint, can be discarded after which the downstream unit is moved to the front and replaced by a new unit.

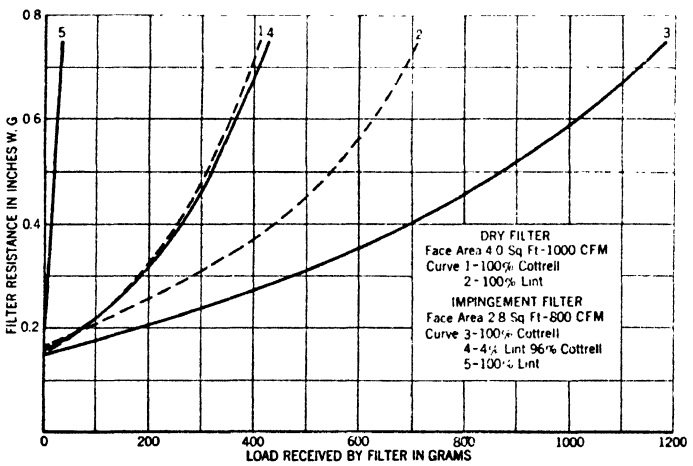

FIG. 3. DUST AND LINT HOLDING CAPACITY OF TWO FILTERS

Viscous impingement unit filters do not have efficiencies as high as can be expected with some other types of unit filters, but their first cost and upkeep are generally lower, whether of the cleanable or the throw-away type. They require more careful attention than the automatic oil type if the resistance is to be maintained within reasonable limits.

METHODS OF INSTALLATION

Many air cleaners are available in units of convenient size for handling when installing, cleaning or replacing. Such units are usually designated as filters or unit filters. A typical unit filter may be 20 in. square and from one to several inches thick, depending on the manufacture and proposed use. In large systems, a number of such units are installed adjacent to each other and collectively called a bank of filters.

Air cleaners are commonly installed in the outdoor air intake ducts of buildings and, often, in the recirculating air ducts as well. Cleaners are logically placed ahead of heating or cooling coils and other air conditioning equipment in the system to protect them from dust. The character of the

dust arrested by the filters in an air intake duct is likely to be mostly particulate matter of a greasy nature, while lint may predominate in dust from within the building.

The published performance data for all air filters are based on *straight through* unrestricted air flow. Filters should be installed so that the face area is at right angles to the air flow whenever possible. Eddy currents and dead air spaces should be avoided and air should be distributed uniformly over the entire filter surface, using baffles or diffusers if necessary.

Failure of air filter installations to give satisfactory results can in most cases be traced to faulty installation or improper maintenance or both.

The most important requirements of a satisfactory and efficiently operating air filter installation are:

1. The filter must be of ample size for the amount of air it is expected to handle. An overload of 10 to 15 per cent is regarded as the maximum allowable. When air volume is subject to increase, a larger filter should be installed.

2. The filter must be suited to the operating conditions, such as degree of air cleanliness required, amount of dust in the entering air, type of duty, allowable pressure drop, operating temperatures, and maintenance facilities.

3. The filter type should be the most economical for the specific application. The first cost of the installation should be balanced against depreciation as well as expense and convenience of maintenance.

The following recommendations apply to filters and washers installed with central fan systems:

1. Duct connections to and from the filter should change size or shape gradually to insure even air distribution over the entire filter area.

2. Sufficient space should be provided in front as well as behind the filter to make it accessible for inspection and service. A distance of two feet may be regarded as the minimum.

3. Access doors of convenient size should be provided in the sheet metal connections leading to and from the filters.

4. All doors on the clean air side should be lined with felt to prevent infiltration of unclean air. All connections and seams of the sheet metal ducts on the clean air side should be as air-tight as possible.

5. Electric lights should be installed in the chamber in front of and behind the air filter.

6. Air washers should, whenever possible, be installed between the tempering and heating coils to protect them from extreme cold in winter time.

7. Filters installed close to air inlet should be protected from the weather by suitable louvers, in front of which a large mesh wire screen should be provided.

8. Filters should have permanent indicators to give a warning when the filter resistance reaches too high a value.

Safety Requirements

An investigation of safety ordinances should be made by the engineer when the installation of an air cleaner of any considerable size is contemplated. It is possible that a combustible filtering media may not be permitted in accordance with some existing local regulations. Combustion of dust and lint on a filtering medium is possible, though the medium itself may not burn.

ADSORPTION OF VAPORS OTHER THAN WATER

Many of the foreign gases in the atmosphere are selectively adsorbed by charcoal. Included are many of the organic gases, such as those

emanating from animals and people, some of the gaseous constituents of combustion; alcohols, ketones, esters, and gaseous products of putrefaction. The selective action of charcoal with a mixture of water vapor and organic gases is shown in Fig. 4.

Charcoals differ widely in their adsorptive capacity. Those which have marked adsorption characteristics, such as properly prepared coconut shell charcoals, are sometimes called *activated charcoals* or *activated carbon.* These materials can adsorb approximately 50 per cent of their own weight of many organic gases at 70 F. The charcoal may be used for a long time by reactivation at high temperatures, under which condition it gives up the adsorbed gases. Temperatures of approximately 1000 F are desirable for reactivation. Charcoals for use in air handling systems should be able to stand physical handling, including reactivation, without excessive loss by breakage or dusting.

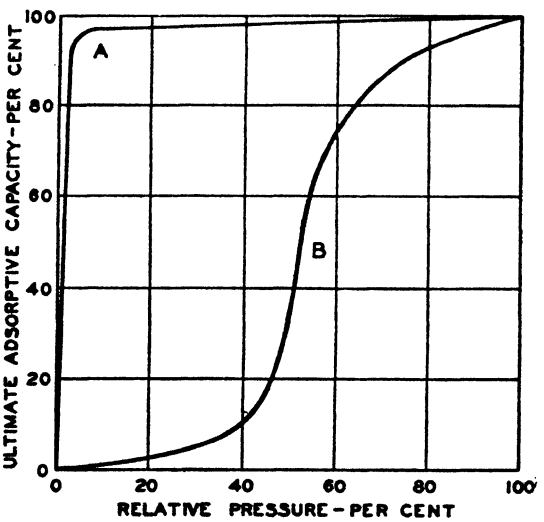

FIG. 4. ADSORPTION AT RELATIVE PRESSURES BY CHARCOAL OF A TYPICAL ORGANIC GAS (A) AND WATER VAPOR (B)

As applied in air handling systems, the charcoal is placed in perforated metal containers which are grouped in frames and set in the air stream. The percentage removal of an organic gas, such as carbon tetrachloride, is 95 per cent or above when placed in intimate contact with the carbon at 70 F. In commercial apparatus there may be a by-pass effect which depends on the physical arrangement of the charcoal containers. This by-passing reduces the percentage removed in the total gas passing through the adsorber. Resistance to air flow is usually selected within the general range of resistance of impingement filters.

The required quantity of recirculated air to be treated is determined by the requirements for contaminant-free air, minus the outdoor air, divided by the fraction denoting the percentage removal of the gas in question in the adsorber bank which is to be used.

Adsorbers may be applied to reduce objectionable gases entering through the outdoor air inlet. They may also be used to reduce the odors caused by exhausts from processing. Adsorber beds, in all cases, should be protected from dust, free oil and grease.

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Chapter 34

AUTOMATIC CONTROL

Basic Types of Control, Types of Controllers, Actuating Devices, Actuated Controls, Residential Control Systems, Zone Control, Automatic Control Application, Control for Central Fan Systems, Terminology of Control Operation, Automatic Control for Year-Round Air Conditioning, Panel Heating Control, Indicating and Recording Equipment

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THE function of *automatic control*, as applied to the heating, ventilating and air conditioning industry, may be broadly subdivided into the maintenance of *temperature*, *humidity*, and *pressure*, within predetermined ranges. It automatically coordinates the operation of the various controlled devices in proper sequence to produce the desired result.

BASIC TYPES OF CONTROL

Available automatic control equipment may be divided into four main groups depending on the primary source of power and can be classed as:

1. *A self-actuated regulator* is one in which all the energy necessary to operate a valve or damper motor is supplied by the responsive element or bulb. Temperature changes at the bulb result in pressure changes of an enclosed fluid which are transmitted directly to the valve or damper motor. Instruments of this type are available either with a rigid bulb or with flexible tubing from the bulb to the operating motor. The flexible tubing may be furnished in varying lengths and is generally protected by a flexible metal armor.

2. *Electrically operated* equipment utilizes electric current as a primary source of energy, its flow being regulated as required to operate motors, relays, or other controlled items.

3. In *pneumatically operated* equipment the primary source of energy is compressed air usually at a pressure of 15 to 25 psig. The flow of this air is proportioned as required to operate valves, dampers, relays, or other controlled devices.

4. In *hydraulically operated* equipment the primary source of power is a suitable liquid at a pressure of 15 to 25 psig or higher which is handled in the same manner as compressed air.

TYPES OF CONTROLLERS

The basic types of controllers which are available may be classed as:

1. *Two position* or *on-off controllers* are the simplest type and are clearly described by the name. With controllers of this type the valve or damper motor can assume only two positions, either open or shut.

2. *Proportional* or *gradual acting controllers* function to re-position the controlled device by small increments of travel to regulate the flow as the controller senses a slight change in the controller condition.

3. *Floating controllers* act to produce valve or damper movement whenever there is a deviation from the control point. Whenever the condition to be controlled is above the control point, the valve closes at a constant rate, and continues to close until the temperature returns to the control point. Below the control point the valve reverses its action and moves in the other direction until the control point is again reached.

4. *Automatic reset (or proportional plus reset) controllers* function to reposition a valve or damper by small increments of travel as in a proportioning controller. In addition, a mechanical device in the controller automatically and constantly resets the instrument to offset the normal drift (inherent in a proportional controller) between maximum and minimum load. The rate of reset is manually adjustable and must be set to meet the load requirements of the individual system. This type of controller provides the accuracy of high sensitivity adjustment with a minimum of hunting.

Controllers may also be designated by types as: (1) a ***non-indicating controller***, when it does not indicate the controlled condition and performs

the control function only; an *indicating controller*, when fitted with a pointer, thermometer, or gauge which indicates the controlled condition; a *recording controller*, when it is combined with a clock mechanism and chart which records the controlled condition.

ACTUATING DEVICES

The starting point of any control system is the thermostat, hygrostat, pressure regulator, or other mechanism which is sensitive to a change and responds in the desired manner.

Thermostats are usually of the room, duct or immersion types. Various types of thermostats found in common use are defined in the following paragraphs.

1. A *thermostat* is an instrument which is responsive to changes in temperature and initiates a force that respositions valves, dampers, etc. to maintain selected temperatures.

2. A *room thermostat* is usually mounted on the wall of the space to be controlled, with the measuring element arranged so that it is affected by the room temperature.

3. A *duct thermostat* is provided with fittings suitable for installation in duct work. The *insertion* type is equipped with a rigid bulb and is arranged so that the temperature responsive element or bulb extends through the wall of the duct. The *remote bulb* type is arranged so that the bulb and instrument head are connected by means of a flexible tube of the desired length. The bulb is inserted in the duct, and the head is located where it is accessible for adjustment and inspection.

4. An *immersion thermostat* is provided with fittings suitable for installation in a pipe line or tank where a fluid tight connection is required. Both insertion and remote bulb types are available. A union connection and separable socket when used permit removal of the bulb without draining the line or tank. The sockets may be of copper, stainless steel or other materials.

5. A *day-night* or *two-temperature thermostat* controls a heating or cooling source to maintain either of two selected temperatures. They may be indexed (set at desired control temperature) individually or in groups from a remote point by means of a manual or time switch.

6. A *summer-winter* or *heating-cooling thermostat* is similar to the Day-Night type except that both the temperature setting and action are changed by the indexing means. Such a thermostat could open a volume damper on a rise in temperature in summer and close the same damper on a rise in temperature in winter.

7. A *submaster thermostat* has its temperature setting raised or lowered a pre-determined amount for a given change in some other variable. For example, the water temperature on a heating system may be raised as the outdoor temperature drops. A *master instrument* is used to reset a submaster thermostat and may be a switch, pressure controller, thermostat, or similar device. In the foregoing example the master thermostat would be located where it would respond to outdoor temperature and the submaster thermostat would be located in the pipe line of the heating system.

A *hygrostat* is a controller which is sensitive to changes in relative humidity, and is available in room and duct types. Where the controlled condition is below 20 per cent or above 80 per cent, or the temperature is above 100 F, selection of a suitable type and kind of hygroscopic element is essential.

A *pressure regulator* is a device which is sensitive to changes in pressure. It is available in types which control a *single* pressure or the *differential* type which maintains a pre-determined difference between two pressures. For pressures in duct work, *static pressure regulators* are available in the *differential* type. They are sensitive to changes of 1/100 in. of water.

ACTUATED CONTROLS

Thermostats, hygrostats, pressure regulators and other actuating devices obtain control of heating and cooling mediums, fuels, liquids,

etc., by actuating various control devices such as control valves, dampers, damper motors, relays, controllers defined in the following paragraphs.

A *control valve* is designed to control the flow of fluids, and may be considered as a variable orifice which is repositioned by a motor operator as directed by a thermostat, or other controlling device.

1. A *normally open* or *direct acting valve* will assume an open position when all operating power is removed.

2. A *normally closed* or *reverse acting valve* will assume a closed position when all operating power is removed.

3. *Single seated valves* are designed for *tight* shut-off using appropriate disc materials for various pressure ranges.

4. *Pilot piston valves* serve a similar function on high pressure installations.

5. *Double seated* or *balanced valves* are designed for applications where tight shut-off is not required. They are not affected by varying inlet pressures or pressure differentials, and thus are widely used where these conditions exist.

6. A *three-way mixing valve* is fitted with a double faced disc, operating between two ports, and functioning to close one port as the other is opened. It is used to mix two fluids as required.

7. A *three-way diverting valve* is fitted with two discs which act to close one outlet port as another outlet port opens, and thus diverts the flow from the inlet port to either of the outlet ports.

Valve discs, poppets, and seats are available in various shapes to meet any desired flow characteristics with various materials as required by service conditions.

A *damper* is designed to control the flow of air or gases and is similar to a valve in this respect. *Single blade dampers* are generally restricted in size because of the difficulty of securing proper operation with high velocity air. *Multi-blade* or *louver dampers* can be furnished so that adjacent blades move in the same direction or in opposite directions. The *opposed blade type* gives better directional and flow characteristics than the parallel blade type.

For long life and trouble free operation, dampers should be constructed with heavy metal frames, blades of iron adequately braced, and ample bearing surfaces of non-corrosive materials. When fairly tight closing is desired felt may be glued and riveted on the edges and ends of the blades. Other materials for blades and frames are also used for special services.

A *damper motor* is repositioned by a controlling instrument, and is connected to the damper blades as required to give the desired movement. It can be mounted on the damper frames or mounted outside the duct and connected to an extended shaft on one or more damper blades. Suitable brackets are available for floor, wall, or duct mounting of the motor.

A *relay* is a device which uses an auxiliary source of energy to amplify or convert the force of a controller into available energy at a valve or damper motor. Various types of relays are designated as follows:

1. An *electro-pneumatic relay* when electrically energized starts or stops the flow of air as required.

2. A *pneumatic-electric relay* when affected by different air pressures starts or stops the flow of electrical energy as required.

3. A *switching relay* or *pilot valve* may be used to switch the operation of a controlled device from one controller to another; or to reverse the action of a controlled device in response to an impulse from a controller.

4. An *averaging relay* is affected by the forces from two or more controllers, and the resulting flow of energy is in accordance with the average of these forces.

5. A *positioning relay* has a direct connection to a valve or damper motor lever, and is affected by both valve or damper position and controller demand. It is repositioned

by a thermostat or other controlling device, and is arranged to give a definite motor position for a given force from the thermostat without regard for motor hysteresis, friction, or pressure variations of the controlled fluid.

A *sequence controller* is used to operate two or more devices in a prearranged sequence. It is generally used in connection with refrigeration compressors, and may be arranged to prevent simultaneous starting in the event of temporary electrical shutdown or control medium failure.

Manual switches are available in the two-position or proportional types. *Two-position switches* change the flow of energy from one line to one or more other lines; or from one pair of lines to another pair of lines. *Proportioning switches* vary the flow of energy as determined by the manual setting of the switch.

RESIDENTIAL CONTROL SYSTEMS

The control equipment function in a residence may vary from the regulation of a coal-fired heating plant to the completely automatic control of an all year air conditioning system. Regardless of the type of heating or air conditioning system used, the control system should be selected to insure safety and comfort of the occupants as well as economy of operation.

Appliance Controls

Typical controls for the appliances used to supply heat in residences are as follows:

1. *Hand Fired Coal Burners.* The control of a hand fired coal burner for a boiler or furnace normally consists of a room thermostat operating a two position electric control motor which in turn opens the draft damper and closes the check damper on a demand for heat. The motor then closes the draft damper and opens the check damper when the thermostat is satisfied. A limit control on the boiler or furnace should be connected to the motor so that it may check the fire whenever a predetermined temperature or pressure has been exceeded. A manually operated basement switch is usually included on the motor so that the draft may be opened and the check closed when the boiler or furnace is being filled with coal.

2. *Coal Fired Stokers.* Domestic stokers are usually controlled by a room thermostat, a limit control, and a stoker relay. When the thermostat calls for heat, the relay causes the stoker motor to increase the flow of fuel and air to the burner to its maximum rate. When the thermostat is satisfied, the relay provides for a minimum flow of fuel and air to the burner to maintain the fire at its minimum rate. The limit control prevents the continuance of the maximum fuel rate if the temperature or pressure in the boiler or furnace exceeds a predetermined point and also stops all fuel feed if the fire goes out. Automatic ignition usually is not available and the firing of a stoker is normally on or off.

3. *Automatic Oil Burners.* Automatic oil burner controls normally consist of a room thermostat, a limit control, a combustion safety control, and a control relay. On a call for heat by the thermostat, the relay starts the oil burner motor which supplies oil and air to the burner. An ignition device consisting of an electric spark or a gas flame ignites the oil automatically. If for any reason the oil and gas mixture does not ignite, a time delay mechanism in the relay is operated by the combustion safety control after a predetermined length of time to cause the oil and air supply to be shut off. If the oil and air mixture ignites properly the burner continues to run until the thermostat is satisfied or until the limit control affected by the temperature or pressure in the boiler or furnace, stops the burner.

4. *Automatic Gas Burners.* The controls for an automatic gas burner usually include a room thermostat, a limit control, a safety pilot, gas pressure regulator and a gas valve (solenoid, motorized or diaphragm type). Upon a demand for heat at the thermostat, the gas valve is opened, admitting gas to the burner. The safety pilot ignites the gas which continues to burn until the thermostat is satisfied or until the limit control shuts off the gas valve. The limit control may also reduce (throttle) the gas flame as required to maintain a desired temperature or pressure of the heating medium. If the pilot flame is extinguished for any reason either before or after the main gas valve is turned on, the

safety pilot closes the gas valve, thus eliminating the danger of delivering gas to the burner without ignition.

5. *Electric Heating.* Electric heating has become popular in those areas where electric power is plentiful and inexpensive. The electric heating elements may be located in each individual room and turned on and off by thermostats in each room or the heat may be supplied by a central heating system. In the case of a central heating system the control is usually of the proportioning type which energizes from five to ten heating elements in sequence according to the demand for heat by means of a sequence controller consisting of a series of switches operated by a proportioning motor. A limit switch recycles the sequence controller if the furnace or boiler exceeds a predetermined temperature.

Limit Controls

A *high limit* control for steam consists of a pressure control having bellows, responsive to the boiler pressure, which breaks an electric contact when the steam pressure exceeds a predetermined point, thereby preventing the burner from delivering additional heat to the boiler. A low water cut-off should also be used to stop the burner if the water in the boiler drops to a dangerous level.

A high limit control for a hot water boiler consists of an immersion thermostat (usually equipped with a bi-metal helix) inserted in a well in the boiler. This control stops the burner when a predetermined water temperature has been reached in the boiler.

In a warm air system the high limit control is a thermostat including a bi-metal helix inserted in the bonnet of the furnace. It will shut off the source of heat when a predetermined furnace temperature is exceeded.

System Control

There are several types of system control in common use for residential applications. They are usually of the two position (on-off) type or of the proportioning type.

1. *Two Position (On-Off) Control.* The most simple type of domestic control is the type in which the room thermostat starts the burner or other source of heat when the temperature of the air at the thermostat falls below the thermostat setting and stops the source of heat when the air temperature rises above the setting. If forced warm air or forced hot water is used, the fan or circulator may be turned on and off at approximately the same time as the source of heat.

2. *Proportioning Control.* When a proportioning type of control is used, the flame of the burner may be varied or the burner may be cycled (started and stopped) frequently to provide for time modulation so that the heat input to the home is proportioned continuously to the heat loss from the home. The fan of a forced warm air system or the circulator of a forced hot water system may be run almost continuously, thereby providing for the constant flow of heat into the home. Such operation eliminates the cold drafts on the floor as caused by cold air dropping from cool walls and windows during the off period of an on-off system.

Room Thermostats

Room thermostats usually employ a bi-metal element or a vapor filled bellows as the temperature sensitive element. They may be of the plain or single temperature type, or of the day-night type providing for automatic night lowering and morning increase of the control point. The automatic setback type usually includes a clock mechanism which accomplishes this result.

In locating a room thermostat the following rules should be observed:

1. It should always be located towards the center of a relatively open room on the coolest rather than the warmest side of the building.

2. It should never be mounted on an outside wall or other cold surface, or where it is exposed to cold drafts from an outside door.

3. It should never be mounted where it will be affected by heat from a nearby warm surface such as chimneys, pipes or ducts in a wall, radiators; or by direct currents from a warm air register.

4. It should never be located where normal circulation of air is impeded by furniture or an opened door.

5. It should be located where it is safe from mechanical injury.

In a typical home, a satisfactory location for the thermostat can usually be found on an inside wall of the living room or dining room.

Air-Conditioning Systems

Year-round residential air-conditioning systems which provide for heating in winter and cooling in summer should be given the same consideration in selecting the control system as required for commercial air-conditioning systems described later in this chapter since the basic principles are the same and the final results must provide for the comfort of the occupants. Economy in first cost may result in both lack of economical operation and discomfort.

ZONE CONTROL

In residential heating, it is often desirable to divide the house into two or more zones for greater accuracy of control and comfort. Each zone may then be maintained individually at the desired temperature level. The division by zones should be based upon exposure and occupancy and the most common division is usually found to be:

1. Living section (Living room, dining room, den, etc.)
2. Sleeping section
3. Service section (Kitchen, pantry, servant's quarters, etc.)

Zone control for steam and hot water heating systems is employed where it is desired to control the heating effect of a multiplicity of radiators or convectors, located in various heated spaces, through the use of a single regulator. Under certain conditions, particularly in buildings of limited size, it is possible to consider the entire building as a single heating zone. In such cases, the zone regulator, or *master controller*, may operate directly the automatic firing equipment of the boiler or the reducing valve in the street steam main. In large buildings the demands of satisfactory temperature control, however, will make it necessary to sub-divide the heating system into suitable zones.

There are a number of factors to be considered in zoning, in order that heating requirements in a single zone will be approximately consistent throughout its extent.

1. Exposure may be a factor to be considered, with particular reference to prevailing winds, sun effect, and the shelter afforded by surrounding structures and topographical features.

2. Occupancy may be a determining factor, in that the indoor temperature requirements for the activities carried on in various portions of the building may vary and the hours of occupancy likewise may differ.

3. The physical characteristics of the building will enter into the sub-dividing of the heating system into zones by reason of the fact that satisfactory temperature conditions throughout a single zone of given extent may not be enjoyed equally in buildings of dissimilar types of construction. Also, the height of the building and its horizontal extent and form are considerations which must be borne in mind.

4. The cost of the zone control equipment for such additional zones as might seem otherwise desirable often will influence the decision as to the final number of zones to be employed. In buildings of considerable size, accepted practice dictates that there shall be at least one zone for each exposure, although each exposure very possibly should be sub-divided vertically into two or more zones, for the higher structures. Also, the

presence of two or more wings, having the same general exposure, may suggest the desirability of more restrictive zoning. In smaller buildings, and in those of larger extent where cost and other conditions limit the number of zones, a common compromise is to combine the North and West exposures in one zone, and the East and South exposures in a second zone. Frequently, when the street floor level is given over to public spaces or to activities which are markedly different from those carried on in the remainder of the building, it is advisable to provide a separate steam main, with conventional room thermostats in each individual area.

For steam heating systems, the radiator output may be varied proportionately to the changes in outdoor temperature, by any of a number of general methods. Those in most common use are:

1. Turning the steam on and off at appropriate intervals as dictated by temperature or time considerations, proportioned to the need for heating.
2. Varying the pressure of steam in the system in accordance with the demand for heat.
3. Throttling the steam pressure, at the demand of the controller, to allow flow through orifices in proportion to the heating requirements.

In hot water heating, the accepted practices are (1) to vary the temperature of the hot water supplied to the system or, (2) to vary the flow of hot water, both proportionately to the heating requirements.

The regulator for each zone usually is of a type which in some manner responds to the outdoor temperature and effect of sun and wind for the zone. Many of the available zone controllers are arranged in such a way as to be affected also by the temperature of the heating system and the indoor temperature in the zone. Whatever the mechanical features of the regulator, its function is to dictate the flow impulse, or rate of flow, in such a way as to maintain the desired indoor temperature in the zone, regardless of the fluctuations in the outdoor temperature. Provisions also may be made to maintain a predetermined low economy temperature in each zone during periods of non-occupancy; to facilitate quick warming-up following such periods; and to follow those portions of the daily cycle of control with normal heating effect during the occupancy period.

A control panel, at a central location, may be arranged so that manual switches for each zone may raise or lower the operating temperature, and time switches, if desired, may be provided for obtaining, automatically, any day-night or other predetermined control program which the operators of the building may desire. The characteristics of the regulators which are operated by the zone controllers depend upon which of the basic systems of zone control is employed in a given installation. Shut-off, mixing or throttling valves and various forms of devices to reset or pilot the action of reducing valves and to control firing means, are some of the more common regulators which are used to control the flow of steam or hot water, under the command of zone controllers. The characteristics of these regulators usually are determined by the manufacturer of the type of controller which is selected.

AUTOMATIC CONTROL APPLICATION

Some of the considerations affecting the selection of automatic controls for applications are given in the following paragraphs which describe controls and operation for various types of units.

Unit Heater Control

Two-position (on-off) control by means of a room thermostat is the standard method of control for unit heaters. A limit control should be

incorporated to prevent operation of the unit heater fan motor when steam or hot water is not available. The limit control can be a surface thermostat or pressure control. Where there is no possibility of drafts and continuous air circulation is required, the unit heater fan motor may operate continuously. In this case, a room thermostat controls a valve (two-position or proportioning) in the steam or in the hot water supply line.

Unit Ventilator Control

Various makes of unit ventilators are designed for different control cycles. Selection of automatic temperature control for unit ventilators is largely determined by the design of the particular unit. The choice of control cycle may also be determined by local and state ventilating codes, particularly where units are installed in school rooms. It is desirable to coordinate the selection of control cycle with the unit ventilator manufacturer since, in many cases, modifications of the unit are required for the installation of the control equipment; and, in some cases, it is desirable to have the equipment factory-mounted. Two typical control cycles are: (1) *Variable Outdoor Air with Fixed Minimum;* and (2) *Variable Outdoor Air without Fixed Minimum.*

Control Cycle No. 1. In full heating position, the outdoor air damper is closed, the recirculating air damper is open, and the supply valve is open.

In full cooling position the outdoor air damper is open, the recirculating air damper is closed and the supply valve is closed or at a minimum position to maintain a minimum discharge air temperature. The sequence of control operations is: On call for cooling, under control of a room thermostat, outdoor air damper opens to minimum setting. The supply valve then closes gradually, after which the outdoor air damper gradually opens to the maximum position and, simultaneously, the recirculating air damper closes. A low limit thermostat mounted above the coil prevents the discharge temperature from dropping below a predetermined minimum.

Control Cycle No. 2. In full heating position the outdoor air damper is closed, the recirculating air damper is open and the supply valve is open.

In full cooling position the supply valve is closed, the outdoor air damper is open and recirculating air damper is closed or at any position required to maintain a minimum discharge air temperature. The sequence of control operations is: On call for cooling, under control of a room thermostat, the valve gradually closes. As the valve leaves full-open position, control of the recirculated air and outdoor air dampers is transferred to a thermostat installed ahead of the heating coil to maintain a minimum air temperature. On continued call for cooling, the valve gradually closes.

If direct radiation is used, it is desirable that it be controlled in sequence with whatever control cycle is adapted for the unit ventilators.

Unit Coolers

Although most unit coolers can be adapted to any control cycle, continuous fan operation is recommended to avoid stratification and wide fluctuations in space temperature. Should the unit be completely self-contained, control of the direct expansion refrigeration unit may be obtained from the temperature of the recirculated air and from suction pressure. In the case of multiple unit systems supplied with refrigerant or chilled water from a central source, a valve in the supply to each cooling coil may be controlled thermostatically from space temperature.

Refrigeration and Dehumidification Equipment

Typical control equipment and its functions are described in the following paragraphs.

Well Water. Where well water is used directly in air washers or cooling coils, control of temperature or humidity is usually obtained by thermostats or humidistats operating valves (two-position or proportioning). The two-position valve will provide better dehumidification since a lower coil temperature will be maintained but the temperature of the discharge air will fluctuate. With proportioning control, better control of dis-

charge air temperatures will be maintained. In both cases the sensible-latent ratio is basically a matter of coil design rather than automatic control. Proportioning three-way valves may be used as mixing or diverting valves for better pump performance and may also be applied to an air washer used with a recirculating pump to control water temperature rather than volume.

Ice Bunkers. Where water is sprayed over the ice in bunkers and circulated to air washers or cooling coils control is obtained by a thermostat in the water line from the bunker. The thermostat proportions a three-way valve to by-pass enough return water around the ice bunker to maintain a constant discharge temperature.

Compressors. Compressors may supply refrigerant to direct expansion cooling coils in air conditioning units or to direct expansion coils in water-chilling units. In either case, the compressor motor may be started and stopped directly by a room or duct thermostat or a pressure controller may be used to regulate the suction pressure of the compressor. In the latter case, a room or duct thermostat may be used to control a solenoid valve in the refrigerant supply line to the cooling coil. A high and low pressure cut-out is standard safety equipment on most compressor installations. Reduced capacity of the refrigerating unit may be obtained by means of temperature or pressure controlled unloading devices which vary the capacity of the compressor in some proportion to variations of cooling load. Program or step controllers, actuated by temperature or pressure, are commonly used in multiple compressor installations. It is desirable in such installations to return the program or step controller to the *off* position when the system is shut down to prevent the full electrical load of multiple compressors from being thrown across the line at the same time. Thermostatic control of water supply to water-cooled condensers may be achieved by means of self-contained controllers or valve and thermostat application.

Steam Jet. A steam jet refrigeration system is commonly controlled by means of a thermostat in the chilled (secondary) water. The thermostat operates a two-position valve in the steam line to the jet. In the case of multiple jet units, program or step control can be achieved by controlling the jets in sequence. As in the case of direct expansion refrigeration units, a system of control is advisable for the watercooled-condensing unit.

Centrifugal Units. The control of centrifugal refrigeration units or other types of vacuum systems is customarily achieved by means of a thermostat in the chilled water to control the operating cycle of the equipment at full or reduced capacity.

Adsorption Units. Control of adsorption units consists of a damper control which, in response to humidity, controls the air flow through or around the activated bed of adsorption material. Standard controls for cooling are used to reduce the dehumidified air to a desired drybulb.

Absorption Units. Since at constant density, the absorption solution will extract water from the treated air in an amount proportional to the solution temperature, the moisture content of the air leaving an absorption unit is regulated by solution temperature. Solution density is held constant by a combination of float control and steam valve controlling the solution regenerator. Two basic methods of control are standard:

1. Constant solution temperature where the solution temperature is set so that, at the full load for which the unit is designed, the discharge air will have the desired moisture content. Proportioning control of the water and two-position control of the steam is recommended to maintain constant temperature.
2. Control by varying the solution temperature so that the moisture content of the discharge air remains constant regardless of load variation. Basically, this control is similar to the constant solution temperature control with the addition of a hygrostat or wetbulb controller controlling the water valve from space conditions. In order to secure a constant discharge drybulb temperature, a coil is provided with proportioning valve controlled by a proportioning thermostat in the unit discharge.

CONTROL FOR CENTRAL FAN SYSTEMS

Automatic temperature control for central fan heating, cooling, ventilating and air conditioning systems involves the proper application of various types of controlling instruments and associated regulators such as valves, dampers and damper operators, relays and other auxiliary equipment which are described in earlier sections of this chapter. In central fan systems the conditions required dictate the type of built up

control system to be used. Otherwise, some arrangement of available *package* equipment probably would be used. For that reason, it is impossible to state in detail the control apparatus which will be required in even the most representative applications.

In general, in so far as automatic temperature and humidity control equipment is concerned, central fan systems may be divided into certain broad classifications, as follows:

1. Heating
2. Humidifying
3. Ventilating and Atmospheric Cooling
4. Cooling and dehumidifying
5. Control of Zone Temperatures
6. Year-round air conditioning with automatic change-over
7. Constant temperature and humidity

The apparatus which enters into the automatic maintenance of temperatures and humidities for central fan systems which are designed to produce each of the effects listed in items 1 to 7 is indicated in the following paragraphs:

1. In *heating control*, there are three considerations to be borne in mind: (1) to control space temperature, (2) to prevent drafts, (3) to guard against freezing. Usually in central fan systems, suitable thermostats operate valves in the steam or hot water supply to heating coils or face dampers across such coils and bypass dampers around them. If the heating coils are sub-divided into two or more groups, such as preheaters and reheaters, a duct thermostat following the preheaters, and located in the entrance to the chamber between the groups of coils, controls the preheaters, but it is essential that the preheater coils be of the steam distributing type. Similarly, a duct thermostat in the fan discharge, where any effect of stratification has been dissipated, operates the valves and dampers associated with the reheaters. In some cases, where there is more than one bank of preheaters, the practice is to place a freeze protection thermostat in the outdoor air intake to control the valve on the first bank of heaters, which is designed so that the heat-rise through it will not cause overheating. A room thermostat in the heated space may serve as the controlling instrument, with a thermostat in the fan discharge serving to prevent the delivery of air at a temperature which might cause drafts. If desired, similar action may be obtained from a thermostat in the return air connection. When there is only one heating coil, a limit thermostat in the fan discharge accomplishes the control, in conjunction with a thermostat in the heated space or in the return air.

2. *Humidity control* may be obtained by means of a hygrostat, usually located in the conditioned space or in the return air. Such controlling instruments may operate steam supply valves to humidifiers, mixing valves to control the temperature of the water to sprays, or a system of dampers to regulate the quantity of air passed through the humidifying chamber or bypassed around it. The control of humidity according to dew-point temperature is sometimes accomplished by means of a thermostat in the outlet of the humidifying chamber. However, the setting of the dew-point thermostat may have to be changed as the humidity in the conditioned space varies.

3. The *control of ventilating* and *cooling* by the use of outdoor air consists of an arrangement of dampers, usually determining the relative quantities of outdoor air and return air which are to be delivered to the conditioned space. The damper positions are regulated by proper types of thermostats, located in the minimum outdoor air intake, the fan discharge, the conditioned space or the return air. Instruments are available which, with an adequate arrangement of dampers, will cause a maximum quantity of outdoor air to be handled until it becomes more economical to utilize return air.

4. *Cooling and dehumidifying* may be controlled by means of thermostats, and hygrostats or dew-point thermostats, which regulate dampers and mixing valves to maintain air of the proper temperature and humidity in the discharge from the central fan plant. Such controlling instruments normally are located in the fan discharge or in the return air, or both, and they may be associated with thermostats or hygrostats in the conditioned spaces.

5. Where a *separate duct serves each zone* of an area with which a central fan system is associated, a room thermostat in each zone may operate mixing dampers in the inlet to each zone duct, determining the quantity of warm air which is required from that portion of a plenum chamber into which heated air is delivered and the quantity of cool air which

should be taken from the other portion of the double plenum chamber. In many instances, separate zone heating and zone cooling coils are employed, instead of mixing dampers.

6. The control hook-up for a typical *year 'round air conditioning system*, including automatic change-over from heating to cooling, is indicated in Fig. 1 and described as follows:

Whenever the fan is started, solenoid air valve or relay E-1, actuated by the fan motor starter, opens minimum outdoor air damper D-1, places hygrostat H, in service, and allows duct thermostats T-3 and T-4 to control the maximum outdoor air damper D-2 and the return air damper D-3.

When the fans stop, E-1 is de-energized, to close the outdoor air dampers and also to close humidifier valve V-4.

Thermostat T-1 positions steam valve V-3 on the reheater coil, to maintain a constant space temperature. As the space temperature rises, T-1 positions reheater valve V-3 to a closed or to a minimum open position, as determined by low limit discharge thermostat T-5. Duct thermostat T-6, in the preheater discharge, positions preheater coil valve V-1, to maintain a constant preheater discharge temperature.

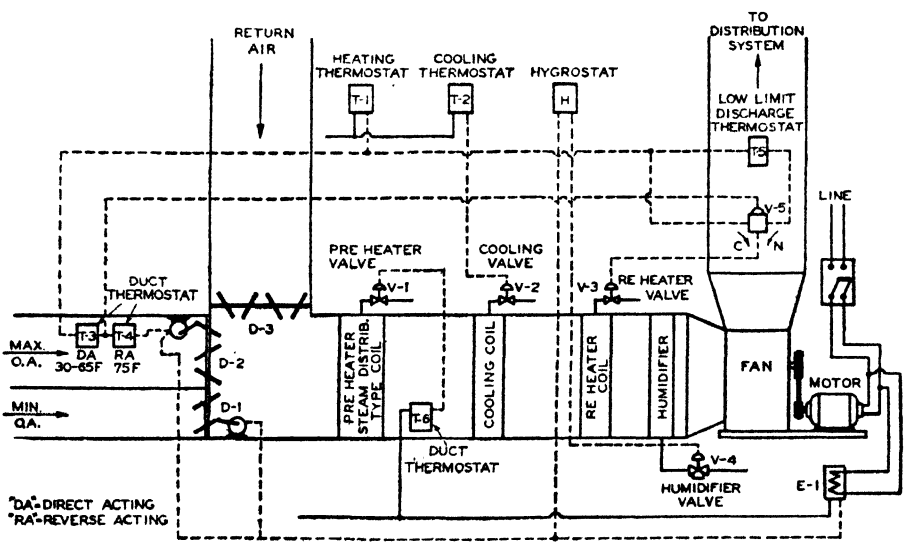

FIG. 1. CONTROL DIAGRAM FOR YEAR 'ROUND AIR CONDITIONING SYSTEM

On rising outdoor temperature, between 30 F and 65 F, duct thermostat T-3, located in the outdoor air intake, moves maximum outdoor air damper D-2 toward the open position. At 65 F, outdoor, D-2 will be fully open and return air damper D-3 will be fully closed.

As the outdoor air temperature rises above 65 F, duct thermostat T-3 positions V-5 in such a way as to by-pass low limit thermostat T-5, so that reheater coil valve V-3 is operated directly from thermostat T-1. As outdoor air temperature rises from 65 F to 75 F, duct thermostat T-4 gradually closes maximum outdoor air damper D-2 and opens return air damper D-3.

Cooling thermostat T-2 positions cooling coil valve V-2, to admit more chilled water, as the space temperature rises.

Hygrostat H positions humidifier valve V-4 to maintain the desired humidity in the conditioned space.

7. The arrangement of automatic control for a *constant temperature and constant humidity air conditioning system*, using 100 per cent outdoor air, is shown in Fig. 2, and the control description follows:

Whenever the fan is running, relay or solenoid air valve E-1, actuated by the fan motor circuit, is energized, opens outdoor air damper D-1, and also permits hygrostat H, in the conditioned space, to control humidifier valve V-2.

When the fan stops, E-1 closes outdoor air damper D-1 and humidifier valve V-2.

Remote bulb thermostat T-2, with bulb located in preheater discharge, operates valve V-3 on the preheater coil, to maintain a constant preheater discharge temperature.

On rising temperature, thermostat T-1, in the conditioned space, closes reheater valve V-1 and, through relay C-1, opens face damper D-2, for cooling. On rising humidity in the conditioned space, hygrostat H closes humidifier valve V-2, and likewise, through C-1 may open face damper D-2 for dehumidification.

For closer control, the face and by-pass dampers should be eliminated and cooling means continuously provided whenever the outdoor dew-point rises above a predetermined maximum. Reheating and humidifying may be required to provide the desired conditions. However, such a system will be less economical in operation.

PANEL HEATING CONTROL

Automatic controls for radiant and convective heating differ somewhat due to the thermal inertia characteristics of the panel heating surface, and the increase in the mean radiant temperature within the space under increasing loads for panel heating.

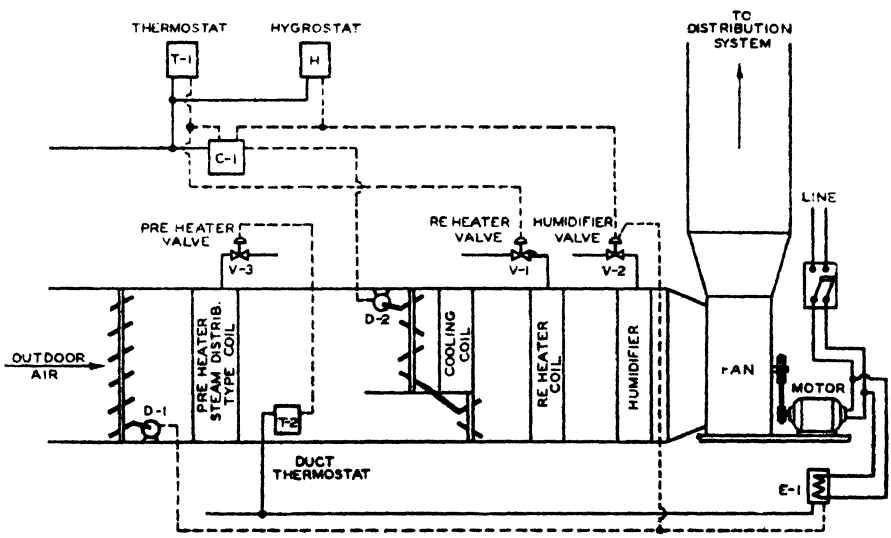

FIG. 2. CONSTANT TEMPERATURE AND HUMIDITY CONTROL FOR YEAR 'ROUND SYSTEM USING 100 PER CENT OUTDOOR AIR

Effect of Inertia of Panel

If a panel has considerable heat storage capacity (as compared with a convector or conventional radiator) it will continue to emit heat for some time after the room thermostat has become satisfied and shut off the supply of heating medium. This will cause uncomfortably warm conditions to exist in a space. Also, there will be a considerable delay between the time the thermostat calls for heat and the time heat is actually delivered to the space (because of the large part of the heat that must first be stored in the thermally "heavy" radiant surface). Whenever inertia exists in the source of heat supply, uncomfortable cycling of space conditions will result unless means of anticipating load changes *before* they occur in the space, or means of setting the basic energy supply rate from load conditions, is provided.

If a thermally heavy radiant surface is used the primary control should be actuated by outdoor temperature (load) to determine the basic temperature of the heating medium supplied to the radiant surface. To

allow for variations in internal load, an inside thermostat should be used as a high limit to reduce further the heat input if necessary. If a thermally *light* radiant surface is used, controls may be applied in the same manner as for typical convection heating.

The terms *thermally heavy* and *thermally light*, referring to capacity for heat storage, are comparative and descriptive rather than exact. For example, a concrete floor panel in a frame structure without insulation would represent a *heavy* panel in a *light* structure. A frame type (metal lath and plaster) panel in a concrete structure would represent a *light* panel in a *heavy* structure. As indicated previously a *heavy* panel in a *heavy* structure provides comfortable conditions if outside controls are used in addition to the inside thermostat. But if a *heavy* panel is used in a *light* structure, rapid changes in outdoor conditions may cause discomfort in spite of outdoor controls, because the structure reacts so much more rapidly than the radiant heating surface.

Compensation for Increase of MRT

In order to maintain comfort, the air temperature in a panel heated space should be lowered as the heating load increases. Usually the required reduction in air temperature is not great and a conventional fixed control point room thermostat may be used unless a rather large infiltration load exists, or if untempered mechanical ventilation is used. Because of the relationships existing between MRT (mean radiant temperature) and air temperature in the space (and the variable MRT from point to point in the space), a conventional type of room thermostat (either fixed or variable control point as previously determined) may provide simple and satisfactory control.

Lowered Night Temperature

In general, lowered night temperature control is not recommended with *heavy* panels though it may be satisfactory with *light* panels. Best practice indicates continuous circulation of the heat in a medium with control provided to vary the temperature of the medium.

INDICATING AND RECORDING EQUIPMENT

In addition to the automatic control of temperature and humidity conditions, visual indication and permanent chart records of the variables involved are desirable. They provide an accurate check on the performance of the system both from the standpoint of conditions maintained and cost of operation. Instruments are available to provide accurate records of these variables, such as pressure, temperature, humidity, flow and CO_2, which go to make up a complete heating or air conditioning system. In some cases the control equipment is provided with indicating or recording mechanisms by means of which the performance of the controls may be observed or recorded and in other cases separate instruments are used for the purpose.

Chapter 35

MOTORS AND MOTOR CONTROLS

Motor Rating; Functions of Motor Control Equipment; Direct Current Motors, Types, Control Equipment and Specifications; Alternating Current Motors, Types, Control Equipment and Specifications; Gear Motors; Glossary of Motor Terms, Enclosures, Speed Classification and Mounting

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THE electric motor, available in many different types suitable for various services, is now the most widely used form of prime mover. The equipment for starting, controlling and protecting these motors varies with the type and with the functions it is desired to attain. Motors are divided into two general classifications, *alternating-current* or *direct-current*, depending on the power source to be used.

In selecting a motor for a particular application consideration must first be given to the type of power supply available. All machinery has certain load characteristics which may vary with speed. Some types may have a constant torque over wide ranges of speed, while others may have changing torques with changing speed. Consideration should be given to selecting the motor and the motor control which best suit the requirements of the drive.

MOTOR RATING

The rating of an electric motor depends upon the total temperature which the motor attains under operating conditions. This total temperature depends on both the ambient temperature and the temperature rise of the motor. As motor temperature rise is in turn determined by the ability of the motor to dissipate heat, circulation to the motor should not be restricted. Improper selection of motors with regard to temperature ratings may result in high motor operating temperatures with accompanying reduction in motor life.

In general, the electrical insulation is the portion of the motor most susceptible to injury from high operating temperatures. Of the several types of insulation which are available, the most common type, specified as Class A by the *National Electrical Manufacturers Association*, consists of cotton, felt, paper or similar organic materials and permits a 55 C rise in temperature over a 40 C ambient temperature. Class B insulation consists of mica, asbestos, fiber glass, or similar inorganic materials and permits a 75 C rise in temperature over the 40 C ambient temperature. Other types of insulation such as silicone resin are available and permit extremely high operating temperatures.

The mechanical construction of the different types of motor enclosures and the rise in temperature with Class A insulation for each type are enumerated in the glossary at the end of this chapter. Since the difference in temperature between the hottest spot and the nominal temperature, as measured by a thermometer, is greater for a completely unprotected machine than it is for an enclosed machine, the permissible temperature rise is smaller for an open motor.

FUNCTIONS OF CONTROL EQUIPMENT FOR MOTORS

In general, control equipment for all types of motors should provide: (1) means of disconnecting the motor from the power supply; (2) means

TABLE 1. CLASSIFICATION OF MOTORS

POWER SUPPLY	TYPE	SPEED CHARACTERISTICS	FULL VOLTAGE		HP RANGE	TYPE OF APPLICATION SEE FOOTNOTE †
			STARTING TORQUE	STARTING CURRENT		
		Constant Speed Drives				
d-c	1. Shunt	Constant	Normal (with controller)	Normal	All	(*a*) Fans and (*c*) centrifugal pumps and centrifugal compressors
	2. Compound	Variable	High (with controller)	Normal	All	(*b*) (*c*) (*e*) Reciprocating pumps and frequent or hard starting
	3. Series	Variable	High (with controller)	Normal	Small	(*d*) Fans direct connected
POLY-PHASE a-c	4. Squirrel-Cage General Purpose Class A	Constant	Normal 0.8–1.5 times	High 6–8 times	All	(*a*) Fans and (*c*) centrifugal pumps and centrifugal compressors
	5. Squirrel-Cage Class B	Constant	Normal 0.8–1.5 times	Normal 5–6 times	Medium Small	(*a*) Fans and centrifugal pumps and centrifugal compressors
	6. Squirrel-Cage Class C	Constant	High 2–2.6 times	Normal 5–6 times	Medium Small	(*b*) Reciprocating pumps (*e*) and compressors started loaded
	7. Wound Rotor	Constant or Variable	High 1–2.5 times (with secondary control)	Low 1–3 times	All	(*a*) Hoists (*b*) reciprocating pumps and compressors (*c*) and frequent (*e*) or hard start
	8. Synchronous High Speed	Exactly Constant	Normal 0.75–1.75 times	Normal 5–7 times	Medium Large	(*a*) Fans and centrifugal pumps and centrifugal compressors
	9. Synchronous Low Speed	Exactly Constant	Low 0.3–0.4 times	Low 3–4 times	Medium Large	(*a*) Reciprocating compressors starting unloaded
SINGLE PHASE a-c	10. Capacitor	Constant	High	Normal	Small	(*b*) Pumps and compressors
	11. Capacitor Fan	Constant	Normal	Normal	Small	(*a*) Fans, centrifugal pumps
	12. Capacitor Start Induction Run	Constant	High	Normal	Small Fractional	(*a*) Fans (*b*) pumps and compressors
	13. Repulsion Induction	Constant	High	Normal	Medium Small	(*a*) Fans (*b*) pumps and compressors
	14. Split Phase	Constant and Adjustable	Normal	Normal	Fractional	(*a*) Fans (*b*) pumps and compressors (*d*) fans—direct

†Applications:

a. Drives having medium or low starting torque and inertia (WR^2) such as fans and centrifugal pumps or reciprocating pumps and compressors started unloaded.

b. Drives having high starting torques, such as reciprocating pumps and compressors started loaded.

c. Similar to (*a*) except where frequent or hard starting (large WR^2) requires a higher starting and accelerating torque.

d. Fans direct connected.

e. Stoker drives.

TABLE 1. CLASSIFICATION OF MOTORS—(Concluded)

POWER SUPPLY	TYPE	SPEED CHARACTERISTICS	FULL VOLTAGE		HP RANGE	TYPE OF APPLICATION SEE FOOTNOTE †
			STARTING TORQUE	STARTING CURRENT		
		Adjustable Speed Drives				
d-c	15. Shunt Field Adjustment	Constant	Normal (with controller)	Normal	All	(*a*) Fans and (*e*) centrifugal pumps
	16. Armature Resistance Adjustment	Variable	Normal (with controller)	Normal	All	(*a*) Fans and (*e*) centrifugal pumps
	17. Variable Voltage Control	Constant	Normal (with controller)	Normal	All	(*d*) Fans and centrifugal pumps
POLY-PHASE a-c	18. Squirrel-Cage High Slip. Transformer Adjustment	Variable	Normal	Normal	Medium Small	(*a*) Fans
	19. Squirrel-Cage Separate Winding or Regrouped Poles	Constant Multi-Speed	Normal or High	Normal or Low	All	(*a*) Fans (*b*) pumps and (*c*) compressors
	20. Wound Rotor	Variable	High (with secondary control)	Low	All	(*a*) Fans (*b*) centrifugal pumps and compressors
SINGLE PHASE a-c	21. Repulsion	Variable	High	Normal	Low and Fractional	(*a*) Fans—centrifugal pumps (*b*) compressors
	22. Capacitor Low Torque Tapped Winding	Variable Two Speed	Low	Normal	Fractional	(*d*) Fans, direct
	23. Capacitor Low Torque Transformer Adjustment	Variable	Low	Low	Fractional	(*d*) Fans
	24. Split Phase Regrouped Poles	Constant	Normal	Normal	Fractional	(*d*) Fans

for starting the motor; (3) overload protection for the motor; (4) protection against low voltage; and (5) means for varying the motor speed.

Full voltage starting for motors is preferable because of its lower first cost and simplicity of control. Except for d-c machines, most motors are mechanically and electrically designed for full voltage starting. The starting inrush current, however, is limited in many cases by regulations of power companies because of the voltage fluctuations which may be caused by heavy current surges. It is therefore often necessary to reduce the starting current below that obtained by across-the-line starting. The power supplier should be consulted to determine the allowable inrush current for any given location.

The choice between full voltage and reduced voltage starting is governed almost entirely by inrush current limitations. The starting torque of all motors varies with the starting current and it is therefore necessary to insure that the motor is supplied with sufficient current to develop enough torque to accelerate the load.

In present practice overload protection of motors is obtained by use of thermal overload inverse time limit type protection. The usual setting of such protection devices is at 125 per cent overload, the element trip-

ping after a definite interval of time. The National Electric Code requires the addition of fuses or circuit breakers to protect the overload elements from severe short circuit currents.

Two types of protection are available against low voltage at the motor terminals. One type, called low voltage release, permits the motor line contactor to drop out on low voltage and to close again when the voltage returns to normal, thereby restarting the motor when the abnormal condition is ended. The second type, called low voltage protection, causes the motor line contactor to drop out on low voltage but prevents restarting when the voltage returns to normal except by the action of an operator. This latter type of protection is desirable where it is necessary for the operator to make initial starting adjustments on the machine.

Manual control for an alternating or a direct current motor is usually located near the motor. When so located an operator must be present to start and stop or change the speed of the motor by operating the control mechanism. Manual control is sometimes employed only as a device to give overload protection and another device is employed to start and stop the motor. Manual control is used particularly on small motors which operate unit heaters, small blowers, and room coolers in an air conditioning system. In other cases manual control in the form of drums, when used with multi-speed motors, is only used as a speed setting device while the starting and stopping functions operate automatically through thermostats and pressure switches.

Because of the increasing complexity of air conditioning systems, the equipment is operated preferably by automatic control and less dependence is placed on manual operation and regulation.

Automatic control of motor starters may be accomplished by the use of remote push button stations, by a thermostat, float switch, pressure regulator, or other similar pilot devices. An added advantage of automatic control is that the main wiring for the starter may be installed near the motor, while the starter may be operated by a control device located elsewhere.

DIRECT CURRENT MOTORS

Direct current motors are classified (see Table 1) according to type of winding as: *shunt wound*, *compound wound*, and *series wound*.

Shunt Wound motors, being suitable for application to fans, centrifugal pumps, or similar equipment where the amount of starting torque required is relatively small, are used for the majority of direct current applications in the field of heating, ventilating, and air conditioning. They may be used on reciprocating pumps and compressors if started under unloaded conditions.

Without auxiliary control the shunt wound motor is designated as *constant speed.** Fig. 1 illustrates the characteristics of direct current motors, showing speed, horsepower, and torque as a function of current. The speed regulation* of small size shunt wound motors from ¾ hp to 5 hp is 12 per cent as specified by the *NEMA* while on larger motors it is 10 per cent.

Compound Wound motors are required for application to reciprocating compressors, stokers, reciprocating pumps when started under loaded

*Refer to Glossary at end of chapter.

conditions, and other similar equipment requiring high starting torque. The characteristics of this type of motor are such that for starting torques above full-load torque the starting current required is somewhat less than for the shunt wound motor. Compound wound direct current motors are normally used whenever frequent starting makes high starting and accelerating torque desirable. Without auxiliary control, compound wound motors are designated as *varying speed*,* and have a speed regulation of 25 per cent.

Series Wound motors find only limited application in a few special cases and are available in a limited range of sizes. The motors are used where extremely high starting torques are required and must be applied only to direct coupled continuous loads due to the fact that the speed

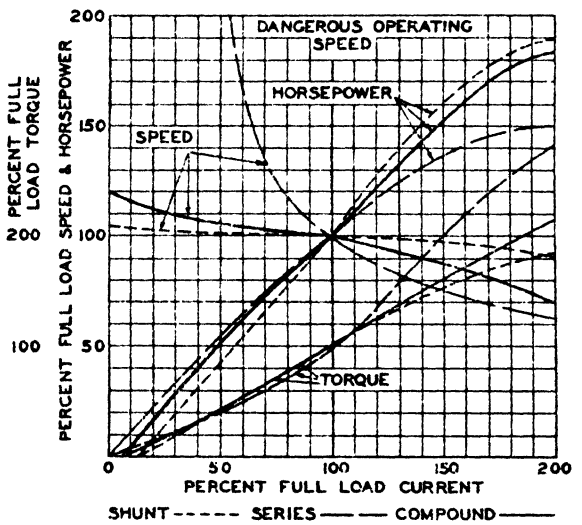


FIG. 1. CHARACTERISTICS OF DIRECT CURRENT MOTORS

of the motor becomes dangerously high when the motor is operated at a light load.

Typical d-c motor specifications are shown on page 625.

DIRECT CURRENT MOTOR CONTROL

Direct current motors are usually started through starting controllers which use a resistance, in series with the motor armature, which is gradually cut out as the motor comes up to speed. Motors up to 2 hp may be linestarted providing the inrush current causes no serious voltage fluctuations in the power supply line.

Constant Speed and Varying Speed Motors. As shown in Fig. 2, the recommended practice for manual starting of motors over ½ hp requires the use of a fused safety switch or circuit breaker and a face-plate type starter. For automatic push button starting a safety switch or circuit breaker and an automatic starter are recommended.

*Refer to Glossary at end of chapter.

Adjustable Speed Motors are normally shunt wound and are operated at various speeds by varying a resistance connected in series with the motor field. A maximum range of speed of about 5 to 1 can be obtained by this means. Rated speed regulation is 22 per cent for motors of this type from 2 to 5 hp; 15 per cent is standard in larger sizes. The *NEMA* practice on rating adjustable speed d-c motors is defined in the Glossary at the end of the chapter.

The control for the adjustable speed motor consists of the addition of a field rheostat for speed control to the equipment specified for the constant speed motor.

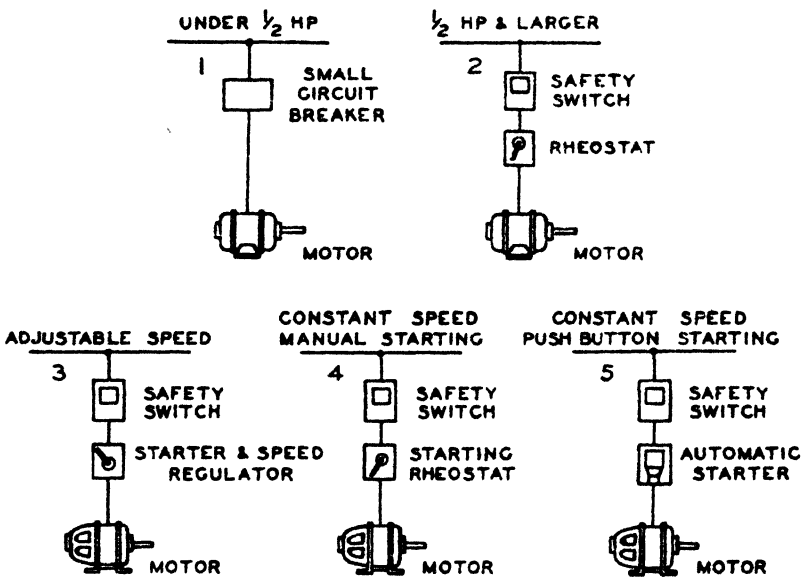


FIG. 2. RECOMMENDED CONTROLS FOR d-c MOTORS

*Adjustable Varying Speed** Motors are d-c motors in which the speed is varied by the addition of resistance in series with the armature. The speed of the motor by this means is always less than the rated full field speed and varies widely with a change in load, especially with high series resistance. Fig. 3 illustrates typical speed characteristics of this type of motor for different values of armature resistance.

The addition of series resistance in the armature circuit reduces the motor speed by lowering the voltage on the armature. At one-half speed the voltage is approximately one-half of line voltage. Consequently, with rated full load current the power delivered by the motor will be only one-half of the maximum, *e.g.*, it will be 5 hp from a 10 hp motor, because the other 5 hp will be lost in the resistance. It is, therefore, evident that the efficiency of the motor is reduced at reduced speeds due to the loss in the resistor.

Control for the adjustable varying speed motor is similar to that for the constant speed motor with the exception that the starting resistor

*Refer to Glossary at end of chapter

Typical Specifications for d-c Motors

.....Hp, ...RPM, {Constant / Adjustable / Varying} Speed, {Shunt / Compound / Series} Wound, {115 / 230 / 600} Volts d-c Motors For Driving ..... (Application) Motor Shall Be Arranged For {Horizontal / Vertical} Mounting And Shall Be Provided With A..... (Open, Splashproof, etc.) Type Of Enclosure, *NEMA* {Class A / Class B} Insulation, And {Ball / Sleeve} Bearings.

Typical Specifications for d-c Motor Control

Control For {Constant / Adjustable / Adjustable Varying} Speed d-c Motors Shall Be {Manual / Magnetic} And Shall Consist of a {Safety Switch / Circuit Breaker} And an Enclosed Controller Providing Overload Protection [And Low Voltage {Protection / Release}].

Typical Specifications for Squirrel-Cage Motors

.....Hp, ...RPM, {25 / 60} Cycles, {208 / 220 / 440 / 550} Volts, {2 / 3} Phase, Squirrel-Cage Induction Motors of the *NEMA* {Class A—Normal Starting Torque, Normal Starting Current / Class B—Normal Starting Torque, Low Starting Current / Class C—High Starting Torque, Low Starting Current / Class D—High Slip} Type Driving..... (Application) Motor Shall Be Arranged For {Horizontal / Vertical} Mounting And Shall Be Provided With A.....(Open, Splashproof, etc.) Type of Enclosure, *NEMA* {Class A / Class B} Insulation, And {Sleeve / Ball} Bearings.

must be designed for speed regulating duty which means that it must be capable of carrying the motor current continuously. Speed controllers are available both for constant torque applications and varying torque drives, such as required by fans, in which the torque is reduced considerably at reduced speed.

The *Adjustable Voltage* type of speed control is also often known as the variable voltage or Ward-Leonard system. For machines requiring a wide range in speed control and a large number of steps of control this type of system is used most extensively. The drive consists of one or more d-c motors, the armatures of which are supplied with power from a d-c generator and the fields of all machines are excited from a constant voltage exciter. A schematic diagram of connections for an adjustable voltage drive is shown in Fig. 4. In most cases the d-c generator is a part of a three-unit set including a constant speed a-c driving motor, and a constant voltage exciter. As the voltage on the generator and consequently on the d-c motor or motors is adjusted by a rheostat in the

generator field circuit, a great many steps are thus obtained in an efficient manner. With constant field excitation on the motor the speed of the motor will vary approximately as the voltage on the generator.

Extremely wide speed ranges are possible with the adjustable voltage type of drive. Ranges as high as 10 to 1 are common and, by the addition of field control on the motors, ranges as high as 40 to 1 are permissible. This type of drive provides the advantage of good speed regulation over the entire speed range, as shown in Fig. 3 in which this type of drive is compared with the adjustable varying speed drive.

Typical specifications for d-c motor control are shown on page 625.

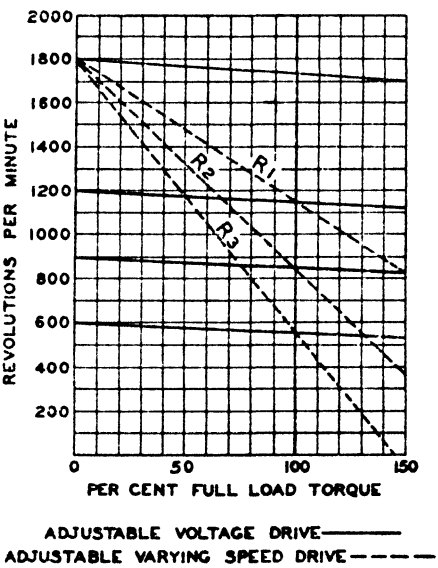


FIG. 3. SPEED TORQUE CHARACTERISTICS OF ADJUSTABLE VARYING SPEED DRIVE AND ADJUSTABLE VOLTAGE DRIVE

ALTERNATING CURRENT MOTORS

Alternating current motors are divided into two main classifications: *polyphase* and *single phase* (see Table 1), according to the type of power supply used. They are further subdivided as to the type of motor winding.

When polyphase power is available it is usually found more economical to apply polyphase motors in preference to single phase motors. A typical 5 hp, 1200 rpm capacitor start-induction run single phase motor, for instance, will cost approximately twice as much as the corresponding three phase Class B squirrel-cage motor. In addition, the polyphase motor has the advantages of higher power factor and higher efficiency.

Polyphase Motors

The three types of polyphase motors are: *squirrel-cage induction* motors, *wound rotor induction* motors, and *synchronous* motors.

Squirrel-Cage motors are specified by *NEMA* in classes providing a variety of speed and torque characteristics. Class A motors provide normal starting torque at normal starting current and are suitable for constant speed application, to equipment such as fans and blowers, in which *starting current need not be limited.* Class B motors provide normal starting torque at low starting current and are used for the same type of application as Class A *where starting current must be limited.* Class C

motors provide high starting torque with low starting current and are used on compressors, started without unloaders, and on reciprocating pumps. Class D motors have high slip* and are used with flywheels for widely pulsating loads on equipment such as reciprocating compressors and pumps where other motors would draw high peak currents.

Figs. 5, 6, 7, and 8 illustrate the characteristics of squirrel-cage motors. It will be noticed by inspection of Fig. 6 that both power factor and efficiency are improved if the motors are operating as near rated load as possible. In addition, as shown in Fig. 8, power factor and efficiency are better for higher speed motors.

Typical specifications for squirrel-cage motors are shown on page 625.

Wound Rotor motors are used for applications requiring high starting torque at low starting current, because a wound rotor motor with its

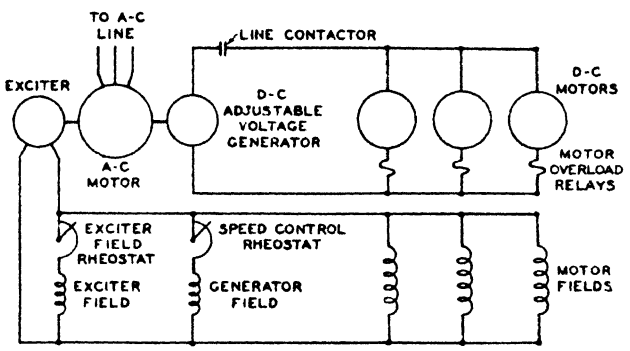


FIG. 4. COMPONENT PARTS OF AN ADJUSTABLE VOLTAGE DRIVE

controller and resistance can develop full load torque when starting with about full load current. For comparison, a squirrel-cage motor would require from 3 to 5 times as much current to develop full load torque at starting. The wound rotor motor is also used for varying speed service to drive fans, blowers, and other continuous duty apparatus. Typical specifications for wound rotor motors are shown on page 628.

The addition of resistance to the secondary winding of the wound rotor motor changes the speed torque characteristics as indicated in Fig. 9. The motor speed, with the resistance added, is dependent on load and consequently the motor has very poor speed regulation when secondary resistance is added to reduce the speed to values below 50 per cent.

Synchronous motors are used for continuous duty applications at constant speed where efficiency and power factor are important. Another advantage of these motors is that of lower initial cost in large sizes and for low speeds when compared with squirrel-cage type motors.

The outstanding advantage of the synchronous motor is that its power factor can be changed to compensate for the low power factor of other drives in the same location. Lagging power factor is an inherent characteristic of all induction apparatus, such as induction motors and neon signs. Unless synchronous motors or capacitors are installed, the plant power factor may be comparatively low. This does not necessarily mean that corrective equipment must always be installed, but in most cases it is desirable to determine what advantages may be gained by improving

*Refer to Glossary at end of Chapter.

Typical Specifications for Wound Rotor Motors

.....Hp, ...RPM, {25/60} Cycles, {208/220/440/550} Volts, {2/3} Phase, Wound Rotor Induction Motors For Driving..... (Application) Motor Shall Be Arranged for {Horizontal/Vertical} Mounting And Shall Be Provided With A..... (Open, Splashproof, etc.) Type of Enclosure, *NEMA* {Class A/Class B} Insulation and {Ball/Sleeve} Bearings.

Typical Specifications for Synchronous Motors

.....Hp, ...RPM, ...Per Cent P.F., ...Volts, {2/3} Phase, {25/60} Cycles, Synchronous Motors of the {Belted/Coupled/Engine} Type for Driving..... (Application) Motor Shall be Arranged for {Horizontal/Vertical} Operation and Shall Be Provided With A.....Type of Enclosure. (Open, Splashproof, etc.) Motor Shall be Capable of Developing A Starting Torque of ..... Per Cent Full Load Torque, A Pull-In Torque of ..... Per Cent Full Load Torque, And A Pull-Out Torque of..... Per Cent Full Load Torque. The Motor Field Shall Be Excited From A {Direct Connected Exciter/Belted Exciter/M-G Set Exciter/d-c Bus} Which {Shall/Shall Not} Be Included With The Motor.

the power factor. With purchased power, if the rates include a clause embodying a penalty for low power factor, or a bonus for high power factor, the saving in power costs may often make a very good return on the investment required for the corrective equipment.

Synchronous motors are used to drive fans, blowers, pumps, compressors and other applications. Compressor applications having a high peak torque require the use of flywheels to smooth out power peaks; and should always be referred to the electrical manufacturer for recommendations.

Synchronous motors are provided with built-in damper windings on the rotor and operate during the starting period similarly to squirrel-cage motors. After the motor is nearly up to speed, field excitation is applied and the motor draws into step at synchronous speed. After excitation is applied the motor runs at exactly constant speed and will remain at this speed until a load approaching the pull-out load is reached, whereupon the motor pulls out of synchronism and stops.

In applying synchronous motors consideration must be given to the torque the motor can develop on pull-in, that is, at the instant when field

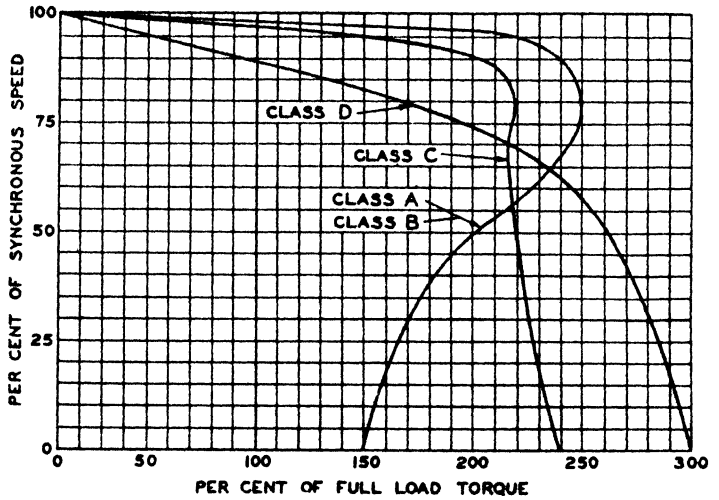


FIG. 5. SPEED TORQUE CHARACTERISTICS OF SQUIRREL-CAGE MOTORS

excitation is applied. Table 2 tabulates typical application requirements of synchronous motor drives, listing starting, pull-in, and pull-out torques.

Typical specifications for synchronous motors are shown on page 628.

Multi-Speed motors provide flexibility in many types of drives. Synchronous motors can be furnished only with a 2 to 1 ratio in speed, single winding. Squirrel-cage induction motors may be 2, 3 or 4 speed. Two-speed induction motors are usually of single winding type, having a 2 to 1 speed ratio such as 600 rpm and 1200 rpm, or may be double winding. Three-speed induction motors are always two winding, and four-speed motors are usually two winding with a 2 to 1 speed ratio

TABLE 2. TYPICAL APPLICATION REQUIREMENTS OF SYNCHRONOUS MOTOR DRIVES SHOWING STARTING, PULL-IN AND PULL-OUT TORQUES

	Application	Method of Connecting Motor to Load	Starting Conditions	Torques			Remarks
				Starting	Pull-in	Pull-Out	
Fans	Exhaust and Ventilating	Coupled or Belted	Usually Loaded	50	60-125	150	WR^2 of Fan Must be Considered
Blowers	Cycloidal Positive	Coupled or Engine Type	Unloaded	40-60	40-60	150	Two-Speed Motors Sometimes Used
Blowers	Blowing Engines Reciprocating	Engine Type	Unloaded	40	40-60	150	
Blowers	Turbo High Speed	Direct Connected or Step Up Gear	Unloaded (Intake Closed)	30	50	150	WR^2 of Blower Must be Considered
Compressors	Air	Engine Type	Unloaded	40	40	150	Flywheel Effect Important
Compressors	Ammonia and Ammonia Booster	High Speed—Belted Low Speed—Engine Type Occasionally Coupled	Unloaded (By By-Pass)	40	40	150	Flywheel Effect Important
Compressors	Freon	High Speed—Belted Low Speed—Engine	Unloaded (By By-Pass)	45	60	150	Flywheel Effect Important
Compressors	Gas Reciprocating	High Speed—Belted Low Speed—Engine	Unloaded (By By-Pass)	40	40	150	Flywheel Effect Important

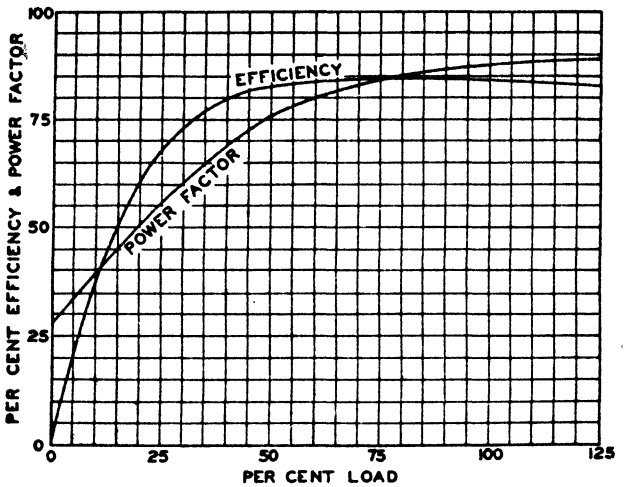


FIG. 6. VARIATION OF EFFICIENCY AND POWER FACTOR WITH LOAD FOR A TYPICAL 5 HP, 4 POLE 60 CYCLE, CLASS B, SQUIRREL-CAGE MOTOR

in each winding. Motors can be provided in constant torque, varying torque or constant horsepower ratings. The constant horsepower type of motor is considerably larger than the constant torque motor due to the fact that the same horsepower must be developed at either reduced speed or high speed.

In selecting two-speed motors for fan, pump, blower, or compressor applications, it is usually found that two winding motors are more expensive than the single winding type. The control cost for two-speed, two winding motors, however, is more economical, and therefore the combined price of both motor and control for the two winding motor is only slightly higher. Because of the improved performance of the two

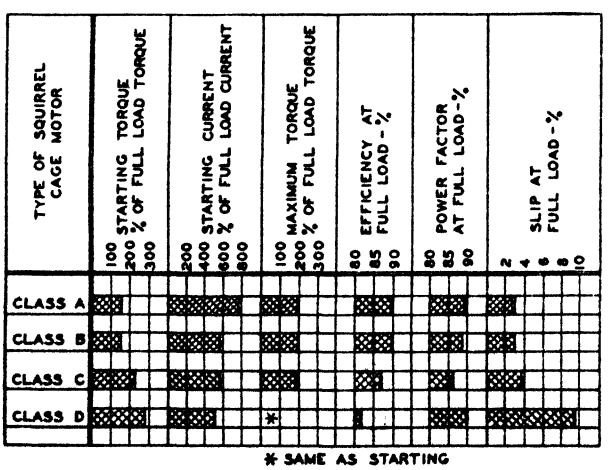


FIG. 7. COMPARATIVE PERFORMANCE OF SQUIRREL-CAGE MOTORS OF 30 HP AND SMALLER SIZES

winding motors and because of the factor of safety provided by two independent windings, the increased cost is frequently worth the difference.

Single Phase Motors

Single phase induction motors inherently develop no starting torque and are provided with auxiliary windings and devices for starting pur-

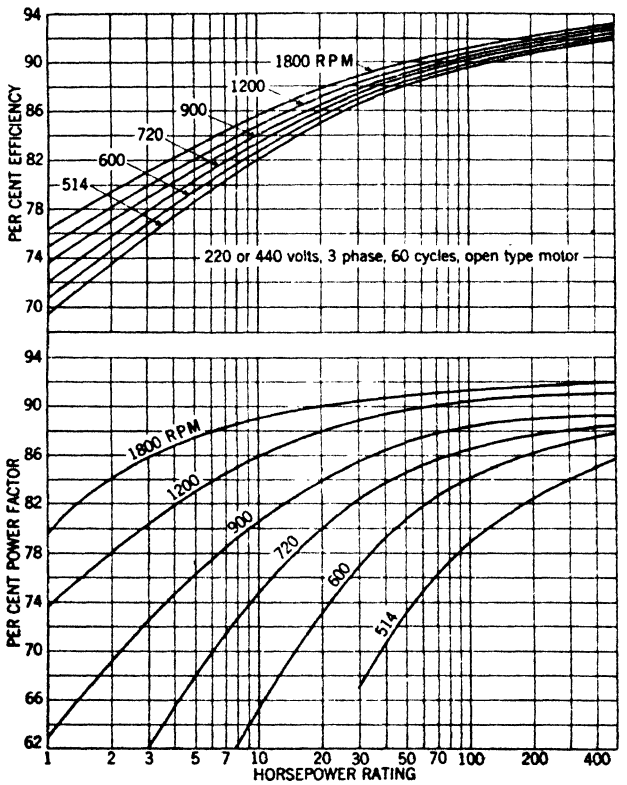


FIG. 8. EFFICIENCIES AND POWER FACTORS FOR SQUIRREL-CAGE INDUCTION MOTORS

poses. The motors are classified as to the type of auxiliary winding provided.

Capacitor Start-Induction Run motors develop high starting torque with low starting current and are used for all types of constant speed heavy duty drives such as compressors, pumps, and stokers. During the starting period, a winding with a capacitor in series is connected in the motor armature circuit and when the motor comes up to speed a centrifugal switch cuts the capacitor and second winding out of the circuit.

Capacitor motors, which are ideally suited for small fan drives, are similar to the capacitor start-induction run type except that the capacitor is not cut out when running.

Repulsion Start-Induction Run motors develop extremely high starting torque. They are supplied with a short-circuiting switch which cuts out

Typical Specifications for Single Phase Motors

.....Hp, ...RPM, {25/60} Cycles, {115/230} Volts, Single Phase Motor of the.....Type for Driving..... Motor Shall
(Capacitor, Split Phase, etc.) (Application)

Be Arranged for {Horizontal/Vertical} Mounting And Shall Be Provided With a.....Type of Enclosure, *NEMA* {Class A/Class B} Insulation, And
(Open, Splashproof, etc.)

{Ball/Sleeve} Bearings.

Typical Specifications for Squirrel-Cage Motor Control

Control for Squirrel-Cage.....Motors Shall Consist of An Enclosed
(Fan, Pump, etc.)

{Manual/Magnetic} Type {Across The Line/Reduced Voltage} Starter Providing Overload Protection And Low Voltage {Protection/Release}. Control Shall Include A Safety Disconnect Switch {Separately Mounted/In a Common Enclosure} With the Starting Controller.

Typical Specifications for Wound Rotor Motor Control

Control for Wound Rotor Motor Control for.....Applications Shall Consist of a Safety
(Fan, Pump, etc.)

Disconnect Switch, a {Separately/Common} Mounted Across the Line Starter Providing Overload Protection, Low Voltage {Protection/Release}, and a Secondary {Starting/Speed Regulating} Controller for {Separate Mounting/Mounting in Same Enclosure}. Primary and Secondary Control Shall Be Interlocked so as to Provide Complete Control from the Rheostat Handle.

the commutator when the motor comes up to speed. These motors are suitable for applications such as industrial compressors where high break-away torque is required and where commutator and brush noise are not factors.

Split Phase motors have a high resistance auxiliary winding which is in the circuit during starting but is disconnected through the action of a centrifugal switch as the motor comes up to speed. Under running conditions it operates as a single phase induction motor with one winding in the circuit. These units are available for the small horsepower ratings and when equipped with a high slip rotor may be used for adjustable

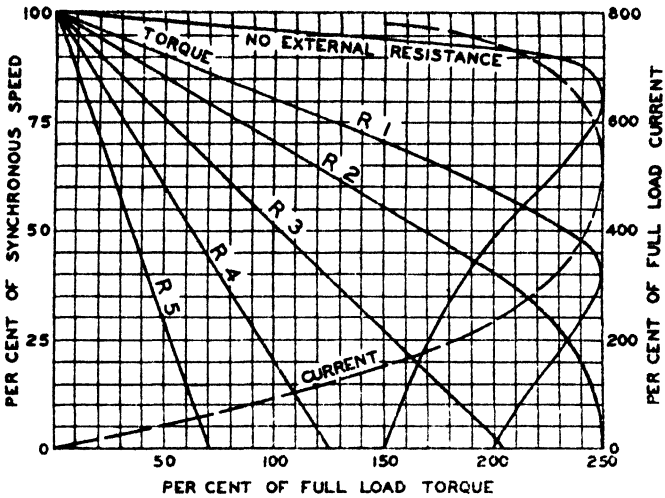


FIG. 9. PERFORMANCE CHARACTERISTICS OF A WOUND ROTOR MOTOR WITH EXTERNAL RESISTANCE

varying speeds through line voltage control. The motors are ideally suited for fan duty.

Speed-torque characteristics of single phase motors are shown in Fig. 10.

Typical specifications for single phase motors are shown on page 632.

CONTROL FOR ALTERNATING CURRENT MOTORS

Squirrel-Cage motors are usually linestarted where power company limitations permit. In sizes up to 2 hp the motors are started by means of manual switches with an overload current element for motor protection.

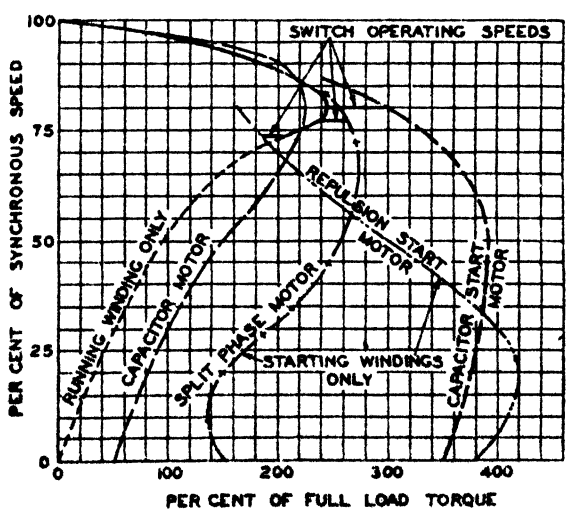


FIG. 10. SPEED-TORQUE CHARACTERISTICS OF SINGLE PHASE MOTORS

Typical Specifications for Synchronous Motor Control

Synchronous Motor Control for ..... (Application) ..... Motors Shall Provide for {Full Voltage / Reduced Voltage} Starting And Shall Be {Full Magnetic / Semi-Magnetic}. (Reduced Voltage Starting Shall Be Obtained By Means of {Autotransformers / Resistors / Reactors} And Shall Limit The KVA Inrush to a Maximum of ..... per cent of Full Load KVA.) The Control Panel Shall Be For {Isolated / Switchboard} Assembly And Shall Be of {Open Switchboard / Enclosed Cubicle} Construction. It Shall Provide Overload, Under Voltage Protection And After Pulling Out of Step Will {Automatically Resynchronize / Automatically Stop} The Motor.

Typical Specifications for Single Phase Motor Control

Control For Single Phase ..... (Fan, Pump, etc.) ..... Motors Shall Consist of a {Manual / Magnetic} Type {Across The Line / Reduced Voltage} Starter Providing Overload Protection (And Low Voltage); And A Separate Safety Disconnecting Switch.

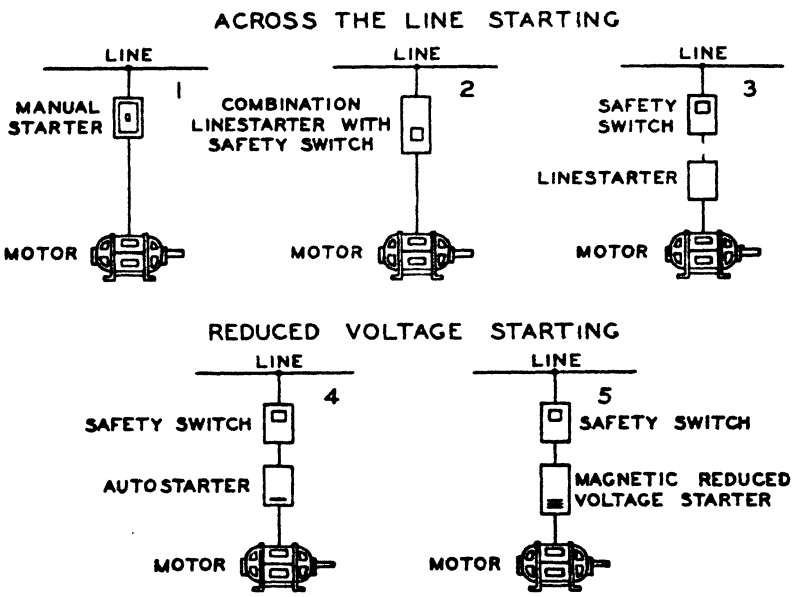
In larger ratings a linestarter is usually provided with either an additional safety switch or circuit breaker for disconnecting and short circuit protection. Reduced voltage starting may be either of manual or push button controlled magnetic type. In specifying this type of starter consideration should be given to the fact that starting torque of squirrel-cage motors varies as the square of the applied voltage. For example, a motor developing 100 lb-ft starting torque on full voltage would produce only 25 lb-ft torque on starting on half rated voltage. Fig. 11 illustrates recommended control practice for squirrel-cage motors. Typical specifications for squirrel-cage motor controls are shown on page 632.

Wound Rotor motors require control of both primary and secondary circuits. The primary* control may be the same as for squirrel-cage motors, manual or magnetic, at full voltage. Secondary* control provides means of varying secondary resistance for starting and speed control. The secondary controller should be specified for starting duty only or for speed regulating duty. Fig. 12 illustrates recommended control practice for wound rotor motors. Typical specifications for wound rotor motor control are shown on page 632.

*Refer to Glossary at end of chapter.

Synchronous motor starters should provide pull-out protection, automatic synchronization or automatic stopping of the motor after pull-out, and insurance of complete starting sequence, as well as overload and low voltage protection. The control may be either magnetic or semi-magnetic at full or reduced voltage. Semi-magnetic starters provide automatic field control but require hand operation for closing the line contactors to start and transfer to full voltage.

In applying reduced voltage starters to synchronous motors it should be remembered that, since these motors are started on damper windings and during the acceleration period function similarly to squirrel-cage motors, the starting torque varies as the square of the applied voltage.



Arrangements 2, 3, 4 and 5 provide automatic push-button starting.

FIG. 11. RECOMMENDED CONTROLS FOR SQUIRREL-CAGE MOTORS

Consideration should be given to insure development of sufficient motor torque to accelerate the load. Typical specifications for synchronous motor control are shown on page 634.

Multi-Speed control may be either manual or magnetic, and at full or reduced voltage. When using automatic magnetic control with two-, three-, and four-speed separate winding or consequent pole motors, control may be obtained from a remote point by means of a push button master switch. The various speeds of the motor are obtained from the master switch by simply depressing the correct push button. This is known as selective speed control. It is commonly used in the smaller theater installations where the fan and motor are located backstage and the speed control is located in the lobby.

Multi-speed motor controllers may be provided with compelling relays which make it necessary for the operator to press the first speed button before regulating the motor to the desired speed. This insures that the motor is always started at low speed before adjusting to a higher speed.

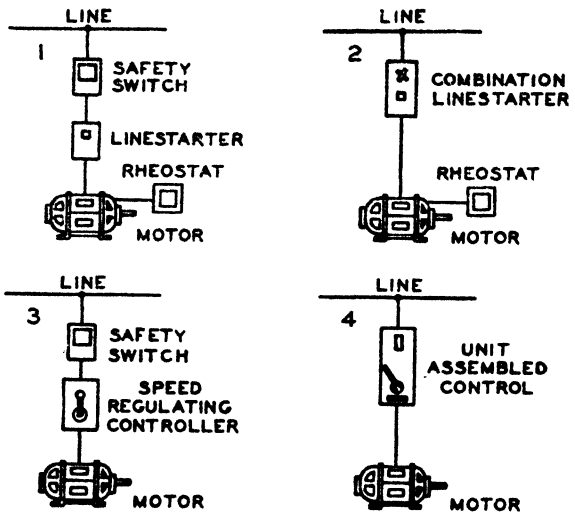
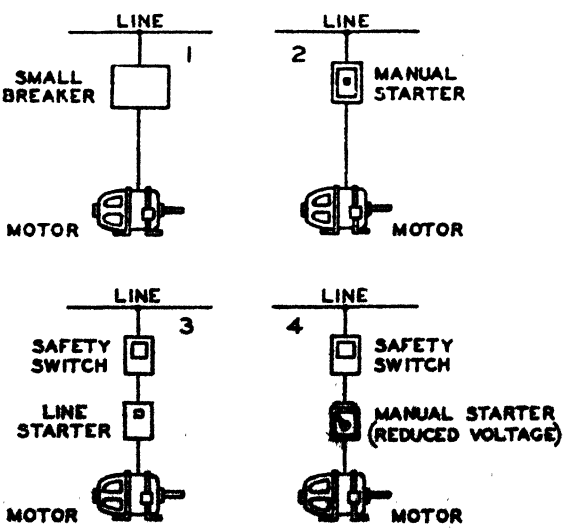


FIG. 12. RECOMMENDED CONTROLS FOR WOUND ROTOR MOTORS

Timing relays which provide for automatic acceleration may be used for control. With this feature the motor will always start at low speed and automatically accelerate to the desired speed. Decelerating relays may be used to reduce the shock effect of the braking action to the motor and drive when the speed is reduced from a higher to a lower speed.

Single Phase motor control usually consists only of a linestarter, either manual or magnetic. In some cases it is desirable also to provide a disconnect switch. Fig. 13 illustrates the recommended controls.

Typical specifications for single phase motor control are shown on page 634.



Arrangements 2, 3 and 4 are optional for motors up to 7½ hp, 220 volts.

FIG. 13. RECOMMENDED CONTROLS FOR SINGLE PHASE MOTORS

GEAR MOTORS

A gear motor is a self-contained combination of any type of a-c or d-c motor and an enclosed speed-reducing gear, providing a more compact and readily adaptable unit than is obtained by using a motor coupled to a gear reducer. Gear motors are available in sizes up to 75 hp with output shaft speeds from about 4 to 1430 rpm, making it possible to couple or to connect by gear or chain to nearly any machine. High speed motors are used, generally 1800 rpm on 60 cycles, thus obtaining the advantages of high motor power factor and efficiency. The gearing efficiency is also high, usually about 98 per cent for a single reduction of the helical or spur type, that is, a 2 per cent loss for one reduction or 4 per cent loss for a double reduction. Consequently, the over-all performance of the gear motors is much higher than a combination of open gearing, belting, countershaft, or other arrangement, which would otherwise be required. Gear motors are used extensively to drive numerous types of slow speed drives. Besides being more effective than other combination drives in saving space, they are important in reducing maintenance and operating hazards.

GLOSSARY

General Definitions

NEMA is the abbreviation for the *National Electrical Manufacturers Association.*

Speed Regulation (d-c motors) is the change in speed between no-load and full-load, expressed in per cent of full-load speed; for example, a motor having a no-load speed of 1200 rpm and a full-load speed of 1140 rpm would have a speed regulation of 5.6 per cent.

Slip (a-c induction motors) is the difference between the motor speed and synchronous speed expressed in per cent of synchronous speed, *e.g.*, a 1200 rpm motor operating at 1140 rpm would have a slip of 5 per cent.

Torque is an expression of the turning effort developed by the motor at the shaft and is usually expressed in ounce-feet for fractional horsepower motors and in pound-feet for motors of larger ratings.

Primary is the term usually applied to the high voltage or line side of a transformer or motor. In the case of the wound rotor motor the primary is the stator winding.

Secondary is the term usually applied to the low voltage or load side of a transformer or motor. In the case of the wound rotor motor the secondary is the rotor winding.

NEMA Classification of Motor Enclosures

Open motors (40 C rise) are self-ventilated machines having no restriction to ventilation other than that necessitated by mechanical construction.

Protected motors (50 C rise) have all ventilating openings in the frame protected by perforated covers.

Semi-Protected motors (50 C rise) have the ventilating openings in the top half of the frame only protected by perforated covers.

Drip Proof motors (50 C rise) are so constructed that drops of liquid or solid particles falling on the machine at any angle not greater than 15 deg from the vertical cannot enter the machine either directly or by striking and running along a horizontal or inclined surface.

Splash Proof motors (50 C rise) are so constructed that drops of liquid or solid particles falling on the machine or coming towards it in a straight line at any angle not greater than 100 deg from the vertical cannot enter the machine either directly or by striking and running along the surface.

Totally Enclosed Non-Ventilated motors (55 C rise) are so constructed as to prevent exchange of air between the inside and outside of the case.

Totally Enclosed Fan-Cooled Motors (55 C rise) are similar to totally enclosed, non-ventilated machines except that exterior cooling is provided by means of a fan or fans integral with the machine.

Explosion Proof motors (55 C rise) have an enclosing case designed to withstand an explosion of a specified gas or vapor which may occur within it, and to prevent the

ignition of the gas or vapor surrounding the motor by sparks, flashes, or explosion of the gas or vapor which may occur within the machine casing.

Water Proof motors (55 C rise) are so constructed as to exclude water applied in the form of a stream from a hose.

Dust Tight motors (55 C rise) are so constructed that the enclosing case will exclude dust.

Motor Speed Classifications

A Constant Speed Motor is one in which the speed remains practically constant with changes in load; *e.g.*, a d-c shunt wound motor or a-c squirrel-cage motor with low slip.

A Varying Speed Motor is one in which the speed varies with the load, usually decreasing when the load increases; *e.g.*, a d-c series motor or an induction motor with large slip.

An Adjustable Varying Speed Motor is one in which the speed can be adjusted gradually, but when once adjusted for a given load will vary in considerable degree with change in load; *e.g.*, a shunt wound d-c motor adjusted by armature resistance control.

An Adjustable Speed Motor is one in which the speed can be varied gradually over a considerable range, but when once adjusted remains practically unaffected by the load; *e.g.*, a d-c shunt motor with field resistance control. The standard ratings for open type, adjustable speed motors, having a speed range of 3 to 1 and greater are in accordance with the following:

(1) A standard continuous horsepower rating at 150 per cent of minimum speed with a temperature rise of 40 C.

(2) The next higher standard continuous horsepower rating at 3 times minimum speed with a temperature rise of 40 C.

(3) Between 150 per cent of minimum speed and 3 times minimum speed, the standard continuous horsepower rating with a temperature rise of 40 C will vary with the speed along a straight line connecting these two horsepower ratings. No further increase in horsepower is recognized above 3 times minimum speed.

(4) Below 150 per cent of minimum speed the lower continuous horsepower rating (see preceding item 1) will apply with a temperature rise of 50 C.

Example: 20/25 hp, 400 to 1600 rpm. This motor may be rated 20 hp, 40 C at 600 rpm and 25 hp, 40 C from 1200 to 1600 rpm. Between 600 and 1200 rpm the rated horsepower increases directly with speed from 20 to 25 hp.

(5) Motors may also be rated 1 hour with temperature rise of 50 C with the higher horsepower rating (see preceding item 2) throughout the entire speed range.

Example: 20/25 hp, 400 to 1600 rpm. This motor may be rated 25 hp, 50 C, 400/1600 rpm; 1 hour.

Mechanical Modifications

Vertical Mountings are available for such applications as pumps, agitators, and so forth. This type of application may require a special umbrella-type hood to protect against dripping liquids.

Flanged Mountings are available for use where motors are built in as part of machines. Motors may also be supplied with flush plate mountings, suitable for close coupled pump and similar applications.

Chapter 36

UNIT AIR CONDITIONERS, UNIT AIR COOLERS

Definitions, Classification of Unit Type Equipment, Component Parts of Unit Type Equipment, Sound Isolation, Modification of Remote Units, Rating of Unit Air Conditioners, Application of Unitary Equipment, Unit Air Coolers

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THIS chapter deals with the general characteristics and selection of factory produced units for air conditioning, air cooling, and attic ventilation, and with the factors involved in their application. In general, factory produced unit equipment can be obtained to accomplish all of the functions possible from field assemblies, but the advantages of unit equipment are most apparent in small and moderate capacities. Above 12,000 cfm capacity, or approximately 40 tons of refrigeration capacity, handling and assembly costs generally favor the use of field assembled units. Multiple application of unitary equipment is frequently justified for large gross tonnage installations where zoning or a minimum amount of air distributing ducts is desirable.

DEFINITIONS

The term *air conditioning unit* has been loosely used as a name for all types of factory produced air handling, cooling, or heating units. The code, Standard Method of Rating and Testing Air Conditioning Equipment[1], defines the various types of unitary equipment:

1. A *Cooling Unit* is a specific air treating combination consisting of means for air circulation and cooling within prescribed temperature limits.

2. An *Air Conditioning Unit* is a specific air treating combination consisting of means for ventilation, air circulation, air cleaning, and heat transfer with control means for maintaining temperature and humidity within prescribed limits.

3. A *Cooling Air Conditioning Unit* is a specific air treating combination consisting of means for ventilation, air circulation, air cleaning, and heat transfer with control means for cooling and maintaining temperature and humidity within prescribed limits.

4. A *Self Contained Air Conditioning or Cooling Unit* is one in which a condensing unit is combined in the same cabinet with the other functional elements. Self-contained air conditioning units are classified [2] according to the method of rejecting condenser heat (water cooled, air cooled, and evaporatively cooled), method of introducing ventilation air (no ventilation, ventilation by drawing air from outside, ventilation by exhausting room air to the outside, or ventilation by a combination of the last two methods), and method of discharging air to the room (free delivery or pressure type).

5. A *Free Delivery Type Unit* takes in air and discharges it directly to the space to be treated without external elements which impose air resistance.

6. A *Pressure Type Unit* is for use with one or more external elements which impose air resistance.

7. A *Forced-Circulation Air Cooler* is a factory encased assembly of elements by which heat is transferred from air to refrigerants [3].

CLASSIFICATION OF UNIT TYPE EQUIPMENT

Field assembled apparatus as described in Chapter 43 can be designed in shape, size, and capacity for any application, with the refrigeration and heating system exactly balanced to load conditions. To obtain the economies of mass production, factory built units must be standardized in a few models per manufacturer. Each model covers a range of capacities within the capacity of its fan to deliver air against the resistance of the unit and against the system resistance. For this reason, the unit

performance will usually represent a compromise between actual load requirements and the rated capacity. Within the range of accuracy of most load calculations, this compromise is not objectionable.

If the condensing unit and cooling and heating coil surfaces are carefully selected, and if proper consideration is given to reduction of piping losses, the performance of the combined system will compare favorably with field assembled apparatus. A system, in which the air handling unit is separated from the condensing unit, is called a remote system, and the conditioning unit is designated as a remote unit. The economical capacities of remote units usually range from 10 to 40 tons.

For applications where load calculations are subject to considerable variance and where close control is not considered essential, further economies of factory assembly can be obtained by combining the air handling and condensing equipment in one unit. This effects another compromise between load calculations and equipment selection, since the capacity of the combined unit is then dependent on the predetermined balance between a particular coil and condensing unit. These combination units are called self-contained units and, under the aptly descriptive name *store conditioners*, find economical application in 3, 5, 7½, 10, and 15 ton refrigeration capacities. These capacities, or limited multiples thereof, meet the load requirements of the majority of small and medium sized commercial establishments. With some modifications, these units can also be adapted to light industrial work.

To meet the requirements of individual comfort in small rooms and offices, where load calculations are subject to the indefinite design condition of *feeling cool*, self-contained units, called room coolers, find extensive and economical application. These units are usually restricted to summer and intermediate season operation, and range from ⅓ to 1½ tons of refrigeration capacity.

A special application of remote units is found in the unit air cooler which is used extensively in refrigeration work. Its primary function is to reduce temperatures in insulated and sealed storage spaces, and humidity control is a secondary consideration. Because of the small temperature differences between the coil and room temperatures, unit coolers handle three to five times as much air per ton as remote units used in air conditioning.

The attic fan completes the range of factory produced units for cooling. As its name implies, it is usually located at the top of a house and arranged to draw cool night air through the house. Its capacity is a function of the air changes per hour necessary to provide appreciable air movement.

COMPONENT PARTS OF UNIT TYPE EQUIPMENT

Units can be obtained for producing any of the required effects on air. As they function most satisfactorily when doing the work for which they were designed, field modifications are usually unadvisable because of expense involved as well as the possibility of causing unexpected difficulties in operation. The basic design considerations of unitary equipment follow.

Remote Units. Remote units can be obtained in two general classes, horizontal as shown in Fig. 1 and vertical as in Fig. 2. Their construction is essentially the same, except for the drain pan and filter locations.

Casings. Casings are generally constructed of sheet metal with angle iron frames and with removable panels for access to coil connections,

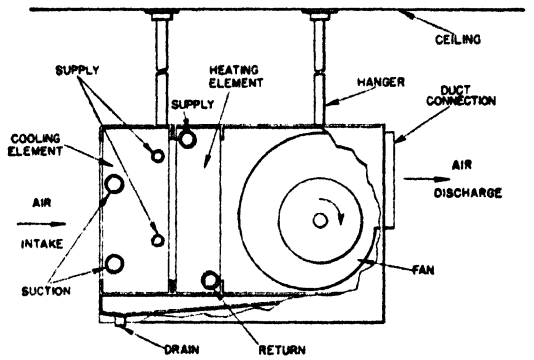

FIG. 1. HORIZONTAL REMOTE TYPE UNIT AIR CONDITIONER

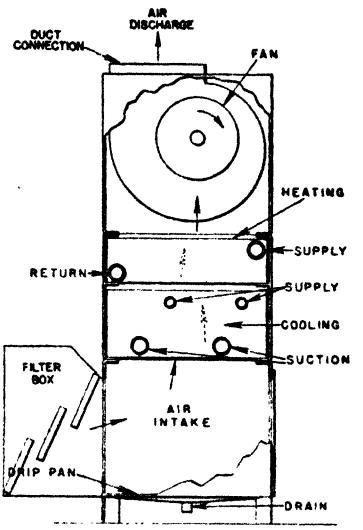

FIG. 2. VERTICAL REMOTE TYPE UNIT AIR CONDITIONER

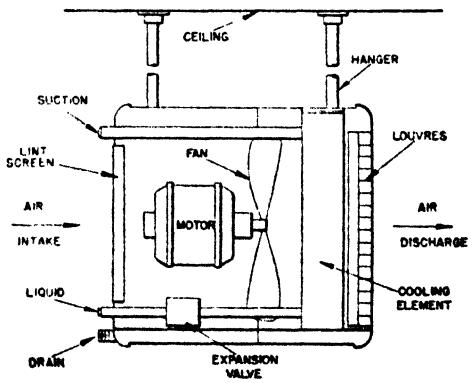

FIG. 3. SUSPENDED PROPELLER FAN TYPE UNIT AIR CONDITIONER

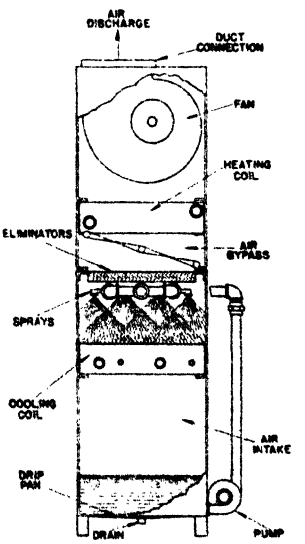

FIG. 4. SPRAY TYPE REMOTE UNIT AIR CONDITIONER

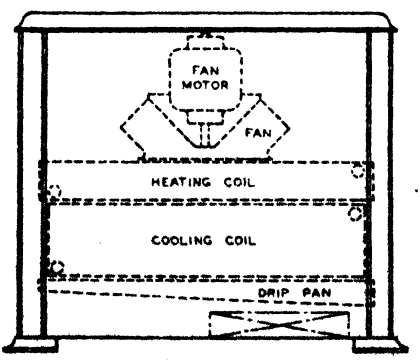

FIG. 5. REMOTE FLOOR TYPE ROOM UNIT AIR CONDITIONER

blower bearings, filters, and drain. Casings should be air tight. Panels should be tight fitting with cam or similar fastenings for easy opening. Panel openings at coils for heavy units should be large enough to receive coils after the casing is suspended. Frames should be fitted with lugs strong enough to suspend horizontal units. Non-metallic casings are of advantage in small remote units for reducing sound, particularly when propeller type fans are used.

Insulation. Remote units are available with waterproof and vermin-proof sound and heat absorbing insulation on the inside of the casing. They are also available with flanges and flanged access doors to permit insulation after installation.

Drain Pans. Because of the corrosive effect of mild picric, carbonic, and sulfurous acids absorbed by condensate, drain pans are usually made of 14 gage or heavier metal. They should be hot dipped galvanized after fabrication or otherwise treated to resist corrosion. Some manufacturers extend the drain pan under the entire unit, but in any case it should extend far enough to catch any condensate carried over from the coils. The drain connection should be readily accessible for cleaning and, in air conditioning work, should be generously sized and trapped. Some municipal codes require a minimum size of 1¼ I.P.S.

Blowers. The usual practice among manufacturers is to use light construction in the blowers in remote units, although a few are available with heavy duty blowers in the larger sizes. These blowers work under almost constant conditions without overload or shock and will usually last as long as the unit with reasonable maintenance. As lubrication of bearings is very important, it is good practice to locate the oil cups conveniently outside of the unit. In any application where considerable dehumidification or humidification is involved, such as in a system where the unit is handling 100 per cent outside air, it is important that the blowers be painted with asphaltum or other corrosion resistant paint to prevent excessive oxidation and corrosion of the blowers.

Some of the smaller suspended type units, Fig. 3, use propeller fans with a trailing edge blade in order to obtain required pressure characteristics with quiet operation. Since most of the motors driving these fans are direct connected and use brushes for starting, adequate access should be provided for maintenance and inspection.

Cooling Coils. The cooling and dehumidifying coils used in unit air conditioners are essentially the same as those used in central station units. The face area of the coil is usually fixed and the number of rows deep in the direction of air flow is the variable that determines capacity. It should be remembered, as noted in Chapter 39, that adequate coil surface is important for efficient performance of any system and that there is little economy in reducing coil depth to less than four rows.

Where multiple circuits are used in the larger coils, equal distribution of the cooling medium to the various circuits is vital in order to develop full capacity of the coil. The cooling coils also perform the function of dehumidification. To prevent carryover of condensate, eliminator plates should be used if face velocities exceed 500 to 530 fpm, unless adequate means of catching the droplets are provided.

When air is drawn upward through dehumidifying coils as in some vertical units, water is entrained within the fins and held in suspension. This increases the resistance pressure against which the blower operates and results in wide variation in air volumes handled between dry and wet

coil conditions. Some unit manufacturers have so designed vertical units that the air passes through the coils horizontally in order to overcome this difficulty.

Heating Coils. Heating coils of unit air conditioners are usually conventional blast coils and can be obtained with or without non-freeze steam distribution features. They usually match the cooling coils in face area and are one or two rows deep depending on the heating requirements. Where coils are selected for hot water and have more than two rows of tubes, the air resistance and the space requirements of the total number of rows of cooling and heating coils should be carefully checked.

Humidification. Spray type humidifiers are usually used in remote systems, but in some cases pan type humidifiers or steam humidifiers are also used. Some condensation on the inside of the unit casing may occur with possible water damage if the unit is located in a cold space without adequate insulation. Spray type humidifiers should be located so that no carryover of moisture occurs.

Filters. It is almost axiomatic that all units should have filters. Some small suspended units of 1 ton capacity or less with low coil face velocities and propeller fans are equipped only with lint screens or operate without filters, but in them the coils must be periodically cleaned and there is constant danger of clogging of the drain with the possibility of water damage. Filters used are usually of the throw-away type, although cleanable filters are available for most of the larger units. Care should be taken to insure adequate filter surface, since the cross-sectional area of the unit is seldom adequate for filter area. V-shaped or staggered filter arrangements are quite commonly used to increase filter area.

Motors. In some units where the motor is mounted inside, adequate access for maintenance and clearance for tightening belts are imperative. When motors are mounted in this manner, all of the heat equivalent motor input must be added to the heat load to be absorbed by the system and this requires a lower exit air temperature at the coils. Usually, however, the motor is located outside of the casing where it is readily accessible for service. In this case, only the brake horsepower required by the fan is transformed into heat to be included in the load calculations.

In either application, motors should be selected with adequate horsepower to handle the design volume of air against the resistance of the system when the coils are wet and then checked against the possible horsepower requirements for the increased volume of air when the coils are dry.

SOUND ISOLATION

Both suspended and vertical floor mounted units can transmit vibration through the supports. Wherever such transmission of sound might be objectionable, the supports should be isolated through rubber-in-shear or other sound deadeners (see Chapter 42).

MODIFICATIONS OF REMOTE UNITS

Features of various modifications of remote air conditioners are given in the following paragraphs.

Spray Type Unit

Fig. 4 shows a spray type unit used by designers who prefer air washing and coil wetting features. These units are equipped with a pump that sprays water or brine over the coils. Due to the direct mixing of the

condensate and the spray, provision must be made for overflow in summer and replacement of water evaporated in winter.

Dehumidifying Units

In a further modification of spray type units, absorbent brine solutions such as lithium chloride are used to remove moisture from the air. As explained in Chapter 38, the latent heat of the moisture removed is changed to sensible heat, so that coils must be used as after coolers to obtain the right dry-bulb temperatures. Factory produced units are also available for use with solid adsorbents such as silica gel. These are also described in Chapter 38.

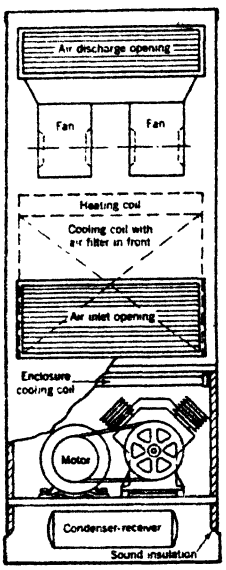

FIG. 6. SELF-CONTAINED WATER-COOLED AIR CONDITIONER

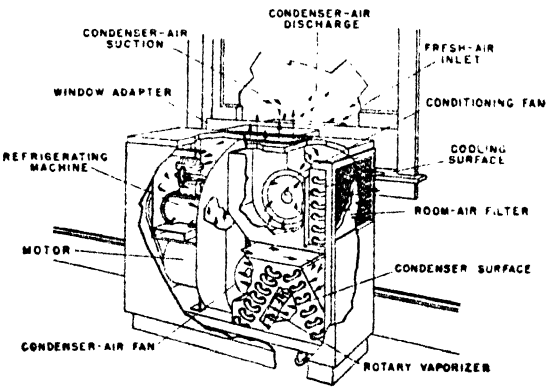

FIG. 7. SELF-CONTAINED AIR-COOLED UNIT AIR CONDITIONER

Remote Room Units

For individual rooms, with cooling load requirements of ½ to 1½ tons, remote units are available in attractive casings for installation within the room. A suspended type is shown in Fig. 3 and a floor type, such as is usually installed in place of an existing radiator, is shown in Fig. 5. Furnished with chilled water from a central plant, these units offer a satisfactory method of conditioning existing offices, hotel, and apartment rooms. These units may be obtained with filters and outside air connections, but for most satisfactory application are used as supplements to central systems that supply properly conditioned and filtered air to the areas served.

Induction type units, using primary conditioned air under pressure to induce local circulation, are described in Chapter 43.

Self-Contained Units

A typical large self-contained unit is shown in Fig. 6. It is essentially a remote vertical type conditioner mounted on top of a sound insulated

enclosure containing the condensing unit. Air distribution is obtained by means of grilles mounted in the discharge plenum when the unit is located in the conditioned area. Duct distribution of conditioned air can be obtained by removing the plenum connecting directly to the blower discharge, and safing the top of the unit.

The heat generated by the compression of refrigerant gases and that given off by the electric motor is removed from the compressor compartment in four ways: by the use of a water coil in the compressor compartment; by utilizing the cold suction gases; by drawing part of the return air through the compressor compartment, and finally by circulating room air through the compressor compartment by means of a fan attached to the motor shaft.

The 7½, 10, and 15 ton self-contained units usually have horizontal type conditioners. The condensing unit enclosures are not completely sound insulated, since they are not usually installed in the conditioned area. Most units can be divided into two or three sections for ease of handling and installation. Although most large self-contained units have water-cooled condensers, the 7½, 10, and 15 ton units can be obtained for operation with evaporative condensers.

Self-Contained Room Cooling Units

Small self-contained units can be obtained with water-cooled condensers but they are generally air cooled.

The air-cooled types are small in capacity, ranging from ⅓ to 1½ hp. Their principal application is for conditioning such spaces as hotel rooms, offices and residential living quarters. A duct connection between the unit and an outside window or ventilated air shaft is required to permit disposal of the heat extracted from the conditioned area. The unit may stand in front of the window or be mounted on the window sill. Various styles and types of windows are encountered which increase the difficulty of making the window connections. The evaporation of condensate on the condenser coils, as a means of disposing of this moisture, tends to increase the condensing capacity and reduce the operating head pressure. Some units add supplementary water so that increased capacity may be obtained from constantly wetted condenser coil surface. Connections to an electrical outlet may be by means of a conventional cord and plug or a permanent electrical connection, depending on local code rulings pertaining to the installation of small motors. The exterior finish of the unit in metal, wood or fabric is decorated to harmonize with office or bedroom furnishings.

A unit of the air-cooled condenser type for floor mounting is shown in Fig. 7. Of the two fans shown, the lower one acts as condenser air fan, and in some units this fan is arranged with slingers for discharging condensate on the condenser coil while the upper fan discharges air into the conditioned area.

A feature of the design shown in Fig. 7 is that the condensate from the cooling coil is sprayed over the condenser surface and vaporized, thus eliminating the need for drain connections. A simple dampering arrangement is generally provided for exhausting some air from the room, in addition to introducing outside air and recirculating required amounts of air. It is possible to remove the equipment for winter storage or utilize the ventilating features for winter operation.

Controls for Room Cooling Units

Control devices for self-contained cooling units are generally provided to include all necessary means for automatic operation. Provision is also made for adding auxiliary external controls when desired. Remote units are not generally equipped with controls. Control systems for remote units, and auxiliary controls for self-contained units, are covered in the general treatment of Controls in Chapter 34.

RATINGS OF UNIT AIR CONDITIONERS

There are two codes governing the rating and testing of unit air conditioners. The first code, Standard Method of Rating and Testing Air Conditioning Equipment [1], covers all types of air conditioning units except the self-contained type. The latter is covered by the second code, The Standard Method of Rating and Testing Self-Contained Air Conditioning Units for Comfort Cooling [2]. The two codes are necessary because of the basic difference caused by the heat given up by the self-contained units. The standard rating conditions for self-contained unit air conditioners, as given in the code, are set forth in Table 1.

The standard rating of a self-contained unit for the conditions specified in Table 1 includes all items which apply to the function of a unit as: (1) name of unit, (2) functions which unit performs, (3) data on cooling, (4) data on heating, (5) data on air flow, and (6) data on humidification.

The standard rating conditions for unit air conditioners, other than the self-contained type, are identical to those in Table 1 except the entering wet-bulb temperature for cooling is expressed as 50 per cent relative humidity (66.7 F wet-bulb) instead of 67 F wet-bulb temperature. In addition, the saturated suction refrigerant temperature for comfort cooling is specified at 40 F. This condition is omitted from Table 1 for self-contained units as immaterial in the rating of a unit that includes the evaporator and condensing unit.

APPLICATION OF UNITARY EQUIPMENT

One of the chief advantages resulting from use of factory produced units is the saving in installation and field assembly labor, a factor that should always be kept in mind when selecting a location for these units. Because of their compactness, the tendency exists to put them in closets, storage rooms, and other inaccessible places, where installation is so difficult that much of this cost advantage is lost.

Access panels are provided on units for the proper servicing and maintenance of the equipment. Adequate outside clearance at these panels is essential. Wherever there is danger of freezing of coils or clogging with dirt, sufficient clearance should be available for replacing them without removing parts of the building.

The outstanding source of difficulties in unitary systems is usually dirty filters. The characteristics of the light weight fans used are such that air volume drops off rapidly with increase in static resistance. Since changing filters is an unpleasant duty likely to be neglected unless it can be done easily, the operator should be at the same level as the filters, rather than under them, when they are being removed.

Fan speeds should be selected accurately for the system resistance.

TABLE 1. STANDARD RATING BASIS FOR SELF-CONTAINED AIR CONDITIONING UNITS

FUNCTIONS	TYPES OF UNITS	RATING CONDITION		
		Item	Description	Value
All	All	a	Barometric Pressure	29.92 in. Hg.
Cooling	Water-Cooled, Air-Cooled and Evaporatively-Cooled Condensers	b	Unit Ambient and Air Entering Room—Air Inlet (1) Dry-Bulb (2) Wet-Bulb	 80 F 67 F
		c	Ventilation Air	See Note
	Water-Cooled Condensers	d	Water Temperature Entering Unit	75 F
		e	Water Temperature Leaving Unit	95 F
	Air-Cooled and Evaporatively-Cooled Condensers	f	Air Entering Outside Air Inlet (1) Dry-Bulb (2) Wet-Bulb	 95 F 75 F
Heating	All Types Provided with Heating Function	g	Unit Ambient and Total Air Entering Unit	70 F
		h	Heating Medium, Pressure or Temperature (1) Dry Saturated Steam (2) Water In (3) Water Out	 16.7 lb per sq in. abs 180 F 160 F
Humidifying	All Types Provided with Humidifying Function	i	Unit Ambient	70 F
		j	Total Air Entering Unit (1) Dry-Bulb (2) Wet-Bulb	 70 F 53 F
Air Circulation	All	k	Filters	New and Clean

Note: Rating shall be based on both ventilation and recirculated room air entering at 80 F dry-bulb and 67 F wet-bulb temperature. (The *Note* as given in the code has been condensed in order to remove material not pertinent to this chapter).

Variable pitch motor pulleys are often used for field adjustments which should be made when filters are slightly dirty to obtain average conditions.

Because varying sizes of coils are used within the same casing, it is very important that coil safing be carefully installed to prevent by-passing of unconditioned air. If coils are not equipped with individual casings, additional safing may be required on top to prevent short circuiting air down through the upper edges of the fins. In this same category is the need for careful installation of the various sections of sectionalized units, using a sealing compound if necessary to prevent air leakage into the fan section of the unit.

Since the drain connection is usually made on the exit side of the coil, it is important that the drain line be properly sealed. This seal should be at least twice as deep as the suction on the fan in inches of water, to prevent gurgling sounds and to insure a positive seal against infiltration of odors and moisture laden air. Drain pans should not be used to support the coils unless they are designed to hold this weight without sagging.

As the movement of air draws the condensate or excess humidification water toward the fan, drain connections are usually located on the exit side of the coil. The advantages of quick drainage are lost if improperly supported coils distort drain pans and cause water to accumulate in the center or back of the pan.

When the fans of vertical units are stopped, condensate that has been held up in the coils by fan suction drops into the drain pan and splashes against the casing. If water damage is to be avoided, flashings should be provided to prevent this water from running out of the unit at the seams.

When locating unitary equipment, floor and beam loadings should be carefully checked. Suspended horizontal units can add 50 to 100 lb per square foot to the loading on the floor above. Should this floor be already heavily loaded, or be a roof structure designed for a 40 lb per square foot snow load, excess beam deflection may occur and cause cracking of plaster or concrete fire-proofing. A small fire, normally of little consequence, may cause a rupture of a heavily loaded structure and permit the equipment to drop with extensive property damage. Self-contained units should be carefully installed since their weights run as high as 200 lb per square foot. When they are installed in street floor shops, the extra precaution of placing a column beneath them in the basement is an inexpensive method of reducing vibration as well as providing insurance against overloaded floor beams.

The services required for operation of unitary equipment should conform to the many restrictive, but necessary, local municipal codes. Existing buildings seldom are wired adequately for the electrical load imposed by the starting of an air conditioning compressor on any branch circuit. Even the smallest room cooler can draw enough current to reduce the voltage of a lighting circuit to the point where it is visibly apparent. This voltage drop may even affect the life of the unit due to the relatively slow starting. The cost of a separate electrical circuit of adequate capacity from the main panel is more than justified; it is a necessary expense in the majority of installations.

A water supply of adequate capacity and pressure is necessary to prevent overloading of electrical equipment by high head pressures. The average city water supply pressure is adequate for installations up to the third floor. Since most water cooled units require about 20 lb pressure, including control valve losses, it is important that any units served by gravity from roof tanks be checked carefully if located less than 40 ft below the tank.

Drain connections from condensers should flow to an open and properly trapped sink as required by most city codes. This prevents back pressures on the city water system in the event of condenser failure. A check valve should also be installed in the water supply as a further precaution against contamination.

When installing small remote or self-contained units with outside air connections in buildings more than 6 stories high, the effect of wintertime stack action in elevator and stairwells requires special attention. This stack action is the cause of negative pressures on the lower floors, tending to draw cold air through the units, and positive pressures on the upper floors preventing adequate ventilation and disrupting air distribution. It can also cause annoying whistling at door openings that is a serious source of complaint in hotels and offices. Wherever the removal of such

units is impractical, it is important that carefully fitted, felt-edged dampers be installed in the outside air intakes with adequate locking devices.

One further consideration when installing self-contained units in conditioned areas is that any maintenance or repairs to be required in future years must be carried on in occupied space. If this is kept in mind in locating units, much inconvenience can be avoided.

UNIT AIR COOLERS

This type of unit is primarily intended to perform the main function of cooling air, with humidity control a secondary function within the limitations of the design. The main application of this equipment is in process and product refrigeration, such as cold storage warehousing, fruit and vegetable packing, in breweries, and in wholesale and retail food markets.

Application of the unit method of air cooling with mechanical circulation is comparatively recent, being an improvement over the pipe or finned coil, which depended on gravity for circulation. Bunkers were sometimes constructed around the coils to direct the air flow and sometimes fans were used for forcing air over the coils. The location of the unit air cooler is usually within the refrigerated area, but the larger, blower type models may be remotely located.

Design and Performance. Greater application and use of commercial refrigeration have resulted from the development of the unit air cooler. Flexibility of design has permitted almost any condition to be met. Finned type coils are usually employed, with continuous fan operation. By varying such physical features as tube size, fin spacing, refrigerant circuiting, the depth of coil rows, and air volume over the coils, the designer is able to produce a wide range of performances and to offer many desirable features not obtainable with the coil and bunker method. Higher suction temperature operation, more uniform temperatures, higher relative humidities with the defrosting cycle, moderate first cost, and a minimum of installation expense are likewise factors in their development.

New uses have appeared for unit air cooler application in industrial and commercial processes involving both the raw materials and finished product, where the maintenance of low temperatures is a necessary part of these processes. Of particular interest is the new field of extreme low temperature application where many new uses for refrigeration are being found.

Types of Units. The two standard types are the suspended or ceiling type, and the vertical or floor mounted type. There are variations of these such as the panel type which is wall mounted and arranged to take in air from the lower section and discharge it from the upper section.

The ceiling type has the appearance of a unit heater, with its propeller type fan blowing air through a bank of coils. Singly or in combination, they are easily installed and occupy little or no useful space. Alterations may be accomplished with little cost by relocating units or adding additional ones for increased capacity.

The floor mounted types employ blower type fans, as their air deliveries are higher and their locations may be remote from the space to be refrigerated. Air velocities and volumes must be designed for the individual application. Due to the small temperature difference between coil and air, the air volumes handled are many times greater than in comfort air conditioning work. Where a defrosting cycle is not practical, this type of

unit may employ a pump to spray a eutectic solution over the coils for the purpose of avoiding frosting.

Ratings. In order to rate and test equipment of this kind which normally operates below the frost temperature, a proposed code, Standard Methods of Rating and Testing Forced-Circulation and Natural Convection Air Coolers for Refrigeration [3], has been issued. In this standard, the gross cooling effects are taken since the motor power input equivalent is to be computed as part of the load.

REFERENCES

[1]—Prepared by a Joint Committee of the *American Society of Refrigerating Engineers*, AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS, *Refrigerating Machinery Association*, *National Electrical Manufacturers' Association*, and *Air Conditioning Manufacturers' Association* (*A.S.R.E. Circular* No. 13-42).

[2]—Standard Method of Rating and Testing Self-Contained Air Conditioning Units for Comfort Cooling prepared by a Joint Committee of the *American Society of Refrigerating Engineers*, AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS, *Refrigerating Machinery Association*, *National Electrical Manufacturers' Association*, and *Air Conditioning Manufacturers' Association* (*A.S.R.E. Circular* No. 16).

[3]—Proposed A.S.R.E. Standard Methods of Rating and Testing Forced-Circulation and Natural Convection Air Coolers for Refrigeration (*A.S.R.E. Circular* No. 25-44).

Chapter 37

SPRAY APPARATUS

Air Washers, Humidification with Air Washer, Dehumidification and Cooling with Air Washers, Well and Water Main Temperatures, Apparatus for Direct Humidification, Atmospheric Water Cooling Equipment, Selection of Water Cooling Equipment, Design Wet-bulb Temperatures for Water Cooling, Cooling Ponds, Spray Towers, Cooling Tower Design, Cooling Tower Performance, Winter Freezing

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AIR humidification is effected by the vaporization of water and always requires heat from some source. This heat may be added to the water prior to the time vaporization occurs or it may be secured by a transformation of sensible heat of the air being humidified to latent heat as the vapor is added to the air. The thermodynamics of the process are discussed in Chapter 3. The removal of moisture from air may or may not involve the removal of heat from the air-vapor mixture. With spray equipment, dehumidification of air always necessitates the removal of heat.

AIR WASHERS

An air washer consists essentially of a chamber or casing in which is provided a spray nozzle system, a tank at the bottom of the chamber for collecting the spray water as it falls, and an eliminator section at the leaving end of the chamber for removal of drops of entrained moisture from the delivered air. Air is drawn through the casing of the washer, where it comes into intimate contact with the spray water. A heat transfer takes place between the air and water, resulting in either humidification or dehumidification of the air, depending upon the method of operation and the relative temperatures of air and spray water.

To prevent backlash of spray ahead of the washer chamber and to aid in more uniform air distribution, inlet diffusion plates or eliminator baffles, where necessary, are provided in the air entrance end of the air washer. Inlet diffusion plates are used when the air flow and water spray are in the same direction; eliminator baffles of special design are used where one or more of the water sprays opposes the air flow. At the outlet end of the washer suitable flooded eliminator plates are used. These plates, for the removal of entrained moisture, usually cause four to six changes in direction of the air flow.

Figs. 1 and 2 show the essential construction features of conventional air washers. Intimate contact between the air and the water is secured; (1) by breaking the water into fine drops, (2) by passing the air over surfaces continuously wetted by water, or (3) by a combination of the two.

The wetted surfaces in an air washer may be of fibre glass, metal or scrubber plate construction. Scrubber plate types of washers are generally used to wash reclaimable products from the air and are composed of several baffle type plates located across the air stream. Water is supplied at the top of the washer to spray over these plates. In the case of the fibre glass or metal surfaces the water spray is usually rather coarse and at low pressure. In many cases these sprays are set at an angle with the air flow. Air washers of this type not only perform necessary heat transfer functions, but also are effective removers of dust and dirt from the air stream.

Essential requirements in the air washer operation are: uniform distribution of the air across the chamber section, moderate air velocity of from 250 to 600 fpm in the washer chamber, an adequate amount of spray water broken up into fine droplets throughout the air stream, at pressures of from 15 to 30 psi, sufficient length of travel through the water spray and wetted surfaces, and the elimination of entrained moisture from the outlet air.

Expected performances, physical size, length, number of sprays, etc., vary greatly, depending upon the functions of the installation. In general, the width and height of an air washer are dictated by the space available. Washers of nearly equal height and width are desirable from an air flow and economic standpoint although not necessary. The length

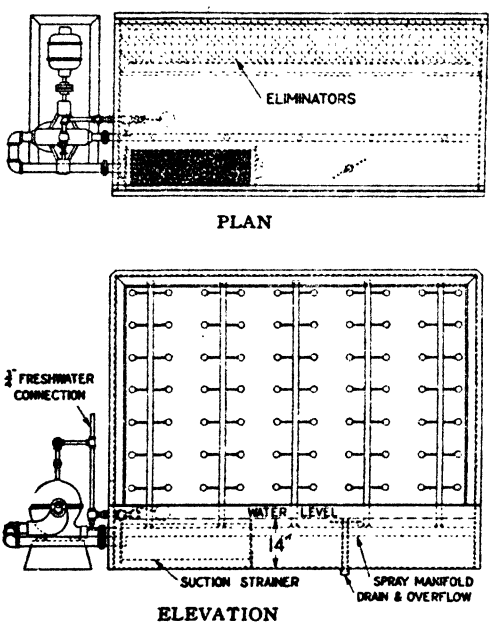

FIG. 1. TYPICAL SINGLE-BANK AIR WASHER

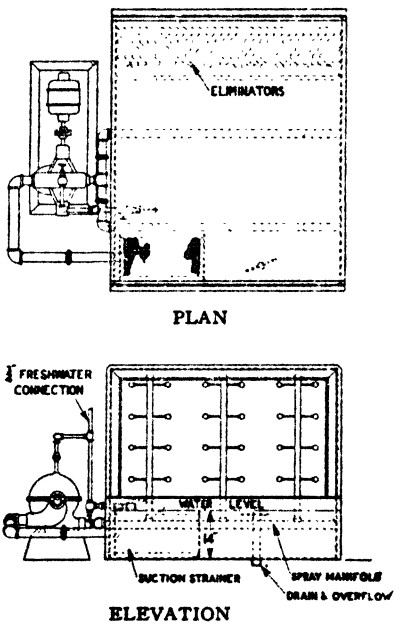

FIG. 2. TYPICAL TWO-BANK AIR WASHER

of washers varies considerably. A space of approximately 2½ ft between spray banks is used and the first and last banks of sprays are located about 1 ft to 1½ ft from the entering or leaving end of the washer. In addition air washers are very often furnished with cooling coils or heating coils within the washer chamber and the use of these coils affects the overall length of the washer.

Where increase of overall heat transfer between the air and water is required, multistage washers are used. These washers are equivalent to a number of washers in series and the water is often pumped from one stage to the other where conditions permit.

The resistance to air flow through an air washer varies with the type of eliminator and wetted surfaces, number of banks of spray and their direction, air velocity, size and type of other resistances such as cooling and heating coils, and other factors such as air density. Resistances vary from as low as ¼ in. to higher than 1 in. and it is therefore necessary that the manufacturer be consulted in regard to the resistance of any particular washer design involved.

HUMIDIFICATION WITH AIR WASHER

Air humidification can be accomplished in three ways with an air washer. These are: (1) use of recirculated spray water without prior treatment of the air, (2) preheating the air and washing it with recirculated spray water, and (3) using heated spray water. In any air washing installation the air should not enter the washer with a dry-bulb temperature less than 35 F in order to eliminate danger of freezing the spray water.

Method 1. Except for the small amount of energy added from outside by the recirculating pump in the form of shaft work, and for the small amount of heat leak from outside into the apparatus, including the pump and its connecting piping, the process would be strictly adiabatic. Evaporation from the liquid spray would therefore be expected to bring the air immediately in contact with it to saturation adiabatically; and, since the liquid is recirculated, its temperature would be expected to adjust to the thermodynamic wet-bulb temperature of the entering air.

It does not follow from the foregoing reasoning that the whole air stream is brought to complete saturation, but merely that its state point should move along a line of constant thermodynamic wet-bulb temperature as explained in Chapter 3. The extent to which the final temperature approaches the thermodynamic wet-bulb temperature of the entering air, or the extent to which complete saturation is approached is conveniently expressed by a ratio known as *humidifying effectiveness* or *saturating effectiveness* and is defined:

$$e_h = \frac{t_1 - t_2}{t_1 - t'} \tag{1}$$

where

e_h = humidifying effectiveness, per cent.
t_1 = dry-bulb temperature of the entering air, Fahrenheit degrees.
t_2 = dry-bulb temperature of the leaving air, Fahrenheit degrees.
t' = thermodynamic wet-bulb temperature of the entering air, Fahrenheit degrees.

The following may be taken as representative humidifying or saturating effectiveness of an air washer for the conditions stated:

1 bank—downstream	60–70 per cent
1 bank—upstream	65–75 per cent
2 banks—downstream	85–90 per cent
2 banks—1 upstream and 1 downstream	90–95 per cent
2 banks—upstream	90–95 per cent

The humidifying or saturating effectiveness of a washer is dependent upon the essential items of design mentioned under Air Washers. Other conditions being the same, low velocity of air flow is more conducive to higher humidification effectiveness.

Method 2. The preheating of the air increases both the dry- and wet-bulb temperatures, lowers the relative humidity, but does not alter the humidity ratio (pound water vapor per pound dry air). At a higher wet-bulb temperature but the same humidity ratio, more water can be absorbed per pound of dry air in passing through the washer, assuming that the humidifying effectiveness of the washer is not adversely affected by operation at the higher wet-bulb temperature. The analysis of the process occurring in the washer itself is the same as that explained under *Method 1.* The final desired conditions are secured by adjusting the amount of preheating to give the required wet-bulb temperature at entrance to the washer.

Method 3. Even if heat is added to the spray water, the mixing occurring in the washer itself may still be regarded as adiabatic. The state

TABLE 1. AVERAGE MAXIMUM WATER MAIN TEMPERATURES[a]

STATE	CITY	TEMP. F
Ala.	Birmingham	84
	Mobile	73
Ariz.	Phoenix	81
	Tucson	80
Calif.	Anaheim	60
	Berkeley	69
	Fresno	72
	Fullerton	75
	Glendale	68
	Los Angeles	75
	Oakland	69
	Ontario	70
	Pasadena	82
	Pomona	75
	Riverside	78
	Sacramento	72
	San Bernardino	65
	San Diego	82
	San Francisco	62
	Whittier	75
Colo.	Denver	75
Conn.	Bridgeport	66
	Hartford	73
	New Haven	76
	Waterbury	72
D. C.	Washington	84
Del.	Wilmington	83
Fla.	Jacksonville	80
	Miami	80
	Tampa	77
Ga.	Atlanta	87
	Macon	80
Ill.	Chicago	76
	Cicero	76
	Evanston	73
	Peoria	67
	Rockford	59
	Springfield	82
Ind.	Evansville	86
	Gary	75
	Indianapolis	80
	South Bend	61
	Terre Haute	82
Iowa	Cedar Rapids	78
	Des Moines	77
	Sioux City	62
Kans.	Concordia	57
	Kansas City	86
	Topeka	88
	Wichita	72
Ky.	Louisville	85
La.	Baton Rouge	85
	New Orleans	85
Me.	Augusta	60
Md.	Baltimore	75
Mass.	Boston	80
	Cambridge	70
	Fall River	76
Mass.	Lowell	50
	Lynn	68
	New Bedford	70
	Salem	68
	Worcester	76
Mich.	Detroit	77
	Flint	70
	Grand Rapids	84
	Highland Park	77
	Jackson	56
	Kalamazoo	53
	Lansing	64
	Saginaw	82
Minn.	Duluth	55
	Minneapolis	80
	St. Paul	77
Mo.	Jefferson City	82
	Kansas City	84
	St. Joseph	84
	St. Louis	85
	Springfield	70
Nebr.	Lincoln	63
	Omaha	87
Nev.	Reno	61
N. H.	Manchester	76
N. J.	Jersey City	63
	Newark	74
	Paterson	78
	Trenton	79
N. Y.	Albany	68
	Buffalo	75
	Jamaica	56
	Mt. Vernon	74
	New Rochelle	75
	New York	72
	Rochester	70
	Schenectady	60
	Syracuse	74
	Utica	69
	Yonkers	70
N. C.	Asheville	74
	Charlotte	85
	Winston-Salem	82
N. M.	Albuquerque	65
Ohio	Akron	76
	Canton	50
	Cincinnati	84
	Cleveland	74
	Columbus	82
	Dayton	60
	Lakewood	82
	Springfield	72
	Toledo	83
Okla.	Oklahoma City	82
	Tulsa	85
Ore.	Eugene	60
	Portland	64
Pa.	Altoona	74
	Erie	75
	Johnstown	74
	McKeesport	82
	Philadelphia	83
	Pittsburgh	81
R. I.	Providence	68
S. C.	Charleston	80
	Greenville	81
	Spartanburg	78
S. D.	Rapid City	55
Tenn.	Chattanooga	84
	Knoxville	89
	Memphis	70
	Nashville	90
Texas	Amarillo	65
	Austin	90
	Beaumont	86
	Dallas	86
	Fort Worth	84
	Galveston	90
	Houston	84
	Port Arthur	83
	San Antonio	76
	Wichita Falls	85
Utah	Logan	44
	Salt Lake City	60
Va.	Fredericksburg	75
	Lynchburg	73
	Norfolk	80
Wash.	Olympia	58
	Seattle	62
	Spokane	51
	Tacoma	57
W.Va.	Charleston	85
	Huntington	78
	Wheeling	78
Wis.	LaCrosse	54
	Madison	58
	Milwaukee	70
	Racine	68
PROVINCE		
Alta.	Calgary	64
B. C.	Vancouver	60
Ont.	London	50
	Toronto	63
P.E.I.	Charlottetown	48
Que.	Montreal	78
	Quebec	68

[a]These averages taken from various city water main locations, with some actual values slightly higher and some lower than values shown.

point of the mixture should move in a direction determined by the specific enthalpy of the heated spray as explained in Chapter 3. It is possible, by elevating the water temperature, to raise the air temperature, both dry-bulb and wet-bulb, above the dry-bulb temperature of the entering air.

In each of the methods, 1, 2 or 3, the air leaving the air washer may require reheating to produce in the conditioned space the required dry-bulb temperature and relative humidity.

DEHUMIDIFICATION AND COOLING WITH AIR WASHERS

Cooling of the wet-bulb temperature of an air vapor mixture can be accomplished by an air washer if the temperature of the spray water is lower than the wet-bulb temperature of the air. Moisture removal is obtained when the spray water temperature is lower than the dew-point of the entering air. In these cases the final dry-bulb temperature and relative humidity of the leaving air are dependent upon the design factors of the air washer.

Both sensible and latent heat are removed in the process of dehumidification by cold spray water. Abstraction of sensible heat occurs during the entire time that the air is in contact with the spray medium. Latent heat removal takes place as condensation occurs. Therefore, the lower the spray temperature the greater the amount of moisture removal per pound of dry air, all other conditions remaining the same.

Washers with two or more banks of spray are usually selected for dehumidifying installations, whether for comfort or industrial installations. Generally such air washers cool the air to within one or two degrees (Fahrenheit) of the leaving spray water temperature; this differential will increase somewhat when the difference between the entering wet-bulb and leaving dew-point is relatively large.

Where a limited supply of cold water is available multiple stage washers may be used to great advantage. In such washers the cool water is pumped through the multiple spray systems in series and counterflow to the air flow. Such an arrangement brings the delivery air in contact with the coldest water, securing a maximum amount of cooling with economy of water.

When using cold well water or water from city water mains care should be used to secure accurate data on the water temperatures. Table 1 lists some approximate water main averages which may be used as a guide but they should be verified from local records. This is particularly true with city water main temperatures. In the case of well water temperatures Fig. 3 shows the approximate temperatures of water to be expected from wells at depths of 30 to 60 ft.

Air washers for dehumidifying and cooling usually have separate recirculating pumps. These pumps deliver a mixture of cold and recirculated water under the control of a three-way valve. The valve may be actuated either by a thermostat in the washer outlet or by a humidity or other controller in the space being conditioned.

Air washers for dehumidifying are very often furnished with direct expansion or water cooling coils within the washer space, in which case water for the washer sprays is entirely recirculated.

APPARATUS FOR DIRECT HUMIDIFICATION

Humidifiers may be divided into the following general types, according to the method of operation: (1) indirect, such as the air washer, which

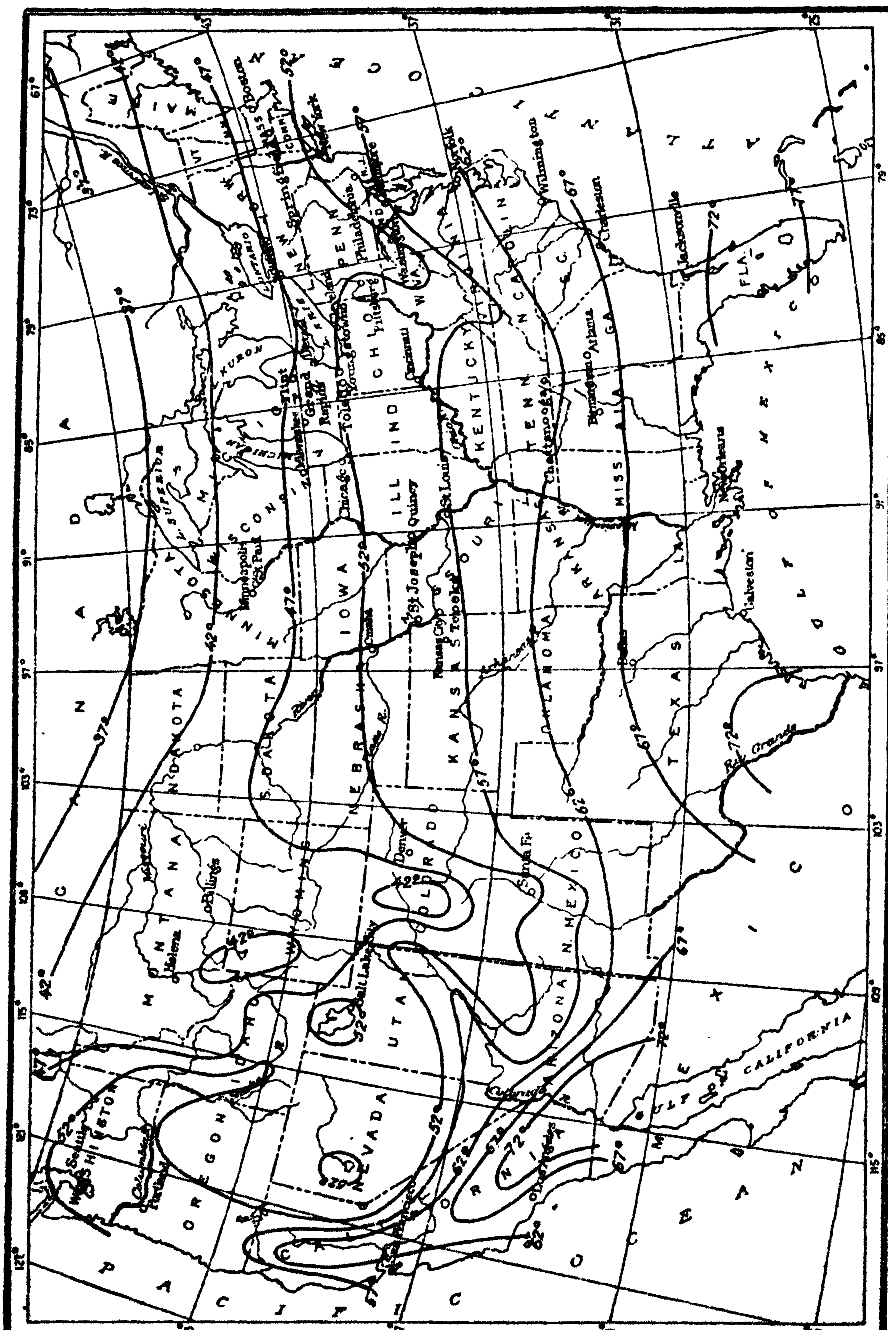

FIG. 3. APPROXIMATE WELL WATER TEMPERATURES AT DEPTHS OF 30 TO 60 FT[1]

introduces moistened air; and (2) direct, which sprays moisture into the room or introduces moisture by means of steam jets.

As in the cases of humidification by use of an air washer, the heat necessary for the vaporization of the moisture added to the air by direct humidification is secured either from heat stored in the spray water or by a transformation of sensible to latent heat in the air humidified. In the latter case the enthalpy of the air remains constant but the dry-bulb temperature of the air is reduced.

Direct humidification is usually preferable where high relative humidities must be maintained, but where there is little cooling or ventilation required. In comfort air conditioning, where both humidification and ventilation are required, the indirect humidifier is preferable. In industrial applications, where the cooling or ventilation load is large and where very high relative humidities must be maintained, a combined system employing both direct and indirect humidifiers is sometimes used.

Spray Generation

Spray generation is obtained by (1) atomization, (2) impact, (3) hydraulic separation, and (4) mechanical separation.

Atomization involves the use of a compressed air jet to reduce the water particles to a fine spray. With the *impact* method, a jet of water under pressure impinges directly on the end of a small round wire. Where *hydraulic separation* is employed, a jet of water enters a cylindrical chamber and escapes through an axial port with a rapid rotation which causes it immediately to separate in a fine cone-shaped spray. In the *mechanical separation* process, water is thrown by centrifugal force from the surface of a rapidly revolving disc and separates into particles sufficiently small to be utilized in certain types of mechanical humidifiers.

Spray Distribution

Spray distribution is obtained by (1) air jet, (2) induction, and (3) fan propulsion.

The air jet which generates the spray in atomizers also carries the spray through a space sufficient for its distribution and evaporation, and this method of distribution is termed *air jet.* Where distribution is obtained by *induction*, the aspirating effect of an impact or centrifugal spray jet is utilized to induce a current of air to flow through a duct or casing, and this air current distributes the spray. *Fan propulsion* obviously consists of the utilization of fans to entrain and distribute the spray.

Industrial type direct humidifiers are commonly classified as (1) atomizing, (2) high-duty, (3) spray and (4) self-contained or centrifugal.

Atomizing Humidifiers

There are several types of atomizing humidifiers which employ nozzles placed within the room and rely upon compressed air to effect complete atomization of the water so that it can be converted to vapor by the heat of the room air. Some of these nozzles depend upon an aspirating effect to draw the water into the nozzle and atomize it, others operate on a combined air and water pressure. It is usual for nozzles of the water pressure type to be controlled by a diaphragm valve actuated by the pressure of the atomizing air.

High-Duty Humidifiers

Water is supplied to high-duty humidifiers under high pressure (usually about 150 lb per square inch) through pipe lines from a centrally-located

pumping unit. The spray-generating nozzle which is of the impact type is located in a cylindrical casing. A drainage pan provides for the collection and return of unevaporated water which flows through a return pipe to a filter tank, from which it is recirculated. A powerful air current is forced through the humidifier by means of a fan mounted above the unit.

The air enters from above, is drawn through the head, charged with moisture, and cooled. It then escapes from the opening below at a high velocity in a complete and nearly horizontal circle. The spray is evaporated and the resulting vapor diffused. This distribution of fine spray over the maximum possible area promotes complete and rapid vaporization.

Spray Humidifiers

This type of humidifier consists of an impact spray nozzle in a cylindrical casing with a drainage pan below it. The aspirating effect of the spray nozzle induces a moderate air current through the casing which distributes the entrained spray. The general method of circulating and returning the water is similar to that employed for high-duty humidifiers. A suitable pump and centrally-located filter tank are required.

Self-Contained Humidifiers

The self-contained or centrifugal humidifier has the ability to generate and distribute spray without the use of air compressors, pumps, or other auxiliaries. These may be used either singly or in groups. In large installations, where suitable connections are provided to permit the cleaning and servicing of individual units without affecting the room as a whole, group control of the water and power may be employed.

ATMOSPHERIC WATER COOLING EQUIPMENT

In the operation of a refrigerating plant or a condensing turbine, one of the main problems is the removal and dissipation of heat from the compressed refrigerant or the discharged steam. This is accomplished ordinarily by first transferring the heat of the gas to water in a heat exchanger, from which water it may then be dissipated in a number of ways. If the plant is situated on the banks of a river or lake, an intake may be taken up-stream or at a considerable distance from the discharge, to prevent mixing of the heated discharged water with the inlet water. If the source of cooling water is a city supply or a well, the discharge water may be run into the nearest sewer or open waterway. Lacking an unlimited water supply, or in cases where purchased water is too expensive or where the water available contains dissolved salts which would form scale on the heat-exchanging apparatus, it is necessary to recirculate the water, and to cool it after each passage through the heat-exchanger by exposure to air in an atmospheric water cooling apparatus.

Air has a capacity for absorbing heat from water when the wet-bulb temperature of the air is lower than the temperature of the water with which it is in contact. The rapidity with which this transfer of heat occurs depends upon (1) the area of water in contact with the air, (2) the relative velocity of the air and water, and (3) the difference between the wet-bulb temperature of the air and the temperature of the water. The rate of heat dissipation is influenced further by many small factors[2] prevailing upon these primary ones, and complicating the design. Selection of equipment for any specified service must ultimately rest in over-all economic considerations established from reliable performance data.

As the heat content of the air increases, its wet-bulb temperature rises. (See Chapter 3.) Because it is impracticable to leave the air in contact with water for a long enough time to permit the wet-bulb temperature of the air and the temperature of the water to reach equilibrium, atmospheric water cooling equipment aims to circulate only enough air to cool the water to the desired temperature with the least expenditure of power.

In an air washer, humidifier or dehumidifier, the air is first conditioned by water to change its temperature and moisture content before entering the place of use. In water cooling equipment the temperature of the water is reduced by air at a lower wet-bulb temperature and the cooled water is used for the purpose desired.

Both types of equipment have a common basis of design in that the size of the equipment is determined by the quantity of air to be handled as well as the quantity of water required. In atmospheric water cooling the purpose is to cool water and the actual quantity of air handled is only incidental to this purpose. In the air washer, the purpose is to condition a fixed quantity of air and the quantity of water is varied as required.

Selection of Water Cooling Equipment

The proper size and type of water cooling equipment for a given installation cannot be determined accurately without considering the characteristics of all types, together with all requirement factors and other matters which influence the selection. Very few installations are exactly alike in details of requirements, and conditions governing performance and operation of the several types of water cooling equipment vary widely with geographical location as well as other considerations. It necessarily holds, therefore, that requirement factors and equipment characteristics are closely interlocked and deserve careful study as a related whole.

Before the characteristics of a specific water cooling apparatus can be judged desirable or undesirable the survey must conclude definitely the importance of each of the following items: first cost including all necessary auxiliaries, area, height, weight, effect of wind velocity and direction, drift nuisance, make-up water requirements and cost of chemical treatment if needed, total power for pumping (plus fan operation in the case of mechanical draft), maintenance, available locations (with due thought to possible future expansion, wind restrictions, space cost, proximity and accessibility, etc.), appearance, the equipment's operating flexibility for most economical conformance to varying loads or seasonal changes, and other considerations occurring with regard to a specific application.

Sizes of Equipment

Assuming a definite quantity of water, the size and design of atmospheric cooling equipment are affected by the following primary conditions:

1. Temperature range through which the water must be cooled.
2. Number of degrees above the wet-bulb temperature of the entering air to which the water temperature must be reduced.
3. Temperature of the atmospheric wet-bulb at which the required cooling must be performed.
4. Time of contact of the air with the water. (This involves height or length of the apparatus and velocity of air.)
5. Surface of water exposed to each unit quantity of air.
6. Relative velocity of air and water.

Items 1, 2, and 3 are established by the type of service and geographical location, while items 4, 5, and 6 depend upon the design of the equipment.

The establishment of a proper cooling range depends upon: (1) type of service (refrigerating, internal combustion engine and steam condensing). (2) wet-bulb temperature at which the equipment must operate satisfactorily, (3) type of condenser or heat-exchanger used.

Because the design of an entire plant is usually affected by the quantity and temperature of the cooling water supply, plants should be designed for cooling water conditions which can be most efficiently attained. The first consideration is usually the limiting temperature of the plant. For example, if an ammonia compressor refrigerating plant is to be designed for 185 psi head pressure as a normal maximum, the limiting temperature of the ammonia in the condenser is 96 F. Should the ammonia temperature go above this figure the head pressure will exceed 185 psi and power consumption increases. To obtain this head pressure, the temperature of the circulating water leaving the condenser must always be less than 96 F by an amount depending upon the size and design of the condenser, the quantity of water being circulated, and the refrigerating tonnage being produced. A condenser having a large surface per ton of refrigeration may be designed to operate satisfactorily with the leaving hot water temperature within 3 or 4 deg of the ammonia temperature corresponding to the head pressure, while a small condenser might require a 10 deg difference.

Table 2 lists several gases with data as to the temperatures and pressures for which commercial condensers are designed. Internal combustion engines have limiting hot water temperatures of 125 F to 140 F for closed systems, and 110 F to 120 F for open systems, depending upon the quality of the cooling water. The cooling of such fluids as milk or wort has variable requirements and is usually done in counter-flow heat-exchangers in which the leaving circulating water is at a much higher temperature than is the leaving fluid.

The temperature range, once the hot water temperature is approximately known, depends upon: (1) the maximum wet-bulb temperature at which the full quantity of heat must be dissipated, and (2) the efficiency of the atmospheric cooling equipment considered.

Design Wet-Bulb Temperatures

The maximum wet-bulb temperature at which the full quantity of water must be cooled through the entire range is never, in commercial

TABLE 2. CONDENSER DESIGN DATA

Gas	Maximum Pressure Desired in Condenser	Gas Temperature in Condenser F Deg	Leaving Hot Water Temperature F Deg	
			Best Condenser Design	Average Condenser Design
Steam	28 in. vacuum	101.2	97	93
Steam	27 in. vacuum	115.1	110	105
Steam	26 in. vacuum	125.9	120	114
Ammonia	185 psi[a]	96.0	92	88
Carbon dioxide	1030 psi[a]	86.0	83	81
Methyl chloride	102 psi[a]	100.0	96	92
Dichlorodi-fluoromethane	117 psi[a]	100.0	96	93

[a]Head pressure.

design, the *maximum* wet-bulb temperature ever known to exist at the location nor the *average* wet-bulb temperature over any period. The former basis would require atmospheric cooling equipment several times greater than normal size, and the latter would result during a large part of the time, in higher condenser water temperatures than those for which the plant was designed.

An accepted design practice for air conditioning cooling towers, evaporative condenser and spray ponds is to use the maximum hourly outdoor dry-bulb temperature which has been equaled or exceeded 2½ per cent of the total hours for the months of June to September and the maximum hourly wet-bulb temperature which has been equaled or exceeded 5 per cent of the total hours for the same period. Tabulation of these data has not been completed. The limited portion of such data as are available is given in Table 3, Chapter 15 for airport weather stations; for other localities design dry-bulb and wet-bulb temperatures in use locally are tabulated as a guide to design temperatures.

Equipment for steam turbine condensers and internal combustion engines is usually based upon somewhat lower design temperatures if peak loads occur at night or during winter months when outdoor temperatures are lower.

Knowing the hot water temperature and the wet-bulb temperature for which the equipment must be designed, the cold water temperature must be chosen to place the requirement within the effectiveness range of the type of atmospheric water cooling apparatus to be used. This effectiveness is expressed as the percentage ratio of the actual cooling effect to the maximum possible cooling effect. Since the wet-bulb temperature of the entering air is the equilibrium temperature to which the water could be cooled, the effectiveness of water cooling apparatus can be indicated thus:

$$\frac{(\text{hot water temperature} - \text{cold water temperature}) \times 100}{\text{hot water temperature} - \text{wet-bulb temperature of entering air}}.$$

Magnitudes of this effectiveness ratio will vary through wide limits in accordance with construction and conditions of operation. Values indicative of the commercial range of the effectiveness ratio are given in Table 3, although unusual designs may operate outside these ranges.

From consideration of the factors which include the cooling range and design wet-bulb temperature, the quantity of water required can be calculated from the amount of heat to be dissipated. The normal amounts of heat to be removed from various processes of the cooling equipment are:

Compressor Refrigeration: 220 to 270 Btu per (minute) (ton). Usual practice is to assume: 250 Btu per (minute) (ton) which is equivalent to 30 gal per (Fahrenheit degree) (minute) (ton).

Steam Turbine Condensers: 950 to 980 Btu per pound of steam. Usual practice is to assume 970 Btu per pound of steam.

TABLE 3. EFFECTIVENESS OF ATMOSPHERIC WATER COOLING EQUIPMENT

Equipment	Cooling Effectiveness—Per Cent		
	Minimum	Usual	Maximum
Spray Ponds	30	40 to 50	60
Spray Towers	40	45 to 55	60
Natural Draft Deck Towers	50	60 to 75	90
Mechanical Draft Towers	50	60 to 75	90

Steam Jet Refrigerating Condensers: 1030 to 1150 Btu per pound of steam. Exact value depends upon initial steam conditions.

Diesel Engine Jackets: 2500 to 4000 Btu per bhp per hour. Usual practice is to assume 3500 Btu per bhp per hour.

Natural Gas or Gasoline Engines: 4500 to 6000 Btu per bhp per hour. Usual practice is to assume 5000 Btu per bhp per hour.

Cooling Ponds

A natural pond is often used as a source of condensing water. The hot water should be discharged close to the surface at the shore line. Natural air movement over the surface of the water will cause evaporation and carry away heat. Because increased density due to the loss of heat causes the cooled water to sink to the bottom of the pond, the suction connection for intake water should be placed as far below the surface as possible, and at as great a distance from the discharge as practicable.

Spray Cooling Ponds

The spray pond consists of a basin, above which nozzles are located to spray water up into the air. Properly designed spray nozzles break up the water into small drops, but not into a mist because the individual drops must be heavy enough to fall back into the basin and not drift away with the air movement. The water surface exposed to the air for cooling is the combined area of all the small drops. Since the rate of heat removal by atmospheric water cooling is a function of the area of water exposed to the air, the difference in temperature between the water and the wet-bulb temperature of the air, the relative velocity of air and water, and the duration of contact of the air with the water, a much larger quantity of heat may be dissipated in a given area with the spray pond than with the cooling pond, because of (1) the speed with which the drops travel as they are propelled into the air and fall back into the water basin, (2) the increased wind velocity at a point above the surrounding structures or terrain, (3) the increased volume of air used, and (4) the vastly increased area of contact between air and water [3].

Spray pond effectiveness is increased by (1) elevating the nozzles to a higher point above the surface of the water in the basin, (2) increasing the spacing between nozzles of any one capacity, (3) using smaller capacity nozzles to decrease the concentration of water per unit area, and (4) using smaller nozzles and increasing the pressure to maintain the same concentration of water per unit area. Usual practice is to locate the nozzles from 5 to 7 ft above the edge of the basin, to supply from 5 to 12 psi pressure at the nozzles, using nozzles spraying from 20 gpm to 60 gpm each and spacing them so the average water delivered to the surface of the pond is from 0.5 to 0.7 gpm per square foot. Best results are obtained by placing the nozzles in a long relatively narrow area located broadside to the wind.

Spray ponds may be located on the ground, or they may be placed on roofs. To prevent excessive drift loss, or the carrying of entrained water beyond the edge of the pond by the air on the leeward side, louver fences are required for roof locations and for those ground locations where space is so restricted that the outer nozzles cannot be located at least 20 ft to 25 ft from the edge of the basin. Such fences usually are constructed of horizontal louvers overlapping so the air is forced to turn a corner in passing through the fence, and the heavier drops of water are thrown back, owing to their inertia. The louvers also restrict the flow of air, particularly at the higher wind velocities, and thus further reduce the

possibility of water being carried off. The height of an effective fence should be equal to the height of the spray cloud. Louver boards are preferably of red gulf cypress or California redwood supported on cast-iron, steel or wood posts. Where building ordinances forbid the use of combustible materials, sheet metal is customarily used.

Algae growths, during warm weather, in cooling towers and spray ponds may be eliminated while the plant is in operation by the use of potassium permanganate. This chemical can be dissolved at the rate of 1 lb in 1¼ to 1½ gal of hot water. About 10 parts of permanganate should be used per million parts of cooling water. Enough of the permanganate solution should be added periodically to cause the water to have a pink color for a period of from 15 to 20 min. The best results are obtained when sufficient quantities are added periodically at intervals of several weeks, the time intervals being dependent upon local operating conditions. The chemical is non-poisonous and non-corrosive when used as directed.

Natural Draft Spray Type Towers

Where not more than 30,000 Btu per minute are to be dissipated, the natural draft spray type tower is a satisfactory apparatus. The word *tower* in this connection is somewhat of a misnomer as the apparatus is essentially a narrow spray pond with a high louver fence. As usually built, the nozzles spray down from the top of the structure and the distance from the center of the nozzle system to the fence on either side is not more than half the distance that the nozzles are elevated above the water basin. Heights range from 6 ft to 15 ft and the total width of a structure is not usually greater than its height. Spray towers occupy less space on small jobs than spray ponds of equivalent capacities because the towers have a capacity of from 0.6 gpm to 1.5 gpm per square foot of tower area. The wet louvers add to the surface exposed to the air.

Natural Draft Deck Type Towers

In past years much of the atmospheric water cooling on refrigeration work has been done with natural draft deck type towers, which are also referred to as *wind* or *atmospheric* towers. These towers consist of heavy wooden or steel framework from 20 to 40 ft high and from 10 to 20 ft wide, having open horizontal lattice-work platforms or decks at regular intervals from top to bottom, and a catch basin at the foot. The hot water is distributed over the upper part of the structure by means of troughs, splash heads, or nozzles, and it drips from deck to deck down to the basin. The object of the decks is to arrest the fall of the water so as to present efficient cooling surfaces to the air, which passes through the tower parallel to the decks. The decks add to the area of water surface exposed to the air both by causing it to splash into fine droplets and to spread over the deck surfaces, but since some deck designs furnish a resistance to air flow, too many decks may be a detriment.

To prevent the loss of water on the leeward side of the tower, wide splash boards are attached at regular intervals from top to bottom. In some towers these boards or louvers extend outward and upward, usually with lower edge (which is attached to the frame of the tower) somewhat below the level of the outer and upper edge of the next louver board below it. Some louvering designs add *secondary* louvering to these *primary* louvers. In such designs the primary louvers are generally broader and do not slope so sharply nor overlap one another since their function is merely to return to the interior of the tower the water caught

by the secondary louvering which extends upward from each primary louver's outer edge to the next primary louver above. The individual slats which comprise the secondary louvering may be arranged either vertically in an overlapping staggered manner with air passage between, or set horizontally with their flat surfaces sloping inward and spaced so their edges over-reach but permit free air passage. Secondary louvering reduces drift loss on this type of tower materially.

Efficiency of a deck tower is improved, within limits, by increased height, increased length, or increased width. The first two increase the area of water exposed to the wind, and the latter increases the time of contact of the air with the water. Performance is best when the wind blows crosswise to the tower and decreases with obliqueness of the angle until the effect of a lengthwise wind is virtually nil.

Wind Velocities on Natural Draft Equipment

Since natural air movement is the prime requirement for a deck type tower, spray cooling tower, or spray pond, the apparatus must be designed to produce the desired cooling at times when the wind velocity is below average, when the wet-bulb temperature is at the maximum chosen for design, and when the plant is operating at full load. The apparatus must also, for best results, be located with its longest axis at right angles to the direction of the prevailing hot weather breeze. Table 3, Chapter 15, gives the average summer wind velocities in representative United States cities. Natural draft cooling equipment should be designed to operate properly with *not more than one-half* of the *average* wind velocity, and in no case for a wind velocity of more than 5 mph. Natural draft equipment must not be obstructed by trees, buildings, or other wind deflectors.

Mechanical Draft Towers

Mechanical draft towers usually consist of box-like shells, constructed of wood, metal, or masonry, in which water is distributed uniformly at the top and falls to a collecting basin at the bottom. The inside of the tower may be filled with wood lattice work over which the water drips, or the water surface may be presented to the air by filling the entire inside of the structure with spray from nozzles.

Air is drawn through the tower by induced draft fans or propelled through it by forced draft fans. Since the air flows at a constantly sustained and comparatively high velocity (by contrast with natural draft equipment which varies in performance with every change of the wind's direction or velocity) the air and water are brought into contact under controlled conditions resulting in more efficient transfer of heat from a given quantity of water into a given volume of air. The least possible operating cost is achieved by that tower design which delivers the desired performance for the lowest total power input, both to fans for air movement and to pumps for raising and distributing the water.

The effectiveness of a mechanical draft tower is improved by increasing height, area, or air quantity. Increasing the height increases the length of time the air is in contact with the water without affecting seriously the fan power required, but it increases the pumping power needed. Increasing the area while maintaining constant fan power increases the air quantity somewhat and because of lowered velocities it increases the time this air is in contact with the water. The surface area of water in contact with the air is increased in both cases. Increasing the air quantity decreases the time the air is in contact with the water, but, since a greater quantity is passing through, the average differential between the water

temperature and the wet-bulb temperature of the air is increased, and this speeds up the heat transfer rate. Increased air quantities are obtained only at the expense of increased fan power, which increases approximately as the cube of the air quantity. Air velocities through mechanical draft towers vary from 250 to 450 fpm over the gross area of the structure.

Inside type cooling towers, where required, draw air from the outside and discharge the exhaust air to the outside at a point considerably distant from outdoor air intake. These indoor cooling towers may be either of the wood filled or the spray filled type but in many cases an air washer similar to a conventional type of air washer is used.

Cooling Tower Design

The method of design of equipment for energy transfer from water to an air-water vapor mixture is similar to that used for absorption equipment. Details of this procedure are available[4, 5, 6] and its application to the problem of the cooling tower operating at atmospheric pressure is illustrated by the following development. The nomenclature used is as follows:

a = over-all average wetted area (surface of water drops plus wetted tower surface) square feet per cubic foot of tower volume.
c = specific heat of liquid water, Btu per (pound) (Fahrenheit degree).
e = effectiveness.
ε = natural base.
G = weight rate of flow of air, pounds of dry air per hour.
h = enthalpy, Btu per pound of dry air.
h_a = enthalpy of air-vapor mixture, Btu per pound of dry air.
h'' = enthalpy of saturated air-vapor mixture at water temperature, Btu per pound of dry air.
K = over-all energy unit conductance, Btu per (hour) (square foot over-all average wetted area) (Btu enthalpy difference per pound of dry air).
Ka = over-all rate coefficient, Btu per (hour) (cubic foot of tower volume) (Btu enthalpy difference per pound of dry air).
L = water rate, pounds per hour.
lm = logarithmic mean.
S = average cross-sectional area of cooling tower for air flow, square feet.
t = water-main body temperature, Fahrenheit degrees.
t_{wb} = wet-bulb temperature, Fahrenheit degrees.
V = tower volume, cubic feet.

Note: Subscripts 1 and 2 when used in equations refer to water entrance and exit sections respectively, for the counter-flow tower.

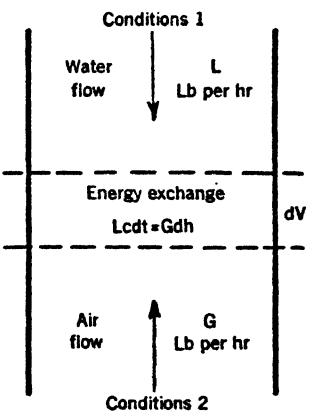

FIG. 4. SECTION OF TYPICAL COUNTER-FLOW TOWER

A section of a typical counter-flow tower is shown in Fig. 4. If the reduction in water rate due to evaporation within the volume is neglected, the energy balance for this differential section of the exchanger volume may be written as:

$$L\,c\,dt = G\,dh \tag{2}$$

The potential for net energy transfer due to heat and mass transfer from the water to the mixture in contact with it may be expressed with reasonable accuracy as the difference between the enthalpy of saturated air at the water temperature, h'', and the enthalpy of the main stream air vapor mixture[7], h_a. The rate of energy transfer is given by the expression:

$$Ka\,(h'' - h_a)\,dV \tag{3}$$

which equation defines the over-all rate coefficient, Ka; the latter being the product of the over-all energy unit conductance, K, and the ratio of the transfer surface to the exchanger volume, a.

Equations 2 and 3 are conveniently illustrated by means of the temperature-enthalpy diagram of Fig. 5. Equation 2 indicates that the

succession of air and water states existing in the exchanger sections must combine to form a straight line (for L = constant) on the temperature enthalpy diagram. The slope of this operating line is:

$$\frac{dh}{dt} = \frac{Lc}{G}$$

Since the heat capacity of water is approximately unity, this slope is the ratio of the water to the air rate. Equation 3 indicates that the potential for energy transfer at any section is the difference between the enthalpy of saturated air at the main-body water temperature at that section and the enthalpy of the air stream in contact with that water. This potential is the difference in the ordinates of the saturation and operating lines for the water temperature at the plane in the tower which is under consideration.

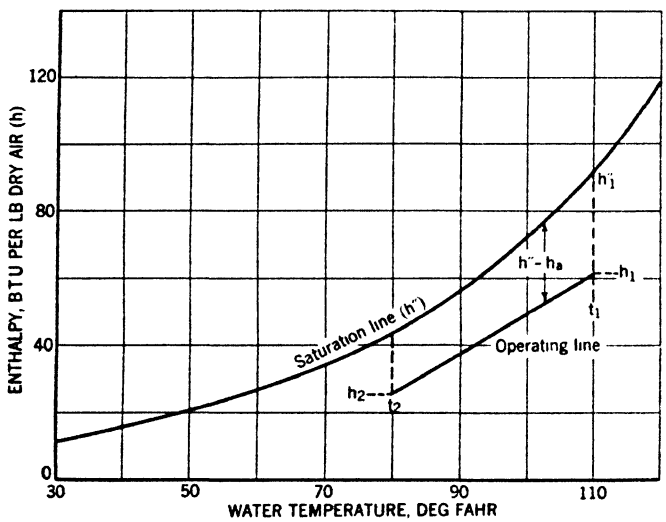

FIG. 5. TEMPERATURE ENTHALPY DIAGRAM FOR AIR WATER VAPOR MIXTURE SHOWING THE OPERATING LINE FOR EXAMPLE 1

Combination of Equations 2 and 3 results in the expression:

$$G\,dh = Ka\,(h'' - h_a)\,dV \tag{4}$$

Integrating this equation over the length of the exchanger:

$$\int_2^1 \frac{G}{Ka}\,\frac{dh}{h'' - h_a} = V \tag{5}$$

The integration of the left side of Equation 5 determines the tower volume required to achieve the desired energy exchange. This summation is readily accomplished for counter and parallel flow arrangements. G and Ka are usually independent of the tower volume and Equation 5 then becomes:

$$NTU = \int_2^1 \frac{dh}{h'' - h_a} = \frac{KaV}{G} \tag{6}$$

Where NTU is defined as the *Number of Transfer Units* and is a measure of the difficulty of the cooling process.

The integration is made numerically or graphically. In the graphical integration $\frac{1}{h'' - h_a}$ is evaluated as a function of h_a. This determination involves the use of the energy balance equation integrated from one section to the section in question. The area under the curve between any two abscissae is the number of transfer units required to change the air state from h_2 to h_1.

An approximate value for the number of transfer units can also be determined by a simple graphical method of direct construction on the temperature enthalpy diagram[8]. This method cannot be applied very satisfactorily to cooling towers as the operating range is small and the value of the NTU is near unity.

When the relationship between the enthalpy of the saturated air and the temperature is linear over the range of water temperatures involved, it can be shown[9] that the logarithmic mean of the terminal potentials, h_{lm}, is the correct driving force. This is true to a good approximation when the water cooling does not exceed 15 deg. The approximation to linearity may be determined by inspection of Table 1, Chapter 3, or the temperature enthalpy diagram of Fig. 5. If the logarithmic mean is a valid potential, Equation 6 may be written:

$$\frac{h_1 - h_2}{\Delta h_{lm}} = \frac{KaV}{G} \tag{7}$$

and the need for the numerical integration for the determination of the tower volume is eliminated.

The over-all rate coefficient, Ka, must be known if the tower volume is to be determined. Experiments conducted on towers containing different packing construction have yielded some magnitudes of this coefficient, evaluated on an over-all basis. These data are presented in Fig. 6 as a function of the gas mass velocity through the packing, and apply only to the particular packing structure for which they were obtained. The over-all rate coefficient (Ka) may also be a function of the water rate, since a reduction of the water rate may reduce the wetted area within the exchanger[5]. The results included in Fig. 6 probably represent magnitudes of Ka which were obtained for complete wetting. Within the cooling tower operating range the over-all rate coefficient for energy transfer is nearly the same numerically as the over-all rate coefficient for mass transfer. The conditions of test corresponding to the data presented in Fig. 6 are not well enough known in most cases to warrant recomputation of Ka. Therefore the magnitudes of the over-all rate coefficient for mass transfer presented in Fig. 6 may be used directly in Equations 5 and 6, the units of Ka in these equations being Btu per (hour) (cubic foot per pound of dry air).

Application of Design Procedure

A typical procedure which may be followed in designing a cooling tower is illustrated in the following Example 1.

Example 1. The rate of air flow, arbitrarily assumed in the data given, is related to the tower volume by economic considerations. A balance between air rate and tower volume rests on consideration of the costs of producing air flow and of the tower construction[10]. A counter-flow forced draft cooling tower is to cool 36,000 lb of water per hour from an initial temperature of 110 F to a final temperature of 80 F. Air having an initial condition of 65 F dry-bulb and 58 F wet-bulb temperature will be forced

through the tower counter to the direction of water flow at the rate of 30,000 lb of dry air per hour.

The cross-section of the tower is to be 8 ft x 8 ft and the packing is to be of the type producing a rate coefficient as indicated in curve No. 2 of Fig. 6. For this type of packing the average cross-sectional area for air flow will be 36 sq ft.

Solution:

Initial air enthalpy = 25.1 Btu per pound of dry air.

Final air enthalpy:

$$(h_1 - h_2) = \frac{Lc}{G}(t_1 - t_2)$$

$$(h_1 - 25.1) = \frac{36{,}000 \times 1}{30{,}000}(110 - 80)$$

$$h_1 = 61.1 \text{ Btu per pound dry air.}$$

A numerical integration (Table 4) is employed to determine the Number of Transfer Units (NTU) required. Temperature increments of 2 F are used between successive determinations of the quantity $\frac{1}{h'' - h_a}$. The energy balance indicates that the enthalpy increments corresponding to these temperature increments are:

$$\Delta h = \frac{Lc}{G}\Delta t = \frac{36{,}000}{30{,}000} \times 2 = 2.4 \text{ Btu per pound of dry air.}$$

The result of the integration is that the Number of Transfer Units required (NTU) = 1.72.

Unit gas mass velocity, $\frac{G}{S} = \frac{30{,}000}{36} = 830$ lb per (hour) (square foot average cross-sectional air flow area).

From Curve 2, Fig. 6, Ka = 138 Btu.

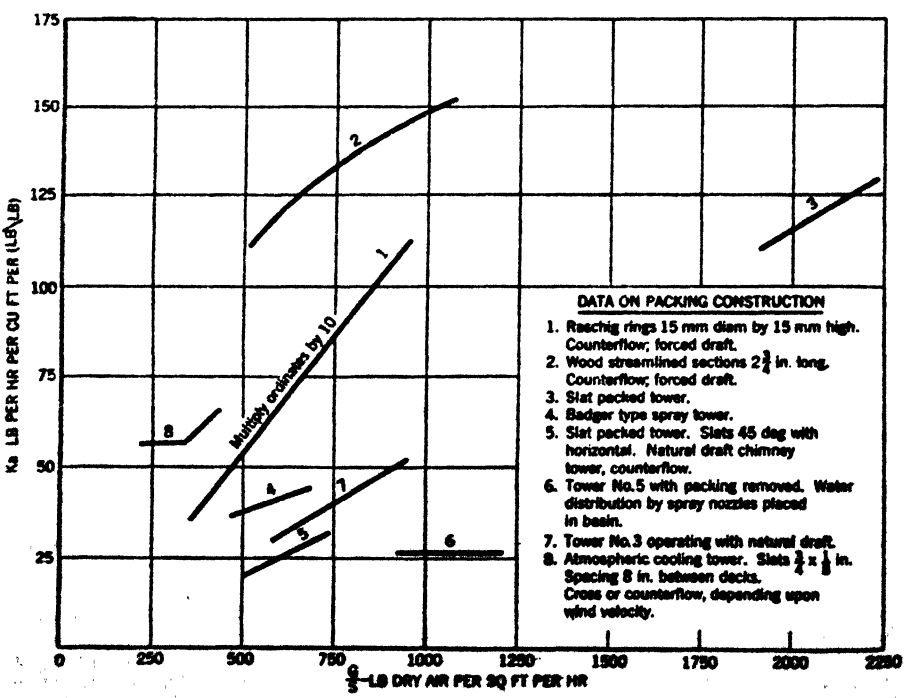

FIG. 6. UNIT CONDUCTANCES FOR VARIOUS TYPES OF PACKING CONSTRUCTION

The tower volume required is:

$$V = \frac{G}{Ka}(NTU) = \frac{30{,}000}{138} \times 1.72 = 217 \times 1.72 = 374 \text{ cu ft.}$$

Height of the packed section is:

$$\frac{374}{8 \times 8} = 5.9 \text{ ft.}$$

The graphical solution for the Number of Transfer Units required for the desired performance is plotted in Fig. 7. $\frac{1}{h'' - h_a}$ is plotted as a function of h, and the area under the curve from the initial enthalpy of the air, 25.1 Btu per pound, to the final enthalpy of the air, 61.1 Btu per pound is 1.72, the Number of Transfer Units required. The effect of the rapid decrease in potential due to the cooling of the water is indicated by comparison of area A_1, A_2, and A_3 of Fig. 7. Each represents the Number of Transfer Units required to achieve a water temperature reduction of about 10 F.

$$A_1 = 0.471\ NTU \text{ (110 to 100 F)}$$
$$A_2 = 0.595\ NTU \text{ (100 to 90 F)}$$
$$A_3 = 0.657\ NTU \text{ (90 to 80 F)}$$

The use of the logarithmic mean driving potential is illustrated by applying Equation 7 to Example 1:

$$NTU = \frac{(Ka)}{G}\frac{V}{} = \frac{h_1 - h_2}{\Delta h_{lm}}$$

$$\Delta h_{lm} = \frac{(h_1'' - h_1) - (h_2'' - h_2)}{\log_e \dfrac{h_1'' - h_1}{h_2'' - h_2}} = \frac{30.7 - 18.4}{\log_e \dfrac{30.7}{18.4}} = 24$$

$$NTU = \frac{61.1 - 25.1}{24} = 1.5$$

The Number of Transfer Units required as determined by use of the logarithmic mean driving potential equals 1.5 which compares favorably with the correct magnitude, 1.72.

TABLE 4. NUMERICAL INTEGRATION FOR THE NUMBER OF TRANSFER UNITS

Water Temperature Interval F Deg	Mean Water Temperature F Deg	Mean Air Enthalpy, h_a Btu per Lb Dry Air	Saturated Air Enthalpy, h'' Btu per Lb Dry Air	Enthalpy Potential $h'' - h_a$	$\frac{\Delta h}{h'' - h_a}$
80–82	81	26.3	44.6	18.3	0.131
82–84	83	28.7	46.9	18.2	0.132
84–86	85	31.1	49.2	18.1	0.133
86–88	87	33.5	51.7	18.2	0.132
88–90	89	35.9	54.4	18.5	0.130
90–92	91	38.3	57.1	18.8	0.128
92–94	93	40.7	60.0	19.3	0.124
94–96	95	43.1	63.0	19.9	0.121
96–98	97	45.5	66.2	20.7	0.116
98–100	99	47.9	69.6	21.7	0.111
100–102	101	50.3	73.2	22.9	0.105
102–104	103	52.7	77.0	24.3	0.099
104–106	105	55.1	80.9	25.8	0.093
106–108	107	57.5	85.1	27.6	0.087
108–110	109	59.9	89.5	29.6	0.081
					1.723

A variation of the design method according to Equation 6 is further possible [11] through the introduction of Equation 2 to yield

$$\int_{t_2}^{t_1} \frac{c\,dt}{h'' - h_a} = \frac{K a V}{L} \tag{8}$$

The advantage of this form is in the fact that the left side of the equation may be dealt with as a thermodynamic function only, while the right side depends upon the tower construction and operation. A series of performance curves may be determined from a graphic evaluation of the integral, which will serve either as a convenient means of analyzing experimental data to determine the conductance Ka, or as a rapid method of performance prediction, once the tower characteristic, $\frac{KaV}{L}$, is known. These performance curves may be expressed in terms of the following variables; approach to wet-bulb, cooling range, L/G, and wet-bulb

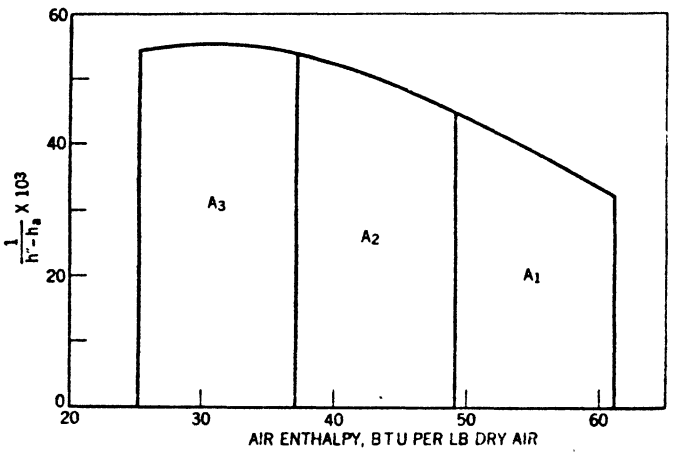

FIG. 7. GRAPHICAL INTEGRATION TO DETERMINE NUMBER OF TRANSFER UNITS REQUIRED FOR DESIRED OPERATING CONDITIONS OF EXAMPLE 1

temperature of the entering air; and as such they will serve to accurately cover the tower performance in consistent terms.

The application of the foregoing design method to atmospheric towers is difficult because rate coefficients and flow conditions are not yet well defined for such equipment. If these are known, application of Equation 7 to sections of the tower small enough to justify use of the logarithmic mean potential will yield the tower volume required for each section. The sections must be taken perpendicular to the path of water flow. A correction to adjust the logarithmic mean potential, evaluated as for counter-flow, to the reduced effectiveness of cross-flow, has been derived for heat transfer and may be applied to this case [12].

For small size counterflow spray towers intended for a low cooling range only considerable data [13, 14] are available on the performance of the spray system in terms of the logarithmic mean enthalpy potential. These data show the importance of proper nozzle arrangement and spray distribution within the tower. The greatest cooling effect is shown to be obtained in a region close to the nozzles; and the beneficial effects of

packing added in the lower section of the tower follow as increasing the cooling range.

Atmospheric towers operate with natural draft, produced in a vertical direction by the stack action of the tower structure, at zero velocity of the approach wind. Approach wind of sufficient magnitude (the magnitude depending on the baffle arrangement which is designed to reduce drift) will cause cross-flow augmenting the natural draft. An adequate design requires the consideration of both flow conditions.

Expression for Cooling Tower Performance

The performance of a cooling tower is described in terms of its effectiveness as an energy exchanger. The effectiveness is defined as the ratio of the energy actually exchanged to the energy available for exchange.

Effectiveness expressions:

Case 1. The slope of the operating line on the $t - h$ diagram exceeds the slope of the saturation line in the region of water temperatures considered.

$$e = \frac{h_1 - h_2}{h_1'' - h_2} \tag{9}$$

Case 2. The slope of the saturation line exceeds that of the operating line.

$$e = \frac{h_1 - h_2}{\frac{Lc}{G}(t_1 - t_{wb})} = \frac{t_1 - t_2}{t_1 - t_{wb}} \tag{10}$$

This equation represents the *approach to wet-bulb.*

Usual tower operating conditions conform to *Case 1.* Because of the curvature of the saturation line, operating conditions may present themselves to which neither *Case 1* nor *2* applies. Since a simple expression for the intermediate case is not available, the expression of *Case 1* may be utilized for the small number of operating conditions falling into the intermediate classification.

Make-Up Water

Since evaporation of water occurs in atmospheric water cooling equipment such evaporation loss must be replaced. Approximately 1 gal of water is lost for every 1000 gal of water cooled per degree of cooling range. There is also an additional amount of spill-over and drift water which must also be replaced. Replacement supply is usually regulated by a float control valve. Chemical treatment of the make-up water is very desirable to avoid excessive deposits in the condensers. Refer to Chapter 51.

Winter Freezing

It is obvious when atmospheric water cooling equipment is operated in freezing weather that the water may freeze. Such freezing may lower the efficiency of the operation. To obviate this freezing an attempt is made, in the case of the spray pond and spray cooling tower, to reduce the quantity of water fed to the apparatus. This reduces the pressure at the nozzles and thereby increases the size of the drops produced. Care must be exercised not to lower the quantity of water too much. On the deck tower the upper system may be shut off and a secondary distribution system put in service midway down the height of the tower. This gives the water less time contact with the air and thus keeps it above freezing. A mechanical draft tower can be protected by reducing the air

flow through the tower. Where intermittent operation of a system is employed, water in outside basins may cause considerable damage due to freezing. To prevent this, such basins are drained when out of service and on some small roof installations a tank large enough to hold all the water in the system may be installed inside the building. In such cases the pump should be protected from the freezing weather.

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Chapter 38

DEHUMIDIFICATION BY SORBENT MATERIALS

Definitions and Principles, Adsorbents, Dehumidification by Solid Adsorbents, Dehumidification Equipment Using Solid Adsorbents, Absorbents, Dehumidification by Liquid Absorbents, Dehumidification Equipment Using Liquid Absorbents, Calculation of Moisture Load, Vapor Barriers

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DEHUMIDIFICATION as used herein is the reduction of the water vapor content of a given volume of air or other gas. The term thus describes a special case of dehydration which covers the removal of moisture in any form from matter. The degree of dehumidification required varies greatly with different applications and is one of the prime considerations influencing the choice of a method. Dehumidification may be accomplished by latent heat removal together with sensible heat removal, as described in Chapters 7, 37, and 43, or by the use of sorbents.

Sorbents are substances which have the property of extracting and holding other substances (usually gases or vapors, *e.g.* water vapor,) brought into contact with them. All materials are sorbents to a greater or lesser degree. The weight of water held by a substance will increase or decrease depending upon whether the vapor pressure of the water held by the substance is less or greater respectively than the partial pressure of water vapor in the surrounding atmosphere. As generally used, however, the term, sorbents, refers to those materials having a capacity for moisture which is large compared to their volume and weight. Such materials are divided into two general classifications:

1. *Adsorbent*—A sorbent which does not change physically or chemically during the sorption process. Certain solid materials, such as activated alumina, silica gel, activated bauxites, and activated charcoal have this property. The action of adsorbents, most of which adsorb some gases and condensible vapors besides water vapor, is selective. Thus, in the case of a mixture containing both water and organic vapors, silica gel would remove the water vapor in preference to the organic vapors, while the reverse would be true in the case of activated carbon. The selective property of adsorbents is made use of in some instances for the removal of objectionable and contaminating vapors from an air or gas mixture. (See Chapter 10.)

2. *Absorbent*—A sorbent which changes either physically, chemically, or both, during the sorption process. Calcium chloride is an example of a solid absorbent, while liquid absorbents include solutions of lithium chloride, calcium chloride, lithium bromide, and the ethylene glycols.

ADSORBENTS

The ability of an adsorbent to remove water vapor from a gas is explained by the fact that the vapor pressure of the water in the adsorbent (when in the reactivated condition) is less than the partial pressure of the water vapor in the surrounding atmosphere. For instance, when an active adsorbent is brought into contact with a gas of high humidity, there is a tendency for the vapor pressure of the water in the adsorbent to reach equilibrium with the partial pressure of the water in the surrounding gas, with the result that water is extracted by the adsorbent and its weight increased, while the moisture content of the gas is correspondingly reduced. (The adsorbent is said to be saturated for a given condition when equilibrium is attained.) The weight of water a given adsorbent will extract is dependent upon the relative humidity (ratio of the partial pressure in the gas to the saturation pressure at a given temperature) and the temperature of the adsorbent. The process is

reversible: if the temperature of the adsorbent is raised until the vapor pressure of the adsorbed water becomes greater than the partial pressure of the vapor in the surrounding atmosphere, water will be released by the adsorbent. After the adsorbent cools to room temperature, for instance, the vapor pressure of the water in the adsorbent falls below the partial pressure of the vapor in the atmosphere, and the adsorbent will again start extracting water. The elimination of water by the addition of heat is known as reactivation and is a means of regenerating the adsorbent so that it may be used repeatedly.

Adsorption is proportional to the amount of surface (internal and external) of the sorbent. The materials that are used commercially as solid adsorbents have a porous structure of sub-microscopic dimensions, which gives them extensive surface area. An adsorbent should meet the following requirements in order to be satisfactory for dehumidification purposes:

1. Have a high adsorptive capacity under normal atmospheric conditions.
2. Be chemically stable, resisting contamination from impurities.
3. Be physically rugged to resist breakdown from handling and use.
4. Be capable of reactivation at temperatures generally obtainable.
5. Be heat-stable at reactivation temperatures.
6. Have a weight per unit volume such as to avoid excessive bed dimensions.
7. Be available at reasonable cost.

Activated Alumina

Activated alumina is a granular porous material which removes by adsorption substantially 100 per cent of the moisture from gases, vapors, and certain liquids. Regeneration or reactivation may be accomplished by employing a heating medium at temperatures ranging from 350 to 600 F. After many cycles of adsorption and reactivation it is substantially as effective as originally and retains its original size and shape.

Activated alumina is produced by chemically controlled precipitation from a sodium aluminate solution resulting from the extraction of alumina from bauxite by the Bayer process. By subsequent processes this precipitate is converted into a highly porous adsorptive material. It is low in iron and silica, each normally less than 1/10 of 1 per cent. Commercially produced material is uniform in analysis and physical form.

Activated alumina is a partially dehydrated aluminum trihydrate containing about 7 per cent water and small amounts of soda, oxides of iron, silicon, and titanium, as well as very minor amounts of other elements indicated spectrographically. Substantially all of the soda is combined with silica and alumina as an insoluble constituent.

Activated alumina is inert chemically to most gases and vapors, is non-toxic, and will not soften, swell or disintegrate when immersed in water. High resistance to shock and abrasion are two of its more important physical characteristics. Commercial sizes range from a powder passing through 300 mesh screen to particles 1 in. in diameter. The sizes commonly used are 8-14 mesh and ¼ in. to 8 mesh. The average weight for most forms is 50 lb per cubic foot. Its high degree of purity warrants classification among commercially pure chemicals.

Silica Gel

Silica gel is a prepared form of silicon dioxide (silica) having an extremely porous structure which makes it an efficient adsorbent. It is

made by mixing predetermined concentrations of an acid, such as sulfuric acid, and a soluble silicate, usually sodium silicate, and allowing the mixture to set to a jelly-like mass called hydrogel. The product takes its name from its condition as a colloid at this stage of its manufacture. After setting, the hydrogel is broken into small lumps, washed, dried, crushed, and screened to the desired particle sizes and then given a final heat treatment or activation. The surface area of silica gel has been found to be in excess of 50,000 sq ft per cubic inch of product. Silica gel has high adsorptive capacity per unit weight and may be reactivated repeatedly at temperatures up to 600 F. Reactivation is generally accomplished by blowing gases through the silica gel at approximately 300 F, or by heating in a well-vented oven maintained at this temperature until no more moisture is given off. Silica gel is a high purity, rugged, non-toxic, heat-stable material, having a specific heat of 0.2 and is most inert. There is no change in the size or shape of the particles as it becomes saturated and no corrosive or injurious compounds are given off. It is available commercially in a number of grades, ranging in particle size from a 3 to 8 mesh product to an impalpable powder passing through a 325 mesh screen. The product generally used for dehumidification applications has a particle size of 6 to 12 mesh and a bulk density of between 40 and 45 lb per cubic foot.

Activated Bauxite

Activated bauxites are certain natural products which after controlled heat treatment have properties which make them suitable for use as solid adsorbents. They are marketed under different trade names by several processors. The activated bauxites consist primarily of Al_2O_3, Fe_2O_3, SiO_2, TiO_2, and H_2O in varying percentages. The surface area, adsorptive capacity, and other properties of the several products differ to some extent depending upon the source of the original material and its subsequent treatment. The available activated bauxites are durable products having a specific heat of about 0.24 and can be regenerated at temperatures between 300 F and 500 F. They are usually supplied in a number of particle sizes and have a bulk density of between 55 and 65 lb per cubic foot.

There are other solid substances having marked adsorbent properties, but details concerning them are not available.

DEHUMIDIFICATION BY SOLID ADSORBENTS

Since adsorption is primarily a condensation process, heat equivalent to the latent heat of evaporation of the vapor plus the heat of wetting, which is an additional amount of heat depending upon the vapor being adsorbed and the adsorbent used, is liberated. The sum of the latent heat of evaporation and the heat of wetting is known as the heat of adsorption. During adsorption it might be said that latent heat is transformed into sensible heat, which is dissipated into the adsorbent, into the metal of the adsorbent container, and into the gas mixture, resulting in a rise in temperature. Fig. 1 shows the relationship between temperature, vapor pressure, and moisture content of a solid adsorbent. These curves indicate the general performance of solid adsorbents, although the exact values vary for the different adsorbents and may vary even for different types of the same compound. The effects of vapor pressure and temperature upon the moisture content of an adsorbent

may be observed by referring to Fig. 1. When the given type of solid adsorbent is in equilibrium with air having a dry-bulb temperature of 70 F and 70 per cent relative humidity, that is, having a dew-point of 60 F or a water vapor pressure of 13.2 mm Hg, the water content of the adsorbent is 33 per cent. With air having the same dry-bulb temperature and a dew-point of 37 F, or a vapor pressure of 5.6 mm Hg, the water content is 20 per cent. The increase in weight for an activated solid adsorbent after it reaches equilibrium with a gas of any given water vapor content may be found by subtracting the residual water content (for example 6 per cent) from the equilibrium value. In the case of the two examples cited, the actual water gain would be 27 per cent and 14 per cent respectively. The effect of temperature upon the adsorptive

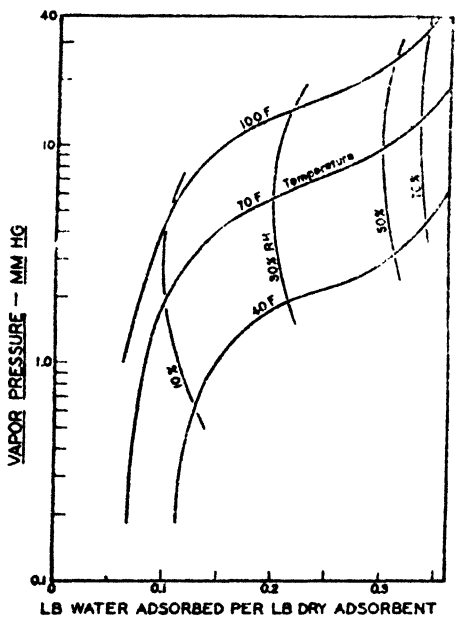

FIG. 1. TEMPERATURE—VAPOR PRESSURE —CONCENTRATION CHARACTERISTICS FOR A TYPICAL SOLID ADSORBENT

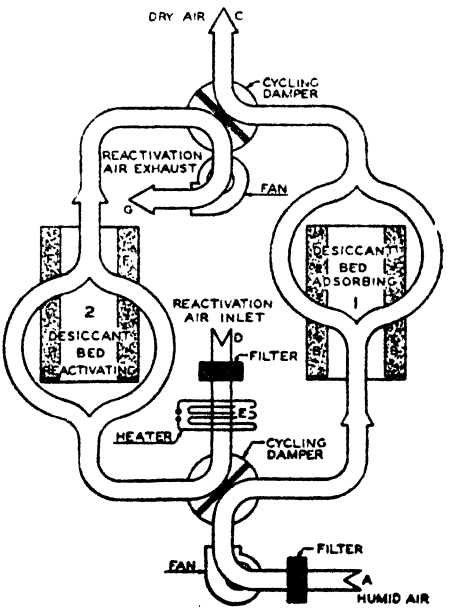

FIG. 2. A TYPICAL SOLID ADSORBENT DEHUMIDIFICATION UNIT AIR FLOW DIAGRAM

capacity may be observed by following the 5.6 mm Hg vapor pressure line. At a temperature of 70 F the moisture content of the adsorbent is 20 per cent, while at 100 F the equilibrium water content is 11 per cent.

In practice the temperature rise in the dehumidified air caused by the adsorption heat is approximately 10 deg F for each grain of moisture removed per cubic foot of air at atmospheric pressure. This temperature rise occurs progressively through the adsorbent bed and is an important consideration in predetermining the performance of a given design of apparatus. Data such as these, together with information covering other characteristics such as specific heat, resistance to air flow, etc., are of value in the basic design of adsorption apparatus. In the solution of air conditioning problems, however, reference must be made to performance data on established apparatus designs.

DEHUMIDIFICATION EQUIPMENT USING SOLID ADSORBENTS

A typical solid adsorbent dehumidification unit air flow diagram is shown in Fig. 2. The apparatus consists of two adsorbent containers (adsorbers) with necessary interconnecting piping, valves, and auxiliaries consisting of filters, fans, activation air heater, controls, and in some instances a cooler for the dehumidified air. Before entering the adsorber the air to be dehumidified is drawn into a filter to remove dust and other impurities. In passing through the adsorbent bed, the moisture content of the air is reduced and the dehumidified air is then introduced into the space or process requiring it. While the first adsorber is dehumidifying the air, the second adsorber is being reactivated by means of outside air drawn through a filter and heater in which its temperature is raised to 300 F. The heat may be supplied by electric heating elements, steam coils, the direct products of combustion of gas, oil, waste heat, or any other convenient source. In passing through the adsorbent bed, the hot gases supply the necessary heat for releasing adsorbed water from the adsorbent and then carry it out of the adsorber to the activation gas outlet, where it is exhausted to the outside atmosphere. In some instances a thermostat placed in the activation outlet connection shuts off the activation fan and heater when the adsorbent is completely reactivated, as indicated by a rapid rise in the temperature of the outlet activation gas. The length of the adsorption period may be controlled by a timing device which changes the valves or dampers from the adsorbing to the activating position, or by a humidistat located in the dehumidified air connection or in the dehumidified space. The majority of commercial units are time controlled.

In applications where a continuous stream of dehumidified air is not required, a single adsorber type unit may be used, while in other cases where a continuous stream of dehumidified air is required, a multiple number of adsorbers or even a continuously rotating system may be used.

If the air to be dehumidified is very warm, and especially where exceedingly low dew-point dehumidified air is required, it is advantageous to install a pre-cooler to reduce the temperature of the inlet air. In this way the working temperature in the adsorber is lowered and the over-all performance appreciably increased. Some equipment manufacturers install cooling coils in the adsorbent beds for the same purpose, while others divide the adsorbent bed and install coolers between the sections.

Dehumidification equipment is employed to the best advantage where the air conditioning problem is primarily one of obtaining low relative humidity control rather than temperature control. This requirement is found in the case of the preservation of inactive naval vessels where the interior of the ship must be kept at a relative humidity below 30 per cent to avoid corrosion, mold, mildew, and other moisture damage that occurs at humidities substantially in excess of this figure. Other advantageous applications for dehumidification systems are found in industrial processes where low relative humidity atmospheres are required during the manufacture as well as for preservation of the finished products. Dehumidification with cooling may be used to advantage in work-rooms or other spaces occupied by humans, where the moisture load is high in comparison to the sensible heat load. In many instances where independent control of temperature and humidity is important dehumidification is used to advantage in conjunction with cooling.

ABSORBENTS

Any absorbent substance may be used as a dehumidifying agent if it has a vapor pressure with respect to water lower than the partial pressure of the water vapor in the mixture from which the moisture is to be removed.

Solid Absorbents. The substances used are generally the solid forms of the liquid absorbents. Calcium chloride is frequently used because of low cost. At present they are used principally in small desiccating chambers and in small dryers of the cartridge type, through which air is forced under pressure.

Liquid Absorbents. These are primarily water solutions of materials in which the vapor pressure is reduced to a suitable level by controlling the concentration and temperature of the dehumidifying solution. Water solutions of the chlorides or bromides of various inorganic elements and certain organic compounds are the liquid absorbents used in air conditioning.

In addition to having suitable water vapor pressure characteristics, an absorbent to be satisfactory should also meet the following requirements:

1. Be widely available at low cost.
2. Be non-corrosive, odorless, non-toxic, and non-inflammable.
3. Be chemically inert against any impurities in the air stream.
4. Be stable over the range of use.
5. Must not precipitate at the lowest temperature to which the apparatus is exposed.
6. Have low viscosity and be capable of being economically regenerated or concentrated after having been diluted by the moisture absorbed.

DEHUMIDIFICATION BY LIQUID ABSORBENTS

In liquid absorption systems the air-vapor stream is brought into intimate contact with the absorbent solution by passing the air stream through a tower into which the brine is introduced as a finely divided spray, or by passing the air through a tower or contactor which is continuously sprayed with the brine, thereby presenting a large surface of absorbent to the air to be dehumidified. The difference in the partial pressure of the water in the concentrated brine and the partial pressure of the water vapor in the air causes the water vapor to be given up by the air to the brine until equilibrium is approached. The water vapor is condensed during this operation, and its addition to the absorbent solution results in a decrease in the concentration of the solution. As the water vapor condenses the latent heat of condensation is released in the absorbent solution. An additional, frequently appreciable, quantity of heat known as the heat of solution or heat of mixing is also released. The heat released as the result of condensation and mixing is directly transferred to the brine, to the equipment, and to the air being dehumidified, thereby causing a rise in temperature.

A modified system includes means for removing heat from the absorbent solution, either within the contactor or externally. Thus the temperature of the solution may be higher than, equal to, or lower than that of the air, depending on the chemical employed and the ultimate use of the dehumidified air.

Fig. 3 shows the relationship between temperature, vapor pressure and moisture content of a typical absorbent of the *inorganic* type. These curves indicate the general performance of such absorbents, although the exact values vary for the different compounds.

When the given absorbent is in equilibrium with air having a dry-bulb temperature of 70 F and a relative humidity of 70 per cent, *i.e.* having a dew-point of 60 F, or a water vapor pressure of 13.2 mm Hg, the water

content of the solution is 4.8 lb water per pound of anhydrous absorbent. With air having the same dry-bulb temperature and a dew-point of 37 F, or a vapor pressure of 5.6 mm Hg, the water content is 2.1 lb per pound of absorbent. Therefore, when a solution of 2.1 lb water per pound of absorbent is exposed to an atmosphere of 70 F and 70 per cent relative humidity, it will absorb an additional 2.7 lb of water in reaching equilibrium.

The effect of temperature on the absorptive capacity may be observed by following a constant vapor pressure line in Fig. 3. At a temperature of 70 F and a vapor pressure of 13.2 mm Hg the moisture content is 4.8 lb

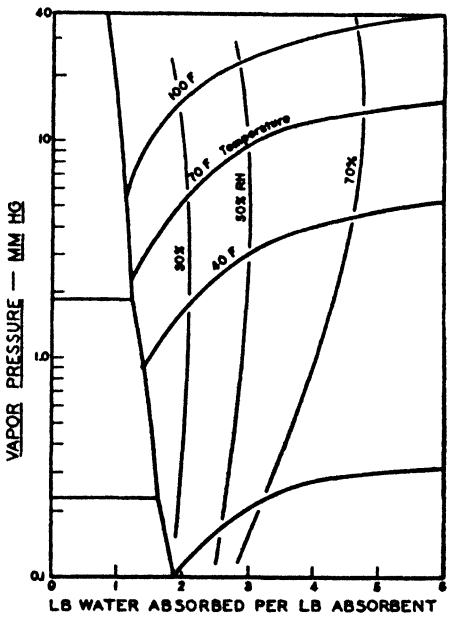

FIG. 3. TEMPERATURE—VAPOR PRESSURE —CONCENTRATION CHARACTERISTICS FOR A TYPICAL INORGANIC ABSORBENT (HALOGEN SALT GROUP)

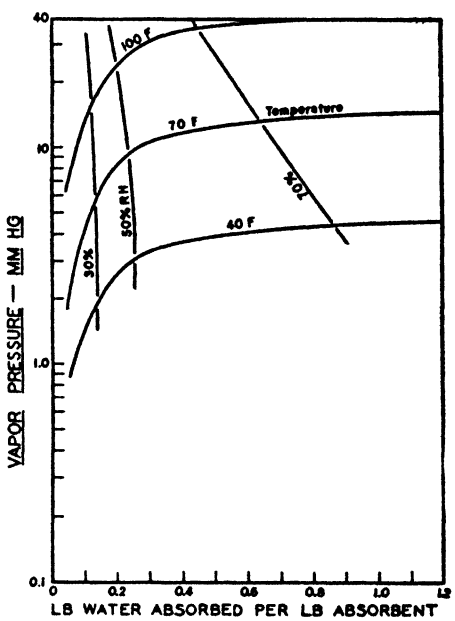

FIG. 4. TEMPERATURE—VAPOR PRESSURE —CONCENTRATION CHARACTERISTICS FOR A TYPICAL ORGANIC LIQUID ABSORBENT

water per pound of absorbent. At 100 F the moisture content is 1.8 lb water per pound of absorbent.

Fig. 4 shows the relationship between temperature, vapor pressure, and moisture content of a typical liquid absorbent of the *organic* type.

DEHUMIDIFICATION EQUIPMENT USING LIQUID ABSORBENTS

One type of system utilizing liquid absorbents includes an external interchanger having essential parts consisting of a liquid contactor, a solution concentrator, a solution heater and a cooling coil all as shown in Fig. 5. The contactor and cooling coil are located in the wet air stream. The air to be conditioned is brought into contact with an aqueous brine solution having a vapor pressure below that of the entering air, resulting in a transfer of moisture from the air to the brine solution. This results in a conversion of latent heat to sensible heat which raises the solution temperature and consequently the air temperature. The temperature

change of the air being processed is determined by the cooling water temperature and the amount of moisture removed in the equipment. Control of leaving air temperature may be obtained by precooling the absorbent solution in a suitable surface cooler, by tap, well, or chilled water.

The excess water of condensation, which dilutes the brine, is removed in the solution concentrator. This is a low pressure steam heat exchanger which over-concentrates a portion of the weak liquor and returns it to the main brine reservoir for re-cycling. The concentrator operates in the manner of an evaporative condenser, whereby moisture is evaporated from the brine by the heating coils into a stream of regeneration air taken from and rejected to the outside atmosphere. Low pressure steam is normally used for heating the brine. When it is desirable or necessary to use gas or electricity, an auxiliary low pressure steam boiler is usually

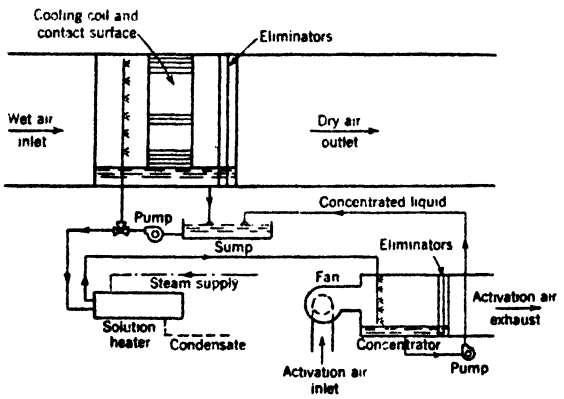

FIG. 5. LIQUID ABSORBENT EQUIPMENT IN WHICH SOLUTION COOLER AND CONTACTOR ARE COMBINED

added to the equipment. Concentrators operating on a simple boiler principle have not as yet been commercially practical.

It should be noted that the solution concentration phase is the reverse of the absorption process. During concentration the aqueous vapor pressure of the solution is greater than that of the surrounding air, while during dehumidification, the reverse is the case. Utilization of this principle permits winter humidification by heating (instead of cooling) the solution pumped to the contactor. Water is thereby evaporated into, instead of being condensed out of, the conditioned air stream. This requires dilution of the brine externally to the contactor, rather than concentration.

CALCULATION OF MOISTURE LOAD

Calculation of the dehumidification required to maintain lower than normal moisture content in a given room begins with determination of the rate of moisture gain in the room from all sources. It is common practice when maintaining a low humidity ratio to recirculate a large percentage of the air in the room through the dehumidifier, and to add only enough outside air to meet the needs of the problem. The humidity ratio of the mixture of outside and recirculated air and the dehumidifier performance data can be used to calculate the humidity ratio of the air leaving the dehumidifier. The difference between the humidity ratio of the air in the room and that of the dehumidified air entering the room

represents the effective dehumidification per pound of air. The rate of internal moisture gain in grains per minute divided by the effective dehumidification in grains per pound of air equals the air quantity required in pounds per minute. The following typical example using arbitrary values shows a general method of determining the dehumidifying requirements. Sensible heat determination considerations are discussed in other chapters and are purposely omitted here.

Example 1. A solid adsorbent dehumidifier having performance characteristics as shown in Fig. 6 is to be used to maintain inside conditions of 73 F and 20 per cent relative humidity, *i.e.* 24.1 grains per pound of dry air, 30 F dew-point, in a room, 20 ft x 30 ft x 10 ft high, having a total wall, ceiling, and floor surface area of 2200 sq ft. Outside design conditions are 72 F dew-point (118.4 grains per pound).

Internal sources of moisture are: 4 occupants; an open natural gas burner using 15 cu ft of natural gas per hour; an open top water tank, having an area of 2 sq ft exposed surface, in which water is maintained at 87 F, with air movement over the water surface being 100 fpm. Determine the quantity and condition of the dehumidified air to be supplied to the room.

Solution. The internal moisture gain consists of items 1 to 5.

		Grains Per Minute
1. From occupants:	$4 \times 1800/60 =$	120
1800 grains per person per hour is obtained from Fig. 7, Chapter 12, by interpolation between curves C and D.		
2. From burned gas:	$15 \times 650/60 =$	162
1 cu ft natural gas produces approximately 650 grains of moisture.		
3. From exposed water surface:	$2 \times 20 =$	40
Evaporation from water surface is assumed to be 20 grains per (minute) (square foot) at 87 F water with air movement of 100 fpm.		
4. From infiltration:	$\frac{6000}{60 \times 13.56} \times (118.4 - 24.1) =$	696
One air change, 6000 cu ft, assumed per hour (see Chapter 8).		
5. Moisture transmitted through room surface:	$\frac{2200}{60} \times 3 \times (0.783 - 0.176) =$	67
Permeability assumed to be 3 grains per (square foot) (hour) (inch Hg vapor pressure difference on two sides of wall).		
Total moisture gain from internal sources		1085

Let q be the air delivered to the room, pounds per minute. Let it be assumed for this problem that 85 per cent of the air is recirculated and 15 per cent is outside air. Enough air must be supplied to replace leakage from the system or to satisfy normal ventilating requirements for the occupants of the room as given in Chapter 12, whichever is greater. The amount is estimated from experience or obtained by test.

The humidity ratio of the mixture of recirculated and outside air entering the dehumidifier is then:

$$\frac{0.85q\ (24.1) + 0.15q\ (118.4)}{0.85q + 0.15q} = 38.3 \text{ grains per pound entering dehumidifier.}$$

For the dehumidifier shown in Fig. 6, for 38.3 grains per pound in entering air, the leaving humidity ratio will be 6.5 grains per pound.

Effective dehumidification in the room is 24.1 — 6.5 or 17.6 grains per pound of supply air.

Then $q = \frac{1085 \text{ grains per minute}}{17.6 \text{ grains per pound}} = 61.6$ lb air per minute ***minimum*** that must be supplied to the room to maintain 30 F dew-point.

Note that this figure represents the minimum requirement for the arbitrary conditions set forth and that in practice safety margins should be added to the outside air percentage figure and to the calculated internal moisture gain.

VAPOR BARRIERS

The walls enclosing a dehumidified space are subjected to a vapor pressure differential. The pressure of the vapor outside the walls tends to force moisture through the walls into the dehumidified zone of relatively low vapor pressure. As this process can be an unnecessary load on the dehumidifying equipment, provisions should be made for keeping the vapor transfer to a minimum. Also, if the space is cooled below the ambient dew-point there is a possibility that condensation may occur within the walls unless vapor transfer is controlled. For these reasons

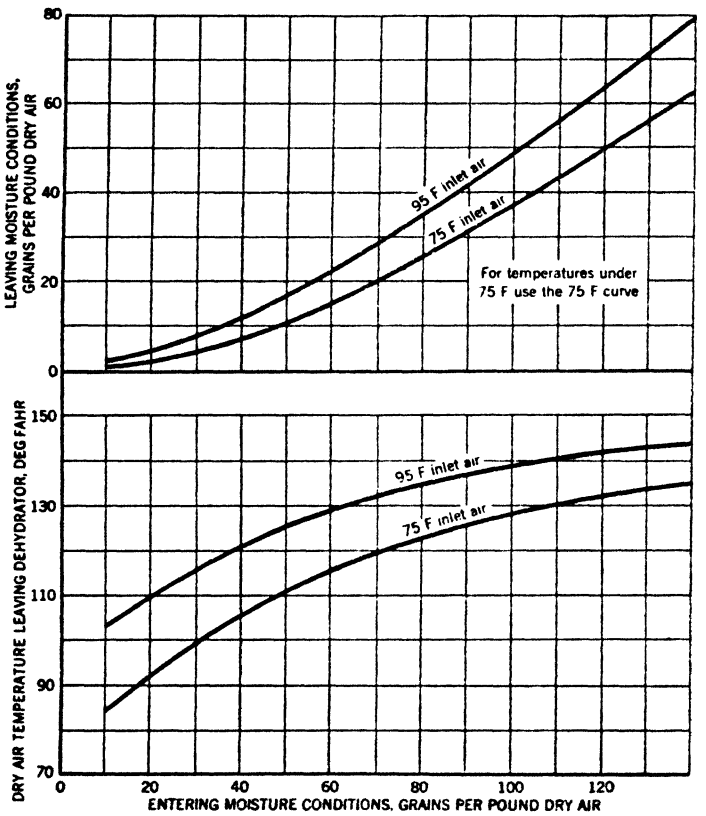

FIG. 6. PERFORMANCE DATA FOR TYPICAL COMMERCIAL SOLID ADSORBENT DEHUMIDIFIER

a vapor barrier should be located within the wall construction as near to the high vapor pressure side as feasible. To be effective a barrier must be continuous and should be so located within the structure that it will be protected from rupture.

Some types of insulation are supplied with the vapor barrier attached. Asphaltic paints, asphalt impregnated and surface coated papers, laminated papers, and combinations of metal foil and kraft papers are among the types of available barriers. Sheet metal linings have been used in rooms where moisture transmission must be eliminated. In existing construction, barriers may be added to the surface of the walls by application of proper paints or the addition of foil or laminated impregnated paper.

When vapor permeability is expressed as grains per (hour) (square foot) (inch of mercury pressure differential) a value not exceeding unity indicates a proper vapor barrier. Moisture vapor transmission rates for various materials are listed in Table 24, Chapter 15.

The formula for the amount of moisture vapor transmitted through a wall is:

$$W = \mu A (P_1 - P_2)$$

where

W = total moisture vapor flow, grains per hour through the wall.
μ = permeability, grains per (hour) (square foot) (unit vapor pressure differential).
A = area of the wall, square feet.
P_1 = vapor pressure on the humid side of the wall, and
P_2 = vapor pressure on the other side of the wall, both in units consistent with the pressure units of the transmission coefficient.

The over-all moisture transfer coefficient for a wall consisting of a combination of several materials in series may be calculated by combining the permeabilities (μ_1, μ_2, μ_3, etc.) of the individual materials according to the formula:

$$\mu = \frac{1}{\frac{1}{\mu_1} + \frac{1}{\mu_2} + \frac{1}{\mu_3} + \ldots \frac{1}{\mu_n}}$$

Example 2. Find the moisture transfer through a wall of 1000 sq ft area if the permeability of the wall is 0.45 grains per (square foot) (hour) (inch Hg) and the air conditions are 85 F dry-bulb with 65 per cent relative humidity outside and 90 F dry-bulb with 20 per cent relative humidity inside.

Solution. The vapor pressures are therefore $0.65 \times 1.21 = 0.787$ in. Hg outside and $0.20 \times 1.42 = 0.284$ in. Hg inside.

The vapor transfer of the wall is therefore $1000 \times 0.45 (0.787 - 0.284) = 226$ grains per hour.

Allowance should be made in design load calculations for imperfections in application of vapor barriers and consequently some judgment is necessary in determining the quality of the workmanship.

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Chapter 39

REFRIGERATION

Theory and Cycle Calculations: Definitions, Simple Refrigeration Cycles, Complex Refrigeration Cycles, Pipe Sizes and Friction Losses, Air Refrigeration Cycle, the Steam Jet System, the Absorption System, Ice Systems, Storage Systems, the Reverse Cycle; Equipment and Arrangements: Types of Compressors, Condensers, Expansion Valves, Evaporators and Coolers, Equipment Selection

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WITH the increasing use of all-year comfort air conditioning installations the importance of refrigeration to the air conditioning engineer has been greatly magnified. The details of equipment operation, maintenance, and design remain problems for the refrigeration engineer, but the air conditioning engineer does retain a responsibility to the customer which requires some knowledge on his part of the different refrigeration cycles and the relative merits of each. In order to assist in meeting this need, the present chapter has been divided into two parts, the first covering the fundamental technical relationships which govern the selection and analysis of an operating cycle and the second presenting brief discussions of some of the equipment and equipment arrangements which are most commonly used.

THEORY AND CYCLE CALCULATIONS

Definitions

The *ton of refrigeration* is a quantity unit which originated in the days when harvested ice was the principal source of summer cooling. By definition the *ton* is the cooling effect realized when one ton of 32 F ice melts to water at 32 F; since the latent heat of fusion of ice is 144 Btu per pound, the *ton* represents a unit cooling effect of 144 × 2,000 = 288,000 Btu. In common practice the ton is usually considered a rate (rather than quantity) unit and is taken as 288,000 Btu per day (24 hours) or 12,000 Btu per hour or 200 Btu per minute. Thus for air conditioning calculations, the size of the requisite refrigeration machine, expressed in tons, can be obtained by dividing the heat gain of the structure, expressed in Btu per hour, by 12,000. In equation form:

$$H_t = (\text{Btu per hour heat gain}) \div 12{,}000 \qquad (1)$$

where

H_t = load in tons.

The *working substance*, or *refrigerant*, is the fluid which carries heat through the refrigeration cycle from the evaporator, where heat enters the refrigerant, to the condenser where the heat is discharged to some cooling medium. The great majority of modern refrigeration systems use a liquefiable vapor as the working substance. By altering the pressure of the refrigerant its boiling temperature is changed, allowing the material to *boil* in the evaporator at a temperature sufficiently lower than that of the conditioned space to insure maintenance of an effective heat transfer rate from the space (or in some cases from a secondary cooling fluid such as brine or cold water) to the refrigerant. The vapor formed in the evaporator is then raised in pressure (by a compressor, or by the absorber-generator combination of the absorption system) until its new

boiling temperature exceeds the temperature of the available cooling medium; under these conditions heat transfer is established from the refrigerant vapor to the cooling medium with resultant condensation of the refrigerant. When condensed, the high-pressure liquid refrigerant is reduced in pressure and again allowed to *boil* in the evaporator.

Thermodynamically, a material for use as a refrigerant should have a large latent heat of vaporization since it is this heat quantity—subject to minor variations—which constitutes the working effectiveness of the refrigerant. Further, since the work required to compress a vapor increases rapidly with the pressure ratio, the thermodynamic characteristics of the fluid should be such that the required low-to-high temperature range can be achieved with only a moderate change in ratio. A further consideration, from the standpoint of practical operating effectiveness, is that the suction pressure should not be below atmospheric (to prevent leakage of air into the refrigerant lines) nor should the condenser pressure be excessively high (to prevent need for extra-heavy construction). The specific volume-specific enthalpy relationship is also important because some materials would have such low density, when in vapor form, that impractical compressor displacements would be needed to handle the suction vapor.

Properties of refrigerants are usually given either in tabular or graphic form. In contrast to the temperature-entropy plotting which is used almost exclusively in steam-power work, refrigeration problems are usually referred to a pressure-enthalpy chart. The advantage of pressure-enthalpy plotting is that linear distances on the chart correspond to energy gains or losses and the two types of processes, constant-pressure and constant-enthalpy, which occur most frequently in refrigeration cycles, can both be represented by straight vertical or horizontal lines. Tabular arrangements of refrigerant properties have the disadvantage common to all point representations, in requiring interpolation between given values, but have the advantage of an accuracy greater than that obtainable from a chart. Tables 1, 2, 3, 4, 5, 6 and 7 give the thermodynamic properties of seven of the more common refrigerants: dichlorodifluoromethane (F-12), monochlorodifluoromethane (F-22), methyl chloride, ammonia, carbon dioxide, monofluorotrichloromethane (F-11), and water; the first five of these materials are commonly used in reciprocating compressors, the last two in centrifugal machines, while water also finds use in steam jet systems.

Referring to Table 1, the first column gives the range of saturation temperatures likely to occur in practice. The second column gives the saturation pressure expressed in pounds per square inch absolute corresponding to a given temperature, while the next six columns give the three fundamental specific properties, volume, enthalpy, and entropy, of the saturated liquid and saturated vapor respectively. The last four columns give values of enthalpy and entropy for gases with 25 deg and with 50 deg of superheat; note particularly that the column heading *50 F superheat* means, not that the gas is at a temperature of 50 F, but that its temperature exceeds by 50 deg the saturation temperature corresponding to its actual pressure. Thus F-12 vapor at 38.0 psig and 91 F possesses 50 deg of superheat since its saturation temperature corresponding to 52.7 psia is 41 F.

The tabular arrangements of refrigerant properties are literally for saturated or superheated materials only. In many cases, however, the engineer must work with sub-cooled liquids. With an accuracy sufficient

Table 1. Properties of Dichlorodifluoromethane (F-12)

Sat. Temp. F	Abs. Press. Lb per Sq In.	Volume		Enthalpy and Entropy Taken From −40 F							
				Enthalpy		Entropy		25 F Superheat		50 F Superheat	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
0	23.87	0.0110	1.637	8.25	78.21	0.01869	0.17091	81.71	0.17829	85.26	0.18547
2	24.89	0.0110	1.574	8.67	78.44	0.01961	0.17075	81.94	0.17812	85.51	0.18529
4	25.96	0.0111	1.514	9.10	78.67	0.02052	0.17060	82.17	0.17795	85.76	0.18511
5	26.51	0.0111	1.485	9.32	78.79	0.02097	0.17052	82.29	0.17786	85.89	0.18502
6	27.05	0.0111	1.457	9.53	78.90	0.02143	0.17045	82.41	0.17778	86.01	0.18494
8	28.18	0.0111	1.403	9.96	79.13	0.02235	0.17030	82.66	0.17763	86.26	0.18477
10	29.35	0.0112	1.351	10.39	79.36	0.02328	0.17015	82.90	0.17747	86.51	0.18460
12	30.56	0.0112	1.301	10.82	79.59	0.02419	0.17001	83.14	0.17733	86.76	0.18444
14	31.80	0.0112	1.253	11.26	79.82	0.02510	0.16987	83.38	0.17720	87.01	0.18429
16	33.08	0.0112	1.207	11.70	80.05	0.02601	0.16974	83.61	0.17706	87.26	0.18413
18	34.40	0.0113	1.163	12.12	80.27	0.02692	0.16961	83.85	0.17693	87.51	0.18397
20	35.75	0.0113	1.121	12.55	80 49	0.02783	0.16949	84.09	0.17679	87.76	0.18382
22	37.15	0.0113	1.081	13.00	80.72	0.02873	0.16938	84.32	0.17666	88.00	0.18369
24	38.58	0.0113	1.043	13.44	80 95	0.02963	0.16926	84.55	0.17652	88.24	0.18355
26	40.07	0.0114	1.007	13.88	81.17	0.03053	0.16913	84.79	0.17639	88.49	0.18342
28	41.59	0.0114	0.973	14.32	81.39	0.03143	0.16900	85.02	0.17625	88.73	0.18328
30	43.16	0.0115	0.939	14.76	81.61	0.03233	0.16887	85.25	0.17612	88.97	0.18315
32	44.77	0.0115	0.908	15.21	81.83	0.03323	0.16876	85.48	0.17600	89.21	0.18303
34	46.42	0.0115	0 877	15.65	82.05	0.03413	0.16865	85.71	0.17589	89.45	0 18291
36	48.13	0.0116	0.848	16 10	82.27	0.03502	0.16854	85.95	0.17577	89.68	0.18280
38	49.88	0.0116	0.819	16.55	82.49	0.03591	0.16843	86.18	0.17566	89.92	0.18268
39	50.78	0.0116	0.806	16.77	82.60	0.03635	0.16838	86.29	0.17560	90.04	0.18262
40	51.68	0.0116	0.792	17.00	82.71	0 03680	0.16833	86.41	0.17554	90.16	0.18256
41	52.70	0.0116	0.779	17.23	82.82	0 03725	0.16828	86.52	0.17549	90.28	0.18251
42	53.51	0.0116	0.767	17.46	82.93	0.03770	0.16823	86.64	0.17544	90.40	0.18245
44	55.40	0.0117	0.742	17.91	83.15	0.03859	0.16813	86 86	0.17534	90.65	0.18235
46	57.35	0.0117	0.718	18.36	83.36	0 03948	0.16803	87.09	0.17525	90.89	0.18224
48	59.35	0.0117	0.695	18.82	83.57	0.04037	0 16794	87.31	0 17515	91.14	0.18214
50	61.39	0.0118	0.673	19.27	83.78	0.04126	0.16785	87.54	0 17505	91.38	0.18203
52	63.49	0.0118	0.652	19 72	83 99	0.04215	0.16776	87.76	0.17496	91.61	0.18193
54	65.63	0.0118	0.632	20.18	84.20	0.04304	0.16767	87.98	0.17486	91.83	0 18184
56	67 84	0.0119	0.612	20.64	84.41	0 04392	0.16758	88.20	0.17477	92.06	0.18174
58	70.10	0.0119	0.593	21.11	84.62	0.04480	0.16749	88.42	0.17467	92.28	0.18165
60	72.41	0.0119	0.575	21.57	84.82	0.04568	0.16741	88.64	0.17458	92.51	0.18155
62	74.77	0.0120	0.557	22.03	85.02	0.04657	0.16733	88.86	0.17450	92.74	0.18147
64	77.20	0.0120	0.540	22.49	85.22	0.04745	0.16725	89.07	0.17442	92.97	0.18139
66	79.67	0.0120	0.524	22.95	85.42	0.04833	0.16717	89.29	0.17433	93.20	0.18130
68	82.24	0.0121	0.508	23.42	85.62	0.04921	0.16709	89.50	0.17425	93.43	0.18122
70	84.82	0.0121	0.493	23.90	85.82	0.05009	0.16701	89.72	0.17417	93.66	0.18114
72	87.50	0.0121	0.479	24.37	86.02	0.05097	0.16693	89.93	0.17409	93.99	0.18106
74	90.20	0.0122	0.464	24.84	86.22	0.05185	0.16685	90 14	0.17402	94.12	0.18098
76	93.00	0.0122	0.451	25.32	86.42	0.05272	0.16677	90 36	0.17394	94.34	0 18091
78	95.85	0.0123	0.438	25.80	86.61	0.05359	0.16669	90.57	0.17387	94.57	0.18083
80	98.76	0.0123	0.425	26.28	86.80	0.05446	0.16662	90.78	0.17379	94.80	0.18075
82	101.70	0.0123	0.413	26.76	86.99	0.05534	0.16655	90.98	0.17372	95.01	0.18068
84	104.8	0.0124	0.401	27.24	87.18	0.05621	0.16648	91.18	0.17365	95.22	0.18061
86	107.9	0.0124	0 389	27.72	87.37	0.05708	0.16640	91.37	0.17358	95.44	0.18054
88	111.1	0.0124	0.378	28.21	87.56	0.05795	0.16632	91 57	0.17351	95.65	0.18047
90	114.3	0.0125	0.368	28.70	87.74	0.05882	0.16624	91.77	0.17344	95.86	0.18040
92	117.7	0.0125	0.357	29.19	87.92	0.05969	0.16616	91.97	0.17337	96.07	0.18033
94	121.0	0.0126	0.347	29.68	88.10	0.06056	0.16608	92.16	0.17330	96.28	0.18026
96	124.5	0.0126	0.338	30.18	88.28	0.06143	0.16600	92.36	0.17322	96.50	0.18018
98	128.0	0.0126	0.328	30.67	88.45	0.06230	0.16592	92.55	0.17315	96.71	0.18011
100	131.6	0.0127	0.319	31.16	88.62	0.06316	0.16584	92.75	0.17308	96.92	0.18004
102	135.3	0.0127	0.310	31.65	88.79	0.06403	0.16576	92.93	0.17301	97.12	0.17998
104	139.0	0.0128	0.302	32.15	88.95	0.06490	0.16568	93.11	0.17294	97.32	0.17993
106	142.8	0.0128	0.293	32.65	89.11	0.06577	0.16560	93.30	0.17288	97.53	0.17987
108	146.8	0.0129	0.285	33.15	89.27	0.06663	0.16551	93.48	0.17281	97.73	0.17982
110	150.7	0.0129	0.277	33.65	89.43	0.06749	0.16542	93.66	0.17274	97.93	0.17976
112	154.8	0.0130	0.269	34.15	89.58	0.06836	0.16533	93.82	0.17266	98.11	0.17969
114	158.9	0.0130	0.262	34.65	89.73	0.06922	0.16524	93.98	0.17258	98.29	0.17961
116	163.1	0.0131	0.254	35.15	89.87	0.07008	0.16515	94.15	0.17249	98.48	0.17954
118	167.4	0.0131	0.247	35.65	90.01	0.07094	0.16505	94.31	0.17241	98.66	0.17946
120	171.8	0.0132	0.240	36.16	90.15	0.07180	0.16495	94.47	0.17233	98.84	0.17939
122	176.2	0.0132	0.233	36.66	90.28	0.07266	0.16484	94.63	0.17224	99.01	0.17931
124	180.8	0.0133	0.227	37.16	90.40	0.07352	0.16473	94.78	0.17215	99.18	0.17922
126	185.4	0.0133	0.220	37.67	90.52	0.07437	0.16462	94.94	0.17206	99.35	0.17914
128	190.1	0.0134	0.214	38.18	90.64	0.07522	0.16450	95.09	0.17196	99.53	0.17906
130	194.9	0.0134	0.208	38.69	90.76	0.07607	0.16438	95.25	0.17186	99.70	0.17897
132	199.8	0.0135	0.202	39.19	90.86	0.07691	0.16425	95.41	0.17176	99.87	0.17889
134	204.8	0.0135	0.196	39.70	90.96	0.07775	0.16411	95.56	0.17166	100.04	0.17881
136	209.9	0.0136	0.191	40.21	91.06	0.07858	0.16396	95.72	0.17156	100.22	0.17873
138	215.0	0.0137	0.185	40.72	91.15	0.07941	0.16380	95.87	0.17145	100.39	0.17864
140	220.2	0.0138	0.180	41.24	91.24	0.08024	0.16363	96.03	0.17134	100.56	0.17856

TABLE 2. PROPERTIES OF MONOCHLORODIFLUOROMETHANE (F-22)

SAT TEMP F	ABS PRESS LB PER SQ IN.	VOLUME		ENTHALPY AND ENTROPY TAKEN FROM −40 F							
				ENTHALPY		ENTROPY		50 DEG SUPERHEAT		100 DEG SUPERHEAT	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
0	38.79	0.01192	1.373	10.63	105.02	0.0240	0.2293	112.35	0.2446	120.00	0.2590
2	40.43	0.01195	1.320	11.17	105.24	0.0251	0.2289	112.59	0.2442	120.26	0.2586
4	42.14	0.01198	1.270	11.70	105.45	0.0262	0.2285	112.83	0.2438	120.52	0.2581
5	43.02	0.01200	1.246	11.97	105.56	0.0268	0.2283	112.95	0.2436	120.65	0.2579
6	43.91	0.01201	1.221	12.23	105.66	0.0274	0.2280	113.07	0.2434	120.78	0.2577
8	45.74	0.01205	1.175	12.76	105.87	0.0285	0.2276	113.31	0.2430	121.04	0.2572
10	47.63	0.01208	1.130	13.29	106.08	0.0296	0.2272	113.55	0.2426	121.30	0.2568
12	49.58	0.01211	1.088	13.82	106.29	0.0307	0.2268	113.79	0.2422	121.56	0.2564
14	51.59	0.01215	1.048	14.36	106.50	0.0319	0.2264	114.02	0.2418	121.82	0.2560
16	53.66	0.01218	1.009	14.90	106.71	0.0330	0.2260	114.25	0.2414	122.08	0.2556
18	55.79	0.01222	0.9721	15.44	106.92	0.0341	0.2257	114.48	0.2410	122.33	0.2552
20	57.98	0.01225	0.9369	15.98	107.13	0.0352	0.2253	114.71	0.2406	122.59	0.2548
22	60.23	0.01229	0.9032	16.52	107.33	0.0364	0.2249	114.94	0.2402	122.84	0.2544
24	62.55	0.01232	0.8707	17.06	107.53	0.0375	0.2246	115.17	0.2398	123.10	0.2540
26	64.94	0.01236	0.8398	17.61	107.73	0.0379	0.2242	115.40	0.2395	123.35	0.2537
28	67.40	0.01239	0.8100	18.17	107.93	0.0398	0.2239	115.62	0.2391	123.60	0.2533
30	69.93	0.01243	0.7816	18.74	108.13	0.0409	0.2235	115.84	0.2387	123.85	0.2529
32	72.53	0.01247	0.7543	19.32	108.33	0.0421	0.2232	116.07	0.2383	124.10	0.2525
34	75.21	0.01250	0.7283	19.90	108.52	0.0433	0.2228	116.29	0.2380	124.35	0.2522
36	77.97	0.01254	0.7032	20.49	108.71	0.0445	0.2225	116.52	0.2376	124.59	0.2518
38	80.81	0.01258	0.6791	21.09	108.90	0.0457	0.2222	116.74	0.2373	124.84	0.2515
40	83.72	0.01262	0.6559	21.70	109.09	0.0469	0.2218	116.96	0.2369	125.08	0.2511
42	86.69	0.01266	0.6339	22.29	109.27	0.0481	0.2215	117.18	0.2366	125.32	0.2508
44	89.74	0.01270	0.6126	22.90	109.45	0.0493	0.2211	117.40	0.2363	125.56	0.2504
46	92.88	0.01274	0.5922	23.50	109.63	0.0505	0.2208	117.61	0.2359	125.80	0.2501
48	96.10	0.01278	0.5726	24.11	109.80	0.0516	0.2205	117.82	0.2356	126.04	0.2497
50	99.40	0.01282	0.5537	24.73	109.98	0.0528	0.2201	118.02	0.2353	126.27	0.2494
52	102.8	0.01286	0.5355	25.34	110.14	0.0540	0.2198	118.22	0.2350	126.50	0.2491
54	106.2	0.01290	0.5184	25.95	110.30	0.0552	0.2194	118.42	0.2347	126.73	0.2488
56	109.8	0.01294	0.5014	26.58	110.47	0.0564	0.2191	118.62	0.2343	126.96	0.2484
58	113.5	0.01299	0.4849	27.22	110.63	0.0576	0.2188	118.82	0.2340	127.19	0.2481
60	117.2	0.01303	0.4695	27.83	110.78	0.0588	0.2185	119.01	0.2337	127.42	0.2478
62	121.0	0.01307	0.4546	28.46	110.93	0.0600	0.2181	119.21	0.2334	127.65	0.2475
64	124.9	0.01312	0.4403	29.09	111.08	0.0612	0.2178	119.40	0.2331	127.87	0.2472
66	128.9	0.01316	0.4264	29.72	111.22	0.0624	0.2175	119.59	0.2327	128.10	0.2469
68	133.0	0.01320	0.4129	30.35	111.35	0.0636	0.2172	119.77	0.2324	128.32	0.2466
70	137.2	0.01325	0.4000	30.99	111.49	0.0648	0.2168	119.96	0.2321	128.54	0.2463
72	141.5	0.01330	0.3875	31.65	111.63	0.0661	0.2165	120.15	0.2318	128.76	0.2460
74	145.9	0.01334	0.3754	32.29	111.75	0.0673	0.2162	120.32	0.2315	128.97	0.2457
76	150.4	0.01339	0.3638	32.94	111.88	0.0684	0.2158	120.50	0.2312	129.19	0.2455
78	155.0	0.01344	0.3526	33.61	112.01	0.0696	0.2155	120.67	0.2309	129.40	0.2452
80	159.7	0.01349	0.3417	34.27	112.13	0.0708	0.2151	120.85	0.2306	129.61	0.2449
82	164.5	0.01353	0.3313	34.92	112.24	0.0720	0.2148	121.02	0.2303	129.82	0.2446
84	169.4	0.01358	0.3212	35.60	112.36	0.0732	0.2144	121.18	0.2300	130.02	0.2443
86	174.5	0.01363	0.3113	36.28	112.47	0.0744	0.2140	121.34	0.2297	130.23	0.2441
88	179.6	0.01368	0.3019	36.94	112.57	0.0756	0.2137	121.50	0.2294	130.43	0.2438
90	184.8	0.01374	0.2928	37.61	112.67	0.0768	0.2133	121.66	0.2291	130.63	0.2435
92	190.1	0.01379	0.2841	38.28	112.76	0.0780	0.2130	121.82	0.2288	130.83	0.2432
94	195.6	0.01384	0.2755	38.97	112.85	0.0792	0.2126	121.97	0.2285	131.03	0.2429
96	201.2	0.01390	0.2672	39.65	112.93	0.0803	0.2122	122.12	0.2282	131.23	0.2427
98	206.8	0.01396	0.2594	40.32	113.00	0.0815	0.2119	122.26	0.2279	131.42	0.2424
100	212.6	0.01402	0.2517	40.98	113.06	0.0827	0.2115	122.40	0.2276	131.61	0.2421
102	218.5	0.01408	0.2443	41.65	113.12	0.0839	0.2111	122.53	0.2273	131.80	0.2418
104	224.6	0.01414	0.2370	42.32	113.16	0.0851	0.2107	122.66	0.2270	131.99	0.2416
106	230.7	0.01420	0.2301	42.98	113.20	0.0862	0.2104	122.79	0.2267	132.17	0.2413
108	237.0	0.01426	0.2233	43.66	113.24	0.0874	0.2100	122.92	0.2264	132.35	0.2411
110	243.4	0.01433	0.2167	44.35	113.29	0.0886	0.2096	123.04	0.2261	132.53	0.2408
112	249.9	0.01440	0.2104	45.04	113.34	0.0898	0.2093	123.16	0.2258	132.71	0.2405
114	256.6	0.01447	0.2043	45.74	113.38	0.0909	0.2089	123.28	0.2255	132.88	0.2403
116	263.4	0.01454	0.1983	46.44	113.42	0.0921	0.2085	123.40	0.2253	133.05	0.2400
118	270.3	0.01461	0.1926	47.14	113.46	0.0933	0.2081	123.51	0.2250	133.22	0.2398
120	277.3	0.01469	0.1871	47.85	113.52	0.0945	0.2078	123.62	0.2247	133.39	0.2395

Data from Kinetic Chemicals, Inc., 1945

TABLE 3. PROPERTIES OF METHYL CHLORIDE

Sat. Temp. F	Abs. Press. Lb per Sq In.	Volume		Enthalpy and Entropy Taken From −40 F							
				Enthalpy		Entropy		100 F Superheat		200 F Superheat	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
0	18.73	0.0162	5.052	14.4	192.4	0.0328	0.4197	215.6	0.467	237.2	0.507
2	19.60	0.0162	4.856	15.1	193.1	0.0344	0.4196	216.2	0.466	237.7	0.505
4	20.47	0.0163	4.661	15.8	193.8	0.0360	0.4195	216.7	0.465	238.2	0.504
5	20.91	0.0163	4.563	16.2	194.1	0.0368	0.4195	217.0	0.464	238.5	0.503
6	21.39	0.0163	4.476	16.6	194.4	0.0376	0.4194	217.3	0.464	238.8	0.502
8	22.34	0.0164	4.303	17.3	195.1	0.0391	0.4193	217.9	0.463	239.4	0.501
10	23.30	0.0164	4.129	18.1	195.8	0.0407	0.4192	218.5	0.463	240.0	0.500
12	24.38	0.0164	3.984	18.8	196.3	0.0423	0.4184	219.0	0.462	240.5	0.499
14	25.46	0.0164	3.839	19.6	196.7	0.0439	0.4176	219.5	0.462	241.0	0.498
16	26.55	0.0165	3.693	20.3	197.2	0.0454	0.4168	220.0	0.461	241.5	0.498
18	27.63	0.0165	3.548	21.1	197.6	0.0472	0.4160	220.5	0.461	242.0	0.497
20	28.71	0.0166	3.403	21.8	198.1	0.0486	0.4152	221.0	0.460	242.5	0.496
22	29.98	0.0166	3.288	22.5	198.5	0.0501	0.4148	221.5	0.459	243.0	0.495
24	31.25	0.0166	3.172	23.3	198.9	0.0516	0.4143	222.0	0.459	243.6	0.495
26	32.53	0.0167	3.057	24.0	199.3	0.0532	0.4139	222.4	0.458	244.1	0.494
28	33.80	0.0167	2.941	24.8	199.7	0.0547	0.4134	222.9	0.458	244.7	0.494
30	35.07	0.0168	2.826	25.5	200.1	0.0562	0.4130	223.4	0.457	245.2	0.493
32	36.55	0.0168	2.734	26.2	200.5	0.0577	0.4124	223.9	0.456	245.7	0.492
34	38.03	0.0169	2.642	27.0	200.9	0.0592	0.4118	224.3	0.455	246.2	0.492
36	39.51	0.0169	2.549	27.7	201.4	0.0607	0.4111	224.8	0.455	246.7	0.491
38	40.99	0.0169	2.457	28.5	201.8	0.0622	0.4105	225.2	0.454	247.2	0.491
39	41.73	0.0170	2.411	28.8	202.0	0.0629	0.4102	225.5	0.453	247.4	0.490
40	42.47	0.0170	2.365	29.2	202.2	0.0637	0.4099	225.7	0.453	247.7	0.490
41	43.33	0.0170	2.328	29.6	202.4	0.0644	0.4096	225.9	0.453	248.0	0.490
42	44.18	0.0171	2.290	29.9	202.6	0.0651	0.4093	226.1	0.452	248.3	0.489
44	45.89	0.0171	2.216	30.7	203.0	0.0666	0.4087	226.6	0.451	248.8	0.489
46	47.61	0.0171	2.141	31.4	203.3	0.0680	0.4081	227.0	0.451	249.4	0.488
48	49.32	0.0172	2.067	32.2	203.7	0.0695	0.4075	227.5	0.450	249.9	0.488
50	51.03	0.0172	1.992	32.9	204.1	0.0709	0.4069	227.9	0.449	250.5	0.487
52	53.00	0.0172	1.931	33.7	204.4	0.0724	0.4063	228.2	0.448	251.0	0.486
54	54.97	0.0173	1.870	34.4	204.7	0.0739	0.4056	228.6	0.448	251.5	0.486
56	56.94	0.0173	1.810	35.2	205.1	0.0754	0.4050	228.9	0.447	252.0	0.485
58	58.91	0.0173	1.749	35.9	205.4	0.0769	0.4043	229.3	0.447	252.5	0.485
60	60.88	0.0174	1.688	36.7	205.7	0.0784	0.4037	229.6	0.446	253.0	0.484
62	63.13	0.0174	1.638	37.4	206.0	0.0798	0.4030	229.9	0.445	253.5	0.483
64	65.37	0.0174	1.588	38.2	206.3	0.0812	0.4024	230.3	0.444	254.0	0.483
66	67.62	0.0175	1.539	38.9	206.6	0.0827	0.4017	230.6	0.443	254.5	0.482
68	69.86	0.0175	1.489	39.7	206.9	0.0841	0.4011	231.0	0.442	255.0	0.482
70	72.11	0.0176	1.439	40.4	207.2	0.0855	0.4004	231.3	0.441	255.5	0.481
72	74.66	0.0176	1.398	41.1	207.5	0.0869	0.3998	231.6	0.440	256.0	0.480
74	77.21	0.0177	1.357	41.9	207.7	0.0883	0.3992	232.0	0.439	256.5	0.480
76	79.76	0.0177	1.315	42.6	208.0	0.0898	0.3985	232.3	0.439	256.9	0.479
78	82.31	0.0178	1.274	43.4	208.2	0.0912	0.3979	232.7	0.438	257.4	0.479
80	84.86	0.0178	1.233	44.1	208.5	0.0926	0.3973	233.0	0.437	257.9	0.478
82	87.74	0.0178	1.199	44.8	208.7	0.0940	0.3967	233.3	0.436	258.4	0.478
84	90.62	0.0179	1.165	45.6	209.0	0.0953	0.3960	233.6	0.435	258.9	0.477
86	93.50	0.0179	1.130	46.3	209.2	0.0967	0.3954	233.9	0.435	259.4	0.477
88	96.38	0.0180	1.096	47.1	209.5	0.0980	0.3947	234.2	0.434	259.9	0.476
90	99.26	0.0180	1.062	47.8	209.7	0.0994	0.3941	234.5	0.433	260.4	0.476
92	102.49	0.0180	1.033	48.6	209.9	0.1008	0.3935	234.8	0.433	260.8	0.476
94	105.72	0.0181	1.005	49.3	210.2	0.1022	0.3929	235.1	0.432	261.2	0.475
96	108.94	0.0181	0.9764	50.1	210.4	0.1035	0.3922	235.4	0.432	261.6	0.475
98	112.17	0.0182	0.9478	50.8	210.7	0.1049	0.3916	235.7	0.431	262.0	0.474
100	115.40	0.0182	0.9193	51.6	210.9	0.1063	0.3910	236.0	0.431	262.4	0.474
102	119.00	0.0183	0.8952	52.3	211.1	0.1076	0.3903	236.4	0.430	262.8	0.474
104	122.60	0.0183	0.8712	53.1	211.3	0.1090	0.3897	236.8	0.430	263.2	0.473
106	126.20	0.0184	0.8471	53.8	211.4	0.1103	0.3890	237.1	0.429	263.5	0.473
108	129.80	0.0184	0.8231	54.6	211.6	0.1117	0.3884	237.5	0.429	263.9	0.472
110	133.40	0.0185	0.7990	55.3	211.8	0.1130	0.3877	237.9	0.428	264.3	0.472
112	137.42	0.0185	0.7786	56.1	212.0	0.1144	0.3871	238.1	0.427	264.6	0.471
114	141.44	0.0185	0.7583	56.8	212.2	0.1157	0.3864	238.3	0.427	264.8	0.470
116	145.46	0.0186	0.7379	57.6	212.4	0.1171	0.3858	238.6	0.426	265.1	0.470
118	149.48	0.0186	0.7176	58.3	212.6	0.1184	0.3851	238.8	0.426	265.3	0.469
120	153.50	0.0187	0.6972	59.1	212.8	0.1198	0.3845	239.0	0.425	265.6	0.468

Table 4. Properties of Ammonia

Sat. Temp. F	Abs. Press. Lb per Sq In.	Volume		Enthalpy and Entropy Taken From −40 F							
				Enthalpy		Entropy		100 F Superheat		200 F Superheat	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
0	30.42	0.02419	9.116	42.9	611.8	0.0975	1.3352	666.8	1.4439	720.3	1.5317
2	31.92	0.02424	8.714	45.1	612.4	0.1022	1.3312	667.6	1.4400	721.2	1.5277
4	33.47	0.02430	8.333	47.2	613.0	0.1069	1.3273	668.4	1.4360	722.2	1.5236
5	34.27	0.02432	8.150	48.3	613.3	0.1092	1.3253	668.8	1.4340	722.6	1.5216
6	35.09	0.02435	7.971	49.4	613.6	0.1115	1.3234	669.3	1.4321	723.1	1.5196
8	36.77	0.02440	7.629	51.6	614.3	0.1162	1.3195	670.1	1.4281	724.1	1.5155
10	38.51	0.02446	7.304	53.8	614.9	0.1208	1.3157	670.9	1.4242	725 0	1.5115
12	40.31	0.02451	6.996	56.0	615.5	0.1254	1.3118	671.7	1.4205	725.9	1.5077
14	42.18	0.02457	6.703	58.2	616.1	0.1300	1.3081	672.5	1.4168	726.8	1.5039
16	44.12	0.02462	6.425	60.3	616.6	0.1346	1.3043	673.4	1.4130	727.8	1.5001
18	46.13	0.02468	6.161	62.5	617.2	0.1392	1.3006	674.2	1.4093	728.7	1.4963
20	48.21	0.02474	5.910	64.7	617.8	0 1437	1.2969	675.0	1.4056	729.6	1.4925
22	50.36	0.02479	5.671	66.9	618.3	0.1483	1.2933	675.8	1.4021	730.5	1.4889
24	52.59	0.02485	5.443	69 1	618.9	0.1528	1.2897	676.6	1.3985	731.4	1.4853
26	54.90	0.02491	5.227	71.3	619.4	0.1573	1.2861	677.3	1.3950	732.4	1.4816
28	57.28	0.02497	5.021	73 5	619.9	0.1618	1.2825	678.1	1.3914	733.3	1.4780
30	59.74	0.02503	4.825	75.7	620.5	0 1663	1.2790	678.9	1.3879	734.2	1.4744
32	62.29	0.02508	4.637	77 9	621.0	0.1708	1.2755	679.7	1.3846	735.1	1.4710
34	64.91	0.02514	4.459	80.1	621.5	0.1753	1 2721	680.4	1.3812	736.0	1.4676
36	67.63	0 02521	4.289	82.3	622.0	0.1797	1.2686	681.2	1.3779	736.8	1.4643
38	70.43	0.02527	4.126	84.6	622.5	0.1841	1.2652	681.9	1.3745	737.7	1.4609
39	71.87	0.02530	4.048	85.7	622.7	0.1863	1.2635	682.3	1.3729	738.2	1.4592
40	73.32	0.02533	3.971	86.8	623 0	0.1885	1.2618	682.7	1.3712	738.6	1.4575
41	74.80	0.02536	3.897	87.9	623.2	0.1908	1.2602	683.1	1.3696	739.0	1.4559
42	76.31	0.02539	3.823	89.0	623.4	0.1930	1.2585	683.4	1.3680	739.5	1.4542
44	79.38	0.02545	3.682	91.2	623.9	0.1974	1.2552	684.2	1.3648	740.4	1.4510
46	82.55	0.02551	3.547	93.5	624.4	0.2018	1.2519	684.9	1.3616	741.3	1.4477
48	85.82	0.02558	3.418	95.7	624.8	0.2062	1.2486	685.6	1.3584	742.2	1.4445
50	89.19	0.02564	3.294	97.9	625.2	0.2105	1.2453	686.4	1.3552	743.1	1.4412
52	92.66	0.02571	3.176	100.2	625.7	0.2149	1.2421	687.1	1.3521	744.0	1.4382
54	96.23	0.02577	3.063	102.4	626.1	0.2192	1.2389	687.8	1.3491	744.8	1.4351
56	99.91	0 02584	2 954	104.7	626.5	0.2236	1.2357	688.5	1.3460	745.7	1.4321
58	103.7	0.02590	2.851	106.9	626.9	0.2279	1.2325	689.2	1.3430	746.5	1.4290
60	107.6	0.02597	2.751	109 2	627.3	0.2322	1.2294	689.9	1.3399	747.4	1.4260
62	111.6	0.02604	2.656	111.5	627.7	0.2365	1.2262	690.6	1.3370	748.2	1.4231
64	115.7	0.02611	2.565	113.7	628.0	0.2408	1.2231	691.3	1.3341	749.1	1.4202
66	120.0	0.02618	2.477	116.0	628.4	0.2451	1.2201	691.9	1.3312	749.9	1.4172
68	124.3	0.02625	2.393	118.3	628.8	0.2494	1.2170	692.6	1.3283	750.8	1.4143
70	128.8	0.02632	2.312	120.5	629.1	0.2537	1.2140	693.3	1.3254	751.6	1.4114
72	133.4	0.02639	2.235	122.8	629.4	0.2579	1.2110	694.0	1.3226	752.4	1.4086
74	138.1	0.02646	2.161	125.1	629.8	0.2622	1.2080	694.6	1.3199	753.3	1.4059
76	143.0	0.02653	2.089	127.4	630 1	0.2664	1.2050	695.3	1.3171	754.1	1.4031
78	147.9	0.02661	2.021	129.7	630.4	0.2706	1.2020	695.9	1.3144	755.0	1.4004
80	153.0	0.02668	1.955	132.0	630.7	0.2749	1.1991	696.6	1.3116	755.8	1.3976
82	158.3	0.02675	1.892	134.3	631.0	0.2791	1.1962	697.2	1.3089	756.6	1.3949
84	163.7	0.02684	1.831	136.6	631.3	0.2833	1.1933	697.8	1.3063	757.4	1.3923
86	169.2	0.02691	1.772	138.9	631.5	0.2875	1.1904	698.5	1.3040	758.3	1.3896
88	174.8	0.02699	1.716	141.2	631.8	0.2917	1.1875	699.1	1.3010	759.1	1.3870
90	180.6	0.02707	1.661	143.5	632.0	0.2958	1.1846	699.7	1.2983	759.9	1.3843
92	186.6	0.02715	1.609	145.8	632.2	0.3000	1.1818	700.3	1.2957	760.7	1.3818
94	192.7	0.02723	1.559	148.2	632.5	0.3041	1.1789	700.9	1.2932	761.5	1.3793
96	198.9	0.02731	1.510	150.5	632.6	0.3083	1.1761	701.5	1.2906	762.2	1.3768
98	205.3	0.02739	1.464	152.9	632.9	0.3125	1.1733	702.1	1.2881	763.0	1.3743
100	211.9	0.02747	1.419	155.2	633.0	0.3166	1.1705	702.7	1.2855	763.8	1.3718
102	218.6	0.02756	1.375	157.6	633.2	0.3207	1.1677	703.3	1.2830	764.6	1.3693
104	225.4	0.02764	1.334	159.9	633.4	0.3248	1.1649	703.8	1.2805	765.3	1.3668
106	232.5	0.02773	1.293	162.3	633.5	0.3289	1.1621	704.3	1.2780	766.1	1.3643
108	239.7	0.02782	1.254	164.6	633.6	0.3330	1.1593	705.0	1.2755	766.9	1.3619
110	247.0	0.02790	1.217	167.0	633.7	0.3372	1.1566	705.5	1.2731	767.6	1.3596
112	254.5	0.02799	1.180	169.4	633.8	0.3413	1.1538	706.1	1.2708	768.3	1.3573
114	262.2	0.02808	1.145	171.8	633.9	0.3453	1.1510	706.6	1.2684	769.1	1.3550
116	270.1	0.02817	1.112	174.2	634.0	0.3495	1.1483	707.2	1.2661	769.8	1.3527
118	278.2	0.02827	1.079	176.6	634.0	0.3535	1.1455	707.7	1.2636	770.5	1.3503
120	286.4	0.02836	1.047	179.0	634.0	0.3576	1.1427	708.2	1.2612	771.3	1.3479
122	294.8	0.02846	1.017	181.4	634.0	0.3618	1.1400	708.6	1.2587	772.0	1.3455
124	303.4	0.02855	0.987	183.9	634.0	0.3659	1.1372	709.1	1.2563	772.8	1.3431
126	312.2	0.02865	0.958	186.3	633.9	0.3700	1.1344	709.6	1.2538	773.5	1.3407
128	321.2	0.02875	0.931	188.8	633.9	0.3741	1.1316	710.0	1.2513	774.2	1.3383

TABLE 5. PROPERTIES OF CARBON DIOXIDE

Sat. Temp. F	Abs. Press. Lb per Sq In.	Volume		Enthalpy and Entropy Taken From −40 F							
				Enthalpy		Entropy		50 F Superheat		100 F Superheat	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
0	305.5	0.01570	0.29040	18.8	138 9	0.0418	0.3024	153.7	0.3342	167.5	0.3612
2	315.9	0.01579	0.28030	19 8	138.8	0 0440	0.3014	153.7	0.3303	167.6	0.3600
4	326.5	0.01588	0.27070	20.8	138.8	0.0461	0.3005	153.7	0.3318	167.7	0.3588
5	332.0	0.01592	0.26610	21.3	138.8	0.0472	0.3000	153.7	0.3312	167.7	0.3582
6	337.4	0 01596	0.26140	21.8	138.7	0.0483	0.2994	153.7	0.3306	167.8	0.3576
8	348.7	0.01605	0.25260	22.9	138.7	0 0504	0.2982	153.7	0.3293	167.9	0.3563
10	360.2	0.01614	0.24370	24.0	138.7	0.0526	0.2970	153.7	0.3281	168.0	0.3550
12	371.9	0.01623	0.23540	25.0	138.6	0.0548	0.2958	153.7	0 3270	168.1	0.3538
14	383.9	0.01632	0.22740	26.1	138.6	0.0571	0.2946	153.7	0.3259	168.2	0.3526
16	396.2	0.01642	0.21970	27.2	138.5	0.0593	0.2933	153.7	0.3249	168.3	0.3513
18	408.9	0.01652	0.21210	28.3	138.4	0.0616	0.2921	153.7	0.3238	168.5	0.3501
20	421.8	0.01663	0.20490	29.4	138.3	0.0638	0.2909	153.7	0.3227	168.6	0.3489
22	434.0	0.01673	0.19790	30.5	138.2	0.0662	0.2897	153.7	0.3214	168.7	0.3479
24	448.4	0.01684	0.19120	31.7	138.1	0 0686	0.2885	153.7	0.3202	168.8	0.3470
26	462.2	0.01695	0.18460	32.9	138.0	0.0710	0.2873	153.7	0.3189	168.9	0.3460
28	476.3	0.01707	0.17830	34.1	137.9	0.0734	0.2861	153.7	0.3177	169.0	0.3451
30	490.8	0.01719	0.17220	35.4	137.8	0 0758	0.2849	153.7	0.3164	169.1	0.3441
32	505.5	0.01731	0.16630	36.7	137.7	0.0781	0.2834	153.7	0.3158	169.2	0.3431
34	522.6	0.01744	0.16030	37.9	137.4	0.0804	0.2820	153.7	0.3151	169.3	0.3421
36	536.0	0.01759	0.15500	39.1	137.2	0.0828	0.2805	153.7	0.3145	169.4	0.3411
38	551.7	0.01773	0.14960	40.4	136.9	0.0851	0.2791	153.7	0.3138	169.5	0.3401
39	559.7	0 01780	0.14700	41.0	136.8	0.0862	0.2783	153.7	0.3135	169.5	0.3396
40	567.8	0.01787	0.14440	41.7	136.7	0.0874	0.2776	153.7	0.3132	169.6	0.3391
41	576.0	0.01794	0.14185	42.3	136.5	0.0887	0.2768	153.7	0.3127	196.6	0.3386
42	584.3	0.01801	0.13930	42 9	136.3	0.0899	0.2761	153.7	0.3122	169.7	0.3381
44	601.1	0.01817	0.13440	44.3	136.1	0.0924	0.2745	153.7	0.3112	169.8	0.3371
46	618.2	0.01834	0.12970	45.6	135.7	0.0950	0.2730	153.7	0.3101	169.9	0.3362
48	635.7	0 01851	0.12500	47.0	135.4	0.0975	0.2714	153.7	0.3091	170.0	0.3352
50	653.6	0 01868	0.12050	48.4	135.0	0.1000	0.2699	153.7	0.3081	170.1	0.3342
52	671.9	0.01887	0.11610	49.8	134.5	0.1027	0.2681	153.7	0.3069	170.2	0.3333
54	690.6	0.01906	0.11170	51.2	133.9	0.1054	0.2663	153.7	0.3057	170.3	0.3324
56	709.5	0.01927	0.10750	52 6	133.4	0.1081	0.2644	153.5	0.3046	170.5	0.3315
58	728.8	0.01948	0.10340	54.0	132.7	0.1108	0.2626	153.7	0.3034	170.6	0.3306
60	748.6	0.01970	0.09940	55.5	132.1	0.1135	0.2608	153.7	0.3022	170.7	0.3297
62	769.0	0.01995	0.09545	57.0	131.3	0.1164	0.2584	153.7	0.3012	170.8	0.3289
64	789.4	0.02020	0.09180	58.6	130.6	0.1194	0.2560	153.7	0 3002	170.9	0.3281
66	810.3	0.02048	0.08800	60.2	129.7	0.1223	0.2535	153.7	0.2991	171.0	0.3273
68	831.6	0.02079	0.08422	61.9	128.7	0.1253	0.2511	153.7	0.2981	171 1	0.3265
70	853.4	0.02112	0.08040	63.7	127.5	0.1282	0.2487	153.7	0.2971	171.2	0 3257
72	875.8	0.02152	0.07654	65.5	126.0	0.1321	0.2450	153.7	0.2962	171.3	0.3250
74	898.2	0.02192	0.07269	67.3	124.5	0.1360	0.2414	153.7	0.2953	171.4	0.3242
76	921.3	0.02242	0.06875	69.4	122.8	0.1398	0.2377	153.7	0.2945	171.5	0.3235
78	944.8	0.02300	0.06473	71.6	120.9	0.1437	0.2341	153.7	0 2936	171.6	0.3227
80	968.7	0.02370	0.06064	73.9	118.7	0.1476	0.2304	153.7	0.2927	171.7	0.3220
82	993.0	0.02456	0.05648	76.4	116.6	0.1578	0.2195	153.7	0.2920	173.8	0.3215
84	1017.7	0.02553	0.05223	79.4	113.9	0.1679	0.2087	153.7	0.2914	176.0	0.3209
86	1043.0	0.02686	0.04789	83.3	110.4	0 1781	0.1978	153.7	0.2907	178.2	0.3204
87.8	1069.9	0.03454	0.03454	97.0	97.0	0.1880	0.1880	153.7	0.2901	180.1	0.3199

for all practical purposes the specific volume and the enthalpy of any sub-cooled refrigerant can be taken as equal to the values read from the tables for a saturated liquid at the same temperature. Thus if F-12 at 121 psia and 40 F is passing through a pipe, its volume and enthalpy can be determined from Table 1 as 0.0116 cu ft per pound and 17.0 Btu per pound.

Frequently it is necessary to determine the properties of a *wet* vapor or of a mixture of liquid with some added vapor, such as is found at discharge from an expansion valve. This can be done from the tables by noting that the specific enthalpy of the mixture must be equal to that of the saturated liquid plus a fraction of the latent heat of vaporization equal to the fraction of refrigerant which is present in vapor form.

TABLE 6. PROPERTIES OF MONOFLUOROTRICHLOROMETHANE (F-11)

Sat. Temp. F	Abs. Press. Lb per Sq In.	Volume		Enthalpy and Entropy Taken From −40 F							
				Enthalpy		Entropy		25 F Superheat		50 F Superheat	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
0	2.59	0.01020	13.700	7.81	90.4	0.0178	0.1975	93.9	0.2049	97.4	0.2120
5	2.96	0.01024	12.100	8.81	91.2	0.0200	0.1974	94.7	0.2047	98.2	0.2117
10	3.38	0.01028	10.700	9.82	92.0	0.0222	0.1973	95.5	0.2045	99.0	0.2114
15	3.85	0.01032	9.530	10.80	92.8	0.0243	0.1971	96.3	0.2043	99.8	0.2111
20	4.36	0.01036	8.490	11.90	93.7	0.0264	0.1970	97.2	0.2041	100.7	0.2109
25	4.94	0.01040	7.580	12.90	94.5	0.0286	0.1969	98.0	0.2039	101.5	0.2107
30	5.57	0.01045	6.770	13.90	95.3	0.0307	0.1969	98.8	0.2038	102.3	0.2105
35	6.27	0.01049	6.080	14.90	96.1	0.0328	0.1968	99.6	0.2037	103.1	0.2103
40	7.03	0.01053	5.460	16.00	96.8	0.0349	0.1968	100.3	0.2036	103.8	0.2101
45	7.88	0.01057	4.920	17.00	97.6	0.0370	0.1967	101.1	0.2035	104.6	0.2099
50	8.79	0.01062	4.440	18.10	98.4	0.0391	0.1967	101.9	0.2034	105.4	0.2098
55	9.80	0.01066	4.020	19.10	99.2	0.0412	0.1967	102.7	0.2033	106.2	0.2097
60	10.90	0.01071	3.640	20.20	100.0	0.0432	0.1967	103.5	0.2033	107.0	0.2096
65	12.10	0.01076	3.300	21.30	100.8	0.0453	0.1967	104.3	0.2032	107.8	0.2094
70	13.40	0.01081	3.000	22.40	101.5	0.0473	0.1967	105.0	0.2032	108.5	0.2093
75	14.80	0.01086	2.740	23.50	102.2	0.0493	0.1967	105.7	0.2031	109.2	0.2092
80	16.30	0.01091	2.500	24.50	102.9	0.0513	0.1966	106.4	0.2030	109.9	0.2090
85	17.90	0.01096	2.280	25.60	103.6	0.0533	0.1966	107.1	0.2029	110.6	0.2089
90	19.70	0.01101	2.090	26.70	104.4	0.0553	0.1966	107.9	0.2028	111.4	0.2088
95	21.60	0.01106	1.918	27.80	105.1	0.0573	0.1966	108.6	0.2028	112.1	0.2087
100	23.60	0.01111	1.761	28.90	105.7	0.0593	0.1965	109.2	0.2027	112.7	0.2085
105	25.90	0.01116	1.620	30.10	106.4	0.0613	0.1965	109.9	0.2026	113.4	0.2084

TABLE 7. PROPERTIES OF WATER

Sat. Temp. F	Abs. Press. Lb per Sq In.	Volume		Enthalpy and Entropy Taken From +32 F							
				Enthalpy		Entropy		50 F Superheat		100 F Superheat	
		Liquid	Vapor	Liquid	Vapor	Liquid	Vapor	Enthalpy	Entropy	Enthalpy	Entropy
32	0.0887	0.01602	3296.0	0.00	1073.0	0.0000	2.1826	1096.9	2.2277	1120.8	2.2688
35	0.1000	0.01602	2941.0	3.02	1074.4	0.0062	2.1724	1098.3	2.2172	1122.2	2.2581
40	0.1217	0.01602	2441.0	8.05	1076.8	0.0163	2.1555	1100.6	2.2000	1124.5	2.2406
45	0.1475	0.01602	2034.0	13.07	1079.2	0.0262	2.1390	1102.9	2.1832	1126.7	2.2234
50	0.1780	0.01602	1702.0	18.08	1081.5	0.0361	2.1230	1105.2	2.1667	1129.0	2.2066
55	0.2140	0.01603	1430.0	23.08	1083.9	0.0459	2.1073	1107.5	2.1506	1131.3	2.1902
60	0.2561	0.01603	1206.0	28.08	1086.2	0.0556	2.0920	1109.8	2.1349	1133.5	2.1742
65	0.3054	0.01604	1021.0	33.08	1088.6	0.0652	2.0771	1112.2	2.1196	1135.8	2.1585
70	0.3628	0.01605	868.0	38.07	1090.9	0.0746	2.0625	1114.5	2.1046	1138.1	2.1432
75	0.4295	0.01606	740.0	43.06	1093.2	0.0840	2.0483	1116.7	2.0900	1140.3	2.1283
80	0.507	0.01607	632.9	48.05	1095.5	0.0933	2.0344	1119.0	2.0758	1142.5	2.1138
85	0.596	0.01609	543.3	53.04	1097.8	0.1025	2.0208	1121.2	2.0619	1144.7	2.0996
90	0.698	0.01610	467.9	58.03	1100.0	0.1116	2.0075	1123.4	2.0483	1146.8	2.0857
95	0.815	0.01612	404.2	63.01	1102.3	0.1206	1.9946	1125.6	2.0350	1148.9	2.0721
100	0.949	0.01613	350.3	68.00	1104.6	0.1296	1.9819	1127.9	2.0220	1151.1	2.0588
105	1.101	0.01615	304.4	72.98	1106.8	0.1384	1.9695	1130.2	2.0093	1153.2	2.0458

Consider, for example, F-12 with a quality (the per cent in vapor form) of 30 per cent; the enthalpy of this material would be equal to:

$$h_m = h_f + 0.30\ (h_v - h_f) \tag{2}$$

where

h_m = specific enthalpy of the mixture.
h_f = specific enthalpy of the liquid.
h_v = specific enthalpy of the saturated vapor.

Values of h_f and h_v are obtained from Table 1 for the actual pressure of the mixture.

By a reversal of this same procedure the tabular data can be used to determine the state of a mixture leaving an expansion valve. Consider a valve to which saturated liquid at pressure p_s is admitted and a mixture of saturated liquid and vapor at pressure p_d is discharged. The quality of the material at discharge is then determined by making use of the fact that the expansion process is completely irreversible, is a throttling process, and hence occurs without change in enthalpy. Thus the enthalpy of the mixture, h_m, is equal to the enthalpy of the saturated liquid at the entrance state, h_{fs}, and can therefore be read from the table.

Thus,

$$h_{fs} = h_m = h_{vd} - (1 - x)\ (h_{vd} - h_{fd}) \tag{3}$$

or,

$$x = (h_m - h_{fd}) \div (h_{vd} - h_{fd}) \tag{4}$$

where

h_{fs} = enthalpy of saturated liquid at entrance to expansion valve.
h_m = enthalpy of mixture.
h_{vd} = enthalpy of saturated vapor at discharge.
h_{fd} = enthalpy of liquid at discharge.
x = proportion of liquid in the mixture, decimal.

The refrigerant *cycle* is the series of state changes which occur in the conditioning processes needed to restore the refrigerant to a condition in which it will possess the ability to extract heat from the space to be cooled. For all compression-type systems the cycle consists of four processes: heat gain in the evaporator; pressure rise in the compressor; heat loss in the condenser; pressure loss in the expansion valve. The compression process is accomplished at the expense of energy added to the compressor in the form of shaft work and the expansion process could be carried out, if the economics of the system would permit, in an expanding engine with consequent release of energy as shaft work. In ordinary systems, however, the additional first cost and maintenance costs of an expanding engine so greatly exceed the advantage resulting from the work realized that such engines are not used and the pressure reduction is allowed to occur irreversibly in an expansion valve. Basically, then, a refrigeration cycle consists of two heat transfer processes and two pressure change processes, no work entering into the heat transfer processes and—in the simple cycle—no heat transfer occurring during the pressure-change processes.

Simple Refrigeration Cycles

The most common and least complicated type of refrigeration cycle is shown in Fig. 1 and is called the *simple saturation cycle.* For this system saturated vapor flows without gain or loss of heat from the

evaporator to the suction of the compressor. During passage through the compressor the energy added as shaft work goes entirely to increase the enthalpy of the refrigerant, and the compression process, which is assumed to occur irreversibly and without external heat transfer, is characterized by constant entropy. Thus the state of the superheated vapor leaving the compressor can be determined from the tables of thermodynamic properties by noting the discharge pressure and fixing also the entropy of the saturated vapor at entrance to the compressor.

Superheated vapor from the compressor flows to the condenser where desuperheating and condensation take place. From the condenser the refrigerant flows to the expansion valve, undergoes a constant-enthalpy pressure reduction and returns to the evaporator where it again removes a quantity of undesired heat. When the evaporator is arranged to permit direct cooling of room air by the refrigerant, the system is said to be

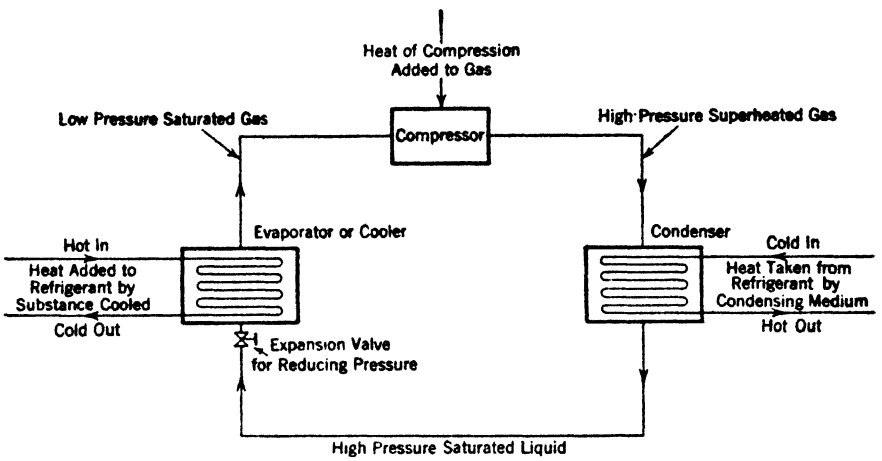

FIG. 1. MECHANICAL REFRIGERATION SYSTEM

of the *direct expansion* type, while a system in which the evaporating refrigerant cools water or brine, which in turn cools the air, is said to be *indirect*. Although many differences exist between most actual systems and that of the simple saturation cycle this latter is nonetheless of great value in that it provides an extremely simple method of rapidly achieving an approximate analysis of probable power requirements, compressor size, etc. Further, the equations used in analysis of a simple saturation cycle form the basis of the more complex treatments required for compound refrigeration cycles. For these reasons a typical simple saturation problem will be worked in detail.

Example 1. A simple saturation cycle carries a 7 ton load when operating between suction and discharge pressures of 52.7 psia and 121 psia with F-12 as the refrigerant. Determine: (*a*) the cooling effect provided by each pound of refrigerant, (*b*) the refrigerant circulating rate, (*c*) the horsepower required, (*d*) the quantity of heat to be dissipated from the condenser, (*e*) the required condenser cooling water, in gallons per minute, if temperature rise of water passing through the condenser is 8 deg, (*f*) the bore and stroke of a double acting cylinder (neglecting the effect of the piston rod) if speed of compressor is 500 revolutions per minute.

Solution. (*a*) Saturated liquid F-12 at 121 psia leaves the condenser and enters the expansion valve. The enthalpy of this material (from Table 1) is 29.68 Btu per pound and this must also be its enthalpy at entrance to the evaporator. Leaving the evaporator as a saturated vapor at 52.7 psia, its enthalpy is 82.82 so the refrigerating effect must be 82.82 − 29.68 = 53.14 Btu per pound.

(*b*) The refrigerant circulating rate is equal to the total heat to be picked up in unit time divided by the pick-up per pound of refrigerant or,

$$W_r = (7 \text{ ton} \times 200) \div 53.14 = 26.3 \text{ lb per minute.}$$

(*c*) The horse power required is equal to the increase in energy of the refrigerant passing through the compressor (expressed in Btu per minute) divided by the conversion factor 42.42, which is the number of Btu per minute corresponding to 1 hp,

$$(\text{hp}) = W_r (h_d - h_{vs}) \div 42.42 \qquad (5)$$

where

hp = horsepower.
W_r = refrigerant circulating rate in pounds per minute.
h_d = enthalpy of vapor at condition of discharge from compressor.
h_{vs} = enthalpy of saturated vapor entering compressor.

W_r is known from (*b*) and h_{vs} is the enthalpy of refrigerant as it enters the compressor in a saturated vapor state at 52.7 psia; thus $h_{vs} = 82.82$.

In order to determine h_d, the state of the refrigerant must first be determined at the compressor discharge. At the known suction state the entropy (from Table 1 for saturated vapor at 52.7 psia) is 0.16828 and, since the compression is assumed to occur isentropically, it therefore follows that the discharge state must have the same entropy at 121 psia. From the table the entropy of vapor superheated 25 deg is 0.17330, so the superheat, t_{sd}, possessed by the actual gas discharged from this compressor can be obtained by interpolation as,

$$\frac{t_{sd}}{25} = \frac{0.16828 - 0.16608}{0.17330 - 0.16608}$$

from which $t_{sd} = 7.6$ deg.

As the saturation temperature at 121 psia is 94 F the actual temperature, t_d, of the vapor leaving the compressor is, $t_d = 94 + t_{sd} = 94 + 7.6 = 101.6$ F. By the same kind of interpolation the enthalpy of the discharged vapor can be determined from the enthalpies given for vapor superheated 25 F and for saturated vapor,

$$\frac{(h_d - 88.10)}{(92.16 - 88.10)} = \frac{(0.16828 - 0.16608)}{(0.17330 - 0.16608)}$$

from which, $h_d = 89.34$ Btu per pound.

Then substituting into Equation 5,

$$(\text{hp}) = 26.3 (89.34 - 82.82) \div 42.42 = 4.03$$

(*d*) The rate of heat loss from the condenser, Q_c, must be equal to the sum of the energies picked up by the refrigerant in the evaporator and the compressor,

$Q_c = 53.14 + (89.34 - 82.82) = 53.14 + 6.52 = 59.66$ Btu per pound or $26.3 \times 59.66 = 1569$ Btu per minute. This same figure can, of course, be determined more directly by subtraction of the enthalpy of liquid leaving the condenser from the enthalpy of superheated vapor going into it, thus,

$$Q_c = 26.3 (89.34 - 29.68) = 1569 \text{ Btu per minute.}$$

(*e*) The cooling water rate (based on a gallon as 8.34 lb) is $1569 \div (8 \times 8.34) = 23.5$ gpm.

(*f*) The compressor size is fixed by the volume of gas which must be drawn into the machine per unit time. Saturated vapor at 52.7 psia has a specific volume, from Table 1, of 0.779 cu ft per pound, hence $26.3 \times 0.779 = 20.49$ cfm of gas must be handled. Assuming a volumetric efficiency of 90 per cent the compressor must then displace $20.49 \div 0.9 = 22.8$ cfm. The speed is given as 500 rpm and as the unit is known to be double-acting the displacement is therefore $(22.8 \times 1728) \div (2 \times 500) = 39.4$ cu in. If the unit were designed so that bore, d, and stroke were the same,

$$(\pi d^3) \div 4 = 39.4 \qquad d = 3.69 \text{ in.}$$

Coefficient of Performance

In order to permit evaluation of the effectiveness with which any given cycle operates, some term is desirable which would be comparable to the *efficiency* that is used for heat engines. In refrigeration the desired effect is heat extraction and the cost of achieving this extraction is the amount of energy which must be supplied as shaft work. Thus the ratio of refrigerating effect to the heat equivalent of the compressor work is used as a measure of effectiveness and is defined as the coefficient of performance, thus,

$$(\text{cop}) = (h_{vs} - h_{fc}) \div (h_d - h_{vs}) \qquad (6)$$

where

cop = coefficient of performance.
h_{vs} = specific enthalpy of saturated vapor entering compressor.
h_{fc} = specific enthalpy of liquid at discharge from condenser.
h_d = specific enthalpy of vapor at discharge from compressor.

The subscripts vs, d, and fc represent state points at suction and discharge of the compressor and at discharge from the condenser. Thus for the conditions of the simple saturation cycle which was used in Example 1,

$$(\text{cop}) = (82.82 - 29.68) \div (89.34 - 82.82) = 8.17.$$

This coefficient can be compared with that which would exist if the system were to operate on an ideal Carnot cycle for which the coefficient of performance would be,

$$(\text{cop}) = \frac{T_s}{T_c - T_s}$$

where

T_s = evaporator temperature, Fahrenheit degrees, absolute.
T_c = condenser temperature, Fahrenheit degrees, absolute.

In problem 1, T_s = 501 F (which is 41 F + 460) and T_c = 554 F (which is 94 F + 460) and,

$$(\text{cop}) = \frac{501}{(554 - 501)} = 9.6$$

The actual cycle is therefore 8.17 ÷ 9.6 or 85 per cent as effective as a Carnot cycle between the same temperature limits.

Influence of Suction Pressure

Brief consideration of the analytical procedure used in discussion of the simple saturation cycle will bring out the need for maintaining the suction pressure on any refrigeration system as high as the load will permit. As the suction pressure increases, for fixed discharge pressure, the enthalpy of refrigerant entering the evaporator remains unchanged, but the leaving enthalpy increases and hence the refrigerating effect increases. Further, compressor energy input is reduced not merely because of the greater enthalpy of the gas at suction, but also because of a reduction in the enthalpy of the superheated gas at discharge. Since the refrigerating effect is greater and the work less, it is obvious that there will be a substantial gain in the coefficient of performance.

The actual value of suction pressure on any system is obviously determined by the required temperature which must be maintained in

the conditioned space. For a direct expansion system the evaporator can be held at a temperature not much less than that of the conditioned enclosure except in cases where lower temperatures may be needed in order to establish a desired ratio of dehumidifying to cooling load. When dehumidification requirements dictate the use of unusually low evaprorato temperatures the increased operating cost should properly be charged against the dehumidification rather than the sensible cooling.

Influence of Discharge Pressure

In contrast to the suction pressure, the compressor discharge pressure should be kept as low as operating conditions will allow. This pressure must be high enough to provide a saturation temperature of refrigerant within the condenser which is greater than the exit temperature of the cooling water. The discharge pressure therefore is a direct function of the temperature of the cooling fluid and will automatically rise whenever the temperature of cooling water (or air) rises; it will also rise when the flow rate of the cooling medium is decreased.

Increase in discharge pressure (for fixed suction pressure) raises the enthalpy of the gas leaving the compressor, hence increases the work of compression. Further, the enthalpy of saturated liquid leaving the condenser increased with pressure so the refrigerating effect must decrease. Thus the effect of such a pressure rise is to require more work per pound of refrigerant handled and at the same time to necessitate an increase in the refrigerant flow rate.

Influence of Water Jacket

The preceding discussion has, in every case, assumed isentropic compression. Where exact performance data are not available this assumption is a desirable one since it leads to a conservatively large determination of the power required. In most actual systems the compression process departs from isentropic due to irreversible heat transfers which occur between the vapor in the cylinder and the cylinder wall and also because of intentional heat dissipation from the outside of the cylinder walls to the surroundings, or to a cooling fluid passing through a water jacket around the cylinder.

Exact measurement of the heat carried away in the jacket cooling water requires facilities which frequently are not available on field installations, but a reasonably close approximation to both the heat loss and the work requirement can be obtained from theory, providing the temperature of the gas leaving the compressor is experimentally determined. Knowing the temperature and pressure at both suction and discharge, the actual state points can be readily determined from the tables of refrigerant properties and the entropies and enthalpies thereby evaluated. Then the energy dissipation to cooling water can be calculated approximately from the equation,

$$Q_j = W_r\,(\Delta s)\,T_{avg} \qquad (7)$$

where

Q_j = energy dissipated to cooling water, Btu per minute.

W_r = weight of refrigerant, pounds per minute.

Δs = entropy change between suction and discharge.

T_{avg} = average temperature of gas passing through compressor, Fahrenheit degrees, absolute.

The work of compression is then given by the equation:

$$(\text{hp}) = [W_r (h_d - h_{vs}) + Q_j] \div 42.42 \qquad (8)$$

where

hp = horsepower.
h_d = enthalpy of vapor at compressor discharge.
h_{vs} = enthalpy of saturated vapor entering compressor.

From the form of Equation 8 it would appear that an increase in the energy loss to the jacket would result in a greater power requirement since the Q_j term is additive; actually, however, computation will readily show that the effect of an increase in the Q_j term is to *decrease* the horsepower since the rate of decrease of enthalpy difference will, in every case, exceed the increase in heat loss. Thus compressor cooling is highly desirable as a method of reducing power consumption.

Influence of Superheating and Subcooling

The most common departure from conditions of the simple saturation cycle is that resulting from admission of superheated vapor to the compressor. Thermodynamically, superheat is undesirable since the enthalpy increase required to compress a vapor through a given pressure range increases with superheat. Further, superheated vapor leaving an evaporator is usually an indication that the suction pressure is lower than necessary. Under practical operating conditions, however, superheat is almost universally used as a means of assuring complete vaporization of the refrigerant going to the compressor. With modern compressors operating at high speed and with relatively small clearance space it is particularly necessary to avoid admission through the suction valves of liquid refrigerant.

Another common departure of actual systems from the simple saturation cycle occurs because of subcooling of refrigerant in the condenser. Thermodynamically such subcooling is advantageous since it increases the refrigerating effect without affecting the unit energy requirements of the compressor. Further, it can be shown that for a fixed ratio of condenser cooling water to refrigerant circulating rate the total compressor power requirements will be greater when operating simple saturation than when operating with maximum sub-cooling. What is even more surprising is that condenser pressure may be lower for the sub-cooling cycle than for the saturation cycle; this condition results from the fact that, for the same capacity on a heavily loaded condenser, the refrigerant flow rate is less when there is sub-cooling.

Because of the advantages attendant upon the use of sub-cooling, many methods are in use for obtaining some sub-cooling effect outside of the condenser. One common procedure is to use the cold vapor leaving the evaporator to cool the liquid flowing from condenser to expansion valve. In this case subcooling is realized at the expense of superheating the suction vapor and thermodynamic analysis will show at once that a definite loss will accrue. The only conditions under which such a system can be justified are those for which the vapor would, in any event, pick up a comparable degree of superheat while en route to the compressor; in this event the deliberate superheating, with useful subcooling as a result, is preferable to the useless superheating which would otherwise occur. In small compressors having large surface area in relation to volume, a definite gain is usually accomplished by such interchange, because for such units there would be considerable heating in any event. On very

large compressors the loss in volumetric efficiency would more than offset any gain, and the capacity would be reduced. Somewhere between these two extremes, the exact point depending on the type of compressor, location of valves, etc., the two factors would offset one another.

Another somewhat unusual subcooling cycle allows cold refrigerant from the downstream side of the expansion valve to cool liquid refrigerant from the condenser down to the evaporator temperature. In such a case the *expansion* valve becomes a simple pressure-reducing valve since there is no vapor formation—hence no expansion—during passage of the liquid refrigerant through it. This system is theoretically identical, from the standpoint of thermodynamic effectiveness, with the simple saturation cycle.

Clearance and Conventional Volumetric Efficiency

Clearance, like displacement, is a characteristic—usually fixed—of a given compressor. In some cases clearance pockets are provided which place within the operator's control the ability to alter the clearance of the machine, but most moderate size compressors are built with fixed clearance. By definition the clearance is the percentage of the volume swept by the piston which is represented by spaces in the end of the cylinder (including valve spaces, etc.) when the piston is at the end of its stroke.

Because of the trapping of high pressure vapor in the clearance space, and its subsequent re-expansion, the suction valves of the compressor do not open until the piston has completed part of its stroke. Hence the volume of fresh vapor introduced into the compressor per stroke is less than the volume swept by the piston. The ratio of actual volume of fresh gas to swept volume is, by definition, the conventional volumetric efficiency, CVE. In equation form,

$$(\text{CVE}) = 100 - V_c \left[\frac{v_s}{v_d} - 1 \right] \tag{9}$$

where

CVE = conventional volumetric efficiency.

V_c = clearance, per cent of volume swept by piston, which is contained in spaces at end of cylinder when piston is at end of stroke (clearance includes valve spaces, etc.)

v_s = specific volume of gas at compressor inlet.

v_d = specific volume of gas at compressor discharge.

Values of v_s and v_d can be obtained directly or by calculation from the tables of properties of refrigerants.

Influence of Wiredrawing and of Piping Losses

The pressure drop which occurs during passage of the refrigerant through suction and discharge valves of the compressor is known as wiredrawing. Its effect is equivalent to that of a reduction in the evaporator pressure (but without the disadvantage of reduced refrigerating effect) and an increase in condenser pressure; hence it is undesirable. In analyzing a cycle, wiredrawing can be taken into account since it amounts to the interposition of a small *expansion valve* between the state point of vapor leaving the evaporator and that of vapor at start of the compression process; a similar equivalent valve can be considered as interposed at the end of the compression process and before the state point corresponding to the condition of the superheated vapor in the discharge line.

In exactly the same way representation on the ideal cycle can be given to the pressure losses that occur in the connecting piping. In each case the entire loss of a given line can be treated as though it occurred during passage through an equivalent expansion (or pressure reducing) valve located at any convenient place in the line. Data to permit evaluation of line losses are given in a subsequent section of this chapter.

Complex Refrigeration Cycles

The preceding sections have dealt only with refrigeration systems in which there is but one evaporator. When two or more evaporators are required, and the pressures differ in each, much greater opportunity is afforded the engineer for obtaining large economies through selection of one of the more complex cycles. Consider, for example, the refrigeration requirements of an air conditioning system which is to cool a very large volume of 90 F outside air down to a conditioned temperature of 40 F. A simple saturation system, operating with evaporator temperature less than 40 F, would accomplish the desired purpose, but at the expense of excess power requirements since 50 per cent of the sensible cooling load could instead be handled by an evaporator operating at a temperature somewhat less than 65 F. The more effective procedure in this case would be to place two direct expansion coils in series, the first operating at a temperature less than 65 F and the second at a temperature below 40 F. In this way approximately one half of the total load would be picked up at the higher evaporator pressure and therefore need be raised through a much smaller thermal height. The theoretical advantage of such operation can be visualized from the increase in Carnot effectiveness; assuming that the condenser temperature is 100 F, the coefficient of performance (cop) of the low temperature evaporator is,

$$(\text{cop}) = (35 + 460) \div (100 - 35) = 7.63$$

while that of the higher temperature evaporator is,

$$(\text{cop}) = (60 + 460) \div (100 - 60) = 12.97.$$

Since the load is assumed to be equally distributed between the two evaporators the cop of the series system is the arithmetical average of the values for the two evaporators or, $(7.63 + 12.97) \div 2 = 10.30$. Thus use of the series cycle would afford a theoretical saving in power of approximately one third.

One common fallacy, with respect to complex systems, is the misconception that a high evaporator pressure necessarily means a low power requirement. In many instances operating conditions will require use of series evaporators, but in a cycle for which the vapor leaving the higher pressure evaporator must be throttled to the pressure of the low pressure evaporator before entering the compressor, there obviously is no advantage resulting from the higher operating pressure of the one evaporator, since the refrigerant which it handles must be compressed through the same *lift* as though both evaporator pressures were the same. Consideration of this case brings out the fact that the effectiveness of a complete cycle depends upon the possibility of operating the system with suction vapor at different pressures. This can be accomplished through use of more than one compressor, or by means of special individual compressor arrangements which permit use of different suction pressures in the opposite ends of a double-acting machine, or introduction of vapor at two different pressures into the cylinder of a dual-effect compressor.

TABLE 8. PRESSURE LOSSES IN DICHLORODIFLUOROMETHANE DISCHARGE OR HOT GAS LINES[a]

CAPACITY BTU PER HOUR	PRESSURE DROP IN POUNDS PER SQUARE INCH PER 100 FT[b]									
	LINE SIZES, INCHES									
	⅝	⅞	1⅛	1⅜	1⅝	2⅛	2⅝	3⅛	3⅝
10,000	2.3	1.0	0.6							
15,000	4.9	2.0	1.0							
20,000	8.5	3.4	1.7	0.6						
25,000		5.3	2.6	0.9						
30,000		7.5	3.6	1.2	0.5					
40,000			6.4	2.1	0.7					
50,000			9.8	3.1	1.0	0.5				
60,000				4.4	1.3	0.7				
70,000				6.0	1.9	0.9				
80,000				8.0	2.5	1.1				
90,000				10.2	3.1	1.4				
100,000					3.8	1.7	0.5			
125,000					6.0	2.6	0.7			
150,000					8.5	3.8	1.0			
175,000					11.6	5.1	1.3			
200,000						6.7	1.7	0.6		
250,000						10.4	2.6	0.9		
300,000							3.7	1.2	0.5	
400,000							6.7	2.2	0.9	
500,000							10.5	3.5	1.5	0.7
600,000								5.0	2.1	1.0
800,000								9.0	3.8	1.8
1,000,000									5.8	2.9
1,250,000									9.5	4.4
1,500,000										6.4
2,000,000										11.3

[a]Soft annealed copper tubing up to and including ⅞ in. outside diameter. Hard copper pipe ⅛ in. outside diameter and larger.

[b]Length of tubing includes the average number of fittings.

Compound Compression Cycles

In large systems the compression process can be carried out in steps as the refrigerant passes through a number of cylinder ends arranged for operation in series. Thermodynamically the advantage of compound compression arises from the fact that intercoolers can be placed between the stages of compression to extract heat from the vapor and thereby cause the over-all compression process to more closely approach the ideal condition of isothermal compression. Essentially, such intercoolers—whether of the water or the flash refrigerant type—serve the same purpose as a cooling jacket, but with greater effectiveness because of the more satisfactory heat transfer conditions.

Multiple Expansion Valves

In the simple saturation cycle the saturated liquid entering the expansion valve commences to vaporize as soon as its pressure starts to drop. The vapor produced during the expansion process has no further use, in terms of refrigerating effect, since it has already picked up its latent heat of vaporization as a result of heat which it has extracted from the unvaporized residue. Thus the instant such vapor forms, its usefulness is at an end, and to allow such material to undergo a further drop in pressure is uneconomical. Unfortunately, however, there is no effective means of extracting vapor continuously during the expansion

TABLE 9. PRESSURE LOSSES IN DICHLORODIFLUOROMETHANE LIQUID REFRIGERANT LINES

CAPACITY BTU PER HOUR	PRESSURE DROP IN POUNDS PER SQUARE INCH PER 100 FT[a]			
	PIPE SIZES, INCHES			
	⅜	1⅛	1⅜	1⅝
100,000	0.6			
125,000	0.9			
150,000	1.3			
175,000	1.8			
200,000	2.3	0.6		
225,000	2.9	0.8		
250,000	3.6	1.0		
275,000	4.3	1.2		
300,000	5.1	1.4		
325,000	5.9	1.6		
350,000	6.9	1.8		
375,000	7.9	2.1		
400,000	9.0	2.3	0.8	
450,000		2.9	1.0	
500,000		3.5	1.3	
550,000		4.3	1.5	0.7
600,000		5.0	1.8	0.8
700,000		6.7	2.4	1.1
800,000		8.7	3.1	1.4
900,000			3.9	1.7
1,000,000			4.7	2.1
1,200,000			6.7	3.0
1,400,000			9.0	4.0
1,600,000				5.1
1,800,000				6.3
2,000,000				7.9
2,200,000				9.2

[a]Length of tubing includes the average number of fittings.

and re-compressing it. Thus in the simple cycle the flash vapor must necessarily be allowed to drop to evaporator pressure.

When a compound compression cycle is used there is at least one intermediate pressure at which flash vapor can be extracted. In such cases all refrigerant from the condenser can be dropped through a first expansion valve to the higher suction pressure and the flash vapor then extracted and returned to the compressor. Some of the resultant liquid refrigerant then passes through the high-pressure evaporator while the remainder proceeds through a second expansion valve in which its pressure is dropped to the valve corresponding to the low-pressure evaporator.

Pipe Sizes and Friction Losses

The effect on performance of pressure losses in the piping of a refrigerating system has already been discussed. In all cases frictional losses should be kept to a minimum and piping should be selected which will give the smallest loss consistent with over-all economy of the system. Actual losses vary, of course, with the physical characteristics of the particular refrigerants, but, by way of example, data will be given for one of the refrigerants, dichlorodifluoromethane (F-12) which finds wide use in air conditioning applications.

Tables 8, 9, and 10 give the pressure loss per 100 ft of piping (including an *average* number of fittings) for oil-free dichlorodifluoromethane;

TABLE 10. PRESSURE LOSSES IN DICHLORODIFLUOROMETHANE SUCTION REFRIGERANT LINES

COPPER PIPE ACTUAL O.D. INCHES	CAPACITY BTU PER HOUR	PRESSURE DROP IN POUNDS PER SQUARE INCH PER 100 FT[a]						
		REFRIGERANT TEMPERATURE F DEG						
		−10	0	10	20	30	40	50
⅜	2,000	0.3	0.3	0.2	0.2	0.2	0.1	0.1
	4,000	1.3	1.0	0.8	0.7	0.6	0.5	0.4
	6,000	2.8	2.2	1.8	1.5	1.2	1.0	0.9
	8,000	4.8	3.8	3.1	2.6	2.1	1.8	1.5
	10,000	7.4	5.8	4.8	3.9	3.3	2.8	2.3
	12,000	10.5	8.4	6.8	5.6	4.7	4.0	3.3
	14,000	14.0	11.0	9.1	7.6	6.4	5.4	4.5
	16,000		14.5	12.0	9.8	8.3	7.0	5.8
	18,000			15.0	12.3	10.4	8.7	7.2
	20,000				15.0	12.7	10.7	8.9
⅛	7,000	0.4	0.3	0.3	0.2	0.2	0.2	0.1
	10,000	1.0	0.7	0.5	0.5	0.4	0.3	0.3
	15,000	1.9	1.5	1.2	1.0	0.8	0.7	0.6
	20,000	3.3	2.6	2.1	1.7	1.4	1.2	1.0
	25,000	5.0	4.0	3.2	2.7	2.2	1.9	1.6
	35,000	9.7	7.7	6.2	5.1	4.3	3.6	3.0
	45,000	15.8	12.6	10.0	8.4	7.0	5.9	4.9
	60,000				14.8	12.2	10.2	8.6
	70,000						14.0	11.7
⅜	10,000	0.3	0.2	0.2	0.2	0.1	0.1	0.1
	15,000	0.7	0.5	0.4	0.3	0.3	0.2	0.2
	20,000	1.2	0.9	0.7	0.6	0.5	0.4	0.4
	30,000	2.6	2.1	1.6	1.3	1.1	0.9	0.8
	40,000	4.6	3.6	2.8	2.3	1.9	1.6	1.4
	50,000	7.0	5.5	4.4	3.5	2.9	2.5	2.1
	60,000	10.0	7.8	6.2	5.0	4.2	3.5	3.0
	80,000		14.0	11.0	8.7	7.3	6.2	5.2
	100,000				13.5	11.3	9.5	8.2
½	30,000	1.6	1.3	1.0	0.8	0.7	0.6	0.5
	40,000	2.7	2.1	1.7	1.4	1.1	0.9	0.8
	50,000	4.2	3.2	2.5	2.1	1.7	1.4	1.2
	60,000	6.1	4.5	3.6	2.9	2.4	2.0	1.7
	70,000	8.7	6.3	4.8	3.8	3.1	2.6	2.2
	80,000		8.4	6.3	4.9	4.0	3.3	2.8
	90,000			8.0	6.2	4.9	4.1	3.5
	100,000			10.0	7.6	6.1	5.0	4.2
	120,000					8.6	7.0	5.9
	140,000						9.5	7.9
⅝	50,000	0.7	0.5	0.4	0.3	0.3	0.2	0.2
	100,000	2.6	1.8	1.4	1.1	0.9	0.8	0.7
	150,000	5.6	3.9	3.0	2.4	2.0	1.6	1.4
	200,000	9.8	6.7	5.2	4.1	3.4	2.8	2.4
	250,000	14.8	10.3	8.0	6.3	5.1	4.2	3.6
	300,000		14.5	11.3	9.0	7.2	6.0	5.0
	350,000		19.5	15.3	12.0	9.7	7.8	6.7
	400,000			19.6	15.3	12.5	10.0	8.5

[a]Length of tubing includes the average number of fittings.

tabular values should be increased if oil is flowing with the refrigerant. For copper pipe the tables are for type L tubing and are based on the outside diameter.

Common practice fixes suction line velocities between 1,500 and 3,000 fpm while 2,000 to 3,500 fpm is the accepted range for discharge lines. Velocities higher than those indicated will result in noisy operation while lower velocity in the suction line may result in the loss of entrained oil. Refrigeration for air conditioning usually involves wide variation in load, requiring double suction risers, one large and one small. The large riser should be trapped to insure oil return while the small riser should be

TABLE 10. PRESSURE LOSSES IN DICHLORODIFLUOROMETHANE SUCTION REFRIGERANT LINES (CONCLUDED)

COPPER PIPE ACTUAL O.D. INCHES	CAPACITY BTU PER HOUR	PRESSURE DROP IN POUNDS PER SQUARE INCH PER 100 FT[a]						
		REFRIGERANT TEMPERATURE DEG F						
		−10	0	10	20	30	40	50
2⅝	50,000	0.2	0.2	0.1	0.1	0.1	0.1	0.1
	100,000	0.7	0.6	0.5	0.4	0.3	0.2	0.2
	150,000	1.6	1.2	1.0	0.8	0.6	0.5	0.4
	200,000	2.8	2.1	1.7	1.4	1.1	0.9	0.7
	250,000	4.3	3.4	2.6	2.1	1.7	1.3	1.1
	300,000	6.1	4.5	3.7	3.0	2.4	1.9	1.5
	350,000	8.2	6.0	5.0	4.0	3.2	2.5	2.0
	400,000		7.8	6.5	5.1	4.2	3.3	2.7
	450,000			7.7	6.4	5.3	4.0	3.5
	500,000				7.8	6.4	5.0	4.2
	550,000					7.7	6.2	5.1
	600,000						7.4	6.2
3⅛	200,000	1.2	1.0	0.8	0.6	0.5	0.4	0.4
	300,000	2.6	2.0	1.6	1.3	1.0	0.8	0.7
	400,000	4.5	3.4	2.6	2.1	1.7	1.4	1.3
	500,000	7.3	5.4	4.1	3.3	2.7	2.2	1.9
	600,000		8.1	6.0	4.7	3.8	3.1	2.7
	700,000			8.4	6.5	5.2	4.2	3.5
	800,000				8.6	6.8	5.5	4.6
	900,000					8.7	7.0	5.9
	1,000,000						8.9	7.3
3⅝	300,000	1.2	0.9	0.7	0.6	0.5	0.4	0.3
	400,000	2.0	1.6	1.3	1.0	0.8	0.7	0.6
	500,000	3.2	2.5	1.9	1.6	1.3	1.0	0.9
	600,000	4.6	3.6	2.8	2.2	1.8	1.5	1.3
	700,000	6.4	4.9	3.8	3.0	2.5	2.0	1.7
	800,000	8.7	6.4	4.9	3.9	3.2	2.5	2.2
	900,000		8.2	6.2	4.9	3.9	3.2	2.7
	1,000,000			7.7	6.1	4.9	4.0	3.3
	1,100,000			9.4	7.3	5.8	4.8	4.0
	1,200,000				8.7	6.9	5.6	4.8
	1,300,000					8.0	6.6	5.6
	1,400,000					9.3	7.6	6.4
4⅛	400,000	1.0	0.8	0.6	0.4	0.4	0.3	0.3
	600,000	2.4	1.8	1.4	1.1	0.9	0.7	0.6
	800,000	4.1	3.1	2.4	2.0	1.6	1.3	1.1
	1,000,000	6.6	4.8	3.7	3.0	2.5	2.0	1.6
	1,200,000	10.0	7.1	5.4	4.4	3.5	2.9	2.4
	1,400,000		10.0	7.5	5.9	4.8	3.9	3.3
	1,600,000			10.0	7.7	6.2	5.1	4.2
	1,800,000				10.0	7.9	6.4	5.3
	2,000,000					9.7	7.9	6.6
	2,200,000						9.5	7.9

[a]Length of tubing includes the average number of fittings.

sized for a velocity of 3,000 fpm at minimum load; and the large riser then sized to handle the balance of the load at a velocity not less than 2,000 fpm. The total pressure loss in the suction piping, including valve losses, is usually between 2 and 3 psi while hot gas line losses are held to approximately 4 psi and liquid line losses are not greater than 5 psi.

As protection against re-condensation on the cylinder head of the compressor, a surge drum is sometimes installed in the discharge line close to the compressor; this protection is especially desirable on systems using evaporative condensers where sun effect during shut-down may be serious.

The Air Refrigeration Cycle

Fundamentally, the air refrigeration cycle is essentially the same as the vapor cycle. The only important difference is that, since air does not change phase between the compressor and the expansion valve, it is necessary—and is also advantageous—to replace the expansion valve with an expanding engine. There is no temperature change in a perfect gas (and air approaches in behavior such a gas) during a constant enthalpy pressure reduction and hence an expansion valve of the usual type would be ineffective as a means of achieving low temperature in an air system. By utilizing an expander, however, the desired temperature drop is obtained, and, with it, a release of a considerable amount of energy as shaft work. In most air systems the expander and the compressor are so

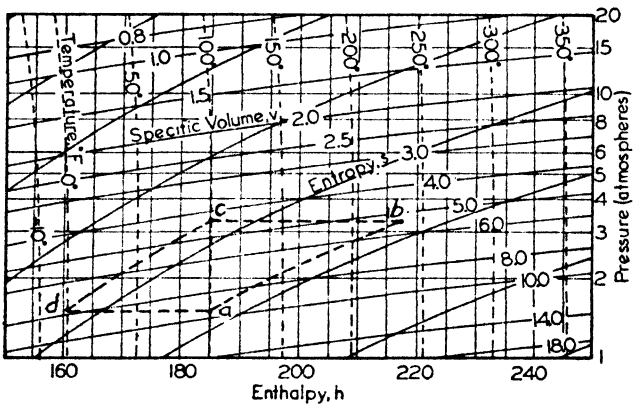

FIG. A. PRESSURE ENTHALPY DIAGRAM FOR DRY AIR

connected that work coming from the expander is supplied to the compressor and the remaining compressor work requirements are then made up from some external energy source.

For vapor cycles work could also be obtained by using an expander in place of an expansion valve, but since material going to the expander would be in liquid form the amount of energy released during the pressure drop (and partial evaporation due to flash) would be relatively small and in most cases insufficient to justify the increased first cost and complexity of the expander.

Fig. A shows the most important working section of a pressure-enthalpy chart for dry air. A typical air cycle is shown by the heavy dashed lines forming the abcd area. Dry air at 100 F and 7 psig (1.5 atmospheres) enters the compressor at a with enthalpy of 185 Btu per pound and is compressed isentropically to the discharge point b where its pressure is 35 psig (3.3 atmospheres), enthalpy 218 Btu per pound and temperature 240 F. From b this hot, high pressure air passes through a cooler in which its temperature and enthalpy are reduced (at constant pressure) to the initial values; point c gives the state of the air leaving the cooler. If, now, this air were allowed to pass through an expansion valve its state at discharge would be a and no refrigerating effect would be available. Actually the air at c goes through an isentropic expander and leaves at state d with enthalpy and temperature of 161 Btu per pound and 0 F.

The refrigerating effect for the cycle shown is enthalpy at a − enthalpy at d = 24 Btu per pound.

The work input to the compressor is 218 − 185 = 33 Btu per pound.

The work obtained from the expander is 185 − 161 = 24 Btu per pound.

The net work required for the cycle is then 33 − 24 = 9 Btu per pound of air per minute.

The coefficient of performance (cop) is 24/9 = 2.67.

The air circulating per ton of load is 200/24 = 8.3 lb per minute.

The power requirement is 9/42.42 = 0.21 hp per pound of air or 0.21 × 8.3 = 1.75 hp per ton.

The example given, based on isentropic compression and expansion, gives a simple and conservative method of checking an air cycle. In practice, better economy is obtained if the compression process approaches isothermal rather than isentropic; the expander preferably operates isentropically. To reduce the size of the expanding cylinder and to avoid frosting difficulties, the air system usually operates with a low

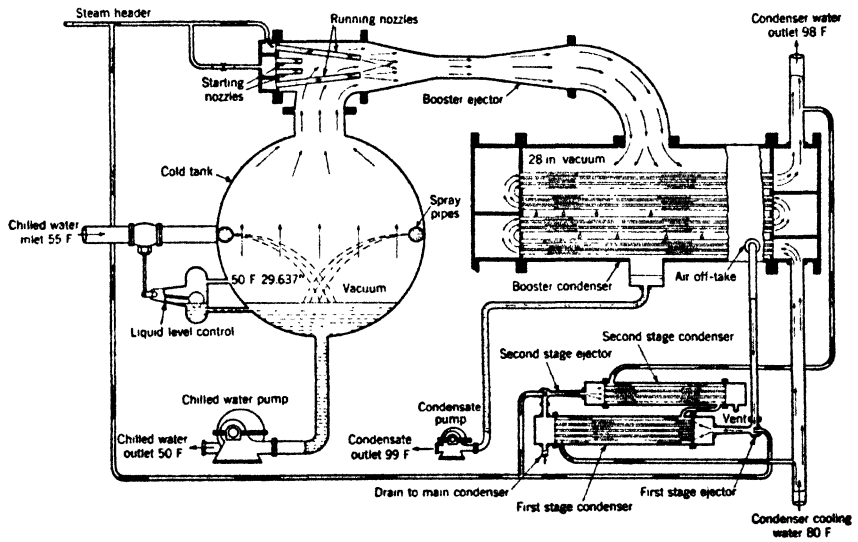

FIG. 2. DIAGRAMMATIC ARRANGEMENT OF STEAM JET VACUUM COOLING UNIT

pressure somewhat more than atmospheric. The usual compression ratio is about 4.

The principal advantage of the air system is that its refrigerant (air) is inexpensive and non-toxic. Serious disadvantages are size and cost of equipment and such a low coefficient of performance, that air refrigeration has no commercial importance today.

The Steam Jet System

The steam jet system under certain circumstances is desirable for use in air conditioning[1]. Steam supplies directly the power used for compressing the refrigerant, thus eliminating the losses connected with other methods of supplying energy. As the compression ratio between the evaporator and condenser under normal circumstances is large, the mechanical efficiency of the equipment is somewhat lower than that of the positive mechanical type compressor. The condensing water requirements are considerably greater, as both the refrigerant and the impelling steam must be condensed.

The steam jet system functions on the principle that water under high vacuum will vaporize at low temperatures. Steam jet boosters or com-

pressors of the type commonly used in power plants for various processes will produce the necessary low absolute pressure to cause evaporation of the water.

A diagrammatic representation of a typical steam ejector water cooling system is shown in Fig. 2. The figures correspond to an average representative system. The water to be cooled enters the evaporator and is cooled to a temperature corresponding to the vacuum maintained. Because of the high vacuum, a small amount of the water introduced in the evaporator is flashed into steam. As this requires heat, and the only source of heat is the rest of the water in the evaporator tank, this other water is almost instantly cooled to a temperature corresponding to the boiling point determined by the vacuum maintained. The amount of water flashed into steam is a small percentage of the total water circulated through the evaporator, amounting to approximately 11 lb per hour per ton of refrigeration developed. The remainder of the water at the desired low temperature is pumped out of the evaporator and used at the point where it is required.

The ejector compresses the vapor which has been flashed in the evaporator, plus any entrained air taken from the circulated water, to a somewhat higher absolute pressure and the vapor and air mix with the impelling steam on the discharge side of the jet. The total mixture then passes from the ejector into the condenser.

The slight amount of air which may be entrained in the cooled water is removed by a small secondary ejector which raises the pressure sufficiently so that the air can be discharged to the atmosphere. A secondary condenser is then necessary to condense the steam in the secondary jet.

While a single booster of smaller than 15 tons capacity is difficult to build, steam jet vacuum cooling units have been built for as small as 5 to 6 tons capacity. They can readily be built for steam pressures of from 5 to 200 lb per square inch and condenser water temperatures as high as 90 F. The steam consumption in pounds per hour per ton of refrigeration increases rapidly as the booster steam pressure is lowered. For example, the lowering of the booster steam pressure from 200 to 90 lb per square inch results in an increase in steam consumption of approximately 5 per cent, whereas a further decrease in booster steam pressure to 10 lb per square inch increases the steam consumption by approximately 72 per cent over that required at 200 lb per square inch.

The capacity of a steam jet system is usually controlled by controlling the number of boosters in use since the unit usually has several boosters operating on the same evaporator. Usually one booster is automatically controlled whereas the others are manually operated. The capacity is dependent, as for all compressors, upon the evaporator temperature, or in other words, the suction pressure. For example, the capacity is lowered approximately 17 per cent if the evaporator or chilled water temperature is lowered from 50 to 45 F. The capacity therefore can be controlled to some extent by regulating the evaporator temperature.

The Absorption System

The work needed for operation of a compressor is given by the equation, Work $= \int PdV$. If the working fluid which is undergoing the pressure rise does not change in volume, the required energy input to the com-

pressor would be negligible; assuming no change in kinetic energy of material between entrance and exit of the compressor the only energy required would be that needed to increase the flow work of the fluid. Calculation will show that energy needed to raise 1 lb of ammonia from the pressure of a 0 F evaporator to that of an 85 F condenser is greater by more than 100 times when the vapor is directly compressed, as compared with energy requirements when it is first absorbed in water ($1\frac{1}{2}$ lb of water per pound of ammonia vapor) and then pumped to the higher pressure. Thus the essence of the absorption refrigeration cycle concept is the idea of raising the refrigerant pressure when the refrigerant is in liquid rather than vapor form.

The absorption and compression refrigeration cycles differ only with respect to the method of compression. Each cycle requires a condenser,

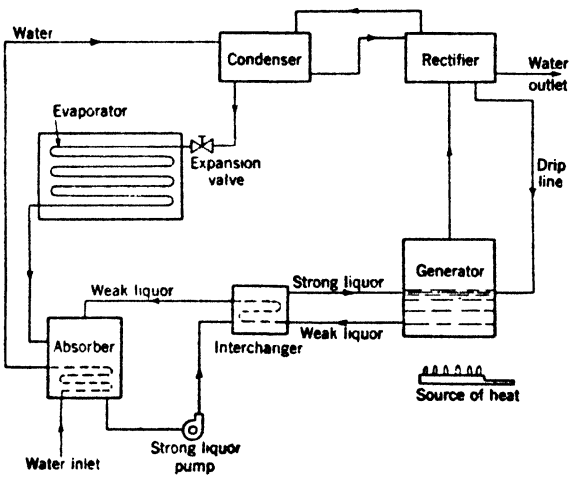

FIG. 3. CLOSED ABSORPTION SYSTEM

expansion valve, and evaporator, but the absorption cycle utilizes three major equipments in place of the mechanical compressor; these equipments are the *absorber*, the *pump*, and the *generator*. Vapor from the evaporator is absorbed by a low temperature absorbent fluid which is then pumped to the generator where heat is supplied to boil off the refrigerant. The absorbent is now cooled and readmitted, through a pressure-reducing valve, to the absorber.

In addition to the three primary equipments of the absorption cycle it is necessary to provide auxiliary equipment, usually an analyzer and a rectifier, to remove from the refrigerant leaving the generator, insofar as is possible, the absorbent which vaporizes and leaves the generator with the refrigerant. Removal of this material is of great importance to effective operation of the system, since even a small concentration of absorbent in the refrigerant will suffice to reduce greatly the evaporator pressure required for maintenance of a given evaporator temperature. Thermodynamic analysis of absorption cycles is relatively complex and requires the use either of tables or graphs showing the equilibrium relationships and thermodynamic properties of the refrigerant-absorbent combination. Data of this kind are available in bibliography item 1 and a discussion of various absorbents is given in bibliography item 6.

Thermodynamically the effectiveness of a refrigerant-absorbent combination increases directly with its negative deviation from Raoult's Law.

Fig. 3 shows a typical absorption cycle flow diagram. Cooling water first goes through the absorber (where it extracts the heat of absorption which is liberated by the refrigerant vapor as it goes into solution), then through the condenser, and finally through the rectifier. Refrigerant from the evaporator enters the absorber where it goes into solution in the absorbent; the high concentration solution is then pumped to the generator where heat is supplied; the refrigerant (with some absorbent vapor) leaves for the rectifier and the warm low concentration solution is returned to the absorber. In the rectifier selective condensation occurs, the concentration of the absorbent in the condensate being much greater than its concentration in the entering vapor mixture; rectifier condensate is dripped back to the generator.

The total energy requirements of an absorption cycle greatly exceed those of a compression system, but the energy required is of low availability (heat) in contrast with the high availability requirements (shaft work) of the mechanical compressor. Thus in localities where heat and cooling water are obtainable at low cost, it will be more economical to use a large quantity of inexpensive thermal energy in preference to a much smaller quantity of expensive shaft energy. For most absorption systems the heat required will be from one and one-half to five times as much as the heat extracted in the evaporator; cooling water requirements are proportionally high.

Ice Systems

Cold water systems using ice as the cooling agent have been installed in many theaters, restaurants, funeral homes, churches and other places where short hours of operation and high peaks of cooling demand make this type of system desirable. A comparatively small quantity of ice in the water cooling tank of such a system can release refrigeration at a relatively rapid rate. For instance, neighborhood theaters having a peak demand of 1,200,000 Btu per hour (100 tons refrigeration) have found 8 ton capacity ice bunkers satisfactory.

In operation, the water in the air conditioning system is circulated over ice placed in an insulated box and is cooled to the 38 or 40 F range or higher if desired. This cold water is pumped from the ice bunker to air cooling coils or spray type air washers. The blowers, coils, air washer or air handling sections are the same as those parts in any system employing cold water as a refrigerant.

The ice water cooler or ice bunker is usually built at the installation in a location where it can easily be iced. It can be constructed of any desired material such as concrete, steel, or wood with an adequate amount of insulation to save the ice from one period of use to the next. The basic requirement is that the tank be durable and water tight. A typical bunker with connections to a coil type air conditioning system is shown in Fig. 4. About 60 cu ft of gross bunker volume are allowed per ton of ice capacity.

The shape of the bunker usually conforms to the available space. The one illustrated has overhead sprays, but if head-room is lacking the ice is placed on the floor of the bunker with the water returned around the lower part of the blocks from a perforated distribution pipe run along one

side of the bunker. To secure good circulation the supply water is extracted from a similar perforated pipe on the opposite side of the bunker.

The temperature of the water is controlled at a predetermined point by a thermostat in the supply line. If the temperature drops too low, a part of the return water is by-passed directly to the sump and is not cooled over the ice. In the larger systems it is customary to install an overflow control which, as the ice melts, discards the excess water through an economizer coil. The surface of the economizer is large in relation to the flow so that the water is warmed to 60 F or more as it is discharged from the system.

Storage Systems

In an attempt to lower initial equipment cost and operating expense, or increase the refrigeration capacity of an existing air conditioning

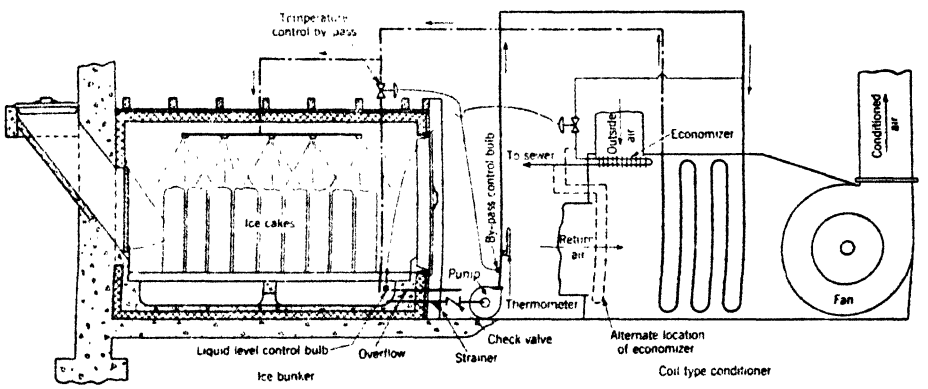

FIG. 4. TYPICAL ICE SYSTEM SHOWING BUNKER DETAILS

system, storage refrigeration has been utilized in a few applications. Some of the methods which have been adopted include the storage of refrigeration in the form of chilled water, chilled brine, ice on evaporator coils[2] and the accumulation of thin sheets of ice on copper plates in a steel tank[3]. If the peak load factor is low as compared with a long period of operation, such as in a restaurant, or if the hours of operation are short but the usage factor high as in a church, then it is possible to consider storage refrigeration. This method of accumulating refrigeration frequently makes it possible to use low cost off-peak electric power. Power costs may also be reduced by installing a smaller refrigeration plant, augmented by a storage system, and by operating it for longer periods.

The Reverse Cycle

The reverse cycle—frequently referred to as a *heat pump*—is identical in theory with the ordinary refrigeration cycle and differs only in the sense that the desired effect is a heat source rather than a heat sink. Since a condenser delivers more heat than is picked up by the evaporator (it discharges the heat equivalent of work supplied during compression) it follows that the effectiveness of a heat pump, its coefficient of perform-

ance, is greater than that of a refrigeration cycle operating between the same temperature limits.

In heating by the reverse refrigeration cycle energy is absorbed in an evaporator from some available source of heat, pumped to a higher temperature and delivered to a condenser[4]. The heat from the condenser is used for heating purposes. The compressor acts as a heat pump whose fundamental function is to raise the potential of the heat. The theoretical ratio of the heat delivered to the work of compression, the coefficient of performance, is given in Equation 10.

$$(\text{cop}) = \frac{T_c}{T_c - T_s} \tag{10}$$

where

cop = coefficient of performance.

T_s = absolute temperature of evaporator.

T_c = absolute temperature of condenser.

Thus, with a small spread of temperature between the evaporator and the condenser, 6 or 8 times as much heat may be obtained theoretically, and 3 to 5 times practically, as the work introduced. There are a number of limitations, however, the most serious of which is the lack of ready availability of a practical source of heat.

1. Well water is the most desirable since its temperature is higher than other sources even in the winter, and thus a large amount of heat may be removed in relation to the weight of water handled.

2. Air may be used but its specific heat is low and its temperature uncertain. When the most heat is needed, the temperature of the air is lowest, thus resulting in the least favorable temperature combination.

3. It has been proposed to obtain heat by freezing water but this is still in the experimental stage.

Some of the other factors which act as limitations are: the large temperature spread when using air as a source of heat and when attempting to cool with even moderately low outside temperatures, the frequent disparity between the size of the cooling load and heating load requiring extra equipment for a complete heating load, and the relatively high initial cost of equipment as compared to that at present available for heating by conventional means.

Because of these limitations, the present application of the system is largely limited to temperate climates, such as Florida and Southern California, or to heating only for intermediate seasons, or to other localities which have peculiar advantages as, for instance, the ready availability of well water. In these locations it is frequently possible to do all of the heating necessary with the refrigeration equipment so that the extra cost is only that of reversing the functions of the condenser and evaporator.

There are a number of reversed systems now in operation, particularly among utility companies, using well water as the source of heat. These systems range in size up to 320 hp. In the case of the largest system in operation at present, the cost of the electrical energy would have to be approximately 0.7 cents per kilowatthour in order to compete with oil at 6 cents per gallon.

A typical arrangement of a reversed cycle conditioning system where air is used as a source of heat is shown in Fig. 5. If the air seldom drops

below freezing, heat is often required in the morning and cooling during the afternoon in order to maintain comfortable conditions in such a system. The arrangement as shown lends itself to automatically changing over as required.

REFRIGERATION EQUIPMENT AND ARRANGEMENTS

Types of Compressors

There are many different types of compressors, using various refrigerants. Each type has its advantages for its particular application, and those generally used for air conditioning are of the following types:

1. Reciprocating compressors (commonly referred to as piston type).
2. Centrifugal compressors.

Reciprocating compressors are available in a wide range of sizes and types. Any of a number of refrigerants, including dichlorodifluoromethane

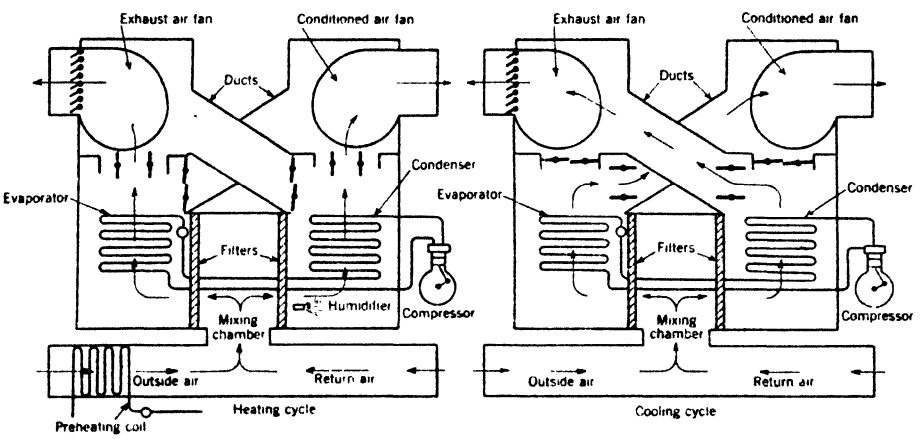

FIG. 5. SCHEMATIC OPERATION OF REVERSED CYCLE CONDITIONING SYSTEM

(F-12), methyl chloride, ammonia, carbon dioxide, and sulphur dioxide may be used in reciprocating machines. The first of these is used extensively in direct expansion systems of comfort air conditioning.

Compressors may be classified into two general types, (*a*) open type, (*b*) enclosed type. If the driving mechanism is external to the compressor, then the shaft must be brought out through the crankcase and a shaft seal or stuffing box must be used to prevent escape of the refrigerant. This type of compressor is known as an open-type compressor. When the driving mechanism is located within the crankcase of the compressor in such a way as to avoid the necessity of a shaft seal, the compressor is known as the completely enclosed or hermetically sealed type.

Open-type compressors may be further classified as belt driven and directly connected. A great number of direct-driven units are now being used which generally operate at higher rotational speeds than the belt-driven type.

The present tendency is toward forced lubrication of the bearings of compressors by means of an oil pump driven from the crankshaft, although there are many splash lubricated compressors on the market. The chief

advantages of the forced lubricated compressor are that the lubrication system requires less energy for its operation than the splash type, the oil can be easily filtered before it enters the bearings, and less oil is usually required.

The compressor capacity must be selected for and matched to the maximum load for the installation on which it is to be used. Air-conditioning loads, however, vary over a wide range, and a wide fluctuation in air conditions may result during periods of light load if on-and-off control of full compressor capacity is used. To prevent such undesirable fluctuation, several methods are employed to vary the capacity of reciprocating compressors, such as:

1. By-passing one or more cylinders, of a multi-cylinder compressor, from discharge to suction.

2. Rendering the suction valves of one or more cylinders of a multi-cylinder compressor inoperative. This is usually accomplished by depressing the suction valves.

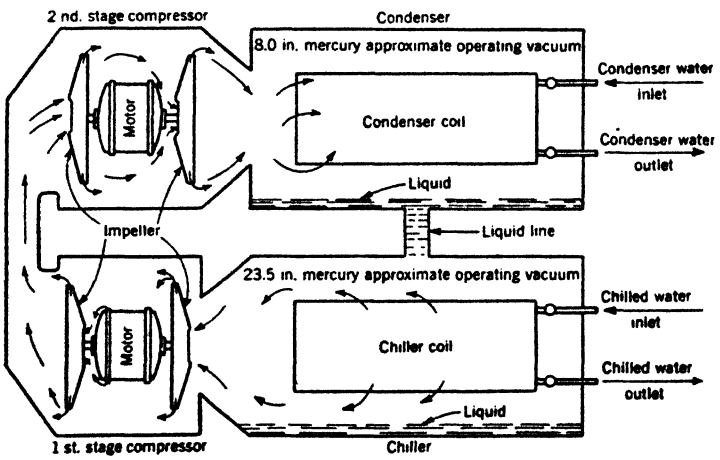

FIG. 6. ENCLOSED TYPE CENTRIFUGAL CONDENSING UNIT

3. Varying the speed of the compressor, usually by using variable speed or two-speed electric motors.

4. Using clearance pockets to control the quantity of refrigerant pumped.

5. Restricting the suction inlet to one or more of the cylinders of a multi-cylinder compressor either by an automatic modulating valve or by an *on* and *off* valve.

All of these methods, with the exception of variable speed, result in a slightly lower over-all compressor efficiency when in use, since the mechanical losses remain constant whereas the quantity of refrigerant pumped is lower.

Centrifugal compressors are used with very low pressure refrigerants; usually both evaporator and condenser work below atmospheric pressure. Water and monofluorotrichloromethane (F-11) are the refrigerants commonly used in centrifugal machines.

Compression of the refrigerant is accomplished by means of centrifugal force; therefore, this type of compressor is inherently suitable for large volumes of refrigerant at low pressure differentials. Two or more stages are usually required and high speeds are necessary to obtain good efficiency.

The evaporator is usually constructed as an integral part of the centrifugal type condensing unit, to chill water which is then circulated to the air conditioning system. This is done because it would not be economical to pipe these large volumes of refrigerant any distance.

Centrifugal compressors like reciprocating compressors can be divided into two general types, open and enclosed. In general, the open type compressor is geared to the driving mechanism, and operates at higher speed than the driving motor or turbine. A modern, completely enclosed, direct-driven centrifugal compressor is illustrated in Fig. 6.

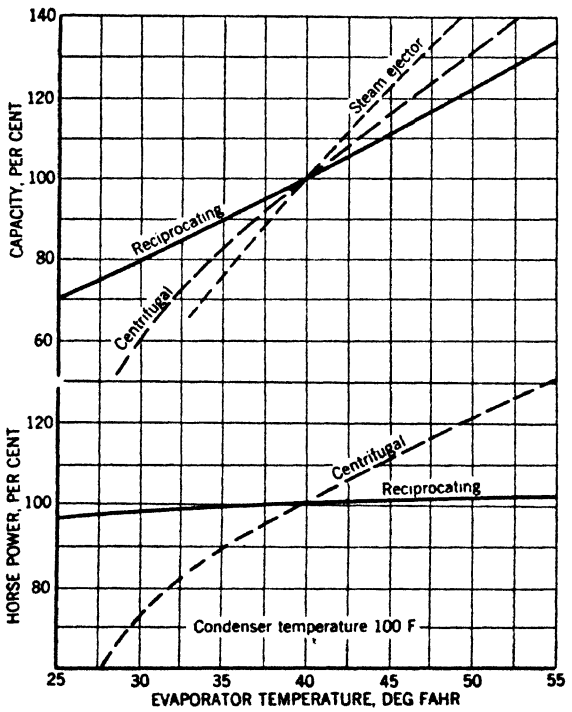

FIG. 7. PERFORMANCE CHARACTERISTICS OF COMPRESSION REFRIGERATION MACHINES AT CONSTANT SPEED

The compressor capacity can be varied by controlling the condensing pressure. This is accomplished by regulating the quantity and temperature of the condenser cooling water. The capacity falls off with increasing condensing pressure. Centrifugal compressors are seldom built for less than 50 tons capacity, since it is not practical to make impellers which pump much less than the volume of refrigerant required for this tonnage.

Characteristics of Compression Systems

The various types of compression systems have quite different characteristics of capacity and power with varying evaporator and condenser temperatures, as may be noted from curves in Figs. 7 and 8.

From Fig. 7 it may be observed that power requirements for the centrifugal compressor increase much more rapidly than for the reciprocating

compressor with increase in evaporator temperature. Similarly, the capacities of the steam ejector and centrifugal compressors increase more rapidly than those of the reciprocating compressor with increase in evaporator temperature. Thus, both the steam jet and centrifugal machines tend to be more self-regulating than the reciprocating. It is also evident from Fig. 7 that the steam jet equipment is best suited for operation at high evaporator temperatures.

The effect of condenser temperature upon the power and capacity of the different types of compressors is shown in Fig. 8. It may be noted that the power required by the reciprocating compressor increases rapidly with increase in condenser temperature, while the power curve for the

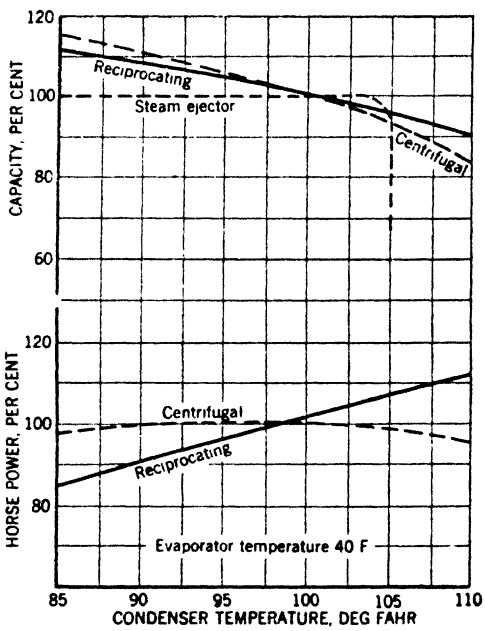

FIG. 8. PERFORMANCE CHARACTERISTICS OF COMPRESSION REFRIGERATION MACHINES AT CONSTANT SPEED

centrifugal compressor is relatively flat. It is also evident that the capacity of the steam jet compressor is independent of condenser temperature until a certain point is reached where it drops to zero. As previously stated, steam jet equipment requires more condensing water than other types of compression systems. Consequently, steam jet systems are well suited to those applications where condensing water is cheap, or where condensing water is rather high in temperature.

Condensers

Condensers used for liquefying the refrigerant are of three general designs: (1) *air cooled*, (2) *water cooled*, and (3) *evaporative* (combination air and water).

1. *Air cooled condensers* are seldom used for capacities above 3 tons of refrigeration, unless an adequate water supply is extremely difficult to obtain, as, for instance, in railway air conditioning. Even on fractional tonnage installations, air is used as the condensing medium only where

water is expensive or where simplicity of installation warrants the higher condensing pressure, and consequent higher power costs than would be obtained using water as the condensing medium.

The conventional air cooled condenser consists of an extended surface coil across which air is blown by a fan. The hot discharge gas enters the coil at the top and, as it is condensed, flows to a receiver located below the condenser. Air cooled condensers should always be located in a well ventilated space so that the heated air may escape and be replaced by cooled air.

The principal disadvantages of air cooled condensers are the power required to move the air and the reduction of capacity on hot days. This loss of capacity due to high condensing pressures on hot days requires that equipment of increased capacity be selected to meet the peak load. Thus at normal loads the equipment is oversized.

2. *Water cooled condensers* are of the double pipe type, the shell and tube type, or the shell and coil type. Double pipe condensers are arranged so that water passes through the inner of two concentric pipes and refrigerant circulates through the annular space between the pipes. Where possible, there should be counter-flow of the refrigerant and the condensing water to obtain maximum temperature differences. This type is usually used only with small condensing units.

The amount and temperature of the condensing water determine the condensing temperature and pressure, and indirectly the power required for compression. It is therefore necessary to determine a balance so that the quantity of water insures economical compressor operation.

Because there is a decided tendency to conserve the water in city mains and because most large cities are restricting the use of water for air conditioning and refrigeration equipment, it is often necessary to install cooling towers or evaporative condensers. Cooling towers, unfortunately, produce the warmest condensing water at the time when the load on the system is greatest, so that the refrigeration equipment must be designed to meet the maximum load at abnormal condensing water temperatures. If properly designed, this makes little difference in the efficiency of operation throughout the year except at those times when the condensing water temperature is highest. As this occurs only for 5 per cent of the entire cooling period it can be disregarded as a factor in establishing yearly operating costs.

The cooling tower has a certain advantage over the use of water from the city mains. Economies are possible when a cooling tower is used, which cannot be achieved by the use of condensing water from city mains. In certain localities, the lowest city water temperature during the summer months is from 65 to 70 F. This temperature range takes place for the entire cooling period, regardless of the outdoor temperature. With a cooling tower, the temperature of the condensing water may rise to 80 or 85 F under maximum conditions, but under less than maximum conditions the temperature of the water leaving the cooling tower drops considerably. It has been established that in these localities during 50 per cent of the time, the outdoor wet-bulb temperature varies from 60 to 70 F and the cooling tower water, for the same periods, varies from 65 to 75 F. When the outdoor wet-bulb temperature drops below 60 F, which occurs approximately 30 per cent of the time, the condensing water temperature is still lower. The cost of water used for condensing is small as the only water required is that used to make up the loss by evaporation

in the cooling tower itself. Refer to the section on Cooling Towers in Chapter 37.

Shell and coil condensers are in general use for medium sized condensing units, and consist of a coil of tubing mounted inside a shell. The cooling water passes through the coil.

3. *Evaporative condensers.* Due to the high cost of city water for condenser purposes, and due to ordinances in some localities prohibiting the discharge of large quantities of such water into the sewage systems,

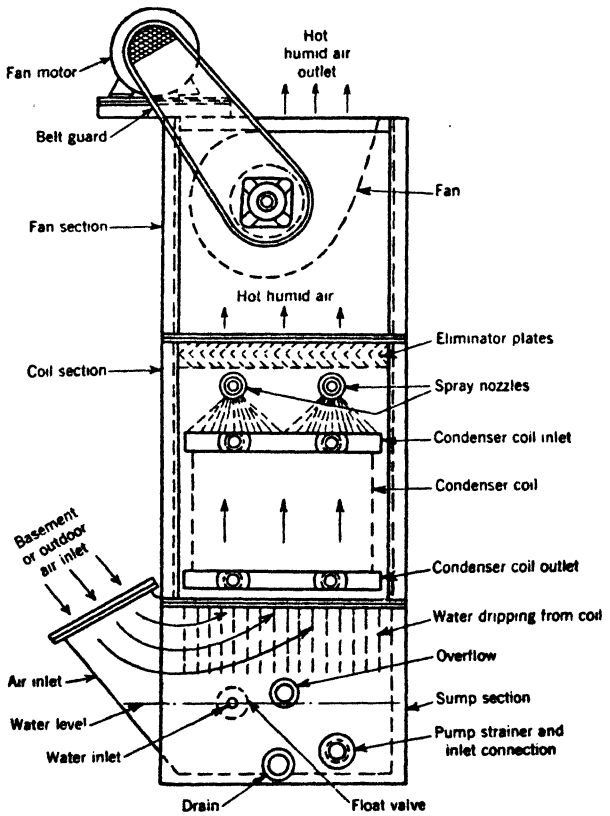

FIG. 9. SCHEMATIC VIEW OF AN EVAPORATIVE CONDENSER

there has been developed a condenser which uses a minimum amount of water on a finned surface, cooling it to approximately the wet-bulb temperature of the surrounding atmosphere.

The end view of a typical evaporative condenser is shown in Fig. 9. The fan draws the air over a finned tube condenser which is kept wet by a water spray. The discharge refrigerant gas from the compressor enters the top of the condenser coil and the liquid refrigerant is drained from the bottom of the coil into a liquid receiver and then circulates through the remaining portion of the system in the usual way.

The water is circulated through the spray nozzles and the level is maintained in the sump by means of a float valve. The eliminator plates are placed in the path of the water-air mixture so as to remove the

entrained water. The air leaving the unit is almost completely saturated, so that care must be taken in locating discharge ducts to prevent condensation.

Evaporative condensers are available in sizes up to 100 tons or more. These units use only a small portion of the water required for a water cooled condenser. The water is vaporized by the heat of the refrigerant so that each pound of water used extracts approximately 1000 Btu from the refrigerant, whereas under standard rating conditions where the water temperature rise is 20 F, each pound of water extracts only 20 Btu from the refrigerant. Including the water lost by entrainment in the discharge air, by overflow and stand-by evaporation, the water used is about 3 to 5 per cent of the amount that would be required for a water cooled condenser.

The evaporative condenser requires more maintenance, occupies greater space (must be located where air is available), and has a higher first cost than the water cooled condenser, but where the use of water is restricted

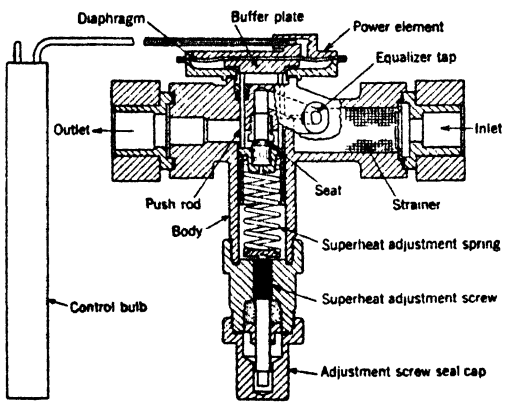

FIG. 10. TYPICAL THERMOSTATIC EXPANSION VALVE

or expensive, the evaporative condenser has become widely accepted. Compared with a water cooled condenser and cooling tower, which combination uses about the same quantity of water, the evaporative condenser has the advantage of lower cost and smaller space requirements.

Expansion Valves

The thermostatic expansion valve is a device to regulate the flow of liquid refrigerant so that the evaporator will always be used to best advantage. The evaporator coil must be kept as full as possible without any chance of liquid refrigerant entering the suction line. The expansion valve accomplishes this by regulating the supply of refrigerant, so that the temperature of the gas leaving the evaporator is always slightly higher than the temperature of the boiling refrigerant inside of it. This difference in temperature between the outgoing (suction) gas and the liquid refrigerant in the evaporator is called the superheat of the gas.

The operation of the thermostatic expansion valve can best be explained by means of a diagram, Fig. 10. A small refrigerant charge in the control bulb exerts a pressure through the tube to the upper side of the diaphragm, which tends to open the valve.

The magnitude of this pressure is determined by the temperature of the suction gas leaving the evaporator, as the control bulb is attached to the suction line at this point and is at approximately the same temperature. The suction pressure in the evaporator is transmitted through the equalizer tube and exerts an opposing force on the other side of the diaphragm in the direction to close the valve. This pressure corresponds to the temperature of the boiling refrigerant. The resulting force on the diaphragm is determined by the differential between the temperature of the suction gas and the boiling point of the refrigerant, which is the amount of superheat in the gas. If this temperature differential becomes greater (superheat increases), the resultant force on the diaphragm opens the valve and admits more refrigerant. The reverse is true if the superheat decreases, and the valve partly closes, thus admitting less refrigerant. The spring keeps the valve closed until the resultant force on the diaphragm corresponds to the desired superheat. The adjustment of the spring will change the amount of superheat to be maintained in the suction gas.

The selection of the expansion valve is, of course, determined by the capacity of the valve. The capacity of a valve with a given orifice is determined by the refrigerant used, the differential of pressure across the valve, and the amount the liquid is sub-cooled as it enters the valve. The expansion valves are usually rated at zero sub-cooling of the liquid, or 100 per cent liquid. Frequently special devices are used to properly distribute the refrigerant among the parallel paths of the evaporator. These distributing devices usually have considerable pressure drop. Where they are used, the pressure drop across the expansion valve is not the difference between suction and discharge pressures, as allowance must be made for the pressure drop across the distributing device. An equalizer connection from the evaporator suction line must be made to the underside of the diaphragm (see Fig. 10) whenever the valve outlet is not at the evaporator pressure so as to insure suction pressure at this point. When distributing devices are used, this equalizer connection is essential for proper operation of the valve. Another pressure drop allowance must be made for the liquid line, particularly when the liquid line has an appreciable vertical rise.

Whenever possible, expansion valves should be installed in a manner which will permit placing thermometer wells in the suction connection and allow sufficient room for free adjustment of the valve.

Evaporators and Coolers

The types of coolers used in connection with air conditioning work fall into three general groups. The *first*, is the direct cooling of water; the *second*, direct cooling of air; and the *third*, cooling of brine for circulation in a closed system, which can cool either water or air. One method of the direct cooling of water is to install direct expansion coils in the spray chamber so that the water sprayed into the air comes in direct contact with the cooling coils. Another common and efficient method of cooling spray water is to use a Baudelot type of heat absorber where the water flows over direct expansion coils at a rate sufficiently high to give efficient heat transfer from water to refrigerant.

Another type of spray water cooler is the shell and tube heat exchanger in which the refrigerant is expanded into a shell enclosing the tubes through which the water flows. The velocity of the water in the tubes affects the rate of heat transfer, and as the refrigerant is in the shell com-

pletely surrounding the tubes at all times, good contact and a high rate of heat transfer are insured. The disadvantage of such a system is that with the falling off of load on the compressor the suction temperature or the temperature in the evaporator drops and there is a possibility of freezing the water in the tubes, which, of course, might split the tubes and allow the refrigerant to escape into the water passage. This danger can be eliminated by automatic safety devices.

Another system of cooling spray water is to submerge coils in the spray collecting tank, or in a separate tank used for storage. The heat transmission through the walls of the coils, however, is low and a great deal

TABLE 11. BASIS OF EQUIPMENT SELECTION

CAPACITY TONS	MAJORITY USED	SOME USED	FEW USED
0 to 5	Unit systems in conditioned space.	Unit central systems using duct distribution.	Built up central systems.
5 to 25	Built up central systems using reciprocating compressors.	Unit central systems using duct distribution.	Unit systems in conditioned space. Built up systems using absorption and adsorption systems.
25 to 50	Built up central systems using reciprocating compressors.	Built up central systems using centrifugal compressors.	Central systems using adsorption systems.
50 to 400	Built up central systems using reciprocating compressors.	Built up central systems using steam jet and centrifugal compressors.	
400 and Over	Built up central systems using centrifugal compressors.	Built up central systems using steam jet.	

more surface is required than for any other type of cooler. However, with large storage tanks this type of cooling can be utilized to advantage.

When direct cooling of air is employed, the refrigerant is inside the coil and the air passes over it. Cooling depends upon convection and conduction for removing the heat from the air. The type of coil used can be either smooth or finned, the finned coil being more economical in space requirement than the smooth coil. The fins, however, must be far enough apart so as not to retain the moisture which condenses out of the air.

The indirect cooler, where brine is cooled by the refrigerant and the resulting cold brine is used to cool either air or water, introduces several other considerations. It is not the most economical from a power consumption standpoint, as it is necessary to cool the brine to a temperature sufficiently low so that there is an appreciable difference between the average brine temperature and that of the substance being cooled. This requires that the temperature of the refrigerant must be still lower, and consequently the amount of power required to produce a given amount of refrigeration increases due to the higher compression ratio. There are

other considerations which make such a system desirable. In the first place, where a toxic refrigerant is undesirable or cannot be used because of fire or other risks, especially in densely populated areas, the brine can be cooled in an isolated room or building and can then be circulated through the air conditioning equipment. This arrangement eliminates any possibility of direct contact between the air and refrigerant.

Equipment Selection

The selection of proper refrigeration equipment for any air conditioning job is of utmost importance for satisfactory results. The most important factors in the selection of the equipment are:

1. Loads (as determined by the conditions of the space to be cooled).
2. Economics (both initial and operating costs).
3. Codes (local safety codes must be adhered to and influence the type of system to be used).

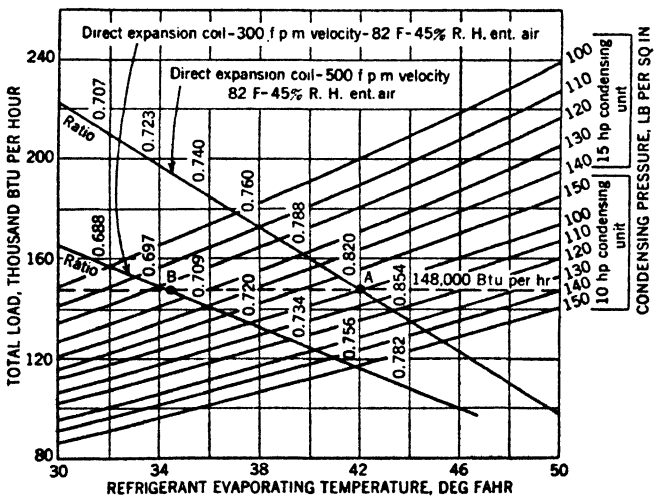

FIG. 11. COMPRESSOR AND COIL PERFORMANCE

A broad division of equipment to be used for a particular installation or application may be made on the basis of the magnitude of the load. Current general practice is outlined in Table 11.

Unit or *packaged* systems, consisting of a reciprocating compressor, condenser, evaporator, and fans, are generally used in the smaller sized jobs where electric power is available, as they are manufactured complete, ready to install and are the most economical (see Chapter 36).

The reciprocating compressor in the built-up central system (see Chapter 43) covers the widest range of application since it is applicable to either the direct expansion or indirect systems and can be driven by steam or gas engines, or by electric motors. The quantity of condensing cooling medium required is also less than for any other system with the exception of the centrifugal compressor, which uses the same amount.

Centrifugal compressors are used for large installations, and usually where the indirect system is required. The driving mechanism can be a

steam turbine or electric motor. The steam jet system is used where steam is available and cooling water can be had in large quantities.

It will be noted by referring to Fig. 7 that all systems using compressors have a common characteristic and that is that the capacity varies with the evaporating temperature. Not only can the equipment be selected to produce a given result, but the performance can be predicted under varying load conditions by the simple expedient of using the variable of evaporating temperature as the abscissa and the load or capacity as the ordinate in a series of curves.

Manufacturers of compressors and cooling coils furnish performance data for apparatus that can be plotted in the form of curves similar to those shown in Fig. 11. The performance of a compressor is plotted as a series of curves, each curve being drawn for a given condensing pressure. The performance of a direct expansion coil at two different air velocities is plotted on the same graph. The operating point will be, of course, where the two curves cross.

Data given in Table 12 illustrate two types of conditioned enclosures having the same total load of 148,000 Btu per hour, but with two different

TABLE 12. TYPICAL OPERATING CONDITIONS FOR TWO TYPES OF LOAD

Type of Enclosure	Load, Btu per Hour			Ratio Sensible to Total	Air Entering Coil		Operating Balance Point		
	Sensible	Latent	Total		F Deg	Per Cent R.H.	Evaporator Temp F Deg	Condenser Pressure Lb per Sq In.	Per Cent Sensible Heat
Restaurant	103,000	45,000	148,000	0.695	82	45	34.4	123	69.9
Office	121,000	27,000	148,000	0.820	82	45	42.2	100	82.1

ratios of sensible to total heat. In the case of the office with a ratio of 82 per cent sensible to total heat, the operating point *A* in Fig. 11 is found to be 42.2 F evaporating temperature with a face velocity of 500 fpm. In the case of the restaurant, with a ratio of 69.5 per cent sensible to total heat, the air velocity is lowered to 300 fpm and the evaporating temperature is lowered to 34.4 F as shown in point *B* of Fig. 11. In order to obtain the same capacity, a larger condensing unit is used. This illustration assumes zero pressure drop through the suction line. The pressure drop can be taken into account by shifting the compressor performance curves by the amount of pressure drop expressed in Fahrenheit degrees.

ABBREVIATIONS AND SYMBOLS IN CHAPTER

cop = coefficient of performance, ratio of refrigerating effect to the heat equivalent of the compressor work.
CVE = conventional volumetric efficiency.
d = internal diameter in inches.
H_t = cooling load in tons.
h_d = enthalpy of vapor at condition of discharge from compressor.
h_{fc} = enthalpy of liquid at discharge from compressor.
h_{fd} = enthalpy of liquid at discharge of expansion valve.
h_{fe} = enthalpy of liquid at entrance to expansion valve.

h_m = enthalpy of mixture.
h_v = enthalpy of saturated vapor.
h_{vd} = enthalpy of saturated vapor at discharge of valve or compressor.
h_{vs} = enthalpy of saturated vapor at state s entering compressor.
hp = horsepower.
p_d = pressure of saturated liquid and vapor at discharge of compressor.
p_s = pressure of saturated liquid.
psig = pressure pounds per square inch, gage.
psia = pressure pounds per square inch, absolute.
Q = quantity of heat, Btu.
Q_c = heat loss from condenser, Btu per pound refrigerant.
Q_j = heat dissipated in cooling water, Btu per hour.
s = entropy.
Δs = entropy change between suction and discharge.
T = absolute temperature, Fahrenheit degrees.
T_{avg} = average temperature, Fahrenheit degrees, absolute, of gas passing through compressor.
T_c = condenser temperature, Fahrenheit degrees, absolute.
T_s = evaporator temperature, Fahrenheit degrees, absolute.
t_{sd} = degrees superheat at discharge condition of vapor leaving compressor.
t_d = discharge temperature, Fahrenheit degrees.
V_c = clearance, percentage of volume, swept by piston, which is contained in spaces at end of cylinder when piston is at end of stroke (clearance includes valve spaces, etc.)
v_s = specific volume of gas at suction, cubic feet per pound.
v_d = specific volume of gas at discharge, cubic feet per pound.
W_r = refrigerant rate, pounds per minute.
x = proportion of liquid in mixture of vapor and liquid.

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Chapter 40

AIR DISTRIBUTION

Standards for Satisfactory Conditions, Definitions, Mechanics of Air Distribution, Outlet Performance, Types of Air Outlets, Outlet Location and Selection, Directional and Volume Control, Return and Exhaust Intakes, Specific Applications

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CORRECT air distribution contributes as much or more to the success of a forced air heating, ventilating, cooling or air conditioning system as does any other single factor. An air conditioning system may deliver the required quantity of conditioned air and still fail to give satisfactory room conditions because of poor air distribution. The scope of the chapter is limited to the air distribution within the conditioned space. Reference is made to the distributing duct system only insofar as it affects the performance of the air distribution outlet. See Chapter 41 for information on air duct design.

STANDARDS FOR SATISFACTORY CONDITIONS

The object of air distribution is to create within the space the proper combination of room temperature, air motion and humidity, whether by cooling, heating or ventilating. The purpose to be accomplished determines the factors to be controlled. For instance, in many industrial applications it is necessary to maintain proper standards throughout a large portion of the space; sometimes almost throughout the entire enclosure. In these cases design room temperature, room air motion and humidity will depend entirely upon the requirements of the product and its manufacturing processes.

If, however, comfort of the occupants is the principal objective, consideration of the occupied zone (floor to 6 ft above floor level) is primarily required. In order to obtain comfort conditions within this zone, standard limits have been set up as acceptable *effective temperatures*. This term comprises air temperature, motion, humidity and their physiological effect on the surface of the human body. Any variation from accepted standards of one of these elements may result in discomfort to the occupants. The same effect may be caused by lack of uniformity of conditions within the space or by excessive fluctuation of conditions in the same part of the space. Such discomfort may arise due to excessive room air temperature variations (horizontally, vertically, or both), excessive air motion (draft), failure to deliver or distribute the air according to the load requirements at the different locations, or too rapid fluctuation of room temperature or air motion (gusts).

In addition the noise level created by the introduction of supply air should be kept within acceptable limits, and streaking or smudging of walls or ceilings should be prevented.

With reference to permissible room air motion it is not possible to establish a specific standard covering the entire complex problem of air distribution. Velocities less than 15 fpm generally cause a feeling of air stagnation, whereas velocities higher than 65 fpm will disturb loose paper sheets on desks and may result in a sensation of draft. Air velocities of 25 to 35 fpm in the occupied zone are most satisfactory, but air motion of 20 to 50 fpm will usually be acceptable, particularly when the lower part of this range of velocity is used in cooling applications and the higher

values on heating jobs. In any case, it is certain that the effect of room air motion on comfort or discomfort depends on air temperature and direction as well as on velocity.

Reference should be made to Chapter 12, Physiological Principles, for information on effective temperature and comfort zones. Material in Chapter 42, Sound Control, covers acceptable room noise levels and noise generated by air outlets.

DEFINITIONS

The following definitions referring to air distribution equipment have gained general acceptance.

1. *Supply Opening or Outlet:* Any opening through which air is delivered into a space which is being heated, or cooled, or humidified, or dehumidified, or ventilated.

2. *Exhaust Opening or Return Intake:* Any opening through which air is removed from a space which is being heated, or cooled, or humidified, or dehumidified, or ventilated.

3. *Outside Air Opening:* Any opening used as an entry for air from outdoors.

4. *Damper:* A device used to vary the volume of air passing through a confined cross-section by varying the cross-sectional area.

5. *Grille:* A covering for any opening and through which air passes. A supply grille discharges air axially with a limited spread.

6. *Register:* A grille equipped with a damper.

7. *Free Area:* The total minium area of the openings in the air outlet or inlet through which air can pass.

8. *Core Area:* The total plane area of the portion of a grille, bounded by a line tangent to the outer edges of the outer openings through which air can pass.

9. *Mean Area:* The total of the core and free areas divided by two.

10. *Percentage Free Area:* The ratio of the free area to the core area expressed in percentage.

11. *Aspect Ratio:* The ratio of length of the core of a grille to the width.

12. *Vane Ratio:* The ratio of depth of vane to shortest opening width between two adjacent vanes.

13. *Plaque:* A ceiling outlet in which the supply air impinges against a plate or series of parallel plates and is discharged horizontally in all directions.

14. *Diffuser:* An outlet discharging supply air in various directions and planes, thereby effecting its mixture with the room air.

15. *Primary Air:* The air delivered to the outlet by the supply duct.

16. *Induction:* The entrainment of room air by an air stream.

17. *Internal Induction:* The induction of room air drawn into an outlet by the primary air stream. (Commonly called *aspiration*).

18. *External Induction:* The induction of room air by the air stream discharged from the outlet (commonly called *secondary air motion*).

19. *Induced Air:* The room air entrained by the primary air through internal induction or by the discharged air through external induction or both.

20. *Total Air:* The mixture of primary air and induced air.

21. *Induction Ratio:* The total air divided by the primary air.

22. *Throw (Blow):* The horizontal distance an air stream travels on leaving the outlet (grille) to a position at which air motion reduces to a maximum velocity of 50 fpm.

23. *Drop:* The vertical distance, the lower edge of the air stream drops between the outlet and the end of its throw.

24. *Rise:* The converse of drop.

25. *Envelope:* The outer boundary of an air stream moving at a perceptible velocity.

26. *Spread:* The divergence of the air stream in a horizontal or vertical plane after it leaves the outlet.

27. *Diffusion:* Distribution and mixing of air within a space, accomplished by an outlet discharging supply air in various directions and planes in order to effect the desired air conditions in the occupied zone of that space.

28. *Radius of Diffusion:* The horizontal distance from the diffuser outlet to the perimeter of the space, within which effective diffusion is accomplished and air motion in the occupied zone is reduced to 50 fpm maximum.

29. *Outlet Velocity:* The average velocity of air emerging from the outlet measured in the plane of the opening.

30. *Terminal Velocity:* The average air stream velocity at the end of the throw.

31. *Temperature Differential:* Temperature difference between primary and room air.

32. *Temperature Variation:* Temperature difference between points of the same space.

MECHANICS OF AIR DISTRIBUTION

In the mechanics of air distribution, two major problems are involved: (1) complete mixing of the primary air and air outside of the zone of occupancy in order to reduce the temperature difference and air motion to acceptable limits before the air enters the occupied zone; and (2) counteraction of the natural convection and radiation effects within the room.

The theory concerning the distribution of conditioned air within an enclosure is still incomplete and no general law governing outlet performance has been formulated. The characteristics and performances of the various existing types of outlets must therefore be evaluated largely by experimental work. Some progress has been made concerning the theoretical analysis of the characteristics of a primary air stream discharged in an unconfined space, i.e., a space large enough so that the primary air stream is not disturbed by contact with surfaces, or by adjacent streams. The approach to this problem is usually made by means of the momentum theory. Development of this theory has so far been confined to side wall distribution of air, because this is its most elementary application. Fundamentally, the same laws apply also to ceiling distribution, but a great amount of additional research is still required to adapt them to the more complicated conditions of deflection of air up to 90 degrees, spread up to 360 degrees and the resulting rapid induction. There is also an element of downward diffusion which usually is not obtainable with side wall grilles.

Momentum Theory

When air is discharged from an outlet into a free open space, the primary air stream entrains room air as it traverses the space. This entraining effect increases the cross-sectional area and reduces the velocity of the resulting air stream. Induction takes place with the conservation of linear momentum; this has been confirmed by tests which indicate that the momentum remains almost constant throughout the entire measurable length of the air stream. This relationship may be expressed by Equation 1:

$$M_1 V_1 + M_2 V_2 = (M_1 + M_2) V_3 \qquad (1)$$

where

M_1 = mass of primary air.
M_2 = mass of induced air.
V_1 = velocity of primary air.
V_2 = velocity of induced air (for practical use, $V_2 = 0$).
V_3 = velocity of the mixture.

If the velocity of induced air is zero, Equation 1 changes to:

$$M_1 V_1 = (M_1 + M_2) V_3$$

or,

$$\frac{V_1}{V_3} = \frac{M_1 + M_2}{M_1} = r \qquad (2)$$

Since in many applications the densities of primary and room air are about equal, air volumes may be substituted for mass and Equation 2 becomes:

$$\frac{V_1}{V_3} = \frac{Q_1 + Q_2}{Q_1} = \frac{Q_3}{Q_1} = r \tag{3}$$

where

Q_1 = volume of primary air, cubic feet per minute.
Q_2 = volume of secondary air, cubic feet per minute.
Q_3 = volume of mixture of primary air and induced air, cubic feet per minute.
r = induction ratio.

Jet Pattern From Round or Rectangular Openings in a Large Room

The relation between the shape of the discharge of a jet and the shape of the conventional outlet has long been the subject of research. It has been proved to be incorrect to assume that the jet retains the outlet shape when it discharges into a free open space [1]. Air streams from rectangular outlets having low aspect ratios develop a symmetrical or cone shape within a few diameters from the outlet face. From there on, the jet continues to expand at a fairly constant rate. Beyond 20 diameters there is very little difference between round and rectangular jets. The assumption can be made that the apex of the cone is in the same position for any jet having a small aspect ratio. For the more usual problems of the conventional room with outlets near the ceiling, there are insufficient experimental data to justify a definite statement on the effect of aspect ratio.

If the round or rectangular opening is divided into a number of orifices having straight sides, the performance of the air stream will be similar to that of a plain opening.

Velocity Across Jets

Results of many tests [1] indicate that the ratio of centerline velocity to average velocity is about 3, irrespective of outlet size, shape or initial velocity. This statement is true for stream cross-sections located beyond 10 diameters from the outlet, and is fairly accurate for distances up to 50 diameters. Experimental data are lacking for distances beyond 50 diameters.

Effect of Aspect Ratio on Entrainment

In slotted outlets, the air entrainment of the primary jet is a function of aspect ratio [1]. This effect is most pronounced when large changes in the ratio are made. A comparison between a slot of aspect ratio 24 and a square opening of the same area is given in curves *A* and *B* of Fig. 1. At a distance of 8 ft from the outlet, the entrainment of the slot is 8.1 as compared with 6.9 for the square, or an increase of about 17 per cent.

Curve *C* shows the further increase in entrainment obtained by using an aspect ratio of 48. An increase of 40 per cent is obtained over the 24 in. x 1 in. slot. This indicates that long narrow slots produce air streams that give high induction of secondary air.

Parallel Slots

The use of several slots in parallel to vary the rate of air entrainment depends mainly on the distance between the slots. If close together, the air pattern is about the same as for a single opening of equal area. Spac-

ing the openings farther apart gives an increase in entrainment as shown on curves D and E of Fig. 1. It will be noted that 2 openings 24 in. x ¼ in. located very close together will obtain an entrainment which is about the same as obtained with one 24 in. x ½ in. opening. However, if the slots are spaced 6½ in. apart there is a marked increase in entrainment.

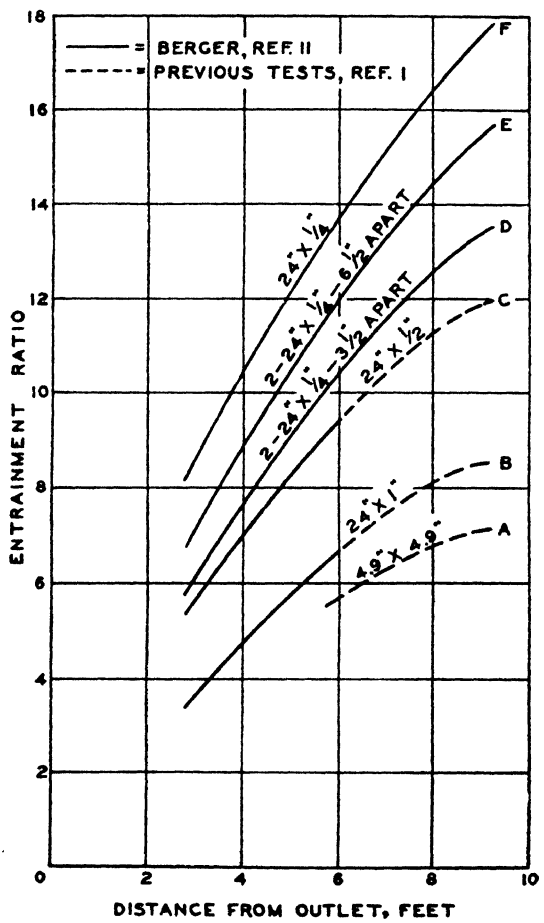

FIG. 1. TYPICAL RELATION OF ENTRAINMENT RATIO TO DISTANCE FROM OUTLET FOR SLOTTED OUTLETS. (BASED ON 800 FPM OUTLET VELOCITY.)

Throw

Equations for the throw of straight flow side wall outlets have been developed on the basis of the momentum theory. Equation 4 states the throw in terms of the area of the outlet and the primary air volume[2]:

$$L = 0.82 \frac{Q_1}{\sqrt{A_1}} \tag{4}$$

where

L = throw, ft.

A_1 = effective outlet area, in square inches = (gross measured area) x (percentage of free area/100) x (discharge coefficient).

The discharge coefficient is approximately 0.8.

Equation 4 has been developed under the assumption that the temperature of the supply air is the same as the temperature of the room air. It applies only to straight flow outlets with aspect ratios less than 16.

Equation 5 for the performance of straight flow outlets evolved from research[1] allows the calculation of the maximum residual velocity at any distance perpendicular to the outlet face. It applies for aspect ratios up to 50.

$$V_r = K \frac{V_1 \sqrt{A_1}}{X} = K \frac{Q_1}{X \sqrt{A_1}} \qquad (5)$$

where

V_r = maximum residual velocity in air stream, i.e., the highest maintained velocity at the given cross section in the room, feet per minute.

V_1 = average initial velocity across outlet, feet per minute.

K = Constant of proportionality.

A_1 = effective outlet area in square feet = (gross measured area) x (percentage of free area/100) x (discharge coefficient).

X = Normal distance from outlet face, feet.

Equation 5 together with Equation 6 (which reduces to Equation 7 if the jet angle is 20 deg) for the entrainment ratio,

$$\text{Entrainment Ratio} = \frac{0.785\ K}{R\ X \sqrt{A_1}} \left(\sqrt{\frac{A_1}{0.785}} + 2\ X \tan \frac{\Theta}{2} \right)^2 - 1 \qquad (6)$$

where

R = ratio of maximum residual velocity to average residual velocity.

Θ = jet angle or spread angle in degrees.

$$\text{Entrainment Ratio (20 deg jet angle)} = \frac{0.785\ K}{R\ X \sqrt{A_1}} \left(\sqrt{\frac{A_1}{0.785}} + 0.35\ X \right)^2 - 1 \qquad (7)$$

has been used to develop charts[3] which provide the graphical solution of problems involving the determination of the throw of air from slots and jets, the residual velocity, and the size of openings. (See Figs. 2 and 3). The charts apply only to *air discharging into room air of same temperature as the stream.* They can be used to determine the throw of air and entrainment ratios up to 40:1 with initial velocities of 1000 to 6000 fpm and with residual velocities of 100 to 1000 fpm. The charts furthermore are for use with sharp-edged orifices or slots, and *include the coefficient of discharge.* If air is discharged from an orifice with a well-rounded entrance or from a length of straight duct, the coefficient of discharge is unity and the actual area of the opening is the effective area. For such rectangular openings the effective diameter is the diameter of a circle with an area equal to the actual area of the rectangle. The following examples will illustrate the use of the charts:

Example 1: Air is delivered to a cooler through independent slots each 24 in. x 2 in. with an initial velocity of 2000 fpm. Determine the maximum residual velocity and the entrainment ratio at a distance of 15 ft from the slot.

From Fig. 3 the effective diameter = 6.2 in. = 0.52 ft. The number of effective diameters in 15 ft = 15/0.52 = 28.8.

From Fig. 2 at 2000 ft initial velocity read entrainment ratio = 6.6 and maximum residual velocity = 390 fpm. From tests it has been shown that the *average* residual velocity may be taken as ⅓ of the *maximum* or 130 fpm in this case.

Example 2: Using the data from *Example 1* determine the distance at which the maximum residual velocity will be 150 fpm.

From Fig. 2 at $V_1 = 2000$ and $V_T = 150$, the number of effective diameters is read directly as 73 and the throw of the air is therefore 73 x 0.52 = 38 ft.

Example 3: Air issues from a round orifice plate with an initial average velocity of 4000 fpm. It is to have a maximum residual velocity of 400 fpm at a distance of 30 ft from the opening. Calculate the size of the opening required and the entrainment ratio.

On Fig. 2 at the intersection of the curve of 4000 fpm, the entrainment ratio is read directly as 15 and the effective diameters of throw = 55.

Since 55 effective diameters are equal to 30 ft as required, 1 effective diameter = $\frac{30}{55}$ = 0.545 ft or 6.56 in.

On Fig. 3 vertically below intersection of 6.56 in. effective diameter line and equivalent round opening line read 8.5 in. in lower margin.

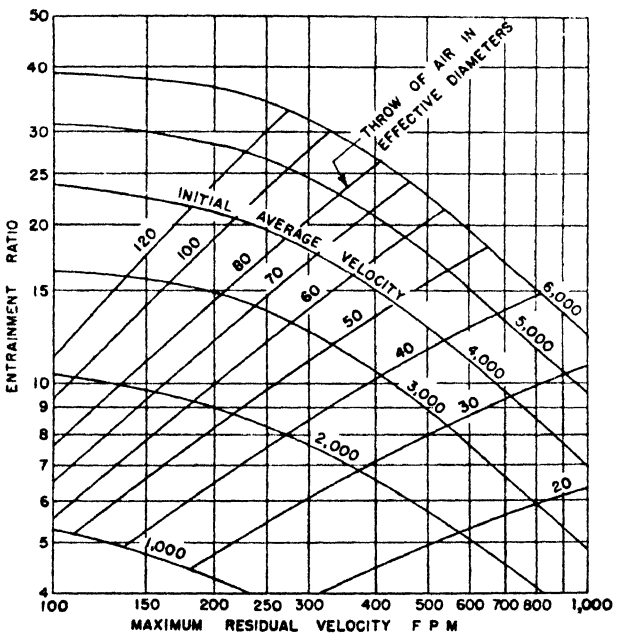

FIG. 2. RELATION BETWEEN INITIAL VELOCITY, RESIDUAL VELOCITY, ENTRAINMENT RATIO AND THROW OF AIR FROM JETS AND SLOTS

Example 4: A jet of air issues from a pipe or from air orifice having a well-rounded entrance (coefficient of discharge =1.0) and delivers air with the same velocities and with the same throw as in *Example 3*. What is the required diameter?

In this case since the coefficient of discharge is unity, the effective diameter of the jet is the actual diameter of the pipe or orifice, or 6.56 in., as obtained in *Example 3*.

Spread

The induction effect results in the spreading of the air stream. The total angle included by the air stream from straight flow outlets has been measured and found to be between 14 and 25 deg. The angle will depend on the type of approach, type of outlet and velocity.

The effect of vertical bars placed in the face of the outlet to increase the spread, may also be deducted from the momentum theory. Assuming that there are no horizontal deflecting bars and that the air spreads vertically through a total angle of 14 deg; that a uniform velocity exists at any section of the air stream; and that the conservation of momentum

principle applies down to a velocity of 60 fpm; the following approximate equations for throw are to be substituted for equation (4)[2]:

For a spread of 15 deg on each horizontal side $$L = 0.55 \frac{Q_1}{\sqrt{A_1}} \quad (8)$$

For a spread of 30 deg on each horizontal side $$L = 0.37 \frac{Q_1}{\sqrt{A_1}} \quad (9)$$

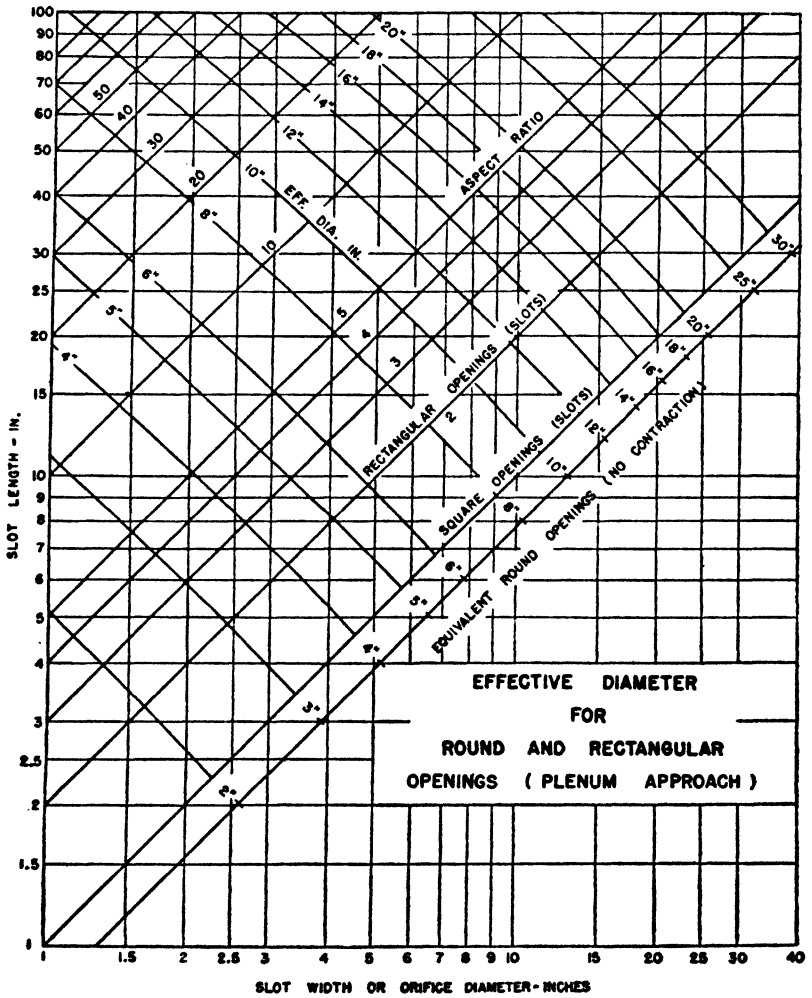

FIG. 3. EFFECTIVE DIAMETERS FOR ROUND AND RECTANGULAR OPENINGS (PLENUM APPROACH)

For a spread of 45 deg on each horizontal side $$L = 0.28 \frac{Q_1}{\sqrt{A_1}} \quad (10)$$

Guide Vanes

Vanes should have a depth of one to two times the spacing between the vanes. If the ratio of vane depth to spacing is less than one, effective control by means of the vanes cannot be obtained. Little improvement is obtained by increasing the ratio beyond two. The effect of various types of vanes is given in following paragraphs.

Straight Vanes. As mentioned previously, the included angle between both planes will be in the neighborhood of 14 deg, for a straight setting of the vanes as shown in Fig. 4.

Diverging Vanes. Such vanes set for an angular spread will have a marked effect on the direction and distance of travel of an air stream. An outlet having vertical vanes set straight forward in the center, with uniformly increasing angular deflection to a maximum at each end of 45 deg, will produce an air stream with a horizontal included angle of approximately 60 deg as shown in Fig. 4. The throw will be reduced one-half for such a vane setting. Increasing the divergence of the vanes reduces the air quantity handled by an outlet for a given duct static pressure. The primary function of the vanes is to spread the air horizontally. Spreading the air vertically entails the risk of hitting beams or other obstructions or of blowing primary air at excessive velocities into the occupied zone.

Converging Vanes. The blow of an outlet may be somewhat increased by converging the vanes of an outlet as illustrated in Fig. 4. Even with

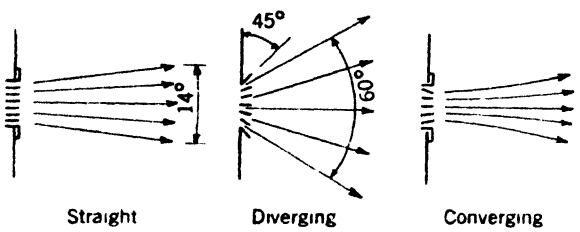

FIG. 4. SPREAD OF AIR STREAM WITH VARIOUS VANES

converging vanes, the resultant angle of spread of an air stream will not be less than 14 deg. The air converges for a few feet in front of the outlet, and then diverges more than if the vanes had been set straight.

Both the horizontal and vertical vanes of an outlet are important. After an installation has been made, many conditions of draftiness or stuffiness can be alleviated by some vane adjustment, provided an independent means for regulation of static pressure behind the vanes is included.

Vertical Drop and Rise

The distance that the lower edge of the air stream drops below the bottom of the outlet is important, since the air stream should not reach the occupied zone until the velocity has fallen to about 50 fpm. The drop (H, ft) is influenced by two forces; the natural vertical spread of the stream and the gravitational force due to the difference in density between supply air and room air. For air emerging at room temperature, the drop will be a function of the spread only and will be equal to:

$$H_1 = L \times \tan\left(\frac{\text{Spread Angle}}{2}\right) \tag{11}$$

where

H_1 = drop due to spread (when emerging air and room temperature are the same), feet.
L = throw, feet.

When there is a temperature difference between the air stream and the room, there is an *additional* drop which is approximately [4]:

$$H_2 = \frac{n_1 (t_r - t_{as}) L^{n_2}}{V_1} \tag{12}$$

where

H_2 = additional drop due to temperature difference, feet.
n_1 and n_2 = constants (tentative suggested values $n_1 = 5$, $n_2 = 1.2$).
t_r = room temperature, degrees Fahrenheit.
t_{as} = supply air temperature, degrees Fahrenheit.
V_1 = jet velocity, feet per minute.

It should be remembered, that the total drop $H = H_1 + H_2$. H_1 is positive for either heating or cooling; H_2 is positive for cooling, negative for heating. In consequence, there will always be a vertical drop in cooling, and a vertical rise in heating only if $H_2 > H_1$.

Another empirical equation for the *total drop* is[2]:

$$H = \frac{m\,(t_r - t_{as})\,L}{V_1} \tag{13}$$

where

m = constant (tentatively suggested value of $m = 16$).

In other words, for a given throw L the drop or rise increases as the temperature difference increases and the outlet velocity decreases. This equation is only valid, if a temperature difference exists between room air and supply air.

Room Air Motion (Wall Outlet)

One of the most important problems in air distribution is to achieve air motion in the occupied zone within acceptable velocity limits. Therefore, outlet performance and characteristics of the space have to be related to this air motion.

The air moving in the occupied zone is (for a side wall outlet) equal in quantity to the total air contained in the outlet stream at the end of the throw and it is generally moving in a direction opposite to the stream. Assuming that the maximum volume of air is in circulation when the air stream velocity V_s drops to 200 fpm, that the free area for return flow is 0.6 of the area of the wall in which the outlets are located, then, according to the momentum theory[2,4]:

$$V = \frac{Q_s}{0.6 \times A_w} \tag{14}$$

where

V = average room velocity, fpm.
Q_s = Volume of room air in motion, cfm.
A_w = area of wall in which outlet is located, sq ft.

Since $Q_s = Q_1 \times r$, (by definition); and $r = \frac{V_1}{V_s}$ according to Equation 3; the average room velocity is:

$$V = \frac{Q_1 r}{0.6\,A_w} = \frac{Q_1}{0.6\,A_w}\left(\frac{V_1}{V_s}\right)$$

or, with $V_s = 200$ fpm

$$V = \frac{Q_1\,V_1^{\frac{2}{3}}}{120\,A_w} \tag{15}$$

When Q_1, the volume of primary air, V_1, the velocity of primary air and A_w, the wall area are known, the average room velocity may be

calculated from Equation 15 in order to determine the acceptability of the air distribution system.

OUTLET PERFORMANCE

The factors of outlet performance, throw, drop, room air motion, capacity, temperature differential, dirt and noise place considerable limitations on the design of a satisfactory distribution system.

1. *Throw.* The throw of a wall outlet must be sufficient to produce satisfactory conditions over the area to be conditioned. Underblowing may cause heated air to rise too rapidly above the occupied zone and thus create excessive vertical temperature variation (stratification); in cooling operation it may cause cold air to drop into the occupied zone before a satisfactory mixing of supply and room air has been accomplished by induction and thereby create a condition of acute discomfort (draft). On the other hand, overblowing will result in objectionable downdrafts from any surface the primary air stream may strike.

On the average it is considered most practicable to select throw as ¾ of the distance toward an exposed wall or window, as shown in A of Fig. 5.

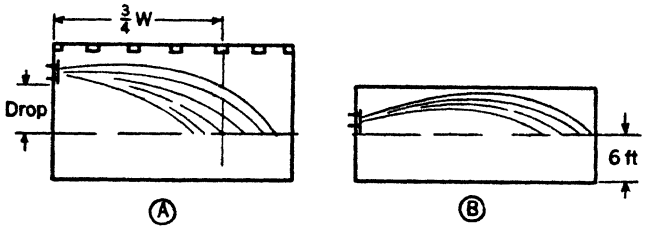

FIG. 5. THROW OF WALL OUTLETS

However, structural characteristics, mounting height, temperature differential and resultant drop or rise, or location of greatest heating or cooling loads strongly affect the selection of the optimum throw. In spaces with beamed ceilings, the outlets should be located below the bottom of the lowest beam level, and preferably low enough so that an upward or arched blow may be employed. The blow should be arched sufficiently to miss the beams and, at the same time, in such a manner as to prevent the primary or induced air stream from striking furniture and obstacles and producing objectionable drafts.

In the case of ceiling diffusers air is distributed with a spread of 360 deg horizontal. In addition there is a downward component of air motion. Therefore, both throw (radius of diffusion) and mounting height are important and interdependent factors. Due to the 360 deg spread of air diffusion the rate of induction will be higher and the throw shorter than that of a wall grille opening handling the same air quantity at the same outlet velocity. Therefore, ceiling diffusers will frequently permit the use of higher air velocities than wall outlets and consequently may be sized smaller to handle the same air volumes. If such ceiling outlets are installed flush with the ceiling, impingement of the air stream along the ceiling surface restricts induction of secondary air and the throw is increased approximately 20 per cent above that of an unrestricted air stream.

In the use of perforated ceiling plates as air distributing devices the term throw could hardly be applied in its proper meaning. Although this type of outlet can handle the greatest amount of air in proportion to room size, jet velocities must be kept low.

In all types of ceiling air distribution the following should be noted:

If cold air is used it must be brought to the proper temperature by mixing with room air before entering the zones of occupancy.

Air slightly above room temperature will usually be properly distributed by outlets selected for cooling.

When delivering warm air the same may be projected downward and the amount of dispersal of the jet varied to obtain proper mixing and control.

2. *Drop.* The outlets should be located so that the air stream at the termination of the blow is not less than 5 or 6 ft above the floor level. As illustrated in *B* of Fig. 5 the maximum permissible blow for a given ceiling height may be obtained by locating the outlet low on the wall, arching the blow, and sweeping the air across the flat ceiling. The air, as it traverses the room, will adhere to the ceiling. The objection to this method is the possible streaking of the ceiling with dirt.

3. *Room Air Motion.* Various features may cause room air motion to exceed acceptable standards. Some of these are: Excessive air discharge velocities; high air volume per cu ft of space (often referred to as number of air changes per hour); premature drop of cold air into the occupied zone; overblow causing spilling of high velocity air into the occupied zone; heating in severe climates by means of downward projection of hot air. It should be realized that these factors will not equally affect all types or designs of outlets at different temperature differentials, mounting heights, etc. For instance, certain outlets may safely handle more air per cubic foot of space at higher discharge velocities than others, and downward projection of supply air will sometimes not be considered excessive if the supply air temperature is substantially higher than the room temperature.

4. *Capacity.* The quantity of air to be handled is determined by the heating, cooling, or ventilating requirements. Manufacturers' rating sheets are usually consulted for selection of the proper number, size and type of outlets for a given air quantity. The basis of rating used should be carefully noted to make certain that resulting velocities are suitable for the application.

5. *Temperature Differential.* This is one of the most important factors affecting outlet performance. The quality of the temperature control, or the extent of the control problem, is directly a function of temperature difference. Obviously a system which carries under design conditions only a 5 deg difference between supply air stream and room temperature would require no control at all, for even a 50 per cent change in load could only effect a 2½ deg change in room temperature under the worst conditions. Because of the self-equalizing nature of most load factors, even this extreme is never realized. It is obvious that the greater the temperature differential between supply air and room temperature, the greater will be the change in room temperature for a given change in load. The use of outlets that give rapid mixing permits greater temperature differentials. These principles apply in both heating and cooling practice.

6. *Dirt.* Although the primary air may be carefully filtered, small particles of dirt and dust will not be captured by mechanical filters and may finally be deposited on the walls or ceiling. With ceiling outlets, dirt streaking may be minimized by carefully controlling the discharge of the outlets. With wall outlets, dirt streaking may be minimized by preventing direct impingement of the air on any ceiling or room surface. Floor outlets may offer objection as dirt collectors.

7. *Noise.* The increase of noise level caused by an outlet is primarily a function of its air discharge velocity and its size. The maximum accept-

able noise level in a space may dictate completely the selection of the permissible outlet velocity. In addition, however, noise may be caused by excessive restriction of free outlet area due to outlet design; by unnecessary turbulence due to one sided air flow through the outlet; or by the impingement of high velocity air on sharp edges. Such high frequency noises due to excessive turbulence are especially annoying (see Chapter 42 for discussion of permissible room noise levels and noise generation by outlets).

TYPES OF AIR OUTLETS

Two types of air supply outlets are commonly used; side wall and ceiling. A variety of designs has been developed for both types and the final selection depends to a large degree upon the specific problems arising in the air distribution system to be used.

In addition to the comments on use and application of outlets which follow, reference should also be made to sections of this chapter on Outlet Location and Selection as well as on Specific Applications.

Wall Outlets

Wall type openings in general use are: perforated grilles, vaned outlets, registers, slotted outlets, ejector nozzles, and wall diffusers.

1. *Perforated Grilles.* Due to the non-adjustability and small vane ratio these outlets, although inexpensive, have not met with favor as wall type supply openings. They are useful primarily where directional air control is unnecessary, and for return air intakes.

2. *Vaned Outlets.* Outlets equipped with either vertical and horizontal adjustable vanes or both are particularly suited to sidewall distribution. For proper control over the air flow, the vane ratio should be from 1 to 2. Outlets with non-adjustable vanes may be employed but they should only be used where the performance is not critical or can be adequately predicted. Vanes should be properly designed to prevent an increase of noise above permissible level.

3. *Registers.* Perforated grilles or vaned outlets equipped with a vane damper are termed registers. They are used primarily for residential heating systems, where the outlet distribution is not critical and low cost is of importance.

4. *Slotted Outlets.* Slotted outlets essentially consist of either flat steel plates containing a number of long narrow slots or a single long narrow slot. In order to give a good conversion from static pressure to velocity pressure, the sides of the slots are rounded to give a venturi effect. Due to their high aspect ratio, the slotted outlets have a greater induction effect than the comparable vaned outlets of equal area and consequently the throw is reduced. They are primarily useful where an unobtrusive means of distribution is desired, and where it is desirable to submerge the outlets into the room decoration and to minimize the effect of obstructions in the line of discharge. They are adaptable to narrow rooms having low ceilings. In this case the slots should extend the full length of the room. In all applications air quantity and distribution must be carefully planned as correction after installation is difficult.

5. *Ejector Nozzles.* These are outlets operating at high static pressure. They give a high conversion from static in the duct to velocity pressure in the outlet, and have a high induction effect due to their high outlet velocity. They are chiefly used for long throw and industrial process installations, such as drying, freezing, cooking, etc. Another type of ejector is

sometimes referred to as a *louver nozzle* having a 45 to 90 deg elbow, which can be rotated similarly to a universal joint about an axis perpendicular to the surface to which it is fastened. These outlets give a considerable degree of adjustability and are, therefore, desirable for use in confined spaces where spot cooling is employed. The use of very high velocities is gradually disappearing due to noise difficulties.

6. *Wall Diffusers.* These outlets incorporate design features originally developed for ceiling outlets and use therefore semi-conical or semi-pyramidal guide vanes instead of the straight vanes of the conventional side wall outlet.

Ceiling Outlets

Generally used ceiling outlets are: plaques, ceiling diffusers, and perforated ceilings and panels.

1. *Plaques.* Plaques are of simple design. The air from the supply opening impinges on a plate, which permits the air to be discharged horizontally in all directions. Plaques, although inexpensive, are difficult to control and are not generally satisfactory. In certain applications a properly designed plaque yields satisfactory results.

2. *Ceiling Diffusers.* Ceiling diffusers are round or rectangular outlets installed on or parallel to the ceiling, discharging supply air in a variety of directions and planes. Performance of the different designs varies according to principle employed. Some have no internal induction, but hasten external induction by supplying air in multiple layers. Others have internal induction and distribute air over an entire half sphere. The induction effect is greatest in the direction of the axis of the outlet, and least in the plane perpendicular to the axis and located at the ceiling level. Thus the induction is greatest in the vertical direction where the least throw can be tolerated and least in the horizontal plane at the ceiling where the greatest blow is both desired and permissible.

3. *Perforated Ceilings and Perforated Panels.* This method obtains air diffusion by discharging air through perforations in the ceiling, or part of the ceiling or walls. Some perforated panels feature a control plate frame which is inserted in the conventional ceiling duct. Supply air enters the plenum above the distribution plates through an adjustable air valve which can be set for varying air quantities and velocities. The advantages are unobtrusive appearance and the ready application of sound absorbing material to the design. Also, if designed properly, this system provides a low rate of room air motion and consequently lends itself to applications having high load or high ventilating requirements. The perforations should be kept free of accumulations of dirt, as clogging will cause uneven distribution and result in smudging of the ceiling. Best results are obtained in systems having efficient cleaning devices.

In present practice relatively low velocities are used because the perforated material offers only small resistance to the air flow. Therefore, great care must be taken to distribute the primary air at uniform velocities over the perforated panels to avoid uneven air distribution and primary air streams of undesirable velocities and direction.

OUTLET LOCATION AND SELECTION

In selecting the location of outlets, consideration must be given to the factors of physical construction, physical appearance, location of heating or cooling loads, and outlet performance:

1. The *physical construction* of a building, particularly of old buildings, immediately places limitations on the type of distribution system which can be employed. The first factor in the selection of outlet locations, therefore, is a consideration of the possible location of the supply duct, that is, whether it is above the ceiling, within the walls, through furred spaces above corridors, or in the conditioned space, etc. A particular method of distribution may be highly desirable but its execution, due to the location of beams and masonry walls, may be impossible.

2. The *physical appearance* of the outlets should conform to the esthetic appearance of the room. In factories, warehouses, etc., the esthetic demand may not be high; however, in department stores, clubs, theaters, etc., the location of the grilles may be dictated largely by such demands.

3. The *location of heating or cooling loads* in a room dictates to a great extent the general location of the outlets. The outlets should be located to neutralize any undesirable cold drafts or radiation effects set up by a concentration of the heating or cooling load. The problem can be divided into *natural loads* due to outside weather and *internal heat loads*.

In winter the natural or primary heating load is caused by exposed walls, windows and skylights. Heat is lost primarily through convection to these exposed surfaces. The convection currents or cold drafts drop down the exposed surfaces and seriously impair the comfort conditions in the room, particularly at the floor level near the exposed surfaces. The outlets should be located to counteract these down drafts. Two methods may be employed:

a. Direct counteraction of convection currents from cold surfaces can be obtained by locating the outlets to blow upward from beneath windows or exposed walls or to blow across the exposed wall. This method is desirable in small offices or bedrooms, or any location where people are seated or working near exposed surfaces. In northern climates, where the outside temperature may be constantly below 40 F, and the construction consists of uninsulated walls and single glass, this method of distribution is particularly useful for the maintenance of comfort requirements.

b. High induction by ceiling or wall outlets may be employed to nullify the convection currents from exposed surfaces. If outside temperatures are consistently below 40 F, and the exposed surfaces are not well insulated, the induction effort required for neutralization of the downdrafts is so great that the air motion in the room may exceed comfort limits unless care is taken in selection and location of the outlet. Where comfort conditions are not critical as in factories for heavy manufacturing, warehouses, etc., satisfactory results can be obtained even in cold climates. For uninsulated walls and glass areas some supplementary heating is often valuable. Wall diffusers, direct radiation or warm panels will satisfy these requirements for supplementary heating.

c. The location of exhaust or recirculated air openings at the base of large areas of glass is sometimes effective in reducing cold downdraft into the occupied space.

If a *concentrated source of heat* creating an *internal heat load* is located at the occupancy level of the room, the heating effect may be counteracted by blowing the supply air toward the heat source or by locating an exhaust or return grille adjacent to the heat source. The latter method will prove more economical, as heat will be withdrawn at its source rather than be dissipated into the conditioned space. Where a lighting load is particularly heavy (five watts per square foot) and located high in a conditioned space, it may be economically desirable to locate the outlets below the lighting load. Warm air from the lights will stratify near the ceiling and can be removed by an exhaust or return fan, the former being advisable if the wet-bulb temperature of the air is above the outside temperature, and the latter being preferable if the wet-bulb temperature is below that of the outside air. Either method reduces the requirements for supply

air. If the lamps are exposed, less saving can be realized than if enclosed, as a considerable portion of the total energy is radiant.

4. *Outlet Performance.* The laws of air distribution, previously discussed, will be found to exercise an important influence upon the design of an acceptable distribution system. This applies particularly to such features as throw, drop, capacity, room air motion, etc.

Procedure for Outlet Location and Selection

In determining outlet location and selecting the type of outlets it is customary to proceed as follows:

1. Study the plan of the building and note the amount of air to be supplied to each enclosure.

2. Select number of outlets for each enclosure considering air quantity required and distance available for throw or as radius of diffusion. The same factors, as well as distance from floor level available as mounting height, structural characteristics of the space and frequently consideration of appearance will determine the type of outlet used.

3. Arrange location of outlets in space. Usually the outlets will be evenly spaced to distribute air uniformly throughout the enclosure. Sometimes, however, more air should be supplied and directed towards zones of exceptional heating or cooling loads. An important point to consider is the combination of proper outlet location and efficient duct design (see Chapter 41). Consult manufacturers' tables for recommended location and spacing of outlets.

4. Select size of outlets according to air quantity handled, permissible throat or discharge velocities or effective throw, taking into consideration other factors such as noise level, static pressure resistance, etc. It will be generally found that most selection tables for grille type outlets are based on capacity and throw, whereas data for ceiling or wall diffusers are usually based upon capacity and permissible outlet velocity. Choice and arrangement of either type of outlet should however satisfy the requirements of all aspects of air distribution. Therefore, type, location and size of any outlet should be checked against manufacturers' ratings to determine whether the selection made would satisfy the requirements of the job. The most important questions to be considered are:

a. Can drafts occur because of divergence between rated throw (radius of diffusion) and distance between outlet and nearest obstacle of air stream (wall, beam, pillar, ledge, etc.)?
b. Can drafts occur because of excessive cooling temperature differential and too low mounting height of the outlet?
c. Can drafts occur because of too low velocity causing a drop in cooling installations?
d. Will the outlet operate at too high a velocity and thereby cause an excessive increase in noise level?
e. Will the outlet operate against an excessive static pressure resistance?

Balancing the System

In designing an air conditioning system it should be the aim of the engineer to size ducts and outlets in such a manner that proper distribution of supply air takes place. In practice, however, this is almost impossible and therefore additional means for regulating air distribution are required to *balance* the system. Some of these means are:

1. Reducing the effective area of some supply openings by blank-offs.
2. Placing dampers in the supply and return (exhaust) openings.
3. Placing dampers in the supply and return (exhaust) ducts.
4. Using combinations of dampers in both supply and return (exhaust) ducts.

In selecting the desired type of damper or balancing method the following points should be kept in mind:

1. Unfavorable effect on air stream and noise level should be avoided. This will often eliminate blank-offs and dampers installed in the supply and return (exhaust) openings, unless such dampers are of special design.

2. It should be possible to alter the volume control setting and measure the amount of air handled without difficulty. This will be particularly difficult to achieve in the case of blank-offs.

Generally speaking, it is most satisfactory to install dampers in the supply duct at some distance back of the outlets, so as to avoid disturbing the air flow. Dampers in both supply and return air ducts form the most flexible means of controlling supply of air to the room and static pressure within the room. Means of volume and directional control are discussed in detail in a following section of this chapter. Many types of air distribution control devices are now commercially available.

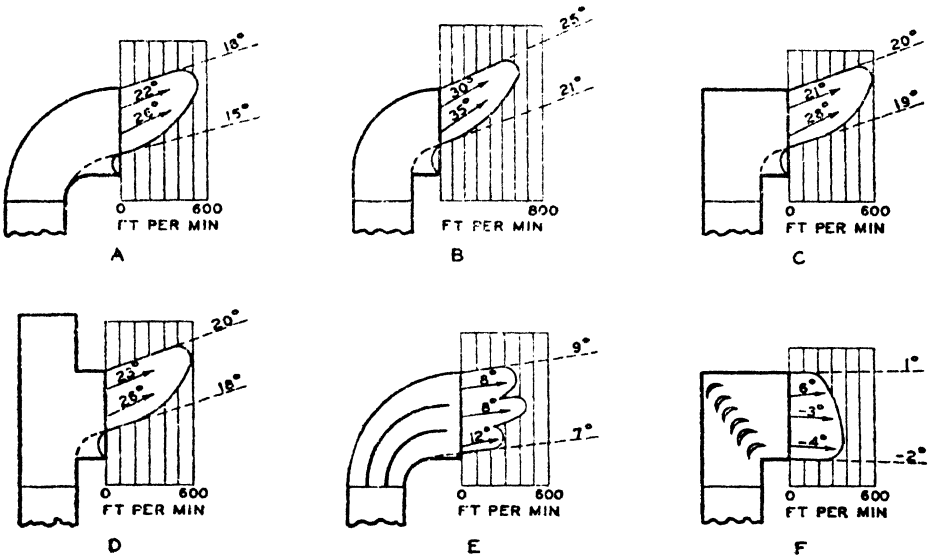

FIG. 6. OUTLET VELOCITY AND AIR DIRECTION DIAGRAMS FOR STACK HEADS WITH EXPANDING OUTLETS

Stack 14 in. x 6 in. Outlets 14 in. x 9 in. Stack Velocity 500 fpm

A. Rounded Throat and Round Back.
B. Square Throat and Round Back.
C. Square Throat and Back.
D. Square Throat and Cushion Chamber.
E. Rounded Throat and Back and 2 Splitters.
F. Square Throat and Back and 6 Guide Vanes.

DIRECTIONAL AND VOLUME CONTROL

Duct Approaches to Outlets

In order to obtain proper direction of flow and distribution of air from outlets it is necessary that the air stream approaching the outlet be of uniform velocity over the entire connection to duct and perpendicular to the face.

Grilles and directional outlets cannot compensate for improper approach. Any attempt to secure a low face velocity and a high duct velocity by constructing an expanding chamber directly behind the grille is likely to be unsuccessful because the enlargement angle in even a straight duct cannot be greater than 7 deg at each side if the stream is to fill the outlet without turbulence.

In elbow outlets or stack heads at the top of vertical stacks it is necessary to provide splitters or guide vanes in the elbows regardless of the shape of the elbows whether of rounded, square or expanding types. Cushion chambers at the top of the stack heads have no beneficial effect. The direction of flow, distribution and velocity (measured 12 in. from

outlet) of the air, based on tests [5], are shown in Fig. 6 for various types of stack heads expanding from a 14 in. x 6 in. stack to 14 in. x 9 in. outlets, without grilles. The air velocity for each was 500 fpm in the stack below the elbow, but the direction of flow and the distribution patterns are generally indicative of performance obtainable with non-expanding elbows of similar shapes for a range of velocities 200 to 1400 fpm. Some of the conclusions drawn from the tests were:

1. Experiments with various elbow outlets on the 14 in. x 6 in. vertical stack [5] with stack air velocities of 200 to 1400 fpm indicated that enlargement of the outlet area, whether used in connection with square or rounded elbows, would not reduce either the angle of discharge (which was 20 to 30 deg above the horizontal) or the outlet velocity. The effect of the enlargement of the outlet was mainly to increase the reverse flow area in the lower part of the outlet, but in each case enlargement of the outlet reduced the static pressure in the duct below the elbow.

2. Splitters in the elbows had the effect of dividing the air stream into a number of streams flowing through rounded elbows and therefore lowered the angle of discharge, reduced or eliminated the reverse flow area, and made the outlet velocity quite uniform.

3. Turning vanes having 2 in. inner and 1 in. outer radii located in the center of the elbow were found most effective in improving performance in regard to angle of discharge, outlet velocity, and elimination of reverse flow area.

4. Pressure loss through stack heads may be reduced by use of splitters or turning vanes or by increasing the inner radius of an elbow. Considering the sum of the velocity and static pressure as a measure of the energy required to change the direction of the air stream and to deliver the air into the atmosphere, and considering the energy required for a plain fitting as 100 per cent, it was found that *turning vanes* dropped the energy requirement of square type stack heads to 45 per cent. Splitters reduced the energy requirement to 90 per cent in long radius elbows and to 74 per cent in short radius turns. In expanding heads splitters reduced the energy requirement to 58 per cent.

Side Outlets in Horizontal Air Ducts

When air is supplied to a room from side outlets in horizontal ducts it is necessary to use directive devices within the duct at each outlet in order to obtain a uniform velocity of delivered air and to obtain a direction of flow perpendicular to the face of the outlet. In tests [6] conducted with 3 in. x 10 in., 4 in. x 9 in., and 6 in. x 6 in. outlets in a 6 in. x 20 in. horizontal duct at duct velocities of 200 to 1400 fpm (in the 6 in. x 20 in. section) it was found that multiple curved deflectors produced the best flow characteristics. Vertical guide strips in the outlet were not so effective as curved deflectors. A single scoop type deflector at the outlet did not improve the flow pattern obtained from a plain outlet and was therefore not found to be desirable.

Ceiling Outlets on Horizontal Ducts

Ceiling outlets are usually installed below horizontal supply ducts so that the supply air has to make a 90 deg turn before entering the outlet itself. The shorter the connection between bottom of duct and outlet, the greater is the need for directive devices to obtain uniformity of flow. Generally speaking, conditions and remedy in such cases strongly resemble those for side outlets in horizontal air ducts. Ceiling ducts often have a rectangular cross section while the connections to the ceiling outlets are circular. It will then be quite difficult to install turning vanes successfully, particularly if the ducts are shallow and the connection areas are comparatively large. This will be the case, when more than one outlet is installed on one duct run and restrictions of duct area must be avoided. In such cases good results have been obtained by using a series of vertical guide strips, installed at right angles to the direction of air approach in the outlet connection where it leaves the horizontal air duct.

Volume Control

Various methods are used to regulate volume of supply and return (exhaust) air. Some of these accomplish only minor changes in volume; most of them however permit a range of adjustment from maximum air supply to complete shut-off.

When selecting type and location of such dampers, the following points must be considered, especially when the volume control feature is to be located near the air outlet itself: (1) deflection of air stream by the damper, need and feasibility of directional control; (2) increase of noise level due to irregular and localized high air velocities caused by damper operation.

The following types of volume control are most frequently encountered:

1. *Slide Damper.* A single plate which can be pushed across the duct. Since its operation changes the free area of air passage in a one sided manner it should not be located near any air outlet and is practical only where no intermediate setting between full open and closed is required.

2. *Hit-and-miss Damper.* Two slotted plates or discs, closely adjacent; by moving one of the two plates the respective slots may be opened or closed. This type of volume

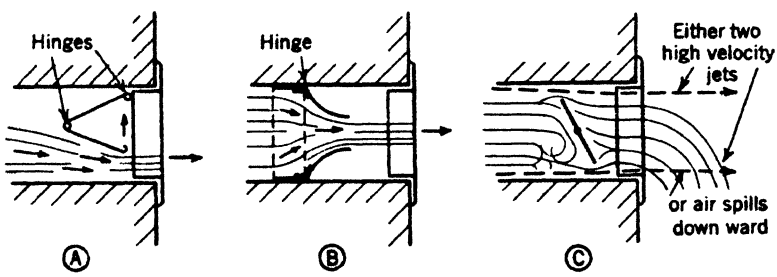

FIG. 7. EFFECT OF VARIOUS DAMPER ARRANGEMENTS DESIGNED FOR STRAIGHT BLOW

control may be installed close to an air outlet and it is easy to operate, but its main disadvantage is that even in the open position the air passage area is blocked by at least 50 per cent. This requires oversizing of the air outlet in order to avoid excessive increase of noise level.

3. *Splitter Damper.* A single blade sheet metal plate hinged at one edge, usually located at the branch connection of a duct or outlet. It is easy to operate but often causes irregular air flow in the duct. When used in connection with, and near an outlet additional directional control is required.

4. *Butterfly Damper.* A single blade sheet metal hinged in the middle, usually located in a straight duct run. It is easier to handle than a splitter damper, since only half the motion is necessary to change its setting. However, if located too close to an air outlet, it is objectionable because its operation frequently results in a condition whereby too high velocity jets are created along the sides of the duct or the air spills immediately downward into the occupied zone (see C Fig. 7).

5. *Louver Dampers.* Numerous designs have been developed incorporating a series of splitter or butterfly dampers across the duct or air outlet. Their main advantage consists in retaining greater uniformity of air flow and in requiring less depth for installation. Some designs provide for louver blades moving in opposite directions, and while decreasing free air passage area, retain a constant air flow direction along the axis of the duct air outlet connection (see A and B in Fig. 7).

RETURN AND EXHAUST INTAKES

The *selection of return and exhaust intakes* depends on: (1) velocity in occupied zone near intake, (2) permissible pressure drop through intake, and (3) noise.

1. *Velocity.* The effect of air flow through return intakes upon air movement in the room is slight. Air handled by the intake is drawn from

TABLE 1. RECOMMENDED RETURN INTAKE FACE VELOCITIES

INTAKE LOCATION	VELOCITY OVER GROSS AREA FPM
Above occupied zone	800 up
Within occupied zone, not near seats	600–800
Within occupied zone, near seats	400–600
Door or wall louvers	500–700
Undercutting of doors (through undercut area)	600

all directions, the velocity dropping off rapidly as distance from intake increases. The only locality where drafts may prove objectionable is adjacent to the intake. To prevent excessive air motion in this area due to the return intake, it is advisable to compute the total air motion toward the exhaust opening as outlined in Equation 14 where A is the exhaust wall area in square feet. Recommended return intake face velocities are given in Table 1.

2. *Permissible Pressure Drop.* The permissible pressure drop will depend on the choice of the designer. Table 2 gives pressure drop through plain lattice intakes as a function of free area and face velocity.

Proper pressure drop allowance should be made for control or directive devices.

3. *Noise.* The problem of *noise* generated by return intakes is the same as that for supply outlets. In computing resultant room noise levels from the operation of an air conditioning system, the return intake must be included as a part of the total grille area. The major difference between the supply outlets and return intakes is the frequent installation of the latter at ear level. When so located, it is recommended that the return intake velocity be not in excess of 75 per cent of the maximum permissible outlet velocity.

Outlet Location

The control of the room air motion for the maintenance of comfort conditions depends on the proper selection of the *supply* outlets. The location of the return or exhaust intakes do not critically affect air motion unless room air velocities in the occupied zone adjacent to the intake exceed comfort limits. The locations of return or exhaust intakes are however important for obtaining the desired room temperature equalization.

4. *Ceiling locations* for outlets are recommended for bars, kitchens, lavatories, dining rooms, club rooms, etc., where warm air will rise to the ceiling level. In heating installations, location of the return grilles in the

TABLE 2. APPROXIMATE PRESSURE DROPS FOR LATTICE RETURN INTAKES

Inches Water Gage—Standard Air

PER CENT FREE AREA	FACE VELOCITY, FPM						
	400	500	600	700	800	900	1000
50	0.06	0.09	0.13	0.17	0.22	0.28	0.35
60	0.04	0.06	0.09	0.12	0.16	0.20	0.24
70	0.03	0.05	0.07	0.09	0.12	0.15	0.18
80	0.02	0.03	0.05	0.07	0.09	0.11	0.14

ceiling or high on the wall will result in stratification of the conditioned air and a high percentage of the heated air will be drawn into the return duct before it has served its purpose. (Refer also to considerations outlined previously in section *Outlet Location and Selection* in this Chapter).

Some circular ceiling outlets combine the supply and return openings in a single unit. The return duct is in the center with the supply pattern on the outside. This method gives best results for cooling applications. The application for heating is more critical and requires consideration of ceiling height, amount of outside wall area, and number of air changes required. In some cases, stratification of warm air may cause short circuiting. Where the wall losses are a small part of the total, little difficulty is encountered with stratification.

Floor locations of outlets are used in heating installations for ceiling or side wall supply. When located so that air is drawn across exposed walls, the performance of the system may be somewhat improved. In general, floor locations tend to collect dirt and refuse.

Wall and door locations of outlets depending on their elevation, have the characteristics of either floor or ceiling returns. In large buildings with many small rooms, the return air may be brought through door grilles or door undercuts into the corridors and then to a common return or exhaust. The pressure drop through door returns should not be excessive; otherwise the air distribution to the room may be seriously unbalanced with the opening or closing of the doors. Outward leakage through doors or windows cannot be counted upon for dependable results.

SPECIFIC APPLICATIONS

For *theaters and auditoriums* the air distribution methods used are the downward distribution system with ceiling diffusers and the horizontal distribution system with ejector nozzles or wall diffusers. Fig. 8 shows both methods. Ceiling distribution is accomplished by ceiling outlets under main ceiling and balcony. It is indicated when main ceiling or balcony are cut up by architectural treatment or beams. The only critical points are under the balcony, and (occasionally) above the very rear of the balcony, where ceiling heights are low and where direct impingement of air is sometimes a hazard.

Wall or ejector distribution is particularly applicable for relatively long and narrow theaters. It is essential with this type of distribution that there be no interference with the movement of air throughout its entire path from the high velocity nozzles to the front of the theater. The ceiling should be smooth without projecting beams or obstructing ornamentation. For large theaters, relatively high velocities can be used. These will work satisfactorily if adjustable outlets are used to avoid areas of local turbulence.

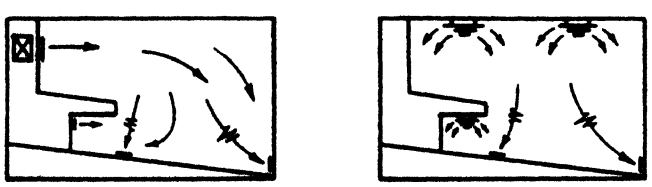

FIG. 8. AIR DISTRIBUTION METHODS FOR THEATERS, CHURCHES, AND AUDITORIUMS

In small or medium size theaters, it is sometimes practicable to use side wall or front wall distribution. For the satisfactory operation of such a system during the winter heating period, the returns should preferably be located at the floor level and near the front of the theater to prevent cold spots which may result from exposed wall convection or infiltration from exits.

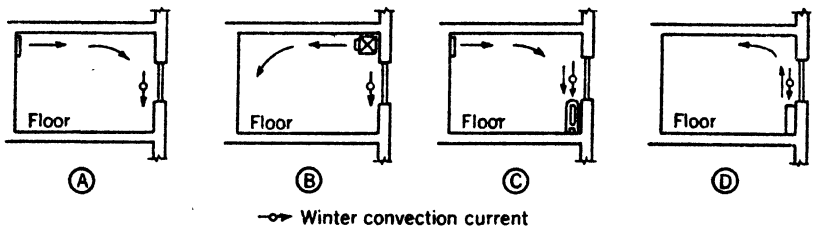

FIG. 9. DISTRIBUTION METHODS FOR SMALL ROOMS

A. Satisfactory for cooling. Unsatisfactory for heating in severe climates where the outside temperature is consistently below 40 F, and single glass and uninsulated walls are prevalent.

B. Performance approximately that of A when small diffusers are used in bottom of the duct.

C. Satisfactory for cooling. Satisfactory for heating if direct radiation is properly controlled.

D. Satisfactory for both cooling and heating. The air should be discharged slightly away from the wall, and for low velocities should be fanned out parallel to the wall.

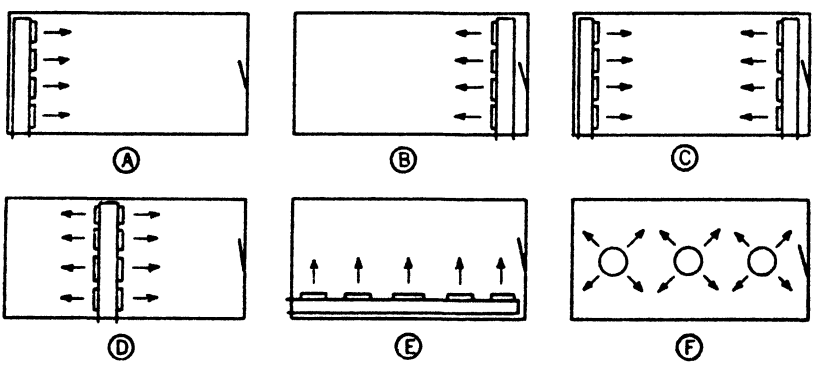

FIG. 10. SMALL STORE COOLING DISTRIBUTION

A. *Rear Wall.* High outlet velocity, satisfactory if properly designed; possibility of excessive air motion and drafts if used for wrong application.

B. *Front Wall.* High outlet velocity, results same as A.

C. *Front and Rear Walls.* Moderate room air motion, outlet blows should not impinge giving rise to down drafts in center.

D. *Center.* Moderate air motion, no impingement of air streams. Good results.

E. *One Side.* Moderate room air motion; should blow toward exposed wall. Good results.

F. *Ceiling.* Low room air motion. Good results. Outlets should be selected of sufficient size to allow for blocking when not located in perfect squares.

For *multi-room buildings* diagrams shown in Fig. 9 illustrate distribution methods for small rooms with exposed wall, such as offices, hotel (guest) rooms, hospital (patients) rooms, apartments, etc.

For *a small store* the cooling performance of various distribution methods is illustrated in Fig. 10. *Marine applications* of air distribution systems are given in Chapter 49.

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Chapter 41

AIR DUCT DESIGN

Pressure Losses, Friction Losses, Friction Loss Chart, Circular Equivalents of Rectangular Ducts, Elbow Friction Losses, Proportioning the Losses, Duct Sizes, Procedure for Duct Design, Air Velocities, Main Trunk Ducts, Velocity Method, Equal Friction Method, Duct Construction Details, Duct Heat Loss and Insulation

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THE theoretical resistance of an air handling system can be computed from the methods and data given in this chapter. The actual resistance for any given installation, however, may vary considerably from the calculated resistance because of variation in the smoothness of materials, the type of joints used and the ability of the mechanics to fabricate in accordance with the design. It is best to select fans and motors of sufficient size to allow a factor of safety. Volume dampers should be installed in each branch outlet to balance the system, and the necessary allowance for this balancing should be made in calculating the pressure loss in the system.

The flow of air due to large pressure differences is most accurately stated by thermodynamic formulae for air discharge under conditions of adiabatic flow, but such formulae are complicated, and the error occasioned by the assumption that the gas density remains constant throughout the flow may be considered negligible when only such pressure differences are involved as occur in ordinary heating and ventilating practice.

The rate of flow of air in a duct may be obtained from Equation 1, which is developed as Equation 69 in Chapter 4:

$$V_m = 1096.5 \sqrt{\frac{h_w}{\rho_a}} \tag{1}$$

where

V_m = velocity of fluid, feet per minute.
h_w = velocity head or pressure, inches of water.
ρ_a = density of air, pounds per cubic foot.

For dry air (69.41 F and 29.921 in. Hg barometer) $\rho_a = 0.075$ lb per cubic foot [1]. Substituting this value in Equation 1:

$$V_m = 1096.5 \sqrt{\frac{h_w}{0.075}} = 4005 \sqrt{h_w} \tag{2}$$

The relation of air velocity and velocity head expressed in Equation 2 is shown diagrammatically in Fig. 1 for dry air at 69.41 F and 29.921 in. Hg barometer.

The drop in pressure in air distributing systems is due to the *dynamic* losses and the *friction* losses. The friction losses for turbulent flow (which occur in all practical air flow problems) are due to the friction of air against the sides of the duct and to internal friction between air molecules. The dynamic losses are those due to the change in the direction or in the velocity of air flow.

Dynamic losses occur principally at the entrance to the piping, in the elbows, and wherever a change in velocity occurs. The entrance loss is the difference between the actual pressure required to produce flow and the pressure corresponding to the flow produced; it may vary from 0.1 to

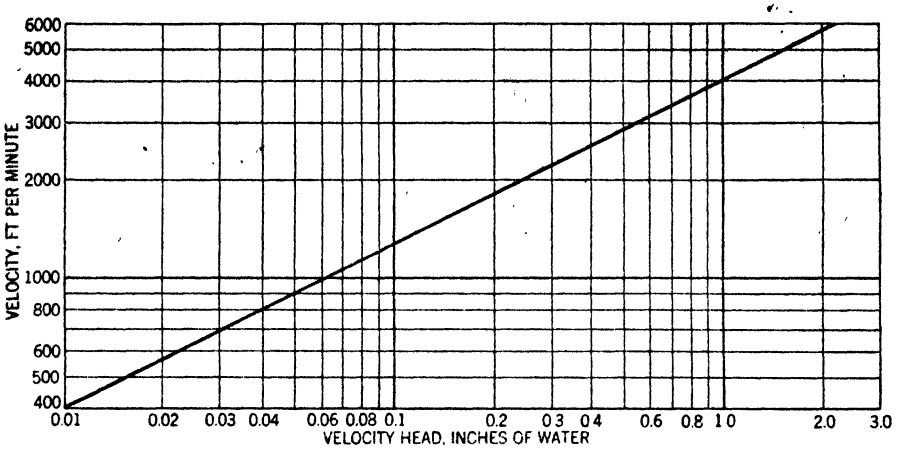


FIG. 1. RELATION BETWEEN VELOCITY AND VELOCITY HEAD FOR STANDARD AIR

0.5 times the velocity head. The pressure loss in elbows must also be allowed for in the design.

FRICTION LOSSES

Friction loss in *straight* ducts is most readily calculated by means of the Air Friction Chart, Fig. 2, which was developed by research at the A.S.H.V.E. Research Laboratory [2]. The range of the chart has recently been modified to include smaller air capacities and duct sizes, and the upper limit of air capacity has been somewhat reduced.

The chart, Fig. 2, is constructed from the basic flow equation:

$$h_f = f \frac{l}{D} \frac{V^2}{2g} \quad (3)$$

where

h_f = head loss due to friction, in feet of fluid flowing.
l = length of conduit, feet.
D = inside diameter of conduit, feet.
V = fluid velocity, feet per second.
g = acceleration due to gravity, 32.17 fps per second.
f = a non-dimensional friction coefficient, which for ventilation work depends upon Reynolds Number and the relative roughness of the conduit. Appropriate values of f were taken from the work of Moody [3].

The air friction chart is based on standard air at 29.921 in. of mercury barometer and 69.41 F, flowing through average, clean, round, galvanized metal ducts having approximately 40 joints per 100 ft. Fig. 2 should not be used to obtain values below the chart by extrapolation because critical flow would occur in this region and values so obtained would be unreliable. For the average application, it should prove sufficiently accurate, without corrections, for any air temperature from 50 F to 90 F, for any relative humidity, and for any normal variation in barometric pressure. For widely varying air pressures or temperatures, or for unusual duct conditions, the friction values obtained from the chart should be corrected.

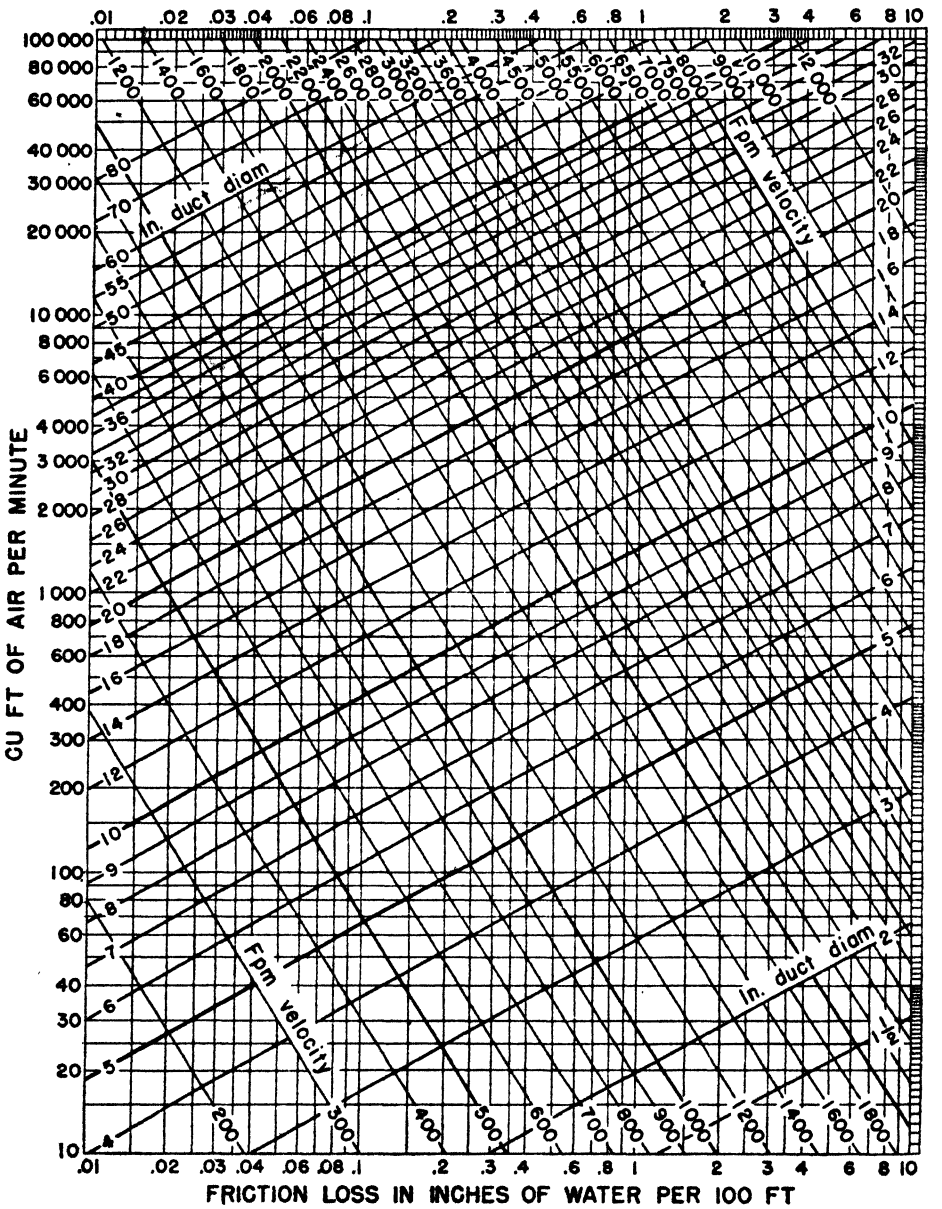


FIG. 2. FRICTION OF AIR IN STRAIGHT DUCTS

(Based on Standard Air at 29.921 In. of Mercury barometric pressure and 69.41 F flowing through average, clean, round, galvanized metal ducts having approximately 40 joints per 100 ft.) Caution: Do not extrapolate below chart.

For ducts of other than standard sheet metal construction, correction factors may be obtained from Fig. 3 [4]. The correction factors shown in Fig. 3 were computed for the values of ϵ, the roughness in feet, shown in Table 1 [4]. The correct friction loss for such ducts may then be determined by multiplying the losses obtained from Fig. 2 by these factors.

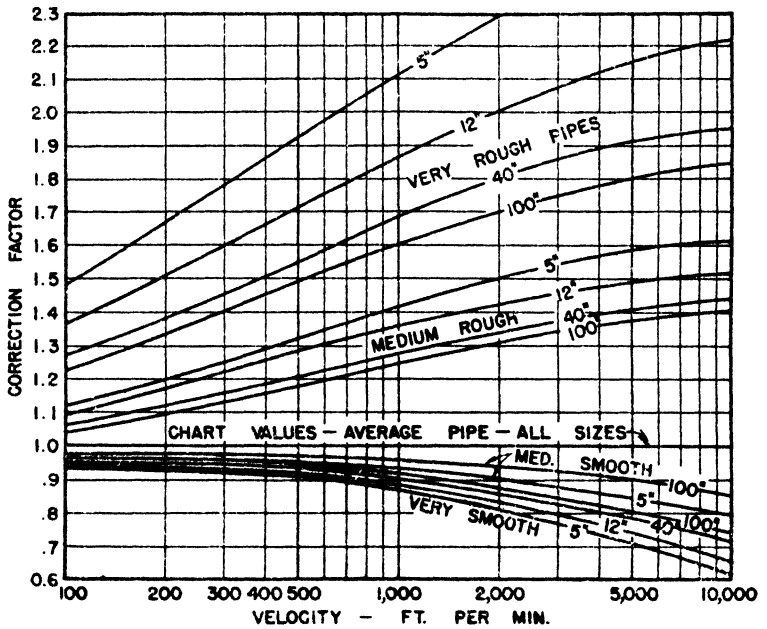


FIG. 3. CORRECTION FACTORS FOR PIPE ROUGHNESS

To correct for pipe roughness multiply friction loss obtained from Fig. 2 by correction factor obtained from Fig. 3

For ordinary ventilating work, friction may be assumed to vary directly as the density without serious error. If temperatures or viscosities are much different from standard, and if precise results are desired, corrections should be made by use of Equation 3, with the appropriate value of the coefficient of friction, f. However, the following approximate equations [2] are presented and will be found sufficiently accurate for most purposes.

For perfectly smooth ducts: $$h_o = h_s \left(\frac{\rho_o}{\rho_s}\right)^{0.81} \left(\frac{\mu_o}{\mu_s}\right)^{0.19} \quad (4)$$

For average ducts, $$h_o = h_s \left(\frac{\rho_o}{\rho_s}\right)^{0.90} \left(\frac{\mu_o}{\mu_s}\right)^{0.1} \quad (5)$$

For very rough ducts, $$h_o = h_s \left(\frac{\rho_o}{\rho_s}\right) \quad (6)$$

where

h = friction loss.

ρ = density.

μ = absolute viscosity.

h, ρ and μ may be in *any consistent units.*
Subscripts o and s refer to *actual operating* and *standard* conditions respectively.

The absolute viscosity of dry air at various temperatures is given in Fig. 4. The effect of relative humidity on viscosity may be neglected.

Examples 1 and 2 illustrate the use of Fig. 2 to determine friction loss and the use of Fig. 3 to apply a correction for roughness.

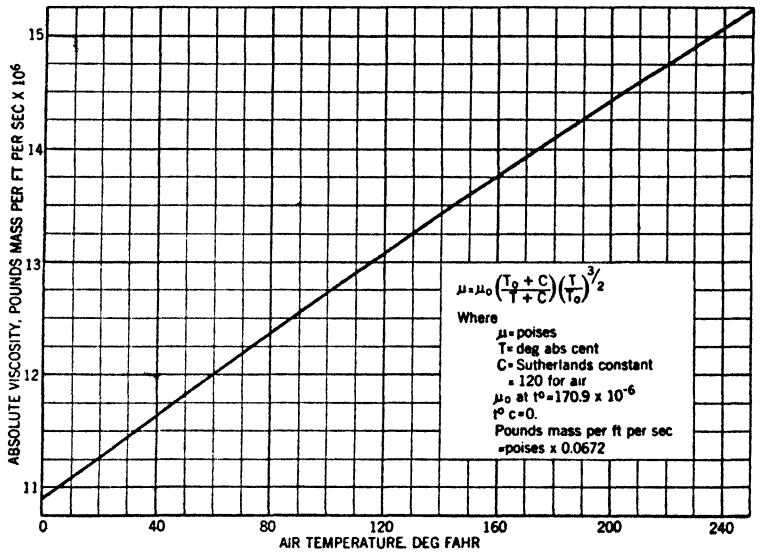


FIG. 4. TEMPERATURE—VISCOSITY CURVE FOR DRY AIR

Example 1. Assume that it is desired to circulate 10.000 cfm of air through 75 ft of 24 in. diameter galvanized duct. Find 10,000 cfm on the left scale of Fig. 2 and move horizontally right to the diagonal line marked 24 in. The other intersecting diagonal shows that the velocity in the pipe is 3200 fpm. Directly below the intersection it is found that the friction per 100 ft is 0.50 in.; then for 75 ft the friction will be 0.75 × 0.50 = 0.38 in. In a like manner any two variables may be determined by the intersection of the lines representing the other two variables.

Example 2. If the duct in Example 1 is very rough, instead of galvanized, with 40 joints per 100 ft, find the total friction.

On Fig. 3 find (by interpolation between 12 in. and 40 in. pipe) the intersection of the 24 in. *very rough pipe* line and the 3200 fpm velocity ordinate and at the left margin read a correction factor of 2. The friction loss in the rough duct is therefore 2 × 0.38 = 0.76 in.

Circular Equivalents of Rectangular Ducts

An air handling system is usually sized first for round ducts and, if rectangular ducts are desired, their sizes are selected to provide air carry-

TABLE 1. VALUES OF ROUGHNESS ε FOR DIFFERENT PIPES[a]

PIPE	DEGREE OF ROUGHNESS	ε ROUGHNESS IN FEET
Drawn Tubing	Very smooth	0.0000015
New Steel or Wrought-Iron Pipe	Medium smooth	0.00015
Galvanized Iron	Average	0.0005
Average Concrete	Medium rough	0.003
Average Riveted Steel	Very rough	0.01

[a]Used in computing values for Fig. 3.

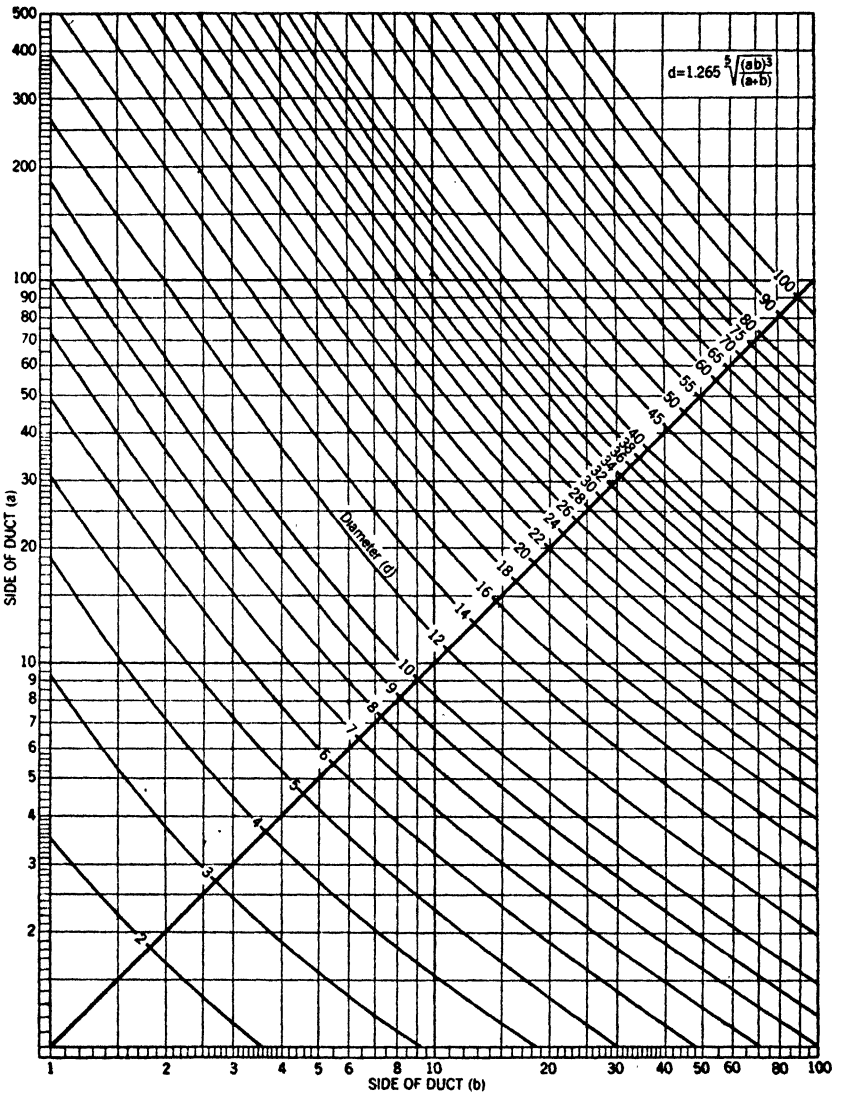


FIG. 5. RECTANGULAR EQUIVALENTS OF ROUND DUCTS

ing capacities equivalent to those of the round ducts originally selected. Table 2 gives directly the rectangular duct sizes equivalent to each size of circular duct in friction and capacity. The values in this table were obtained from the equation:

$$d = 1.265 \sqrt[5]{\frac{(a\,b)^3}{a + b}} \tag{7}$$

where

a = one side of rectangular duct, feet or inches.

b = other side of rectangular duct, feet or inches.

d = equivalent diameter of round pipe for equal friction per foot of length to carry the same capacity, feet or inches.

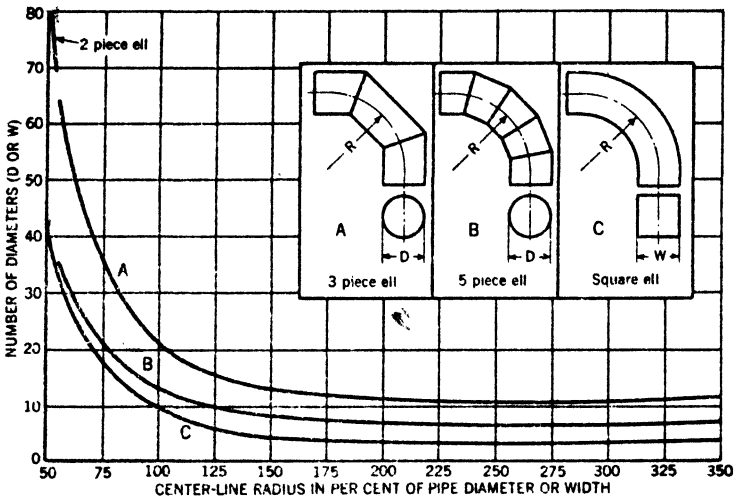


FIG. 6. LOSS OF PRESSURE IN ELBOWS

Rectangular equivalents of round ducts are also given in the curves of Fig. 5 which are plotted from data based on Equation 7. To use the chart, locate the diagonal curve giving the diameter of the round duct. The width and height of an equivalent rectangular or square duct may then be read as the abscissa and the ordinate of any point on the curve.

Multiplying or dividing the length of each side of a pipe by a constant is the same as multiplying or dividing the equivalent round size by the same constant. Thus, if the circular equivalent of an 80 x 24-in. duct is required, it will be twice that of a 40 x 12-in. duct, or $2 \times 23.3 = 46.6$ in.

A comprehensive study of equivalent duct sizes is to be made by the A.S.H.V.E. Research Laboratory for the purpose of determining whether Table 2 and Fig. 5 should be revised.

Elbow Friction Losses

It is customary to express the dynamic and friction losses in elbows as equal to a number of diameters of round pipe, or a number of widths of rectangular pipe, or equivalent length of duct [5]. The curves in Fig. 6 give the number of diameters or widths of pipe which have a frictional

TABLE 2. CIRCULAR EQUIVALENTS OF RECTANGULAR DUCTS FOR EQUAL FRICTION[a]

Side Rectangular Duct	8	8.5	9	9.5	10	10.5	11	11.5	12	12.5	13	13.5	14	14.5	15	15.5	16
3	5.2	5.4	5.5	5.7	5.8	5.9	6.0	6.2	6.3	6.4	6.5	6.6	6.7	6.8	6.9	7.0	7.1
3.5	5.7	5.9	6.0	6.2	6.3	6.5	6.6	6.7	6.9	7.0	7.1	7.3	7.4	7.5	7.6	7.7	7.8
4	6.1	6.3	6.5	6.7	6.8	7.0	7.1	7.2	7.4	7.5	7.7	7.8	7.9	8.1	8.2	8.3	8.4
4.5	6.5	6.7	6.9	7.1	7.2	7.4	7.6	7.7	7.9	8.0	8.2	8.4	8.5	8.6	8.7	8.9	9.0
5	6.9	7.1	7.3	7.5	7.7	7.8	8.0	8.2	8.3	8.5	8.7	8.8	8.9	9.1	9.2	9.4	9.5
5.5	7.3	7.5	7.7	7.8	8.1	8.3	8.5	8.6	8.8	9.0	9.2	9.4	9.5	9.6	9.8	9.9	10.1

[a]Additional sizes: 4 × 5 = 4.9; 4 × 6 = 5.4; 4 × 7 = 5.8; 5 × 5 = 5.5; 5 × 6 = 6.3; 5 × 7 = 6.5.

TABLE 2. CIRCULAR EQUIVALENTS OF RECTANGULAR DUCTS FOR EQUAL FRICTION—(Continued)

Side Rectangular Duct	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	24
8	6.1	6.9	7.6	8.2	8.8															
9	6.5	7.3	8.0	8.7	9.3	9.9														
10	6.8	7.7	8.4	9.2	9.8	10.4	11.0													
11	7.1	8.0	8.8	9.6	10.2	10.9	11.5	12.1												
12	7.4	8.3	9.2	10.0	10.7	11.4	12.0	12.6	13.2											
13	7.6	8.7	9.6	10.4	11.1	11.8	12.5	13.1	13.7	14.3										
14	7.9	8.9	9.9	10.8	11.5	12.3	12.9	13.6	14.3	14.9	15.4									
15	8.2	9.2	10.2	11.1	11.9	12.7	13.4	14.1	14.7	15.3	16.0	16.5								
16	8.4	9.5	10.5	11.4	12.3	13.1	13.8	14.5	15.2	15.8	16.5	17.1	17.6							
17	8.6	9.8	10.8	11.8	12.6	13.5	14.2	15.0	15.7	16.3	17.0	17.6	18.2	18.7						
18	8.9	10.0	11.1	12.1	13.0	13.8	14.6	15.4	16.1	16.8	17.4	18.1	18.7	19.2	19.8					
19	9.1	10.3	11.4	12.4	13.3	14.2	15.0	15.8	16.5	17.2	17.9	18.6	19.2	19.8	20.4	20.9				
20	9.3	10.5	11.6	12.7	13.6	14.5	15.4	16.2	17.0	17.6	18.4	19.0	19.7	20.3	20.9	21.5	22.0			
22	9.7	11.0	12.1	13.2	14.2	15.2	16.1	16.9	17.8	18.5	19.2	19.9	20.6	21.3	21.9	22.5	23.1	23.6	24.2	
24	10.0	11.4	12.6	13.8	14.8	15.8	16.8	17.6	18.5	19.3	20.0	20.8	21.5	22.2	22.8	23.5	24.0	24.7	25.2	26.4
26	10.4	11.8	13.1	14.3	15.4	16.4	17.3	18.3	19.2	20.0	20.8	21.6	22.3	23.0	23.8	24.4	25.1	25.7	26.3	27.5
28	10.8	12.2	13.5	14.8	15.9	17.0	18.0	19.0	19.8	20.7	21.5	22.4	23.1	23.9	24.6	25.3	26.0	26.6	27.3	28.5
30	11.0	12.6	13.9	15.2	16.4	17.5	18.5	19.5	20.5	21.4	22.2	23.1	23.9	24.7	25.4	26.2	26.8	27.5	28.2	29.5
32	11.3	12.9	14.3	15.6	16.9	18.0	19.1	20.1	21.1	22.0	22.9	23.8	24.6	25.4	26.2	27.0	27.7	28.4	29.1	30.5
34	11.6	13.2	14.7	16.1	17.3	18.5	19.6	20.7	21.6	22.6	23.5	24.4	25.3	26.2	26.9	27.7	28.5	29.2	30.0	31.3
36	11.9	13.6	15.1	16.4	17.7	19.0	20.1	21.2	22.2	23.2	24.2	25.1	26.0	26.8	27.7	28.5	29.3	30.0	30.8	32.2
38	12.2	13.9	15.4	16.8	18.2	19.4	20.6	21.7	22.8	23.8	24.8	25.8	26.7	27.5	28.4	29.2	30.0	30.8	31.5	33.1
40	12.5	14.3	15.7	17.2	18.6	19.8	21.1	22.2	23.3	24.4	25.4	26.4	27.3	28.2	29.1	29.9	30.8	31.6	32.4	33.9
42	12.7	14.5	16.1	17.6	19.0	20.3	21.6	22.7	23.8	24.9	25.9	26.9	27.9	28.8	29.8	30.7	31.4	32.2	33.0	34.5
44	13.0	14.8	16.4	18.0	19.4	20.7	22.0	23.1	24.3	25.4	26.5	27.5	28.5	29.5	30.3	31.2	32.1	32.9	33.7	35.3
46	13.3	15.1	16.7	18.4	19.8	21.1	22.4	23.6	24.8	25.9	27.0	28.1	29.1	30.1	31.0	31.9	32.8	33.8	34.6	36.2
48	13.5	15.4	17.0	18.7	20.1	21.5	22.8	24.1	25.2	26.4	27.5	28.6	29.6	30.5	31.6	32.5	33.4	34.3	35.2	37.0
50	13.7	15.7	17.3	19.0	20.4	21.9	23.2	24.5	25.7	26.9	28.0	29.2	30.3	31.3	32.2	33.1	34.1	35.0	35.9	37.6
52	13.9	15.9	17.6	19.2	20.8	22.2	23.6	24.9	26.2	27.4	28.5	29.6	30.7	31.8	32.9	33.8	34.7	35.6	36.5	38.3
54	14.1	16.1	17.9	19.6	21.1	22.6	24.0	25.3	26.6	27.8	29.0	30.1	31.2	32.3	33.4	34.4	35.3	36.3	37.2	38.9
56	14.3	16.3	18.2	19.9	21.5	22.9	24.4	25.7	27.0	28.3	29.5	30.6	31.7	32.8	33.9	34.9	35.9	36.9	37.8	39.6
58	14.6	16.6	18.4	20.2	21.8	23.3	24.7	26.1	27.4	28.7	30.0	31.1	32.2	33.3	34.4	35.4	36.4	37.4	38.4	40.3
60	14.7	16.8	18.7	20.4	22.1	23.6	25.1	26.5	27.8	29.1	30.5	31.6	32.7	33.8	34.9	36.1	37.1	38.1	39.1	40.9
62	15.0	17.0	19.0	20.7	22.4	24.0	25.5	26.9	28.2	29.5	30.9	32.1	33.2	34.3	35.4	36.6	37.7	38.7	39.6	41.6
64	15.1	17.3	19.2	21.0	22.7	24.3	25.9	27.3	28.6	29.9	31.3	32.6	33.7	34.8	35.9	37.1	38.2	39.2	40.2	42.2
66	15.3	17.5	19.5	21.2	23.0	24.6	26.2	27.7	29.0	30.3	31.7	33.0	34.2	35.3	36.4	37.6	38.7	39.8	40.8	42.8

TABLE 2. CIRCULAR EQUIVALENTS OF RECTANGULAR DUCTS FOR EQUAL FRICTION—(CONCLUDED)

SIDE RECTANGULAR DUCT	26	28	30	32	34	36	38	40	42	44	46	48
26	28.6											
28	29.7	30.8										
30	30.7	31.9	33.0									
32	31.7	32.9	34.1	35.2								
34	32.7	33.9	35.1	36.3	37.4							
36	33.7	34.9	36.1	37.3	38.5	39.6						
38	34.6	35.9	37.1	38.4	39.5	40.7	41.8					
40	35.3	36.7	38.0	39.3	40.5	41.7	42.9	44.0				
42	36.0	37.6	39.0	40.3	41.5	42.7	44.0	45.1	46.2			
44	36.9	38.5	39.9	41.2	42.5	43.7	44.9	46.1	47.2	48.4		
46	37.8	39.3	40.8	42.2	43.5	44.8	46.0	47.2	48.4	49.5	50.6	
48	38.5	40.0	41.5	43.0	44.4	45.6	46.9	48.1	49.3	50.5	51.6	52.8
50	39.2	40.8	42.3	43.8	45.2	46.5	47.9	49.1	50.4	51.6	52.9	54.0
52	40.0	41.6	43.1	44.7	46.1	47.5	48.9	50.1	51.3	52.5	53.8	55.0
54	40.7	42.4	44.0	45.5	47.0	48.4	49.9	51.1	52.3	53.5	54.8	56.0
56	41.3	43.0	44.6	46.2	47.7	49.1	50.6	52.0	53.3	54.6	55.9	57.0
58	42.1	43.8	45.4	47.0	48.5	50.0	51.5	52.9	54.2	55.5	56.8	58.0
60	42.7	44.5	46.1	47.8	49.3	50.9	52.3	53.8	55.0	56.4	57.7	58.9
62	43.4	45.1	46.8	48.4	50.0	51.7	53.0	54.5	55.9	57.2	58.5	59.7
64	44.0	45.8	47.5	49.2	50.9	52.4	53.9	55.4	56.8	58.1	59.4	60.6
66	44.7	46.5	48.2	50.0	51.6	53.1	54.7	56.2	57.6	59.1	60.4	61.6
68	45.3	47.2	48.9	50.7	52.2	53.8	55.5	56.9	58.4	59.9	61.3	62.6
70	46.0	47.8	49.5	51.3	52.9	54.5	56.2	57.7	59.1	60.6	62.1	63.5
72	46.5	48.4	50.1	51.9	53.7	55.4	57.0	58.7	60.0	61.3	63.0	64.5

SIDE RECTANGULAR DUCT	50	54	60	66	72	78	84	88
50	55.0							
52	56.1							
54	57.2	59.4						
56	58.3	60.5						
58	59.3	61.6						
60	60.3	62.7	66.0					
62	61.3	63.7	67.1					
64	62.2	64.7	68.2					
66	63.2	65.7	69.3	72.6				
68	64.1	66.6	70.3	73.7				
70	65.0	67.6	71.3	74.8				
72	65.9	68.5	72.3	75.9	79.2			
74	66.8	69.4	73.3	76.9	80.3			
76	67.6	70.3	74.2	77.9	81.4			
78	68.4	71.2	75.2	78.9	82.5	85.8		
80	69.2	72.1	76.1	79.9	83.6	86.9		
82	70.1	73.0	77.1	80.9	84.6	88.0		
84	70.9	73.8	78.0	81.9	85.6	89.1	92.4	
86	71.7	74.6	78.9	82.9	86.6	90.2	93.5	
88	72.5	75.5	79.8	83.9	87.5	91.2	94.6	96.8
90	73.3	76.3	80.6	84.7	88.5	92.2	95.7	97.9
92	74.1	77.1	81.4	85.6	89.5	93.2	96.7	99.0
94	74.8	77.8	82.2	86.5	90.4	94.2	97.8	100.1
96	75.5	78.7	83.0	87.4	91.3	95.2	98.8	101.2

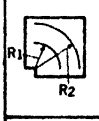
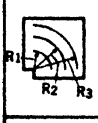
resistance equivalent to the pressure drop in the elbows. Curves *B* and *C* are based on tests of round and square elbows [6] of ordinary good sheet metal construction.

Values obtained from Curve *A* should be used when there is any doubt as to quality of duct construction. It is suggested that this curve be used for rectangular elbows and five-piece elbows as it will thus allow an additional factor of safety without seriously affecting the design.

As indicated in Fig. 6, long radius elbows will offer much less resistance to the flow of air than short radius elbows. Experience has

TABLE 3. EFFECT OF VANES ON PRESSURE LOSS OF 7-INCH SQUARE VENTILATING DUCT[a]

Expressed in feet of total equivalent length of duct (ELD)

SQUARE MITER ELBOW								STANDARD ELBOWS WITH VARIOUS RADII							
	Radius Ratio	R_1/W	0	.2	.4	.6	.8	1.0		Radius Ratio	R_1/W	0	.2	.4	.6	.8	1.0
	ELD, ft		41.1	30.5	27.5	30.1	37.7	38.5		ELD, ft		39.7	23.3	22.0	25.7	28.9	39.7
	Radius Ratio	R_1/W	0	.2	.3					Radius Ratio	R_1/W	0	.2	.3	.4	.5	.6
		R_2/W	0	.4	.5						R_2/W	0	.4	.5	.6	.7	.8
	ELD, ft		41.1	23.5	23.3					ELD, ft		39.7	20.0	22.0	23.0	23.8	25.7
	Radius Ratio	R_1/W	0	.2	.3					Radius Ratio	R_1/W	0	.4	.6	.8	1.0	1.2
		R_2/W	0	.4	.5												
		R_3/W	0	.6	.7												
	ELD, ft		41.1	20.7	22.2					ELD, ft		25.3	17.7	16.5	18.7	23.5	25.6
										Radius Ratio	R_1/W	0	.7	.8	.9	1.0	1.2
VANE	A	B		C		D											
ELD, ft	21.8	17.0		17.9		17.8				ELD, ft		14.2	13.3	13.0	12.7	12.5	12.7

[a]For more complete data see A.S.H.V.E. RESEARCH REPORT No. 1216—Effect of Vanes in Reducing Pressure Loss in Elbows in 7-Inch Square Ventilating Duct, by M. C. Stuart, C. F. Warner and W. C. Roberts (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 409).

Note A: Vane *A* made up of a large number of small splitters; *B* made up of a small number of large splitters bent on a large radius; *C* hollow vanes having different outside and inside curvature; and *D* four splitters with $R/W = 0.4$. Elbow same as *D* except 2 in. trailing edge on the end of each splitter, ELD in feet = 17.0.

Note B: The air velocity has no effect on the loss of elbows when the loss is expressed as equivalent length of duct.

shown that good results may be expected when the radius to the center of the elbow is 1.5 times the pipe diameter or duct width parallel to the radius. Examination of the curve will indicate that little advantage is to be gained by selecting elbows having a centerline radius of more than two diameters[7]. Elbows having a radius of more than three diameters show a slightly increased resistance due to the increased length of pipe but, when used, they reduce the over-all resistance of the system and therefore should not be avoided.

Where space conditions necessitate the use of short radius or miter elbows in square or rectangular duct work, turning vanes should be used to reduce the pressure losses. Rough or raw edges on the vanes should be avoided to prevent objectionable noise. Table 3 shows typical types

of vanes and gives the resistance, expressed in equivalent length of straight pipe, for a 7-in. x 7-in. elbow of each type.

The pressure loss through elbows of less than 90 deg may be assumed to be directly proportional to the ratio of the angle through which the turn is made. The resistance will vary widely for the large degree turns depending upon the aspect ratio and the length of straight pipe between the elbows but, for practical purposes, it may be assumed that the ratio remains proportional to the angle through which the turn is made. Reverse 90 deg elbow turns should be avoided wherever possible but, where used, the friction indicated in Fig. 6 should be doubled for the second elbow. Additional tests are needed on the loss of pressure in elbows and other types of duct fittings in order to reconcile the difference between values shown in Fig. 6 and results of more recent tests shown in Table 3. A study of this subject will be undertaken at the A.S.H.V.E. Research Laboratory for the purpose of obtaining such data.

PROPORTIONING THE LOSSES

The entrance loss through the outside air intake louvers will vary with the design of the louvers and method of connection to the system. The louvers and connecting duct will have a friction resistance of from 0.25 to 1.00 times the velocity pressure. Therefore, the total entrance loss will vary from 1.25 to 2.00 h_w. Common practice is to use 1.5 h_w for a 75 per cent free area louver with connecting duct having 15 deg tapered sides. Wherever air passes through a plenum space having a negligible velocity, allowance must be made for the loss in velocity head. This loss in velocity head may be taken as the difference in velocity heads in the plenum and the duct. Where the ducts are very smooth with long transformation fittings, a regain in static pressure is sometimes allowed, but ordinary construction does not warrant a consideration of this factor, and it is customary to neglect it. When it is allowed, the regain is estimated at one-half the difference between the velocity pressure at the fan outlet and at the last run of pipe.

Other losses of pressure occur through the heating units, at the air washer and at air filters. In the design of an ideal duct system, all factors should be considered and the air velocities proportioned so that the resistance will be practically equal in all ducts regardless of length.

DUCT SIZES

Ducts and flues for gravity circulation must be sized so that the friction loss will not exceed 50 per cent of the available chimney effect due to the temperature and height of the column of heated air. Duct systems for mechanical circulation may be sized so as to have much higher pressure losses than gravity systems. The total pressure of these systems is limited to the pressure which the fan will produce.

The general rules to be followed in the design of a duct system are:

1. The air should be conveyed as directly as possible at reasonable velocities to obtain the results desired with greatest economy of power, material and space.

2. Sharp elbows and bends should be avoided unless turning vanes are used.

3. Transformation pieces should be made as long as possible. The angle between the sides and axis of the duct should never exceed 30 deg and, where possible, 15 deg should be made the maximum.

4. Especial care should be taken to maintain a true cross-section and not to restrict the air flow either in transformation pieces or in elbows.

5. Rectangular ducts or flues should be made as nearly square as possible. Good practice limits the ratio between the long side and the short side to 3 to 1. In no case should this ratio exceed 10 to 1.

6. Wherever possible, ducts should be constructed of smooth material such as sheet metal. Where masonry ducts are used, proper allowance for the surface friction coefficient should be made.

7. The use of furred spaces, spaces between joists, etc., should be avoided unless lined with sheet metal.

Procedure for Duct Design

The general procedure for designing a duct system is outlined in the several items listed herewith:

1. Study the plan of the building and draw in roughly the most convenient system of ducts, taking cognizance of the building construction, avoiding all obstructions in steel work and equipment, and at the same time maintaining a simple design.

2. Arrange the positions of duct outlets to insure the proper distribution of air.

3. Divide the building into zones and proportion the volume of air necessary for each zone.

4. Determine the size of each outlet, based on the volume as obtained in the preceding paragraph, for the proper outlet velocity and throw.

5. Calculate the sizes of all main and branch ducts by either of the following two methods:

a. Velocity Method. Select the velocity in the various sections, reducing the velocity from the point of leaving the fan to the point of discharge to the room. In this case the pressure loss of each section of the duct is calculated separately and the total loss found by adding together the losses of the various sections of the continuous run.

b. Friction Pressure Loss Method. Proportion the duct for equal friction pressure loss per foot of length.

6. Calculate the friction for the duct offering the greatest resistance to the flow of air, which resistance represents the static pressure which must be maintained at the fan outlet or in the plenum space to insure distribution of air in the duct system. The duct having the greatest resistance will usually be that having the longest run, although not necessarily so.

Air Velocities

The air velocities given in Table 4 have been found to give satisfactory results in engineering practice. Where the higher velocities are used, the ducts should be cross-braced to prevent breathing, buckling or vibration, and should be constructed of heavier gage metal. At the higher velocities it is particularly important to design the ducts for minimum resistance. As high velocities at one point offset the effect of proper design in all other parts of the system, emphasis should be placed on the importance of air velocities, elbow design, location of dampers, fan connections, grille and register approach connections, and similar details. For industrial buildings, noise is seldom given much consideration, and main duct velocities as high as 2800 or 3000 fpm are sometimes used but, when these velocities are used, due consideration should be given to duct design, resistance pressure, fan efficiencies and motor horsepower. For department stores and similar buildings, 2000 to 2200 fpm are sometimes used in main ducts where noise is not objectionable and space conditions warrant it.

Where high velocity diffusing outlets are used, the duct velocity should not be less than the throat velocity of the diffusers, as dynamic losses

occur wherever velocities are stepped up or down. One recent trend in grille design is toward the use of much higher grille and branch duct velocities. Some installations have been made with velocities as high as 1600 fpm in branches and through the net area of grilles, but many of these have proven unsatisfactory because of noise and drafts.

Grille manufacturers publish selection tables which size the grilles for volume of air, temperature differential, and distance of throw. In following these tables, maximums should be avoided and the manner in which the duct connects to the grille should be given careful consideration. Most of the selection tables are based on straight approach to the grille. Elbow connections to supply grilles should be provided with turning vanes to equalize the face velocity. See Chapter 40 for a discussion of grilles.

TABLE 4. RECOMMENDED AND MAXIMUM DUCT VELOCITIES

DESIGNATION	RECOMMENDED VELOCITIES, FPM			MAXIMUM VELOCITIES, FPM		
	Residences	Schools, Theaters, Public Buildings	Industrial Buildings	Residences	Schools, Theaters, Public Buildings	Industrial Buildings
Outside Air Intakes[a]	700	800	1000	800	900	1200
Filters[a]	250	300	350	300	350	350
Heating Coils[a]	450	500	600	500	600	700
Air Washers	500	500	500	500	500	500
Suction Connections	700	800	1000	900	1000	1400
Fan Outlets	1000–1600	1300–2000	1600–2400	1700	1500–2200	1700–2800
Main Ducts	700–900	1000–1300	1200–1800	800–1000	1100–1400	1300–2000
Branch Ducts	600	600–900	800–1000	700	800–1000	1000–1200
Branch Risers	500	600–700	800	650	800–900	1000

[a]These velocities are for total face area, not the net free area.

Fan outlet velocities are discussed in Chapter 32 and will not be dealt with here except to indicate that fan noises should be given proper consideration.

Main Trunk Ducts

Main trunk ducts with branches are commonly used to convey the air from the fan to the grille or register outlets in preference to individual ducts from the fan to these outlets. The velocities in these ducts and branches vary according to the nature of the installation and the degree of quietness desired. The recommended velocities in Table 4, with good construction, should give satisfactory results. The maximum velocities indicated should not be used except where noise is not a deciding factor.

Velocity Method

The velocity method of designing a duct system involves the arbitrary selection of velocities for various sections of the duct system with the

highest velocities at the fan and progressively lower velocities toward the duct openings to the room. To find the total static pressure against which the fan must operate, the static pressure loss of each section must be calculated separately and the total loss found by adding the individual losses of the various sections of the run having the highest resistance. Usually this is the longest run but in some cases a shorter run may have more elbows, transformations, booster heaters, etc., which will cause it to have a higher resistance pressure. This method requires judgment and experience in choosing the proper velocities to approach equal friction for all lengths of run but many engineers believe that the velocity method is handier to use than other methods and will give satisfactory results for most practical applications. The air velocities given earlier in this chapter are helpful in choosing proper velocities. Adjustable dampers or splitters are used to regulate air quantities delivered.

Equal Friction Method

The equal friction method of design is sometimes preferred because it does not require nearly so much judgment and experience in selecting the proper velocities in the various sections of a system. The usual procedure in this method of design is to select the main duct velocity to be consistent with good practice from a standpoint of noise for a particular type of building. This velocity should be less than the fan outlet velocity. All main ducts and branch ducts are sized for equal friction per unit length by the use of Fig. 2, and Table 2 or Fig. 5.

In cases where the fan or factory assembled air conditioning unit has a limited external resistance, it is necessary to divide the available resistance by the total equivalent length of the longest or most complicated run of duct to determine the resistance per 100 ft and then to size all ducts at this resistance value. This will automatically determine the duct velocities and give the desired total duct resistance. A further refinement, which is sometimes used in large systems, is to size each branch duct so that it has a resistance equal to the resistance of the main system at the point of juncture. Even when this refinement is added, regulating dampers are recommended in each branch.

After the duct system is designed the frictional resistance is calculated and tabulated together with the resistance of all component parts. The fan is then selected for the required volume of air, static pressure and outlet velocity.

Typical calculations for design of an air distribution system are given in Examples 3 and 4.

Example 3. Fig. 7 shows a typical layout of an air distribution system which is applicable for ventilation of hotel dining rooms and offices. The volume of air in cubic feet per minute for the room is determined on the basis of the number of air changes per hour required. In the example shown, the room ventilated is a hotel dining room 135 ft x 85 ft x 15 ft. A 7½-min air change (8 air changes per hour) is assumed for proper ventilation, giving 22,935 cfm as the air required.

The free area of the outdoor air inlet is based on a velocity of 1000 fpm or 22,935 ÷ 1000 = 22.94 sq ft. The main duct velocity selected from Table 4 is 1250 fpm which gives a main duct area of 22,935 ÷ 1250 = 18.354 sq ft (60 × 44 in.). From Table 2 a 60 × 44 in. duct is approximately equivalent to 56 in. diameter.

Referring to Fig. 2, a volume of 22,935 cfm through a 56 in. diameter duct gives a resistance of 0.033 in. per 100 ft. The amount of air to be handled by each section of pipe is shown in Fig. 7, and by locating each of these values on the 0.033 in. friction line,

the round pipe sizes are obtained and then, referring to Table 2, the equivalent rectangular sizes are selected as shown in Table 5.

The pressure at the outlets nearest the fan will be greater than at the pipes farther along the run so that the former will tend to deliver more than the calculated amount of air. To remedy this condition, volume regulating dampers should be located at the base of each riser, or in each branch duct, and adjusted for proper distribution. At points where branches leave the main it may be advisable, depending upon the nature of the installation, to install adjustable splitters similar to those shown in Fig. 7 where the main duct divides into the 58 x 30 in. and 50 x 30 in. branches.

Resistance Losses for the System

(1)	Outdoor air intake, 1000 fpm velocity (1.5 heads × 0.0625)	0.094 in.
(2)	Filters (from manufacturer's tables)	0.250 in.
(3)	Tempering coil loss (from manufacturer's tables)	0.074 in.
(4)	Air washer loss (from manufacturer's tables)	0.250 in.
(5)	Reheating coil loss (from manufacturer's tables)	0.083 in.
(6)	Duct resistance:	
	The longest run is	= 150 ft
	Two, 58 x 30 in. elbows (150% ratio) $\frac{2 \times 13 \times 58}{12}$	= 126 ft
	Two, 30 x 15 in. elbows (150% ratio) $\frac{2 \times 13 \times 30}{12}$	= 65 ft
	Three, 15 x 30 in. elbows (75% ratio) $\frac{3 \times 35 \times 15}{12}$	= 131 ft
	Total equivalent run	472 ft
	472 ft at 0.033 in. per 100 ft	0.156 in.
(7)	Allowance for damper adjustment, 25% of 0.156	0.039 in.
(8)	Supply grille resistance (from manufacturer's tables)	0.036 in.
	Total static pressure loss of system	0.982 in.

The fan is selected from the manufacturer's ratings to deliver 22,935 cfm at a static pressure of 0.982 in. as outlined in Chapter 32.

Example 4. If the rooms and offices of the hotel building of Example 3 are to be served from a manufactured unit with a capacity of 22,935 cfm against an external resistance of 0.35 in., the known resistances are calculated as:

(1)	Outdoor air inlet	0.094 in.
(2)	Supply grille resistance (from manufacturer's tables)	0.036 in.
	Total known resistance	0.130 in.

Subtracting this from the total available resistance: 0.35 in. − 0.130 in. = 0.220 in. available for duct resistance and damper adjustment.

If 25 per cent is allowed for damper adjustment, the total allowable duct friction = 0.220 ÷ 1.25 = 0.176 in.

Known length of run	150 ft

The duct width is then estimated for the following elbow calculations:

Four 150% ratio elbows, 4 x 13 x 3.5 ft	182 ft
Three 75% ratio elbows, 3 x 35 x 1.5 ft	158 ft
Total estimated length	490 ft

The duct friction per 100 ft is then 0.176 ÷ 4.90 = 0.036 in. and the mains and branches are sized from the 0.036 in. friction line in Fig. 2.

If it is desired to size each branch for equal resistance, the total resistance back to the point of juncture is calculated and the branch is then sized in a manner similar to that outlined in Example 4.

TABLE 5. PIPE SIZES FOR EXAMPLE 3[a]

VOLUME OF AIR (CFM)	DIAMETER OF PIPE (INCHES)	EQUIVALENT SIZE OF RECTANGULAR DUCT (INCHES)
22,935	56	60 x 44
12,510	45	58 x 30
10,425	42	50 x 30
8,340	39	42 x 30
6,255	35	42 x 24
4,170	29.5	30 x 24
2,085	23	30 x 15

[a]Velocity through grilles (not shown) to be approximately 300 fpm.

DUCT CONSTRUCTION DETAILS

Straight sections of round duct are usually formed by rolling the sheets to the proper radius and grooving the longitudinal seam. Rectangular ducts are generally constructed by breaking the corners and grooving the longitudinal seam, although some fabricators still use the standing seam due to lack of equipment. Elbows and transformation sections are generally formed with *Pittsburgh* corner seams because this seam is easier to lock in place than the double seam, but complicated fittings such as double compounded elbows are usually constructed with double seam corners. The construction of these various seams as well as the types of girth connections are shown in Fig. 8. The application of the various slips and connections is outlined in Table 6. The end slip may be used wherever *S* slips are recommended. Where drive slips are used the end slip may be applied on the narrow side of the duct and the drive slips on only the maximum side. Ducts 25 to 30 in. in size should be reinforced between the joints, but not necessarily at the joint. Ducts 31 in. and up should be reinforced at the joint and between the joints; if drive slips are used the

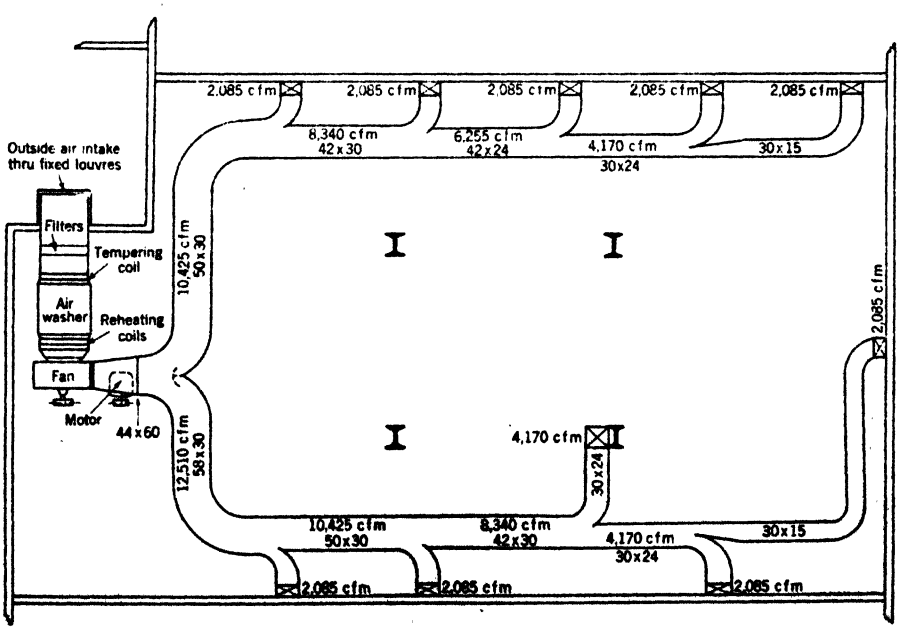


FIG. 7. TYPICAL LAYOUT OF AIR DISTRIBUTION SYSTEM

angles are usually riveted to the duct about 2 in. from the slips. It is good practice to cross-break or kink all flat surfaces to prevent vibration or buckling due to the air flow and accompanying variations in internal pressure. Round ducts are sometimes swedged 1.5 in. from the ends so that the larger end will butt against the swedge and are held in place with sheet metal screws. Where swedges are not used it is general practice to paste the joint with asbestos paper to insure a tight joint.

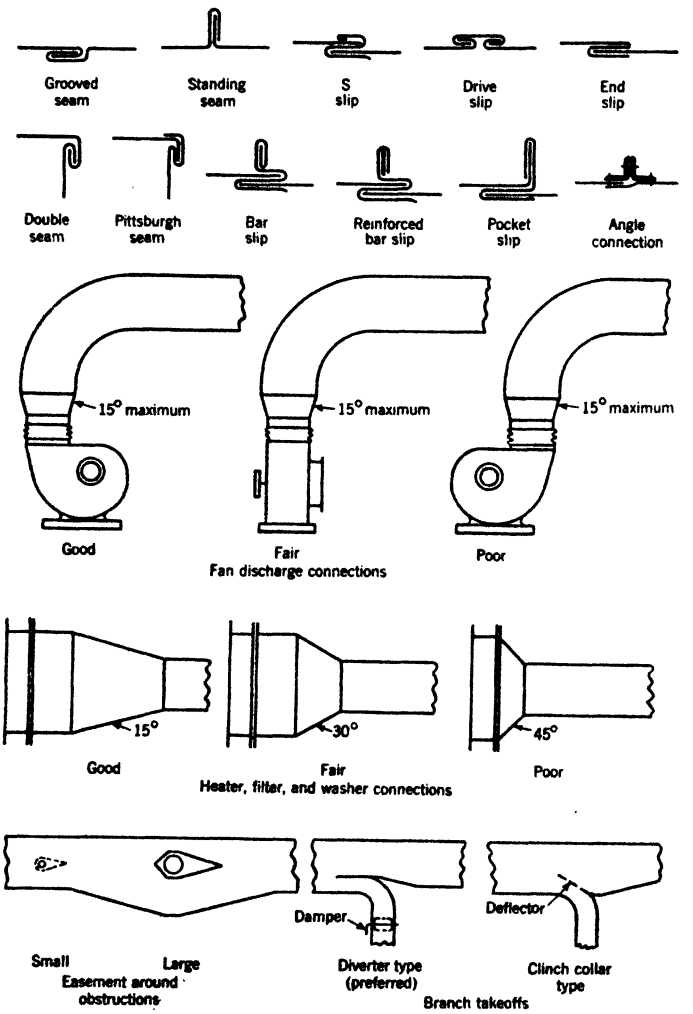


FIG. 8. SHEET METAL DUCT AND ARRANGEMENT DETAILS

The construction of elbows and changes of shape cannot be definitely outlined because of the varied conditions encountered in the field, but in general long radius elbows and gradual changes in shape tend to maintain uniform velocities accompanied by decreased turbulence, lower resistance and a minimum of noise.

Heavy canvas connections (asbestos cloth if there is a fire hazard) are recommended on both the inlet and outlet to all fans. The fan discharge connections shown in Fig. 8 are marked *good*, *fair*, and *poor* in the order

TABLE 6. RECOMMENDED SHEET METAL GAGES FOR RECTANGULAR DUCT CONSTRUCTION[a]

U. S. STD. GAGE	MAXIMUM SIDE, INCHES	TYPE OF TRANSVERSE JOINT CONNECTIONS[b]	BRACING
26	Up to 12	S, Drive, Pocket or Bar Slips, on 7 ft 10 in. centers	None
24	13 to 24	S, Drive, Pocket or Bar Slips, on 7 ft 10 in. centers	None
	25 to 30	S, Drive, 1 in. Pocket or 1 in. Bar Slips, on 7 ft 10 in. centers[c]	1 x 1 x ⅛ in. angles 4 ft from joint
22	31 to 40	Drive, 1 in. Pocket or 1 in. Bar Slips, on 7 ft 10 in. centers[c]	1 x 1 x ⅛ in. angles 4 ft from joint
	41 to 60	1½ in. Angle Connections, or 1½ in. Pocket or 1½ in. Bar Slips with 1⅜ in. x ⅛ in. bar reinforcing on 7 ft 10 in. centers[c]	1½ x 1½ x ⅛ in. angles 4 ft from joint
20	61 to 90	1½ in. Angle Connections, or 1½ in. Pocket or 1½ in. Bar Slips 3 ft 9 in. maximum centers with 1⅜ x ⅛ in. bar reinforcing	1½ x 1½ x ⅛ in. diagonal angles, or 1½ x 1½ x ⅛ in. angles 2 ft from joint
18	91 and up	2 in. Angle Connections or 1½ in. Pocket or 1½ in. Bar Slips 3 ft 9 in. maximum centers with 1⅜ x ⅛ in. bar reinforcing[d]	1½ x 1½ x ⅛ in. diagonal angles, or 1½ x 1½ x ⅛ in. angles 2 ft from joint

[a]For normal pressures and velocities (see Table 4) utilized in typical ventilating and air conditioning systems. Where special rigidity or stiffness is required, ducts should be constructed of metal two gages heavier. All uninsulated ducts 18 in. and larger should be cross-broken. Cross-breaking may be omitted on uninsulated ducts if two gages of heavier metal are used.

[b]Other joint connections of equivalent mechanical strength and air tightness may be used.

[c]Duct sections of 3 ft 9 in. may be used with bracing angles omitted, instead of 7 ft 10 in. lengths with joints indicated.

[d]Ducts 91 in. and larger require special field study for hanging and supporting methods.

of the amount of turbulence produced. An inspection of the heater connections shown in Fig. 8 will readily show that uniform velocity through the heater cannot be expected in the diagram noted *poor*. When obstructions cannot be avoided, the duct area should never be decreased more than 10 per cent and then a *streamlined* collar should be used. Larger obstructions require an increase in the duct size in order to maintain as nearly uniform velocity as possible. Branch take-offs should always be arranged to cut or slice into the air stream in order to reduce as far as possible the losses in velocity head.

The recommended gages for sheet metal duct construction are given in Table 6. Weights of sheet metal per square foot of surface for different gages are given in Table 7. The weights of various gages and the areas for any length of run of rectangular sheet metal ducts may also be determined from Fig. 9. The bottom scale represents the sum of the two sides of the duct and the oblique lines give the length of run in feet. Proceeding horizontally to the right from the intersection of vertical and oblique lines on the chart, the area of the duct may be determined in the first vertical scale. The scales to the right give the weights of the duct run for different gages of metal. In calculating the weights of duct, it is considered good practice to allow 20 per cent additional for weights of joints and bracings. Various weights and thicknesses of standard copper sheets will be found in Table 8.

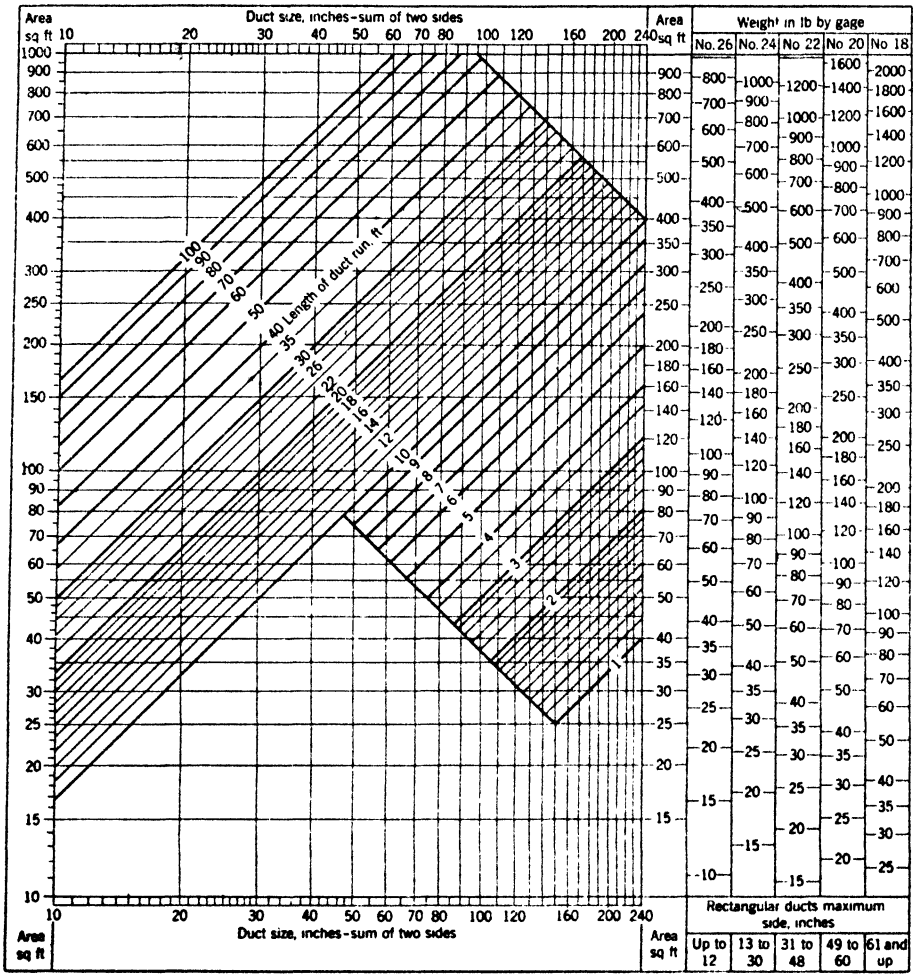


FIG. 9. AREA AND WEIGHT OF RECTANGULAR SHEET METAL DUCTS

HEAT LOSSES FROM DUCTS

The thermal transmittance U for ducts can be found as follows:

For uninsulated metal duct, $$U = \frac{1}{\frac{1}{f_i} + \frac{1}{f_o}} \quad (8)$$

For uninsulated non-metallic ducts, $$U = \frac{1}{\frac{1}{f_i} + \frac{x}{k} + \frac{1}{f_o}} \quad (9)$$

where U, f_i, f_o, x and k are as defined on page 769.

Where x is small and k is large, however, this factor $\frac{x}{k}$ is of little importance and may be neglected.

Film conductance f_i for air flowing in ducts apparently depends only on the velocity of the air and the diameter of the duct. A fairly reliable inside coefficient can be calculated from Schultz's modified equation:

$$f_i = \frac{0.32 V_a^{0.8}}{D^{0.25}} \quad (10)$$

TABLE 7. WEIGHTS OF SHEET METAL USED FOR DUCT CONSTRUCTION

U. S. STD. GAGE	BLACK SHEETS				GALVANIZED SHEETS[a]			
	Approximate Thickness, In.		Weight Per Square Foot		Approximate Thickness, In.		Weight Per Square Foot	
	Steel	Iron	Ounces	Pounds	Steel	Iron	Ounces	Pounds
30	0.0123	0.0125	8	0.500	0.0163	0.0165	10.5	0.656
28	0.0153	0.0156	10	0.625	0.0193	0.0196	12.5	0.781
26	0.0184	0.0188	12	0.750	0.0224	0.0228	14.5	0.906
24	0.0245	0.0250	16	1.000	0.0285	0.0290	18.5	1.156
22	0.0306	0.0313	20	1.250	0.0346	0.0353	22.5	1.406
20	0.0368	0.0375	24	1.500	0.0408	0.0415	26.5	1.656
18	0.0490	0.0500	32	2.000	0.0530	0.0540	34.5	2.156
16	0.0613	0.0625	40	2.500	0.0653	0.0665	42.5	2.656
14	0.0766	0.0781	50	3.125	0.0806	0.0821	52.5	3.281
12	0.1072	0.1094	70	4.375	0.1112	0.1134	72.5	4.531
11	0.1225	0.1250	80	5.000	0.1265	0.1290	82.5	5.156
10	0.1379	0.1406	90	5.625	0.1419	0.1446	92.5	5.781

[a]Galvanized sheets are gaged before galvanizing and are therefore approximately 0.004 in. thicker.

where

V_a = velocity of air in duct, feet per second.

D = inside diameter of duct, feet.

Film conductance f_o depends on a number of variables including temperature, diameter, and emissivity of the outer surface and can be calculated from data in Chapter 5. From this explanation, it is seen that it is unwise to recommend a given value of U for all uninsulated metal ducts.

The heat loss from a given length of duct can be expressed by:

$$Q = UPl\left[\left(\frac{t_1 + t_2}{2}\right) - t_3\right] \tag{11}$$

The heat given up by the air in the duct is:

$$Q = 0.24\ W\ (t_1 - t_2) = 14.4\ A V_m \rho_v\ (t_1 - t_2) \tag{12}$$

Equating (11) and (12):

$$\frac{t_1 + t_2 - 2t_3}{t_1 - t_2} = \frac{28.8\ A V_m \rho_v}{UPl}$$

Let $y = \dfrac{28.8\ A V_m \rho_v}{UPl}$ for rectangular ducts, and $\dfrac{7.2DV_m \rho_v}{Ul}$ for round

TABLE 8. WEIGHTS AND THICKNESSES OF STANDARD COPPER SHEETS[a]
Rolled to Weight

WEIGHT PER SQUARE FOOT		THICKNESS, INCHES		NEAREST GAGE NO.		
Ounces	Pounds	Decimal Equivalent	Nearest Fraction	B. & S.	Stubs	U. S. STD.
10	0.625	0.0135	1/64	27	29	29
12	0.750	0.0162	1/64	26	27	28
14	0.875	0.0189	1/64	25	26	26
16	1.000	0.0216	1/32	23	24	25
18	1.125	0.0243	1/32	22	23	24
20	1.250	0.0270	1/32	21	22	23
24	1.500	0.0324	1/32	20	21	22
28	1.750	0.0378	1/32	19	20	20
32	2.000	0.0432	3/64	17	19	19
36	2.250	0.0486	3/64	16	18	18
40	2.500	0.0540	3/64	15	17	17
44	2.750	0.0594	1/16	15	17	17
48	3.000	0.0648	1/16	14	16	16
56	3.500	0.0756	5/64	13	15	14
64	4.000	0.0864	3/64	11	14	13

[a]Variations from these weights must be expected in practice.

ducts, and solve for t_1 and t_2:

$$t_1 = \frac{t_2 (y + 1) - 2t_3}{(y - 1)} \quad (13) \qquad t_2 = \frac{t_1 (y - 1) + 2t_3}{(y + 1)} \quad (14)$$

For low velocities and long ducts of small cross-section, a somewhat more accurate formula may be used as follows:

$$t_2 = \frac{t_1 - t_3}{e^{\left(\frac{UPl}{14.4 A \rho_v V_m}\right)}} + t_3 \quad (15)$$

Symbols used in these equations are listed at end of chapter.

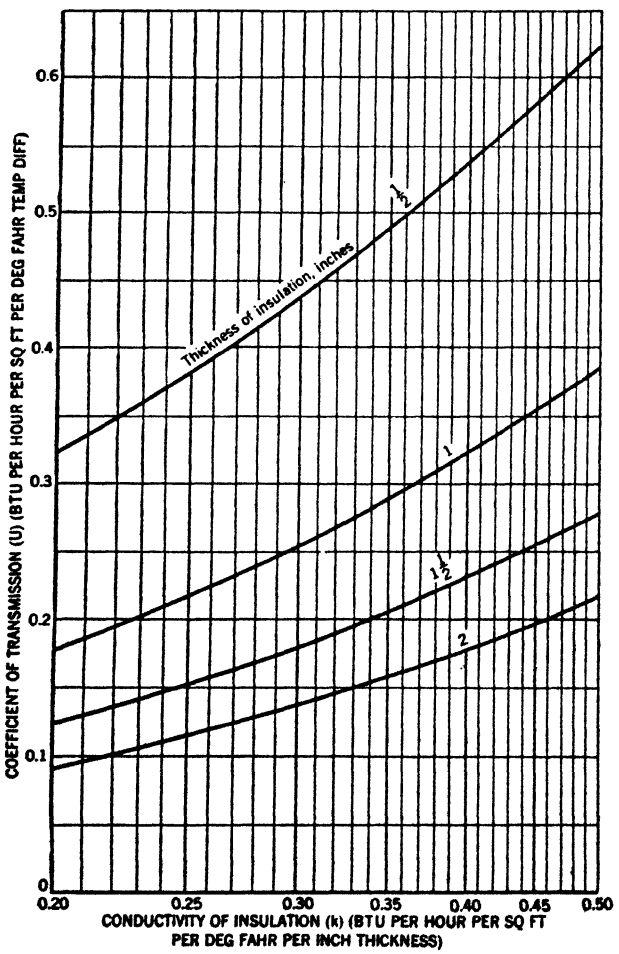


FIG. 10. HEAT LOSS COEFFICIENTS FOR INSULATED DUCTS[a]

[a]For round ducts less than 30 in. diameter, increase heat transmission values by the percentages shown.

THICKNESS OF INSULATION (Inches)	½	1	1½	2
21 to 30 in. Duct Diameter	1%	2%	3%	4%
12 to 21 in. Duct Diameter	3%	5%	7%	9%

In using Equations 13, 14, and 15, one of the duct air temperatures will be unknown and will be obtained by substitution of the other known or assumed values.

Heat loss coefficients for insulated ducts with various conductivities are given in Fig. 10. The conductivities of various materials, which are based on mean temperatures, ranging from about 70 to 90 F, will be found in Table 2 of Chapter 6. For cases where the mean temperature is other than that at which the test was conducted, a correction should be made. However, in most cases the effect of this factor will be small and may be neglected.

Example 6. Determine the entering air temperature and heat loss for a duct 24 × 36 in. cross-section and 70 ft in length, insulated with ½ in. of a material having a conductivity of 0.35 Btu at 86 F mean temperature, carrying air at a velocity of 1200 fpm, measured at 70 F, to deliver air at 120 F with air surrounding the duct at 40 F.

Solution. Referring to Fig. 10, the over-all heat transmission coefficient is found to be 0.49 Btu. From Table 1, Chapter 3 the density of air at 70 F and 29.921 in. Hg is found to be 1/13.348 = 0.0749 lb per cubic foot. Substituting these and the other given values in Equation 13:

$$y = \frac{28.8 \times 6 \times 1200 \times 0.0749}{0.49 \times 10 \times 70} = 45.3$$

$$t_1 = \frac{120\ (45.3 + 1) - 80}{45.3 - 1} = 123.7$$

Substituting in Equation 11:

$$Q = 0.49 \times 10 \times 70 \left[\left(\frac{123.7 + 120}{2} \right) - 40 \right] = 28{,}100 \text{ Btu per hour.}$$

For special considerations which apply to insulation of ducts in marine installations see Chapter 49.

LETTER SYMBOLS USED IN CHAPTER 41

μ_o = absolute viscosity of air under actual (operating) conditions, any consistent units.
μ_s = absolute viscosity of air under standard conditions, any consistent units.
ρ_a = density of air, pounds per cubic foot.
ρ_o = density of air under actual (operating) conditions, any consistent units.
ρ_s = density of air under standard conditions, any consistent units.
ρ_v = density of air at specified temperature at which velocity, V_m, is measured, pounds per cubic foot.
A = cross-section area of duct, square feet.
a = length of one side of rectangular duct, feet or inches. (Other side is b.)
b = length of one side of rectangular duct, feet or inches. (Other side is a.)
D = inside diameter of conduit, feet.
d = equivalent diameter, feet or inches.
e = Naperian base of logarithms = 2.718.
f = non-dimensional friction coefficient.
f_i = surface conductance (inside) Btu per (hour) (square foot) (Fahrenheit degree).
f_o = surface conductance (outside) Btu per (hour) (square foot) (Fahrenheit degree).
g = acceleration due to gravity, 32.17, feet per (second) (second).
h_o = friction loss under actual (operating) conditions, any consistent units.
h_f = friction loss, feet of fluid flowing.
h_s = friction loss under standard conditions, any consistent units.
h_w = velocity head or pressure, inches of water.
l = length of conduit, feet.
P = perimeter of duct, feet.
Q = heat loss through duct walls, Btu per hour.
t_1 = temperature of air entering duct, Fahrenheit degrees.

t_2 = temperature of air leaving duct, Fahrenheit degrees.
t_3 = temperature of air surrounding duct, Fahrenheit degrees.
U = thermal transmittance coefficient, Btu per (hour) (square foot) (Fahrenheit degree).
V = fluid velocity, feet per second.
V_a = velocity of air in duct, feet per second.
V_m = velocity of fluid, feet per minute.
W = weight of air through duct, pounds per hour.
x = thickness, inches.

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Chapter 42

SOUND CONTROL

Unit of Noise Measurement, Apparatus for Measuring Noise, General Problem, Kinds of Noise, Noise Transmitted Through Ducts, Design Room Noise Level, Noise Generated by Fan, Natural Attenuation of Duct System, Duct Sound Absorbers, Air Supply Noises, Grille Selection, Cross Transmission Between Rooms, Controlling Vibration from Machine Mountings

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IN ventilating and air conditioning a building or a room, the effect of the mechanical system employed must be considered on the acoustics of the space conditioned. It is important to consider also that the use of air conditioning often permits keeping the windows closed, thus giving relief from certain external noises, but at the same time increasing the necessity of providing adequate sound control.

It is assumed that in a given space the architect and acoustical engineer have produced a room or rooms which are satisfactory for speech, music, or other uses. The ventilating engineer's sole function is to ventilate and air condition these rooms properly so that they will be physically comfortable without adding any acoustical hazards.

UNIT OF NOISE MEASUREMENT

According to an international standard, two terms are used for noise measurement. The *decibel* (db) is the physical unit for expressing intensity or pressure levels. The *phon* is the unit of loudness level. The loudness level, in phons, of any sound is by definition equal to the intensity level in decibels of a thousand cycle tone which sounds equally loud. The decibel is defined by the relation $N = 10 \log_{10} \frac{I_i}{I_o}$, where N is the number of decibels by which the intensity flux I_i exceeds the intensity flux I_o. The intensity flux is the measure of the intensity of a sound wave and is defined in terms of watts per square centimeter passing through a unit area of wave front in a freely traveling plane wave. It is usually more convenient to select an arbitrary reference intensity for I_o and express all other intensities in terms of decibels above that level. For this purpose a reference intensity of 10^{-16} watts per square centimeter has been selected. This intensity is slightly less than the threshold of audibility for the average ear at a frequency of 1,000 cycles per second. This reference level also corresponds to a pressure of 0.0002 dynes per square centimeter for sound in air at usual room temperatures.

A stated sound level in decibels, unless otherwise defined, will thus be related to a threshold of 10^{-16} watts. For example, a level of 60 db above this reference threshold is 10^{-10} watts. In a similar manner, when sound measurements are given in actual intensity or energy units, they can be converted to decibels by this relation.

Since the decibel is based on a ratio, it can only be employed when related to a reference threshold level as given. Noise levels, which vary with frequency as well as intensity, must not only be related to this reference threshold level, but also to a reference frequency, which is taken as 1000 cycles. These terms and procedures may be found in Standards[1] published by the *American Standards Association.*

APPARATUS FOR MEASURING NOISE

Since the relative loudness to the ear, rather than the actual physical intensity, is the quantity in which engineers are usually interested, it has been found necessary to allow for the varying response of the ear at different frequencies in designing noise measuring equipment. It is most satisfactory to measure noise by means of a sound level meter, which usually consists of a microphone, a high gain audio-amplifier, and a rectifying milliammeter which will read directly in decibels. This meter is calibrated to give readings above the standard reference level and usually contains a weighting network to make it less sensitive at those frequencies where the ear is less sensitive. Three types of weighting networks may be provided. The "A" network is intended to provide relative frequency sensitivity corresponding to the characteristics of the ear at a loudness level of 40 decibels. The "B" network is weighted to correspond to the ear characteristic at a loudness level of 70 decibels. The meter may also be provided with a "flat" network which provides no weighting by frequency. For complete details on standards for sound level meters, refer to the information[2] published by the *American Standards Association.*

GENERAL PROBLEM OF SOUND CONTROL

As previously stated, the problem confronting the air conditioning engineer is that of designing a system which will operate without increasing the noise level in the conditioned space. To be sure that this is accomplished, it is necessary:

1. To determine the noise level existing without the equipment.
2. To ascertain the noise level which would exist if the equipment were installed without sound control.
3. To provide as a part of the installation sufficient sound control appliances to reduce the noise level substantially to that found in Item 1.

To accomplish this the engineer should have information of three kinds:

1. A knowledge of the noise levels currently considered acceptable in various rooms in order that he may have a basis on which to proceed.
2. A knowledge of the nature and intensity of the noise created by the various parts of the equipment.
3. A knowledge of how, when necessary, to vary and control the noise level between the equipment and the conditioned space.

In addition, the engineer should have sufficient information to predict the levels produced by noises which may be transmitted by the duct system from one conditioned space to another or from an outside space to the conditioned space. In either case, the designer must know the probable noise level at the point where the noise originates. From this he can compute the attenuation or transmission loss required in order to bring this level down to that required in the conditioned space. If there is likelihood of direct transmission through a duct, the attenuation required may be computed as shown on page 771. If the transmission is through dividing walls, it will be necessary to refer to published information on the transmission losses of standard building constructions[3].

Information concerning the noise levels created by ventilating and air conditioning equipment such as fans, motors, air washers, and similar items is not yet on a basis which permits tabular presentation, although certain manufacturers are prepared to offer such data and do state the noise producing properties of their products. A sound test code for fans

has been developed by the *National Association of Fan Manufacturers* which uses the flat response network of the sound level meter. However, when determining the noise generated by an air distribution system, it is customary to use the noise level of the fan as determined by the weighting network most nearly approaching the noise level of the space. In most cases this will be the noise level of the fan as determined on the 40 decibel weighting network. Refer to Table 1 for typical noise levels.

KINDS OF NOISE

To solve a sound problem of this type it is desirable to consider separately the several means by which noise reaches the room. This avoids to some extent the necessity of knowing the noise level at the source, and instead, places the emphasis on ascertaining the level at the point where the sound enters the room.

The noise introduced into a room or building by ventilating or air conditioning equipment may be divided into two general kinds depending on how it reaches the room with various sub-divisions:

1. Noise transmitted through the ducts.
   - *a*. From equipment such as sprays, fans, etc.
   - *b*. From outside, and transmitted through duct walls into air stream.
   - *c*. From air currents, including eddying noises.
   - *d*. Cross talk and cross noises between rooms connected by the same duct system.
   - *e*. Noise produced by the grilles.
2. Noise transmitted through the building construction.
   - *a*. From machine mountings as vibration.
   - *b*. From equipment through room wall surfaces.

The next step in the solution of this problem is to present data and discuss methods whereby solutions to the noise problem can be obtained when the allowable room noise level and the path through which the noise reaches the room are known.

NOISE TRANSMITTED THROUGH DUCTS

Operation of an air distribution system results in the generation of noise which may be transmitted through the ducts to the ventilated or conditioned room. The transmission of this noise may be controlled by the proper application of sound absorptive material within the ducts. The application of the absorptive material is a problem in balancing the room noise level requirements against the intensity of the noise generated. The four steps in the problem are:

1. Determination of acceptable room noise level resulting from the operation of the equipment.
2. Determination of noise level generated by the equipment.

The difference between items 1 and 2 in decibels is the over-all noise reduction required between the equipment and the room. In the discussion which follows reduction of noise will be referred to as *attenuation* of noise.

3. Determination of the natural attenuation of the duct system.
4. Selection of the proper sound treatment for the duct system.

The difference in decibels between the over-all attenuation required and the natural attenuation (3) is the additional sound attenuation to be provided by absorptive materials installed in the duct system or by special constructions designed to absorb sound. Experience has shown, for example, that where ventilating requirements permit, introduction of an expansion chamber or a change in area in the duct will frequently provide more reduction in low frequency noise.

DESIGN ROOM NOISE LEVEL

Measurements of noise levels have been observed by several investigators in various rooms and locations and are listed in Table 1. The values given were determined with the air conditioning or ventilation equipment not in operation, and with all windows and doors closed simulating the conditions of an actual installation.

This is an important consideration, for in offices or stores adjacent to busy thoroughfares the difference between the typical noise level in the

TABLE 1. TYPICAL NOISE LEVELS[a]

ROOMS	NOISE LEVEL IN DECIBELS TO BE ANTICIPATED		
	Min.	Representative	Max.
Sound Film Studios	10	14	20
Radio Broadcasting Studios	10	14	20
Planetarium	15	20	25
Residence, Apartments, etc.	33	40	48
Theaters, Legitimate	25	30	35
Theaters, Motion Picture	30	35	40
Auditoriums, Concert Halls, etc.	25	30	40
Churches	25	30	35
Executive Offices, Acoustically Treated Private Offices	30	38	45
Private Offices, Acoustically Untreated	35	43	50
General Offices	50	60	70
Hospitals	25	40	55
Class Rooms	30	35	45
Libraries, Museums, Art Galleries	30	40	45
Public Buildings, Post Offices, etc.	45	55	60
Court Rooms	30	35	45
Small Stores	40	50	60
Upper Floors Department Stores	40	50	55
Stores, General, Including Main Floor Dept. Stores	50	60	70
Hotel Dining Rooms	40	50	60
Restaurants and Cafeterias	50	60	70
Banking Rooms	50	55	60
Factories	65	77	90
Office Machine Rooms	60	70	80
VEHICLES			
Railroad Coach	60[b]	70	80
Pullman Car	55[b]	65	75
Automobile	50	65	80
Vehicular Tunnel	75	85	95
Airplane	75	80	90

[a]These values are tentative. More detailed measurements by D. F. Seacord, Bell Telephone Laboratories (*Journal Acoustical Society of America*, Vol. 12, pp. 183-187, 1940) give average values and standard deviations of room noise in residences, offices, stores, factories, etc., in large American cities.

[b]For train standing in station a level of about 45 db is the maximum which can ordinarily be tolerated.

space with the windows and doors open and closed may be as high as 10 db. Minimum, representative, and maximum levels are given for each type of space. The values are intended to give the variation with respect to location and not to time, and may be roughly classified by the following:

Minimum loudness refers to: Spaces of expensive construction, typified by double windows, carpeted floors, heavy upholstered furniture, or acoustically treated walls and ceilings.

Representative loudness refers to: Spaces of average construction and furnishings which are exposed to external noises typical of the locality in which the space is usually found.

Maximum loudness refers to: (1) Any space of inexpensive construction, and bare furnishings where noise is not an important factor. (2) Spaces in close proximity to very intense street traffic or to intense factory noise.

In general, if the noise level in the space resulting only from the operation of the air conditioning equipment is equivalent to or less than the typical level given in Table 1, the installation will prove satisfactory. If the typical level and the equipment level are equal and heard together the resultant level will be 3 db higher than either of them alone.

In some cases it is desirable to keep the equipment noise level in the ventilated or conditioned room at such a value that it actually will not increase the noise level in the room to any measureable degree. This can be accomplished if the equipment noise at the room can be kept 10 db below the noise levels shown in Table 1.

NOISE GENERATED BY FANS

Noise generated by fan wheels may be divided into two classifications, rotational noise and vortex noise. In ventilation and air conditioning work, where the maximum ratio between the fan tip speed and the velocity of sound is not greater than 0.12, vortex noise is by far the most important. The rotational noise may be described as that due to the thrust and torque applied to the air. Vortex noise is that due to the shedding of vortices from the blade and is dependent on the angle of attack, velocity, air turbulence, and blade shape. Vortex noise is due to pressure variations on the blade as a result of variations of air circulation. Given the noise level at the outlet or inlet of one type of fan construction under specific conditions of size, tip speed, and total pressure, noise levels at other values of tip speed, total pressure, and size may be approximated by the relationships:

1. For constant size and point of rating, the noise level of a fan will increase with increasing speed.

$$db \text{ (change)} = 55 \log_{10} \left(\frac{RPM_2}{RPM_1} \right) \quad (1)$$

2. For constant pressure and tip speed, the noise level of a given type of fan will increase with increasing fan size.

$$db \text{ (change)} = 20 \log_{10} \left(\frac{\text{Size}_2}{\text{Size}_1} \right) \quad (2)$$

Fan size refers to wheel diameter, housing height or some dimension that is directly proportional to lineal units. Fan sizes based on arbitrary systems or systems of preferred numbers have no significance.

The noise of a given fan is not constant at constant speed if the air delivery changes due to change of resistance. In general, a backward curved blade fan is lowest in noise at or near the point of maximum efficiency; a forward curved blade fan at or between the point of maximum efficiency and shut-off; an axial flow fan at or between the point of maximum efficiency and free delivery. The noise level of a double width fan

TABLE 2. ATTENUATION IN STRAIGHT SHEET METAL DUCT RUNS

DUCT	SIZE, IN.	ATTENUATION PER FT, db
Small	6 x 6	0.10
Medium	24 x 24	0.05
Large	72 x 72	0.01

TABLE 3. ATTENUATION OF ELBOWS[a]

ELBOW	SIZE, IN.[b]	ATTENUATION PER ELBOW, db
Very small	2 wide	3
Small	3 to 15	2
Medium	15 to 36	1.5
Large	36 plus	1

[a]The attenuation in vaned elbows should be considered the same as in elbows having the same dimensions as the radius of curvature of the vanes. If the vanes are lined for the purpose of damping any vibrations in them, one third may be added to the attenuation values listed.

[b]These attenuation values are based on elbows having a center line radius 1.5 to 2 times the diameter or width of the duct. The attenuation will be greater if the ratio is less than 1.5 and less when the ratio is greater than 2.

may be taken as 3 db higher than a similar single width fan operating under the same conditions of speed and pressure.

NATURAL ATTENUATION OF DUCT SYSTEM

Straight Sheet Metal Ducts. The attenuation of sound in straight sheet metal ducts is a function of the length, shape, and size of the duct[4]. Attenuation values are given in Table 2. In general this attenuation is so negligible except for long runs that it may be disregarded for all practical purposes.

Elbows and Transformations. Due to reflective interference, attenuation will take place at elbows and transformations. The magnitude of the attenuation will depend on the size and abruptness of the elbow or transformation as shown in Table 3.

When the area of a duct increases abruptly, an attenuation of noise level takes place in the duct. In duct design practice the total area of the branch ducts is greater than the supply duct. Similarly with outlets, the area of the outlet plus the area of the duct after the outlet is greater than the duct area before the outlet. Therefore in an outlet run, attenuation occurs in the duct as it passes each outlet. Table 4 gives the *db* reduction for various ratios of total branch duct and outlet area to supply duct area.

Grilles to Room. The large abrupt change in area between the grilles and the surfaces within a room results in an appreciable noise attenuation. This attenuation is a function of the total grille area (supply and return) and the total sound absorption of the room in *sabines*. (The sound absorption of a room in *sabines* is the summation of the products of each surface of the room measured in square feet multiplied by its corresponding absorption coefficient). The attenuation is given in Equation 3 as:

TABLE 4. ATTENUATION AT DUCT BRANCHES OR OUTLETS

RATIO: BRANCH DUCT + OUTLET AREA / SUPPLY DUCT AREA OR SUM OF BRANCH AREAS / SUPPLY DUCT AREA	ATTENUATION PER TRANSFORMATION, db
1.00	0.0
1.20	0.8
1.35	1.3
1.50	1.8
1.75	2.5
2.00	3.0

$$db\left(\begin{matrix}\text{Attenuation between}\\ \text{grilles and room}\end{matrix}\right) = 10\log_{10}\frac{\text{Total Room Absorption in Sabines}}{\text{Total Grille Area}} \quad (3)$$

Values in Table 5 approximate the attenuation for various rates of air change, and general types of room surfaces.

DUCT SOUND ABSORBERS

The difference between the required sound attenuation and the natural attenuation is that which must be supplied by the proper sound treatment of the ducts.

Selection of the Absorptive Material

When a sound wave impinges on the surface of a porous material, a vibrating motion is set up within the small pores of the material by the

TABLE 5. APPROXIMATE ATTENUATION BETWEEN GRILLES AND ROOM

OUTLET VELOCITY FPM	AIR CHANGE MIN.	LIVE ROOM[b] $a^a = 0.05$ db	MEDIUM ROOM[c] $a = 0.15$ db	DEAD ROOM[d] $a = 0.25$ db
500	5	11	16	18
	10	14	19	21
	15	16	21	23
	20	17	22	24
750	5	13	18	20
	10	16	21	23
	15	18	23	25
	20	19	24	26
1000	5	14	19	21
	10	17	22	24
	15	19	24	26
	20	20	25	28
1250	5	15	20	22
	10	18	23	25
	15	20	25	27
	20	21	26	28

[a]Average absorption coefficient for the room.

[b]Live room-average absorption coefficient 0.05. Bare wood or concrete floor—hard plaster walls and ceiling—minimum of furniture.

[c]Medium room-average absorption coefficient 0.15. Carpeted floor, upholstered furniture, hard plaster walls and ceiling or bare room with acoustically treated ceiling.

[d]Dead room-average absorption coefficient 0.25. Heavy carpeted floor. Walls and ceiling acoustically treated. Upholstered furniture.

alternating sound waves. As the ratio of the cross-sectional area of the pores to their interior surface is small, the resistance to the movement of air in the pores is large. This viscous resistance within the pores of the material converts a portion of the sound energy into heat. The decimal fraction representing the absorbed portion of the incident sound wave is called the absorption coefficient. Considerable absorption may also result, particularly in the low frequency range, from the flexural vibrations of the duct. In the selection and application of the absorptive material, several points should be considered.

1. For the absorption of the low frequencies below 500 cycles per second the material should be at least 1 to 2 in. thick. Thin materials, particularly when mounted on hard solid surfaces, will absorb the high frequencies and reflect the low.

2. In order to provide as much low frequency noise absorption as possible by means

of flexural vibration, it is desirable to fasten the absorptive panels discontinuously. This result may be attained to some extent by spot cementing, but better results are obtained when it is possible to fasten the absorptive panels to furring strips, leaving an air space behind. However, the exact resonance characteristics of the panels, and thus their absorption, are so unpredictable that flexural vibration cannot be relied upon for a specific value of attenuation.

Requirements for a good sound absorption material are: (1) high absorption at low frequencies[5], (2) adequate strength to avoid breakage, (3) fire resistance and compliance with national and local code requirements, (4) low moisture absorption, (5) freedom from attack by bacteria and algae, (6) low surface coefficient of friction, (7) particles should not fray off at the higher design velocities, and (8) freedom from odor when either dry or wet.

With every application the use of sound absorptive material should be considered in the dual function of insulation and sound absorption. It has been shown theoretically[6] that the reduction, in decibels per linear foot, of sound transmitted through a duct lined with sound absorbing material is related in a rather complicated manner to the size and shape of the duct, to the frequency of the sound, and to the sound absorbing char-

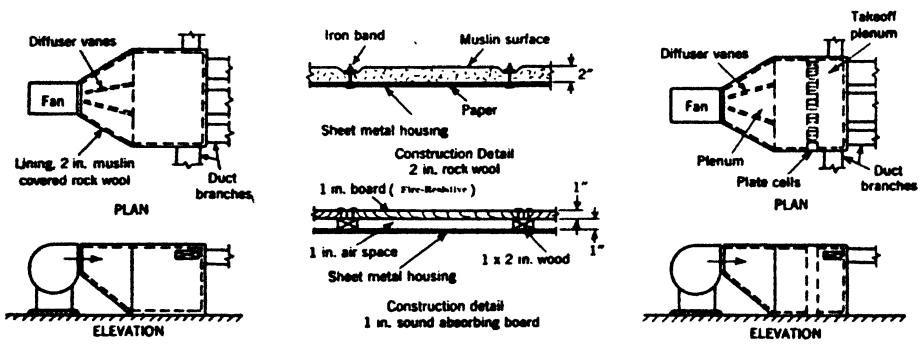

FIG. 1. ABSORPTION PLENUMS WITH AND WITHOUT SOUND CELLS

acteristics of the lining. Experimental evidence likewise indicates that there is no simple formula involving the variables which will apply accurately to all cases. However, it may be stated generally that the attenuation in decibels at a given frequency is directly proportional to the length of lined duct. It decreases as the cross-sectional area increases, and increases as the aspect ratio is increased.

The noise reduction varies to a considerable extent with the frequency of the sound. In calculating noise reduction, consideration should be given both to the comparative efficiency of the duct lining material at different frequencies, and to the frequency distribution of the noise to be quieted. In the case of fan noise, it is recommended that calculations be based on the frequency 256 cycles, since most of the noise energy is in the region of this frequency. In quieting noise due to air turbulence and eddy currents, in which the high frequencies predominate, the frequency 1024 cycles should be used.

Since ventilating system noise contains many frequencies, an exception should be noted to the statement above that attenuation in decibels is directly proportional to length of duct. Most sound absorbent materials are more efficient at high frequencies than at low frequencies. In consequence, the attenuation in the first five or ten feet of lined duct will be greater because the high frequencies are being absorbed. Thereafter,

since low frequencies will be predominant, the over-all noise attenuation per foot will gradually be less.

Acoustic Impedance of Absorptive Materials

In the past five years considerable literature has collected describing methods of determining the acoustic impedance of sound absorbent materials and methods of utilizing this quantity for predicting the acoustics of rooms [7] and the attenuation of sound in ventilating ducts[8]. Acoustic impedance as a concept is derived from electrical circuit theory. The effect of the sound absorbent material upon incident sound waves is described in terms of a resistive and a reactive component which may be determined by specifically devised apparatus[9].

Generally speaking, however, the use of acoustic impedance theory involves rather elaborate mathematical calculations, and the improved accuracy obtained is largely off-set by variations in the materials themselves and in their methods of mounting. It has been difficult to measure the acoustic impedance of large areas of material mounted in a manner typical of standard construction. P. E. Sabine [7] concludes that the assumptions required by acoustic impedance theory make this method of calculation of no immediate practical advantage in the measurement of sound absorption coefficients.

Beranek [8] compares results of sound attenuation observed for rectangular ducts lined with absorbent material computed by acoustic impedance theory with data reported by H. J. Sabine[10], using the methods of this chapter. Beranek concludes that the conventional P/A relation is valid for rectangular ducts not too far from square. His analysis indicates that other cases require more exact theory. However, it seems questionable whether the improvement in accuracy offered by the impedance method overbalances the additional computation time required and out-weighs other sources of error such as variations between samples of material.

Plenum Absorption

In systems, where individual ducts are directed to a number of rooms and sound treatment is required in every duct, a sound absorption plenum on the fan discharge as shown in Fig. 1 will often prove the most economical arrangement. The absorption in the plenum may be approximated by Equation 4.

$$db \text{ (Attenuation)} = 10 \log_{10} \frac{\text{Plenum Absorption in Sabines}}{\text{Area Fan Discharge}} \qquad (4)$$

The area of the plenum should be at least ten times as great as the fan discharge area. The plenum should be lined with 2 in. of muslin covered rock wool blanket or 1 in. sound absorbing board preferably nailed to wood strips on the inside of the plenum. With such a lining the plenum

TABLE 6. END REFLECTION OF PLATE ABSORBERS

PERCENTAGE FREE AREA OF ABSORBER	ATTENUATION, db
50	1
40	2
30	4
25	5
20	6

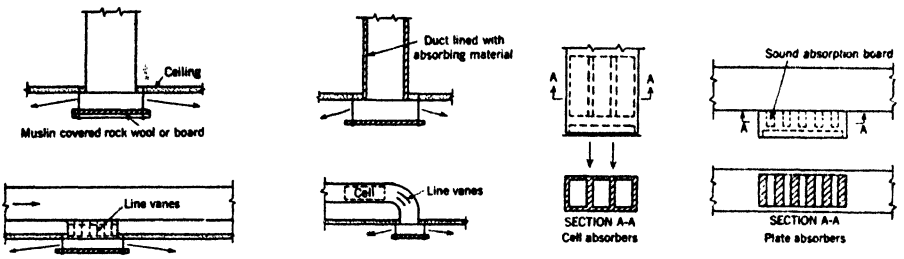

FIG. 2. OUTLET CELLS FOR PAN OUTLETS OR GRILLES

is particularly effective in reducing low frequency fan noise. The absorption of the plenum in sabines is the sum of the products of each interior area of the plenum measured in square feet multiplied by its corresponding absorption coefficient.

Plate Cells

One of the most economical methods of applying sound absorbent material from the standpoint of both labor and material is the plate cell. The plate cell consists of ½ or 1 in. sound absorbent board, spaced on 2, 3 or 4 in. centers. The attenuation due to the plate cell may be divided into two parts. There is reflection at each end due to the change in area and the absorption at the ends. Values for this attenuation are given in Table 6 which depend on the spacing. There is also attenuation due to absorption of sound within the passages of the cell, which depends on the length and the spacing. The attenuation within the cell for 1 in. board neglecting the end effect is given approximately by Equation 5.

$$R = \frac{10La^{1.4}}{S} \qquad (5)$$

where

R = attenuation, decibels.
L = linear length of duct, feet.
S = spacing in inches between plates up to 3 in.
a = absorption coefficient for the full thickness of the cell material. For typical value of a see Table 7.

An important objection to the plate cell is the increase in duct cross-sectional area required. Often on the fan discharge, particularly with unitary equipment, where a number of branch ducts take off, the plate cell may be installed with little or no difficulty.

Outlet Sound Absorbers

Outlet sound absorbers are rectangular or plate cells installed directly behind an outlet or they may be the lining of a pan or plaque outlet. They are particularly effective in the elimination of high frequency

TABLE 7. ATTENUATION FORMULAE FOR 1 IN. THICK TYPICAL DUCT LINING BOARD

FREQUENCY	ABSORPTION COEFFICIENT	ATTENUATION REDUCTION, db
256	0.37	3.0 L P/A
512	0.69	7.5 L P/A
1024	0.78	9.5 L P/A
2048	0.78	9.5 L P/A

whistles which are generated by air flow in the ducts. They are also employed in large systems with long runs where only a few outlets near the fan require treatment. Frequently outlet cells are the only means of correcting existing noisy installations, as the duct sections directly behind the outlets may be the only sections accessible for treatment. (See Fig. 2.)

Duct Lining or Rectangular Cells

One series of experiments[10] made on a commonly used type of duct lining material (1 in. rock wool sheet) has shown that, subject to certain restrictions, the attenuation of single-frequency sounds may be expressed by the approximate Equation 6. This equation is accurate within plus or minus 10 per cent for duct sizes ranging from 9 x 9 in. to 18 x 18 in., for

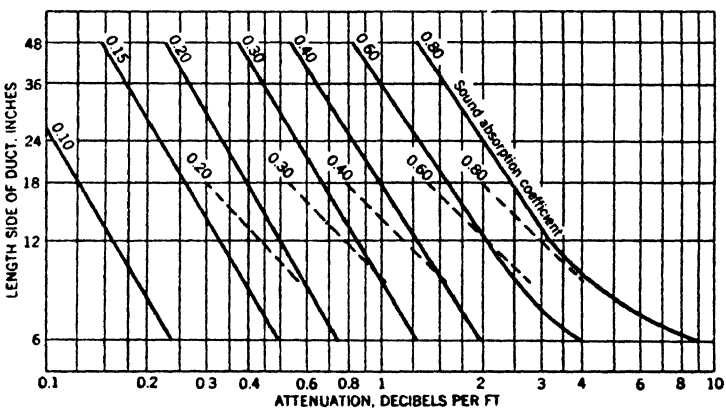

FIG. 3. SOUND ATTENUATION FOR VARIOUS ABSORBING DUCT LINERS

cross-sectional dimension ratios of 1:1 to 2:1, for frequencies between 256 and 2048 cycles, and for absorption coefficients between 0.20 and 0.80.

$$R = 12.6\, L \frac{P}{A}\, a^{1.4} \qquad (6)$$

where

R = attenuation, decibels.
L = length of lined duct, feet.
P = perimeter of duct, inches.
A = cross-sectional area of duct, square inches.
a = absorption coefficient of lining.

In Table 7, the absorption coefficients at different frequencies of a material of the previously mentioned type are listed, together with the corresponding values for Equation 6.

Results of other experiments indicate, however, that Equation 6 may be in error when applied to other types of duct lining material and to duct sizes and shapes outside of the range specified. An empirically derived chart[11] representing the *average* experimental data on a number of different types of materials including the rock wool sheet mentioned as applicable to Equation 6 is shown in Fig. 3. Since individual materials vary, the curves in Fig. 3 are given only as representing the best available averages for duct sizes of square cross-sections from 6 x 6 in. to 48 x 48 in. As an illustration, the dotted lines in the chart show values calculated from Equation 6 which indicate that the slope for this particular material is somewhat different than from the average curves. The curves in Fig. 3,

as well as Equation 6, show that the attenuation in decibels is directly proportional to the length of duct lined, and that the larger the duct the greater will be the length which must be lined in order to obtain a given noise reduction.

If the length of duct from the main duct to a grille is shorter than the length of lining indicated by the calculations, this duct may be subdivided into smaller ducts, as shown in Fig. 4. The increase in noise reduction thus obtained may be calculated from Equation 7, provided the splitters are installed parallel to the long side of the duct:

$$R_s = R_o \frac{a + bn}{a + b} \tag{7}$$

where

R_s = reduction with splitters, decibels.
R_o = reduction in same length of duct, without splitters, decibels.
a = dimension of short side of duct, inches or feet.
b = dimension of long side of duct, inches or feet.
n = number of channels formed by splitters.

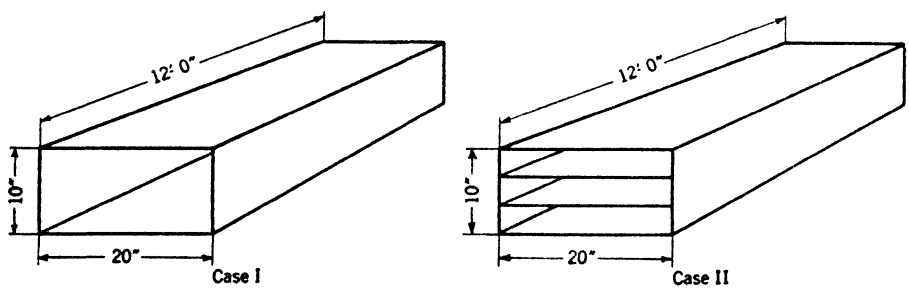

FIG. 4. DIAGRAM OF BRANCH DUCT TREATMENT WHERE LENGTH IS INSUFFICIENT FOR ADEQUATE ABSORPTION

Example 1. An air conditioning installation is to be installed in a small theater. Determine the necessary sound treatment for the air distribution system to provide a satisfactory noise level in the theater utilizing these conditions:

Fan tip speed 4000 fpm, total pressure 1.25 in.	77 db
Acceptable room noise level (Table 1)	40 db
Required attenuation	37 db

Solution: Natural attenuation of supply duct.

Sheet metal duct 50 ft long 48 in. x 36 in. (Table 2) 50 x 0.01	0.5 db
Elbows, two size 48 in. x 36 in. (Table 3) 2 x 1	2.0 db
Attenuation grilles to theater air change 10 min (Table 5) outlet velocity 1000 fpm	22.0 db
Total natural attenuation	24.5 db

Difference between required and natural attenuation, 37 minus 24.5, is 12.5 db. This attenuation must be supplied by sound treatment in the duct, either in the form of duct lining or plate cells.

A similar analysis of the return duct system shows that 15 db attenuation is to be furnished by absorptive material. An inspection of the installation shows that the lining of the plenum on the suction side of the fan would prove the most economical, where it would secure the dual function of heat insulation and sound absorption.

Example 2. A 10 x 20 in. duct is connected to a private office space in a quiet location. Determine the length of lining necessary to attenuate average fan noise satisfactorily, using a lining material of a type to which Equation 6 applies, and having an absorption coefficient of 0.40 at 256 cycles. Assume that the duct is only 12 ft long as shown in Fig. 4, and that a 30 db reduction is required in this length.

Solution:

Case 1. (No splitters), From Equation 6,

$$R_o = 12.6 \times 12 \times \frac{60}{200} \times 0.40^{1.4} = 12.6 \text{ db}$$

Case 2. (Two splitters, three channels), From Equation 7,

$$R_s = 12.6 \times \frac{10 + (20 \times 3)}{10 + 20} = 29.6 \text{ db}$$

AIR SUPPLY OPENING NOISES

When air is introduced into a room through a grille or register at a constant velocity, sound energy is being introduced into the enclosure at a constant rate [12]. Due to partial reflection at the boundaries of the enclosure, the intensity of sound at any point in the space builds up to some maximum value. In a large room at a point remote from the source of sound (the supply opening) the intensity can be shown to be substantially

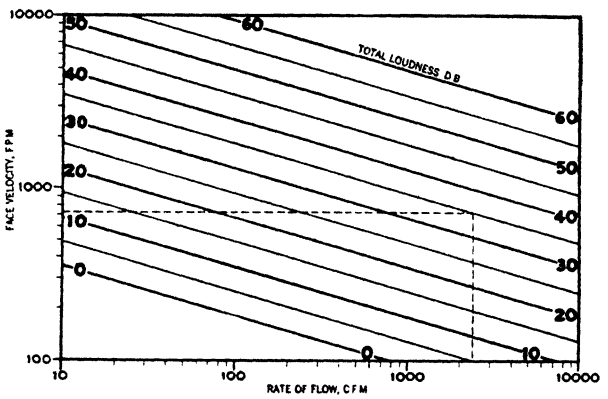

FIG. 5. AIR FLOW AND LOUDNESS CHART

proportional to the rate at which sound energy is generated and inversely proportional to the number of sound absorption units (sabines) in the room. It would thus appear that doubling the sound absorption of the room would halve the intensity and result in a noise level decrease of 3 db.

Grille noise is similar in character to fan vortex noise. Knowing the noise level at the face of a grille for a given grille blade setting, the noise will vary as given in Equation 8 where V is the velocity of the air through the grille.

$$db \text{ (change)} = 55 \log_{10} \left(\frac{V_2}{V} \right) \tag{8}$$

For a change in blade setting Equation 9 applies and in this case the total pressure is measured directly behind the face of the grille. For a typical air conditioning grille the noise level at the grille face may be approximately 48 db with a total pressure behind the grille of 0.1 in.

$$db \text{ (change)} = 27.5 \log_{10} \left[\frac{(\text{Total Pressure})_2}{(\text{Total Pressure})_1} \right] \tag{9}$$

The resultant room noise level can be approximated by Equation 10.

$$\text{Room Level} = \left[\begin{matrix} \text{Noise Level at Face} \\ \text{of Grille} \end{matrix} \right] - 10 \log_{10} \frac{\text{Total Room Absorption in Sabines}}{\text{Total Grille Area}} \tag{10}$$

Grille Selection

In practice the allowable total sound and the required air flow are usually known, and it is desired to determine the maximum allowable velocity. In comparing sound ratings of various grilles several factors must be known if the information is to be properly applied:

1. The threshold intensity on which the decibel ratings are based.
2. The distance from the grille at which data were taken.
3. If stated as loudness level versus velocity for a given grille, the *core area* (not nominal area) must be known.
4. The sound absorbing characteristics of the test room.
5. Whether or not corrected for test room loudness level: if not, the room level (without grille noise) must be known.
6. Methods used for recording data. (Characteristics of sound meter).

Since total loudness and air flow are both functions of velocity and area, the solution of the problem implies a trial and error method. It has been found possible to present these data with sufficient practical accuracy as a family of uniform curves, as illustrated in Fig. 5, which are based on these assumptions:

1. Threshold intensity = 10^{-16} watts per square centimeter [1].
2. Microphone location 5 ft from lower edge of supply opening on a line downward at 45 deg and in a plane bisecting the supply opening perpendicularly.
3. Where data are given as loudness level versus velocity, the rating is per square foot of core area.
4. The room is assumed to have 100 sabines absorption.
5. Plotted data are loudness levels of *supply openings only*, correction having been made for test room level.
6. Data taken with a direct reading sound-level meter with frequency weighing network intended to approximate the response of the human ear.

If the published ratings are in terms of decibels per square foot, correction must be made for area to secure the total sound level of supply openings of more or less than one square foot area from Equation 11.

$$\text{Decibel Addition} = 10 \log_{10} A \tag{11}$$

where

A = core area, square feet.

With Fig. 5 it is possible to find directly the velocity in feet per minute which will give a predetermined total loudness at a predetermined rate of flow expressed in cubic feet per minute. The values used are arbitrarily chosen for the purpose of discussion and do not necessarily represent data referring to any particular design of air supply opening. A correction chart is shown in Fig. 6 for a room having a sound absorption other than 100 sabines.

Example 3. Determine the core area (see Chapter 40) of an air supply grille which will maintain a noise level of not more than 40 db in a room having 100 sabines of sound absorption, if an air volume of 2400 cfm is required to maintain the proper air conditioning.

Solution. Assuming a grille noise rating of at least 5 db below the noise level of the room, Fig. 5 shows that the limiting grille velocity for a total loudness of 35 db is about 725 fpm and the core area becomes fixed at 2400 ÷ 725 or 3.31 sq ft.

If the room absorption had been greater, the previously selected velocity of 725 fpm would be safe, since the loudness reduces. If the room absorption had been 200 sabines a correction of plus 1.3 should be made by reference to Fig. 6, and the permissible velocity becomes that corresponding to a total loudness of 36.3 or approximately 800 fpm.

If the room had been highly reflective with an absorption of less than 100, the cor-

rection would be much more important. For instance, for a room of 35 sabines a correction of minus 3 db should be made and the maximum velocity corresponding to the 32 db total loudness would be approximately 600 fpm.

Where more than one supply opening must be considered, the problem is more complicated. If a similar supply opening is added in a far corner of a highly absorbent room, the change in noise level at the 5 ft station at the first supply opening is small; however, if the room is small, or highly reverberant or both, the intensity at the 5 ft station may be almost doubled and the noise level increased nearly 3 db thereby. The simplest method of handling this problem is to treat the room as though all the air were being supplied by one supply opening. Thus, if two outlets, each supplying 1000 cfm are used, the value 2000 cfm should be used with

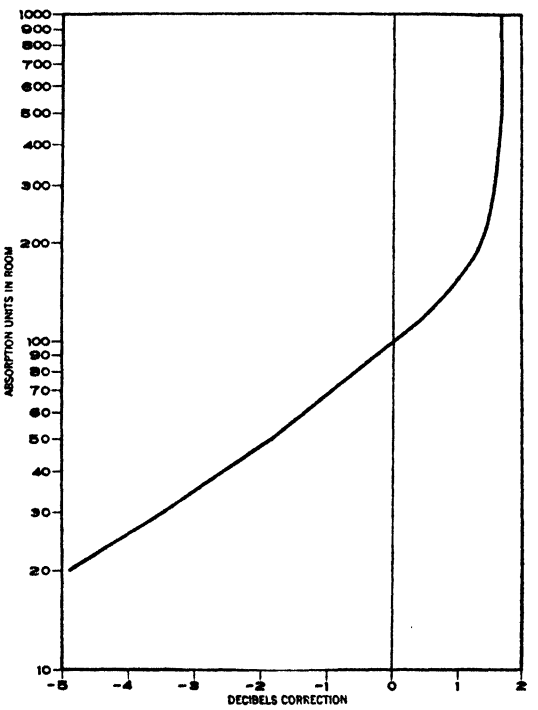

FIG. 6. ROOM ABSORPTION CORRECTION CHART

Fig. 5. Although this method may place an unwarranted limit on velocity when used in a large room, it is seldom that such a room has a noise level low enough to justify a more complicated though more exact procedure.

In general, return grilles are selected for velocities about half the supply velocity, and when this is done, they may be neglected in sound computations. However, if supply and return grilles are the same size, resulting in the same face velocity, they must be treated as two supply openings. That is, if 1000 cfm are supplied and exhausted through grilles of the same area, 2000 cfm must be used in the solution with Fig. 5.

CROSS TRANSMISSION BETWEEN ROOMS

Ducts serving more than one room permit cross talk between the rooms and should be lined with acoustical material. Where the rooms are close together and the ducts short, the ducts should be sub-divided to provide

ample acoustical treatment. Lagging material similar in character to acoustical board, when placed on the outside of ducts, serves to prevent noise originating outside the ducts being carried inside the ducts and into the air stream.

A case where outside lagging is desirable occurs when ducts originate at the fan in the equipment room and pass through this room on the way to the room being conditioned or ventilated. Unless the ducts are lined some of the mechanical noise from the equipment room air may be transmitted through the wall of the duct into the air stream and thereby carried into the room. In such cases, that portion of the duct which is exposed to the sounds in the equipment room should be lagged with material such as cork, pipe covering or other sound damping material to prevent the sound from entering the duct at this point. Numerical data are not available to permit a simple and practical calculating procedure to determine thickness of covering which should be used for this purpose.

Laboratory measurements have shown that the loss through a sheet of No. 22 gage metal is 24 db. When a sheet of rock wool insulation 1 in. thick and weighing 1.4 lb per square foot is added to this, the insulation value is increased to 29 db. In general, however, adding a layer of insulation or pipe covering does not materially increase the sound insulation value unless the material is dense, or unless it is surfaced with another sound impervious layer such as metal or board. Standard reference books should be consulted for sound insulating properties of various materials. Inside lining material used in the case previously mentioned would serve as an absorber of the sound transmitted through the duct walls, and thus act as a means of preventing the transfer of noise into the air stream. Inside lining may also be used in ducts to absorb noise which reaches the air stream from equipment such as fans, sprays and coils; noise due to eddying currents set up by elbows, dampers and similar obstructions; and noise transmitted from room to room where there is a common duct system.

CONTROLLING VIBRATION FROM MACHINE MOUNTINGS

It is impossible to select equipment which will operate without producing some mechanical noise and, since the equipment must be mounted in a building, it is probable that a part of this noise will be transmitted to the building to such a degree as to make noisy conditions in the rooms which are to be air conditioned.

Much of this noise may be transmitted by the duct if it is rigidly connected to the fan outlet. It is common practice to make the connection between the fan and the duct with a canvas sleeve which effectively restricts noise at this point. Noise may also enter the building through the mounting of the motor and the fan. Flexible mountings should be provided in all installations but these mountings must be carefully designed so that they will actually reduce the energy transmitted between the machinery and the supporting floor. If a flexible material is used, it is desirable to investigate the installation so that it is not short-circuited by through bolts which are improperly insulated and by electrical conduit which is not properly broken and is attached both to the equipment and to the building. The flexible mounting, if improperly engineered, may actually increase the energy transmitted between the equipment and the floor upon which it is supported.

In the proper isolation of vibration, which is usually in the lower range of frequencies and does not include the *airborne* vibrations known as

sound, there is one basic formula which is important in the solution of the problem. It is the formula of transmissibility as governed by the equation:

$$T = \frac{1}{1 - \left(\frac{f}{f_n}\right)^2} \tag{12}$$

where

T = transmissibility of the support.

f = frequency of the vibratory force.

f_n = natural frequency of the machine unit on its support (Damping = 0).

Equation 12 shows that the transmissibility approaches unity for disturbing frequencies considerably lower than the natural frequency of the mounting. As the disturbing frequency is increased the transmissibility is also increased until at the resonant frequency, where $f = f_n$ the transmissibility becomes infinite. This is not true in practice because all materials have some internal damping effect. However, operating at or very close to the resonant frequency is always serious as forces and stresses may be multiplied 10 to 100 times. As the disturbing frequency becomes greater than the natural frequency the transmissibility becomes a smaller quantity and at the value of $f/f_n = \sqrt{2}$ it again has the value of unity. Beyond this point true isolation is first accomplished. At a ratio of 3 to 1 for f to f_n the isolation is effective enough for practical application, and experience and economical design have shown that a ratio of 5 to 1 is good. For high speeds, higher ratios for f to f_n are easily attained and give better results for effective vibration control, but for the lower speeds as experienced with compressor work the higher ratios become uneconomical.

For a given installation the speed of the compressor is fixed by the specifications, therefore the value of f is fixed. That leaves only f_n to be determined and that is accomplished by the choice of mounting material and design for the support of the machine. It is well to keep in mind that when trying to isolate vibration, no attempt should be made to isolate the driving and driven piece of equipment separately. The two should be mounted on a rigid frame and then the entire assembly isolated according to the rules presented in this chapter.

The value of f_n can be controlled by the flexibility of the machine support, and when the deflection of the machine support is proportional to the load applied (such as with springs or nearly so with rubber in shear) the value of f_n can be determined by Equation 13.

$$f_n = \frac{1}{2\pi}\sqrt{\frac{g}{d}} \tag{13}$$

where

g = gravitational constant.

d = static deflection of supporting material.

f = frequency of the vibratory force.

f_n = natural frequency of the machine unit on its support (damping = 0).

By the use of Equation 13 a set of curves may be plotted as shown in Fig. 7. The first line AB, plotted as the critical frequencies for the various

static deflections, is a curve showing the worst possible conditions or resonant conditions.

Plotting another curve *CD*, which is $\sqrt{2}$ times curve *AB*, shows the area *MCDN* in which the resilient material or mounting does more harm than good. Plotting two more curves *EF*, 3 times curve *AB*, and *GH*, 5 times curve *AB*, shows area *EGHF* which represents efficient and economical isolation. Area *GPOH* is excellent isolation, but for all except the highest speeds becomes rather uneconomical because of the large deflections required.

Example 4. An electric motor driven compressor unit is to be isolated. The compressor is partially balanced and operates at a speed of 360 rpm. The speed of the motor is 1160 rpm and is belt connected to the compressor. Total weight of the compressor and motor is 4500 lb.

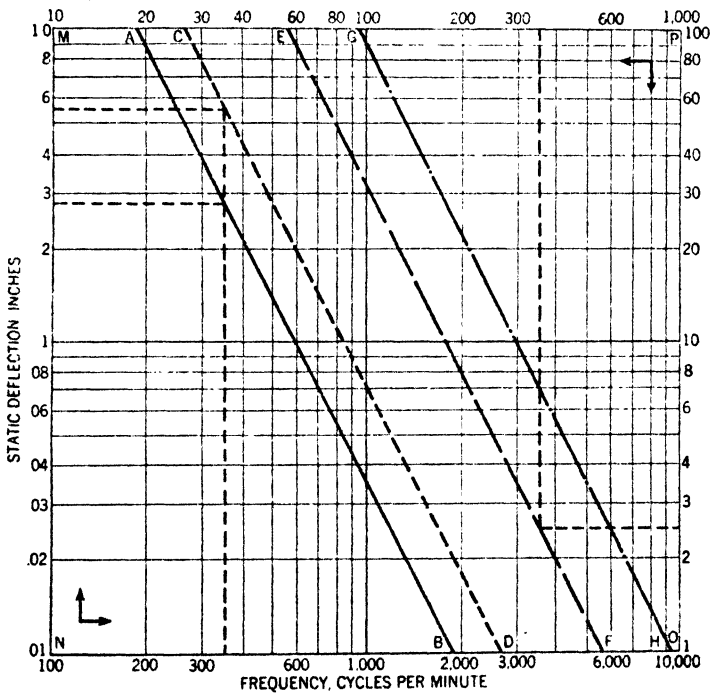

FIG. 7. STATIC DEFLECTION FOR VARIOUS FREQUENCIES

Solution: The minimum disturbing frequency to be isolated is 360 cycles per minute. Assume that the desired ratio of forced to natural frequency is 3 as a minimum and that 5 is desired. The desired natural frequency of the mounting is 360 ÷ 5 = 72 cycles per minute.

From Fig. 7 a deflection of 7 in. is required to attain a natural frequency of 72 cycles per minute. This value may be obtained from critical curve *AB* for 72 cycles or from curve *GH* (5 times critical) for 360 cycles. For the minimum ratio of 3 the deflection would be 2.5 in.

The next step is to determine the total weight to be supported by the springs. For low speed partially balanced compressors, it has been found necessary to add a foundation weighing 2 to 3 times the weight of the motor and compressor, in order to maintain the machine movement below 0.03 in.

Compressor and motor	4,500 lb
Concrete foundation	9,000 lb
Total	13,500 lb

Practical application dictates the number of springs to be used, which is based on the design of the machine foundation and the supporting floor structure. However, it is desirable to design for at least 8 springs and one or two spares for cases of unknown weights. As many as 50 springs have been used on one installation. The distribution of the springs must be balanced against the masses to be supported, otherwise the foundation design and supporting structure determine the location of the springs.

The choice of the material used in the design of the resilient mounting is also important. For the slow-speed type compressor a common speed found in practice is 360 rpm. For speeds below this, isolation should not be attempted except under careful supervision. Referring to Fig. 7, it is found that for 360 rpm the static deflection required for a ratio of f/f_n of 3 to 1 (line EF) is 2.5 in. and for a ratio of 5 to 1 (line GH) it is 7 in. For these values of deflection the only choice of material is the coil spring. This is also true for speeds up to about 700 rpm. In consideration of the transverse spring constant (so as to maintain good ratios among the various degrees of freedom) experience has shown that the spring should be designed with a *working height* equal to 1.0 to 1.5 times the outside diameter. A long spring of small outside diameter has very low transverse rigidity and therefore requires some additional means of preventing side drift of the unit and on very sensitive applications this may tend to destroy the isolation efficiency. For speeds of 700 to 1200 rpm the required deflections range from 0.22 in. to 1.75 in. For these conditions rubber in shear serves as a rather satisfactory material if protected from oil. For speeds higher than 1200 rpm cork specially made for vibration damping can be applied with good results. These limitations are by no means absolute, because certain liberties may be taken without impairing the result if all possible degrees of freedom have been taken into account in the design of the installation.

When a machine unit is properly isolated it will have a definite amount of movement which is determined by the ratio of the unbalanced forces to the total mass of the machine. If this resultant machine movement is too great for the necessary connections or the satisfaction of the customer it can be reduced only in two ways without destroying the quality of the isolation; first, adding mass or dead weight to the machine (such as concrete) common in the application of low speed, partially balanced machinery; second, accurately balancing (both statically and dynamically) all moving parts so as to eliminate the vibration at the source. This latter method is the best engineering practice and is the modern trend. However, even with well balanced machinery, installed in the vicinity of quiet offices it is usually necessary to properly isolate the equipment to prevent the transmission of vibration likely to cause complaints.

Where limitation of machine movement is desired during the starting and stopping periods, the application of friction or hydraulic damping will serve without seriously interfering with the efficiency of the isolation.

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Chapter 43

CENTRAL SYSTEMS FOR AIR CONDITIONING

Features of Systems, Zoning, Apparatus Dew-Point, Cooling Load, Heating Load, Air Quantity and Effective Temperature Difference, Low and High Pressure Induction Convectors, Evaporative Cooling, Precooling, Sensible Cooling with Unwetted Coils, Run-Around System; Selection of Type of System, Location of Apparatus

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THE term central applied to an air conditioning system implies that the equipment such as fans, coils, filters and their encasement are designed for assembly in the field rather than in a factory as a unit. As a central system usually serves several different rooms, individual controls are required for each room.

FEATURES OF CENTRAL SYSTEMS

One advantage of a central air supply system is that one apparatus serving many rooms may involve a lower investment cost than that for a number of self-contained plants, each serving a single room. A central system may occupy basement or attic space that is relatively unimportant, whereas individual factory-assembled apparatus placed in each room may occupy otherwise valuable space. Another advantage of a central system is accessibility for servicing, since it is possible to provide doors in the encasement for cleaning and inspecting all of the component parts in a manner usually superior to that practicable with compact factory-assembled equipment.

Central air conditioning systems usually are connected by ducts with the various rooms served, and preferably have exhaust fans that may effect complete removal and disposal of any desired proportion of the air. The exhaust fan may return air to the supply system for recirculation, as a measure of economy of fuel or refrigeration.

Central air conditioning systems are served by heating and refrigerating equipment which may be located at some distance from the air supply apparatus and which may serve one or more central air supply systems.

Year-Round Air Supply System

Fig. 1 is a plan of a year-round air supply system. Outside air may enter from the left at A, desirably from an intake on the side of the building least exposed to solar heat and not close to the ground or to a sun-heated or dust-gathering roof. A damper B for proportioning the volume of outside air, is interlocked with the return air damper C in such manner that as the outside air volume increases the return air volume decreases. The return air duct D, shown diagrammatically, comes from the exhaust fan. All the air, it will be observed, must pass through the filters E and there is ample room on both the inlet and outlet sides of the filters for servicing them. The filters may be of mechanically cleaned type, of replaceable cell type, or may be electronic, as described in more detail in Chapter 33.

The cleaned air passes to the equipment that changes its temperature and humidity. Except in very warm climates, a heating or tempering

coil F is required to warm the air to a temperature above freezing. Usually, the heat is supplied by means of hot water or steam. During many hours of most days it is practicable to recirculate enough of the air so that the air drawn from outside, after mixing with the relatively warm return air, will not be cold enough to freeze the water in the humidifier.

Upon leaving the tempering coil, the air enters the humidifier G. This may be a spray of warmed water, circulated by a small pump from a water tank under the spray chamber, or may be other means of supplying water vapor. The supply of moisture must be under automatic and very reliable control. Following the humidifier a heater I is required, for controlling the temperature of the air entering the supply fan.

The second group of heat transfer devices in a year-round system includes an air cooling component H, for use in warm weather. Its surface may be chilled by direct expansion of an approved refrigerant

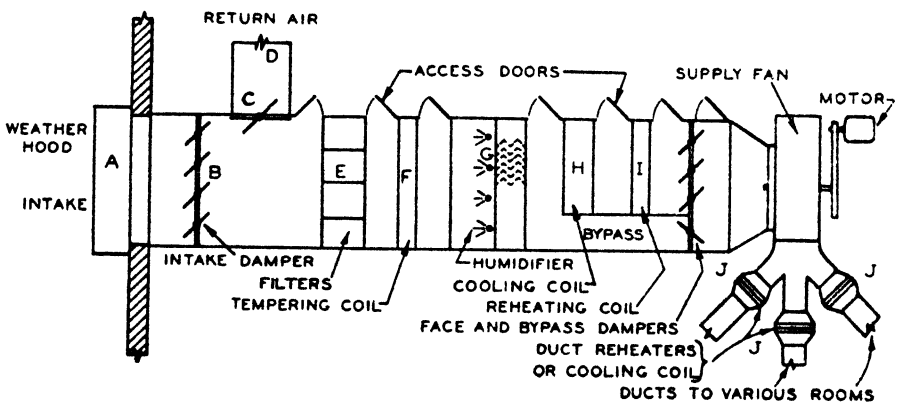

FIG. 1. ARRANGEMENT OF EQUIPMENT FOR YEAR-ROUND AIR SUPPLY SYSTEM

within its tubes, or the surface may be cooled by a pump-circulated liquid such as water or brine. This device must be sufficiently cold to cool the summer air to a temperature below the existing dew-point, and may be expected to be wetted constantly by the moisture condensed from the air. A water-tight drainage tank must be installed under the cooling coil and should extend for a distance toward the fan. Water should be drained by means of a trapped waste through a vented air-break. The second group of heat transfer devices also includes an air-heating component (reheater) similar to the tempering coil and capable of warming the chilled, saturated air leaving the cooling surface, to a temperature sufficiently high to prevent complaint of drafts, when the air is delivered into the rooms.

ZONING AND ZONE CONTROL

It is apparent that while an apparatus like that of Fig. 1 would be very desirable for any single room, since in that case the air could be delivered at optimum conditions, the cost of a complete individual system for each room and the space required for the equipment generally would be prohibitive. Economy is favored if the varying requirements of numerous

rooms or zones can be simultaneously satisfied by air from a single central supply system.

Various methods are practicable for controlling the temperature, humidity and air movement in various rooms or zones. A measure of control is attainable merely by proportioning the flow of air to each room, though usually such control by throttling dampers is difficult to maintain and should be avoided when possible.

Another scheme is to install a properly proportioned coil in the branch air supply duct serving each room to warm the air to suit the individual need. The air, for example, leaving the fan that serves several rooms, may be cooled before entering the fan, to the condition favorable for one room, and the air for each other room may be reheated by the branch duct coil to the required temperature. It is also possible to circulate a heat absorbing medium in the branch duct coils to reduce the temperature of the air passing to rooms that would be overheated if they received air at the condition leaving the central air supply system. In Fig. 1 such coils J are indicated in the three branch ducts leaving the supply fan.

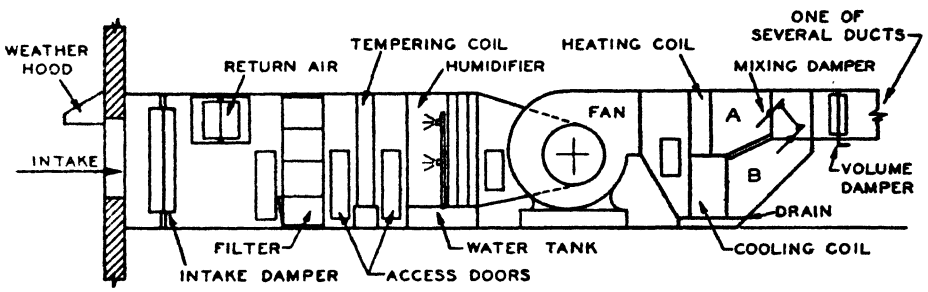

FIG. 2. ALTERNATE ARRANGEMENT OF EQUIPMENT FOR CONTROLLING AIR CONDITION IN CENTRAL AIR SUPPLY SYSTEM

When heat transfer devices are placed in branch ducts for improved temperature control, mechanically circulated water gives excellent results as a heat carrier. The water usually is warmer than the air but it is possible to use water colder than the air.

It is practicable also to use single central air conditioning equipment similar to that shown in Fig. 1, in conjunction with several fans; one for each room or zone. In such cases there may be a separate reheater on the suction side of each relatively small supply fan.

The designer must remember that the various supply fans will compete with each other for air, against the resistance interposed by the filters, coils, etc., that are used in common under such circumstances, and that, therefore, unless the fans are of backward-curved blade, non-overloading type, they may alternate in carrying more than their share of the air, and thereby cause the air distribution to be chaotic and unsatisfactory.

Another method of controlling temperature in various rooms served by a central air supply system is shown in the sectional elevation, Fig. 2. The supply fan is placed immediately after the humidifier. When cooling the air in hot weather, the humidifier is not operated. The fan will deliver the air through the heating coil and through the cooling coil to

the two air pressure chambers A and B at the right of these coils. From these chambers many separate ducts, one of which is shown, each with a double-blade mixing damper, may convey the air to the various rooms. The mixing dampers, one of which is shown, are interlocked so that as the upper one closes the lower one opens; selecting between them, air in the required quantity from either the warmer chamber A or the cooler one B. In cold weather no refrigerant is required in the cooling coil and in hot weather no heating medium is circulated in the heating coil. With this scheme, the control of relative humidity in warm weather is not always sufficiently precise to meet requirements, since the untreated air delivered through the upper coil may be so high in relative humidity that it cannot sufficiently compensate for the nearly saturated air leaving the lower coil. A reheater could be placed if desired, to the right of the lower coil to bring the air in the lower chamber to the desired relative humidity. The

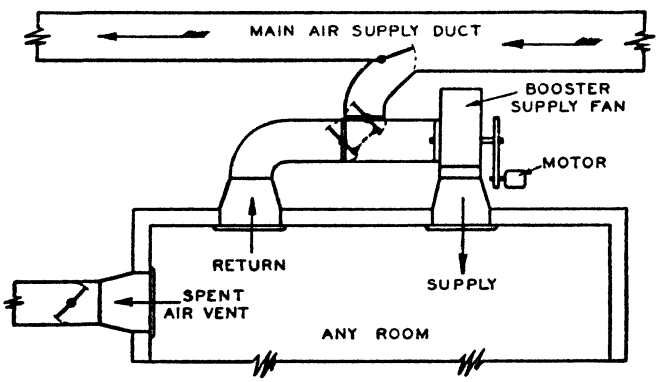

FIG. 3. ARRANGEMENT FOR INDIVIDUAL ROOM TEMPERATURE CONTROL WITH CENTRAL AIR SUPPLY SYSTEM

simple arrangement of Fig. 2 is admirable in winter and, except where close control of relative humidity is important, may be acceptable in summer.

Another method of attaining temperature control in individual rooms with a year-round central air supply system is to install a booster fan between the main air supply duct and the air delivery opening to each zone or room, as shown in Fig. 3. Air can then be delivered from the central supply fan through the main duct at some desired condition, for instance, 60 F, 45 per cent relative humidity. A double mixing damper near the intake opening of the booster fan, controlled by a thermostat in the room or zone that is served by the fan is interlocked with an outlet exhaust damper in the spent air opening, so that as more of the room air is recirculated, and as less new air from the main air supply duct is delivered into the room, the spent air outlet is throttled in proportion. In many large installations this principle is applied successfully for zoning different stories in multi-story office buildings, the main supply fan being on the roof, and each booster fan used for supplying the rooms of one orientation of each story. In other cases the booster fans serve only single offices and therefore are small enough to be concealed above ceilings alongside the main supply duct.

There may be installations in which the use of recirculated air for mixing with new refrigerated and nearly saturated air to control temperature and relative humidity is objectionable. In such cases the general recirculation arrangements of Fig. 1 may be omitted, and the heat transfer coils located in the ducts may be used. In some cases where general recirculation is not acceptable, as for all the rooms in an entire building, use of the local circulation of Fig. 3 may solve the problem.

APPARATUS DEW-POINT

In ordinary practice, with commercial apparatus, complete saturation of the air is seldom obtained. Four-row finned cooling coils contact approximately 80 per cent of the air, whereas six-row finned coils contact approximately 95 per cent of the air. In spray type dehumidifiers of good design the air leaves the dehumidifier at 1 to 2 deg higher wet-bulb temperature than the spray water leaving the dehumidifier, and the difference between the dry-bulb and wet-bulb temperatures leaving the dehumidifier may be as low as 1 deg. A spray type dehumidifier having sufficient length of spray chamber and density of spray, together with proper arrangement of nozzles, may approach saturation very closely.

As explained in Chapter 3, the slope of the line on the psychrometric chart connecting the room condition with the apparatus dew-point on the saturation line, determines the ratio of sensible heat absorbing capacity to the moisture absorbing capacity of the supply air. Therefore the room condition can be maintained as long as the supply air temperature lies on this line, but a greater volume of supply air must be used to satisfy the room load if the cooling coil does not contact 100 per cent of the air. For a given room load, the same apparatus dew-point will be required whether the cooling appliance contacts all the air or only part of the air.

From the point of view of satisfying the given cooling load requirements, the air passing through the apparatus without being cooled below the dew-point temperature produces two effects:

1. The air quantity which must be passed through the dehumidifier must be increased. Thus, if 20 per cent of the air passing is contacted, then 25 per cent ($0.20 \div 0.80 \times 100$) more air must be used than would be necessary if all of it were contacted.

2. Passing untreated air may change the room cooling load, which in turn may change the sensible heat factor. If return air only is passed through the dehumidifier or if room air only is by-passed, the room load would not change, but if some outside air is passed through, the room sensible heat gain and room latent heat gain will be changed due to the addition of untreated outside air, which changes the sensible heat factor. When a load calculation is made, it is necessary to know the percentage of air affected in the dehumidifier and calculation must be made accordingly.

If the ventilation air is drawn through the dehumidifier before it goes into the room, only that portion of the air not saturated must be included in the room load for the purpose of determining the apparatus dew-point and supply air quantity. It should be noted when evaluating the load added by untreated outside air that the temperature difference between room air and outside air and the moisture content difference between room air and outside air should be used, rather than the difference between outside air and apparatus dew-point, since the rise from the apparatus dew-point to room condition is charged against the dehumidifier as the cooling and dehumidifying load.

In winter, room relative humidities in excess of 30 per cent are seldom required in a system designed for comfort conditioning only, and a low

saturating efficiency may be desirable, or even necessary, especially if the same volume of air is handled as in summer. With a spray type dehumidifier the main sprays may be shut off and only the eliminators need be flooded; which may give sufficient moisture. In other cases, such as those in which cooling coils are sprayed, the spray water supply may be throttled. If the saturation efficiency of the sprays is too low, the spray water may be heated. The amount of heat put into the spray water by open or closed water heaters will be equal to that required to bring the dew-point temperature of the air entering the sprays up to that required before entering the preheater. It is possible, where clean steam is available, to introduce steam directly into the air stream to produce the desired dew-point temperature of supply air. However, the steam must be exceptionally clean, or objectionable odors will result.

It should be noted that the quantity of outdoor air to be introduced is affected by infiltration and leakage. Infiltration will reduce the quantity to be introduced by the system, while leakage may have to be offset by an increase in the quantity of outdoor air.

COOLING LOAD

The method of determining the cooling load for a conditioned space or spaces is outlined in Chapter 15. As pointed out therein, many of the items of heat gain are variable and do not reach their maximum values simultaneously. Proper consideration of these peaks and the avoidance of pyramiding these peaks in the cooling load calculations are stressed. Maximum solar heat gain on an east exposure is seldom coincident with the maximum outdoor wet-bulb.

A large difference in the time-incidence of the peaks between various spaces or parts of the same space indicates the necessity for zoning. In a building having an east and west exposure where solar heat gain forms a fair share of the cooling load, the times of their individual peaks are apt to be some hours apart, and the peak load of one plus the off-peak load of the other will be substantially less than their combined peak loads. Proper zoning will permit operation to take full advantage of this condition or of similar conditions of non-simultaneous peaks and will result in a lower total load and in savings in equipment.

A factor, similar in effect and closely related to the non-simultaneous occurrence of peak loads, is diversity. Typical of this is the case of a large department store where the air handling equipment serving a certain space must be sufficient to handle the load created by the throngs of people attending sales in that space. Under such a condition the number of people in other spaces is usually normal or below. While this means that the air handling equipment for certain departments must be large enough to cope with the situation, the refrigeration equipment need be only large enough to handle the average maximum. If a system employing zone recirculating fans and a single central fan and dehumidifier were used, the saving would be reflected in the capacity of the central fan and dehumidifier. Another example of this diversity is found in an office building having restaurants and stores of certain types in the first story and basement. At noon, when the restaurants and stores are crowded, the offices are below normal occupancy.

Heat lag should be carefully considered in the cooling load calculations. In certain types of buildings the effect of solar radiation is still apparent several hours after the sun has shifted from that exposure. In other

types having a much lighter construction, the heat gain due to solar radiation decreases markedly with the passing of the sun. Some walls, having been warmed by the sun, may radiate heat long after the passing of the sun, thus requiring lower inside temperatures to offset the radiant energy.

Buildings have considerable heat storage capacity which can often be utilized to great advantage and which has more than once provided an unexpected safety factor. If a space is kept below the design inside temperature for some time, the interior walls, floors, furniture and fixtures begin to assume the temperature of the space. Where the time is sufficient, the entire mass rather than merely its surface may reach the room temperature. Thus, when a space has been precooled below the design maximum temperature for a period of time prior to the advent of the peak load, and the heat gain begins to increase to peak conditions, some of the increase is used in raising the temperature of the furniture, fixtures, etc., to the design conditions and the cooling load can be reduced accordingly. However, unless very accurate data with regard to the mass, surface, specific heat, etc., of the items within the space are available, due caution must be used in discounting the cooling load for this storage effect. In the absence of reliable data this allowance is often a matter of experience rather than calculation.

Where air conditioning supply and return ducts pass through unconditioned spaces, there will be a transfer of heat from these spaces to the air in the ducts, even though these ducts are well insulated. An allowance should be made for this heat gain and included in the heat estimate so that air can be supplied at a temperature low enough to offset the rise caused by this heat gain (see Chapter 41). There will also be some heat gain to the air in ducts passing through conditioned spaces, but since a cooling effect is produced in the space through which the duct passes, this is not a loss and usually can be compensated for by adjustment of air quantities between the various spaces.

HEATING LOAD

Methods of calculating the heating load are shown in Chapter 14. Many of the factors outlined previously under Cooling Load, such as zoning, non-simultaneous peaks, and diversity, apply in the reverse manner due to the heating requirements instead of the cooling requirements. However, these factors affect the heating load from the standpoint of control of inside conditions, over-all performance, and economy of operation more than from a capacity of equipment standpoint. It is not only necessary to heat a building or space to its design conditions when there is but the merest fraction of normal occupancy, and when there are practically no lights, internal heat, or solar radiation, but it is also necessary to provide capacity to heat the building quickly when sudden cold follows relatively warm weather, as may occur after a week-end or holiday shut-down. However, in normal operation during week-ends and holidays, buildings are usually kept at a holding temperature to prevent the freezing of services. In many cases, less fuel is required to continue operation of the heating plant at a near-normal rate and maintain the building or space at a temperature of 50 to 65 F for some time than to shut the system down and then bring the temperature back to normal through forced operation of the heat generating equipment with a consequent loss in efficiency.

AIR QUANTITY AND EFFECTIVE TEMPERATURE DIFFERENCE

The difference between the room air temperature and the supply air temperature at the outlet to the room is known as the effective temperature difference. In the theoretical case of a dehumidifier having 100 per cent saturating efficiency and where this air is delivered directly to the room without temperature increases due to heat gain, then the effective temperature difference is the difference between room temperature and apparatus dew-point temperature. If duct heat gains are considered a part of the room load, this still holds true. The apparatus dew-point, as outlined previously, is fixed by the latent and sensible loads of the space, but in many cases, it is desirable to deliver more air to the spaces than is indicated by the difference between the room temperature and the apparatus dew-point.

It has been indicated that where a percentage of air is passed through the dehumidifier without being treated, the relationship is modified in direct proportion, and that if room air is passed through untreated, no effect on the heat balance results. Similarly, if room air is passed around the dehumidifier and mixed with the treated air the heat balance is not adversely affected. Therefore, if the quantity of air passed through the dehumidifier is determined by the usual methods, room air can be passed around the dehumidifier and mixed with the dehumidified air, increasing the supply air quantity and temperature and decreasing the effective temperature difference. Thus if the difference between the room temperature and the apparatus dew-point indicates that 10,000 cfm at 30 deg below room temperature will be required to hold conditions, that quantity can be passed through the dehumidifier and cooled to 30 deg below the room temperature, then mixed with 10,000 cfm of room air; resulting in a supply air quantity of 20,000 cfm and an effective temperature difference of 15 deg instead of 30 deg. Air supply outlets and grilles that have a high induction ratio are available and cause a large amount of room air to be mixed with the air leaving the outlet within a short distance of the outlet through the induction effect of the air stream. A proper selection of outlets may make it possible to introduce air at low temperatures and high velocities without causing objectionable drafts or cold spots, but care must be used to see that too little air motion is not a result. Low effective temperature differences may be required for this reason. While the use of a high effective temperature difference results in a saving in initial cost of fans and ducts and in the operating cost of fans, this difference should be carefully considered. If the sensible heat load of a space is subjected to substantial variations, low effective temperature differences should be considered, since systems employing low effective temperature differences require less precision in controls.

Reduction of air quantity by slowing down the fans for the winter season and increasing the temperature difference often is feasible. A saving in fan power can thus be effected, provided the air distribution remains adequate.

Extremes should be avoided in all cases. For summer air conditioning, low supply air temperatures result in larger heat gains to the air passing through the ducts, as well as in poor control. Too high a supply air temperature may result in excessive initial and operating costs. Suggested limits for the effective temperature difference are from 12 to 20 deg; the actual selection being based on the requirements of the particular case. For winter air conditioning, too high supply air temperatures result in

excessive heat losses from the ducts and stratification within the room unless thorough mixing is assured, while too low supply air temperatures may cause drafts, high operating costs, etc. Suggested limits are from 15 to 35 deg. There can be no set rule and each case should be judged according to its particular requirements.

Reference may be made to Chapter 40 for further discussion of the most satisfactory design difference between the entering air temperature and volume in relation to the desired room condition.

INDUCTION CONVECTORS—LOW PRESSURE TYPE

Induction convectors, located in the room that is to be served, utilize a jet of conditioned air (or primary air) to induce a flow of room or secondary air which mixes with the primary air Fig. 4. The mixture is discharged

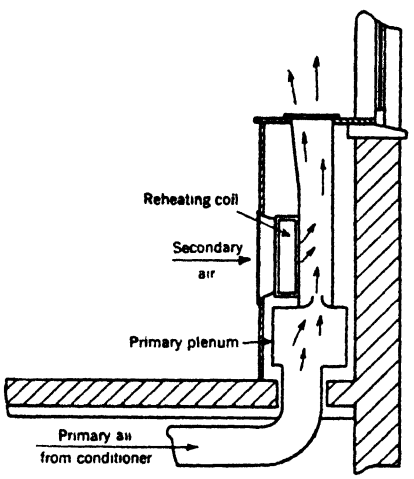

FIG. 4. INDUCTION UNIT (LOW PRESSURE TYPE)

into the room through a grille at the top of the convector. Heating coils are located in the secondary air stream. The output is controlled either by manually or automatically throttling the air jet. Heat may be supplied to the coil in summer as well as in winter. These induction convectors present several advantages. Since the secondary air stream is thoroughly mixed with the high velocity low temperature air stream before leaving the discharge outlet of the device, the resultant temperature of the mixture is satisfactory even though the primary air is introduced at a temperature too low for ordinary methods of distribution. One of these devices usually is provided under each window in place of the customary direct radiator, and combines the air distribution system with the heating system. With a conventional system it may be necessary to provide supplementary heating in the form of direct radiation. Induction convectors may be selected with heating coils having sufficient capacity under gravity conditions (that is, with the fan system shut off and no primary air entering the device) to maintain the room at a reasonable temperature in winter. The use of low temperature, dehumidified air which has not been reheated or mixed with room air before

delivery to the room may permit a reduction in fan capacity and the use of smaller ducts. In some cases a by-pass may be desirable in order to maintain the primary air volume and to provide additional control. This system can provide a degree of zoning that is usually difficult with conventional design since the air delivered by each unit can be controlled individually. Selection of induction convectors should be made with due regard to noise level. The inductive capacity of the device increases with the jet velocity, but high jet velocities may result in objectionable noise.

INDUCTION CONVECTORS—HIGH PRESSURE TYPE

Another type of induction convector Fig. 5 employs nozzles which produce a high velocity air jet without objectionable noise. The term,

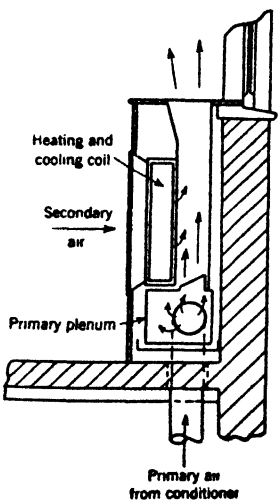

FIG. 5. INDUCTION UNIT (HIGH PRESSURE TYPE)

high pressure, is to some extent inaccurate, since the air pressure at the nozzles, while several times that used with a low pressure induction convector, is still less than the total resistance pressure of a conventional central system. The high velocity jet of primary air induces a flow of air from the room through coils located in the secondary air stream and supplied with chilled water in summer and with hot water in winter. The chilled water removes a large portion of the sensible heat in summer and the hot water supplies the sensible heat loss in winter. The primary air is delivered at a sufficiently low dew-point to compensate for the latent heat gain in summer. In winter the primary air is supplied at a sufficiently high dew-point to take care of latent heat losses. Control of temperature is obtained by throttling the water quantity supplied to the secondary coil. The required flow of primary air is greatly reduced due to the fact that a portion of the sensible heat load is carried by the secondary air stream. Since the primary quantity is small, very high velocities can be maintained in the supply ducts without requiring fan power in excess of that for a conventional system. This means that the supply ducts or pipes can be very small and can be run in chases, or

furred in at columns along with the water pipes. The primary air is treated in the usual manner to reach the required dew-point and a surface or spray dehumidifier or a dehydrator may be used. The primary air quantity is sufficient for ventilation purposes and frequently consists entirely of outdoor air. The water piping for the coils can be so valved that hot water will be supplied to one zone that may require heating while cold water may be supplied at the same time to a zone that requires cooling.

This system usually is limited in application to hotels, apartments, office buildings and other multi-room installations having a large perimeter with relation to the floor area. The units usually are installed beneath the windows, replacing direct radiation or thermally-circulating enclosed convectors. Where the spaces to be conditioned extend a considerable distance from the outer wall into the interior of the building, a separate system or zone for the conditioning of the interior portions may be required.

EVAPORATIVE COOLING

In climates where, on the hottest days, the outdoor wet-bulb depression is relatively great, it may be possible to dispense with refrigeration or other cooling sources by use of the evaporative cooling effect. A well designed air washer using recirculating sprays will reduce the entering dry-bulb temperature to within a degree or two of the entering wet-bulb condition. Thus, it may be possible that, with air entering at 100 F dry-bulb, 60 F wet-bulb, a leaving condition of 62 F dry-bulb, nearly saturated, can be obtained. Under some conditions of latent and sensible heat load, evaporative cooling may be adequate.

At times when the outdoor wet-bulb temperature is not quite low enough to permit the use of straight evaporative cooling it is possible to use precooling convectors with refrigeration, well water or a cooling tower as the basic source of sensible heat removal to reduce the wet-bulb temperature of the air before it enters the spray chamber. Where internal heat loads are high, this scheme may be more economical than one using return air. Where the required supply air dew-point is too low to permit straight evaporative cooling and where the sensible heat load is not too great, intentional partial saturation may be employed. That is, the low dew-point of the outdoor air is utilized by permitting some of this air to pass through the humidifying sprays untreated, or to by-pass the humidifier. All of these remarks with regard to evaporative cooling are based on the assumption that all of the supply air will be taken from outside. Provision should be made in most cases for the return of some air from the conditioned spaces for control purposes as well as for economy of fuel in winter.

PRECOOLING

Where sufficiently cold water from wells or streams is available, a saving in refrigeration may be obtained by the use, in location ahead of the dehumidifier, of precooling coils through which the cold water is circulated. The resultant cooling of the air decreases the load to be carried by the dehumidifier and refrigeration plant. In normal practice the water, after passing through the precooling coils may be further utilized in the refrigeration plant condenser. The economic advantages of this scheme are apparent and it is frequently used.

SENSIBLE COOLING WITH UNWETTED COILS

Under favorable atmospheric conditions where a large wet-bulb depression exists and the dew-point of the outdoor air is sufficiently low at all times, acceptable cooling may be obtained by removing only the sensible heat from the outdoor air delivered to the rooms. Under this condition of a great wet-bulb depression, a temperature-reducing coil may be located in the air stream and supplied with water from a cooling tower. When humidity control is desired, sprays to saturate or partially saturate the air may be used down-stream from the unwetted coil. Saturation or partial saturation after the coil will reduce further the dry-bulb temperature and the air quantity required. This system has very definite application in hot dry climates.

RUN-AROUND SYSTEM

An interesting method of control is found in the use of combined reheating and precooling usually termed the run-around system. Typically three coils are placed in series in the air stream. The primary one receives liquid that has been cooled in the third coil. The center coil is maintained at a temperature colder than the dew-point of the air. The primary coil thus pre-cools the air and the third coil reheats the saturated air from the center coil. The third coil is heated by the relatively warm water coming to it from the primary coil. The run-around scheme has the advantage of permitting a higher supply air dew-point temperature than would be possible otherwise. This is due to the fact that continual reheating is available, which is not a large penalty on the refrigeration plant since it provides precooling at the same time. This reheating at peak load creates an artificial sensible heat gain which increases the ratio of sensible heat to total heat and for a given room temperature results in a higher apparatus dew-point. Thus, while the volume of supply air is increased, the low-side temperature level of the refrigeration plant is raised and this may effect savings in initial and operating costs. The run-around system has the disadvantage of providing a decreasing amount of heat for reheating as the demand for reheating increases.

SELECTION OF TYPE OF SYSTEM

If the perimeter of the building is large with regard to the area, and if there are many rooms, induction convectors of either the low or high pressure type may be employed. Occasionally a dual system, one duct carrying air at a warmer temperature than the other, may be considered.

Low buildings with large floor areas may be divided into sections or zones with separate central air supply systems to facilitate temperature control. In the case of large department stores it may be possible to provide a single conditioner with a fan delivering the conditioned air to local mixing fans which supply the various departments or spaces. This application is limited by the practicability of running the large conditioned air ducts to the various recirculating fans. Each vertical section of the building also may be supplied by a separate fan delivering conditioned air to local mixing fans. In many cases the most economical and satisfactory scheme may be to employ a hot water or steam reheater in each branch duct to each room. Where vertical sectionalizing is not indicated, the building may be divided into horizontal groups, each handled by a central system and adequately zoned. In some large

buildings, apparatus rooms for the systems may be located in the basement and in the attic and on intermediate floors.

In high buildings the necessity for horizontal sectionalizing may be suggested by the size of air supply and return risers and by the extent to which they encroach upon usable space. Each story should be cut off by doors from other stories as otherwise the cool air tends to collect in the lower story and the warm air is forced to the upper story.

Balconies and large lobbies in theatres and similar high rooms frequently justify the use of separate zoning fans, to counteract the tendency of the heavier, cooler air to collect at the lower levels.

Fans operate at full capacity continuously in many systems and therefore should be selected for good efficiencies. In winter when higher temperature differentials are used, it is sometimes practicable to deliver smaller air quantities than when cooling.

In climates where winter temperatures fall below freezing, the tempering coils should be of the steam-distributing type; or if they are heated by a liquid, this liquid should contain some anti-freezing substance such as ethylene glycol. If hot water is employed in cold climates, the temperature control of the air should be obtained through use of face and by-pass dampers rather than by throttling the valves, to prevent damage due to freezing.

If zone reheaters placed in supply duct branches are employed, they should be of such type as to be heated over the entire surface so that no temperature-stratification can occur in the delivered air. Steam distributing-tube coils or mechanically circulated water coils are serviceable in such cases and throttling valves may be used.

Refrigeration equipment must be carefully selected to satisfy the particular requirements of each installation. For some small plants the evaporator may be placed in the air stream, when type of refrigerant and nature of occupancy permit. In many cases, chilled water coils are required by considerations of safety. Where low temperature and relative humidity are necessary, brine, often of calcium chloride, may be indicated.

Condensing requirements must have economic analysis. Wells, public water service, cooling towers and evaporative condensers present possibilities for consideration. Condenser water may have a secondary use for roof sprays in hot weather, and is usually suitable for lawn sprinkling. Most health department rules in cities prohibit any connection from refrigerant condensers that might permit the water to be used for drinking or lavatory purposes.

Practically without exception, air cleaners should be provided for both outside and recirculated air.

Control of temperature and of relative humidity by automatic means is vital, if comfort and economical operation of air conditioning equipment are to be attained.

The insulation of ductwork is not merely a matter of economics but sometimes is a necessity from the standpoint of limiting the temperature change of the air between the conditioning apparatus and the point of final delivery. Such temperature change of the air should be taken into account when apportioning the air and sizing the ducts. When computing heating or cooling loads, due allowance must be made for the effect of any hot or cold ducts or pipes contained in the space under consideration and insulation must be incorporated where necessary or justified. Con-

sideration must also be given to the possibilities of condensation of moisture on either the inside or outside surfaces of pipes, ducts, housings, fan encasements, etc., and insulation should be applied to prevent corrosion and water damage and to conserve refrigeration.

The location of the apparatus room often is determined by building construction or available space. The closer the apparatus room is to the conditioned space, the less expensive are the ducts. If the equipment is noisy, it should be located at some distance from the occupied spaces or be provided with adequate sound and vibration treatment. The scattering of wet apparatus throughout a building is to be avoided unless suitable precautions are taken. It must be remembered that encroachment on spaces that are otherwise usable can be charged against the system as an operating cost.

In general the apparatus should be arranged to have straight line air flow. Each change in direction is the cause of air resistance, and in addition elbows and offsets may cause eddy currents resulting in stratification. The usual order of equipment, beginning at the outside air intake is: weather hood or louvers, outside air dampers, return air connection, filters, tempering coils, cooling coils or sprays, by-pass connection with or without reheaters, reheaters, fan and distributing ducts.

Screens at the intake prevent the entry of large foreign matter, birds, etc. A hood or louver at the outside air intake prevents the entry of rain and snow. Since in most climates there are many days during which use of 100 per cent outside air unheated or uncooled may be economical, the areas of all air-passing and treating apparatus should be large enough for such a volume, and the exhaust or spent air equipment should be capable of discharging out of doors, all of the air admitted.

The by-pass connection normally connects the return air duct system with the apparatus casing between the conditioner and the supply fan. Usually the by-pass opening is sized to handle about 50 per cent of the fan capacity where a variable by-pass is used, though extreme load variations may require a larger size. It is at times good design to locate a reheating coil in the by-pass connection to permit using some by-pass air when heating is required. Since the relatively high resistance of the cooling coil or spray is to be balanced by the heating coil and by-pass connection, enough heating surface can be provided to raise the temperature of the by-pass air to the point where the mixture of by-passed air and conditioned air will have the required temperature. When a variable by-pass is used, a damper working in opposition to the by-pass damper should be placed across the face of the dehumidifier, for unless the resistances of the two are carefully balanced at all operating points, the proper mixtures of air will not be obtained. Outside air that has not been dehumidified should not be by-passed around a cooling coil or spray dehumidifier if accurate control of the delivered relative humidity is desired. Where the by-pass is made a part of the dehumidifier or conditioner and is located on the top or side of it, the return air connection should be arranged so that stratification of return air is insured, baffles being provided to accomplish this purpose if necessary. Where return air and by-pass air connections are taken off a return duct system, it may be necessary to install a back-draft damper between the return air connection and the by-pass connection. When the by-pass damper is at maximum opening it may be much easier for outside air to pass through the return damper, into the return duct connection and through the by-pass than for return air to pass through the by-pass connection into the

fan. Air tends to take the path of least resistance and, if the dehumidifier resistance is high, and if the return duct resistances are low, this situation is apt to occur. A recirculating air fan instead of a back-draft damper may be required for this case if the failure of return air to reach the dehumidifier or conditioner is a serious matter under reduced load conditions.

LOCATION OF APPARATUS

In general, the outside air intake, preheaters, and return air connections precede the conditioner, while the by-pass, reheaters and fan follow it. In the case of a blow-through system, where the fan is located ahead of the conditioner, the leakage of air at the conditioner is outward instead of inward and may be accompanied by water leakage.

The location of the complete apparatus assembly including the dehumidifier will be dependent on the type of building, spaces available, structural characteristics, etc. The type of conditioner used may limit the location under certain conditions. Where cooling coils employing chilled water or brine as the cooling agent are used, there are few limitations with regard to location other than those of pumping power, working pressures, piping costs, etc. Where spray dehumidifiers are used, very definite limitations present themselves, and these may require certain extraneous equipment to make the system workable. If several spray type dehumidifiers are located on different levels, thus involving different water pressures, a surge or storage tank to which the return water from each dehumidifier can be taken is required. Should the water level in the pan of the dehumidifiers be low in relation to that of the surge tank, return water pumps will be required, and these pumps will have to be operated until the water supply lines are drained in order to prevent flooding of the lower dehumidifiers. Where spray dehumidifiers are on the same level, equalizing lines between the pans may be required if a storage tank is not provided. It is exceedingly important that water-tight drained floors shall be provided under all overhead cooling systems, since water condensed out of the air generally will be present and may damage the interior finish of the rooms below the apparatus.

All of the various pieces of equipment from the outdoor air intake through the fan usually are connected together by sheet metal casings. Frequently the building structure or specially constructed walls or partitions may be used to form a portion of the casing. In any case the casing or connection must be sufficiently sturdy for the required duty. Sheet metal work must be well braced not only to prevent vibration under pulsations in air flow but also to withstand the abuse of normal usage. Casings should be braced wherever access doors are installed and all large panels should be adequately reinforced by structural steel.

Accessibility for Service

Each apparatus layout is to be made with accessibility in mind. Where cooling convectors are used, space for removing and repairing or replacing them should be provided. Adequate space is to be provided for the servicing and replacement of eliminators. Whether these accompany sprays or wetted coils, filters must be so located that the proper cleaning, replacement or routine servicing can be accomplished without difficulty. Free access to the bearings of all moving machinery is a necessity. Provision should be made for the complete removal and replacement of

any parts of the apparatus that are subject to wear, deterioration or damage, whether it may be filter, fanwheel, motor, pump, impeller or heat transfer surface.

DESIGN PROCEDURE

The customary design procedure is outlined herewith. For simplification the procedure is set up on the basis of a year-round system. For systems designed only for winter or summer, the unrelated parts may be omitted.

1. Selection of design conditions (inside and outside).
   a. Summer.
   b. Winter.
2. Determination of outside air requirements.
3. Determination of cooling load.
   a. Room sensible heat gain.
   b. Room latent heat gain.
   c. Room total heat gain.
   d. Grand total heat gain.
4. Determination of heating load.
   a. Room sensible heat loss.
   b. Room moisture loss.
   c. Humidification requirement.
   d. Total heating requirement.
5. Determination of apparatus dew-point and dehumidified or humidified air quantity.
   a. Summer (full load and part load).
   b. Winter.
6. Supply air temperature difference and quantity.
   a. Summer.
   b. Winter.
7. Equipment selection.
8. Equipment layout.

The foregoing steps are merely typical. Many applications will require at least a preliminary investigation of some of the latter steps before proceeding with the earlier steps. A permanent record of all design assumptions and computations should be made and preserved for comparison with the performance of the installation.

Chapter 44

OWNING AND OPERATING COSTS

Fixed Charges: Amortization, Interest, Taxes, Insurance, Rent; Maintenance Costs, Service Costs: Operating Refrigeration Equipment, Condenser Water, Heating

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THE purpose of this chapter is to discuss the owning and operating costs of heating, ventilating, air conditioning and refrigeration systems for buildings from an economic standpoint so that owners or prospective purchasers may compare the operating economics of one system with another and evaluate properly the over-all costs of the systems instead of considering only the first cost.

There are cases in which it may be desirable to study the possibilities of installing a system for the purpose of obtaining a substantial increase in income or a better return on the investment due to: increased patronage in theaters, stores, or hospitals; increased occupancy in office buildings; improved efficiency of employees in offices or factories; or improvement in a manufactured product or a decrease in its cost of production.

Owning and Operating Costs may be grouped under three headings: (1) *Fixed Charges*, (2) *Maintenance Costs*, and (3) *Service Costs*.

FIXED CHARGES

Fixed Charges, which are the costs of owning the system, include: (1) Amortization, (2) Interest, (3) Taxes, (4) Insurance, and (5) Rent.

Amortization

Amortization cost will depend on: (1) the total first cost, and (2) the amortization period.

The *total first cost* of an installation is the actual dollar outlay or capital expenditure required to buy and install the air conditioning, or heating and ventilating system ready for operation. It can be divided into two parts: (*a*) The first cost of the air conditioning or heating and ventilating system itself, and (*b*), other first costs incurred because of the installation of the air conditioning or heating and ventilating system.

The *first cost* of air conditioning or heating and ventilating systems includes the following:

1. Heat producing equipment including boilers, burners, etc.
2. Heat distributing equipment including direct radiation, piping, etc.
3. Air handling equipment including fans, air heaters, air conditioners, filters, controls, etc.
4. Air distributing equipment including ducts, outlets, grilles, etc.
5. Refrigerating equipment including piping, pumps, etc.
6. Water conservation devices including towers, evaporative condensers, etc.

The best procedure for establishing the first cost of any system is to select the various parts after thorough engineering study, and then to estimate the installed costs of same. When such detailed work is not warranted or when only rough comparisons are desired between several types, approximate unit costs are of value as time savers.

Approximate installed prices of the various parts are shown in Tables 1, 2, and 3 and, as indicated, vary with the size or capacity of the equip-

ment. The apparatus and items included in each group are stated in the footnotes beneath the tables. By use of these three tables it is possible to obtain a reasonable approximation of the cost of heating or air conditioning a given space or building. In order to use the approximate values indicated in Tables 1, 2 and 3, a rough estimate of the load is required. If time does not permit a determination of the load and if extremely rough figures will suffice, Table 4 may be used as an indication of the price of various types of air conditioning applications.

Other first costs, incurred because of the installation of the air conditioning or heating and ventilating system, include costs of electrical work, plumbing, miscellaneous piping, building alterations, cutting, patching, remodeling, or redecorating after installation, consulting engineer's fees, licenses, permits, etc. These vary so widely that no approximations are possible and each case must be considered alone.

The length of the amortization period to be used depends upon: the type and remaining life of the building or space for which the system is to be used; the type of equipment to be employed as a part of the system; the character of the business; and the lease or ownership conditions. For small shops in rented quarters on short term leases, a period of 5 years or less may be proper, whereas for larger installations in buildings that are owned outright a period of 10 or 20 years or more may be used.

Depreciation due to deterioration and obsolescence must also be considered in arriving at the amortization period. Deterioration and

TABLE 1. TYPICAL INSTALLED COSTS OF HEAT PRODUCING AND HEAT DISTRIBUTING SYSTEMS

BTU PER HOUR (MILLIONS)	SQ FT EDR (STEAM) THOUSANDS	BOILER HORSE POWER	COST IN DOLLARS—PER MILLION BTU PER HOUR[a,b]			
			1	2	3	4
			BOILERS WATER TUBE	BOILERS FIRE-TUBE	HOT WATER SYSTEM FORCED CIRCULATION	DIRECT RADIATION SYSTEM STEAM
0.8	3.3	24		2100	8500	7850
1.2	5.0	36	2300	1750	8200	7600
1.6	6.6	48	2000	1570	8000	7350
2.0	8.3	60	1850	1460	7800	7200
3.0	12.5	90	1600	1230	7600	7000
4.0	16.6	119	1400	1100	7500	7000
5.0	20.8	149	1250	980	7500	7000
6.0	25.0	179	1160	920	7500	7000
7.0	29.2	209	1100	880	7500	7000
8.0	33.3	239	1050	850	7500	7000
10.0	41.6	299	1000		7500	7000
12.0	50.0	358	970		7500	7000
14.0	58.3	418	930		7500	7000
16.0	66.6	478	900		7500	7000
18.0	75.0	538	860		7500	7000

[a]Columns 1 and 2 include hand fired boiler erected, with shaking grates and standard trimmings. Column 1 includes brickwork and rotating soot blowers. Foundations and piping are not included.

Columns 3 and 4 include direct radiation, piping, valves, specialties, and insulation. Boilers, condensate and circulating pumps, boiler connections, and all building construction or alterations are not included.

[b]The approximate figures given above may vary as much as 30 per cent due to job conditions, labor rates, and locality. These figures represent the selling prices of the individual items indicated above based on costs encountered in the year 1940. It is suggested that correction be made according to the particular locality for increases in labor and material costs since that year.

TABLE 2. AVERAGE INSTALLED COSTS OF FORCED AIR HEATING AND AIR CONDITIONING APPARATUS

CFM Supply Air (Thousands)	Cost per CFM—Dollars[d]			
	1	2	3	4
	Air Conditioning Equipment[a]	Heating and Ventilating Equipment[b]	Ducts Office Bldgs.[c]	Ducts Specialty Stores[c]
5	0.300	0.210		0.250
10	0.270	0.180		0.249
15	0.250	0.155		0.247
20	0.235	0.140		0.245
30	0.220	0.120		0.240
40	0.210	0.110	0.340	0.235
60	0.210	0.110	0.330	0.230
80	0.210	0.110	0.325	
100	0.210	0.110	0.320	
120	0.210	0.110	0.310	
140	0.210	0.110	0.305	
160	0.210	0.110	0.295	
180	0.210	0.110	0.290	
200	0.210	0.110	0.280	

[a] *Air conditioning equipment* includes fans and drives, filters, heaters, spray dehumidifiers or cooling coils, automatic controls, apparatus casings and insulation, and recirculating pumps.

[b] *Heating and ventilating equipment* includes fans and drives, filters, heaters, automatic controls and apparatus casings.

[c] Includes ducts, grilles, outlets, insulation where required and specialties.

[d] The approximate figure given above may vary as much as 35 per cent due to job conditions, labor rates and locality. Figures are based on conventional systems. Building alterations, piping, plumbing and wiring are not included. These figures represent the selling prices of the individual items indicated above based on costs encountered in the year 1940. It is suggested that correction be made according to the particular locality for increases in labor and material costs since that year.

TABLE 3. AVERAGE INSTALLED COSTS OF REFRIGERATION SYSTEMS AND WATER SAVING DEVICES

Tons Refrigeration	Cost—Dollars Per Ton[e]					
	1	2	3	4	5	6
	Reciprocating (Water Cooling)[a]	Centrifugal (Water Cooling)[a]	Reciprocating Direct Expansion[b]	Evaporative Condenser[c]	Cooling Tower Steel[d]	Cooling Tower Wood[d]
25	147		106	47		
50	132		86	40		
75	125		77	35		
100	120		72	32	47	40
150	115	137	68	30	45	38
200	113	124			44	36
250	110	115			42	35
300		107			40	33
400		97			38	31
500		93			36	29

[a] Columns 1 and 2 include compressors, evaporators, and water-cooled condensers; auxiliaries; electric motor, starter and drive; refrigeration piping, refrigerant and insulation of cooler and suction lines. Turbine driven centrifugal equipment may cost about 4 to 6 per cent more than motor driven, if condensing turbine and steam condenser, with supplementary equipment, are used.

[b] Column 3 includes same items as Column 2 except evaporator and auxiliaries are omitted.

[c] Column 4—These values are additive to Columns 1 and 3.

[d] Columns 5 and 6 include towers erected and a reasonable allowance for condenser water piping and pumps.

[e] The approximate figures given above may vary as much as 25 per cent due to job conditions, labor rates and locality. Building alterations, supply water and plumbing connections, wiring, chilled water piping and pumps are not included in these figures and may vary widely. Chilled water piping and pump costs may vary between $10 and $50 per ton of refrigeration effect. These figures represent the selling prices of the individual items indicated above based on costs encountered in the year 1940. It is suggested that correction be made according to the particular locality for increases in labor and material costs since that year.

TABLE 4. APPROXIMATE COSTS OF ALL-YEAR AIR CONDITIONING[a,b]

APPLICATION	SELLING PRICE PER UNIT INDICATED											
	SQ FT NET AREA			PERSON			TON REFRIGERATION			CFM SUPPLY AIR		
	LOW	AVG	HIGH	LOW	AVG	HIGH	LOW	AVG	HIGH	LOW	AVG	HIGH
Banks	$1.25	$2.00	$3.50	$80	$140	$320	$350	$480	$700	$0.95	$1.40	$2.75
Department Stores — Basement	0.60	1.00	1.15	25	40	100	250	325	400	0.60	0.80	1.00
Department Stores — Main Floor	0.60	1.05	1.25	25	40	80	250	325	400	0.60	0.75	0.90
Department Stores — Upper Floors	0.60	0.90	1.10	30	45	100	300	350	400	0.60	0.80	1.00
Hotels—Guest Rooms				$240[c]	$300[c]	$420[c]						
Office Buildings	$0.85	$1.25	$2.00	110	135	180	$300	$375	$500	$0.75	$1.05	$1.50
Offices—Small Suites	1.00	1.75	3.25	110	180	350	300	450	800	0.75	1.25	2.50
Restaurants	1.40	2.20	3.50	15	18	25	215	280	400			
Specialty Shops — Barber Shops and Beauty Parlors	$1.50	$2.50	$4.00	$50	$100	$150	$325	$400	$500	$0.70	$1.00	$1.50
Specialty Shops — Dress Shops	1.25	1.50	2.00	45	55	75	230	275	350			
Specialty Shops — Drug Stores	1.25	1.50	2.00	45	55	75	240	275	325			
Specialty Shops — Five-and-Ten	0.90	1.20	2.80	22	33	55	220	270	425	0.80	0.95	1.50
Specialty Shops — Shoe Stores	0.95	1.20	1.75	35	40	50	230	275	350			
Theaters				$9[d]	$15[d]	$23[d]	$215	$300	$450	$0.65	$1.00	$1.25

[a]Modern Air Conditioning, Heating and Ventilating, by W. H. Carrier, R. E. Cherne and W. A. Grant (*Pitman Publishing Corp.* 1940, p. 64).

[b]There is a wide variation in unit prices such as shown above, due to differences in load concentration and in complexity of physical layout. Prices cover air-conditioning work only, for year-round use (except the *low* column, which in general includes summer cooling only). Net area (square feet) includes corridors, but excludes elevators and service spaces. ***Excluded*** are the cost of plumbing and steam connections, electrical wiring, painting and redecorating, building construction and alterations, and boilers or burners. Low figures in general are simply direct expansion systems using city water for condensing. High figures are usually chilled water systems with cooling towers or evaporative condensers, and may be considered high quality systems as well.

[c]Price per room.

[d]Price per seat.

maintenance generally go hand in hand. If a long depreciation period is to be used, then the item for maintenance, repair and replacement of wearing parts must be greater than for a short depreciation period.

Obsolescence depends mainly on time required for the equipment to become out-moded. Air conditioning, particularly, would probably

TABLE 5. APPROXIMATE LIFE OF EQUIPMENT

(Including Obsolescence and Deterioration)[a]

	LIFE IN YEARS
1. HEAT PRODUCING EQUIPMENT	
(*a*) Boilers	15
(*b*) Stokers and burners	10
2. HEAT DISTRIBUTING EQUIPMENT	
(*a*) Piping—copper	20
(*b*) Piping—iron	10
(*c*) Radiation—concealed	12
(*d*) Radiation—direct	10
(*e*) Valves and specialties	5
3. AIR HANDLING EQUIPMENT	
(*a*) Filters—automatic	8
(*b*) Heating and cooling coils	10
(*c*) Spray humidifiers and dehumidifiers	10
(*d*) Fans	10
(*e*) Air conditioning units	10
(*f*) Motors	15
(*g*) Electrical starting equipment	8
(*h*) Pneumatic control systems	10
(*i*) Electric control systems	8
4. AIR DISTRIBUTING EQUIPMENT	
(*a*) Ductwork	20
(*b*) Outlets, grilles	20
(*c*) Duct insulation	10
(*d*) Painting	
5. REFRIGERATING EQUIPMENT	
(*a*) Centrifugal refrigerating machines	15
(*b*) Reciprocating refrigerating machines	10
(*c*) Motors and starters (see Item 3 above)	
(*d*) Piping—copper	20
(*e*) Piping—steel	15
(*f*) Pumps	15
6. WATER SAVING DEVICES	
(*a*) Evaporative condensers	10
(*b*) Cooling towers	10
(*c*) Wells	Varies Widely

[a]Modern Air Conditioning, Heating and Ventilating, W. H. Carrier, R. E. Cherne and W. A. Grant (*Pitman Publishing Corp.* 1940, p. 66).

suffer more from obsolescence in small plants than in large establishments. In addition the obsolescence of the building or property in which the equipment is installed may have a similar effect upon the equipment.

An approximation of the useful life of various items of equipment and parts of systems is shown in Table 5. It should be noted that if an appropriate maintenance item is not established, the rate of equipment deterioration may be substantially increased.

Interest

The interest chargeable may not represent the existing money rates. It may include an item to cover the diversion of capital or other items depending on existing tax laws which may make it necessary to charge interest due to diversion of capital as a cost item. It should be noted that interest may be based on an unamortized balance. As an example, a 15 year amortization period with a 4 per cent interest rate will approximate a 2.1 per cent average annual interest rate.

TABLE 6. OWNING AND OPERATING COST

FIRST COST		ANNUAL SERVICE COST	
Cost of mechanical system		Electric Power Costs	
Other costs		Fans	
First Cost (FC)—Total		Pumps—Chilled water	
		Pumps—Condenser water	
ANNUAL FIXED CHARGES		Pumps—Well water	
		Cooling tower fans	
Amortization—Depreciation period Y years		Cooling tower pumps	
Interest rate I%		Refrigeration machines	
Amortization and Depreciation $\frac{FC}{Y}$ =		Miscellaneous or other	
		Gas	
Interest: $\frac{Y+1}{2Y} \times I$ =		Coal	
Taxes		Oil—for boilers or Diesel engines	
Insurance		Steam	
Rent		For direct heating	
Annual Fixed Charges: (Total)		For Ventilation—preheaters	
		For Ventilation—reheaters	
ANNUAL MAINTENANCE COSTS		For Turbine driven equipment	
		For Engine driven equipment	
Lubricating oil and grease		Sewers	
Painting for corrosion protection or other purposes		Charges for discharging well water into public drainage systems	
Replacement of worn parts		Annual Service Costs—TOTAL	
Refrigerant			
Wages of engineer or operator		SUMMARY	
Annual Maintenance Cost—TOTAL		Annual Fixed Charges	
		Annual Service Costs	
		Annual Maintenance Costs	
		Annual Owning and Operating Costs—TOTAL	

Insurance

The rate for insurance may vary considerably depending on the type of structure in which the equipment is located and upon other governing factors. A rate of about $0.60 per $1,000 may be considered as being representative for normal installations.

Rent

If the equipment under consideration is to be located in rented or leased quarters it may be necessary to include an item for space rental.

An orderly arrangement of the various components of owning and operating costs, which will also serve as a check list to forestall inadvertent omissions, is illustrated in Table 6. The formulae for computing amortization and interest are given in the table. Interest should be computed on the undepreciated portion of investment only.

MAINTENANCE COSTS

Maintenance costs include replacement parts and the labor required for making repairs, replacing parts, cleaning, painting, etc. It should be noted that major overhauling or complete replacement may restore the capital value of certain items of equipment, and in such cases the costs incurred may not necessarily be charged as maintenance costs. Generally, routine labor requirements will be the function of an operating engineer or staff and the responsibility of this group may extend beyond the equipment being discussed here; hence, it is important to include only an equitable share of the time of this group. Extraordinary repairs involving special machinery will usually be covered by contract with equipment service divisions and should be accounted for on that basis.

Many of the items included in maintenance costs are highly variable and depend on the type and quality of the purchased equipment. For large air conditioning installations, using high quality equipment, some approximate costs per ton are given in Table 7.

In addition to the costs listed in Table 7, consideration should possibly be given to other items such as: water treatment for boilers; other boiler and heating plant cleaning and repairs; repair and replacement of heating plant valves, traps, and vents; water treatment for cooling tower or chilled spray water; drive belts, possible damage due to freezing weather; cleaning of air ducts; and repairs to insulation.

SERVICE COSTS

Service costs include the costs for power, water, steam, coal, oil, etc., consumed to operate the system.

From the selected equipment and type of installation, it is possible to segregate the relatively constant power loads and the total brake horsepower. Annual power cost can then be figured from the following formula:

$$\text{Annual power cost} = \frac{0.746\ (\text{bhp})\ H\ R}{\eta} \qquad (1)$$

where

bhp = Brake horsepower.
H = Annual operating hours.
R = Power rate, dollars per/kwhr.
η = Motor efficiency (decimal).

In using Equation 1 it must be pointed out that the electric rate, R must reflect the proper combination of energy and demand rates. These vary widely between the utility companies, and sometimes the rate structure is such that it is largely the demand charge which determines the proper value of R to use in Equation 1.

Refrigerating Equipment Operating Cost

In an air conditioning system, the refrigerating equipment is usually the largest power-consuming item to be considered. Also, the prediction

TABLE 7. APPROXIMATE MAINTENANCE COST FOR LARGE AIR CONDITIONING INSTALLATIONS, USING HIGH QUALITY EQUIPMENT

	DOLLARS PER TON PER YEAR
Repairs for refrigeration machinery	0.60
Refrigerant	0.25
Oil and grease	0.07
Painting (Water boxes and dehumidifiers)	0.25
Filters, clean and recoil 4 times per year	0.85
Controls, outside service	0.15
Cleaning air conditioners	1.15

of operating cost is more complex, since the power required for summer cooling is affected by many factors which are of a variable nature. Among these are solar radiation, temperature difference between outside and inside, sensible and latent heat brought in with outside air, sensible and latent heat from people, heat released by electric lights, and, in some cases motor-driven equipment, cooking devices, and other equipment used in the conditioned spaces. Some of these factors vary with the weather while others are substantially independent of it. The relative proportion of each factor varies widely even among installations of the same application, depending on building layout and location, the size and quality of the establishment, the personal idiosyncracies of the owner, and other items.

In a strict sense, it is necessary to evaluate the effect of all such factors in order to predict the operating cost of a refrigeration plant. In most cases this procedure will prove to be too tedious, or it may not be possible because the exact breakdown of load data is unknown. The use of a simplified semi-rational formula, Equation 2, which takes into account for each application the number of hours open for business and the geographical location, will provide a value of H which may be used in Equation 3 to determine the *Season Power Cost.*

$$H_e = m\,(b + cf) \tag{2}$$

where

H_e = Equivalent full load operating hours of refrigeration equipment used for summer cooling during period May 15 to October 15.

m = Total hours during period May 15 to October 15 that the establishment is open for business.

b = Fraction of maximum load from internal heat under average operating conditions.

c = Fraction of maximum load which is due to external sources at maximum design conditions.

f = Ratio of the number of hours for a particular city, when the outside wet-bulb exceeds 65 F, during the period June 1 to October 1 to the total number of hours during that same period. Total hours are assumed as 8 hr per day period for barber shops, department stores, funeral parlors, offices, short hour restaurants, and specialty shops and 12 hr per day period for drug stores, long hour restaurants, and theaters.

Table 8 was calculated from Equation 2. It should be pointed out that certain southern cities may have seasons longer than the 5-month period indicated in Table 8. If it is desired to consider a longer season of operation, the ratio of full load operating hours to hours open for business is smaller; in other words, the *refrigeration load factor* is lower. This is true because the extra increment of days added will be at relatively light load, since the table already includes the more severe part of the season.

TABLE 8. EQUIVALENT FULL LOAD OPERATING HOURS OF REFRIGERATION EQUIPMENT USED FOR SUMMER COOLING MAY 15 TO OCT. 15[a]

APPLICATION	HR OPEN FOR BUSINESS	ATLANTA	BOSTON	CHICAGO	DETROIT	LOS ANGELES	NEW ORLEANS	NEW YORK	PHILADELPHIA	OKLAHOMA CITY	ST. LOUIS	WASHINGTON D.C.
Barber shops	1280	1010	650	720	720	680	1080	830	860	1020	890	940
Department Stores	940	840	560	610	610	580	890	700	720	840	750	780
Drug Stores	2100	1630	950	1060	1060	980	1790	1280	1330	1650	1420	1530
Funeral Parlors	600	440	300	330	330	310	470	370	380	440	400	410
Offices	940	870	560	620	620	580	900	710	740	880	770	810
Restaurant (Short Hour)	1290	970	535	620	620	570	1060	760	800	980	830	880
Restaurant (Long Hour)	2100	1510	820	930	930	850	1690	1170	1210	1530	1300	1400
Specialty Shops (5 & 10)	1090	800	530	590	590	560	860	670	690	810	720	750
Theaters—Continuous	1500	1010	700	750	750	720	1080	850	870	1020	910	950
Theaters—Neighborhood	900	640	420	450	450	430	650	500	520	650	550	580

[a]Modern Air Conditioning, Heating and Ventilating, by W. H. Carrier, R. E. Cherne and W. A. Grant (*Pitman Publishing Corp.* 1940, p. 73).

The season electrical power cost for refrigerating equipment is then given by the following equation:

$$\text{Season power cost} = \frac{0.746\,(\text{bhp}_t)\,T\,H_e\,R}{\eta} \qquad (3)$$

where

bhp_t = Brake horsepower per ton (see Fig. 1) for *average* load during period. (Due allowance should be made for poorer compressor efficiency at light load).

T = Tons of refrigeration at maximum design load.

H_e = Equivalent full load refrigeration operating hours (Table 8).

R = Power cost, dollars per kwhr, including demand and energy charges.

η = Motor efficiency at average load (decimal).

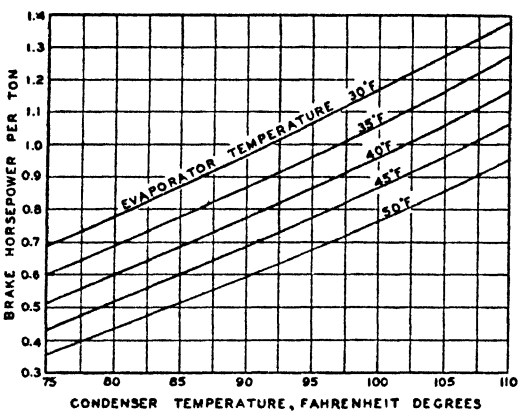

FIG. 1. TYPICAL BRAKE HORSE POWER REQUIREMENTS FOR REFRIGERATION[a]

[a]Values given are representative of "F-12" reciprocating machines of about 25 tons capacity in air conditioning applications. Requirements of smaller machines are usually higher, and for larger machines may be lower. Values shown are for liquid refrigerant at condenser temperature (no subcooling). Subcooling of the liquid may decrease these values approximately 0.3 per cent to 0.5 per cent for each Fahrenheit degree the liquid temperature is lowered.

Table 9 will be useful in estimating the design load in the absence of detailed load estimates.

In considering refrigeration power consumption, it should be noted that the use of weather records for a specific year may lead to large inaccuracies in estimating operating costs, since there may be wide variations from year to year, and therefore, average yearly weather records should be used rather than those for any individual year.

If the refrigeration compressor is steam turbine driven, the same general method can be followed, taking into account average water rate per bhp-hr and the cost of steam.

Condenser Water

Condenser water cost estimates can also be based on equivalent full load operating hours of the refrigeration equipment. The varying temperature of the water at its source, as well as the temperature of the discarded water, must however be taken into account. In general, when water is purchased, control is provided to hold the leaving water temperature (or condensing temperature) constant; and in such case the entering water temperature becomes the major variable and the gpm per ton can readily be calculated for any water temperature rise.

The following equation for cost of condenser water is useful:

$$B = 0.060\, a\, T\, H_e\, C \quad (4)$$

where

B = Cost of water for refrigeration during period, dollars.
a = Average gallons per minute (ton).
T = Tons of refrigeration at maximum design load.
H_e = equivalent full load refrigeration operating hours (Table 8).
C = Water cost, dollars per 1000 gal.

The average gpm per ton must take into account the variable water temperature. When well water is used as a source, and entering and leaving temperatures are considered constant, the average gpm per ton obviously is equal to the design gpm per ton. However, when the source is river or lake water, its maximum seasonal temperature will generally be reached at the same time that the refrigeration load factor is highest.

TABLE 9. REPRESENTATIVE TONS PER 100 SQ FT FOR VARIOUS APPLICATIONS

	LOW	AVG	HIGH
Department Store (Main Floor)	0.50	0.58	0.67
Department Store (Upper Floors)	0.29	0.46	0.54
Dress Shop	0.29	0.50	0.71
Drug Store	0.33	0.54	0.83
Lunch Room	0.83	1.08	1.33
Office Bldg	0.21	0.25	0.38
Restaurant	0.58	0.75	1.00
Shoe Shop	0.29	0.42	0.63
Theater (Tons per Seat)	0.064	0.078	0.093

The average gpm per ton should be calculated from known or estimated water temperatures because they vary through the season. Maximum water main temperatures are given in Chapter 37 but should always be verified locally. In lieu of this tedious work, the average gpm per ton may be taken as 80 per cent of design gpm per ton with reasonable accuracy, for the condition of variable temperature of entering water obtained from rivers and lakes.

When cooling towers or evaporative condensers are used, the windage and evaporation losses are usually between 3 per cent and 5 per cent of the water circulated.

Heating

The method of estimating fuel consumption to balance the building heat loss is given in Chapter 20. It is important to include the fuel required to heat ventilation air as used in ventilating and air conditioning systems. In estimating fuel consumption for ventilation air, the tendency of the conventional control systems to use less than the estimated quantity of outside air in cold weather should be considered in its effect in lowering fuel consumption. In addition, the heat required to accomplish winter humidifying must not be neglected, when this feature is included in the equipment.

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Chapter 45

INDUSTRIAL AIR CONDITIONING

General Requirements; Typical Applications in Storage and Processing: Air Quality Control, Control of Moisture Content and Regain, Conditioning and Drying, Control of Rate of Chemical and Biochemical Reactions, Control of Rate of Crystallization, Elimination of Static Electricity.

INDUSTRIAL air conditioning is as much concerned with the atmospheric conditions required for maintaining the health, safety and efficiency of workers as with those required for the manufacture, processing, and preservation of material, equipment and commodities.

GENERAL REQUIREMENTS

Specialists in the field of industrial hygiene should be consulted in case of doubt concerning the presence of airborne industrial hazards to health. Chapter 10, Air Contaminants, Chapter 12, Physiological Principles, and Chapter 13, Air Conditioning in the Prevention and Treatment of Disease, will be of help in determining the atmospheric conditions which should be maintained around the worker. Comfortable conditions are desirable because they are likely to increase the efficiency of workers.

Table 1 lists the temperatures and relative humidities required for storage of certain commodities and for manufacturing and processing of others. The desirable relative humidity may range from a low of 5 per cent in certain industrial applications, such as insulation winding processes, up to a condition approaching saturation, as in processes relating to textile, tobacco and baking industries. Relative humidities of 50 per cent or less are on the dry side and are conductive to low regains in hygroscopic materials, drying out, increased brittleness of fibrous materials, increased static electricity, and tendencies toward increased dust liberation from the product. Relative humidities higher than 50 per cent are considered to be on the damp side. These conditions are conducive to high regain, promote softness and pliability in materials, decrease static electricity and tend to reduce the generation of product dust.

The most favorable temperature will vary according to the specific material and particular process. In some cases the temperatures listed in Table 1 have no direct influence upon the product itself but do affect the efficiency of employees, which in turn affect workmanship, uniformity and the cost of production. Frequently a compromise between the known optimum condition for processing and that required for worker comfort is unavoidable.

In many processes, the optimum air conditions are variable according to the stage and progress of the processing cycle from the raw material to the finished product. Some materials, such as cotton textiles, begin with a low relative humidity in the carding and picking rooms, and after passing through the various intermediate steps with a gradual increase of relative humidity, are subjected to relative humidities of from 75 to 85 per cent in the final stage of weaving. Other processes are encountered that require the reverse of this procedure, starting with a high relative humidity and finishing with a low relative humidity, as in the manufacture of glue and gelatinous materials and making gelatine capsules.

Safeguarding the health, safety and efficiency of workers requires control of dusts, fumes, smokes, mists, fogs, vapors, and gases, and control of the effective temperature, which includes temperature, humidity and motion of air about the worker.

General ventilation may be relied upon in some cases to control air contaminants. Chapter 9 gives information on natural ventilation. If mechanical ventilation is to be used, Chapter 32, Fans; Chapter 40, Air Distribution; Chapter 41, Air Duct Design; Chapter 33, Air Cleaning Devices; and Chapter 37, Spray Apparatus, furnish information on a broad range of industrial design conditions. If ventilation is to be provided for isolated areas using booths or enclosures, or if local exhaust ventilation is to be employed using hoods, exhaust slots or flexible tubes, fundamental design information will be found in Chapter 46 Exhausting and Conveying Systems.

In controlling effective temperature, or in providing appropriate air conditions for storage and for processing, it may be necessary to humidify or dehumidify, to heat or cool, to clean and to transport the air. These subjects are treated in other chapters in the Guide. When exhaust ventilation is used, care should be taken to properly admit a supply of air into the building to replace that removed; otherwise the exhaust system may fail to perform its intended function. Chance infiltration should not be depended upon for this supply. Optimum results are most probable if the industrial process or project and its air conditioning system are designed together.

TYPICAL APPLICATIONS IN STORAGE AND PROCESSING

Air conditioning in storage and processing may have one or more of the following objectives: (1) air quality control, (2) control of moisture regain, (3) control of rate of chemical reactions, (4) control of rate of biochemical reactions, (5) control of rate of crystallization, and (6) elimination of static electricity.

Air Quality Control

The control of humidity has proved to be useful in blast furnace operations; better uniformity of product and increased rate of production are the result. Very low humidity, with or without control of air flow and temperature, is essential in preserving stored machinery and instruments against corrosion. Control of temperature is necessary in high precision manufacturing. If, in addition to temperature, humidity is controlled and air cleanliness maintained, good conditions for gaging laboratories, for optical goods production, and for such processes as photographic film and pharmaceutical manufacturing may be provided. In libraries and museums, control of humidity and temperature is important to the preservation of the materials stored there; air cleanliness is of almost equal importance in minimizing damage during use or when cleaning the materials. In drafting rooms, control of temperature and humidity to eliminate sweating of workers reduces damage to drawings and tracings, improves accuracy of work that is to be used in direct transfer processes, and improves worker efficiency.

Moisture Content And Regain

In the manufacture or processing of hygroscopic materials such as textiles, paper, wood, leather, tobacco and foodstuffs, the temperature and relative humidity of the air have a marked influence upon the rate of

TABLE 1. TEMPERATURES AND HUMIDITIES APPLICABLE TO INDUSTRIAL AIR CONDITIONING

INDUSTRY	PROCESS	TEMPERATURE FAHRENHEIT DEGREES	RELATIVE HUMIDITY PER CENT
AUTOMOBILE	Assembly line	65 to 80	40 to 55
	Precision parts—honing—machining	75 to 80	40 to 55
BAKING	Cake icing	70	50
	Cake mixing	75	65
	Dough fermentation room	80	76 to 80
	Dough retarding	32 to 40	76 to 85
	Loaf cooling	70	60 to 70
	Make-up room	75 to 80	55 to 70
	Mixing room	75 to 80	55 to 70
	Paraffin paper wrapping	80	55
	Proof boxes	90 to 95	80 to 90
	Storage of flour	65 to 75	55 to 65
	Storage of yeast	32 to 45	60 to 75
BIOLOGICAL PRODUCTS	Vaccines	below 32	
	Antitoxins	38 to 42	
	Blood bank	38 to 42	60 to 65
	Penicillin (dehydrated)	36 to 40	
BREWING	Fermentation in vat room	44 to 50	50
	Storage of grains	60	30 to 45
CERAMIC	Drying of auger machine brick	180 to 200	
	Drying of refractory shapes	110 to 150	50 to 60
	Molding room	80	60
	Storage of clay	60 to 80	35 to 65
CHEMICAL	General storage	60 to 80	35 to 50
CONFECTIONERY	Chewing gum rolling	75	50
	Chewing gum wrapping	70	45
	Chocolate covering	62 to 65	50 to 55
	Hard candy making	70 to 80	30 to 50
	Packing	65	50
	Starch room	75 to 85	50
	Storage	60 to 68	50 to 65
DISTILLERY	General manufacture	60 to 75	45 to 65
	Storage of grains	60	30 to 45
DRUG	Deliquescent powder	75	35
	Effervescent granulations	80	40
	Liver extracts (powdered)	70	20 to 30
	Storage of powders and tablets	70 to 80	30 to 35
	Tablet compressing	70 to 80	40
	Packaging	80	40
ELECTRICAL	Insulation winding	104	5
	Manufacture of cotton covered wire	60 to 80	60 to 70
	Manufacture of electrical windings	60 to 80	35 to 50
	Storage of electrical goods	60 to 80	35 to 50
FOOD	Butter making	60	60
	Dairy chill room	40	60
	Preparation of cereals	60 to 70	38
	Preparation of macaroni	70 to 80	38
	Ripening of meats	40	80
	Slicing of bacon	60	45
	Storage of apples	31 to 34	75 to 85
	Storage of citrus fruit	32	80
	Storage of eggs in shell	30	80
	Storage of meats (frozen)	0 to 5	85
	Storage of meats (above freezing)	36	85
	Storage of sugar	80	35
FUR	Drying of furs	110	
	Storage of furs	28 to 40	50 to 65

TABLE 1. TEMPERATURES AND HUMIDITIES APPLICABLE TO INDUSTRIAL AIR CONDITIONING—(Concluded)

INDUSTRY	PROCESS	TEMPERATURE FAHRENHEIT DEGREES	RELATIVE HUMIDITY PER CENT
INCUBATORS	Chicken	99 to 102	55 to 75
INSTRUMENTS	Repair and calibration	68	50 to 55
LABORATORY	General analytical and physical	60 to 70	60 to 70
	Storage of materials	60 to 70	35 to 50
LEATHER	Drying of hides	90	
	Mulling	95 to 100	95
LIBRARY	Book storage	65 to 70	38 to 50
LINOLEUM	Printing	80	40
MATCHES	Manufacturing	72 to 74	50
	Storage of matches	60	
MUNITIONS	Fuse loading	70	55
PAINT	Air drying lacquers	70 to 90	25 to 50
	Baking lacquers	180 to 300	
	Air drying of oil paints	60 to 90	25 to 50
PAPER	Binding, cutting, drying, folding, gluing	60 to 80	40 to 60
	Storage of paper	75 to 80	40 to 60
	Testing Laboratory	60 to 80	55 to 65
PHOTOGRAPHIC	Development of film	70 to 75	60
	Drying	75 to 80	50
	Printing	70	70
	Cutting	72	65
PRINTING	Binding	70	45
	Folding	77	65
	Press room (general)	75	60 to 78
	Press room (lithographic)	75 to 80	50 to 60
	Storage of rollers	70 to 90	50 to 55
RUBBER	Manufacturing	90	
	Dipping of surgical rubber articles	75 to 80	25 to 30
	Standard laboratory tests	80 to 84	42 to 48
	Cementing	80	25 to 30
SOAP	Drying	110	70
TEXTILE	Cotton— carding	75 to 80	50 to 55
	combing	75 to 80	60 to 65
	roving	75 to 80	50 to 60
	spinning	60 to 80	50 to 70
	weaving	68 to 75	85
	Rayon— spinning	70	85
	throwing	70	60
	weaving	75 to 88	60 to 75
	Silk— dressing	75 to 80	60 to 65
	spinning	75 to 80	65 to 70
	throwing	75 to 80	65 to 70
	weaving	75 to 80	60 to 70
	Wool— carding	75 to 80	65 to 70
	spinning	75 to 80	55 to 60
	weaving	75 to 80	50 to 55
	Testing Laboratory	70	65
TOBACCO	Cigar and cigarette making	70 to 75	55 to 75
	Softening	90	85
	Stemming or stripping	75 to 85	70

production and upon the weight, strength, appearance and general quality of the product. The moisture content of materials having a vegetable or animal origin, and to a lesser extent minerals in certain forms, comes to equilibrium with the moisture of the surrounding air. This is the fundamental basis for the control of certain physical qualities of the material during manufacture. With increase in moisture content, hygroscopic materials ordinarily become softer and more pliable. Standards of regain are fixed in the trade.

Manufacturing economy therefore requires that the moisture content be maintained at a percentage favorable to rapid and satisfactory manipulation and to a minimum loss of material through breakage. A uniform condition is desirable in order that high speed machinery may be adjusted permanently for the desired production with a minimum loss from delays, wastage of raw material and defective product.

In the processing of hygroscopic materials, it is usually necessary to secure a final specified moisture content suitable for the goods as shipped. *Moisture content* refers to free moisture (as in a sponge) and to hygroscopic moisture (which varies with atmospheric conditions). It is usually expressed as a percentage of the total weight of material. *Regain* is more specific and refers only to hygroscopic moisture. It is expressed as a percentage of the *bone-dry* weight of material. For example, if a sample of cloth weighing 100.0 grains is dried to a bone-dry weight of 93.0 grains, the loss in weight, or 7.0 grains, represents the weight of moisture originally contained. This expressed as a percentage of the total weight (100.0 grains) gives the moisture content or 7 per cent. The regain, which is expressed as a percentage of the bone-dry weight, is $\frac{7.0}{93.0}$ or 7.5 per cent.

The use of the term *regain* does not imply that the material as a whole has been completely dried out and has re-absorbed moisture.

A basis for calculating the regain of textiles is obtained by drying, under standard conditions, a sample from the lot and the dry weight thus obtained is used in the calculations to determine the regain.

Table 2 shows the regain or hygroscopic moisture content of several organic and inorganic materials when in equilibrium at a dry-bulb temperature of 75 F and various relative humidities. The effect of relative humidity on regain of hygroscopic substances is clearly indicated. The effect of temperature is comparatively unimportant. Changes in temperature do, however, affect the rate of absorption or drying. Sudden changes in temperature cause temporary fluctuations in regain even when the relative humidity remains stationary. The rate of absorption or drying varies with the nature of the material, its thickness and density.

During the preparation processes in a cotton mill, the cotton fibers should be in a condition to be easily carded. These preliminary processes are carried out best in a relative humidity of 50 to 55 per cent. As the cotton fiber comes to the spinning operation, more flexibility is needed and the relative humidity is increased in this department. Winding, warping and weaving are all processes calling for great flexibility and a consequent need for higher humidity.

Rayons, like cotton, require different humidities and temperatures at different steps in manufacture, but on account of great loss of strength with the higher regains, should be finished in a relative humidity of 55 to 70 percent.

TABLE 2. REGAIN OF HYGROSCOPIC MATERIALS

Moisture Content Expressed in Per Cent of Dry Weight of the Substance at Various Relative Humidities—Temperature, 75 F

CLASSIFICATION	MATERIAL	DESCRIPTION	RELATIVE HUMIDITY—PER CENT									AUTHORITY
			10	20	30	40	50	60	70	80	90	
Natural Textile Fibers	Cotton	Sea island—roving	2.5	3.7	4.6	5.5	6.6	7.9	9.5	11.5	14.1	Hartshorne
	Cotton	American—cloth	2.6	3.7	4.4	5.2	5.9	6.8	8.1	10.0	14.3	Schloesing
	Cotton	Absorbent	4.8	9.0	12.5	15.7	18.5	20.8	22 8	24.3	25.8	Fuwa
	Wool	Australian merino—skein	4.7	7.0	8.9	10.8	12.8	14.9	17.2	19.9	23.4	Hartshorne
	Silk	Raw chevennes—skein	3.2	5.5	6.9	8.0	8.9	10.2	11.9	14.3	18.8	Schloesing
	Linen	Table cloth	1.9	2.9	3 6	4.3	5.1	6.1	7 0	8.4	10.2	Atkinson
	Linen	Dry spun—yarn	3.6	5.4	6.5	7.3	8.1	8.9	9.8	11.2	13.8	Sommer
	Jute	Average of several grades	3.1	5.2	6.9	8.5	10.2	12.2	14.4	17.1	20.2	Storch
	Hemp	Manila and sisal—rope	2.7	4.7	6.0	7.2	8.5	9.9	11.6	13.6	15.7	Fuwa
Rayons	Viscose Nitrocellulose Cupramonium	Average skein	4.0	5.7	6.8	7.9	9.2	10.8	12.4	14.2	16.0	Robertson
	Cellulose Acetate	Fiber	0.8	1.1	1.4	1.9	2.4	3.0	3.6	4.3	5.3	Robertson
Paper	M. F. Newsprint	Wood pulp—24% ash	2.1	3.2	4.0	4.7	5.3	6.1	7.2	8.7	10.6	U. S. B. of S.
	H. M. F. Writing	Wood pulp—3% ash	3.0	4.2	5.2	6.2	7.2	8 3	9.9	11 9	14.2	U. S. B. of S.
	White Bond	Rag—1% ash	2 4	3.7	4.7	5.5	6.5	7.5	8.8	10.8	13.2	U. S. B. of S.
	Com. Ledger	75% rag—1% ash	3.2	4.2	5.0	5.6	6.2	6.9	8.1	10.3	13.9	U. S. B. of S.
	Kraft Wrapping	Coniferous	3.2	4.6	5.7	6.6	7.6	8.9	10.5	12.6	14.9	U. S. B. of S.
Misc. Organic Materials	Leather	Sole oak—tanned	5.0	8.5	11.2	13.6	16.0	18.3	20 6	24.0	29.2	Phelps
	Catgut	Racquet strings	4.6	7 2	8.6	10.2	12.0	14.3	17.3	19.8	21.7	Fuwa
	Glue	Hide	3.4	4.8	5.8	6.6	7 6	9 0	10.7	11.8	12.5	Fuwa
	Rubber	Solid tires	0.11	0.21	0.32	0.44	0.54	0.66	0.76	0.88	0.99	Fuwa
	Wood	Timber (average)	3 0	4.4	5.9	7.6	9.3	11.3	14 0	17.5	22.0	Forest P. Lab.
	Soap	White	1.9	3.8	5.7	7.6	10.0	12.9	16.1	19.8	23.8	Fuwa
	Tobacco	Cigarette	5.4	8.6	11.0	13.3	16.0	19 5	25.0	33.5	50 0	Ford
Foodstuffs	White Bread		0.5	1.7	3.1	4.5	6.2	8.5	11.1	14.5	19.0	Atkinson
	Crackers		2.1	2.8	3.3	3.9	5.0	6.5	8.3	10.9	14.9	Atkinson
	Macaroni		5.1	7.4	8.8	10.2	11 7	13.7	16.2	19.0	22.1	Atkinson
	Flour		2.6	4.1	5.3	6.5	8.0	9.9	12.4	15.4	19.1	Bailey
	Starch		2.2	3.8	5.2	6.4	7.4	8.3	9.2	10.6	12.7	Atkinson
	Gelatin		0.7	1 6	2.8	3.8	4.9	6.1	7.6	9.3	11.4	Atkinson
Misc. Inorganic Materials	Asbestos Fiber	Finely divided	0.16	0.24	0.26	0.32	0.41	0.51	0.62	0.73	0.84	Fuwa
	Silica Gel		5.7	9.8	12.7	15.2	17.2	18.8	20.2	21.5	22.6	Fuwa
	Domestic Coke		0.20	0.40	0.61	0.81	1.03	1.24	1.46	1.67	1.89	Selvig
	Activated Charcoal	Steam activated	7.1	14.3	22.8	26.2	28.3	29.2	30.0	31.1	32.7	Fuwa
	Sulfuric Acid	H_2SO_4	33.0	41.0	47.5	52.5	57.0	61.5	67.0	73.5	82.5	Mason

Other textile fibers, due to their different natural characteristics, are processed under relative humidities and temperatures applicable to each.

When hygroscopic materials absorb moisture from the surrounding air they deliver to the air sensible heat equivalent to the latent heat released by the moisture to the material. This may account for a small part of the total heat load of the conditioned space.

Conditioning and Drying

In general, the exposure of materials to desirable humidities for treatment may be coincidental with the manufacture or processing of the materials, or they may be treated separately in special enclosures. This latter treatment may be classified as conditioning or drying. The purpose of conditioning or drying is usually to establish a desired condition of moisture content and to regulate the physical properties of the material. When the final moisture content is lower than the initial one, the term *drying* is applied (See Chapter 47). If the final moisture content is to be higher, the process is termed *conditioning*. In the case of some textile products and tobacco, for example, drying and conditioning may be combined in one process for the dual purpose of removing undesirable moisture and accurately regulating the final moisture content. Frequently conditioning or drying is made a continuous process in which the material is conveyed through an elongated compartment by suitable means and subjected to controlled atmospheric conditions.

Control of Rate of Chemical Reactions

A typical example of control of the rate of chemical reactions occurs in the manufacture of rayon. The pulp sheets are conditioned, cut to size, and passed through a mercerizing process. It is essential that during this process close control of both temperature and relative humidity should be maintained. The temperature controls the rate of reaction directly, while the relative humidity maintains a constant rate of evaporation from the surface of the solution and obtains a solution of known strength throughout the mercerizing period.

Another well-known example in this class is the *drying* of varnish which is an oxidizing process dependent upon temperature. High relative humidities have a retarding effect on the rate of oxidization at the surface and allow the internal gases to escape freely as the chemical oxidizers *cure* the varnish from within. This produces a surface free from bubbles and a film homogeneous throughout. Desirable temperatures for *drying* varnish vary with the quality. A relative humidity of 65 per cent is beneficial for obtaining the best processing results.

Control of Rate of Biochemical Reactions

In the field of biochemical control, industrial air conditioning has been applied to many different and well-known products. All problems involving fermentation are classed under this heading. As biochemistry is a subdivision of chemistry, subject to the same laws, the rate of reaction may be controlled by temperature. An example of this is the dough room of the modern bakery. Yeast develops best at a temperature of 80 F. A relative humidity of 65 per cent is maintained to hold the surface of the dough open to allow the carbon dioxide gases formed by the fermentation to pass through and produce a loaf of bread, when baked, of even, fine texture without large voids.

The curing of fruits, such as bananas and lemons, also comes under this classification. Bananas require a cycle of temperatures and relative humidities for ripening. The starches in the pulp of the fruit must be changed and the skin cured and colored, after which the fruit is cooled to maintain as low a rate of metabolism as possible. Ideal storage conditions range between 56 and 60 F with about 75 per cent relative humidity and ventilation at the rate of three or four air changes per hour.

The curing of lemons is an entirely different problem. Bananas are cured for a quick market, while lemons are held for a future market. The process, therefore, varies in the temperature used. Temperatures from 54 to 59 F have been found to be best suited for this process. A high relative humidity of 88 to 90 per cent is necessary to hold shrinkage to a minimum and, at the same time, develop the rind so it will be sufficiently tough to permit handling.

Tobacco from the field to the finished cigar, cigarette, plug or pipe tobacco, offers another interesting example of what may be done by industrial air conditioning in the control of color, texture and flavor. In the processing of tobacco, control of regain, of chemical and biochemical reactions is involved, and only through close atmospheric control can the best quality of leaf be developed.

Control of Rate of Crystallization

The rate of cooling of a saturated solution determines the size of the crystals formed. Both dry- and wet-bulb temperatures are of importance, as the one controls the rate of cooling, while the other, through evaporation, changes the density of the solution.

In the coating pans for pills, gum and nuts, a heavy sugar solution is added to the tumbling mass. As the water evaporates, each separate piece is covered with crystals of sugar. A smooth, opaque coating is only accomplished by blowing into the kettle the proper amount of air at the right dry- and wet-bulb temperatures. The wet-bulb depression determines the rate of moisture pick-up or drying by the air and may be termed the *drying head*. Of equal importance is the uniformity at which the wet-bulb is maintained. If this is allowed to vary, poor results will follow due to checking and cracking of the unfinished coating.

Elimination of Static Electricity

The presence of static electricity is very detrimental to the staisfactory and economical processing of many light materials, such as textile fibers, paper, etc. It is also extremely dangerous where explosive atmospheres or materials are present. Fortunately, this hazard is minimized by increasing the relative humidity if the material being processed is not damaged thereby.

In attempting to eliminate static electricity, it must be borne in mind that for successful elimination the air that actually comes in contact with the material in the machine must be at a relative humidity of 50 per cent or more. As some machines consume a great deal of power which is converted directly into heat, the temperature in the machine may be considerably higher than the temperature adjacent to the machine where the relative humidity is normally measured. In such cases, the relative humidity in the machine will be appreciably lower than that elsewhere in the room, and it may be necessary to maintain a room relative humidity of 65 per cent, or even more, before the desired results can be obtained inside the equipment.

CALCULATIONS

The methods for determining the heating and cooling loads for the various industrial processes are similar to those outlined in Chapters 14 and 15. The several other chapters previously cited call attention to additional phases of calculation which may be needed. Because of the

large number of motors and heat producing units usual in an industrial application, it is particularly important that operating allowances for the latent and sensible heat loads be definitely ascertained and used in the calculations to determine the total design load.

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Chapter 46

EXHAUSTING AND CONVEYING SYSTEMS

Classification of Systems, Hood Design Principles, Hood Suction and Indraft Velocities, Duct System Design, Air Cleaning Equipment, Resistance of Systems, Air Flow Producing Equipment, Protection Against Corrosion

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IN many industrial plants some type of exhaust system designed to collect and remove dusts, fumes, mists, vapors and gases is essential in order to promote efficiency, economy, and safety of operation. Definitions of these various contaminants are included in Chapter 10, Air Contaminants.

The theory of air flow in an exhaust system in the following paragraphs *A* to *D* will be found in a publication [1] of the *American Foundrymen's Association.*

A. When the air flow producing equipment of an exhaust system is properly operated it will produce a negative pressure (below atmospheric) in the exhaust side of the system sufficient to overcome all resistance and to sustain the desired air velocity; and, further, will overcome all resistances on the discharge or positive pressure side of the system so that the air drawn through exhaust inlets will be discharged against atmospheric pressure.

B. An exhaust system is entirely dependent on a *sufficient volume* of air flowing into the exhaust inlets to catch the matter to be exhausted before such matter has an opportunity to diffuse into the general atmosphere of the work place or room.

C. The velocity of the air flowing into an exhaust inlet is usually of secondary importance and becomes an essential factor only when a certain velocity is required to overcome some force acting on the matter to be caught. The velocity within an exhaust system is only important to the extent that it shall be sufficient to convey the entrained matter and prevent it from settling or dropping out in the piping system. Velocity in terms of velocity pressure is most essential in designing a system because it is the basis upon which all calculations are made. In testing and checking a system the velocity as determined from the velocity pressure reading obtained by means of a Pitot tube is the only true indication of the exact air flow in a pipe or system.

D. The total pressure within an exhaust system is only of importance in determining the power required to operate the system. Total pressure tests do not indicate the proper functioning of an exhaust system as related to the volume and velocity of the air flowing into an exhaust inlet.

General design information is included in this chapter which is intended to relate primarily to industrial exhaust systems.

CLASSIFICATION OF SYSTEMS

In general there are two basic layouts of exhaust systems, the central and the multiple unit system. In the central system a fan is located near the center of operations with a piping system radiating to the various machines to be served. In the multiple unit system, which is sometimes employed where the machines to be served are widely scattered, or where the operations are apt to be independent or intermittent, small individual exhaust fans are located at the center of the machine groups or at each machine. The unit arrangement has the advantage of flexibility.

Exhaust systems may be classified with respect to the nature of the material to be handled by them as (*a*) those handling dust and (*b*) those handling fumes, mists, vapors and gases. There is a marked difference in design details of systems serving dust producing operations and those exhausting the more vapor-like matter even though the same basic

theories govern both classes. The type of hood and exhauster, the adaption of general ventilation, the conveying velocities and duct construction differ substantially.

Exhaust systems are also classified by the means employed to collect the material. The dust or refuse may be collected and controlled by enclosed hoods or open hoods with positive inward air movement or by diluting or exhausting the general air of the room. With some classes of machinery it is not feasible to hood the machines closely and in these cases open hoods over or adjacent to the machines are provided to collect as much as possible of the dust and fumes. This class includes such machines as rubber mills, package filling machinery, sand blast, crushers, forges, pickling tanks, melting furnaces, and the unloading points of various types of conveyors.

Open hoods should be placed as close to the source of dust or fumes as possible, with due regard to the movements of the operator, and should be placed so that the operator is in no case in the path of the exhausted material. When the hood must be placed at some distance above the machine it should be large enough to cover a large area as diffusion is usually quite rapid.

Some consideration should be given to the natural movement of the fumes. For those that are lighter than air, the hood may be over or above the machine; and where a heavy vapor, or dust-laden air at ordinary temperature is to be removed, horizontal or floor connections are sometimes preferable. In many cases there are convection currents and other atmospheric disturbances in the work room which should be given consideration. These disturbances diminish the tendency of dust and fumes to settle from the room air because of their density.

In another class of operation the main objective is to prevent the escape of dust into the surrounding atmosphere, and the removal of some dust from the machine or enclosure may be merely incidental. The dust-creating apparatus is enclosed within a housing which is made as tight as practicable, and sufficient suction is applied to the enclosure to maintain an inward air leakage, thus preventing escape of the dust. While the exhaust system is required to handle only the air which leaks in through the crevices and openings in the enclosure, yet in many installations leakages are very high and great care is required to obtain satisfactory results with a system of this kind. The inward-leakage principle is utilized for controlling dust in the operating of tumbling barrels, grinding, screening, elevating, and similar processes.

Certain dust and fume producing operations are best carried on by isolating the process in a separate compartment or room and then applying general ventilation to this space. The compartment or room in which the work is performed should be as small as is consistent with convenience in handling the work. The ventilating system should be designed so that a current of clean air is drawn across the work in such a manner as to carry the dust or fume away from the operator and out of the work space. Another method of accomplishing the control of this type of installation, and one usually applied in the case of gases and fumes, is the dilution method. In this case sufficient clean air is introduced generally into the work space to dilute the contamination to a safe level.

HOOD DESIGN PRINCIPLES [2, 3]

The first step in the design of an exhaust system is to determine the number and size of the hoods and their connections. No general rules,

however, can be given since hood and duct dimensions are determined by the characteristics of the operations to which they are applied. When a tentative decision regarding the set-up has been made, it is then necessary to obtain the suction and air velocities required to effect control. At this point the designer must rely upon the prevailing practice and on such physical data relating to hoods, duct systems and collectors as are available. The fan speed must be sufficient to maintain the estimated suction and air velocities in the system. In general, the most important requirements[4] of an efficient exhaust and collecting system are:

1. Hoods, ducts, fans, motors and collectors should be of adequate size and type.
2. The air velocities should be sufficient to control and convey the materials collected.
3. The hoods and ducts should be placed so as not to interfere with the operation of a machine or any working part.
4. The system should do the required work with a minimum power consumption.
5. When inflammable dusts and fumes are conveyed, the piping should be provided with an automatic damper in passing through a fire-wall.
6. Ducts and all metal parts should be grounded to reduce the danger of dust explosions by static electricity.
7. The exhaust system should be readily accessible for inspection and care.

HOOD SUCTION AND INDRAFT VELOCITIES

The removal of dust or waste by means of an exhaust hood requires a movement of air at the point of origin sufficient to carry it into a collecting system. The air velocities necessary to accomplish this depend upon the physical properties of the material to be eliminated and the direction and speed with which it is thrown off. If the dust to be removed is already in motion, as is the case with high-speed grinding wheels, the hood must be installed in the path of the particles so that a minimum air volume may be used effectively. It is always desirable to design and locate a hood so that the volume of air necessary to produce results is as small as possible. This will reduce the size of equipment, the power required by the system, and also the heating load requirements in winter.

Air Flow from Static Readings

The static suction at the throat of a hood is frequently used in practice as a measure of the effectiveness of control. Where the hood coefficient is known the volume of air flow through any hood may be determined from the equation:

$$Q = 4005 f A \sqrt{h_t} \qquad (1)$$

where

Q = volume of air flow, cubic feet per minute.
A = area of connecting duct, square feet.
h_t = static suction measured 3 diameters from throat of hood, inches of water.
= orifice or restriction coefficient which varies from 0.6 to 0.9 depending on the shape of the hood.

An average value of f is 0.71, although for a well-shaped opening a value of 0.8 may be used. The factor f is determined from the equation:

$$f = \sqrt{\frac{h_v}{h_t}} \qquad (2)$$

where h_v is the velocity head in the connecting duct.

The *static suction* is not a good measure of the effectiveness of a hood unless the area of the opening and the location of the operation with

respect to the hood are known. This is clearly indicated by Equation 3 which shows that the velocity at any point along the axis varies approximately inversely as the square of the distance. This formula coupled with Equation 1 should serve to indicate the velocity conditions to be expected when operations are conducted externally to the hood opening.

Design Based on Total Air Flow

Where the foregoing factors are not known, the usual method of designing an exhaust system is to base the air flow through the system on rates of flow through each hood which have been found by experience to provide adequate control. For woodworking systems the rates of flow given in Table 1, calculated on the basis of a branch velocity of 4000 fpm, are adequate for control. Using these air flow rates, Table 2 gives the size of pipe connections to be used with the more common woodworking machines. Properly designed grinding and buffing wheel hoods have been found to be adequately controlled when the rates of air flow given in Table 3, calculated on the basis of a branch velocity of 4500 fpm, are used. Table 4 gives the minimum branch pipe sizes to be used on the more common sizes of grinding and buffing wheels.

In some states grinding, polishing and buffing wheels are subject to regulation by codes. The static suction requirements, which range from 1½ to 5 in. water displacement in a *U*-tube, must be followed in such states although in several instances they appear to be excessive. Frequently, in these operations, a large part of the wheel must be exposed and the dust-laden air within the hood is thrown outward by the centrifugal action of the wheel, thus counteracting useful inward draft. This tendency may be diminished by locating the connecting duct so as to create an air flow of not less than 200 fpm past the lower edge of the wheel.

Controlling Air Velocities

Exact determinations of hood control velocities are not available, but it is safe to assume that for most dusty operations velocities should not be less than 200 fpm at the point of origin. Recommended air velocities through hood openings for various processes are given in Table 5. For granite dust generated by pneumatic devices, velocities from 150 to 200 fpm, depending on the type of hood used, are recommended as sufficient for safe control [5]. Considering the character of the industry, air velocities of this order may be extended to similar dusty operations. The method for approximately determining these velocities in terms of the velocity at the hood opening is given in Equation 3.

No set rule can be given regarding the shape of a hood for a particular operation, but it is well to remember that its essential function is to create an adequate velocity distribution. The fact that the zone of greatest effectiveness does not extend laterally from the edges of the opening may frequently be utilized in estimating the size of hood required. Where complete enclosure of a dusty operation is contemplated, it is desirable to leave enough free space to equal the area of the connecting duct. Hoods for grinding, polishing and buffing should fit closely, but at the same time should provide an easy means for changing the wheels. It is advisable to design these hoods with a removable hopper at the base to capture the heavy dust and articles dropped by the operator. Such provisions are of assistance in keeping the ducts clear. Air volumes used to control many dust discharges may often be reduced by effective baffling or partial

TABLE 1. RATES OF FLOW THROUGH BRANCH PIPES OF WOODWORKING MACHINES

PIPE DIAMETER, IN.	AIR VOLUME, CFM	PIPE DIAMETER, IN.	AIR VOLUME, CFM
3	200	6	800
4	350	7	1100
5	550	8	1400

TABLE 2. BRANCH PIPE SIZE FOR WOODWORKING MACHINE HOODS

TYPE OF MACHINE	SIZE, IN.		NO. OF BRANCHES	MINIMUM DIAMETER, IN.		
	Min.	Max.		BOTTOM BRANCH	TOP BRANCH	OTHERS
Self feed table saw			2	5	4	
Other single saws	18	18	1 1		4 5	
Saws with Dado Head			1		5	
Band saws	2 3	2 3 6	2 2 2	4 5 5	4 4 5	
Disc sanders	18 26 32 38	18 28 32 38 48	1 1 2 2 3	4 5 4 5 5	 4 4 4	 4
Triple drum sanders	30 36 42	30 36 42 48	1 1 1 1	7 8 9 10		
Single drum sanders: (area in sq in.)	350 700 1400	350 700 1400 2800	1	4[a] 5 6 7		
Horizontal belt sanders	9	9 14	2 2	5 6	4 4	
Vertical belt sanders	6 9	6 9 14	1 1 1	4 5 6		
Jointers	8	8 20	1 1	4 5		
Single planers	20 26	20 26 36	1 1 1	5 6 7		
Tenoner			2	5	5	

[a]Not over 10 in. diameter.

TABLE 3. RATES OF FLOW THROUGH BRANCH PIPES, GRINDING AND BUFFING WHEELS

PIPE DIAMETER, IN.	AIR VOLUME, CFM	PIPE DIAMETER, IN.	AIR VOLUME, CFM
3	225	6	900
4	400	7	1200
5	600		

TABLE 4. BRANCH PIPE SIZES FOR GRINDING AND BUFFING HOODS

TYPE OF WHEEL	WHEEL SIZE DIAMETER, IN.		MAXIMUM		BRANCH PIPE MINIMUM DIAMETER, IN.
	Min.	Max.	Width In.	Area Sq In.	
Grinding	....	9	1	30	3
	9	18	3	175	4
	18	24	4	300	5
	24	30	5	500	6
	30	36	6	700	7
Disc Grinding	....	20	....	300	4
	20	30	....	....	5
Buffing, Polishing and Scratch Brushing	....	8	2	50	3½
	8	16	3	150	4
	16	24	4	300	5
	24	30	6	600	6

enclosure of an operation. This procedure is strongly urged where dusts are directed beyond the zone of influence of the hood.

Axial Velocity Formula for Hoods

When the normal flow of air into a hood is unobstructed, Equation 3 may be used to determine the air velocity at any point along the axis[6]:

$$V = \frac{0.1\,Q}{x^2 + 0.1\,A} \tag{3}$$

where V = velocity at point, feet per minute.
Q = volume of air handled, cubic feet per minute.
x = distance along axis, feet.
A = area of opening, square feet.

Velocity Contours

It is possible by use of a specially constructed Pitot tube[7] to map contours of equal velocity in any axial plane located in the field of influence. It has been found that the positions of these contours for any hood can be expressed as percentages of the velocity at the hood opening and are purely functions of the shape of the hood[8].

TABLE 5. RECOMMENDED AIR VELOCITIES THROUGH OPENINGS IN HOODS ENCLOSING OPERATIONS OR LOCATED OVER ZONES OF GENERATION OF DUSTS, FUMES, VAPORS AND GASES RELEASED IN CERTAIN MANUFACTURING PROCESSES

CONDITION OF GENERATION OF CONTAMINANT	MINIMUM AIR VELOCITY, FPM	PROCESS
Released without noticeable movement	50–100	Evaporation of vapors, exhaust from pickling, washing, degreasing, plating, welding, etc.
Released with low velocity	100–200	Paint spraying in booth; inspection, sorting, weighing, packaging, low speed conveyor transfer points, rotating mixtures, barrel filling.
Active generation	200–500	Foundry shakeout, high speed conveyor transfer points, crushers, screens.
Released with great force	500–2000	Grinding, tumbling mills, abrasive cleaning.

Further, the velocity contours are identical for similar hood shapes when the hoods are reduced to the same basis of comparison. These facts are applicable to all hood problems so that when the velocity contour distribution is known, the air flow required can be determined. Fig. 1 shows the contour distribution in two axial planes perpendicular to the sides of a rectangular hood with a side ratio of one-half. The distribution shown is identical for all openings with a similar side ratio provided the mapping is as shown in the figure. The contours, of course, are expressed as percentages of the velocity at the opening.

Low Velocity Systems

On multiple installations of the same operation it is often possible to institute a great saving in power cost by designing an exhaust system

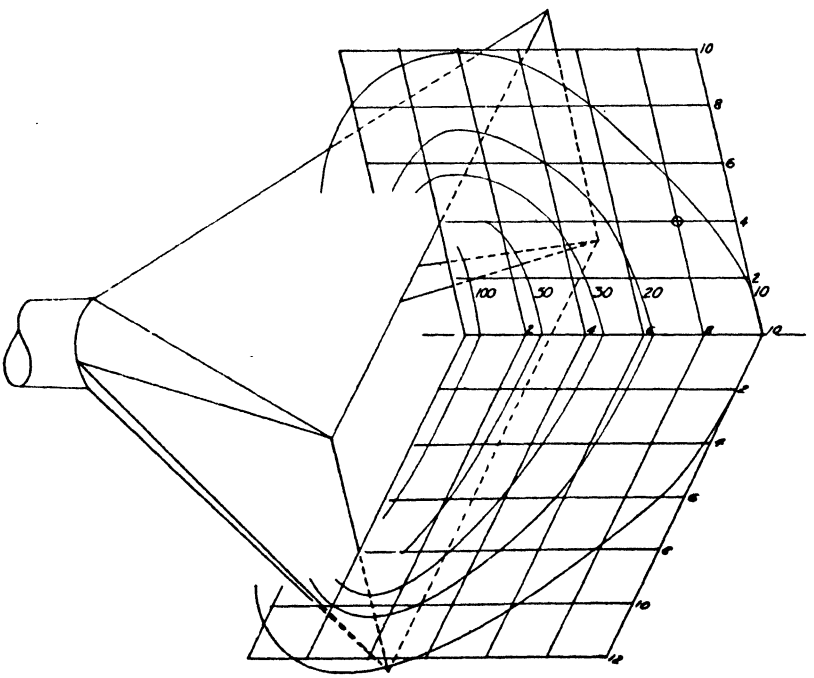

FIG. 1. VELOCITY CONTOURS FOR A RECTANGULAR OPENING WITH A SIDE RATIO OF ONE-HALF. CONTOURS ARE EXPRESSED AS PERCENTAGES OF THE VELOCITY AT THE OPENING

using low velocities in the main ducts. Such a system for use in grinding and shaping porcelain has been described[9]. In these operations, the separate machines are grouped around a central plenum chamber and exhausted by means of a low pressure fan connected to the plenum. In this case a power saving of over 90 per cent was obtained. A similar design technique[10] has been described for use in ventilating plating tanks.

Large Open Hoods

Large hoods, such as may be used for electroplating and pickling tanks, should be sub-divided so the area of the connecting duct is not less than one-fifteenth of the open area of the hood. Frequently, it will be found necessary to branch the main duct in order to obtain a uniform distri-

bution of flow. *Canopy hoods* should extend 6 in. laterally from the tank for every 12 in. elevation, and wherever possible they should have side and rear aprons so as to prevent short circuiting of air from spaces not directly over the vats or tanks. In most cases, hoods of this type take advantage of the natural tendency of the vapors to rise, and air velocities may be kept low. Cross drafts from open doors or windows disturb the rise of the vapors and therefore provision must be made for them. The air velocities required also depend upon the character of the vapors given off, cyanide fumes, for example, requiring an air velocity of approximately 75 fpm on the surface of the tank and acid and steam vapors requiring velocities as low as 25 to 50 fpm. The total volume of air flow necessary to obtain these velocities may be approximately determined from the equation:

$$Q = 1.4\,PDV \tag{4}$$

where

Q = total volume of air handled by hood, cubic feet per minute.
P = perimeter of the tank, feet.
D = distance between tank and hood opening, feet.
V = air velocity desired along edges and surface of tank, feet per minute.

Lateral Exhaust Systems

The lateral exhaust method, as developed for chromium plating [11], is applicable in many instances in preference to the canopy type hoods. The method makes use of drawing air and fumes laterally across the top of vats or tanks into slotted ducts at the top and extending fully along one or more sides of the tanks. The slots are 1 in. wide and for effective ventilation a 2000 fpm exhaust air velocity at the slot face is advisable. In addition, the duct should not be required to draw the air laterally for a distance of more than 18 in. and the level of the solution should be kept 6 to 8 in. below the top of the tanks. If width of tank is over 18 in. a double lateral exhaust may be used with slots on both sides.

It has also been determined that a similar control may be used for tanks wider than 3 ft when the same velocity (2000 fpm) is maintained through a slot which is increased ¼ in. for every foot of width greater than 3 ft. When these slots must be extended more than 6 ft in length, some method of spreading the flow is necessary to provide even air flow distribution through the entire slot length. This can be accomplished by tapering the slot, which incidentally will add to the resistance of the system. A more economical approach is to place properly spaced vanes in the side ducts, or to branch the side ducts [12].

The flexible exhaust tube method may be advantageously used for removing dust or fumes. Flexible tubes having one end connected to an exhaust system and a slotted hood attached to the other end may be shaped at will to fit in with industrial processes without affecting the ease of operation. Efficient dust or fume removal may be had with use of relatively small exhaust volumes. This type of system may be used on swing grinders, portable grinding wheels, soldering operations, stone cutting, rock drilling, etc.

Spray Booths

In the design of an efficient spray booth, it is essential to maintain an even distribution of air flow through the opening and about the object being sprayed. While in many instances spraying operations can be

performed mechanically in wholly enclosed booths, the volatile vapors may reach injurious or explosive concentrations. At all times the concentrations of these vapors, and particularly those containing benzol, should be kept well below 100 parts per million in the breathing zone of the worker. Spray booth vapors are dangerous to the health of the worker and care should be taken to minimize exposure to them.

It is recommended in the design of spray booths that the exhaust duct be located at the end of the booth opposite the opening. In front of this duct should be placed baffle plates which will cause a uniform air velocity distribution across the frontal area. The air volume should be sufficient to maintain a velocity of not less than 100 fpm over the open area of the booth (150 fpm is preferable where benzol or lead is present in the paint) and the vapors should be discharged through a suitable stack to permit dilution. It is good practice to pass the fumes or vapors through baffle type washers or scrubbers designed for efficient spray removal.

Hoods for Chemical Laboratories

Hoods used in chemical laboratories are generally provided with sliding windows which permit positive control of the fumes and vapors evolved by the apparatus. Their design should offer easy access for the installation of chemical equipment and should be well lighted. Air velocities should exceed 50 fpm when the window is fully open.

Kitchen Hoods

The length and width of kitchen hoods should be such as to extend beyond the extreme projection of the ranges, broilers, etc., over which they are installed. The minimum projection or overlap should be 12 in. Where space conditions permit, range hoods should be about 2 ft high so as to provide a reservoir to confine momentary bursts of smoke and steam until the exhaust system can evacuate the hood. Range hoods should be located as low as possible to increase their effectiveness.

A steel plate placed horizontally within a kitchen hood and located sufficiently high above the level of the bottom of the hood to permit use of a row of lights within the hood along the edge has been found effective in improving the operation. The area between the edges of the plate and the edges of the hood should be selected according to the exhaust volume and velocity required.

In general the amount of air to be exhausted from restaurant range hoods is at the rate of 100 fpm per square foot of face area. Thus, a hood 4.5 ft wide by 30 ft long has a face area of 135 sq ft, which multiplied by 100 fpm velocity results in a total air quantity to be exhausted of 13,500 cfm. In some cases, where the application is principally frying and where it is not practical to install a hood 2 ft high, it is recommended that the face velocity be increased from 100 to 150 fpm, depending on peak load conditions in the kitchen. Exhaust connections to range hoods should always be made at the top and back of hoods, and should be spaced preferably not more than 6 ft apart and be rectangular in shape with the long side parallel to the back of the hood. Exhaust openings into range hoods should be designed to maintain a velocity of 1500 to 1800 fpm.

An approved fire damper with fusible link should be (and is required by code in many states) installed in the main exhaust duct or branch adjacent to the range hood. Should there be more than one hood connected to a common duct, then the branch duct to each hood should be provided with a fire damper. Access doors should be provided at the fire

damper for purpose of inspection, cleaning, or for renewal of fusible link. All exhaust piping to range hoods, commonly called grease ducts, should be provided with tight fitting cleanout doors of adequate size to permit easy removal of grease. Some engineers use filters to advantage in hoods which are subject to grease conditions.

Hoods over steam tables should be of similar construction to range hoods. It is good practice to design such hoods with a face velocity of 60 to 70 fpm. Hoods over dishwashing machines are usually relatively small and generally 1500 to 2000 cfm per hood is allowed, which is equivalent to a velocity of approximately 100 fpm per square foot of face area. Range hoods in diet kitchens are constructed the same as restaurant range hoods but with less exhaust air per square foot of face area, depending upon the nature of the food cooked.

Hoods are not often used in private residences unless they are quite large and the consideration of expense is not important. For such residences the hoods should be designed on the same basis as diet kitchens. Most all residence kitchens can be effectively and economically ventilated by the installation of a built-in kitchen ventilator, which should be located in an outside wall and in close proximity to the kitchen range. It has been found that the capacity of the built-in kitchen ventilator should be at least 350 cfm regardless of the size of kitchen. This can be justified on the basis that the smaller the kitchen the more concentrated the heat will be thus requiring a more rapid rate of air change. Standard size built-in kitchen ventilators are generally available in three sizes, namely 350, 500 and 800 cfm. The proper size to use will depend on design conditions and available wall space.

DUCT SYSTEM DESIGN

In designing a duct system it is necessary to recognize a few fundamental principles (see also Chapter 41). Knowing the quantity of air required, the size of the duct may be computed from Equation 5:

$$A = \frac{Q}{V} \tag{5}$$

where

A = cross-section area of duct, square feet.
Q = air quantity to be handled by the duct, cubic feet per minute.
V = velocity of air, feet per minute.

Air Velocities in Ducts

Where it is necessary to transport the particulate material collected in an exhaust system, minimum carrying velocities must be maintained in the ducts preceding the collector. It has been found that good results are obtained when design air velocities in horizontal runs are not less than 2000 fpm or not greater than 5000 fpm. When the dust being carried is organic and other than wood flour, or similar material, a velocity of 2500 fpm is adequate. Approximate required conveying velocities are given in Table 6.

For duct systems wherein the air has no dust or solid load, a lower velocity is desirable, which may range from 1200 to 2000 fpm. In view of the fact that the horsepower required by a system depends directly on the resistance and the resistance is a function of the velocity, economical design requires velocities of this magnitude.

The equal friction method is generally used for designing a duct system as this insures equal resistance to air flow in all branches throughout the system (see Chapter 41). Long main ducts do not generally provide the most economical layout. Where it is necessary to ventilate a large number of machines, or machines which are widely separated, it is desirable to locate the fan at approximately the center of the system. With this arrangement it is possible to choose a fan which will deliver the required air quantity against a lower resistance pressure, and this will generally result in a horsepower saving.

When a system carrying dust is designed with an oversize main duct to allow for future extension, the air velocity may be found to be too low to carry the dust, and serious plugging may occur. In this case it is desirable to install an orifice in the end of the pipe to allow for the lower air quantity.

Construction

The interior of all ducts should be smooth and free from obstructions at joints and soldered air-tight. Other sealing mediums are permissible where soldering is impracticable.

Ducts should be constructed of galvanized sheet metal except when the presence of corrosive fumes or gases, temperatures above 400 F, or other factors would make galvanized material impractical. For the usual exhaust systems the metal thicknesses shown on Table 7 are recommended. Elbows and angles should be a minimum of two gages heavier than straight lengths of equal diameter. Hoods should be a minimum of two gages heavier than straight sections of a connecting branch.

Longitudinal joints of ducts should be lapped and riveted or spot-welded on 3-in. centers maximum. Girth joints or ducts should be made with lap in direction of air flow, with 1 in. lap for duct diameters through 19 in. and 1¼ in. lap for diameters over 19 in. Elbows and angles should have an inside or throat radius of two pipe diameters whenever possible. Large radii are recommended for heavy concentrations of highly abrasive dusts. Elbows 6 in. or less in diameter should be constructed of at least 5 sections and, if over 6 in. in diameter, of 7 sections, with angles pieced proportionally. Hoods should be free of sharp edges or burrs and reinforced to provide necessary stiffness. Transitions in mains and submains should be tapered with a taper 5 in. long for each 1 in. change in diameter whenever possible. All branches should enter the main at the large end of the transition at an angle not to exceed 45 deg or preferably 30 deg. Branches should be connected only to the top or sides of mains, with no two branches entering diametrically opposite to each other. Dead end caps should be provided within 6 in. from last branch of all mains and sub-mains. Cleanouts should be provided every 10 ft and near each elbow, angle, or duct junction in horizontal sections. Ducts should be supported sufficiently to place no loads on connected equipment and to carry weight of a system plugged with material. The

TABLE 6. APPROXIMATE CONVEYING VELOCITIES

MATERIAL CONVEYED	DESIGN VELOCITY FPM
Vapors, gases, fumes, very fine dust	2,000
Fine dry dusts	3,000
Average industrial dusts	3,500
Coarse particles	3,500–4,500
Large particles, heavy loads, moist materials	4,500 and over

maximum distance between supports should be 12 ft for 8 in. or smaller ducts and 20 ft for larger ducts. Six inches minimum clearance should be provided between ducts and the ceiling, wall or floor. Blast gates for adjustment of the system should be placed near the connection of a branch to the main and means of locking gates after the adjustments have been made should be included. Rectangular ducts should be used only when clearances prevent the use of round construction. Rectangular ducts should be as nearly square as possible. The weight of metal and the lap, and other construction details, should be the equal of round duct construction having a diameter equal to the longest side. All pipes passing through roofs should be equipped with collars so arranged as to prevent water from leaking into the building.

The main trunks and branch pipes should be as short and straight as possible.

Cleanout openings having suitable covers should be placed in the main and branch pipes so that every part of the system can be easily reached in case the system clogs. Either a large cleanout door should be placed in the main suction pipe near the fan inlet, or a detachable section of pipe, held in place by lug bands, may be provided.

Every pipe should be kept open and unobstructed throughout its entire length, and no fixed screen should be placed in it, although the use of a trap at the junction of the hood and branch pipe is permissible, provided it is not allowed to fill up completely. The passing of pipes through fire-walls should be avoided wherever possible, and floor sweep connections should be so arranged that foreign material cannot be easily introduced into them.

At the point of entrance of a branch pipe with the main duct, there should be an increase in the latter equal to their sum. Some state codes specify that the combined area be increased by 25 per cent. While this is not always good practice and is frequently done at the expense of a reduced air velocity, it is often done where future expansion of the exhaust system is contemplated.

Duct Resistance

The resistance to flow in round galvanized duct riveted and soldered at the joints may be obtained from Fig. 2, Chapter 41. The pressure drop through elbows depends upon the radius of the bend. For elbows whose centerline radii vary from 100 to 300 per cent of pipe diameter, the loss may be estimated from Table 8. It is sometimes convenient to express the resistance of an elbow in terms of an equivalent length of duct of the same diameter. Thus with a center line radius equal to the pipe diameter the resistance is equivalent to a section of straight pipe approximately

TABLE 7. GAGES OF METALS FOR EXHAUST SYSTEMS[a]

DIAMETER OF ROUND PIPE OR GREATEST DIMENSION OF RECTANGULAR PIPE, INCHES	THICKNESS OF DUCT MATERIAL U. S. GAGE NUMBER	
	For Highly Abrasive Matter	For Other Matter
Up to 8 inclusive	20	22
Over 8 to 18 inclusive	18	20
Over 18 to 30 inclusive	16	18
Over 30	14	16

[a]Fundamentals of Design, Construction, Operation and Maintenance of Exhaust Systems (*American Foundrymen's Association*, p. 53).

10 diameters long, while with a center line radius 1½ times the diameter, the resistance is apparently the same as that of seven diameters of straight pipe.

AIR CLEANING EQUIPMENT

Primary dust separators depend for their air cleaning action on centrifuging out the dust particles or on imparting to the transporting air stream a quick change in direction, accompanied by a sudden reduction in velocity. They may be applied to exhaust systems from polishing and buffing wheels and, in some cases, as a preliminary separator ahead of a final dust arrester.

Dust particles which cannot be caught in inertia type separators are usually removed by one of the following methods:

1. *Filtration.* Of the filter arresters the cloth type, either of the screen, envelope, or bag construction, is most generally used for industrial exhaust systems. Cloth arresters properly engineered for this job and handling dust for which they are suited operate at a good efficiency.

2. *Wet Collectors.* Wet collectors have been in use for many years, but only recently have been introduced for collection of industrial dust from exhaust systems. They are particularly applicable where moisture is present in the air being exhausted. The resistance is relatively low in wet collectors suitable for dust removal and remains constant for a given exhaust system.

3. *High-tension Electrical Precipitation.* High-tension electrical precipitation has been applied to removal of dust, fumes, and mists from air and other gases. (See section on Electric Precipitators in Chapter 33.)

4. *Dynamic Precipitators.* This equipment effects removal of entrained dusts by means of a specially designed fan in which the rotating element imparts a centrifugal force to the dust particles. Originally these precipitators were intended for the collection of dry dust, but recently the construction has been modified to permit the introduction of water into the dirty air intake, thus increasing its application to more kinds of dust. Consideration must be given to the type of dust handled [13].

For additional information on dust and cinders, see Chapter 33, Air Cleaning Devices.

RESISTANCE OF SYSTEM

The maintained resistance of the exhaust system is composed of three factors: (1) loss through the hoods, (2) collector drop, and (3) friction drop in the duct system.

The loss through the hoods is usually assumed to be equal to the suction maintained at the hoods. Where possible the resistance of the particular collector to be used should be obtained from the manufacturer.

TABLE 8. LOSS THROUGH 90-DEG ELBOWS

ELBOW CENTER LINE RADIUS IN PER CENT OF PIPE DIAMETER OR DEPTH	APPROXIMATE LOSS IN PER CENT OF VELOCITY HEAD
50	75
100	26
150	17
200–300	14

TABLE 9. CORROSION RESISTING MATERIALS FOR EXHAUST SYSTEMS[a]

MATERIAL	ACID[b]															
	ACETIC		CHROMIC		HYDRO-CHLORIC		HYDRO-FLUORIC		NITRIC		PHOS-PHORIC		SUL-PHUROUS		SUL-PHURIC	
METALS	Dil.	Conc.	Dil.	Conc.	Dil.	Conc.	Dil.	Conc.	Dil.	Conc.	Dil.	Conc.	Dil.	Conc	Dil.	Conc.
Aluminum	Good		Fair		Poor		No Data		Poor	Good	Poor		Poor		Poor	
Magnesium and Alloys	No Data		Good	Poor	No Data		Poor	Good	No Data		No Data		No Data		No Data	
Lead and Lead-Coated	Poor		Good		Poor		Poor		Poor		Poor		Good		Good	Poor
Moly Alloy (60 *Ni* – 20*Mo* – 20 *Fe*)	Good		No Data		Fair		No Data		Poor		Poor		No Data		Good	
Monel Metal	Fair		Poor		Fair	Poor	Good[d]		Fair	Poor	Fair		Poor		Good[e]	Poor
Bronze	Poor												Good			
Silicon Iron	Fair	Good	No Data		Fair		Poor		Good		Good		No Data		Good	
Stainless Steel[c] (18 *Cr*-8 *Ni*)	Good		Good		Poor		No Data		Good		Poor		Good		Poor	Good[e]
Enameled Steel	No Data		No Data		Good		Poor		Good		Poor		No Data		Good	
MISCELLANEOUS																
Asbestos Comp.					Good except against strong acids and alkalies											
Wood	Some woods are decomposed or softened faster than others.															
Rubber									Poor						Poor	
Plastics	In general plastics resist weak acids and are decomposed by concentrated acid.															

[a] Standard Practice Sheet No. 115 (Division of Industrial Hygiene, New York State Labor Department).
[b] Acid mists in air are more corrosive than as liquid in storage tank. Galvanized iron not resistant to acid.
[c] Stainless steel of (24 *Cr*—10 *Ni*) fairly resistant at low temperature for HCl and H_3PO_4.
[d] Under most conditions.
[e] At room temperatures.

Friction drop in the pipes must be computed for each section where there is a change in area or in velocity. The velocities should be found in each section of pipe starting with the branch most remote from the fan. The friction drop for these sections can be determined by reference to Table 8 in this chapter and Fig. 2, Chapter 41. Total friction loss in the piping system is the friction drop in the most remote branch plus the drop in the various sections of the main, plus the drop in the discharge pipe.

EFFICIENCY OF EXHAUST SYSTEMS

The efficiency of an exhaust system depends upon its effectiveness in reducing the concentration of dusts, fumes, vapors and gases below the safe or threshold limits [14].

Too much emphasis cannot be placed on the necessity of testing exhaust systems frequently by determining the concentration of atmospheric contamination at the worker's breathing level [15]. Commonly accepted values of threshold limits for usual atmospheric contaminants will be found in Tables 3, 4 and 5, Chapter 10.

AIR FLOW PRODUCING EQUIPMENT

In any type of exhaust system some form of air flow producing equipment should be required to create the pressure necessary to cause the air

to flow through the system to the discharge stack. Natural draft should not be depended on to remove harmful or dangerous gases, fumes, mists, dusts, or other matter when it is imperative that such matter be removed from the work place or room atmosphere.

The principal types of air moving equipment are chimney exhausts, venturi ejectors, centrifugal exhaust fans, disc or propeller fans, and axial flow fans [16].

Manufacturers generally provide special fans for the collection of various industrial wastes. These are available for the collection of coal dust, wood shavings, wool, cotton and many other substances. When substances having an abrasive character are conveyed, the fan blades and housing should be protected from wear. This may be accomplished by placing a collector on the negative side of the fan or by lining the housing and blades with rubber.

PROTECTION AGAINST CORROSION

The removal of gases and fumes in many chemical plants requires that metals used in the construction of the exhaust system be resistant to chemical corrosion. A list of the materials which may be used to resist the action of certain fumes is given in Table 9. Hoods and ducts, when short, may frequently be constructed of wood and be quite effective. Rubberized paints are available and may be applied as protective coatings in handling such gases and fumes as chlorine and hydrochloric acid.

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Chapter 47

DRYING SYSTEMS

Mechanism of Drying, Omissions in Drying Cycle, Factors Influencing Drying Rates, Drying Methods and Equipment, Radiant Drying, Conduction Drying, Convection Drying, Calculation and Design, Estimating Methods

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THE term drying in a broad sense encompasses the removal of water, and occasionally other liquids, from gases, liquids, or solids. However, the common usage of the word confines the meaning principally to the removal of water or solvent from solids. Dehumidification is the term that is commonly assigned to the drying of gases. This is usually accomplished by condensation or adsorption by various drying agents and is treated in Chapter 38. Distillation and more particularly fractional distillation is associated with the drying of liquids.

It is usually more economical to employ, whenever possible, mechanical means of separating as much water as is practicable from the solid materials before undertaking drying or dehydration steps. These mechanical methods such as filtration, screening, pressing, centrifuging, or settling usually require much less power and frequently less capital outlay, thereby making the operation cheaper in terms of cost per pound of water removed.

MECHANISM OF DRYING

The course of drying of any substance under constant conditions of temperature, humidity, and air velocity and distribution, follows a definite pattern which can be represented by a graph such as Fig. 1, which is that for a slab of whiting, wherein the rate of drying is plotted against the moisture content. The drying cycle may then be divided into three components: (1) Constant rate period. (2) Uniform falling rate period. (3) Varying falling rate period.

One or more of these components may be missing for a substance under a particular set of conditions.

During the *constant rate* period, water is being evaporated from the surface of the material at a rate comparable to that of a free water surface and moisture is being supplied by diffusion or capillarity to the surface at a rate equal to or greater than the evaporative rate. However, a point is reached at which the moisture reaches the surface at a rate less than the potential evaporative rate. The moisture content of the substance at which this occurs is known as the *critical moisture.* Up to this point the material is generally considered to assume the wet bulb temperature of the air. This is not strictly true as in many cases radiant heat is absorbed or some heat is supplied by conduction.

During the *uniform falling rate* period, moisture is still evaporating from the surface, but the area of wet surface is constantly diminishing.

During the *varying falling rate* period the water is vaporized beneath the surface and escapes as the vapor. As the thickness of the dried material increases, it becomes more difficult for the vapors to escape.

Finally all drying stops at the *equilibrium moisture content,* where the vapor pressure of water in the air is equal to the vapor pressure of water in the material. The *equilibrium moisture content* varies with the humidity

of the air and the hygroscopic properties of the material as explained in Chapter 45.

Omissions in Drying Cycle

Many solids, such as lumber, are so dry at the beginning of the drying operation that the constant rate period of free surface evaporation does not occur. Frequently the surface of the material is dry enough so that no surface drying can take place, in which case only the final stage of sub-surface drying is involved. In other instances, the critical moisture content of a wet solid is sufficiently low that sub-surface drying starts almost immediately after the conclusion of the constant rate period. Thus the intermediate state of unsaturated surface drying does not occur and the drying is of the sub-surface type during practically the whole of the falling rate period. With other kinds of material, particularly thin sheets, such as newsprint paper, sub-surface drying may occur at such a low moisture content that it is not encountered in commercial work, the falling rate period being confined in practice to unsaturated surface drying.

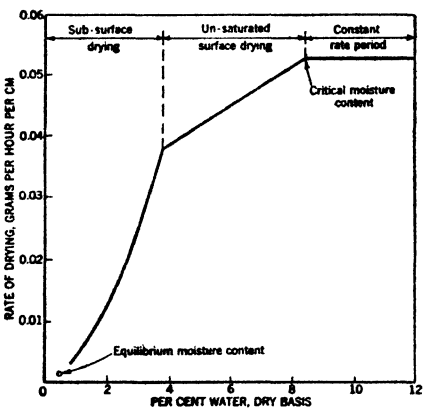

FIG. 1. RATE OF DRYING OF WHITING SLAB

FACTORS INFLUENCING DRYING RATES

Temperature

The driving force for evaporation is directly proportional to the difference between the absolute humidity of the air being used and the absolute humidity of saturated air at this temperature. It may be seen from the psychrometric chart, Fig. 2, that as the temperature increases the humidity of saturated air corresponding to that temperature increases immensely. For example, at 100 F one pound of dry air will carry about 0.04 pounds of water, while at 120 F this figure has become 0.08 pounds. Thus during the constant rate and uniform falling rate periods an increase in temperature will increase the drying rate. During the varying falling rate period, i.e., sub-surface drying where diffusion is the controlling factor, an increase in temperature will lower the viscosity permitting a more rapid drying. Temperature and thickness of the material are the only external variables which affect the drying rate during the variable falling rate period. The drying rate varies inversely with the square of the thickness of the material.

In general, then, it is preferable to use as high a temperature as possible for any drying operation because of the faster rate of drying and the greater capacity of the air to remove water. During the constant rate

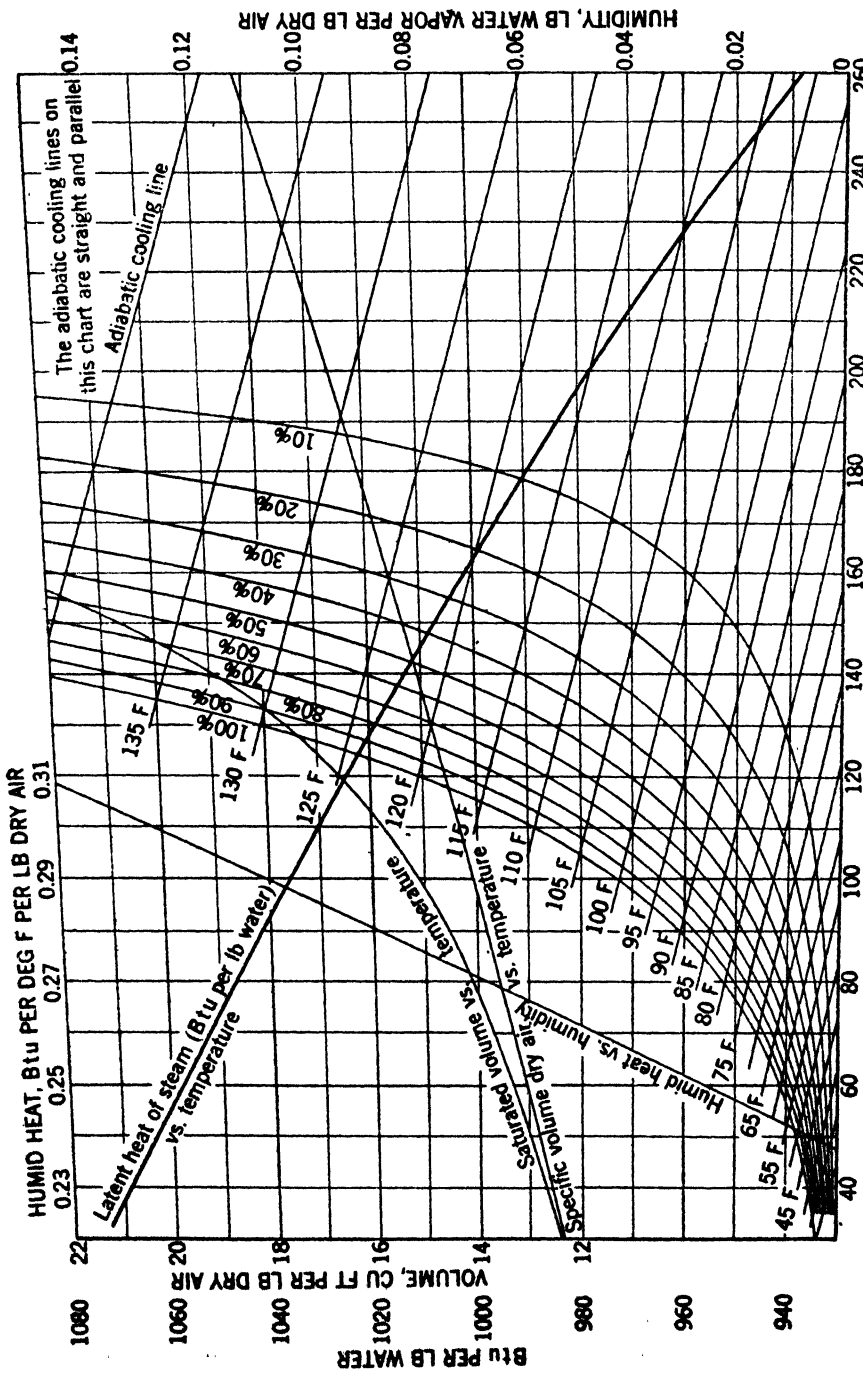

FIG. 2. PSYCHROMETRIC CHART

period of drying, the temperature of the material approximates the wet bulb temperature of the air. Therefore, high dry-bulb temperatures may be employed.

The nature of the material and its characteristics often determine the temperatures that can be employed with safety. For example, chemically combined water may be lost, cells may be steam exploded, charring may take place or exothermic reactions initiated if the product temperature exceeds a critical value.

Humidity

As previously pointed out, absolute humidity is the driving force for evaporation, therefore, a low humidity increases the drying rates. However, certain materials if dried too rapidly may case harden, i.e., form a nearly impermeable skin which greatly reduces the drying rate. Also, certain undesirable physical changes may take place such as the cracking and warping of lumber. In such instances, it may even be necessary to increase artificially the humidity to assure satisfactory drying by the recirculation of moist air or the use of water or steam jets.

In the case of substances that must be dried at relatively low temperatures (120-140 F) it is often necessary to dehumidify the air to secure satisfactory drying rates. In such instances, a closed system using the adsorptive methods described in Chapter 38, is frequently applicable.

Air Circulation

Air velocity and distribution are important factors only in the first two periods of drying when surface evaporation is taking place. During the varying falling rate period of gaseous diffusion enough ventilation must be provided to prevent stagnation. The velocity of the air passing over the surface to be dried determines the rate at which the moisture-laden air is swept away. The more rapidly this moist air can be removed the more rapidly can evaporation occur. It has been demonstrated that this drying rate is a function of the 0.8 power of the velocity. Air directed perpendicularly to the drying surface exhibits the greatest efficiency in dispersing the *dead air* film. The limiting factors in air velocity are the power requirements to remove the air and the danger of blowing away the lighter particles of material.

DRYING METHODS AND EQUIPMENT

Drying systems are sometimes classified according to the method of heat transfer that is employed since the entire problem of drying resolves itself into individual problems of heat transfer and the thermodynamics of air and water vapor. The methods of heat transfer are radiation, conduction and convection. Many types of dryers have been built on these principles for different purposes.

Radiant Drying

Sun drying, the oldest form known to man, is still practiced where the material is amenable to such treatment, where the necessary time can be allowed, and where there is little danger of rain or atmospheric pollution.

In artificial systems radiating surfaces, heated by steam, electricity or other means, afford a good method of heat distribution and control. Radiant heating sets up convection currents, and in low-temperature dryers only about one-third to one-half of the total heat for evaporation

is actually sypplied to the material by radiation. At high temperatures the radiation output increases rapidly, according to the *fourth-power law.* The total radiation may be computed by the equations and tables given in Chapter 5. In general, fins and irregular surfaces do not increase radiation, hence the area to be used in calculations is the area of a smooth-surface envelope enclosing the radiating elements.

A certain amount of air circulation is required through a radiant dryer, in order to carry off the vapor.

Radiant heat from infra-red lamps has been accepted by certain industries as practicable for their specific problems. An example of successful application is found in the drying of lacquers.

Another highly specialized field coming under this heading is electronic drying in which ultra short waves are broadcast into the material and, by interference and adsorption, create heat internally. Some systems have a rather critical optimum frequency. Similarly a high frequency induction field may be employed (See Chapter 30).

Conduction Drying

Drying rolls or drums, flat surfaces, open kettles and immersion heaters are examples of the direct-contact method. Intimate contact of the material with the heating surface is important, and in some cases agitation is desirable to increase the uniformity of heating or to prevent overheating.

Greatest resistance to heat transfer occurs on the air side of the material being dried. The rate of heat transfer from the surface of the heated material to the air, and hence the rate of drying, may be increased by: (a) forced convection or air circulation and (b) vacuum operation to lower the boiling point of the liquid being evaporated.

A rather interesting method of conduction drying was put into practical use during the war for the drying of blood plasma and has since been expanded to other fields such as the preservation of bacteria and other micro-organisms. This has come to be known as freeze drying or drying by sublimation. The material to be dried is first frozen and then placed in a high vacuum chamber connected to extremely low temperature condensers. The water is removed by vaporizing from the solid directly to the gas without ever becoming liquid.

Convection Drying

A limited amount of convection drying takes place in almost any dryer such as those described in the preceding paragraphs. However, to be classified as a convection dryer the principal source of heat is the heated air or other gases circulated in the dryer. There are a number of mechanical means of accomplishing this circulation of air or gases, each of which has some particular virtue. Brief descriptions of some important types of convection dryers follow:

Rotary Dryers. These dryers are cylindrical drums usually having internal flights, as shown in Fig. 3, which cascade the material being dried through the air stream. The driers may be heated directly or indirectly and the air circulation may be parallel or counter flow. A variation is the roto-louvre type dryer, which introduces the air beneath the flights thus securing very intimate contact.

Cabinet and Compartment Dryers. These are generally considered batch dryers wherein each charge is dried to completion before removal. A wide range includes types from the heated loft with only natural con-

vection, and usually poor and non-uniform drying, to the self contained units with forced draft and properly designed baffles which give positive results. It is also possible to evacuate some of the systems for low temperature drying of delicate or hygroscopic materials. These dryers are usually loaded with material spread in trays to increase the exposed surface. The trays are loaded directly into the dryer or may be stacked on trucks which are wheeled in.

Tunnel Dryers. Tunnel dryers are a modification of the compartment dryer and as a rule are continuous or semi-continuous in operation. Heated air or combustion gas is usually circulated by means of fans although a few natural draft units are still in use. The material is handled on trays or racks on trucks and move through the dryer either intermittently or continuously. The air flow may be parallel, counter flow or a combination of the two, obtained by center exhaust. Further, the air flow may be across the surface of the trays or up or down through the bed

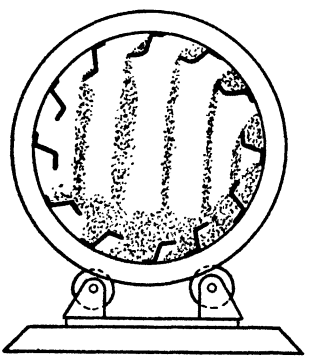

FIG. 3. SECTION OF ROTARY DRYER

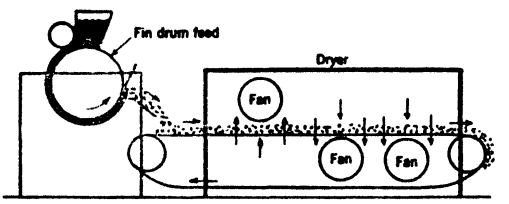

FIG. 4. SECTION OF CONTINUOUS DRYER, BLOW-THROUGH TYPE

or in any combination of directions. By reheating the air in this type of dryer or recirculating it a high degree of saturation is achieved before exhusting the air. This reduces the waste of sensible heat.

A variation on this type dryer is the strictly continuous type having one or more mesh belts which travel through the dryer carrying the product, such as Fig. 4. Innumerable combinations of temperature, humidity and air direction and velocity are possible. The labor requirement is low on such a dryer as it can be loaded and unloaded mechanically. There is the disadvantage of hot air leaks at the entrance and exit although these can be minimized by means of baffles or inclined ends where the material enters and leaves from the bottom.

Spray Dryers. In recent years the spray dryer has become important for the drying of liquids in many fields, especially in the food industry.

The liquid is atomized by means of pressure nozzles, air jets or centrifugal bowls into the air stream of a tower or chamber. Inlet air temperatures may run from 250-300 F up as high as 1200 F. Drying is almost instantaneous because of the minute particle size. The dry powder is separated from the air by cyclone separators which are sometimes followed by cloth bags or scrubbing towers.

Because of the high inlet temperatures and the relatively large volume of air required the efficiency of the spray dryer is not too good and consequently is seldom used for dilute solutions (less than 30 per cent solids).

CALCULATION AND DESIGN

Calculation of the factors involved in drying systems is very complex and frequently inaccurate. For typical examples of the calculations involved the reader is referred to the literature references. Under ideal conditions, however, the following relations hold for convection dryers during the constant rate period.

Constant-Rate Period

The rate of drying by air passing over a wet surface is directly proportional to the vapor pressure difference, and also proportional to the 0.8 power of the air velocity. For practical calculations the wet surface is assumed to attain the wet-bulb temperature of the air passing over it, and evaporation takes place at constant rate under equilibrium conditions. The equation may then be expressed in three forms:

$$R = C\,A\,V^{0.8}\,(\Delta P) \tag{1}$$

$$R = C'\,A\,V^{0.8}\,(\Delta H) \tag{2}$$

$$R = C''\,A\,V^{0.8}\,(\Delta T) \tag{3}$$

where

R = rate of drying during constant-rate period, pounds of moisture per hour.

A = area of bed or material in contact with air, square feet.

V = air velocity over material, feet per minute.

ΔP = difference between vapor pressure at wet-bulb (surface) temperature and at dew-point of air.

ΔH = difference between humidity ratio of saturated air, at the surface temperature, and the actual humidity ratio of the air stream, pounds of water per pound of dry air.

ΔT = difference between dry-bulb and wet-bulb temperatures of air, *i.e.*, the wet-bulb depression.

C, C', C'' = proportionality constants (for numerical values consult references).

These equations are useful mainly for computing the effects of changes in operating conditions, such as changes in air velocity, air temperature, humidity and surface area. The equations assume that the material is in equilibrium at the wet-bulb temperature of the air. If equilibrium has not been reached, or if heat is being added to the charge by radiation or conduction, such conditions must be taken into account. For large tray dryers or continuous surfaces, the logarithmic mean difference should be substituted for the simple difference in ΔP, ΔH and ΔT.

Calculations other than these are probably best left in the hands of experts since considerable data with respect to time, temperature, humidity, air velocity and direction, bed load, pressure drop, recirculation, etc., must be obtained. These data may be based on past experience but are preferably obtained from experiments employing the conditions which are expected in commercial large-scale practice.

Calculations involving the falling rate period are seldom satisfactory because of the number of variables involved but approximations may be made from empirical data obtained by experimentation.

ESTIMATING METHODS

Values based on practical experience are available for rough estimating of drying problems. The temperature will drop approximately 8.5 F deg per (grain of water evaporated) (cubic foot of air, measured at 70 F deg)

or approximately 0.62 F deg per pound of air at any temperature. Air will drop 55 F deg per cubic foot for each Btu extracted. Generally, air will absorb from 2 grains to 5 grains per cubic foot of air in one passage through an air dryer, depending on the temperature and the degree of contact with the material. The amount of steam required to evaporate a pound of water will vary from 1.5 lb to a more usual figure of from 2.5 to 3 lb of steam per pound of water evaporated.

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Chapter 48

TRANSPORTATION AIR CONDITIONING

Railway Passenger Car Ventilation, Method of Air Distribution, Air Cleaning, Winter and Summer Air Conditioning, Humidity and Temperature Control, Summer Air Conditioning for Buses and Automobiles, Airplane Air Conditioning

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THE principles of air conditioning applying to stores, restaurants, hospitals, theaters, and homes are in general applicable to railway passenger cars, buses, automobiles, and ships. However, the equipment used for mobile applications must meet additional requirements. Especially important are features of lightness, compactness, and accessibility for quick inspection and servicing. Freedom from vibration which could be transmitted to the passengers is essential. (For Air Conditioning of Ships see Chapter 49.)

RAILWAY PASSENGER CAR VENTILATION

In non-air-conditioned cars, ventilation is accomplished by exhaust fans, roof ventilators, and by opening doors and windows. This practice provides an ample supply of outside air but does not prevent the entrance of smoke, cinders, and other dirt.

An average passenger car contains approximately 5000 cu ft of air and may seat 80 passengers, who are continually liberating heat, carbon dioxide, moisture, odors, and some organic matter from their breath, skin and clothing. The heat and moisture can be removed by cooling and dehumidification, but the other constituents can be successfully handled only by proper ventilation and air cleansing. In the average car, from 2000 to 2500 cfm should be circulated by the air conditioning unit. Some of this air may be recirculated, but a portion of it should always be brought in from the outside. The amount of outside air will vary from 15 to 90 per cent of the total air circulated depending upon the type of car, number of passengers, air temperature, humidity, odors, and smoking.

Careful attention must be exercised in specifying the rate of outside air taken in so as to fit the type of service adequately and yet not to supply more ventilation than is necessary. Conditioning this outside air is a major factor in determining the size of summer and winter equipment. With present average ventilation requirements, about 30 per cent of the cooling capacity and sometimes as high as 50 per cent of the heating capacity are necessary to handle the outside air load.

For normal conditions, 10 cfm of outside air per passenger is sufficient. When smoking is permitted, at least 15 cfm should be admitted. In some of the dining cars and de luxe sleeping cars, outside air rates as high as 20 and 30 cfm per occupant are used.

Method of Air Distribution

Railway cars present critical problems in air distribution because the air space per passenger is small and the sun load is great. Three principal methods are used to distribute the air to the interior by fans or blowers:

1. A ceiling duct lengthwise along the center of the car.

2. One or two side ducts built on the outside of monitor-roofed cars, or on the inside of turtle-backed or arch-roofed cars.

3. A perforated ceiling supplied by an overhead duct. From one-half to the full area of the ceiling is used for distribution of air although practical considerations generally limit the available area to about two-thirds.

Delivery grilles and plaques designed to give considerable entrainment and mixing are often used to prevent cool drafts.

Smoking rooms present a special problem. The cloud of smoke that usually hangs near the ceiling can be broken up by directing the incoming air along the ceiling at a velocity somewhat higher than that used for the rest of the car. The air should be exhausted through the washroom or lavatory. For compartments an adjustable supply grille of suitable size and design should be provided and provision should be made in the door or partition for the removal of used air.

Lower berths should be provided with an adjustable air outlet which will discharge air at low velocity in any desired direction.

Recirculating air grilles are usually of the straight flow type. Outside air intakes are usually located in the vestibule, on the side of the car, or on the roof, depending upon location of cooling coils. On many of the recently air-conditioned cars, there are no dampers or shutters at the outside air intakes; the percentage of outside air is controlled by adjusting the flow through the recirculating grille.

A considerable number of coach cars is now being equipped with return air ducts fitted in the structure of the baggage racks. Part of the air circulated is returned to the blower unit through these ducts and part through the car body. This arrangement reduces the velocity of air returning through the car body and removes smoke fumes at the source.

Air Cleaning

All air circulated by the blower is filtered before passing over the cooling coils. In some cars the outside and recirculated air is filtered separately before mixing, while in others the air from the two sources is mixed before passing through a common filter. Filters in use are made of metal, wool, cloth, spun glass, hemp, paper, hair, and wire screen. Most filters have a viscous coating of oil for greater cleaning efficiency. Some types may be cleaned, retreated, and re-used while other types are discarded when dirty.

Activated carbon units sometimes are used in addition to the regular filters for adsorbing odors and other impurities, thus reducing the amount of outside air necessary for ventilation.

Trials are also being made of electric precipitation for air cleaning. In this system the coarser particles are removed from the air by mechanical separation, the finer materials being precipitated by electro-static action.

RAILWAY PASSENGER CAR WINTER AIR CONDITIONING

The majority of cars in service use steam from the locomotive or from an oil-fired boiler for winter heating. In some instances electrical energy from a generating set or motive power supply is utilized for heating. In still other cases electrical energy and waste heat from individual car engine-generator sets are employed. The peak heating loads may vary from 150,000 to 250,000 Btu per hour, depending largely upon the amount of insulation used in the car, the type of windows (whether single or double glazed), and the ventilation rate.

From 30 to 50 per cent of the total heat required is supplied by means of finned tempering coils or resistance heaters located in the outside air

duct. The remainder is usually supplied by finned tubing located along the sides of the car near the floor to prevent drafts about the feet.

RAILWAY PASSENGER CAR SUMMER AIR CONDITIONING

Three general types of refrigerating equipment are being used in conditioned railway cars and rail motor cars in the United States. Of these approximately 23 per cent use ice, 19 per cent use steam jet systems, and 58 per cent employ mechanical compression refrigeration systems. The systems were modified somewhat to meet the requirements of mobile service.

Air cooled or evaporative condensers are always used, with the result that mobile cooling equipment operates at higher temperature, pressure, and power requirement levels than stationary equipment.

The maximum cooling and dehumidifying load may vary from 60,000 to 96,000 Btu per hour per car. An average ice-activated system for such capacities uses about 500 lb of ice and 1.2 kw per hour. The increase in car weight due to such a system is approximately 8500 lb.

A steam jet system will require 180 lb of steam and 3.3 kw per hour, and will add weight per car of 8000 lb.

With mechanical compression systems, all of which use dichlorodifluoromethane as a refrigerant, the problem of driving the compressor (approximately 10 hp) is complicated by the necessity of having motive power available at all times whether the car is in motion or standing still on the right-of-way or in a terminal where auxiliary power plug-ins are available. Where compressors are driven from car axles, additional refinements in the drive are necessary in order to obtain the required cooling capacity from a variable speed power source. Numerous schemes for generating sufficient electrical energy from the car axle for lighting, ventilation, and summer air conditioning are in use, and their operation is closely interlocked with compressor demands, battery charging, etc. It is difficult therefore to estimate the weight of a compression air conditioning system, but it is probably in the vicinity of 6000 to 8000 lb. The power required by such systems is from 5 to 10 per cent of the total locomotive power.

Several schemes for relieving the locomotive of this compression load are used. Some of the articulated trains, which run as unit equipment—the same cars always in the same train—employ a head-end, engine-generator unit for supplying power to compressor motors. In other cases, especially in many of the new streamlined trains, propane fueled engine-driven generators on individual cars are used to supply power to motors, and power for car lighting and accessories. Gas engine compressor combinations on individual cars provide attractive low weight equipment where automatic engine operation is permissible under all circumstances. Diesel-powered generator units have been used experimentally on individual cars for supplying electrical energy and in some cases waste engine heat has been used either for modulating refrigeration with a reheat cycle or for car heating purposes.

RAILWAY PASSENGER CAR HUMIDITY AND TEMPERATURE CONTROL

Little humidity control has been attempted on cars up to the present time. A certain degree of automatic humidity control is secured with cooling, but the relative humidity obtained depends largely upon the

temperature of the evaporator, which should be below the dew-point temperature of the air. With certain outside atmospheric conditions it may not be possible to operate conventional equipment with a sufficiently low evaporator temperature to reduce the humidity without dropping the temperature too low.

There is at present a trend toward the reheat system in which the evaporator temperature is carried sufficiently below the dew point to obtain proper dehumidification; the dehumidified air is then heated to the proper dry-bulb temperature for comfort by passing it over a steam coil, or a coil heated by high temperature liquid from the condenser. Where an internal combustion engine is used as a power source the waste engine heat can be used to good advantage for reheating the dehumidified air.

During the heating season a steam or water spray controlled by a humidistat can provide moisture for humidification, but unless properly controlled, condensation will appear on the windows. There are several cars using this feature.

Temperature control, by thermostats and relays capable of withstanding vibrations, is usual equipment. Manual zone control for varying outdoor conditions, as well as controls which regulate the car temperature automatically in accordance with outdoor conditions, are employed.

A system coming into extended use has a thermostat controlling the dry-bulb temperature, and reset by the wet-bulb temperature, in order to approximate best comfort conditions.

Simplified controls from the standpoint of operation by train crews and especially from the servicing viewpoint are very desirable. The control of summer temperatures is accomplished mainly by cycling the complete cooling system; however, modulation is being effected by using multiple evaporators in which a fixed portion may automatically be cut out of operation to suit the cooling capacity requirements and to keep the equipment in operation for longer periods. With motor or engine driven compression equipment modulation of compressor capacity to suit the reduced evaporator capacity is accomplished by changing motor or engine speed, or by varying the number of compressor cylinders in operation.

For further information on controls, see Chapter 34.

PASSENGER BUS SUMMER AIR CONDITIONING AND VENTILATION

The highways in the United States are now traveled by thousands of air-conditioned passenger buses. Many of the facts stressed in connection with the design and installation of summer conditioning equipment in railway cars are even more important in these newer vehicles. Weight and space limitations are more stringent, and the problem of circulating from 900 to 1200 cfm of air in coaches carrying from 25 to 40 passengers with about 35 cu ft of space per passenger without drafts is not easy to solve.

Some bulkhead delivery systems have been used and, while the overhead package racks have served to break up drafts to some extent, these installations are not gaining in popularity. Longitudinal ducts in the corners above the package racks are sometimes used to carry conditioned air to a series of outlet louvers along the top of the windows. Other designs provide for false spaces below the package racks which serve as ducts to distribute air to entrainment grilles in the bottom of the racks

or to distributing slots at the edges of the package racks. Some coaches employ a false ceiling to provide a duct, with delivery taking place from numerous perforations in the ceiling.

Return air grilles and filters are usually located near the rear ceiling where the evaporator is placed. Outside air intakes and filters are located preferably near the front of the vehicle so as not to contaminate this supply with exhaust fumes and road dust. Of the 30 cfm circulated per person, about 8 to 10 cfm are outside air. Power for the motor driving the centrifugal fans is obtained from the bus battery.

More recently a coach design has been brought out which provides for a number of return air outlets below the seats; these permit return air to enter a longitudinal duct below the floor. The filters and evaporator are located in this duct near the front of the vehicle. A central heating coil utilizing waste heat from the coach engine is also located in this duct. Conditioned air is delivered through a pair of vertical ducts to a package rack distribution scheme.

Summer conditioning systems for these vehicles range in cooling capacity from 36,000 to 48,000 Btu per hour. Mechanical compression systems using dichlorodifluoromethane are used, and are powered by water cooled, gasoline engines of approximately 14 hp.

Complete systems add from 800 to 1300 lb to the weight of a coach. Sometimes an auxiliary generator driven by the air conditioning engine is used and serves to help charge the bus battery, thereby offsetting the power drain imposed by the ventilating blower. Belted reciprocating compressors and direct driven V-type and rotary compressors are used, with engine speeds up to about 1800 rpm. Air cooled condensers for this service require about 5000 cfm of outdoor air, and this is provided by either centrifugal or propeller type fans belted or direct driven by the air conditioning engine. Preventing noise and vibration from affecting passengers is of vital importance. Installations must be made so that quick daily servicing of the engine is possible. In all cases fuel is obtained from the main bus tanks, and in some cases the main engine water cooling system is used to cool the air conditioning engine.

In the de luxe equipment, after the driver has started the air conditioning engine by means of its own cranking motor, the engine speed is modulated automatically as the refrigeration demand is partially met, and if this demand is then fully met, the engine is stopped thermostatically. Restarting when the cooling thermostat is no longer satisfied is accomplished either automatically or manually. The various protective and automatic devices on the refrigerant and engine systems make some of the bus air conditioning control systems quite complicated.

AUTOMOBILE SUMMER AIR CONDITIONING

Recently summer cooling has been applied to automobiles. The average present day automobile with little insulation, large, single glazed window areas, and high infiltration and exfiltration losses, requires about 15,000 Btu per hour of cooling capacity. One system utilizes a reciprocating compressor belted from the main engine fan shaft thus operating at varying speeds up to 3000 rpm. The resulting refrigeration capacity varies from about 6000 Btu per hour at idling speed to 24,000 Btu per hour at maximum car speed.

A dry air condenser is placed in front of the engine radiator, and the liquid and suction refrigerant lines run back under the car floor to the

evaporator which is located in back of the rear seat. Conditioned air is delivered into the car just above the shelf near the back of the rear seat. A return grille is provided under the rear seat, and the recirculated air is filtered. Outdoor air is provided by infiltration. Power for the air circulating blowers is obtained from the car storage battery. Equipment of this nature increases the car weight approximately 200 lb.

AIRPLANE AIR CONDITIONING

Complete air conditioning of planes in flight has received little attention probably because of added weight of equipment necessary. Under ordinary conditions heating and temperature control become the chief considerations. Passenger and military planes even at low level flying require no cooling and at extreme altitudes the design temperature of the atmosphere is as low as 60 deg below zero.

In the operation of internal combustion engines the heating value of fuel appears approximately one-third as power, one-third transferred to cooling fluid, and one-third in the exhaust gases.

Ordinarily, the heat in the exhaust gases is ample for all heating needs, despite the excessive transmission loss due to high speed, low temperatures, and light wall construction. The maximum coefficient of heat transmission without insulation is found to be 2.3. The minimum coefficient with insulation is 0.3. For present day construction a value of 0.6 may be assumed for speeds not exceeding 300 mph. Naturally, the waste heat in the exhaust gases offers an attractive source for designers of heating equipment, who have followed closely the development of heating as applied to land structures. In first attempts heat was obtained from an annular space surrounding the exhaust pipe, from which branches conducted the heated air to grilles or to seats of passengers. The speed of the plane eliminates the need for a fan or pump. In present practice danger of carbon monoxide contamination is reduced by the use of both primary and secondary heat exchangers.

Heating systems using hot air are in use for passenger and military planes. Steam systems have been used with boilers located in the path of exhaust gases but difficulty experienced in preventing freezing of the water has apparently rendered this system unattractive. A similar system using glycol is in use and requires special care because of the peculiar qualities of glycol. Thermostatic control, mixing dampers and air distribution vary little from standard practice. Controlling devices are built to withstand the extensive vibrations experienced. Planes requiring air conditioning when on the ground are satisfactorily serviced by portable air conditioning machines. High flying airplanes—above an elevation of 14,000 ft—require oxygen supply or pressurized cabins. The compression of the outside air by the supercharger raises the temperature of the cabin air from an extremely low to a comfortable high. The compression of the air also increases the humidity. Cleanliness at flying altitude is not a consideration, except under special conditions such as above deserts or upon encountering dust storms. In small planes carrying several passengers or crew, localized heating and ventilation are provided. Electrically heated clothing and oxygen masks often are required in combat aircraft. At high altitudes pressurized cabins require no special oxygen supply.

Medium bombers at one time were equipped with separately fired heating units, but larger bombers, to meet the heating load imposed by

crew and equipment, demand too much heat to be supplied in this manner. The recovery of heat from waste gases is therefore imperative. In airplane operations light weight is a more important requirement than in any other type of transportation. Noise should be reduced to a minimum and combined use may be made of material for insulating and noise reduction.

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Chapter 49

MARINE HEATING, VENTILATION, AIR CONDITIONING

General Considerations, Ship Construction Features, Factors Affecting Design, Ventilation Requirement for Various Types of Space, Air Conditioning Space Treatment, Typical Air Conditioning Systems, Types of Refrigerating Systems, Dehumidification, Ship Insulation

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THE importance of adequate shipboard heating, ventilation, and air conditioning arrangements cannot be overemphasized. Installations must be designed to keep the passengers comfortable and the operating personnel physically and mentally fit. The provision of satisfactory living and working conditions is one of the most economical means of keeping a high morale.

GENERAL CONSIDERATIONS

A ship must be self-sufficient and provide for all human needs. Facilities must be limited to the minimum space and weight practicable to conserve dead weight and to increase the pay load. The pay load may be expressed in terms of cargo carrying ability, passenger carrying capacity, fighting strength, or towing ability.

Conditions in living spaces must permit adequate rest and comfort. Passenger accommodations must be treated to provide service and living conditions similar to those afforded by the various classes of hotels. Many of the expedients used ashore for this purpose are not applicable afloat. For instance, all living quarters aboard ship cannot be located at a distance from the power plant, but must often have boundaries in common with heat producing spaces. The thermal conductivity of shipbuilding materials such as steel, copper, brass, etc., is many times the value for building materials used ashore, and this, together with concentrated arrangement of equipment, produces a difficult heat transfer and insulation problem. Furthermore, the use of portholes, windows, skylights, and similar openings is greatly restricted in marine applications because of the necessity for strength, water-tightness and protection from the sea in foul weather. During wartime, the utility of portholes, windows, and skylights is greatly restricted because they must be fitted with light-excluding devices.

Mechanical ventilation is absolutely necessary for most shipboard spaces to enable the crew to operate the vessel, to prevent the accumulation of objectionable combustible and toxic gases, and to preserve stores and cargo. Shipboard equipment must also be reliable inasmuch as specialized servicing facilities are not available at sea and failure during an emergency may jeopardize the vessel's safety. Adequate spare parts form an integral part of all equipment furnished. Experience has demonstrated that *simple* and *foolproof* heating, ventilating, and air conditioning arrangements are essential for satisfactory service. The only variation between ship and shore applications is that emphasis is placed on different practical aspects of the design.

SHIP CONSTRUCTION FEATURES

The seaworthiness of a vessel is increased by subdividing the main hull space into a number of watertight compartments, so arranged that the vessel

will not sink even when the hull is pierced in one or more places, by collision, torpedoing, or other causes. Every effort is made to avoid penetration of watertight subdivisions and, where openings must be cut, special closures are fitted.

The ship's interior is fitted with decks and flats (partial decks). The deck heights (floor heights) in cargo spaces generally vary from 9 to 30 ft and in living quarters from 7½ to 9 ft. Usually in main machinery spaces, the entire depth is subdivided only by a few flats, with gratings provided where necessary to service equipment.

There is very little unassigned space on a ship, and many studies must be made to ascertain the arrangement of equipment which will best suit the conditions. Cuts in structural members must be limited in number and size. Lack of headroom and floor space often causes unsatisfactory drainage, inaccessibility, and other undesirable conditions. Air conditioning equipment must be located where it will interfere least with basic arrangements of major equipment and construction, and with ship stability.

FACTORS AFFECTING DESIGN

A ship is a self-contained structure capable of operating in a wide range of climates. The ventilation of most ships is designed on the basis of an 88 F outside dry-bulb temperature. Heating facilities on merchant vessels are invariably selected for an outside temperature of 0 F dry-bulb, although ships encountering only moderately cold weather in normal service are designed for higher outside temperatures. Designers of naval vessels commonly use 10 F outside dry-bulb temperature for estimating heating loads.

Cooling loads for most comfort systems are based on 95 F dry-bulb and 80 F wet-bulb temperatures. Inside conditions equivalent to from 73 to 75 effective temperature are used. An 81 F dry-bulb temperature and 50 per cent relative humidity are generally used for the design of comfort systems, except those serving public spaces having relatively large latent loads. These are designed for 80 F dry-bulb and approximately 55 per cent relative humidity. Bracket fans are supplied in many instances. Systems on naval vessels are designed for higher effective temperatures, and outside design temperatures of 88 F dry-bulb and 80 F wet-bulb are used.

Preliminary design is simplified by the uniformity of the conditions which apply to most ships. Among such conditions are (1) the necessity for the vessel to supply its own power, (2) the availability of an unlimited supply of cooling water, (3) the all-year-round supply of low cost steam at suitable pressure, (4) the drastic restriction of shipbuilding materials because of strength requirements, corrosion resistance, and fire hazard, and (5) the limitation of available space and permissible weight. These limitations require precise layouts, with minimum design safety factor, and unusual attention to design details and to means for balancing systems.

The relation between supply and exhaust ventilation depends on the type of space, and the relation of the space to the weather. Positive means for supply and exhaust must be provided. Ventilation through doors, windows, hatches, etc., should not be considered in the basic design.

It is usually most economical to heat spaces served by mechanical supply systems with steam duct heaters, in order to save weight and space. Spaces which do not have mechanical supply or do not require

ventilation in cold weather are heated by steam convectors, or unit heaters where the load is large. Ventilation air, except that supplied to auxiliary and main machinery spaces, is usually preheated (50 to 70 deg). In addition, where blast heating is used, zone reheaters are provided. No recirculation is used on combined ventilation and heating systems, but manual speed reduction (25 to 50 per cent) is provided during the heating cycle. All heaters are automatically controlled, and preheaters are designed and installed to minimize the possibility of freezing of condensate.

The usual combinations or variations of duct type and convection or radiant heaters are used, depending on basic design requirements, such as weight and space limitations, and economic justification for refinements.

VENTILATION REQUIREMENT FOR VARIOUS TYPES OF SPACE

In the paragraphs which follow the most important considerations are given for the treatment of the various spaces, but the resulting quantities of air should in all cases be checked with those shown in Table 1.

Machinery Spaces

The prime purpose of machinery space ventilation is to maintain a habitable temperature for the operating personnel. Of secondary importance is the necessity for maintaining temperature conditions satisfactory for the successful operation of machinery. It is more practicable to use *spot cooling* of personnel at working areas than to attempt to obtain uniform ambient temperature. The permissible temperature rise at working stations is usually about 15 deg while the over-all temperature rise is usually between 30 and 50 deg.

These spaces must be exhausted adequately, preferably by mechanical means. Every attempt should be made to remove air at or close to heat sources. The capacity of the mechanical exhaust systems should take into consideration the expansion of the supply air, and should be sufficient to insure an indraft through access openings to the space.

Normally, heat is not required for machinery spaces except for those fitted with electrically operated equipment, which may remain inactive during periods while in port. Such spaces should be equipped so as to be heated to about 50 F during such periods.

Living Spaces

The minimum quantity of air required for any space which is fitted for sleeping or office work, including hospital space, should be that which will limit the temperature rise over the outside air conditions to not more than 10 deg (a rise of 7 deg is more satisfactory if practicable), or a minimum of 30 cfm per person, whichever is the greater. For spaces fitted for eating, recreation, or manual work the rise may be taken at 10 deg with not less than 20 cfm per person. The same requirement applies to mechanical exhaust, although natural exhaust may be used where only a short run of duct exists.

Heat should be furnished to maintain the following temperatures:

Staterooms, Berthing, Messing and Office Spaces	70 F
Working Spaces and Shops	60 F
Hospital Spaces	75 to 78 F

TABLE 1. TYPICAL HEATING AND VENTILATION PRACTICES FOR SHIPS

SPACE	TYPE OF VENTILATION		TYPE OF HEATING	AIR CHANGE MINUTES	REMARKS
	Sup.	Exh.			
Living Quarters	Mech.	Mech. or Nat.	H.B.[a] or D.R.[b]	3-6	
Toilets and Showers	Nat.	Mech.	D.R.	3-4	
Chart House	Mech.	Mech. or Nat.	H.B. or D.R.	5-6	
Office and Similar Spaces	Mech.	Mech. or Nat.	H.B. or D.R.	4-6	
Mess Rooms	Mech.	Mech. or Nat.	H.B. or D.R.	4-6	May be exhausted through Galleys and Pantries
Dining Salons	Mech.	Mech. or Nat.	H.B. or D.R.	3-6	May be exhausted through Galleys and Pantries.
Galley and Pantry	Mech. & Nat.	Mech.	T.A.[c]	½-1	Tempered Air Supply
Deck Pantries (No Cooking Equipment)	Mech. & Nat.	Mech.	H.B. or D.R.	3-6	
Stores Spaces (Isolated Locations)	Mech. or Nat.	Nat. or Mech.	.....	15-30	
Hospital Spaces	Mech.	Mech.	H.B. or D.R.	3-4	
Soiled Linens and Oilskin Lockers	Nat.	Mech.	.....	6-10	
Shops	Mech.	Mech. or Nat.	H.B. or D.R.	4-10	
Group Berthing Spaces	Mech.	Mech. or Nat.	H.B. or D.R.	3-6	
CO_2 Bottle Space	Nat.	Mech.	.....	10	
Battery Room	Nat.	Mech.	D.R.	2	
Laundry	Mech.	Mech.	H.B.	1-4	Tempered Air Supply
Dry Cargo Holds	Mech.	Nat. or Mech.	.....	20-30	
Stearing Gear Space	Mech. or Nat.	Mech. or Nat.	H.B. or D.R.	2-6	Unit Heater if desired.
Gyro Room	Mech.	Nat. or Mech.	.....	3-6	
Theaters and Halls	Mech.	Nat. or Mech.	H.B. or D.R.	4-6	
Passageways and Stairwells	Nat.	Nat. or Mech.	D.R.	.....	Exhausting Adjacent Quarters.
Engine and Boiler Rooms	Mech.	Mech. or Nat.	.....	1-2	
Misc. Machinery	Mech. or Nat.	Mech. or Nat.	.....	2-4	
Resistor Spaces	Nat.	Mech.	.....	10	

[a]H. B.—Hot Blast System.
[b]D. R.—Direct Radiation.
[c]T. A.—Tempered Air.

Toilets, Washrooms, Showers and Baths

Spaces for these purposes should be fitted with mechanical exhaust ventilation for odor and steam removal. Generally, the surrounding living or working spaces are exhausted through them. Air requirements on merchant vessels are commonly estimated on the basis of a 4 min rate of change. Where the amount of available air is limited by outside air requirements of air conditioning systems, rates of change as high as one change

in 6 min are used for private bathrooms. On naval vessels, the minimum total quantity of exhaust is that which changes the air within the compartment in 6 min, plus 25 cfm for each toilet fixture, plus 50 cfm for each shower head.

Heat is obtained by use of convector radiators which should maintain a temperature of 70 F.

Galleys, Bakeries, Laundries, and Food Handling Spaces

The problem of the ventilation of spaces fitted for cooking and food preparation is primarily one of heat and smoke or fume removal. Complete mechanical exhaust is always provided, and the mechanical supply is made equivalent to at least 50 per cent of the exhaust. Sufficient natural supply to provide an indraft is required. The exhaust quantities should be predicated on restricting the ambient temperature rise to about 15 deg above the outside summer design air conditions. The resulting quantity will change the air in these spaces in about $\frac{3}{8}$ to 1 min. All of the exhaust should be arranged to remove air from the space through hoods fitted over the heat producing equipment. The mechanical supply should blow air directly on the personnel, but away from the equipment and so as not to interfere with the flow of exhaust air to the hoods.

The problem of ventilating laundries is somewhat similar to that for galleys. Experience indicates that the quantity of mechanical supply ventilation should be sufficient to change the air in the spaces in 1 to 4 min. The total exhaust (including tumbler dryers) should be equivalent to at least one air change per minute and at least equal to 120 per cent of the supply so as to insure an indraft of air. Generally, no heat is required for these spaces in winter, but preheaters are provided to temper the supply to between 45 and 60 F.

Storerooms and Cargo Spaces

The ventilation provided for these spaces depends on the type of vessel, location of space, and nature of cargo.

On merchant vessels ventilation is required for all closed spaces. Even if ventilation is not necessary to preserve the stores or cargo, it is required to prevent the accumulation of toxic or combustible gases and putrid odors. One air change in 15 to 30 min is common practice, except where inflammable liquids or proximity to hot spaces requires additional ventilation. Mechanical supply and natural exhaust are usually used. However, where inflammable gases may exist, natural supply and mechanical exhaust are provided.

It is the practice on naval vessels to omit ventilation where it is not necessary to preserve the stores, except for those spaces which hold inflammable liquids. The latter are provided with mechanical exhaust systems and natural supply. As spaces below the waterline are frequently damp, those which are unventilated may require chemical desiccants for removing moisture.

Refrigerated stores and cargo spaces requiring constant temperature and humidity control require special treatment.

AIR CONDITIONING SPACE TREATMENT

The extent of the application of air conditioning to new American passenger ships is fairly well established. All passenger staterooms, except steerage and third class, are usually air conditioned. This includes state-

rooms for ship's personnel and offices within conditioned passenger areas. Third class staterooms are air conditioned on some ships, depending on the particular trade. Theaters, lounges, smoking rooms, beauty shops, barber shops and similar closed public spaces are usually air conditioned.

All messrooms, recreation rooms, captain's and chief engineer's staterooms and offices, crew's inboard rooms and those having fixed portlights are usually air conditioned on passenger vessels. Other living spaces are air conditioned on some ships and only ventilated and heated on

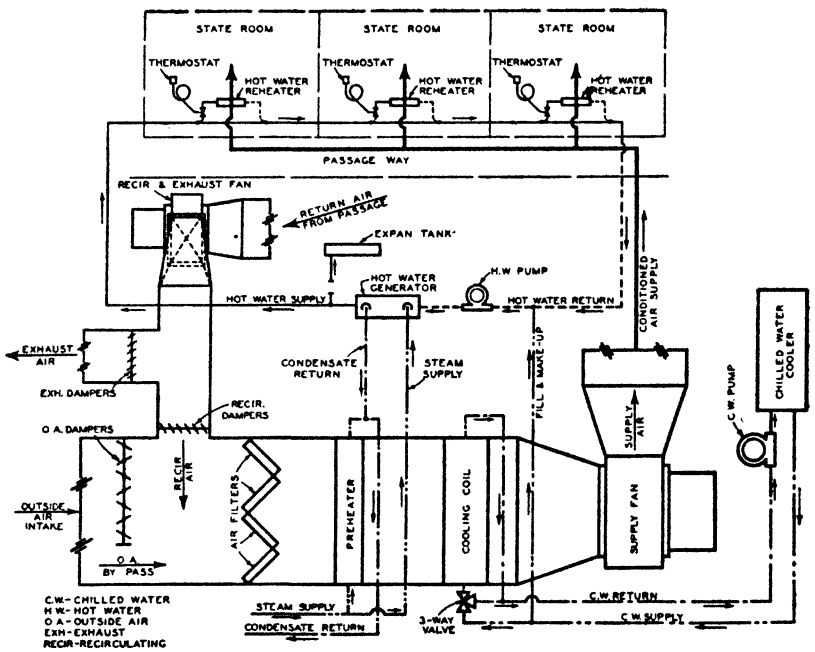

FIG. 1. ARRANGEMENT OF AIR CONDITIONING SYSTEM WITH CENTRAL SUPPLY EQUIPMENT AND INDIVIDUAL HOT WATER ROOM REHEATERS

others. The treatment depends on the requirements of the operator and the proposed itinerary of the vessel.

TYPICAL SYSTEMS OF COMFORT AIR CONDITIONING

The various types of comfort conditioning systems used to date generally have followed conventional lines, except for those serving staterooms, offices, and similar small spaces. Large public spaces are fitted with individual systems which supply dehumidified and cooled air during the cooling cycle and warm air during the heating cycle. In many cases these rooms are fitted with large glass windows and doors, and require direct radiation to offset the downdraft which would occur in cold weather. Finned-tube radiation running the full length of the glass area is commonly used for this purpose.

Systems serving most public spaces are designed to provide all outside air as long as the refrigeration load is less than the capacity of the cooling equipment. Many central systems are simplified by using 100 per cent outside air all-year-round.

An important problem in ship air conditioning concerns the treatment of the small spaces such as passenger staterooms, offices, and crew quarters. Low headroom, congested quarters, double berths, and unsymmetric arrangements make each space a problem in air distribution and treatment.

The simplest system used for small spaces consists of a central filter bank, supply fan, preheater, and cooling and dehumidifying coil. Zone

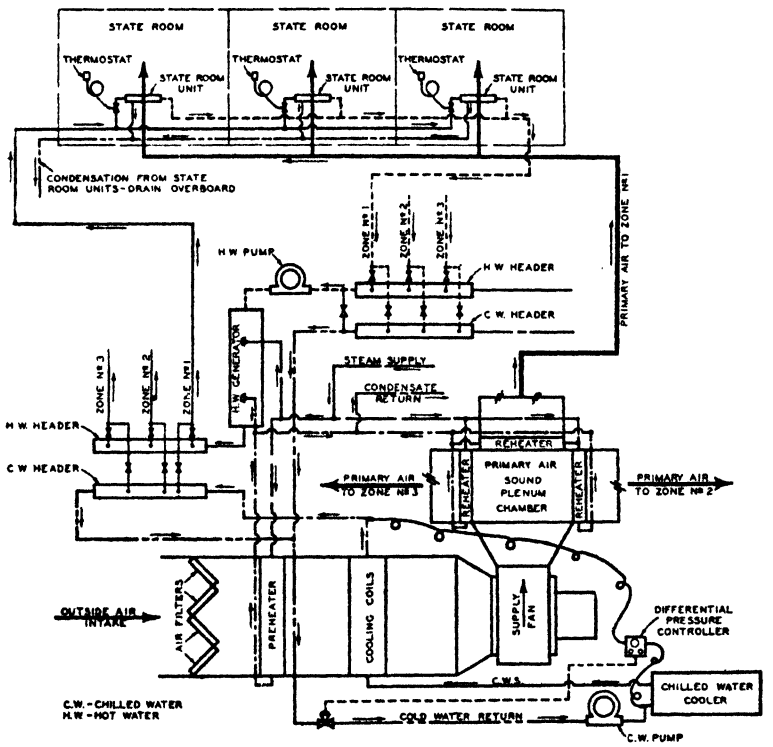

FIG. 2. ARRANGEMENT OF AIR CONDITIONING SYSTEM WITH CENTRAL SUPPLY EQUIPMENT AND INDIVIDUAL ROOM INDUCTION UNITS

reheaters are provided to take care of variations in heating loads. Control of room temperature is achieved by manual dampers in the air supply to the space. A recirculation-exhaust fan is provided, which operates in conjunction with automatic dampers to utilize the maximum quantity of outside air consistent with the capacity of the cooling coils. Manual speed reduction, without recirculation, is normally provided during the heating cycle. This system is used principally for third class, crew, and officer's accommodations. The average total air per person is about 45 cfm, and average outside air about 15 cfm.

A more popular system utilizes the same central supply equipment and recirculation-exhaust system as the one just described, except that the zone reheaters are omitted. Each space is provided with a small hot water reheater, automatically controlled by a room thermostat. Heat is provided through a forced circulation, single pipe, hot water system in most cases. Fig. 1 shows a diagrammatic arrangement of this system. It

should be noted that reheat is used to eliminate overcooling of the individual spaces during mild cooling conditions. This system is generally used for staterooms and small spaces devoted to first and second class passengers. The average total air per person is about 60 cfm and average outside air per person is about 18 cfm.

A third, less common, arrangement is a primary air system consisting of central filters, preheaters, cooling and dehumidifying coil, supply fan, and zone reheaters. In addition, each room is provided with an induction unit (floor type where possible) which reheats or recools the primary air supply. Automatic regulation of chilled or hot water flow, achieved by a room thermostat, controls the space temperature. The unit is provided with a drip pan and drain piping is required to remove condensation. Fig. 2 shows a diagram of this system, which is generally confined to passenger accommodations. The average primary (outside) air is about 35 cfm per person. No recirculation is used. The amount of induced air varies with the unit design.

Another system, which may be used to a limited extent, is similar to the third system, except that the room induction unit is used only to reheat the primary air, as all cooling and dehumidifying is done centrally. This simplifies the system and eliminates the unit drainage facilities. However, as no recirculation is used, the primary (outside) air requirements are somewhat larger, averaging about 40 cfm per person.

The duct work for all of the above systems may be designed for conventional velocities. However, if power is available, high velocity systems may be used providing suitably strong duct construction and adequate sound absorbing facilities are provided.

TYPES OF REFRIGERATION SYSTEMS

The kind of refrigeration equipment chosen for a particular vessel depends on the same factors which would govern selection on land.

Small tonnages use reciprocating or radial (Freon) compressors. Ships requiring in excess of approximately 125 tons of refrigeration generally use centrifugal compressors. Steam jet refrigeration has proven satisfactory on several large foreign liners and is being seriously considered in this country for similar applications. The two essential prerequisites of the steam jet—low-cost steam and condenser cooling water—are available. Also, the simplicity of principle and operation are very desirable features even for small installations.

Many ships have considerable refrigerated cargo space. The type of equipment used for this application should be kept in mind when selecting equipment to be used for air conditioning. This consideration can reduce materially the over-all cost, because a stand-by unit is always provided for cargo refrigeration. Also, most cargo systems are designed for cooling hot cargoes, and thus a large part of the capacity is available for comfort air conditioning most of the time.

DEHUMIDIFICATION

Merchant Vessels

Many merchant ships are fitted with dehumidification facilities for eliminating damage to the dry cargo by preventing condensation and dampness. The dehumidification load consists of moisture removed from the ventilation air passed through the dehumidifier, and also the

moisture on, or given off by, the cargo, packaging, dunnage, battens, and other materials in the ship's holds. The most severe outside condition requires a moisture removal of 90 grains (140-50) per pound of dry air, with 88 F cooling water. The largest cargo ships are provided with equipment for removing about 250 lb of water per hour.

The dehumidification systems generally utilize silica gel or lithium chloride with inhibitor (see Chapter 38). In most cases central drying equipment is provided and a simple duct system distributes the dry air to the hold supply ventilation system. These ventilation systems use outside air when weather conditions are favorable. Recirculation and dehumidification are used only when necessary; *i.e.* when the weather dew-point approaches or exceeds the temperature in the hold. On large passenger ships consideration is given to the use of two dehumidifying units, because the cargo carrying spaces are usually concentrated at the extreme ends of the vessel. With this arrangement, almost all of the dry air distributing system may be eliminated.

Naval Vessels

The end of the war terminated the current need for a great number of naval vessels and presented the problem of their economical preservation and readiness for speedy return to active service. This problem has been solved by making the ship a warehouse for its own non-perishable stores and supplies, painting the exterior, applying polar type rust preventives (requiring no later removal) to corrodible exposed metal, and sealing and dehumidifying the interior. Such ships can be returned to service in 10 to 30 days.

The dehumidifiers developed for this purpose are dual bed, electric heat reactivating types and represent improvements for their special application over commercially available equipment, with respect to compactness, weight, reliability, performance, and economy. On most ships dry air from the machine is delivered to the remote portions of the vessel through the fire mains, which provide the most extensive piping system available. The air returns to the machine via accesses and passageways. Humidity is maintained constant at a prescribed value, usually 30 per cent, by a recorder-controller developed especially for the preservation program. This device continuously checks, records, and averages humidity readings of 8 *sensing* stations, located throughout the vessel, and starts or stops the dehumidifier accordingly.

SHIP INSULATION

In order to limit one of the major ventilation heat loads which is that made necessary by heat transmission, and to prevent condensation, it is necessary to use insulation judiciously. The principal sources of heat in a ship are the power plant and sun load. The confinement or exclusion of this heat in the structure of a ship is not easy, principally because of the complex structural nature of the beams, stiffeners, bulkheads, decks, and hull. The continuous metal paths offer easy means of heat flow throughout the structure.

Insulation cannot be used indiscriminately because of weight and space limitations. Therefore higher heat transmission coefficients are accepted for insulated structures of certain classes of vessels, than would be considered satisfactory ashore. Particular care must be taken to prevent metal to metal contact, which greatly reduces the effectiveness of the insulation.

Hull insulation must be of high quality with particular attention given to fireproofness, low density, low thermal conductivity, ruggedness, vermin resistant ability, and ease of application. Board or blanket types are most common.

Duct insulation must have the same characteristics as hull insulation. Semi-rigid board is most common, and the blanket type is used only for curved surfaces. Corrugated asbestos is not used because the presence of moisture tends to disintegrate it.

Preheaters are frequently located close to the outside air intake in order to conserve insulation, and for the same reason zone reheaters are located as close as possible to the zone. Where a reheater serves only one space, the heater is commonly located in the space.

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Chapter 50

WATER SERVICES

Estimate of Demand Load, Estimate of Pipe Capacity, Sizing of Cold Water Supply Piping, Hot Water Supply Piping, Storage Capacity and Heating Load, Methods of Heating Water, Computing Area of Heat Transmitting Surface, Control of Service Water Temperature, Solar Water Heaters

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PROPER design of the water distributing system in a building is necessary in order that the various fixtures may adequately perform their function. The amount of either hot or cold water used in any building is variable, depending on the type of structure, usage, occupancy, and time of day. It is necessary to provide piping, water heating, and storage facilities of sufficient capacity to meet the peak demand without wasteful excess in either piping or equivalent cost. Most of the following data on the sizing of water supply pipes have been taken from various publications of the National Bureau of Standards [1].

ESTIMATE OF DEMAND LOAD

The demand load in building water supply systems is based on the number and kind of fixtures installed and on the probable simultaneous use of these fixtures. The essentials for making these estimates consist principally of Table 1 giving demand weights in terms of fixture units for different plumbing fixtures under different conditions of service and Fig. 1 giving estimated demand in gallons per minute corresponding to any total number of fixture units. Fig. 2 shows an enlargement of Fig. 1 for a range up to 250 fixture units.

The estimated demand load for fixtures used intermittently on any supply pipe will be obtained by multiplying the number of each kind of fixture supplied through that pipe by its weight from Table 1, adding the products, and then referring to the appropriate curve of Figs. 1 or 2 with this sum. In using this method it should be noted that the demand for fixture or supply outlets other than those listed in the table of fixture units is not yet included in the estimate. The demands for outlets—such as hose connections, air conditioning apparatus, etc.—which are likely to impose continuous demand during times of heavy use of the weighted fixtures should be estimated separately and added to the demand for fixtures used intermittently, in order to estimate the total demand.

ESTIMATE OF PIPE CAPACITY

The size of iron pipe required to carry a given rate of flow with a given pressure drop may be determined from Fig. 3 for *Fairly Rough*, or Fig. 4 for *Rough* Pipe, respectively [2].

Ferrous pipe, after a few years of water supply service even with the best of waters in respect to corrosion and caking, will have become sufficiently roughened so that it may be considered as fairly rough pipe and, hence, Fig. 3 may be used to estimate the capacity of ferrous pipe which will carry such water. With badly corrosive or badly caking water, the flow chart in Fig. 4 should be used to estimate capacities of ferrous pipe and no pipe should be smaller than ¾ inch.

As copper tubing is not likely to retain interior incrustration to any

TABLE 1. DEMAND WEIGHTS OF FIXTURES IN FIXTURE UNITS[a]

FIXTURE OR GROUP[b]	OCCUPANCY	TYPE OF SUPPLY CONTROL	WEIGHT IN FIXTURE UNITS[c]
Water closet	Public	Flush valve	10
Water closet	Public	Flush tank	5
Pedestal urinal	Public	Flush valve	10
Stall or wall urinal	Public	Flush valve	5
Stall or wall urinal	Public	Flush tank	3
Lavatory	Public	Faucet	2
Bathtub	Public	Faucet	4
Shower head	Public	Mixing valve	4
Service sink	Office, etc.	Faucet	3
Kitchen sink	Hotel or restaurant	Faucet	4
Water closet	Private	Flush valve	6
Water closet	Private	Flush tank	3
Lavatory	Private	Faucet	1
Bathtub	Private	Faucet	2
Shower head	Private	Mixing valve	2
Bathroom group	Private	Flush valve for closet	8
Bathroom group	Private	Flush tank for closet	6
Separate shower	Private	Mixing valve	2
Kitchen sink	Private	Faucet	2
Laundry trays (1-3)	Private	Faucet	3
Combination fixture	Private	Faucet	3

[a] For supply outlets likely to impose continuous demands, estimate continuous supply separately and add to total demand for fixtures.

[b] For fixtures not listed, weights may be assumed by comparing the fixture to a listed one using water in similar quantities and at similar rates.

[c] The given weights are for total demand. For fixtures with both hot and cold water supplies, the weights for maximum separate demands may be taken as ¾ the listed demand for the supply.

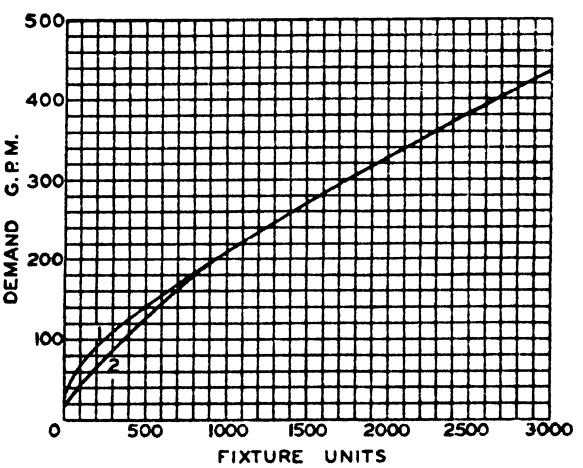

FIG. 1. ESTIMATE CURVES FOR DEMAND LOAD

No. 1 for system predominantly for flush valves.

No. 2 for system predominantly for flush tanks.

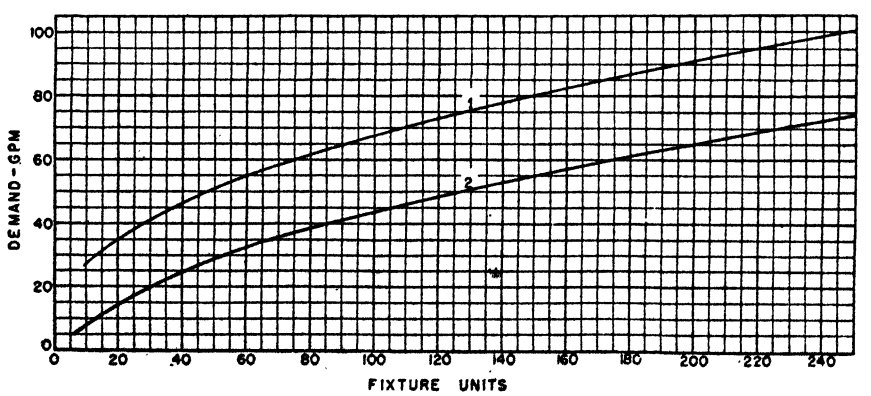

FIG. 2. SECTION OF FIG. 1 ON ENLARGED SCALE

TABLE 2. PERFORMANCE REQUIREMENTS OF WATER METERS[a]

SIZE IN.	NORMAL TEST-FLOW LIMITS GPM	MINIMUM TEST-FLOW GPM
⅝	1 to 20	¼
¾	2 to 34	½
1	3 to 53	¾
1½	5 to 100	1½
2	8 to 160	2
3	16 to 315	4
4	28 to 500	7
6	48 to 1,000	12

[a] *American Water Works Association Standards:*
Registration. The registration on the meter dial shall indicate the quantity recorded to be not less than 98 per cent nor more than 102 per cent of the water actually passed through the meter while it is being tested at rates of flow within the specified limits herein under normal test flow limits: There shall be not less than 90 per cent of the actual flow recorded when a test is made at the rate of flow set forth under minimum test flow.

serious extent, Fig. 5 may be used safely to estimate carrying capacity of copper tubing[2].

SIZING OF COLD WATER SUPPLY PIPING

In order to apply the foregoing principles to the sizing of the supply pipes in the usual up-feed system, it is necessary to ascertain the minimum pressure in the street main, and from this should be subtracted the minimum pressure required for the operation of the topmost fixture. (A pressure of 15 psi is ample for flush valves but reference should be made to the manufacturers' requirements. A minimum of 8 psi should be allowed for other fixtures.) The pressure differential thus obtained will be available for overcoming pressure losses in the distributing system and in overcoming the difference in elevation between the water main and the highest fixture.

The pressure losses in the distributing system will consist of the pressure losses in the piping itself, the pressure losses in the pipe fittings, and the pressure losses in the water meter, if any. Estimated pressure losses for disc-type meters for various rates of flow are given in Fig. 6. Flow limits for disc-type meters, which may be regarded as the limits of recommended ranges in capacities, are given in Table 2. For information on other types of meters the manufacturers should be consulted.

TABLE 3. ALLOWANCE IN EQUIVALENT LENGTH OF PIPE FOR FRICTION LOSS IN VALVES AND THREADED FITTINGS

DIAMETER OF FITTING IN.	EQUIVALENT LENGTH OF PIPE FOR VARIOUS FITTINGS						
	90 Deg Standard Ell Ft	45 Deg Standard Ell Ft	90 Deg Side Tee Ft	Coupling or Straight Run of Tee Ft	Gate Valve Ft	Globe Valve Ft	Angle Valve Ft
⅜	1	0.6	1.5	0.3	0.2	8	4
½	2	1.2	3	0.6	0.4	15	8
¾	2.5	1.5	4	0.8	0.5	20	12
1	3	1.8	5	0.9	0.6	25	15
1¼	4	2.4	6	1.2	0.8	35	18
1½	5	3	7	1.5	1.0	45	22
2	7	4	10	2	1.3	55	28
2½	8	5	12	2.5	1.6	65	34
3	10	6	15	3	2	80	40
3½	12	7	18	3.6	2.4	100	50
4	14	8	21	4.0	2.7	125	55
5	17	10	25	5	3.3	140	70
6	20	12	30	6	4	165	80

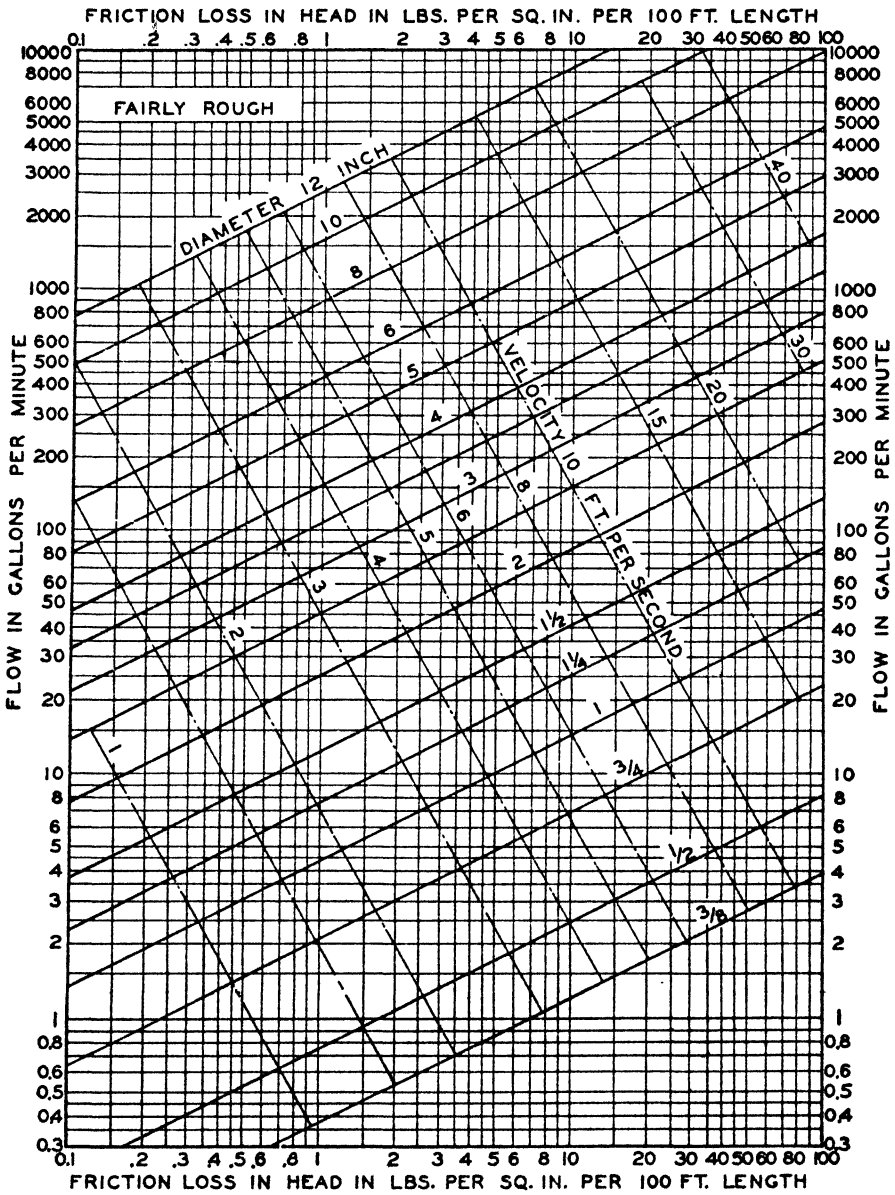

FIG. 3. FLOW CHART FOR FAIRLY ROUGH PIPE

Estimated pressure losses for pipe fittings and valves in terms of equivalent pipe length are shown in Table 3.

The pressure loss, in pounds per square inch, caused by the difference in elevation between the street main and the highest fixture may be obtained by multiplying the difference in elevation in feet by 0.43.

Example 1. Assume: a minimum street main pressure of 55 psi; a height of topmost fixture above street main of 50 ft; a developed pipe length from water main to highest fixture of 100 ft; a total load on the system 50 fixture units; and that the water closets are flush-valve operated. Find the required size of supply main.

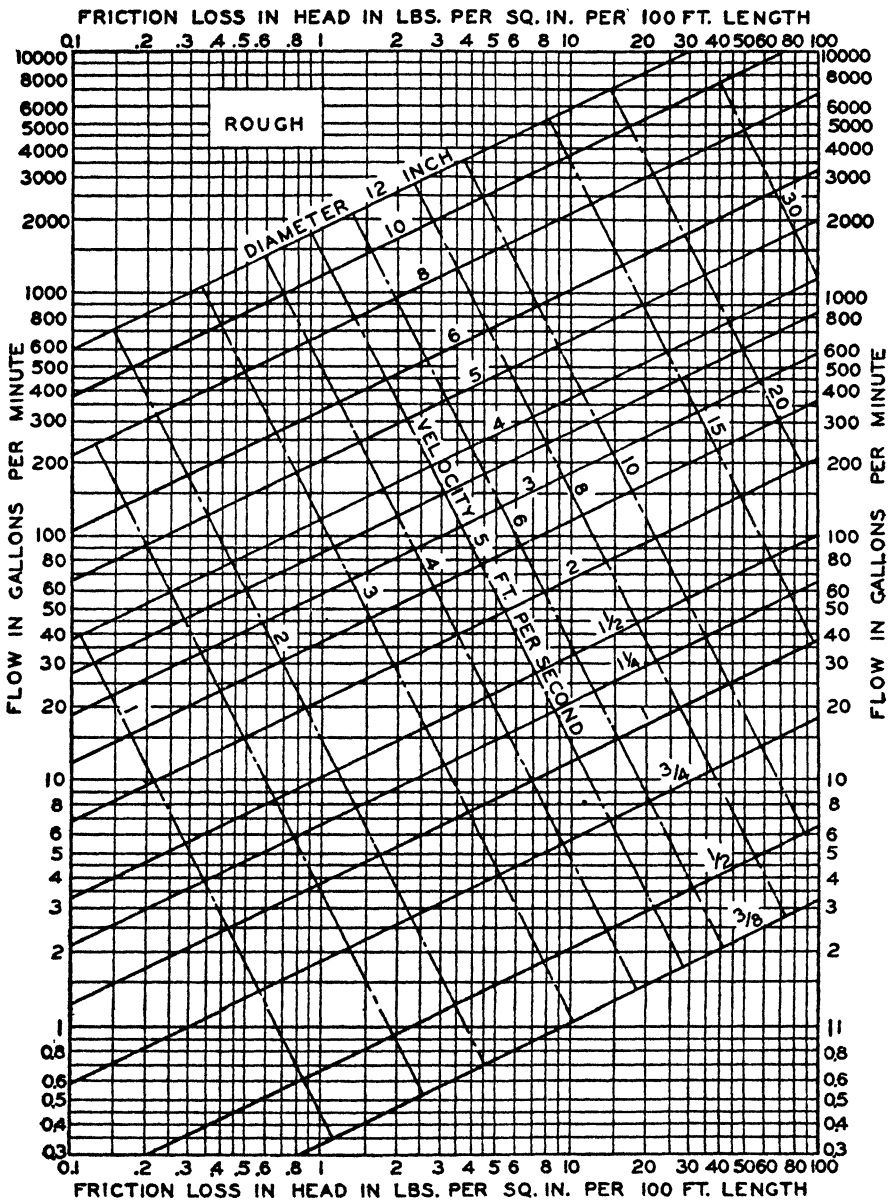

FIG. 4. FLOW CHART FOR ROUGH PIPE

From Fig. 2 the estimated peak demand is found to be 51 gpm. From Table 2 it is evident that several sizes of meters would adequately measure this flow. For a trial computation choose the 1½ in. meter. From Fig. 6 the pressure drop through a 1½ in. disc-type meter for a flow of 51 gpm is found to be 6.5 psi.

Then the pressure drop available for overcoming friction in pipes and fittings is $55 - (15 + 50 \times 0.43 + 6.5) = 12$ psi.

At this point it is necessary to make some estimate of the equivalent pipe length of the fittings on the direct line from the street main to the highest fixture. The exact equivalent length of the various fittings cannot now be determined since the pipe sizes of the building main, riser, and branch leading to the highest fixture are not known as yet, but a first approximation is necessary in order to make a tentative selection of pipe sizes.

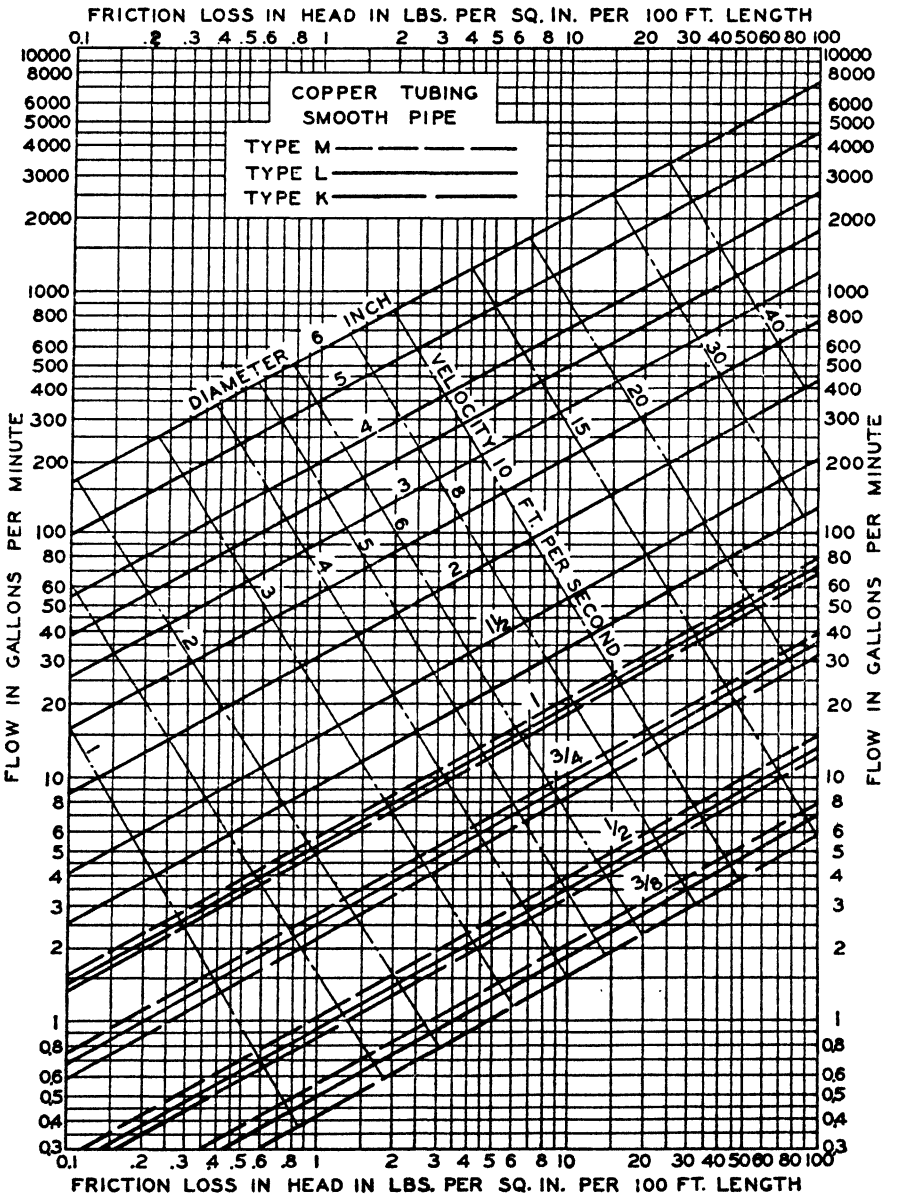

FIG. 5. FLOW CHART FOR COPPER TUBING

If the computed pipe sizes differ from those used in determining the equivalent length of pipe fittings, a recalculation will be necessary, using the computed pipe sizes for the fittings. For the purposes of this example assume that the total equivalent length of the pipe fittings is 50 ft.

Then the permissible pressure loss per 100 ft of equivalent pipe is $12 \times 100/(100 + 50) = 8$ psi.

Assuming that the corrosive and caking properties of the water are such that Fig. 3 for fairly rough pipe is applicable, a 2 in. building main is found adequate.

The sizing of the *branches* of the building main, the *risers*, and *fixture branches* follow the principles outlined. For example, assume that one of the branches of the building main carries the cold water supply for 3 water closets, 2 bath tubs, and 3 lavatories. Using

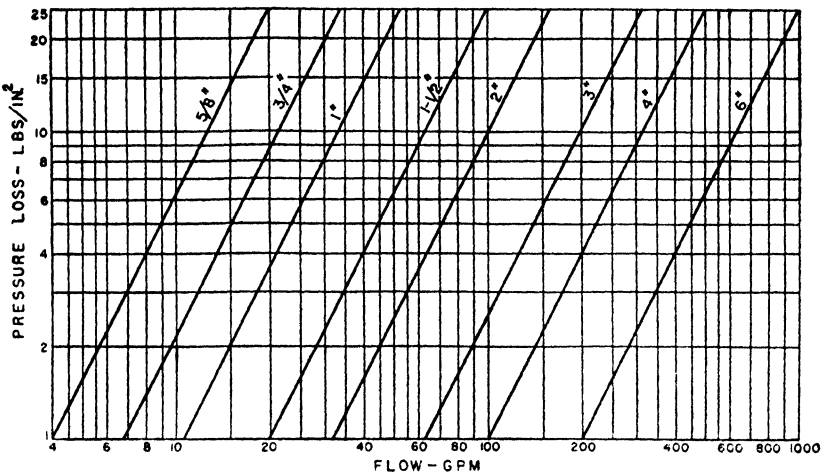

FIG. 6. PRESSURE LOSSES IN WATER METERS

the permissible pressure loss of 8 psi per 100 ft, the size of branch determined from Table 1 and Figs. 1 and 3 is found to be 1½ in. Items entering the computation of pipe size are given in Table 4.

The principles involved in sizing either up-feed or down-feed systems are the same. The principal difference in procedure is that in the down-feed system the difference in elevation between the house tank and the fixtures provides the pressure required to overcome pipe friction.

The water demand for hose bibbs or other large demand fixtures taken off the building main is frequently the cause of inadequate water supply to the upper floor of a building. This robbing of upper floor fixtures of water may be prevented by sizing the distribution system so that the pressure drops from the street main to all fixtures are the same. It is good practice to maintain the building main of ample size (not less than 1 in. where possible) until all branches to hose bibbs have been connected. Where the street main pressure is excessive and a pressure reducing valve is used to prevent water hammer or excessive pressure at the fixtures, it is frequently desirable to connect hose bibbs ahead of the pressure reducing valve.

HOT WATER SUPPLY PIPING

It is common practice to provide circulating piping in all hot water supply systems in which it is desirable to have hot water available continuously at the fixtures. In average sized and small residences and systems, in which the piping from the heater to the fixtures is short, return circulating piping is generally omitted in order to reduce installation cost and to reduce heat loss from the piping, particularly during periods of no water demand.

TABLE 4. COMPUTATION OF BRANCH SIZE IN EXAMPLE 1

FIXTURES NO. AND KIND	FIXTURE UNITS (FROM TABLE 1 AND NOTE C)	DEMAND (FROM FIG. 2) GPM	PIPE SIZE (FROM FIG. 3) IN.
3 flush valves	3 x 6 = 18		
2 bath tubs	¾ (2 x 2) = 3		
3 lavatories	¾ (3 x 1) = 2.25		
Total	23.25	38	1½

The hot water supply may be distributed by either an up-feed or down-feed piping system. Three common methods of arranging the circulating lines are shown in Fig. 7. Although the diagrams apply to multi-story buildings the arrangements (*a*) and (*b*) are sometimes used in residential designs.

A check valve should be provided in the run-out from each return riser to prevent temporary reversal of flow in the piping when a faucet is open. Proper air venting of a circulating system is extremely important, particularly if gravity circulation is employed. In Fig. 7 (*a*) and (*b*) this is accomplished by connecting the circulating line below the top fixture supply. With this arrangement, air is eliminated from the system each time the top fixture is opened.

Where an overhead supply main is located above the highest fixture as in Fig. 7 (*c*), an automatic float type air vent is installed at the highest

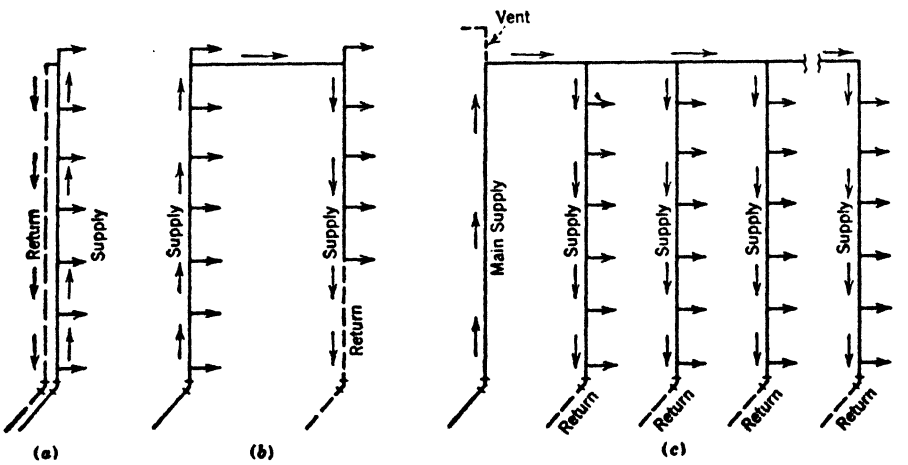

FIG. 7. METHODS OF ARRANGING HOT WATER CIRCULATION LINES

point of the system or a fixture branch is connected to the top of the main where air venting is desired and then dropped to the fixture outlet.

It is sometimes necessary to make an allowance for pressure drop through the heater when sizing hot water lines, particularly where instantaneous hot water heaters are used and the available pressure is low.

The principles involved in the sizing of the hot water supply pipes are the same as those for the sizing of cold water supply lines. For small and medium sized installations a ¾-in. hot water return will be ample. For larger installations the size of the hot water return may be computed from considerations of the heat losses in the hot water piping[8]. A throttling valve should be placed in the hot water return pipe so that the rate of circulation may be adjusted.

Where the hot water piping system is exceedingly long, a water circulator is frequently installed and controlled from an immersion thermostat, in the return line, set to start and stop the pump over approximately a 20 F deg temperature range.

STORAGE CAPACITY AND HEATING LOAD

In estimating the size of hot water storage tank required and the heating capacity to be provided either from the boiler or from an inde-

pendent domestic hot water heater, it is necessary to know the total quantity of water to be heated per day, and the maximum amount which will be used in any one hour, as well as the duration of the peak load.

In cases where the requirements for hot water are reasonably uniform, as in residences, apartment buildings, hotels, and the like, smaller storage capacity is required than in the case of factories, schools, office buildings, etc., where practically the entire day's usage of hot water occurs during a very short period. Correspondingly, the heating capacity must be proportionately greater with uniform usage of hot water than with intermittent usage where there may be several hours between peak demands during which the water in the storage tank can be brought up to temperature. As a general rule it is desirable to have a large storage capacity in order that the heating capacity, and consequently the size of the heater, or the load on the heating boiler, may be as small as possible.

TABLE 5. ESTIMATED HOT WATER DEMAND PER PERSON FOR VARIOUS TYPES OF BUILDINGS

TYPE OF BUILDING	HOT WATER REQUIRED AT 140 F	MAX. HOURLY DEMAND IN RELATION TO DAY'S USE	DURATION OF PEAK LOAD HOURS	STORAGE CAPACITY IN RELATION TO DAY'S USE	HEATING CAPACITY IN RELATION TO DAY'S USE
Residences, apartments, hotels, etc.	40 gal per person per day	1/7	4	1/5	1/7
Office buildings	2 gal per person per day	1/5	2	1/5	1/6
Factory buildings	5 gal per person per day	1/3	1	2/5	1/8
Restaurants $0.50 meals $1.00 meals $1.50 meals	1.5 gal per meal 2.5 gal per meal 4.5 gal per meal			1/10	1/10
Restaurants 3 meals per day		1/10	8	1/5	1/10
Restaurants 1 meal per day		1/5	2	2/5	1/6

In estimating the hot water which can be drawn from a storage tank it should be borne in mind that only about 75 per cent of the volume of the tank is available, as by the time this quantity has been drawn off the incoming cold water has cooled the remainder down to a point where it can no longer be considered hot water.

Where steam from the heating boiler is used to heat domestic hot water, the computed load on the boiler should be increased by 4 sq ft EDR (equivalent direct radiation) for every gallon of water per hour heated through a 100 F rise. The actual requirement is $(100 \times 8.33)/240 = 3.48$ sq ft per gallon of water heated 100 F. The value of 4 allows for transmission losses, etc.

There are two ways in common use of estimating the hot water requirements of a building; first, by the number of people and second, by the number of plumbing fixtures installed. Where the number of people to be served is known or can be reasonably estimated, the data in Table 5 may be used.

Example 2. From Table 5, a residence housing five people would have a daily requirement of $5 \times 40 = 200$ gal per day, and a maximum hourly demand of $200 \times 1/7 = 28.5$ gal. The heater should have a storage capacity of $200 \times 1/5 = 40$ gal and a heating capacity of $200 \times 1/7 = 28.5$ gal per hour.

The conditions given in Example 2 may be cited as average. It is possible to vary the storage and heating capacity by increasing and decreasing one over the other. Such a condition is illustrated in Example 3.

Example 3. Assume an apartment house housing 200 people. From the data in Table 5: Daily requirements = 200 × 40 = 8000 gal. Maximum hours demand = 8000 × ¼ = 1140 gal. Duration of peak load = 4 hr. Water required for 4-hr peak = 4 × 1140 = 4560.

If a 1000 gal storage tank is used, hot water available from the tank = 1000 × 0.75 = 750. Water to be heated in 4 hr = 4560 − 750 = 3710 gal. Heating capacity per hour = 3710/4 = 930 gal.

If instead of a 1000 gal tank, a 2500 gal tank had been installed, the required heating capacity per hour would be $\frac{4560 - (2500 \times 0.75)}{4}$ = 671 gal.

Table 6 may be used to determine the size of water heating equipment from the number of fixtures. To obtain the *probable maximum demand* multiply the total quantity for the fixtures by the Demand Factor in line 11. The heater or coil should have a water heating capacity equal to this *probable maximum demand.* The storage tank should have a capacity equal to the *probable maximum demand* multiplied by the storage capacity factor in line 12. Example 4 will illustrate the procedure.

Example 4. Determination of heater and storage tank size for an apartment building from number of fixtures.

60 lavatories	× 2	=	120 gal per hour
30 bath tubs	× 20	=	600 gal per hour
30 showers	× 75	=	2250 gal per hour
60 kitchen sinks	× 10	=	600 gal per hour
15 laundry tubs	× 20	=	300 gal per hour
Possible maximum demand		=	3870 gal per hour
Probable maximum demand	= 3870 × 0.30	=	1161 gal per hour
Heater or coil capacity		=	1161 gal per hour
Storage tank capacity	= 1161 × 1.25	=	1450 gal

METHODS OF HEATING WATER

Hot water may be heated either by the direct combustion of fuel, by an intermediate carrier such as steam or hot water, or by electrically heated surfaces. The simplest method is to have the fire on one side of a metal barrier and water on the other. In such a method if the water surfaces of heat transfer are small, and if the water carries a heavy proportion of precipitable salts, the water passages may soon clog and then burn out. A familiar example of such trouble is the water back of the firebox in the kitchen stove or the pipe coil inserted into the firebox of a warm air furnace or small boiler. The critical water temperature, at which the lime, magnesia, etc. collect on hot surfaces, varies with the character and proportions of the solids, but generally such deposits are not a serious trouble with water temperatures lower than 140 F.

Coal-burning direct-fired water heaters may be constructed of cored cast-iron sections or of steel. In some cases the external appearance of the cast-iron sections is the same as in heating boilers, but internally the cores are changed to enable the sections to withstand the city water pressure. In small capacity water heaters, efficiency is not considered so

important as low first cost and ability to maintain a fire at a low rate of combustion, and consequently such heaters are generally built with a *dry* section or fire-brick lining at the base of the fire-pot to prevent too much chilling of the fuel. While mud and scale will eventually clog the water ways of any direct-fired heater, increased life may be obtained by providing a three-way cock in the return line between the heater and the bottom of the storage tank, so that water can be blown through the heater or the tank separately at full line pressure to clean out loose sediment. Clean-out openings in the bottom of the heater are advantageous if used by operators of water heaters for periodic cleaning out of sediment.

Oil-burning direct-fired water heaters usually are of steel and operate with higher flame temperature and better efficiency than commensurate sized coal-burning heaters. They have the same tendency as coal boilers

TABLE 6. HOT WATER DEMAND PER FIXTURE FOR VARIOUS TYPES OF BUILDINGS

Gallons of water per hour per fixture, calculated at a final temperature of 140 F

	APARTMENT HOUSE	CLUB	GYMNASIUM	HOSPITAL	HOTEL	INDUSTRIAL PLANT	OFFICE BUILDING	PRIVATE RESIDENCE	SCHOOL	Y.M. C.A.
1. Basins, private lavatory	2	2	2	2	2	2	2	2	2	2
2. Basins, public lavatory	4	6	8	6	8	12	6	....	15	8
3. Bathtubs	20	20	30	20	20	30	....	20	....	30
4. Dishwashers	15	50-150	..	50-150	50-200	20-100	...	15	20-100	20-100
5. Foot basins	3	3	12	3	3	12	....	3	3	12
6. Kitchen sink	10	20	..	20	20	20	...	10	10	20
7. Laundry, stationary tubs	20	28	....	28	28	....	....	20	....	28
8. Pantry sink	5	10	...	10	10	..	....	5	10	10
9. Showers	75	150	225	75	75	225	....	75	225	225
10. Slop sink	20	20	....	20	30	20	15	15	20	20
11. Demand factor	0.30	0.30	0.40	0.25	0.25	0.40	0.30	0.30	0.40	0.40
12. Storage capacity factor*	1.25	0.90	1.00	0.60	0.80	1.00	2.00	0.70	1.00	1.00

*Ratio of storage tank capacity to probable maximum demand per hour.

to *lime up*, and the water passages should be large in cross-section and accessible for periodic cleaning.

Gas-burning direct-fired water heaters may be of the instantaneous or storage type. Instantaneous heaters are generally constructed of spiral water tubes of copper around which the products of combustion circulate upward from high capacity burners. Storage-type heaters may include in one unit an insulated storage tank, a combustion chamber, flues, burner equipment, and controls, or may consist of a separate storage tank and external direct-fired water heater, which may be a so-called *side-arm* heater for small capacity or a gas-fired boiler for larger capacity. Gas boilers used for direct hot water supply must be able to withstand the city water operating pressure. While direct-fired gas heaters are used generally for residences and small installations of 100 gal storage capacity or less, indirect heaters are recommended for larger installations.

Electric water heaters for domestic hot water supply are described in the section Heating Domestic Water by Electricity in Chapter 30.

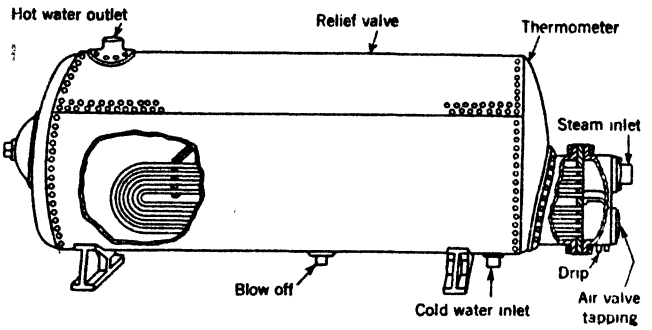

FIG. 8. INDIRECT WATER HEATER

In the indirect method either steam or hot water is used for heating the water. With steam the water to be heated is preferably circulated around the outside of the steam tubes which are submerged within a tank. A typical indirect heater using steam is shown in Fig. 8. The coils usually are of copper and are *U*-shaped to permit expansion and contraction. The shell may be of steel, copper, or with a special inside protective lining. Where straight heating tubes are used, one end of the tube is usually expanded into a *floating* head to take care of expansion. The coils should be capable of easy withdrawal for inspection and for removal of scale. Instead of steam the heating medium may also be hot water inside the tubes.

Another method of transferring heat from a heating boiler to the domestic water is illustrated in Fig. 9. The water heater is generally a cast-iron shell within which there is located a spiral copper coil. Hot water from the boiler circulates inside the shell and around the coil and returns to the boiler, while domestic water from the storage tank circulates inside the coil. The storage tank should be installed with the bottom of the tank as far above the boiler as possible. Horizontal storage tanks smaller than 18 or 20 in. diameter are not recommended because of the difficulty of preventing the hot and cold water from mixing, and especially is this an important consideration when large quantities of water are withdrawn. In Fig. 10 the heat transfer surface is placed inside the boiler instead of in a separate vessel, but otherwise the operation is

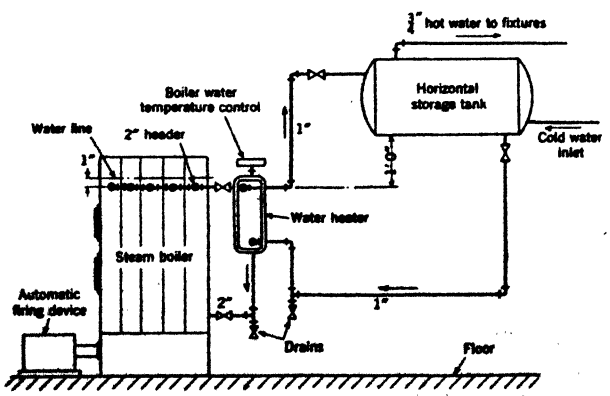

FIG. 9. INDIRECT WATER HEATER MOUNTED ON SIDE OF BOILER

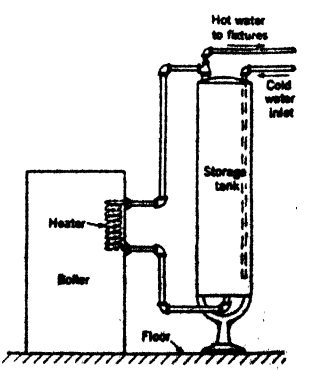

FIG. 10. INDIRECT WATER HEATER PLACED IN BOILER

similar to that of Fig. 9. This arrangement with vertical tank is commonly used for small domestic installations.

Sometimes the heating element is located inside of the larger type fire tube boilers and small residential boilers. In this case the heat transfer surface is in the form of a number of straight copper tubes with rear U bends or a floating head, inserted through a special opening in the boiler. While the coil may be located in the steam space above the water line of a steam boiler, it operates more satisfactorily when below the water line since clogging of the water tubes may thereby be delayed. This method is widely used without storage tanks since the intimate contact and efficient circulation of the water in this arrangement permit the utilization of the heat stored in the water of the boiler. A thermostatic three-way mixing valve is frequently used to maintain a uniform temperature of the hot water supply to the plumbing fixtures.

In order to reduce clogging by precipitated solids, water heating plants sometimes develop steam in a closed circuit, transferring the heat through a tubular heater to the domestic water. The water in the primary heater, exposed to the high temperature of the fire, is repeatedly used and hence has no appreciable tendency to deposit scale, while the domestic water, heated by steam at a much lower temperature than that of the fire, also exhibits a much reduced tendency to precipitate dissolved salts.

COMPUTING AREA OF HEAT TRANSMITTING SURFACE

The area of the inside surface of a heating coil may be determined from Equation 1.

$$A = \frac{Q \times 8.33\ (t_2 - t_1)}{U \times t_m} \qquad (1)$$

where

A = surface area of coil, square feet.

Q = quantity of water heated, gallons per hour.

t_2 = hot water outlet temperature, degrees Fahrenheit.

t_1 = cold water inlet temperature, degrees Fahrenheit.

U = coefficient of heat transmission, Btu per (hour) (square foot) (degree Fahrenheit logarithmic mean temperature difference).
For copper or brass coils $U = 240$ (steam) and 100 (hot water).
For iron coils $U = 160$ (steam) and 67 (hot water).

t_m = logarithmic mean of the difference between the temperature of the heating medium and the average water temperature and is *approximately*:

$$t_s - \left[\frac{(t_2 + t_1)}{2}\right]$$

t_s = temperature of the heating medium, degrees Fahrenheit.

Equation 1 may be used to check the heating coil ratings under temperatures other than those stated in the manufacturer's published ratings.

Example 5. What area of copper transfer surface will be required to heat 70 gal of water per hour from 40 to 180 F with boiler water at 220 F?

$$t_m = \left[220 - \frac{(180 + 40)}{2}\right] = 110 \qquad A = \frac{70 \times 8.33\ (180 - 40)}{100 \times 110} = 7.42 \text{ sq ft.}$$

For instantaneous submerged heaters the surface required will depend upon (1) the velocity of water in the tubes, (2) the boiler water temperature, (3) the inlet water temperature, (4) the outlet water temperature, (5) the cleanliness of the coil surface, and (6) the condition of the boiler

TABLE 7. COEFFICIENT OF HEAT TRANSFER OF INSTANTANEOUS WATER HEATERS
U = Btu per (hr) (sq ft) (Fahrenheit degree logarithmic mean temperature difference)

Boiler Water Temperature	210	200	180
U	225	175	150

water surrounding the coil. If the heater is located in the water of an actively steaming part of a boiler the heat transfer may be twice as great as would be obtained if the water surrounding the coil were circulating slowly. Ratings of instantaneous water heating coils will therefore vary greatly depending upon the assumptions made regarding the conditions of operation. The values of the coefficient of heat transmission for instantaneous heaters shown in Table 7 are conservative.

For a coil in which heat is transferred from steam to water the value of $U = 300\sqrt{v}$ may safely be used (v = velocity of water in feet per second).

The rate of heat transfer between steam or water as the carrier and the domestic water is influenced by the rate of movement of both the carrier and the water which receives the heat. For this reason, where the transfer occurs from heating system water to domestic water, it is good practice to install a circulating pump to insure rapid movement of the boiler water.

In view of the high condensation rates obtained when steam is used with gravity circulation from the boiler, as when there is a sudden demand followed by an inflow of cold water, the bottom of a steam heating transfer element always should be at least 30 in. above the boiler water line, and the steam and condensate return pipes should be of liberal size. Otherwise water hammer and reduced capacity may result due to imperfect drainage of condensate.

When connecting a transfer-type hot water heater below the water line of a cast-iron steam boiler having vertical sections, there should be a separate tapping for water circulation into every section of the boiler, as shown in Fig. 9, unless the boiler has large top nipple ports providing inter-sectional circulation. If the top nipples are entirely within the boiler steam space, no internal circulation occurs between sections and steaming may occur in sections not connected to the heater and further the unconnected sections will not deliver any heat to the heater.

CONTROL OF SERVICE WATER TEMPERATURE

Coal-fired boilers are usually controlled by an immersion thermostat located in the heated water, which opens or closes draft dampers at the boiler to adjust the rate of fuel combustion. With oil or gas-fired boilers the immersion thermostat controls the oil burner or the automatic gas valve. The gas pilot flame usually burns continuously. With electric heaters the immersion thermostat operates a switch on the source of energy.

When steam or hot water is the medium for heating the water in the tank, an immersion thermostat is used to control a valve in the steam or hot water supply line. In small residence installations, using water as the carrier, a combined immersion thermostat and butterfly valve in one simple fitting may be installed in the transmitting circuit to prevent overheating of the service water.

In residences heated by pump circulated hot water, the house temperature is controlled by operating the circulating pump intermittently, while domestic hot water is warmed by transfer from the house boiler,

independent of the pump operation. The domestic water is heated from the heating boiler the year 'round. Under such an arrangement, to prevent overheating the house by thermal circulation when the pump is not running, it is usual to insert a weighted check-valve in the house heating main, so that no circulation to the house heating system can occur unless the pump operates. In summer the fire may be controlled to maintain a boiler water temperature lower than when heating and generally about 20 F warmer than that desired in the domestic hot water system.

In buildings which have restaurants it is generally desirable to install two separate service hot water systems so that water at about 180 F minimum may be available for dish washing, while water at 140 F maximum may be used for lavatory and bath purposes.

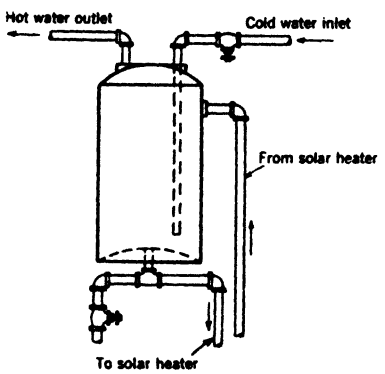

FIG. 11. SOLAR HEATER TANK CONNECTIONS

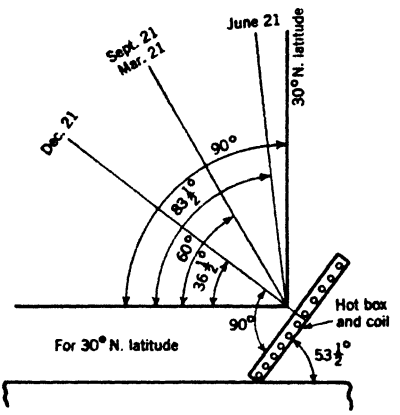

FIG. 12. SOLAR HEATING COIL INCLINATION

The immersion thermostat in a hot water storage tank should be located no higher than the center of the tank, and possibly should be even closer to the bottom since water in a tank stratifies proportionally to the temperature. When hot water is removed, the cold water entering to replace it quickly reduces the temperature in the lower parts of the tank.

SOLAR WATER HEATERS

Solar heaters utilize the energy of the sun for heating hot water. The successful operation of such heaters requires the availability of sunshine practically every day in the year, which has limited their use to Florida and the southern portions of California. When supplemented with some other means of gas, coal or, oil water heating, solar heaters may be used in climates where sunshine may be more or less intermittent. They have been used in summer homes as far north as Chicago. When properly installed and proportioned, solar water heaters render satisfactory service especially in climates where the outside temperatures are high and extremely hot water is not necessarily desirable. Such installations consist essentially of a storage tank, heating coil, and hot box. The coil is installed in the hot box and is arranged to circulate water to and from the storage tank. The advantage in the use of this type of heater is the fact that it requires no fuel. The same materials should be used for the coil,

TABLE 8. SUGGESTED SOLAR HEATER DESIGN DATA[a]

DESIGN ITEM	BASED ON RATE OF 30 GAL PER DAY PER PERSON								BASED ON RATE OF 40 GAL PER DAY PER PERSON							
No. of Occupants in Residence	1	2	3	4	5	6	7	8	1	2	3	4	5	6	7	8
Hot Water Used at Night, gal per person	15	15	15	15	15	15	15	15	20	20	20	20	20	20	20	20
Hot Water Used at Night, gal total	15	30	45	60	75	90	105	120	20	40	60	80	100	120	140	160
Retained in Tank, 25 per cent, gal	4	8	11	15	19	23	27	30	5	10	15	20	25	30	35	40
Tank Capacity Required, gal	20	40	59	75	94	113	130	150	25	50	75	100	125	150	175	200
Hot Water Used During Day, gal	15	30	45	60	75	90	105	120	20	40	60	80	100	120	140	160
Total Water to be Heated:																
Gal per 8 hr period	35	70	104	135	169	203	235	270	45	90	135	180	225	270	315	360
Gal per hour	4.5	9	13	17	21	26	29	34	6	12	17	23	28	34	39	45
Copper Coil Required:																
Surface area, sq ft	25	50	75	100	121	145	168	192	32	64	96	128	160	192	224	256
Equivalent length 1 in. coil, ft	100	200	300	400	484	580	664	768	128	256	384	512	640	768	896	1024
Box Size:																
Area, sq ft	25	50	75	100	121	145	168	192	32	64	96	128	160	192	224	256
Width, ft	4	6	7	8	9	10	10	11	4	6	8	9	10	11	12	12
Length, ft	6	8	11	12.5	13.5	14.5	16.5	17.5	8	10	12	14	16	18	19	21

[a] Sun Effect and the Design of Solar Heaters, by H. L. Alt (A.S.H.V.E. TRANSACTIONS, Vol. 41, 1935, p. 131).

circulation lines, and tank. A copper coil is more efficient in absorbing heat in the box but galvanized iron or steel may be substituted depending on the local water conditions, cost, and other considerations.

The storage tank must be able to store sufficient heated water for the night period of about 16 hours when the coil is not functioning or is operating under such poor sun conditions as to make its heating effect negligible. Due to the fact that the *no sun* period includes the night period when little or no hot water is used, an available storage of 50 per cent of the average daily usage is considered adequate. Since about 25 per cent of stored hot water cannot be drawn out of a storage tank before the incoming cold water reduces the temperature of all of the water in the tank to an unsatisfactory point for usage, the equation for calculating the storage capacity of the tank becomes:

$$S = \frac{Q \times 0.50}{0.75} = 0.666Q \qquad (4)$$

where

S = storage capacity of tank, gallons. Q = average daily usage, gallons.

Thus for a family of four persons using an average of 40 gal of hot water per person per day the size of the tank would be 4 persons x 40 gal x 0.666 or 106 gal, and the nearest standard size of tank to this theoretical capacity would be used. The tank should be well insulated to prevent undue loss of heat during the 16-hour period when the coil is inoperative, and it should be located as high as possible in the building (under the peak of the roof if such exists) so as to secure a maximum circulation head from the coil. The hot water supply to the house, as shown in Fig. 11, is located at the top of the tank, which serves to vent the air from the tank through the hot water faucets as fast as it accumulates.

The coil should be of the return-bend type, square or slightly rectangular in form, and should have the pipes running east and west, with the coil on the south side of the building where it can receive the full sun

effect all day long without shadows from the building itself or from adjacent obstructions such as trees or other structures. The coil should be placed as low as possible in relation to the storage tank level, such as on a porch roof, the roof of a one-story extension or, if necessary, even on the ground. Both the coil and the circulation lines should be designed to facilitate the circulation flow as much as possible, using long radius copper fittings or recessed galvanized iron fittings to match the materials of the coil, circulation lines, and tank. The coil should be inclined as shown in Fig. 12 so that the north end is raised above the south end to secure an angle with the horizontal of about 53 deg. This will result in the inlet end of the coil being on the south side (or bottom) and the outlet end being on the north side (or top). This will satisfy conditions along the 30 deg N latitude which includes the portions of Florida and Southern California where these heaters are most frequently used.

The hot box is usually constructed of wood on the four sides and bottom, and is insulated. Over the top of the box glass sash are placed and the box should be constructed as near air-tight as possible. The interior surfaces should be painted white to reflect the heat, while the coil should be painted black to absorb the heat. The box need not be deeper than necessary to house the coil and to protect it from the weather.

The addition of a light gage copper plate on the bottom of the box to which the pipe of the coil is soldered, for good metallic contact, will add to the amount of heat received by the coil due to the fact that this plate will receive all of the sun rays which fail to directly strike the coil. The heat from this source is transmitted to the coil through the plate instead of by heating the air surrounding the coil and from which only part of the heat enters the coil, the balance being transmitted through the glass sash.

Design data given in Table 8 may be used with some judgment in selecting the size of solar heater coil and box for a particular application. These data are based on consumptions of 30 and 40 gal of hot water per day per person.

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Chapter 51

CORROSION AND WATER FORMED DEPOSITS CAUSES AND PREVENTION

Definitions, Classification and Characteristics of Water, Causes and Prevention of Scales and Sludges, Causes and Prevention of Slimes, Under-Water Corrosion, Atmospheric Corrosion, Buried Pipe Lines, Handling Water Treating Chemicals, Legal Regulations

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THE surfaces of heating and ventilating equipment that are in intimate contact with water sometimes are affected by the chemical characteristics of the contacting waters to such extent that prohibitive amounts of insoluble materials are formed or corrosion ensues at an insufferable rate. To avoid or to correct such troubles, it is desirable that heating and ventilating engineers have a general appreciation of industrial water chemistry. The principal purpose of this chapter is to provide those criteria by which the average engineer may judge whether a problem is one that will yield to rather simple remedies or will require the skill of an experienced water technologist.

DEFINITIONS

The following definitions for water-formed deposits, corrosion, and closely allied terms have been proposed:

Water-Formed Deposits. A water-formed deposit [1] is any accumulation of insoluble material derived from water or formed by the reaction of water upon surfaces in contact with water.

Deposits formed from or by water in all of its phases may be further classified as scale, sludge, corrosion products, or biological deposits.

Scale. Scale [1] is a deposit formed from solution directly in place upon a confining surface. It is a deposit which will retain its physical shape when mechanical means are used to remove it from the surface on which it is deposited. Scale, which may or may not adhere to the underlying surface, is usually crystalline and dense, frequently laminated, and occasionally columnar in structure.

Sludge. Sludge [1] is a water-formed sedimentary deposit. It usually does not cohere sufficiently to retain its physical shape when mechanical means are used to remove it from the surface upon which it deposits. Sludge is not always found at the place where it is formed. It may be hard and adherent and baked to the surface on which it has been deposited.

Biological Deposits. Biological deposits [1] are water-formed deposits of biological organisms or the products of their life processes. Biological deposits may be microscopic in nature, such as slimes, or macroscopic, such as barnacles or mussels. Slimes are usually composed of deposits of a gelatinous or filamentous nature.

Corrosion. Corrosion [2] is destruction of a metal by chemical or electrochemical reaction with its environment. In the corrosion process, the reaction products formed may be soluble or insoluble in the contacting environment. Insoluble corrosion products may deposit at or near the attacked area or be carried along and deposited at considerable distance from the attacked area.

Corrosivity. Corrosivity [3] is the capacity of an environment to bring about destruction of a metal by the process of corrosion. Corrosivity is a property of the environment, but it has no significance until the metal in question is specified.

CLASSIFICATION AND CHARACTERISTICS OF WATER

For industrial use there is no accepted conventional classification of water. Rather, each industry usually develops a body of ideas applicable to its own water problems [4]. For heating and ventilating engineers, it is

perhaps most convenient to distinguish between mineralized waters and condensates.

Mineralized Waters

All the waters found in streams, wells, lakes, and the ocean are mineralized. The same is true of all municipal supplies even though they may have been *treated*. For a given area ground waters are likely to be more highly mineralized than are surface waters. Conversely, surface waters are more likely to be contaminated with municipal sewage and trade wastes. Virtually all mineralized waters also contain biological organisms.

Mineralogical Characteristics. The character and amount of extraneous inorganic materials—including deleterious gases—dissolved and sus-

TABLE 1. MINERAL ANALYSES TYPIFYING COMPOSITION OF WATERS AVAILABLE AND USED INDUSTRIALLY IN THE USA

SUBSTANCE	UNIT	LOCATION OR AREA[a,b]								
		(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)
Silica	SiO_2	2	6	12	37	10	9	22	14	.....
Iron	Fe	0	0	0	1	0	0	0	2	.....
Calcium	Ca	6	5	36	62	92	96	3	155	400
Magnesium	Mg	1	2	8	18	34	27	2	46	1,300
Sodium	Na	2	6	7	44	8	183	215	78	11,000
Potassium	K	1	1	1	.....	1	18	10	3	400
Bicarbonate	HCO_3	14	13	119	202	339	334	549	210	150
Sulphate	SO_4	10	2	22	135	84	121	11	389	2,700
Chloride	Cl	2	10	13	13	10	280	22	117	19,000
Nitrate	NO_3	1	...	0	2	13	0	1	3	.....
Dissolved Solids	.....	31	66	165	426	434	983	564	948	35,000
Carbonate Hardness	$CaCO_3$	12	11	98	165	287	274	8	172	125
Non-Carbonate Hardness	$CaSO_4$	5	7	18	40	58	54	0	295	5,900

[a]All values are parts per million of the unit cited to nearest whole number (see Reference 5).

[b]Numbers indicate location or area as follows:

(1) Catskill supply—New York City
(2) Swamp Water (Colored) Black Creek, Middleburg, Florida
(3) Niagara River (Filtered) Niagara Falls, New York
(4) Missouri River (Untreated) Average
(5) Well Waters—Public Supply—Dayton, Ohio—30-60 ft.
(6) Well Water—Maywood, Illinois—2090 ft.
(7) Well Water—Smithfield, Va.—330 ft.
(8) Well Water—Rosewell, N. Mexico
(9) Ocean Water—Average

pended therein describe the mineralogical charateristics of any water. Revealing such information is the function of a mineralogical chemical analysis.

The analyses in Table 1 disclose the composition of the public water supplies used by about 45 per cent of the total population of the cities, in the United States, having more than 20,000 inhabitants[5].

All values recorded are in terms of parts per million *. This is the approved standard terminology for reporting the results of mineral analyses[6]. Values reported in the other terms commonly used may be converted into the standard form by using the conversion factors listed in Table 2.

Data for dissolved gases or pH values have been omitted in Table 1 because even waters of the same mineral contents may vary widely in these respects. Unpolluted natural waters usually have pH values within the range 5 to 8, depending upon their *free* CO_2 contents. Polluted

* Parts per million are hereinafter abbreviated ppm. A part per million signifies a unit weight of material per million unit weights of the solution.

TABLE 2. CONVERSION FACTORS FOR WATER ANALYSES

TO CONVERT	INTO	MULTIPLY BY
Grains per U. S. gallon	ppm	17
Grains per Imperial gallon	ppm	14¼
Grams per liter	ppm	1000
Mg per liter	ppm	1

waters, which include those derived from wells or swamps in marshy ground, may have pH values well below 5.

Biological Characteristics. The slime-forming organisms are mostly lower plants, grouped by botanists into the Phylum Thallophyta. This group is distinguished by the absence of leaves, roots, or stems from the mosses, ferns, and seed plants which comprise the three other phyla of the plant kingdom.

The Thallophyta (see Table 3) are divided into algae, which can synthesize chlorophyll for the production of sugar, and the fungi which lack chlorophyll and must therefore secure already synthesized carbohydrates.

All Thallophyta are of universal distribution and many of them are slime forming. Of the five divisions of algae, only three (the green, the blue-green, and the diatoms) are found in fresh water. Of the five divisions of fungi, all may occur in fresh water, the principal slime formers being indicated in Table 3.

The methods of analysis commonly used in the sanitary examination of a water have, as their principal object, to identify and count pathogens.

Most slime-forming organisms are not pathogens. When a water is subjected to a biochemical analysis for the purpose of evaluating its slime producing characteristics, tests, widely different from sanitary bacteriological tests, must be made. Tests upon the water itself are seldom satisfactory, and true indications of the sliming characteristics of a water can only be determined for the analysis of deposits on surfaces having the temperature close to the temperature of the final design equipment. The results of such a test are commonly reported in the manner illustrated in Table 4.

Condensates

All condensates result from the chilling of water vapor. Such chilling may result from natural causes, thus producing *dews, sweats, rain, and*

TABLE 3. PRINCIPAL SLIME FORMERS

PHYLA	ROUGH DIVISION OF PHYLA
Algae	Single celled, sometimes forming slimy sheets. Many celled in either sheets or fronds.
Fungi	*Bacteria* (Schizomycetes) frequently forming slimy surface coatings. *Slime Molds* (Myxomycetes) forming slimy sheets as one stage of their life history. *Sac fungi* (Ascomycetes) of which one division, the yeasts, occasionally form slimy aggregates. The alga-like fungi (*Phycomyceles*) and the stalked fungi (Basidomycetes) rarely form slimes but their filaments may hold together the slimes of other organisms.

TABLE 4. PLANT WATER SUPPLY EXAMINATION

WATER SUPPLY—	200 ft deep well—average water temperature 53 F—water is producing a brown stain in plumbing fixtures.
SAMPLE—	The sample was scraped from the surface of the shell and tube condenser of #2 Freon Compressor on the meat chilling room. The sterile sample bottle was filled one-half with deposit and the balance with circulating water. No preservative was added—pH at time of collection was 7.4.

ANALYSIS REQUIRED—

MACROSCOPIC	[√]	MICROSCOPIC	[√]
BACTERIOLOGICAL	[√]	ORGANIC CONTENT	[√]

PROBLEM—	A 25-ton Freon—12 Compressor has head pressure about 10# higher than during initial operation, without change in water temperature. Deposits have been observed on heat exchanger surfaces. It is desired to know the nature of these deposits and if they are the cause of this increased head pressure.
MACROSCOPIC EXAMINATION—	Heavy brown flocculent material settles rapidly in clear water. pH—7.3 Odor—woody, mouldy.
MICROSCOPIC EXAMINATION—	INORGANIC MATERIAL—small amount white crystals. AMORPHOUS MATERIAL—small amount—brown. IRON BACTERIA—profuse growth of crenothrix—(Photo usually included).
CULTURAL EXAMINATION—	SABOURAUD'S AGAR 1. Aerobic gram positive spore-forming rod with mucoid sheaths (Photo usually included). 2. Short gram negative coccibacilli (Photo usually included).
TOTAL COUNT	100,000 organism/cc.

ORGANIC CONTENT (by WEIGHT, DRY BASIS)—60%

DISCUSSION—	The presence of common slime-forming organisms in the deposit combined with high organic content indicates that the deposit is bacterial in origin. Heat transfer reductions would be caused by such a deposit. These deposits, combined with crenothrix, can cause corrosion of both ferrous and non-ferrous metals.
RECOM-MENDATIONS—	It is recommended that the water be treated at the suction side of the deep well pump with chlorine in quantities sufficient to maintain a free chlorine residual of 1.0 ppm at the discharge of the shell and tube cooler. This treatment can be scheduled on an intermittent basis.

snow, or from artificial causes, as in steam condensing equipment, producing condensate or return water.

In the heating and ventilating field, the biological characteristics of condensates are likely to be of concern *only* where the condensate is used as cooling water in recirculating systems. The deleterious gas contents of condensates, however, very often create serious corrosion troubles.

The data in Table 5 typify the chemical composition of the atmosphere in rural and metroplitan areas, and of stack gases when various types of common fuels are used. The curves in Fig. 1 disclose the solubility of the major deleterious gases present in such atmospheres in otherwise pure water, when the partial pressure of the gas is one pound per square inch absolute.

The most common deleterious gases entrained by steam are oxygen and

carbon dioxide. In rare instances, hydrogen sulphide, sulphur dioxide, or ammonia are present.

In most steam condensing equipment[7, 8], the non-condensable gases entrained with steam accumulate so that the amount present in the vapor space is several hundred times higher than in the incoming steam and, the amount dissolved in the condensate may therefore approach, or even exceed for short periods, the amount entrained by the steam.

CAUSES AND PREVENTION OF SCALES AND SLUDGES

Scales may be formed on surfaces of equipment in contact with water, and sludges in the body of the water, by the separation from the water of dissolved or suspended solids. According to the nature of a particular piece of equipment and the method of its operation such separation may be promoted by one or more than one, of several factors:

a. The concentration of solids may be increased by the evaporation of water.

b. The dissolved solids may be rendered less soluble in the water by changes in temperature.

c. Conditions may favor the decomposition of unstable compounds with the formation of less soluble compounds.

TABLE 5. DATA TYPIFYING THE DELETERIOUS GAS CONTENT OF DIFFERENT ATMOSPHERES

Name of Gas	Chemical Formula	Air				Flue Gases					
		Rural		Metropolitan		Bitum. Coal		Fuel Oils		Natural Gas	
		% by Volume	Partial Pressure psia	% by Volume	Partial Pressure psia	% by Volume	Partial Pressure psia	% by Volume	Partial Pressure psia	% by Volume	Partial Pressure psia
Oxygen	O_2	21	3.143	21	3.143	2	0.299	7	1.048	10	1.497
Carbon Dioxide	CO_2	0.03	0.004	0.06	0.009	15	2.245	13	1.946	10	1.497
Sulphur Dioxide	SO_2	None	None	0.003	0.004	0.07	0.010	0.03	0.004	0.0001	0.0015

Figs. 2 and 3 show that the solubilities of both calcium carbonate and calcium sulphate decrease with the rising temperature within a moderate range of temperatures. Surfaces transferring heat into water, such as condensers and coolers, are more susceptible to scale and sludge formation than are the cold parts of the same system using the same water.

The most common of the unstable soluble salts are the bicarbonates of calcium, magnesium, and occasionally iron. Under conditions favoring the removal of carbon dioxide, as when the water is strongly aerated or when it is boiled, the bicarbonates are readily converted to the relatively insoluble carbonates (or, in the case of iron in the presence of oxygen, ferric hydroxide or oxide may be formed). Conversely, carbonates are readily converted to the more soluble bicarbonate by the addition of carbon dioxide or other acidic materials. This explains the increase in the apparent solubility of calcium carbonate at decreasing pH values (increasing concentration of hydrogen ion) shown in Fig. 2, the carbonate really going into solution largely as bicarbonate.

It is sometimes desired to evaluate the tendency in a particular water toward the separation of calcium carbonate, which may be desirable as a means of establishing a corrosion-resistant film on metal surfaces, or in

other circumstances may be undesirable because of the impedance of the calcium carbonate film to heat transfer. This tendency is indicated approximately by the Langelier Index [9], which is obtained by subtracting the actual pH of a particular water from the pH at which it is estimated precipitation of calcium carbonate would just begin. This estimate may be made by the use of Fig. 4.

There are various expedients which may be employed for avoiding or mitigating difficulties due to scales:

a. The water may be treated before use to remove elements such as calcium, magnesium, and iron, which form relatively insoluble compounds. In the various softening processes this removal of these elements is accompanied by the addition of other elements, particularly sodium, the compounds of which are relatively soluble.

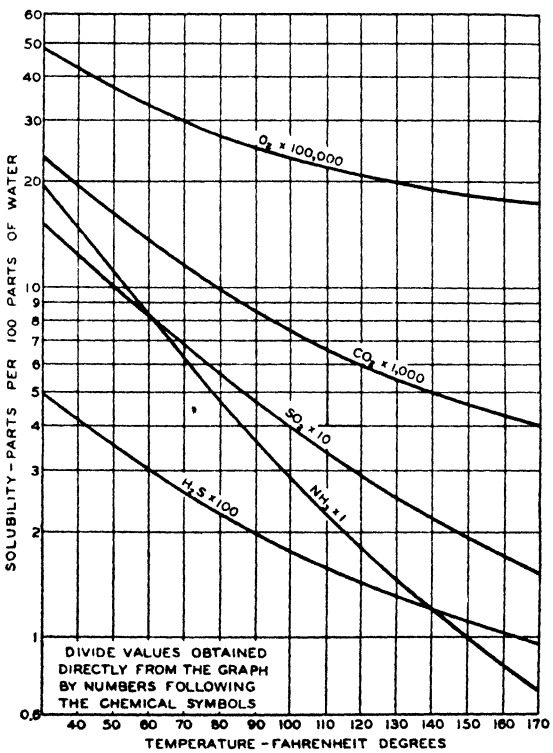


FIG. 1. SOLUBILITY OF GASES AT PARTIAL PRESSURE OF 1 PSI

b. The water may be treated within the equipment to promote the separation of dissolved solids as sludges, rather than as scale which is in most cases more objectionable.

c. The increase in total solids due to the evaporation of water may be controlled by the displacement, continuously or intermittently, of some of the used water by fresh supply.

d. Substances, such as the polyphosphates, having the property of inhibiting the precipitation of calcium carbonate from solutions supersaturated with it, may be added.

e. The pH of the water may be lowered (hydrogen ion concentration raised) to reduce the tendency for precipitation of carbonate. This is permissible only to such an extent as will not cause a serious increase in rate of corrosion.

The choice of the best expedient must be made for each type of equipment and will be affected by local considerations.

Once-Through Equipment and Closed Recirculating Systems

Where abundant supplies of water are available at low cost, the cooling water may pass through the equipment once, undergoing a slight rise in temperature. Little difficulty from scale should be experienced in this case unless the carbonate hardness is more than 200 ppm, or the water has been treated to induce incipient calcium carbonate precipitation. Closed recirculating systems in which the water is cooled indirectly, as in radiators, and returned to the equipment, should usually be little troubled with scale. However, in both once-through and closed recirculating systems, slimes may cause trouble.

If there is some tendency for scaling, it may usually be prevented by the addition of small amounts, about 5 ppm or less, of polyphosphate [10]. Alternately, a minor lowering of pH by the addition of carbon dioxide or sulphuric acid may be effective if this is permissible from the standpoint of corrosion.

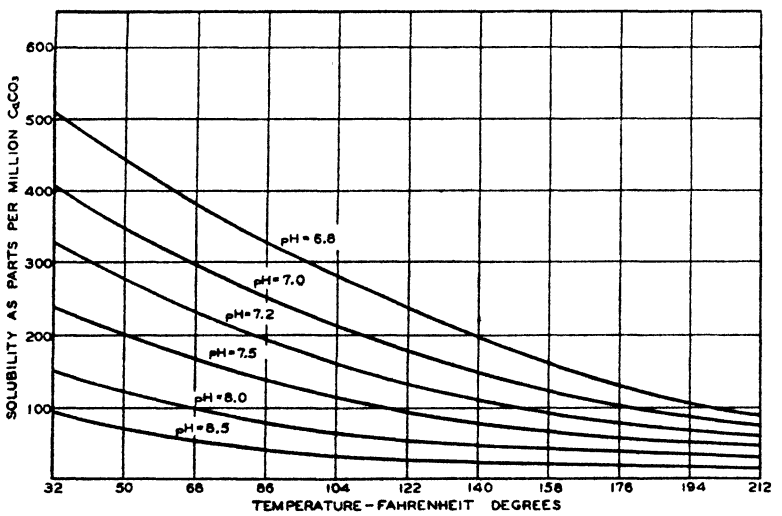


FIG. 2. SOLUBILITY OF CALCIUM CARBONATE IN DISTILLED WATER CONTAINING CARBON DIOXIDE

(*pH Values at Approximately 78 F*)

Fig. 2 Adapted from (1) Ind. & Eng. Chem., 20 (1928) 1197—by Baylis. (2) J.A.C.S. 50 (1929) 2086—Frear & Johnson.

Open Recirculating Systems

Where water from condensers and similar equipment is passed through a spray pond or cooling tower and then returned to the equipment, there is an increase in the concentration of solids because of the evaporation of some of the water into the cooling air, and, moreover, the aeration removes carbon dioxide. Both factors promote the tendency to deposit scale. If the conditions are particularly adverse, it may be necessary to subject the water to a softening treatment before use, this being the more feasible because of the reduced water requirement in such a recirculating system. When this is not practicable, or when the tendency to scale formation is only moderate, a considerable improvement may be effected by the addition to the water of organic compounds such as gelatine, glucosates, dextrine, and tannin which tend to prevent precipitated material from

forming adherent scales. In systems of this kind, the loss of liquid as spray from the cooling towers or spray ponds may limit adequately the final concentration of solids in the cooling water. If not, provision must be made for sufficient purging of used water.

Heating Systems

In hot water heating systems or in steam heating boilers where all condensate is returned, troubles from scaling should not be severe. If necessary, sodium phosphate or sodium carbonate may be added to the water to prevent the formation of adherent calcium sulphate scale.

Boilers and High Temperature Equipment

Where temperature exceeds 250 F, complete softening of the water is the only practical method for minimizing sludge formation. This is

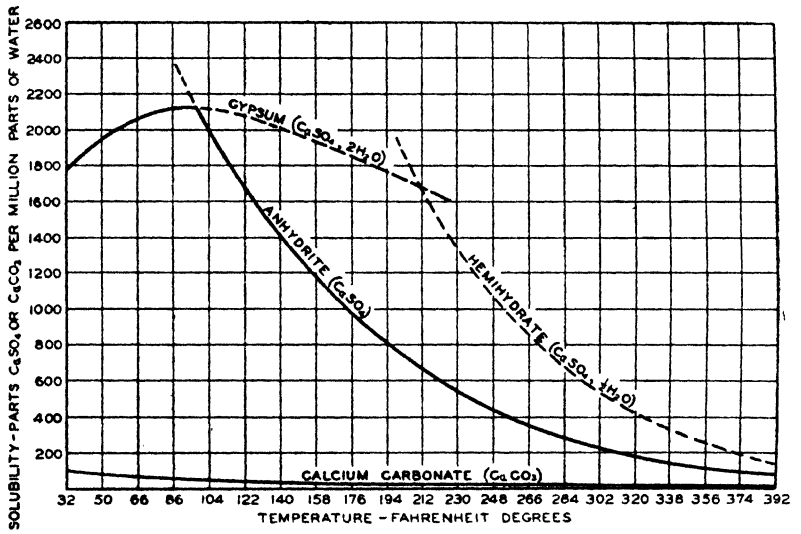


FIG. 3. SOLUBILITY OF CALCIUM SULFATE AND OF CALCIUM CARBONATE FOR COMPARISON

(*$CaCO_3$ in Equilibrium with Normal CO_2 Content of the Atmosphere*)

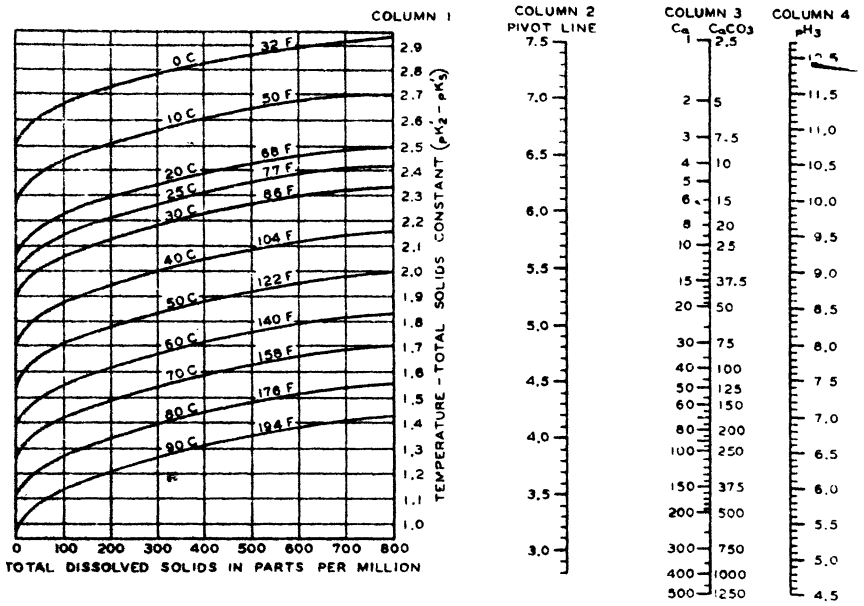
Fig. 3 Adapted from Bul. No. 15, Univ. of Mich. "Formation and Properties of Boiler Scales" by E. P. Partridge.

usually accomplished by artificial or natural zeolites (called also ion-exchange materials) or by hot-process precipitation softeners.

In boilers operating at pressures above 100 psi virtually all the calcium, magnesium, silica, iron, and manganese salts entering with the feed water are potential scale or sludge formers.

In low pressure boilers (100-250 psig), the formation of adherent calcium sulphate (anhydrite) scales is most to be feared. Such deposits form on the *hottest* evaporative surfaces. It is a material of low heat conductivity. Even a layer of egg shell thickness may so impede the rate of heat transfer as to bring about over-heating of the metal.

The ortho-phosphates of sodium are most frequently used to prevent sulphate scales. The concentration of phosphate required is such as to cause the precipitation of calcium phosphate as sludge, thus keeping the boiling water under-saturated with respect to calcium sulphate. To a



(Data required for determining pH saturation.

(1) Total alkalinity, as parts per million of $CaCO_3$.

(2) Calcium in parts per million.

(3) Total dissolved solids, in parts per million.

(4) Temperature, in degrees centigrade, at which pH saturation is desired.

FIG. 4. GRAPH AND NOMOGRAM FOR DETERMINATION OF pH SATURATION BY LANGELIER'S FORMULA

(Applicable within pH Range 7.0—9.5)

[a]Based on article in Oct. 1936 issue of American Water Works Association Journal and later corrections for Tables 2 and 4. Prepared for Charles P. Hoover of the Columbus, Ohio, Water Softening and Purification Plant by M. L. Riehl.

Instructions for Using Chart:

1. **Knowing temperature and total dissolved solids, find temperature and total solids constant on Col. 1.**
2. **Align this constant with given value of calcium on Col. 3 of Chart, then locate point on Col. 2 of Chart (Pivot Line).**
3. Align this point on Pivot Line with given alkalinity on Col. 5; read pH saturation on Col. 4.

Saturation index is pH actual minus pH saturation.

E. G.—pH actual. pH saturation. Saturation index.

7.6	8.1	−0.5 (corrosive)
8.4	7.8	+0.6 (scale forming)

lesser extent, sodium carbonate (called also soda ash and sal soda) is also used. Most of the effective boiler compounds contain either phosphates or soda ash, or both. Certain organic materials and colloids are sometimes found to minimize scale formation. Where chemicals are introduced directly into the boiler in amounts adequate to prevent scale, sludge is formed in amounts proportionate to the calcium and magnesium salts entering with the feed water. To prevent troublesome accumulation of this sludge, as well as soluble salts, as evaporation occurs some *blowdown* of boiler water is necessary.

CAUSES AND PREVENTION OF SLIMES

A water containing slime-producing organisms will produce prohibitive amounts of slime *only* when the conditions of use are such as to propagate their life processes. Whenever sufficient food material from normal water or from air-borne dust combines with optimum temperature conditions such as exist on cooling surfaces and air washers, serious quantities of slime will be produced.

TABLE 6. COMMON CHEMICALS USED FOR SLIME CONTROL

CHEMICAL	TRADE NAME	PHYSICAL STATE*
Chlorine	Chlorine	Gas
Hypochlorites	Calcium Hypochlorites Sodium Hypochlorites	Crystalline
Chlorinated Phenols Sodium -	Chlorophenylphenate Tetrachlorophenate Pentachlorophenate	Briquettes Briquettes Briquettes
Potassium Permanganate	Permanganate of Potash	Crystalline
Copper Sulphate	Blue Vitriol	Crystalline

*As shipped.

Some natural well waters do not contain sufficient foods to support luxuriant slime growths. Algae which require light for carrying on their life processes are likely to cause difficulty in cooling towers and other areas where sunlight is abundant. The ordinary slime-forming bacteria are capable of using a wide variety of nitrogenous and cellulose material as food sources. These bacteria thrive best under dark conditions such as exist in condensers and other heat transfer surfaces. Other organisms capable of causing similar difficulties use such a wide variety of food material as algae [11], iron compounds [12], and inorganic sulphates [13].

At present, the use of toxic chemicals and irradiation are the two general means employed in slime control. The value of ultra violet light, used so broadly in the beverage industry, is somewhat in dispute.

Anti-fouling paints have been developed and are fairly satisfactory for the prevention of the growth of micro-organisms such as *barnacles* and *mussels*, but these paints must be renewed at frequent intervals and are not applicable to inaccessible areas such as the inside of pipe lines and cooling towers. Satisfactory *anti-sliming* paints have *not* been found.

Names and other pertinent data relating to some of the more common chemicals used in slime control, are shown in Table 6.

Chlorine is the only chemical to which is attributed the ability to de-

stroy slime-forming organisms. The others are presumed to poison marine organisms, most of which *recover* when the chemical is not used regularly.

While chlorine is the most generally used chemical, others may occasionally prove to be more practicable. Choice of the chemical is conditioned largely by the design and operation of the system.

Open Recirculating Systems

In spray ponds and cooling towers of the open type, light-loving algae growths are likely to cause blocking of the distribution piping and troughs. These organisms are most troublesome in areas accessible to sunlight. Algae slimes are usually stringy in character.

In open recirculating systems, continuous use of small quantities of chlorine is generally most satsifactory. In once-through systems, where large quantities of water are used, intermittent treatment a few times each day will usually result in satisfactory slime removal and chemical economies.

Neither the phenols nor copper sulphate may be used for the removal of slime already formed. For this purpose, chlorine gas is used. After being cleaned, the other chemicals may be used to prevent the reestablishment of slime in the system. The removal of green algae from a cooling tower should never be used as an indication that the true slime-forming organisms on heat exchanger surfaces have been removed. The more resistant slime formers, which so materially reduce heat transfer efficiency, will often be unaffected by treatment which completely eliminates algae.

Closed Once-Through Systems

In equipment where light is excluded, slime formations are due to fungi. Usually, they predominate on the heat exchange surfaces. Bacteria form thick, soft slime. Yeasts and molds form tough rubbery slimes. Chlorine and hypochlorite solutions, fed intermittently, are used to prevent such slimes.

UNDER-WATER CORROSION

When deleterious substances are present in water, the corrosivity of the solution is increased in proportion to the amount of deleterious substances present, the temperature, and usually the rate of flow of the solution over the metal surfaces. There are other relevant factors, but their influence in general is subordinate to those mentioned. Dissolved oxygen, acid gases, and chloride salts are the corrosion accelerators most frequently encountered.

Neutral and slightly alkaline waters saturated with air, corrode iron at a rate about triple that for the same water free of air. Hot water containing oxygen will corrode iron at a rate three to four times that for the same water when cold.

Corrosion of iron decreases as the pH of water solutions increases and practically ceases at a pH of 11. If the metal contains film forming agents, such as chromium, nickel, and silicon or if the water contains inhibitors such as silicates and chromates, corrosion may in some instances be minimized.

Cold Water Services

Where water from municipal supplies is used industrially in a closed system with little or no increase in temperature, it is seldom necessary or

feasible to treat the water to reduce its corrosivity. When it is mandatory, the addition of caustic soda to *maintain* a pH over 11 *plus* the addition of sufficient sodium sulphite to maintain a residual of over 100 ppm (as Na_2SO_3) usually suffices to prevent serious troubles. However, in some cases the cost may be prohibitive.

When the use of sodium sulphite or a comparable chemical for oxygen removal is prohibited, as in potable waters, the addition of small amounts of lime to maintain a Langelier Index (See Fig. 4) of 0.5 or more may prove helpful.

In systems exposed to the atmosphere, as for example air washers or storage tanks, both laboratory [14] and field tests [15] have shown that the addition of alkalies to maintain a pH greater than 8.5, plus the addition of other chemicals that produce protective films on the metal surface, will measureably decrease corrosion. Sodium dichromate, sodium silicate, and tri-sodium orthophosphate have been shown to be effective film formers in the order mentioned.

Caustic soda is usually used to raise the pH value, and sodium dichromate is most often employed as a film former in industrial waters. In old systems, not previously inhibited, about 500 ppm of sodium dichromate are usually maintained at the start. After two or three months and in new systems, a residual of about 300 ppm of dichromate usually proves effective. When insufficient dichromate is employed, pitting is sometimes accelerated. Aeration does not impair the efficiency of dichromates, but does deplete the caustic soda concentration.

In large industrial systems, the use of vacuum deaeration has been shown to be effective [16]. In small systems, the equipment required can seldom be justified, economically.

Soft water, as for example the effluent from zeolite softeners, is likely to be several times more corrosive to iron than hard waters. In small installations, the use of copper or brass pipe usually is a practical expedient. Cement lined pipe and tanks suitably resist attack.

Where the water contains slime-forming organisms, especially those bacteria that thrive on iron, chlorination of the water is imperative to inhibit tuberculation and subsequent pitting.

Bitumastic paints, applied at *regular* intervals upon *well cleaned* surfaces, will measurably prolong the life of equipment handling cold waters.

Hot Water Services

As a usual thing, corrosion does not create important troubles when temperatures are maintained below 140 F.

In closed systems where little fresh water is introduced, such as in a hot water space heating system, corrosion is usually negligible because the oxygen released in heating the water is purged through the vents.

Where large amounts of fresh water are constantly entering and are being heated, the use of mechanical deaeration is the most universally satisfactory expedient to employ. Where the use of such equipment cannot be justified economically, anti-corrosive chemicals, and the use of corrosion resistant metals, are the more practical expedients to be used.

Treating Chemicals. Alkalies, such as lime and caustic soda, silicates of soda (water glass), the poly-phosphates of soda, sodium sulphite, and sodium dichromate are usually used. Organic compounds, such as the glucosates, dextrines, and tannins are sometimes used, but their value is

still a controversial matter. When any chemical is used, so many relevant factors are involved that it is always advisable to seek adequate technical counsel in inaugurating the treatment. Very often, where such precaution is not taken, new troubles are created that are more aggravating than the original difficulty [17].

Silicate of soda is used to protect iron, lead, and brass water pipe [18]. For most waters, a solution of $Na_2O;3SiO_2$ is recommended. Sodium silicate equivalent to about 10 ppm added silica, should be fed to the water for the first month after which it may be reduced to give 5 or 6 ppm added silica. Where careful control of the silicate feed is exercised, the water is not injured for domestic use by this treatment. The rate of corrosion of iron pipe has been reduced by 70 per cent and dezincification of brass pipe practically stopped by this simple treatment. The amount required and the effect are not the same in all waters.

Pipe Materials. Brasses with 60 to 67 per cent copper are dezincified in some corrosive waters and in certain localities are not much more service-

TABLE 7. QUANTITIES OF SODIUM DICHROMATE TO BE ADDED TO MAINTAIN INITIAL CONCENTRATION

SPECIFIC GRAVITY OF BRINE TO BE STRENGTHENED	LB SODIUM DICHROMATE PER 100 LB $CaCl_2$ ADDED
1.16	0.695
1.18	0.621
1.20	0.556
1.22	0.502
1.24	0.455
	LB OF SODIUM DICHROMATE PER 100 LB NaCl ADDED
1.12	1.79
1.14	1.47
1.16	1.32
1.175	1.18

able than galvanized iron or steel pipe. The zinc in brass pipes is leached out locally, leaving a plug of porous copper. The weakening of such pipe is especially noticeable under the threads. Dezincification is retarded by the use of silicate of soda (8 ppm added silica) [19].

In salt or fresh water, there is no material difference in rate of pitting of wrought iron, steel, low metalloid steels, or copper bearing steels. This is contrary to the relative performance of these metals in atmosphere.

Refrigerating Systems

Corrosion in refrigerating systems is confined to surfaces in contact with brines and/or those in contact with the refrigerant.

Brines. Refrigerating brines usually are comprised of sodium chloride, calcium chloride, or calcium and magnesium chlorides. The corrosivity of dilute brines is higher than their more concentrated solutions. The corrosivity of sodium brines, other conditions being fixed, is about 1.5 times greater than brines of the alkaline earth metals.

Brines are excellent electrolytes. Contact of dissimilar metals of wide potential differences when in contact with brines results in rapid corrosion by galvanic action.

The leakage of air, acid refrigerants, or both, accelerates the corrosivity of brines. Ammonia precipitates calcium and magnesium salts thus clogging the system at restricted points.

The addition of caustic soda and sodium dichromate to brine solutions to inhibit corrosion of iron is a more or less general practice. Sodium silicate and sodim phosphate are also used at times, but tests indicate they are not as effective as is sodium dichromate. It has been suggested [20] that 125 lb of sodium bichromate per 1000 cubic feet of calcium chloride brine, and 200 lb per 1000 cubic feet of sodium chloride brine be added to inhibit brines; that when salt or calcium chloride is added to "strengthen" brine, sodium dichromate also be added in the amounts shown in Table 7.

Refrigerants. The common refrigerants, except those of the hydrocarbon type, will attack the common metals and alloys if *moisture is present.* Even a very small amount of water may cause severe corrosion with certain refrigerants. The amount required need only be sufficient to produce a water film on the metal surface.

With the halogenated hydrocarbons, complete elimination of water is much to be desired. Where ammonia is used, copper and its alloys, aluminum and zinc, are attacked especially at elevated temperatures. When sulphur dioxide is used more than 50 ppm (0.005 per cent) of water will cause appreciable corrosion of virtually all the common materials.

Minimizing Condensate Corrosiveness

There are four expedients that may be utilized to minimize corrosion in steam condensate systems: (1) treatment of the boiler feedwater so as to eliminate deleterious gases entrained with the steam, (2) design of the condensing equipment to minimize dissolution in the condensate of the deleterious gases entrained with the steam, (3) chemical treatment of the condensate, (4) use of resistant metals.

Boiler Feedwater Treatment. Elimination of oxygen from boiler feedwater and, therefore, from the steam developed, can be accomplished either mechanically or chemically. In some steam generating stations, both expedients are employed.

Tests [21] have indicated that in small low-pressure heating boilers, where the boiler input contains less than about 50 ppm of carbonate hardness, the CO_2 in the steam can be controlled by adding calcium hydroxide to the boiler. In Fig. 5 are shown the equilibria conditions proposed for boilers operating at pressures up to about 5 psi gage. This expedient may *not* be used in higher pressure boilers, because of the possibilities of scale and sludge formations. In the latter, the only method used to date for treating the feedwater consists (a) in removing the alkaline earth salts, *i.e.*, softening (b) in subsequent acidulation followed by deaeration at temperatures near the atmospheric boiling point of water [22].

Design of Condensing Equipment. In the design of water heaters and comparable types of condensing equipment [23], it is possible to shift the accumulation of non-condensible gases to a location away from the condensate level and, subsequently, vent these gases to the atmosphere. Venting an amount of steam equal to about one-half per cent of the total steam entering the condenser is the optimum vent rate.

Venting, is of little practical value, when the CO_2 content of the incoming steam is below about 5 ppm. When the steam contains more than 5 ppm, venting provides a means of producing a condensate containing a

minimum of about 3 ppm. However, even as little as 3 ppm of dissolved CO_2 can produce active corrosion if large amounts of condensate are flowing.

Chemical Treatment of Condensate. Condensates containing comparatively large amounts of oil, are practically non-corrosive, due to the protective film provided by the oil. When oil is intentionally added to condensate[24], inadequate quantities may accelerate rather than decelerate corrosion on those surfaces not covered by the oil. Sodium silicate added to CO_2-bearing condensate has been shown to decrease, but not entirely prevent, corrosive action. It is not definite whether the protection afforded by silicate solutions is due to the establishment of a protective film on the metal surface or to neutralization of the CO_2 by the alkali in the silicate solution.

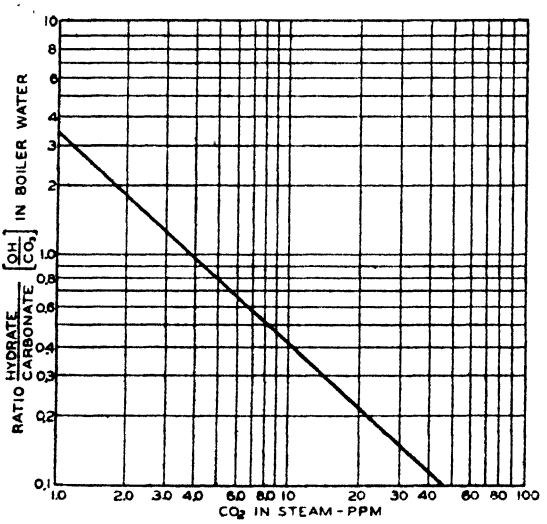


FIG. 5. RELATION OF HYDRATE/CARBONATE CONTENT IN *Hard* BOILER WATER AND CO_2 IN STEAM AT ABOUT 5 PSI OPERATING PRESSURE

(All analytical values are ppm by weight)

It has been postulated that ammonia[25], cyclohexylamine[26], ethylene diamine, and morpholine[27] will retard corrosion of condensate lines. Tests with benzylomine have also been reported[28]. Where copper and its alloys are involved, the use of alkaline inhibitors is believed inadvisable. The use of small amounts of sodium hexametaphosphate has been suggested too, but tests[29] indicate that this salt accelerates rather than decelerates, the rate of attack of steel by condensate containing CO_2 and oxygen. Whether chemical treatment of steam or condensate is feasible, must be determined not only upon the basis of the acuteness of corrosion troubles, but also upon the uses to which the steam or condensate are put.

Use of Resistant Metals. For economic reasons, the metals known to resist corrosion can seldom be used exclusively for condensate lines in any sizeable enterprise. Nevertheless, there may be instances where the use of a limited amount of the more costly, but resistant, materials can be justified. The data in Fig. 6 are the results of tests[30] designed to reflect the corrosion resistance of the more commonly used metals to attack by condensate containing oxygen and CO_2.

In contemplating the use of a resistant metal, as a section of a condensate line, it should be remembered that, if other conditions are *right*, corrosive attack will merely be transferred down stream in the system. Galvanic corrosion resulting from the contact of dissimilar metals in a condensate line seldom occurs. No paint or similar protective coating have thus far proven satisfactory. Tests of cement lined and vitreous lined pipe have shown the linings to be readily dissolved by hot condensates.

ATMOSPHERIC CORROSION

Most of the problems originated by atmospheric corrosion occur in connection with the fire-side of boilers and furnaces (including their flues and stacks), sewer vents, air ducts, coal and ash handling equipment. Usually such equipment is fabricated from common types of ferrous metals.

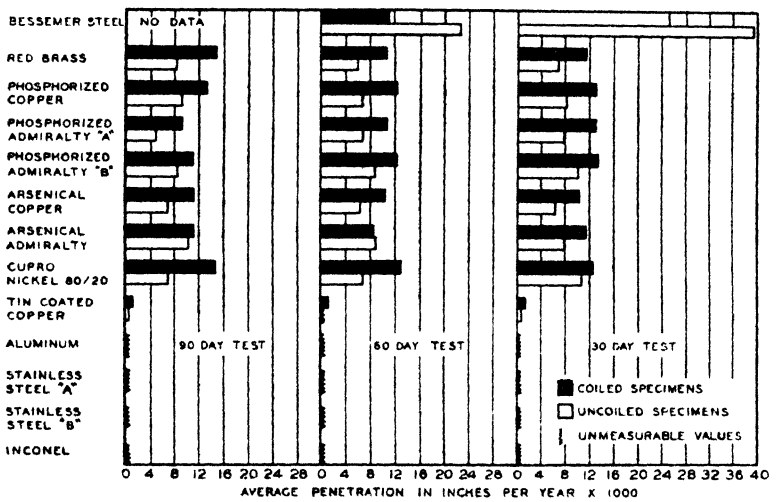


FIG. 6. COMPARATIVE CORROSION RESISTIVITY OF 10 MATERIALS EXPOSED TO CONDENSATE

Generally little or no atmospheric corrosion occurs at temperatures higher than the boiling point of water, because at such temperatures little or no condensate is formed. If it does form at the higher temperatures, only negligible amounts of carbon dioxide and oxygen, present in the atmosphere, will dissolve in the hot liquid but sulphur gases may dissolve and cause rapid attack. Oxygen, sulphur dioxide, sulphur trioxide, and carbon dioxide are the deleterious gases most frequently accountable for corrosion in moist atmospheres.

Coal Storage and Handling Equipment

Virtually all coals contain sulphur in the form of pyrite, and some moisture. In storage, the pyrite is likely to be decomposed by oxidization. Moisture dissolves the products of decomposition forming sulphurous and sulphuric acid. The acid solutions vigorously attack the supporting metal.

Rubber linings have been developed for coal chutes and bins that effectively resist corrosion and the abrasive action of the coal, but they are expensive[31]. Concrete linings for steel bunkers have also been effectively employed[32].

The use of high chromium steels is not always a sure cure, especially with coals treated with dust allaying agents high in chlorides.

Flues, Stacks, and Fire-side of Boilers

The surfaces of flues and boilers contacting the products of combustion, seldom experience corrosive attack when the equipment is in operation. Breechings, smoke hoods and canopies in contact with flue gas may, however, be subject to attack during the warming-up period of an appliance or when the rate of operation is so low that the temperature of the flue gas is below the dew-point. It is common practice to use cast-iron or acid resistant vitreous enameled steel in flue gas connections to appliances to prolong the life of these parts. The shut-down period when condensation of moisture occurs on the metal surfaces is usually the time when most damage is done [33]. In those sections of the stacks where flue gas temperature drops below the dew-point, corrosion is inevitable during operation.

It is clear that where long shut-down periods are anticipated, a practical method for mitigating corrosion is to clean the surface thoroughly and to provide adequate clean, dry air circulation to prevent condensation (See also Care of Idle Heating Boilers, p. 357, Chapter 18).

Protective coatings with organic binders are destroyed rather rapidly above 400 F because of the decomposition of the organic materials. The surfaces of metals whose temperature does not exceed 400 F, may be protected by periodically applying paints such as those specified in the following paragraphs entitled Air Ducts.

Air Ducts

The most practical method for protecting air duct surfaces made of steel from atmospheric corrosion is to apply protective paints. One of the most effective protective coatings is red lead paint.

Three coats of paint should be applied, of which the first two coats should be rust inhibitive paint such as red lead paint with the second coat tinted to a light brown color with carbon black, and the finishing coat may be red lead paint tinted to a black or brown color, black paint made according to Federal Specification TT-P-61, red iron oxide paint conforming to Federal Specification TT-P-31, or white or light tinted paint made according to Federal Specification TT-P-40.

Another paint which has had some use for priming iron and steel is zinc chromate paint.

Under some conditions, a chlorinated rubber base paint made according to Federal Specification TT-P-91 may be used for the finishing coat, particularly where the presence of highly corrosive gases or contact with strong alkaline water would injure the standard paints. Rubber base paints should be used only for the finishing coat over regular priming and second coats.

BURIED PIPE LINES

Lines that are cold and in intimate contact with the earth are corroded from the same causes as in mineral waters, but pitting is usually more intense due to variations in concentration of salts and oxygen in solution and presence of solid materials, such as cinder in contact with metal pipe. Galvanic currents induced by contact of certain dissolved constituents in the soil often act over a large area, and accelerate corrosion where they leave the pipe line.

Certain bacteria that thrive in the absence of oxygen have the power to obtain hydrogen and dissociate sulphates in the soil with a resultant production of hydrogen sulfide which attacks the iron to form iron sulphide. Other bacteria have preference for cathodic hydrogen and by removing it keep natural corrosion going on at a rapid rate.

Stray electric currents from electric power generating stations sometimes find their way into buried steel structures and do damage in proportion to the current density where the current leaves the metal to enter the ground.

Pipe Materials

Under many conditions where steel would be corroded, the use of corrosion-resistant metals other than steel may be desirable even if greater in first cost. Stainless steel, copper, red brass, and bronze will resist corrosion and may, at times, be used to advantage. Sheet lead linings are excellent to prevent corrosion, and lead pipe will resist corrosion both on the exterior and interior when used for buried pipe lines as well as for pipe for general purposes. Galvanized iron pipe will resist corrosion for various periods of time depending on the soil and how long the galvanized coating lasts. The zinc used for the galvanized coating is on the electrochemical protective side of the iron and the zinc is corroded and changed to zinc compounds before the iron is attacked. This accounts for the protection afforded by galvanized iron. Even if some protection is obtained, eventually the galvanized coatings are destroyed by chemical action and the corrosion of the steel begins.

Protective Coating

Protective coatings for buried pipe lines are in a class by themselves because of the unusual service conditions and because it is not possible to maintain them by recoating when necessary. Buried steel pipe lines have been protected against corrosion with considerable success by the use of very thick bituminous coatings applied in molten condition. The best results are obtained by applying the bituminous coatings over a standard priming coat such as red lead or a bituminous paint, and for long service it has been found that after the bituminous coatings are applied, a wrapping of asbestos fabric saturated with bitumens will prevent movement and displacement of the bituminous coatings and add greatly to the length of time.satisfactory protection will be maintained.

Cathodic Protection

Protection is obtained by rendering the structure cathodic to the surrounding water or soil by means of a controlled difference of potential. This method, which has proved satisfactory and economical on a number of gas and oil pipe lines underground, has also been applied with some success to the protection of the inside of water storage tanks and other structures that are in contact continuously with water. Protective coatings that insulate a large portion of the metal surface will reduce very materially the total amount of protective current that it is necessary to impress on bare anodic areas to arrest corrosion.

For each structure, it is necessary to determine or estimate the minimum current density required and design the anode or anodes so that the necessary protection can be obtained most economically. In water having relatively high electrical conductivity such as in sea water, this is comparatively easy compared with fresh water. In the latter, the composition

of the water is a major factor. It is therefore desirable to obtain an accurate estimate of the minimum current density required. The current is then controlled by the potential between the anode and the structure to be protected.

Rectifiers have generally proved to be the most practical means for supplying the necessary current for protection of surfaces in contact with neutral waters[34].

HANDLING WATER TREATING CHEMICALS

Virtually all the chemicals used in water conditioning are injurious if taken internally in large doses. Many also cause severe skin irritation. Thus, they should be handled with caution.

Caustic soda, lime, and concentrated sulphuric acid will burn the flesh. In addition, if mixed with small amounts of water, sufficient heat may be generated so that spattering occurs or the container becomes too hot to handle.

The chlorophenol compounds, even in the low concentrations used in water conditioning, have been reported[35] to produce dermatitis. Chromitch is not uncommon among workers handling chromates. The amines are said to be absorbed through the skin[36]. Morpholine is said to cause kidney and lung trouble when so absorbed.

Chlorine gas irritates the skin, eyes, and mucous membranes. Concentrations as low as 0.004 per cent by volume in air cause dangerous illness in 0.5 to 1 hour.

When relatively large amounts of the non-gaseous chemicals are to be handled, protective clothing, including goggles, should always be provided, and a shower head or its equivalent provided at or very near the point where the chemicals are mixed. *Chemicals should always be washed from the skin with large volumes of water.*

For the handling of chlorine and chlorinators, the U. S. Public Health Service[37] stipulates the following safety requirements:

1. Suitable gas masks and a small bottle of ammonia for testing for leaks should be kept at convenient points immediately outside the room or enclosure in which chlorine is being stored or is in use. Gas masks should be inspected at regular intervals and kept in serviceable condition. Note:—All purpose masks offer adequate protection only when the concentration of acid gases does not exceed two per cent—See "Safe Practises Pamphlet #64 National Safety Council".

2. Chlorinating equipment and cylinders of chlorine should be housed preferably in separate buildings above the ground level.

3. The room or building housing chlorinators in service should be maintained at a temperature above 60 F, but never in excess of the normal summer temperature. The cyclinders of chlorine should be shielded, where necessary, from excessive heat or cold. Direct heat should not be applied to cylinders of chlorine nor should hot water be poured over them or come in contact with the cylinder valve.

4. Adequate ventilation should be provided for all enclosures in which chlorine is being fed or stored.

5. All joints of tubing connecting chlorine cylinder and chlorinators should be kept absolutely tight and inspected frequently to insure tightness. Tubing should slope upward from the cylinder.

LEGAL REGULATIONS

In a number of states, the water used for humidification, even in industrial plants, is required to meet drinking water standards insofar as bacteriological quality is concerned. A ruling of the U. S. Department of

Agriculture, Meat Inspection Division prohibits the use of chromate in water used for air washing when the air later contacts foodstuffs[38].

There is an ever growing consciousness on the part of public health officials of the necessity for regulations to *protect* potable water supplies. Attesting this is an ordinance[39] now in effect in Detroit, Michigan, which stipulates in part:

"No physical connection shall be maintained between lines carrying city water and pipes, pumps, or tanks supplied from any other source. Where dual supplies are necessary or desired, lines carrying city water must be protected against back flow of polluted water by an *atmospheric gap*—Secondary supplies and emergency sources shall include: surface waters from rivers, lakes, ponds, lagoons, and reservoirs; well waters both deep and shallow; any supply of water which has been stored, held, or reserved after being used for industrial purposes; cooling water, or water which has in any way been treated, processed, or has been subjected or exposed to any contamination of a bacteriological or chemical nature; and water from any other source than the city supply."

The U. S. Public Health Service stipulates:

"Salts of barium, hexavalent chromium, heavy metal glucosides, or other substances with deleterious physiological effects, shall not be allowed in the water supply system."

The same agency recommends that the concentration of the substance hereinafter listed be held below the values cited:

Substance	Max. Concentration, ppm
Copper	3.0
Iron & Manganese (Total)	0.3
Magnesium	125.0
Zinc	15.0
Lead	0.1
Fluorine	1.0
Arsenic	0.05
Selenium	0.05
Phenols (Total)	0.001
Poly-phosphate of Sodium	10.0
pH Value @ 25C	10.6

The Board of Directors of the American Water Works Association has accepted these values as standard for *all* public water supplies in the United States[40]. While their action is not binding, prudence dictates that no form of treatment should be used that will result in raising the concentration of the substances listed above the value cited.

Since virtually all of the permissible chemicals used for scale slime, and corrosion control have deleterious, physiological effects if taken internally in *relatively large doses*, they should always be carefully *proportioned*. To insure this, the Detroit Ordinance stipulates that the chemical feeding device must have the following major characteristics:

"1. There shall be a visible means of checking the quantity of material being applied by the feeding device.

2. A water metering device, sealed to prevent tampering, shall be installed to measure the flow of water being treated.

3. The device shall be constructed so that in the event of back-flow or vacuums, the maximum amount of material that may be possibly back-siphoned from the device or any of its attachments or parts shall not exceed one fluid ounce.

4. Should there be a failure of the water metering device or the water supply, the feeding device shall automatically cease operating."

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Chapter 52

CODES AND STANDARDS

THE Codes and Standards listed in Table 1 represent accepted practice, methods, or standards prepared and accepted by the organizations indicated. They are valuable guides for the practicing engineer in determining test methods, ratings, performance requirements, and limits applying to equipment used in heating, ventilating, and air conditioning. Copies can usually be obtained from the organization listed in the reference column.

TABLE 1. CODES AND STANDARDS PREPARED AND ACCEPTED BY VARIOUS SOCIETIES AND ASSOCIATIONS

SUBJECT	TITLE	SPONSOR	REFERENCE
Air Conditioning	Code of Minimum Requirements for Comfort Air Conditioning (1938).	A.S.H.V.E. *A.S.R.E.*	A.S.H.V.E.
Air Conditioning (150,000 Btu/Hr or less)	Code and Manual for the Design and Installation of Warm Air Winter Air Conditioning Systems (1945).	*N.W.A.H. & A.C.A.*	*N.W.A.H. & A.C.A* No. 7
Air Conditioning (Above 150,000 Btu/Hr)	The Technical Code for the Design and Installation of Mechanical Warm Air Heating Systems (1942).	*N.W.A.H. & A.C.A.*	*N.W.A.H. & A.C.A.*
Airplane	Aeronautical Recommended Practice for Heating and Ventilating Airplanes (1943).	*S.A.E.*	*S.A.E.* ARP 85
Airplane	Aeronautical Recommended Practice for Internal Combustion Type Airplane Heaters (1945).	*S.A.E.*	*S.A.E.* ARP 143A
Attic Ventilation	Attic Ventilation Code (1946)	*P.P.M.A.*	*P.P.M.A.*
Boilers	I=B=R Testing and Rating Codes for Low Pressure Heating Boilers (1947).	*I.B.R.*	*I.B.R.*
Boilers	Net Square Feet Radiation Loads in 70 Deg Fahr, Recommended for Low Pressure Heating Boilers (1943).	*H.P. & A.C.C N.A*	*H.P. & A.C.C.N.A.*
Boilers	Net Load Recommendations for Heating Boilers.	*H.P. & A.C.C.N.A.*	*H.P. & A.C.C.N.A.*
Boilers	Standard and Short Form Heat Balance Codes for Testing Low Pressure Steam Heating Solid Fuel Boilers (Codes 1 and 2) (1929).	A.S.H.V.E.	A.S.H.V.E.
Boilers	A.S.H.V.E. Performance Test Code for Steam Heating Solid Fuel Boilers (Code No. 3) (1929).	A.S.H.V.E.	A.S.H.V.E.
Boilers	A.S.H.V.E. Standard Code for Testing Steam Heating Boilers Burning Oil Fuel (1932).	A.S.H.V.E.	A.S.H.V.E.
Boilers	A.S.H.V.E. Standard Code for Rating Steam Heating Solid Fuel Hand Fired Boilers (Revised April 1930).	A.S.H.V.E.	A.S.H.V.E.
Boilers	A.S.H.V.E. Standard Code for Testing Stoker-Fired Steam-Heating Boilers (1938).	A.S.H.V.E	A.S.H.V.E
Boilers	*A.S.M.E.* Boiler Construction Code for Low Pressure Heating Boilers.	*A.S.M.E.*	*A.S.M.E.*
Boilers (Miniature)	*A.S.M.E.* Miniature Boiler Code (1946).	*A.S.M.E.*	*A.S.M.E.*
Boilers	*A.S.M.E.* Boiler Construction Code (Combined Edition) (1946 with 1947 Addenda).	*A.S.M.E.*	*A.S.M.E.*
Boilers (Power)	*A.S.M.E.* Power Boiler Code, Including Rules for Inspection (1946 with 1947 Addenda).	*A.S.M.E.*	*A.S.M.E.*
Boilers (Power)	Suggested Rules for Care of Power Boilers (1946).	*A.S.M.E.*	*A.S.M.E.*
Boilers (Steel)	Steel Boiler Institute Rating Code for Commercial Steel Boilers and Residential Steel Boilers (1945).	*S.B.I.*	*S.B.I.*
Boilers (Steel)	Simplified Practice Recommendation for Steel Firebox Heating Boilers (1937).	*B. S. S.B.I.*	*B.S.* R157-37

TABLE 1. CODES AND STANDARDS—(Continued)

SUBJECT	TITLE	SPONSOR	REFERENCE
Building Requirements	American Standard Building Requirements (1946)	*N.H.A.* *U.S.P.H.S.*	*A.S.A.* A53.1-1946
Burners (Gas)	American Standard Testing Requirements for Gas Conversion Burners (1941).	*A.G.A.*	*A.S.A.* Z21.17-1940
Burners (Gas)	American Standard Requirements for Installation of Gas Burning Equipment in Power Boilers (1942).	*A.G.A.*	*A.S.A.* Z21.33-1942
Burners (Anthracite)	Commercial Standard for Domestic Burners for Pennsylvania Anthracite (Underfeed Type) (1940).	*B.S.* *A.I.L.*	*B.S.* CS48-40
Burners (Oil)	Commercial Standard for Mechanical-Draft Oil Burners Designed for Domestic Installations (1942).	*B.S.* *O.B.I.*	*B.S.* CS75-42
Cleaners (Air)	A.S.H.V.E. Standard Code for Testing and Rating Air Cleaning Devices Used in General Ventilation Work (1934).	A.S.H.V.E.	See A.S.H.V.E. TRANSACTIONS, Vol. 39, 1933, p. 225
Color Scheme (Piping)	Scheme for Identification of Piping Systems (1945).	*H.P. & A.C.C.N.A.*	*H.P. & A.C.C.N.A* Engrg. Stds., Sec. 2. Part V
Color Scheme (Piping)	Scheme for Identification of Piping Systems (1928).	*A.S.M.E.*	*A.S.A.* A13-1928
Coils	Proposed Commercial Standard for Rating and Testing Air Cooling Coils Using Non-Volatile Refrigerants (1945).	*B.C.M.I.* *B.S.*	*B.S.* T.S. 4044
Compressors	Tentative *A.S.R.E.* Standard Methods of Rating and Testing Refrigerant Compressors.	*A.S.R.E.* A.S.H.V.E. *A.C.R.M.A.*	*A.S.R.E.* Circular No. 23
Condensers	*A.S.R.E.* Standard Methods of Rating and Testing Evaporative Condensers.	*A.S.R.E.* A.S.H.V.E. *A.C. & R.M.A.*	*A.S.R.E.* Circular No. 20
Condensers	Tentative *A.S.R.E.* Standard Methods of Rating Water-Cooled Refrigerant Condensers.	*A.S.R.E.* A.S.H.V.E *A.C. & R.M.A.*	*A.S.R.E.* Circular No. 22
Condensing Units	*A.S.R.E.* Standard Methods of Rating and Testing Mechanical Condensing Units (1940).	*A.S.R.E.* A.S.H.V.E. *A.C. & R.M.A.*	*A.S.R.E.* Circular No. 14-41
Condensing Units	Commercial Standard for Commercial Electric Refrigeration Condensing Units (1945).	*B.S.* *S.R.C.A.*	*B.S.* CS107-45
Conductivity	Standard Method of Test for Thermal Conductivity of Materials by Means of the Guarded Hot Plate (Tentative) (1942).	A.S.H.V.E. *A.S.R.E.* *A.S.T.M.* *N.R.C.*	A.S.H.V.E.
Control Equipment (Industrial)	Underwriter's Laboratories, Inc., Standard for Industrial Control Equipment (July 1938, reprinted Sept. 1945).	*U.L.*	*U.L* Subject 508
Controls	Underwriter's Laboratories, Inc., Standard for Temperature Indicating and Regulating Equipment (Jan. 1947).	*U.L.*	*U.L.* Subject 873
Convector	A.S.H.V.E. Standard Code for Testing and Rating Concealed Gravity Type Radiation (Steam Code) (1931).	A.S.H.V.E.	A.S.H.V.E. TRANSACTIONS, Vol. 37, 1931, p. 367
Convector	A.S.H.V.E. Standard Code for Testing and Rating Concealed Gravity Type Radiation (Hot Water Section) (1933).	A.S.H.V.E.	A.S.H.V.E. TRANSACTIONS, Vol. 39, 1933, p. 237
Convector	Recommended Commercial Standard for Testing and Rating Convectors (1946).	*B.S.* *C.M.A.* *I.B.R.*	*B.S.* TS-4169
Coolers (Air)	Proposed *A.S.R.E.* Standard Methods of Rating and Testing Forced Circulation and Natural Convection Air Coolers for Refrigeration (1945).	*A.S.R.E.* A.S.H.V.E. *A.C. & R.M.A.* *R.E.M.A.*	*A.S.R.E.* Circular No. 25-44
Coolers	Tentative *A.S.R.E.* Standard Methods of Rating and Testing Water and Brine Coolers.	*A.S.R.E.* A.S.H.V.E. *A.C. & R.M.A.*	*A.S.R.E.* Circular No. 24
Cooling Units	Standard Methods of Rating and Testing Self Contained Air Conditioning Units for Comfort Cooling (1940).	*A.S.R.E.* A.S.H.V.E. *R.M.A.* *N.E.M.A.* *A.C.M.A.*	*A.S.R.E.* Circular No. 16

TABLE 1. CODES AND STANDARDS—(Continued)

SUBJECT	TITLE	SPONSOR	REFERENCE
Ducts and Fittings	Simplified Practice Recommendation for Pipes, Ducts and Fittings for Warm Air Heating and Air Conditioning (1945).	*Mfrs.* *B.S.*	*B.S.* R207-45
Exchangers (Heat)	Standards of *Tubular Exchanger Manufacturers Association* (1941).	*T.E.M.A.*	*T.E.M.A*
Exhaust Systems	American Standard for Grinding, Polishing, and Buffing Equipment Sanitation (1941).	*A.F.A.*	*A.S.A.* Z43-1941
Exhaust Systems	Tentative Code of Recommended Practices for Testing and Measuring Air Flow in Exhaust Systems (1937).	*A.F.A.*	*A.F.A.* Preprint 36-27
Exhaust Systems	Tentative Recommended Good Practice Code and Handbook on the Fundamentals of Design, Construction. Operation and Maintenance of Exhaust Systems.	*A.F.A.*	*A F.A.*
Fans	Definitions and Terms in Use by the Blower Industry (1940).	*N.A.F.M.*	*N.A.F.M.* Bulletin No. 105
Fans	Standard Test Code for Centrifugal and Axial Fans (1938).	*N.A.F.M.*[a] A.S.H.V.E.	*N.A.F.M.* Bulletin No. 103
Fans	*N.E.M.A.* Fan Standards (1944).	*N.E.M.A*	*N.A.F.M.* Publ. 44-95
Fire Prevention	Building Code Recommended by the *National Board of Fire Underwriters* (1943).	*N.B.F.U.*	*N.B.F.U.*
Fire Prevention	National Fire Codes (1944).	*N.F.P.A.*	*N.F.P.A.*
Fire Prevention	National Fire Code for the Prevention of Dust Explosions (1943)	*N.F.P.A.*	*N.F.P.A.*
Furnaces (Duct)	American Standard Approval Requirements for Gas-Fired Duct Furnaces (1942).	*A.G.A.*	*A.S.A.* Z21.34-1942
Furnaces (Gas, Floor)	Commercial Standard for Gas Floor Furnaces—Gravity Circulating Type (1942).	*B.S.* *A.G.A.E.M.*	*B.S.* CS99-42
Furnaces (Gas)	American Standard Approval Requirements for Central Heating Gas Appliances (1943).	*A.G.A.*	*A.S.A.* Z21.13-1943
Furnaces (Forced Air, Solid-Fuel)	Commercial Standard for Solid-Fuel-Burning Forced Air Furnaces (1944).	*F.H.A.* *N.W.A.H. & A.C.A* *A.I.L.*	*B.S.* CS109-44
Furnaces (Oil-Fired)	Commercial Standard for Warm Air Furnaces Equipped with Vaporizing Pot Type Oil Burners (1943).	*Mfrs.* *B.S.*	*B.S* CS(E)104-43
Furnaces (Oil)	A Tentative Code for Testing Oil-Fired Furnaces	*N.W.A.H. & A.C.A.*	*N.W.A H. & A.C.A*
Furnaces (Oil)	Commercial Standard for Oil Burning Floor Furnaces Equipped with Vaporizing Pot-Type Burners (1944).	*B.S.* *O.P.A.*	*B.S.* CS113-44
Garages	Code of Minimum Requirements for Heating and Ventilating Garages (1935).	A.S.H.V.E.	A.S.H.V.E.
Gases (Toxic) and Dust	American Standard Allowable Concentration of Harmful Gases:	*A.S.A.*	*A.S.A.*
	Carbon Monoxide		Z37.1-1941
	Hydrogen Sulfide		Z37.2-1941
	Carbon Di-sulfide		Z37.3-1941
	Benzene		Z37.4-1941
	Cadmium		Z37.5-1941
	Manganese		Z37.6-1942
	Chromic Acid and Chromates		Z37.7-1943
	Mercury		Z37.8-1943
	Metallic Arsenic and Arsenic Trioxide		Z37.9-1943
	Xylene		Z37.10-1943
	Lead and Certain Inorganic Lead Compounds		Z37.11-1943
	Toluene		Z37.12-1943
	Oxides of Nitrogen		Z37.13-1944
	Methanol		Z37.14-1944
	Styrene-Monomer		Z37.15-1944
	Formaldehyde		Z37.16-1944
Heat Transfer (Walls)	A.S.H.V.E. Standard Test Code for Heat Transmission Through Walls (1928)	A.S.H.V.E.	A.S.H.V.E.

[a]Also endorsed by *P.F.M.A.*

TABLE 1. CODES AND STANDARDS—(Continued)

SUBJECT	TITLE	SPONSOR	REFERENCE
Mineral Wool	Commercial Standard for Mineral Wool: Blankets, Blocks, Insulating Cement, and Pipe Insulation for Heated Industrial Equipment (1944).	*B.S.* *I.M.W.I.*	*B.S.* CS117-44
Mineral Wool	Commercial Standard for Mineral Wool: Loose, Granulated or Felted Form, in Low Temperature Installations (1943).	*B.S.* *I.W.M.I.*	*B.S.* CS105-43
Mineral Wool	Recommended Commercial Standard for Industrial Mineral Wool Products—All Types—Testing and Reporting (1946).	*I.M.W.A.* *B.S.*	*B.S.* CS131-46
Motors	Nema Motor and Generator Standards (June 1945).	*N.E.M.A.*	*N.E.M.A.* 45-102
Piping	American Standard Code for Pressure Piping (1942).	*A.S.M.E.*	*A.S.A.* B31.1-1942
Pumps	Hydraulic Institute Test Code for Centrifugal Pumps. Hydraulic Institute Test Code for Rotary Pumps (1943).	*H.I.*	*H.I.* Section F
Radiators	Code for Testing Radiators (1927).	A.S.H.V.E.	A.S.H.V.E.
Radiators	Simplified Practice Recommendation for Cast Iron Radiators (1943).	*I.B.R.* *B.S.*	*B.S.* R174-43
Refrigeration (Equipment)	Underwriter's Laboratories, Inc., Standard for Air Conditioning and Commerical Refrigerating Equipment (Feb. 1946).	*U.L.*	*U.L* Subject 207A
Refrigeration (Mechanical)	American Standard Safety Code for Mechanical Refrigeration (1939).	*A.S.R.E.*	*A.S.R.E.* Circular No. 15
Refrigeration (Unit Systems)	Underwriter's Laboratories, Inc., Standard for Unit Refrigerating Systems (Feb. 1946).	*U.L.*	*U.L.* Subject 207C
Refrigerators (Gas-Fired)	American Standard Approval Requirements for Refrigerators Using Gas Fuel (1941).	*A.G.A.*	*A.S.A.* Z21.19-1941
Refrigerators (Household)	American Standard Test Procedures for Household Electric Refrigerators (Mechanically Operated) (1944).	*A.S.R.E.* *U.S.D.A.*	*A.S.A.* B38.2-1944
Sound	Sound Measurement Test Code for Centrifugal and Axial Fans (1942).	*N.A.F.M.*	*N.A.F.M* Bulletin No. 104
Sound	American Recommended Practice for the Calibration of Microphones (1938).	*A.S. of A.*	*A.S.A.* Z24 4-1938
Space Heaters	American Standard Approval Requirements for Gas Space Heaters (1942).	*A.G.A.*	*A.S.A.* Z21.11-1942
Space Heaters	Commercial Standard for Flue Connected Oil-Burning Space Heaters Equipped with Vaporising Pot-Type Burners (1943).	*I.C. & H.A.M.*	*B.S.* CS101-43
Stokers	Code for Determination of Rated Capacities of Anthracite Underfeed Stokers (1944).	*S.M.A.*	*S.M.A.*
Stokers	Code for Determination of Rated Capacities of Bituminous Underfeed Stokers (1944).	*S.M.A.*	*S.M.A.*
Stokers	Recommended Minimum Firebox Dimensions and Base Heights (1944).	*S.M.A.*	*S.M.A.*
Stokers	Recommended Standards Governing Minimum Setting Heights (1944).	*S.M.A.*	*S.M.A.*
Unit Heaters	Standard Code for Testing and Rating Steam Unit Heaters (1930).	A.S.H.V.E. *I.U.H.A.*	A.S.H.V.E *I.U.H.A.*
Unit Heaters	Standard Code for Testing Hot Water Unit Heaters (1942).	*I.U H.A.*	*I.U.H.A.*
Unit Heaters	American Standard Approval Requirements for Gas Unit Heaters (1940).	*A.G.A.*	*A.S.A.* Z21.16-1940
Unit Ventilators	A.S.H.V.E. Standard Code for Testing and Rating Steam Unit Ventilators (1934).	A.S.H.V.E.	A.S.H.V.E.
Unfired Pressure Vessels	Unfired Pressure Vessel Code (1946 with 1947 Addenda).	*A.S.M.E.*	*A.S.M.E.*

TABLE 1. CODES AND STANDARDS—(Concluded)

SUBJECT	TITLE	SPONSOR	REFERENCE
Vacuum Pumps	A.S.H.V.E. Standard Code for Testing and Rating Return Line Low Vacuum Heating Pumps (1934).	A.S.H.V.E.	A.S.H.V.E.
Warm Air (Gravity)	Gravity Code and Manual for the Design and Installation of Gravity Warm Air Heating Systems (1945).	*N.W.A.H. & A.C.A.*	*N.W.A.H. & A.C.A* Section No. 5
Water Heaters	*N.E.M.A.* Standards for Electric Water Heaters (1945).	*N.E.M.A.*	*N.E.M.A.* 45-104
Water Heaters	American Standard Approval Requirements for Gas Water Heaters (1944).	*A.G.A.*	*A.S.A.* Z21.10-1944
Water Heaters	Testing and Rating Hand-Fired Hot Water Supply Boilers (1948).	*F.H.A.*	*B.S.* CS145-47
Wiring	National Electrical Code, Standard of N.B.F.U. and N.F.P.A. (1947).	*N.B.F.U.* *N.F.P.A.*	*N.B.F.U.*

ABBREVIATIONS

A.C.M.A.[1]	Air Conditioning Manufacturers Association.	*I.M.W.I.*	Industrial Mineral Wool Institute.
A.C.R.M.A.	Air Conditioning and Refrigerating Machinery Association.	*I.U.H.A.*	Industrial Unit Heater Association.
A.F.A.	American Foundrymen's Association.	*N.A.F.M.*	National Association of Fan Manufacturers.
A.G.A.	American Gas Association.	*N.B.F.U.*	National Board of Fire Underwriters.
A.G.A.E.M.[2]	Association of Gas Appliance and Equipment Manufacturers.	*N.E.M.A.*	National Electrical Manufacturers Association.
A.I.L.	Anthracite Industries Laboratory.	*N.F.P.A.*	National Fire Prevention Association.
A.S.A.	American Standards Association.	*N.H.A.*	National Housing Agency.
A.S. of A.	Acoustical Society of America.	*N.R.C.*	National Research Council.
A.S.H.V.E.	American Society of Heating and Ventilating Engineers.	*N.W.A.H.&A.C.A.*	National Warm Air Heating and Air Conditioning Association.
A.S.M.E.	American Society of Mechanical Engineers.	*O.B.I.*[3]	Oil Burner Institute.
A.S.R.E.	American Society of Refrigerating Engineers.	*O.H.I.A.*	Oil Heat Institute of America.
A.S.T.M.	American Society for Testing Materials.	*O.P.A.*	Office of Price Administration.
B.S.	National Bureau of Standards.	*P.F.M.A.*	Propeller Fan Manufacturers Association.
C.M.A.	Convector Manufacturers Association.	*R.E.M.A.*	Refrigeration Equipment Manufacturers Association.
F.H.A.	Federal Housing Administration.	*R.M.A.*[1]	Refrigerating Machinery Association.
G.A.M.A.	Gas Appliance Manufacturers' Association.	*S.A.E.*	Society of Automotive Engineers.
H.I.	Hydraulic Institute.	*S.B.I.*	Steel Boiler Institute.
H.P. & A.C.C.N.A.	Heating, Piping and Air Conditioning Contractors National Association.	*S.R.C.A.*	Standard Refrigeration Compressor Association.
I.B.R.	Institute of Boiler and Radiator Manufacturers Association.	*T.E.M.A.*	Tubular Exchanger Manufacturers Association.
I.C.H.A.M.	Institute of Cooking and Heating Appliance Manufacturers.	*U.L.*	Underwriter's Laboratories
		U.S.D.A	United States Department of Agriculture.
		U.S.P.H.S.	United States Public Health Service

[1]Superseded 1940 by *A.C.R.M.A.*
[2]Superseded 1945 by *G.A.M.A.*
[3]Superseded 1942 by *O.H.I.A*

SPECIFIC HEAT

TABLE 1. SPECIFIC HEAT OF SOLIDS[a]

MATERIALS	TEMPERATURE F	SPECIFIC HEAT	AUTHORITY
Alloys			
Brass, Red	32	0.0899	S
Brass, Yellow	32	0.0883	S
Bronze (80Cu, 20Sn)	57–208	0.0862	S
Monel Metal	68–2370	0.127	S
Aluminum	80–212	0.212	S
Asbestos	68–208	0.195	S
Brickwork	.....	0.195	H
Carbon (Graphite)	104–1637	0.314	I
Coal	.....	0.278	H
Coke	.....	0.201	H
Concrete	.....	0.270	H
Copper	64–212	0.0928	S
Fire Clay Brick	77–1832	0.258	I
Glass			
Crown	50–122	0.161	S
Flint	50–122	0.117	S
Gold	64	0.0312	S
Gypsum	.....	0.259	H
Ice	32	0.487	S
Ice	−40	0.434	S
Iron, Pure	32	0.1043	S
Iron, Pure	32–600	0.127	M
Iron, Cast	68–212	0.1189	H
Iron, Wrought	59–212	0.1152	H
Lead	32	0.0297	S
Nickel	32	0.1032	S
Masonry	.....	0.2159	H
Plaster	.....	0.2	H
Platinum	58–212	0.0319	S
Rocks			
Gneiss	63–210	0.196	S
Granite	54–212	0.192	S
Limestone	59–212	0.216	S
Marble	32–212	0.21	S
Sandstone	.....	0.22	S
Silver	32	0.0536	S
Steel	.....	0.1175	H
Sulphur	240–320	0.220	S
Silica Brick	77–1832	0.263	I
Tin	77	0.0548	S
Woods (Average)	68	0.327	S
Zinc	32	0.0913	S

TABLE 2. SPECIFIC HEAT OF LIQUIDS

LIQUID	TEMPERATURE F	SPECIFIC HEAT	AUTHORITY
Alcohol, Ethyl	32	0.548	S
Alcohol, Methyl	59–68	0.601	S
Glycerine	59–122	0.576	S
Lead (Molten)	360	0.041	H
Mercury	68	0.03325	S
Petroleum	70–136	0.511	S
Sea Water			
Sp Gr 1.0043	64	0.980	S
Sp Gr 1.0463	64	0.903	S
Water	59	1.000	S

TABLE 3. SPECIFIC HEAT OF GASES AND VAPORS

SUBSTANCE	TEMPERATURE F	SPECIFIC HEAT AT CONSTANT PRESSURE	RATIO OF SPECIFIC HEAT C_p/C_v	SPECIFIC HEAT AT CONSTANT VOLUME (COMPUTED)	AUTHORITY
Air	32–392	0.2375	1.405	0.169	S
Ammonia	80–392	0.5356	1.277	0.419	S
Carbon Dioxide	52–417	0.2169	1.3003	0.1668	S
Carbon Monoxide	79–388	0.2426	1.395	0.1736	S
Coal Gas	68–1900	0.3145	.....	.....	S
Flue Gas	.....	0.24 (Approx.)	.....	.....	H
Hydrogen	70–212	3.41	1.419	2.402	S
Nitrogen	32–392	0.2438	1.41	0.1729	S
Oxygen	55–404	0.2175	1.3977	0.155	S
Water Vapor	212	0.421	1.305	0.322	S
Water Vapor	356	0.51	.....	.....	S

[a]See also The Specific Heat of Thermal Insulating Materials, by Gordon B. Wilkes and Carl O. Wood (A.S.H.V.E. TRANSACTIONS, Vol. 48, 1942, p. 493).

NOTES: When one temperature is given the true specific heat is given, otherwise the value is the mean specific heat between the given limits.

AUTHORITIES: S—Smithsonian Physical Tables, 1933; I—International Critical Tables; H—Heating, Ventilation and Air Conditioning, by L. A. Harding and A. C. Willard; M—Engineers' Handbook, by Lionel S. Marks.

CIRCUMFERENCES AND AREAS OF CIRCLES

Diameter in Inches	Area: Sq In.	Area: Sq Ft	Circumference: Inches	Circumference: Feet	Diameter in Inches	Area: Sq In.	Area: Sq Ft	Circumference: Inches	Circumference: Feet
¼	0.049	0 0003	0.785	0.0652	28	615.8	4.276	87.97	7.330
½	0.196	0 0014	1.571	0.1309	28½	637.9	4.430	89.54	7.462
¾	0 442	0.0031	2.356	0.1964	29	660.52	4.587	91.11	7.592
1	0.785	0.0054	3.142	0.2618	29½	683.5	4.747	92.63	7.725
1¼	1.227	0.0085	3.927	0.3273	30	706.8	4.909	94.25	7.854
1½	1 767	0.0123	4.712	0.3927	31	754.8	5.241	97.39	8.116
1¾	2.405	0.0167	5.498	0.4582	32	804.3	5.585	100.5	8.378
2	3.142	0.0218	6.283	0.5236	33	855.3	5.940	103.7	8.639
2¼	3.976	0.0276	7.069	0.5891	34	907.9	6.305	106.8	8.901
2½	4.909	0.0341	7.854	0.6546	35	962.1	6.681	109.9	9.163
2¾	5.939	0.0412	8.639	0.7200	36	1018.0	7.069	113.1	9.425
3	7.069	0.0491	9.425	0.7854	37	1075.0	7.467	116.2	9.686
3¼	8.296	0.0576	10.21	0.8510	38	1134.0	7.876	119.4	9.948
3½	9.621	0.0668	10.99	0.9160	39	1195.0	8.296	122.5	10.21
3¾	11.04	0.0767	11.78	0.9818	40	1256 0	8.727	125.6	10.47
4	12.57	0 0873	12.57	1.047	41	1320 0	9.168	128.8	10.73
4¼	14.19	0.0986	13.35	1.113	42	1385.0	9 621	131.9	10.99
4½	15.90	0.1104	14.14	1.178	43	1452.0	10.08	135.1	11.26
4¾	17.72	0.1231	14.92	1.243	44	1521.0	10.56	138.2	11.52
5	19.64	0.1364	15.71	1.309	45	1590.0	11.04	141.4	11.78
5¼	21.65	0.1504	16.49	1.374	46	1662.0	11.54	144.5	12.04
5½	23 76	0.1650	17.28	1.440	47	1735.0	12.05	147.7	12.30
5¾	25.97	0.1840	18.06	1.505	48	1810.0	12.51	150.8	12.57
6	28.27	0 1964	18.85	1.571	49	1886.0	13.09	153.9	12.83
6¼	30.68	0.2131	19.64	1.637	50	1963.0	13.64	157.1	13.09
6½	33.18	0.2304	20.42	1.702	51	2043.0	14 19	160.2	13.35
6¾	35.79	0.2486	21.21	1.768	52	2124.0	14.75	163.4	13.61
7	38.49	0.2673	21.99	1.833	53	2206.0	15.32	166.5	13.88
7¼	41.28	0.2867	22.78	1.899	54	2290.0	15.90	169.6	14.14
7½	44.18	0.3068	23.56	1.964	55	2376.0	16.50	172.8	14.40
7¾	47.17	0.3276	24.35	2.029	56	2463.0	17.10	175.9	14.66
8	50.27	0.3491	25.13	2.094	57	2552.0	17.72	179.1	14.92
8¼	53.46	0.3713	25.92	2.160	58	2642.0	18.35	182.2	15.18
8½	56.75	0.3942	26.70	2 225	59	2734.0	18.99	185.4	15.45
8¾	60.13	0.4175	27.49	2.291	60	2827.0	19.63	188.5	15.71
9	63.62	0.4418	28.27	2.356	61	2922.0	20.29	191.6	15.97
9¼	67.20	0.4668	29.06	2.422	62	3019.0	20.97	194.8	16.23
9½	70.88	0.4923	29.85	2.488	63	3117.0	21.65	197.9	16.49
9¾	74.66	0.5185	30.63	2.553	64	3217.0	22 34	201.1	16.76
10	78.54	0.5454	31.42	2.618	65	3318.0	23.04	204.2	17.02
10½	86.59	0.6010	32.99	2.750	66	3421.0	23.76	207.3	17.28
11	95.03	0.6600	34.56	2.880	67	3526.0	24.48	210.5	17.54
11½	103.9	0.7215	36.13	3.011	68	3632.0	25.22	213.6	17.80
12	113.1	0.7854	37.70	3.142	69	3739.0	25.97	216.8	18.06
12½	122.7	0.8520	39.27	3.273	70	3848.0	26.73	219.9	18.33
13	132.7	0.9218	40.84	3.403	71	3959.0	27.49	223.1	18.59
13½	143.1	0.9937	42.41	3.535	72	4072.0	28.27	226.2	18.85
14	153.9	1.069	43.98	3.665	73	4185.0	29.07	229.3	19.11
14½	165.1	1.146	45.55	3.796	74	4301.0	29.87	232.5	19.37
15	176.7	1.227	47.12	3.927	75	4418.0	30.68	235.6	19.63
15½	188.7	1.310	48.69	4.058	76	4536.0	31.50	238.8	19.90
16	201.1	1.396	50.27	4.189	77	4657.0	32.34	241.9	20.16
16½	213.8	1.485	51.84	4.321	78	4778.0	33.18	245.0	20.42
17	226.9	1.576	53.41	4.451	79	4902.0	34.04	248.2	20.68
17½	240.5	1.670	54.98	4.582	80	5027.0	34.91	251.3	20.94
18	254.5	1.767	56.55	4.712	81	5153.0	35.78	254.5	21.21
18½	268.8	1.867	58.12	4.845	82	5281.0	36.67	257.6	21.47
19	283.5	1.969	59.69	4.974	83	5411.0	37.57	260.8	21 73
19½	298.6	2.074	61.26	5.105	84	5542.0	38.48	263.9	21.99
20	314.2	2.182	62.83	5.236	85	5675.0	39.41	267.0	22.25
20½	330.1	2.293	64.40	5.367	86	5809.0	40.34	270.2	22.51
21	346.4	2 405	65.97	5.498	87	5945.0	41.28	273.3	22.78
21½	361.1	2.508	67.54	5.629	88	6082.0	42.24	276.5	23.04
22	380.1	2.640	69.12	5.760	89	6221.0	43.20	279.6	23.30
22½	397.6	2.761	70.69	5.891	90	6362.0	44.18	282.7	23.56
23	415.5	2.885	72.26	6.021	91	6504.0	45.17	285.9	23.82
23½	433.7	3.012	73.83	6.153	92	6648.0	46.16	289.0	24.09
24	452.4	3.142	75.40	6.283	93	6793.0	47.17	292.2	24.35
24½	471.4	3.274	76.97	6.415	94	6940.0	48.19	295.3	24.61
25	490.9	3.409	78.54	6.545	95	7088.0	49.22	298.4	24.87
25½	510.7	3.547	80.11	6.676	96	7238.0	50.27	301.6	25.13
26	530.9	3.687	81.68	6.807	97	7390.0	51.32	304.7	25.39
26½	551.6	3.832	83.25	6.938	98	7543.0	52.38	307.9	25.66
27	572.6	3.976	84.82	7.069	99	7698.0	53.46	311.0	25.92
27½	593.9	4.125	86.39	7.199	100	7854.0	54.54	314.2	26.18

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Atlantic Metal Hose Co., 1012
Chicago Metal Hose Co., 1013
Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1127

BENDS, Pipe, Ferrous and Non-Ferrous
Condenser Service & Engineering Co., Inc., 1053
Eagle-Picher Co., The, 1254
Arthur Harris & Co., 1120
Mueller Brass Co., 1010-1011
Parks-Cramer Co., 960

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BLOCKS, Asbestos
Philip Carey Mfg. Co., The, 1238-1239
Grant Wilson, Inc. 1240

BLOCKS, Glass
Owens-Illinois Glass Co., 1248
Pittsburgh Corning Corp., 1246-1247

BLOCKS, Mineral Wool
Baldwin-Hill Co., 1251
Eagle-Picher Co., The, 1254

BLOWER HOUSINGS
Aladdin Heating Corp., 1066
Bishop & Babcock Mfg. Co., The, (Massachusetts Blower Div.), 1068
Burden Co., 1070
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
General Blower Co., 1074
Hastings Air Conditioning Co., Inc., 958
Jaden Mfg. Co., 990
Lau Blower Co., The, 1078
Morrison Products, Inc., 1079
Schwitzer-Cummins Co., 1082
Torrington Mfg. Co., The, 1084-1085
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Westinghouse Electric Corp., Sturtevant Div., 1032-1039

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BLOWERS, Centrifugal (*See Fans*)

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Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Coolair Corp., 1064-1065

Bayley Blower Co., 1067
Buffalo Forge Co., 1069
Campbell Heating Co., 968-969
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
General Blower Co., 1074
Joy Mfg. Co., 1076-1077
Marlo Coil Co., 1060
National Heater Co., 983
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Western Blower Co., 1087
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

BLOWERS, Heating and Ventilating

Air Controls, Inc., Div of The Cleveland Heater Co., 1063
Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
Bayley Blower Co., 1067
Bishop & Babcock Mfg. Co., The, (Massachusetts Blower Div.), 1068
Buffalo Forge Co., 1069
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Campbell Heating Co., 968-969
Carrier Corp., 952-953
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
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C. A. Dunham Co., 1212-1216
Electromode Corp., 984-985
General Blower Co., 1074
Hastings Air Conditioning Co., Inc., 958
Ilg Electric Ventilating Co., 989, 1075
Jaden Mfg. Co., 990
Joy Mfg. Co., 1076-1077
Lau Blower Co., The, 1078
Morrison Products, Inc., 1079
L. J. Mueller Furnace Co., 974-975
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
Niagara Blower Co., 959
Schwitzer-Cummins Co., 1082
Torrington Mfg. Co., The, 1084-1085
Trade-Wind Motorfans, Inc., 1083
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Western Blower Co., 1087
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

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Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
Bayley Blower Co., 1067
Buffalo Forge Co., 1069
Burden Co., 1070
Campbell Heating Co., 968-969
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
General Blower Co., 1074
Ilg Electric Ventilating Co., 989, 1075
Ingersoll-Rand, 1204
Joy Mfg. Co., 1076-1077
Jos. A. Martocello & Co., 1047
Nash Engineering Co., 1202-1203
United States Air Conditioning Corp., 962
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

BLOWERS, Turbine

DeBothezat Fans Div., American Machine & Metals, Inc., 1073
Ilg Electric Ventilating Co., 989, 1075
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

BLOWERS, Warm Air Furnace

Air Controls, Inc., Div. of The Cleveland Heater Co., 1063
Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Radiator & Standard Sanitary Corp., 1146-1147
Bishop & Babcock Mfg. Co., The (Massachusetts Blower Div.), 1068
Buffalo Forge Co., 1069
Burden Co., 1070
Campbell Heating Co., 968-969
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
Duo-Therm Div. of Motor Wheel Corp., 967
General Blower Co., 1074
Hastings Air Conditioning Co., Inc., 958
Ilg Electric Ventilating Co., 989, 1075
Jaden Mfg. Co., 990
Joy Mfg. Co., 1076-1077
Lau Blower Co., The, 1078
Meyer Furnace Co., The, 972-973
Morrison Products, Inc., 1079
L. J. Mueller Furnace Co., 974-975
Schwitzer-Cummins Co., 1082
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
United States Radiator Corp., 1156-1157
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Western Blower Co., 1087
L. J. Wing Mfg. Co., 1003-1005

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Airtemp Div., Chrysler Corp., 970-971
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American Radiator & Standard Sanitary Corp., 1146-1147
Automatic Burner Corp., 1177
Bryant Heater Co., 966
Crane Co., 1148-1149
General Electric Co. (Bloomfield, N. J.), 956-957
Iron Fireman Mfg. Co., 1174-1175
National Radiator Co., The, 1150-1151
Petroleum Heat & Power Co., 1182-1183
Preferred Utilities Mfg. Corp., 1188
United States Radiator Corp., 1156-1157
Webster Engineering Co., The, 1173
York-Shipley, Inc., 1189

BOILER COMPOUNDS (*See Compounds, Boiler*)

BOILER COVERING (*See Covering, Pipe and Surfaces*)

BOILER FEED PUMPS (*See Pumps, Boiler Feed*)

BOILER FEEDERS (*See Feeders, Boiler*)

BOILER WATER FIELD KIT, for Testing and Treating

Vinco Co., Inc., The, 1190-1191

BOILER WATER TREATMENT

Vinco Co., Inc., The, 1190-1191

BOILERS, Cast-Iron

Airtemp Div., Chrysler Corp., 970-971
American Radiator & Standard Sanitary Corp., 1146-1147
Bryant Heater Co., 966
Burnham Corp., 1145
Crane Co., 1148-1149
National Radiator Co., The, 1150-1151
H. B. Smith Co., Inc., The, 1154
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
United States Radiator Corp., 1156-1157
Weil-McLain Co. 1158
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

BOILERS, Down Draft

Farrar & Trefts, Inc., 1163
Kewanee Boiler Corp., 1166-1169
H. B. Smith Co., Inc., The, 1154

BOILERS, Gas Fired

Airtemp Div., Chrysler Corp., 970-971
American Radiator & Standard Sanitary Corp., 1146-1147
Babcock & Wilcox Co., The, 1159
Bryant Heater Co., 966
Burnham Corp., 1145
Condenser Service & Engineering Co., Inc., 1053
Crane Co., 1148-1149
Farrar & Trefts, Inc., 1163
Fitzgibbons Boiler Co., Inc., 1164-1165
General Electric Co. (Bloomfield, N. J.), 956-957
International Boiler Works Co., 1172
Kewanee Boiler Corp., 1166-1169
L. J. Mueller Furnace Co., 974-975
National Radiator Co., The, 1150-1151
Pacific Steel Boiler Div., U. S. Radiator Corp., 1155
H. B. Smith Co., Inc., The, 1154
Spencer Heater Div., The Avco Mfg Corp., 1152-1153
Titusville Iron Works Co., The (Div. of Struthers Wells Corp.), 1170-1171
Trane Co., The, 1000-1001
United States Radiator Corp., 1156-1157
Weil-McLain Co., 1158

BOILERS, Heating
Airtemp Div , Chrysler Corp., 970-971
Aldrich Co., 1176
American Radiator & Standard Sanitary Corp., 1146-1147
Babcock & Wilcox Co., The, 1159
Bigelow Co., The, 1160
Brownell Co., The, 1161
Bryant Heater Co., 966
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Crane Co., 1148-1149
Farrar & Trefts, Inc., 1163
Fitzgibbons Boiler Co., Inc., 1164-1165
International Boiler Works Co., The, 1172
Iron Fireman Mfg. Co., 1174-1175
Kewanee Boiler Corp., 1166-1169
L. J. Mueller Furnace Co., 974-975
National Radiator Co., The, 1150-1151
Pacific Steel Boiler Div., U. S. Radiator Corp., 1155
Petroleum Heat & Power Co., 1182-1183
Preferred Utilities Mfg. Corp., 1183
H. B. Smith Co., Inc., The, 1154
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
Titusville Iron Works Co., The (Div. of Struthers Wells Corp.), 1170-1171
United States Radiator Corp., 1156-1157
Weil-McLain Co., 1158
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

BOILERS, Magazine Feed
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
York-Shipley, Inc., 1189

BOILERS, Oil Burning
Airtemp Div., Chrysler Corp., 970-971
Aldrich Co., 1176
American Radiator & Standard Sanitary Corp., 1146-1147
Automatic Burner Corp., 1177
Babcock & Wilcox Co., The, 1159
Bigelow Co., The, 1160
Brownwell Co., The, 1161
Burnham Corp., 1145
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Fitzgibbons Boiler Co., Inc., 1164-1165
General Electric Co. (Bloomfield, N. J.), 956-957
International Boiler Works Co., The, 1172
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S. T. Johnson Co., 1180-1181
Kewanee Boiler Corp., 1166-1169
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Pacific Steel Boiler Div., U. S. Radiator Corp., 1155
Petroleum Heat & Power Co., 1182-1183
Preferred Utilities Mfg. Corp., 1188
H. B. Smith Co., Inc., The, 1154
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
Titusville Iron Works Co., The (Div. of Struthers Wells Corp.), 1170-1171
United States Radiator Corp., 1156-1157
Weil-McLain Co., 1158
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

BOILERS, Steel
Airtemp Div., Chrysler Corp., 970-971
Aldrich Co., 1176
Babcock & Wilcox Co., The, 1159
Bigelow Co., The, 1160
Brownell Co., The, 1161
Burnham Corp., 1145
Combustion Engineering Co., Inc., 1162
Condenser Service & Engineering Co., Inc., 1053
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Fitzgibbons Boiler Co., Inc., 1164-1165
General Electric Co. (Bloomfield, N. J.), 956-957
International Boiler Works Co., The, 1172
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Kewanee Boiler Corp., 1166-1169
National Radiator Co., The, 1150-1151
Pacific Steel Boiler Div., U. S. Radiator Corp., 1155
Preferred Utilities Mfg. Corp., 1188
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
Titusville Iron Works Co., The (Div. of Struthers Wells Corp.), 1170-1171
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

BOILERS, Unit Steam Generator
Aldrich Co., 1176
Foster Wheeler Corp., 1041
Preferred Utilities Mfg. Corp., 1188
York-Shipley, Inc., 1189

BOILERS, Water Tube
Babcock & Wilcox Co., The, 1159
Bigelow Co., The, 1160
Combustion Engineering Co., 1162
Farrar & Trefts, Inc., 1163
Foster Wheeler Corp., 1041
International Boiler Works Co., The, 1172
H. B. Smith Co., Inc., The, 1154
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
Titusville Iron Works Co., The (Div. of Struthers Wells Corp.), 1170-1171

BRACKETS, Radiator
Carty & Moore Engineering Co., 1209
United States Radiator Corp., 1156-1157

BREECHINGS AND CHIMNEYS
Bigelow Co., The, 1160
Brownell Co., The, 1161
Farrar & Trefts, Inc., 1163

BURNERS, Automatic (*See Coal Burners, Stokers*)
R. W. Beckett Corp., 1178
Combustion Engineering Co., 1162
General Electric Co. (Bloomfield, N. J.), 956-957
Iron Fireman Mfg. Co., 1174-1175
S. T. Johnson Co., 1180-1181
Preferred Utilities Mfg. Corp., 1188
Ray Oil Burner Co., 1185
United States Air Conditioning Corp., 962
York-Shipley, Inc., 1189

BURNERS, Combination Gas and Oil
Babcock & Wilcox Co., The, 1159
Combustion Engineering Co., 1162
Combustion Equipment Div., Todd Shipyards Corp., 1186
Enterprise Engine & Foundry Co., Burner Div., 1179
S. T. Johnson Co., 1180-1181
Ray Oil Burner Co., 1185
Webster Engineering Co., The, 1173

BURNERS, Gas (*See Gas Burners*)

BURNERS, Oil (*See Oil Burners*)

CALKING, Building
Baldwin-Hill Co., 1251
Eagle-Picher Co., The, 1254
Insul-Mastic Corp. of America, 1255
Kimberly-Clark Corp., 1262-1263

CARBON, Activated
W. B. Connor Engineering Corp., 1020-1021, 1100-1101

CASTINGS, Bronze and Dairy Nickel Silver Metal
Arthur Harris & Co., 1120
D. J. Murray Mfg. Co., 996

CEILING PLATES
Pyle-National Co., The, 1108
United States Radiator Corp., 1156-1157
United States Register Co., 1112

CELLULAR GLASS (*See Glass, Cellular*)

CEMENT, Asbestos
Eagle-Picher Co., The, 1254
Mundet Cork Corp., 1265
United States Register Co., 1112
Grant Wilson, Inc., 1240

CEMENT, Insulating
Armstrong Cork Co., 1250
Baldwin-Hill Co., 1251
Philip Carey Mfg. Co., The, 1238-1239
Eagle-Picher Co., The, 1254
Johns-Manville, 1260-1261
Owens-Corning Fiberglas Corp., 1026-1027
United States Register Co., 1112
Grant Wilson, Inc., 1240

CEMENT, Mineral Wool
Baldwin-Hill Co., 1251
Eagle-Picher Co., The, 1254
Owens-Corning Fiberglas Corp., 1026-1027
Grant Wilson, Inc., 1240

CEMENT, Refractory (*See Refractories*)

CHAIN, Furnace Pulleys (*See also Pulleys, Chain*)
Hart & Cooley Mfg. Co., 1102-1103
Hendrick Mfg. Co., 1104-1105
Revere Copper & Brass, Inc., 1007
United States Register Co., 1112

CHIMNEY TOPS
Air Devices, Inc., 1014, 1096
G. C. Breidert Co., 1092

CIRCULATORS, Hot Water Heating
Allis-Chalmers Mfg. Co., 964-965
Crane Co., 1148-1149
Hoffman Specialty Co., 1218-1221
Iron Fireman Mfg. Co., 1174-1175
Jas. P. Marsh Corp., 1232-1233
Minneapolis-Honeywell Regulator Co., 1136-1137
Taco Heaters, Inc., 1197
H. A. Thrush & Co., 1198-1199
Trane Co., The, 1000-1001

CLEANERS, Air (*See Air Cleaning Equipment*)

COAL BURNERS (*See Burners, Automatic*)

COATINGS, Protective
Philip Carey Mfg. Co., The, 1238-1239
Insul-Mastic Corp. of America, 1255

COILS, Aluminum
Marlo Coil Co., 1060
McQuay, Inc., 992-993
John J. Nesbitt, Inc., 997
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Westinghouse Electric Corp., Sturtevant Div. 1032-1039
Young Radiator Co., 1006

COILS, Ammonia
Acme Industries, Inc., 1049
Baker Ice Machine Co., Inc., 1057
Condenser Service & Engineering Co., Inc., 1053
G & O Manufacturing Co., The, 1054
General Refrigeration, Div. Yates-American Mch. Co., 955
Kennard Corp., 991
Marlo Coil Co., 1060
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Worthington Pump & Machinery Corp., 1062
Yarnall-Waring Co., 1235
York Corp., 963

COILS, Blast
Aerofin Corp., 1050-1052
Airtherm Mfg. Co., 978
American Blower Corp., 948-949
Electromode Corp., 984-985
G & O Mfg. Co., The, 1054
Hastings Air Conditioning Co., Inc., 958
Kennard Corp., 991
Marlo Coil Co., 1060
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
D. J. Murray Mfg. Co., 996
John J. Nesbitt, Inc., 997
New York Blower Co., The, 1080
Niagara Blower Co., 959
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Young Radiator Co., 1006

COILS, Brass
E. B. Badger & Sons Co , 1116-1117
Arthur Harris & Co., 1120
Marlo Coil Co., 1060
McQuay, Inc., 992-993
Trane Co., The, 1000-1001

COILS, Cooling
Acme Industries, Inc., 1049
Aerofin Corp., 1051-1053
American Blower Corp., 948-949
Baker Ice Machine Co., Inc., 1057
Bell & Gossett Co., 1194-1195
Carrier Corp., 952-953
Condenser Service & Engineering Co., Inc., 1053
Frick Co., 1059
G & O Mfg. Co., The, 1054
General Electric Co., (Bloomfield, N. J.), 956-957
General Refrigeration, Div. Yates-American Mch. Co., 955
Hastings Air Conditioning Co., Inc., 958
Insul-Wool Insulation Corp., 1258
Kennard Corp., 991
Marlo Coil Co., 1060
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
John J. Nesbitt, Inc., 997
New York Blower Co., The, 1080
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062
York Corp., 963
Young Radiator Co., 1006

COILS, Pipe, Copper
Acme Industries, Inc., 1049
E. B. Badger & Sons Co., 1116-1117
Bell & Gossett Co., 1194-1195
General Refrigeration, Div. Yates-American Mch. Co., 955
Arthur Harris & Co., 1120
Marlo Coil Co., 1060
McQuay, Inc., 992-993

COILS, Pipe, Iron
Acme Industries, Inc., 1049
Bayley Blower Co., 1067
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062

COILS, Pipe and Tube, Non-Ferrous
Acme Industries, Inc. 1049
Arthur Harris & Co., 1120
Marlo Coil Co., 1060
John J. Nesbitt, Inc., 997
Refrigeration Economics Co., Inc., 1002
Westinghouse Electric Corp., Box 868, Pittsburgh, 1032-1039
York Corp., 963

COILS, Stainless Steel
Arthur Harris & Co., 1120
McQuay, Inc., 992-993

COILS, Tank
Baker Ice Machine Co., Inc., 1057
Bell and Gossett Co., 1194-1195
Refrigeration Economics Co., Inc., 1002
Taco Heaters, Inc., 1197

COMBUSTION CHAMBERS
Babcock & Wilcox Co., The, 1159
Combustion Engineering Co., 1162
Dravo Corp., 980-981

COMPOUNDS, Boiler
Vinco Co., Inc., The, 1190-1191

COMPOUNDS, Boiler and Radiator Sealing
Dole Valve Co., The, 1236
Vinco Co., Inc., The, 1190-1191

COMPOUNDS, Soot Destroyer
Vinco Co., Inc., The 1190-1191

COMPRESSOR MOTORS (*See Motors, Electric*)

COMPRESSOR TUBING, Flexible (*See Tubing, Flexible Metallic*)

COMPRESSORS, Air
Curtis Refrigerating Machine Div. of Curtis Mfg. Co., 1058
Ingersoll-Rand, 1204
Nash Engineering Co., 1202-1203
Worthington Pump and Machinery Corp., 1062

COMPRESSORS, Refrigeration
Airtemp Div., Chrysler Corp., 970-971
Baker Ice Machine Co., Inc., 1057
Carrier Corp., 952-953
Curtis Refrigerating Machine Div. of Curtis Mfg. Co., 1058
Frick Co., 1059
General Electric Co. (Bloomfield N. J.), 956-957
General Refrigeration, Div. Yates-American Mch. Co., 955
Joy Mfg. Co., 1076-1077
Mills Industries, Inc., 1061
Trane Co., The, 1000-1001
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062
York Corp., 963

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Acme Industries, Inc., 1049
Aerofin Corp., 1050-1052
Baker Ice Machine Co., Inc., 1057
Bell & Gossett Co., 1194-1995
Carrier Corp., 952-953
Condenser Service & Engineering Co., Inc., 1053
Curtis Refrigerating Machine Div. of Curtis Mfg. Co., 1058
Farrar & Trefts, Inc., 1163
Fedders-Quigan Corp., 987
Foster Wheeler Corp., 1041
Frick Co., 1059
G & O Mfg. Co., The. 1054
General Refrigeration, Div. Yates-American Mch Co., 955
Kennard Corp., 991
Marlo Coil Co., 1060
D. J. Murray Mfg. Co., 996
National Radiator Co., The, 1150-1151
Niagara Blower Co., 959
J. F. Pritchard & Co., 1043
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962

Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062
Young Radiator Co., 1006

CONDUIT, Refrigeration (*See Hose, Flexible Metal, and Liquid, Gas, Vapor*)

CONDUITS, Underground Fittings

Durant Insulated Pipe Co., 1241
H. W. Porter & Co., Inc., 1242
Ric-wiL Co., The, 1243

CONDUITS, Underground Pipe

E. B. Badger & Sons Co., 1116-1117
Durant Insulated Pipe Co., 1241
H. W. Porter & Co., Inc., 1242
Ric-wiL Co., The, 1243

CONTROL, Air Volume Damper

Air Devices, Inc., 1014, 1096
Anemostat Corp. of America, 1094-1095
Barber-Colman Co., 1098
W. B. Connor Engineering Corp., 1020-1021, 1100-1101
Johnson Service Co., 1132-1133
Minneapolis-Honeywell Regulator Co., 1136-1137
Powers Regulator Co., The, 1140
Register & Grille Mfg. Co., Inc., 1109
Tuttle & Bailey, Inc., 1110-1111
Young Regulator Co., 1113

CONTROL, Boiler Water Level

Crane Co., 1148-1149
McDonnell & Miller, Inc., 1192-1193
Mercoid Corp., The, 1134-1135
Mueller Steam Specialty Co., Inc., 1234
Sarco Co., Inc., 1224-1225

CONTROL EQUIPMENT, Combustion

Automatic Products Co., 1123
Condenser Service & Engineering Co., Inc., 1053
Detroit Lubricator Co., Div. of American Radiator & Standard Sanitary Corp., 1124-1125
Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1126-1127
General Electric Co., (Schenectady, N. Y.), 1088-1089
Illinois Engineering Co., 1222-1223
Iron Fireman Mfg. Co., 1174-1175
Mercoid Corp., The, 1134-1135
Minneapolis-Honeywell Regulator Co., 1136-1137
Penn Electric Switch Co., 1139
Photoswitch, Inc., (Affiliate of Combustion Control Corp.), 986
Webster Engineering Co., The, 1173
White-Rodgers Electric Co., 1144
L. J. Wing Mfg. Co., 1003-1005

CONTROL EQUIPMENT, Time

Minneapolis-Honeywell Regulator Co., 1136-1137
Photoswitch, Inc., (Affiliate of Combustion Control Corp.), 986

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Alco Valve Co., 1122
Allis-Chalmers Mfg. Co., 964-965
American Moistening Co., 1046
Automatic Products Co., 1123
Barber-Colman Co., 1098
Detroit Lubricator Co., Div. of American Radiator & Standard Sanitary Corp., 1124-1125
C. A. Dunham Co., 1212-1216
Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1126-1127
General Controls, 1128-1129
Henry Valve Co., 1130
Hoffman Specialty Co., 1218-1221
Illinois Engineering Co., 1222-1223
Iron Fireman Mfg. Co., 1174-1175
Johnson Service Co., 1132-1133
Jas. P. Marsh Corp., 1232-1233
Minneapolis-Honeywell Regulator Co., 1136-1137
Mueller Steam Specialty Co., Inc., 1234
Parks-Cramer Co., 960
Penn Electric Switch Co., 1139
Photoswitch, Inc., (Affiliate of Combustion Control Corp., 986
Powers Regulator Co., The, 1140
Sarco Co., Inc., 1224-1225
Taylor Instrument Cos., 1142
United States Gauge, 1143
Webster Engineering Co., The, 1173
Westinghouse Electric Corp., Box 868, Pittsburgh, 1032-1039
White-Rodgers Electric Co., 1144

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Airtherm Mfg. Co., 978
American Radiator & Standard Sanitary Corp., 1146-1147
Bell & Gossett Co., 1194-1195
C. A. Dunham Co., 1212-1216
Electromode Corp., 984-985
General Electric Co., (Schenectady, N. Y.), 1088-1089
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
D. J. Murray Mfg. Co., 996
John J. Nesbitt, Inc., 997
Shaw-Perkins Mfg. Co., 1055
Trane Co., The, 1000-1001
Tuttle & Bailey, Inc., 1110-1111
United States Radiator Corp., 1156-1157
Warren Webster & Co., 1226-1229
Young Radiator Co., 1006

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National Radiator Co., 1150-1151
United States Radiator Corp., 1156-1157

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Acme Industries, Inc., 1049
Aerofin Corp., 1050-1052
Airtemp Div., Chrysler Corp., 970-971
Buffalo Forge Co., 1069
Carrier Corp., 952-953
Condenser Service & Engineering Co., Inc., 1053
Curtis Refrigerating Machine Div. of Curtis Mfg. Co., 1058
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
Farr Co., 1024
Fedders-Quigan Corp., 987
Frick Co., 1059
G & O Mfg. Co., The, 1054
General Electric Co. (Bloomfield, N. J.), 956-957
General Refrigeration, Div. Yates-American Mch. Co., 955
Hastings Air Conditioning Co., Inc., 958
Joy Mfg. Co., 1076-1077
Kennard Corp., 991
Marlo Coil Co., 1060
Modine Mfg. Co., 994-995
L. J. Mueller Furnace Co., 974-975
John J. Nesbitt, Inc., 997
Niagara Blower Co., 959
Pan-L-Heat Corp., 1196
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
L. J. Wing Mfg. Co., 1003-1005
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Aerofin Corp., 1050-1052
Airtemp Div., Chrysler Corp., 970-971
Bell & Gossett Co., 1194-1195
Carrier Corp., 952-953
Condenser Service & Engineering Co., Inc., 1053
Fedders-Quigan Corp., 987
General Electric Co. (Bloomfield, N. J.), 956-957
Marlo Coil Co., 1060
Modine Mfg. Co., 994-995
New York Blower Co., The, 1080
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
Worthington Pump & Machinery Corp., 1062
Young Radiator Co., 1006

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Acme Industries, Inc., 1049
Aerofin Corp., 1050-1052
Airtemp Div., Chrysler Corp., 970-971
April Showers Co., 1044
Baker Ice Machine Co., Inc., 1057
Bell & Gossett Co., 1194-1195
Campbell Heating Co., 968-969
Carrier Corp., 952-953
Condenser Service & Engineering Co., Inc., 1053
Curtis Refrigerating Machine Div. of Curtis Mfg. Co., 1058
Fedders-Quigan Corp., 987
Frick Co., 1059
General Electric Co. (Bloomfield, N. J.), 956-957
Kennard Corp., 991
Marley Co., The, 1042
Marlo Coil Co., 1060
John J. Nesbitt, Inc., 997
New York Blower Co., The, 1080
Niagara Blower Co., 959
Pan-L-Heat Corp., 1196
J. F. Pritchard & Co., 1043
Refrigerating Machinery Co., 1044
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
Water Cooling Equipment Corp., 1045
Worthington Pump & Machinery Corp., 1062
Yarnall-Waring Co., 1235
York Corp., 963
Young Radiator Co., 1006

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American Blower Corp., 948-949
Burden Co., 1070
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
Joy Mfg. Co., 1076-1077
Marley Co., The, 1042

Herman Nelson Corp., The, 998-999
J. F. Pritchard & Co., 1043
Propellair Div., Robbins & Myers, Inc., 1081
Refrigerating Machinery Co., 1044
Trane Co., The, 1000-1001
Water Cooling Equipment Corp., 1045
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1002-1005

COOLING TOWERS, Atmospheric, Mechanical Draft, Forced Draft, Induced Draft (*See also Cooling Equipment, Water*)
Air & Refrigeration Corp., 947
Condenser Service & Engineering Co., Inc., 1053
Curtis Refrigerating Machine Div. of Curtis Mfg. Co., 1058
Foster Wheeler Corp., 1041
Kennard Corp., 991
Marley Co., The, 1042
Marlo Coil Co., 1060
Jos. A. Martocello & Co., 1047
D. J. Murray Mfg. Co., 996
J. F. Pritchard & Co., 1043
Refrigerating Machinery Co., 1044
Trane Co., The, 1000-1001
Water Cooling Equipment Corp., 1045
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062
Young Radiator Co., 1006

CORK PRODUCTS (*See Insulation*)
Armstrong Cork Co., 1250
Insul-Mastic Corp. of America, 1255
Korfund Co., Inc., The, 1259
Mundet Cork Corp., 1265

CORROSION, Treatment of
Insul-Mastic Corp. of America, 1255
Research Products Corp., 1030
Vinco Co., Inc., The, 1190-1191

COVERING, Pipe
American Flange & Mfg. Co., Inc., 1249
Armstrong Cork Co., 1250
Baldwin-Hill Co., 1251
Philip Carey Mfg. Co., The, 1238-1239
Durant Insulated Pipe Co., 1241
Eagle-Picher Co., The, 1254
Insul-Mastic Corp. of America, 1255
Johns-Manville, 1260-1261
Mundet Cork Corp., 1265
Owens-Corning Fiberglas Corp., 1026-1027
Pittsburgh Corning Corp., 1246-1247
H. W. Porter & Co., Inc., 1242
Ric-wil Co., The, 1243
Grant Wilson, Inc., 1240

CUT-OFFS, Low Water
Combustion Control Corp., 986
General Controls, 1128-1129
McDonnell & Miller, Inc., 1102-1193
Mercoid Corp., The, 1134-1135
Minneapolis-Honeywell Regulator Co., 1136-1137
United States Radiator Corp., 1156-1157
Warren Webster & Co., 1226-1229

DAMPER REGULATOR SETS
Automatic Products Co., 1123
Barber-Colman Co., 1098
Hart & Cooley Mfg. Co., 1102-1103
Mercoid Corp., The, 1134-1135
Minneapolis-Honeywell Regulator Co., 1136-1137
Penn Electric Switch Co., 1139
Trane Co., The, 1000-1001
United States Register Co., 1112
White-Rodgers Electric Co., 1144
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American Radiator & Standard Sanitary Corp., 1146-1147
Automatic Products Co., 1123
Barber-Colman Co., 1098
Detroit Lubricator Co., Div. of American Radiator & Standard Sanitary Corp., 1124-1125
Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1126-1127
General Controls, 1128-1129
Minneapolis-Honeywell Regulator Co., 1136-1137
H. A. Thrush & Co., 1198-1199
Trane Co., The, 1000-1001
United States Radiator Corp., 1156-1157
Warren Webster & Co., 1226-1229
Webster Engineering Co., The, 1173
White-Rodgers Electric Co., 1144

DAMPER REGULATORS, Furnace
Automatic Products Corp., 1123
Barber-Colman Co., 1098
Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1126-1127
General Controls, 1128-1129
Hart & Cooley Mfg. Co., 1102-1103
Mercoid Corp., The, 1134-1135
Minneapolis-Honeywell Regulator Co., 1136-1137
Penn Electric Switch Co., 1139
United States Register Co., 1112
White-Rodgers Electric Co., 1144
Young Regulator Co., 1113

DAMPERS, Air Volume Control
Anemostat Corp. of America, 1094-1095
Barber-Colman Co., 1098
W. B. Connor Engineering Corp., 1020-1021, 1100-1101
Hendrick Mfg. Co., 1104-1105
Johnson Service Co., 1132-1133
Minneapolis-Honeywell Regulator Co., 1136-1137
Powers Regulator Co., The, 1140
United States Gauge, 1143
United States Register Co., 1112
Webster Engineering Co., The, 1173
Young Regulator Co., 1113

DAMPERS, Back Draft (*See Dampers, Air Volume Control*)

DAMPERS, Flue
Tuttle & Bailey, Inc., 1110-1111
United States Register Co., 1112
Young Regulator Co., 1113

DAMPERS, Mechanical
Barber-Colman Co., 1098
Johnson Service Co., 1132-1133
Minneapolis-Honeywell Regulator Co., 1136-1137
Powers Regulator Co., The, 1140
Young Regulator Co., 1113

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Air & Refrigeration Corp., 947
American Blower Corp., 948-949
Bayley Blower Co., 1067
Bryant Heater Co., 966
Buffalo Forge Co., 1069
Carrier Corp., 952-953
Clarage Fan Co., 954
Marlo Coil Co., 1060
McQuay, Inc., 992-993
John J. Nesbitt, Inc., 997
New York Blower Co., The, 1080
Niagara Blower Co., 959
Pittsburgh Lectrodryer Corp., 961
J. F. Pritchard & Co., 1043
H. J. Somers, Inc., 1028-1029
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062
York Corp., 963

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DEHYDRATION SYSTEM, Compression Equipment
Mills Industries, Inc., 1061

DEHYDRATORS, Refrigerant
Automatic Products Corp., 1123
Vulcan Radiator Corp., 1056

DESTROYERS, Soot (*See Soot Destroyers*)

DIFFUSERS, Air (*See Air Diffusers, and Ventilators, Floor and Wall*)

DISTRICT HEATING (*See Corrosion, Treatment of—Expansion Joints—Insulation, Underground—Meters, Pipe*)
H. W. Porter & Co., Inc., 1242
Ric-wil Co., The, 1243

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DRAFT CONTROL, Barometric
Preferred Utilities Mfg. Corp., 1188

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Aerofin Corp., 1050-1052
Airtherm Mfg. Co., 978
Buffalo Forge Co., 1069
Campbell Heating Co., 968-969
Carrier Corp., 952-953
Clarage Fan Co., 954
Electromode Corp., 984-985
G & O Mfg. Co., The, 1054
Modine Mfg. Co., 994-995
National Heater Co., 983
Niagara Blower Co., 959
Pittsburgh Lectrodryer Corp., 961
J. F. Pritchard & Co., 1043
Shaw-Perkins Mfg. Co., 1055
Trane Co., The, 1000-1001
Vulcan Radiator Corp., 1056
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005
Worthington Pump & Machinery Corp., 1062
York Corp., 963

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DUCTS, Prefabricated
Campbell Heating Co., 968-969
Philip Carey Mfg. Co., The, 1238-1239
United States Register Co., 1112
Grant Wilson, Inc., 1240

DUST COLLECTING EQUIPMENT
Air Devices, Inc., 1014, 1096
Air Filter Corp., 1015
Air-Maze Corp., The, 1016-1017
Aladdin Heating Corp., 1066
American Air Filter Co., Inc., 1018-1019
American Blower Corp., 948-949
Buffalo Forge Co., 1069
Chelsea Fan & Blower Co., Inc., 1072
Dollinger Corp., 1022-1023
Farr Co., 1024
General Blower Co., 1074
Ilg Electric Ventilating Co., 989, 1075
Owens-Corning Fiberglas Corp., 1026-1027
Westinghouse Electric Corp., Sturtevant Div., 1032-1039

DUST COLLECTORS, Cloth Type
American Air Filter Co., Inc., 1018-1019
Dollinger Corp., 1022-1023

EJECTORS, Sewage
Chicago Pump Co., 1201
Condenser Service & Engineering Co., Inc., 1053
Nash Engineering Co., 1202-1203

ELECTROSTATIC AIR CLEANERS
American Air Filter Co., Inc., 1018-1019
Raytheon Mfg. Co., 1025
Westinghouse Electric Corp., Sturtevant Div., 1032-1039

ENGINES, Diesel
Ingersoll-Rand, 1204
Worthington Pump & Machinery Corp., 1062

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EVAPORATORS
Acme Industries, Inc., 1049
Carrier Corp., 952-953
Condenser Service & Engineering Co., Inc., 1053
Curtis Refrigerating Machine, Div. of Curtis Mfg. Co., 1058
Farrar & Trefts, Inc., 1163
Fedders-Quigan Corp., 987
General Electric Co. (Bloomfield, N. J.), 956-957
Kennard Corp., 991
Mario Coil Co., 1060
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Worthington Pump & Machinery Corp., 1062
York Corp., 963
Young Radiator Co., 1006

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Air Devices, Inc., 1014, 1096
Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
Buffalo Forge Co., 1069
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
General Blower Co., 1074
Ilg Electric Ventilating Co., 989, 1075
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
Schwitzer-Cummins Co., 1082
Trade-Wind Motorfans, Inc., 1083
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Western Blower Co., 1087
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

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Atlantic Metal Hose Co., Inc., 1012
E. B. Badger & Sons Co., 1116-1117
Philip Carey Mfg. Co., The, 1238-1239
Chicago Metal Hose Corp., 1013
Crane Co., 1148-1149
Durant Insulated Pipe Co., 1241
Foster Wheeler Corp., 1042
Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1126-1127
Arthur Harris & Co., 1120
Illinois Engineering Co., 1222-1223
Warren Webster & Co., 1226-1229
Yarnall-Waring Co., 1235

EXPANSION LOOPS
E. B. Badger & Sons Co., 1116-1117
Durant Insulated Pipe Co., 1241
Ric-wil Co., The, 1243

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Burden Co., 1070
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
J. F. Pritchard & Co., 1043
Schwitzer-Cummins Co., 1082
Torrington Mfg. Co., The, 1084-1085
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Water Cooling Equipment Co., 1045
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

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FANS, Attic
Air Controls, Inc. (Div. of The Cleveland Heater Co.), 1063
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
G. C. Breidert Co., 1092
Buffalo Forge Co., 1069
Burden Co., 1070
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
C. A. Dunham Co., 1212-1216
Eagle-Picher Co., The, 1254
Ilg Electric Ventilating Co., 989, 1075
Jaden Mfg. Co., 990
Joy Mfg. Co., 1076-1077
Lau Blower Co., The, 1078
Herman Nelson Corp., The, 998-999
Schwitzer-Cummins Co., 1082
H. J. Somers, Inc., 1028-1029
Torrington Mfg. Co., The, 1084-1085
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Water Cooling Equipment Co., 1045
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

FANS, Axial Flow
American Blower Corp., 948-949
Bahnson Co., The, 950-951
Buffalo Forge Co., 1069
Burden Co., 1070
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
Ilg Electric Ventilating Co., 989, 1075
Joy Mfg. Co., 1076-1077
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
J. F. Pritchard & Co., 1043
Propellair Div., Robbins & Myers, Inc., 1081
Refrigerating Machinery Co., 1044
Schwitzer-Cummins Co., 1082
Water Cooling Equipment Co., 1045
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

FANS, Centrifugal
Air Controls, Inc., Div. of The Cleveland Heater Co., 1063
Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
Bayley Blower Co., 1067
Bishop & Babcock Mfg. Co., The (Massachusetts Blower Div.), 1068
Buffalo Forge Co., 1069
Burden Co., 1070
Campbell Heating Co., 968-969
Carrier Corp., 952-953
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
Eagle-Picher Co., The, 1254
Etablissements Neu, 1106
General Blower Co., 1074
Hastings Air Conditioning Co., Inc., 958
Ilg Electric Ventilating Co., 989, 1075

Jaden Mfg. Co., 990
Joy Mfg. Co., 1076-1077
Lau Blower Co., The, 1078
Morrison Products, Inc., 1079
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
Niagara Blower Co., 959
Schwitzer-Cummins Co., 1082
Torrington Mfg. Co., The, 1084-1085
Trade-Wind Motorfans, Inc., 1083
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Western Blower Co., 1087
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

FANS, Electric

Air Control Products, Inc., 1063
American Coolair Corp., 1064-1065
Buffalo Forge Co., 1069
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
General Electric Co., (Schenectady, N. Y.), 1088-1089
Ilg Electric Ventilating Co., 989, 1075
Joy Mfg. Co., 1076-1077
Herman Nelson Corp., The, 998-999
Torrington Mfg. Co., The, 1084-1085
Trade-Wind Motorfans, Inc., 1083
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

FANS, Furnace

Air Controls, Inc., Div. of The Cleveland Heater Co., 1063
Aladdin Heating Corp., 1066
American Blower Corp., 948-949
Bishop & Babcock Mfg. Co., The (Massachusetts Blower Div.), 1068
Buffalo Forge Co., 1069
Burden Co., 1070
Campbell Heating Co., 968-969
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
Duo-Therm Div. of Motor Wheel Corp., 967
General Blower Co., 1074
Hastings Air Conditioning Co., Inc., 958
Ilg Electric Ventilating Co., 989, 1075
Jaden Mfg. Co., 990
Joy Mfg. Co., 1076-1077
Lau Blower Co., The, 1078
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Morrison Products, Inc., 1079
L. J. Mueller Furnace Co., 974-975
Schwitzer-Cummins Co., 1082
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

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Bayley Blower Co., 1067
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
Etablissments Neu, 1106
General Blower Co., 1074
Ilg Electric Ventilating Co., 989, 1075
Joy Mfg. Co., 1076-1077
New York Blower Co., The, 1080
Propellair, Inc., 1081
Schwitzer-Cummins Co., 1082
Torrington Mfg. Co., The, 1084-1085
United States Air Conditioning Corp., 962
Westinghouse Electric Corp., Sturtevant Div., 1032-1039

FANS, Propeller

Air Controls, Inc., Div. of The Cleveland Heater Co., 1063
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
Bahnson Co., The, 950-951
Bishop & Babcock Mfg. Co., The (Massachusetts Blower Div.), 1068
Buffalo Forge Co., 1069
Burden Co., 1070
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
General Blower Co., 1074
Ilg Electric Ventilating Co., 989, 1075
Lau Blower Co., The, 1078
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
J. F. Pritchard & Co., 1043
Propellair, Inc., 1081
Refrigerating Machinery Co., 1044
Schwitzer-Cummins Co., 1082
Torrington Mfg. Co., The, 1084-1085
Trade-Wind Motorfans, Inc., 1083
Trane Co., The, 1000-1001
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Water Cooling Equipment Co., 1045
Western Blower Co., 1087
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

FANS, Supply and Exhaust

Air Controls, Inc., Div. of The Cleveland Heater Co., 1063
Aladdin Heating Corp., 1066
American Blower Corp., 948-949
American Coolair Corp., 1064-1065
Bayley Blower Co., 1067
Bishop & Babcock Mfg. Co., The (Massachusetts Blower Div.), 1068
Buffalo Forge Co., 1069
Carrier Corp., 952-953
Champion Blower & Forge Co., 1071
Chelsea Fan & Blower Co., Inc., 1072
Clarage Fan Co., 954
DeBothezat Fans Div., American Machine & Metals, Inc., 1073
General Blower Co., 1074
Ilg Electric Ventilating Co., 989, 1075
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Joy Mfg. Co., 1076-1077
Lau Blower Co., The, 1078
Herman Nelson Corp., The, 998-999
New York Blower Co., The, 1080
Propellair Div., Robbins & Myers, Inc., 1081
Schwitzer-Cummins Co., 1082
H. J. Somers, Inc., 1028-1029
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Trane Co., The, 1000-1001
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Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Water Cooling Equipment Co., 1045
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005

FANS, Ventilating (*See Fans, Attic, Axial Flow, Centrifugal, etc.*)

FEED WATER HEATERS (*See Heaters, Feed Water*)

FEED WATER REGULATORS (*See Regulators, Feed Water*)

FEEDERS, Boiler Water

Combustion Control Corp., 986
McDonnell & Miller, Inc., 1192-1193
Mueller Steam Specialty Co., Inc., 1234
Penn Electric Switch Co., 1139
Sarco Co., Inc., 1224-1225
Warren Webster & Co., 1226-1229

FELT, Insulating (*See Insulation, Felt*)

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Douglas Co., 1253
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Korfund Co., Inc., The, 1259
Lockport Cotton Batting Co., 1264
Owens-Corning Fiberglas Corp., 1026-1027
Grant Wilson, Inc., 1240
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Air Devices, Inc., 1014, 1096
Air Filter Corp., 1015
Air-Maze Corp., The, 1016-1017
Air & Refrigeration Corp., 947
American Air Filter Co., Inc., 1018-1019
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Dollinger Corp., 1022-1023
Farr Co., 1024
Owens-Corning Fiberglas Corp., 1026-1027
Raytheon Mfg. Co., 1025
Research Products Corp., 1030
H. J. Somers, Inc., 1028-1029
Supreme Air Filter Co., 1031
Westinghouse Electric Corp., Sturtevant Div., 1032-1039

FILTERS, Grease

Research Products Corp., 1030
Supreme Air Filter Co., 1031

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Air-Maze Corp., The, 1016-1017
Condenser Service & Engineering Co., Inc., 1053
Dollinger Corp., 1022-1023

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Armstrong Cork Co. (Building Materials Div.), 1250
Babcock & Wilcox Co., The, 1159
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FITTINGS, Flared
Grinnell Co., Inc., 988, 1118-1119

FITTINGS, Hot Water Heating Systems
Jas. P. Marsh Corp., 1232-1233
Taco Heaters, Inc., 1197
H. A. Thrush & Co., 1198-1199
Trane Co., The, 1000-1001

FITTINGS, Jacketed Steam and Oil
Parks-Cramer Co., 960

FITTINGS, Pipe, Flanged
Baker Ice Machine Co., Inc., 1059
Crane Co., 1148-1149
Grinnell Co., Inc., 988, 1118-1119
Henry Valve Co., 1130
Mueller Brass Co., 1010-1011
Worthington Pump & Machinery Corp., 1062
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Crane Co., 1148-1149
Grinnell Co., Inc., 988, 1118-1119
Henry Valve Co., 1130
Mueller Brass Co., 1010-1011
Worthington Pump & Machinery Corp., 1062
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Crane Co. 1148-1149
Mueller Brass Co., 1010-1011

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Durant Insulated Pipe Co., 1241
H. W. Porter & Co., Inc., 1242
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Grinnell Co., Inc., 988, 1118-1119
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Carnegie-Illinois Steel Co., 1115
Grinnell Co., Inc., 988, 1118-1119
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FORCED DRAFT COOLING TOWERS (*See Fans, Cooling Towers, Induced Draft, Mechanical Draft*)
Air & Refrigeration Corp., 947
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J. F. Pritchard & Co., 1043
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Combustion Equipment Div., Todd Shipyards Corp., 1186

FURNACE PIPE
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L. J. Mueller Furnace Co., 974-975
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FURNACES, Electric
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FURNACES, Oil Burning, Floor
Air Devices, Inc., 1014, 1096
Automatic Burner Corp., 1177
H. C. Little Burner Co., 1184

FURNACES, Wall
H. C. Little Burner Co., 1184
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086

FURNACES, Warm Air, Heavy Duty
Airtherm Mfg. Co., 978
Campbell Heating Co., 968-969
Chicago Steel Furnace Co., 979
Dravo Corp., 980-981
Iron Fireman Mfg. Co., 1176-1177
Lee Engineering Co., 982
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
Ray Oil Burner Co., 1185
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Airtemp Div., Chrysler Corp., 970-971
Aladdin Heating Corp., 1066
American Radiator & Standard Sanitary Corp., 1146-1147
Bryant Heater Co., 966
Campbell Heating Co., 968-969
Crane Co., 1148-1149
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General Electric Co. (Bloomfield, N. J.), 956-957
Hoffman Specialty Co., 1218-1221
Iron Fireman Mfg. Co., 1174-1175
S. T. Johnson Co., 1180-1181
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Waterman-Waterbury Co., The, 976-977
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Jas. P. Marsh Corp., 1232-1233
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GAGES, Ammonia
Baker Ice Machine Co., Inc., 1057
Crane Co., 1148-1149
Jas. P. Marsh Corp., 1232-1233
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GAGES, Compound
Crane Co., 1148-1149
Dole Valve Co., The, 1236
Jas. P. Marsh Corp., 1232-1233
Trane Co., The, 1000-1001
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Minneapolis-Honeywell Regulator Co., 1136-1137
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GAGES, Pressure
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Fulton Sylphon Div., Robertshaw-Fulton Controls Co., 1126-1127
Jas. P. Marsh Corp., 1232-1233
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Taylor Instrument Cos., 1142
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GAGES, Steam
Crane Co., 1148-1149
Hoffman Specialty Co., 1218-1221
Jas. P. Marsh Corp., 1232-1233
Minneapolis-Honeywell Regulator Co., 1136-1137
Trane Co., The, 1000-1001
United States Gauge, 1143
Warren Webster & Co., 1226-1229

GAGES, Tank
Jas. P. Marsh Corp., 1232-1233
Minneapolis-Honeywell Regulator Co., 1136-1137
United States Gauge, 1143

GAGES, Vacuum
Crane Co., 1148-1149
Hoffman Specialty Co., 1218-1221
Jas. P. Marsh Corp., 1232-1233
Minneapolis-Honeywell Regulator Co., 1136-1137
Moeller Instrument Co., 1138
Taylor Instrument Cos., 1142
United States Gauge, 1143
Warren Webster & Co., 1226-1229

GAGES, Vapor
Crane Co., 1148-1149
Hoffman Specialty Co., 1218-1221
Jas. P. Marsh Corp., 1232-1233
Minneapolis-Honeywell Regulator Co., 1136-1137
United States Gauge, 1143
Warren Webster & Co., 1226-1229

GAGES, Water
Crane Co., 1148-1149
H. A. Thrush & Co., 1198-1199
United States Gauge, 1143
Yarnall-Waring Co., 1235

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Bryant Heater Co., 966
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L. J. Mueller Furnace Co., 974-975
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Pittsburgh Corning Corp., 1246-1247

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Armstrong Cork Co. (Building Materials Div.), 1250
Owens-Illinois Glass Co., 1248
Pittsburgh Corning Corp., 1246-1247

GOVERNORS, Pump
Combustion Control Corp., 986
McDonnell & Miller, Inc., 1192-1193
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Anemostat Corp. of America, 1094-1095
Auer Register Co., The, 1097
Barber-Colman Co., 1098
Etablissements Neu, 1106
General Blower Co., 1074
Hart & Cooley Mfg. Co., 1102-1103
Hendrick Mfg. Co., 1104-1105
Independent Register Co., The, 1107
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Pyle-National Co., The, 1108
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Tuttle & Bailey, Inc., 1110-1111
United States Air Conditioning Corp., 962
United States Register Co., 1112
Vulcan Radiator Co., 1056
Young Regulator Co., 1113

GUIDES, Pipe
H. W. Porter & Co., Inc., 1242

HANGERS, Pipe
Grinnell Co., Inc., 988, 1118-1119
H. W. Porter & Co., Inc., 1242
Ric-wil Co., The, 1243

HANGERS, Radiator
Bell & Gossett Co., 1194-1195
Carty & Moore Engineering Co., 1209
Shaw-Perkins Mfg. Co., 1005
United States Radiator Corp., 1156-1157
Vulcan Radiator Co., 1056

HEADS, Exhaust
G. C. Breidert Co., 1092
Crane Co., 1148-1149
Mueller Steam Specialty Co., Inc., 1234

HEADS, Sprinkler (*Fire Protection*)
Grinnell Co., Inc., 988, 1118-1119

HEAT EXCHANGERS
J. F. Pritchard & Co., 1043

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Airtherm Mfg. Co., 978
General Electric Co., (Schenectady, N. Y.), 1088-1089
G & O Mfg. Co., The, 1054
Kennard Corp., 991
Marlo Coil Co., 1060
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
John J. Nesbitt, Inc., 997
New York Blower Co., The, 1080
Pan-L-Heat Corp., 1196
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
Warren Webster & Co., 1226-1229
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Young Radiator Co., 1006

HEATERS, Air
Aerofin Corp., 1050-1052
Airtherm Mfg. Co., 978
Buffalo Forge Co., 1069
Campbell Heating Co., 968-969
Carrier Corp., 952-953
Chicago Steel Furnace Co., 979
Combustion Engineering Co., 1162
Condenser Service & Engineering Co., Inc., 1053
Dravo Corp., 980-981
Duo-Therm Div. of Motor Wheel Corp., 967
Electromode Corp., 984-985
Etablissements Neu, 1106
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Fitzgibbons Boiler Co., Inc., 1164-1165
General Electric Co., (Schenectady, N. Y.), 1088-1089
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Ilg Electric Ventilating Co., 989, 1075
Kennard Corp., 991
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John J. Nesbitt, Inc., 997
Pan-L-Heat Corp., 1196
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005
Young Radiator Co., 1006

HEATERS, Automatic Hot Water, Domestic
Air Devices, Inc., 1014, 1096
Airtemp Div., Chrysler Corp., 970-971
American Radiator & Standard Sanitary Corp., 1146-1147
Automatic Burner Corp., 1177
Bryant Heater Co., 966
Crane Co., 1148-1149
General Electric Co., (Schenectady, N. Y.), 1086-1087
S. T. Johnson Co., 1180-1181
H. C. Little Burner Co., 1184
Pan-L-Heat Corp., 1196
Petroleum Heat & Power Co., 1182-1183
Preferred Utilities Mfg. Corp., 1188
Ray Oil Burner Co., 1185
Westinghouse Electric Corp., Box 868, Pittsburgh, 1032-1039
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

HEATERS, Blast
Aerofin Corp., 1050-1052
Airtherm Mfg. Co., 978
Buffalo Forge Co., 1069
Carrier Corp., 952-953
Clarage Fan Co., 954
Electromode Corp., 984-985
G & O Mfg. Co., The, 1054
Kennard Corp., 991
Lee Engineering Co., 982
Marlo Coil Co., 1060
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
D. J. Murray Mfg. Co., 996
John J. Nesbitt, Inc., 997
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Vulcan Radiator Co., 1056
Warren Webster & Co., 1226-1229
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
Young Radiator Co., 1006

HEATERS, Cabinet
Airtherm Mfg. Co., 978
C. A. Dunham Co., 1212-1216
Modine Mfg. Co., 994-995
Herman Nelson Corp., The, 998-999
John J. Nesbitt, Inc., 997
Trane Co., The, 1000-1001
Warren Webster & Co., 1226-1229
Young Radiator Co., 1006

HEATERS, Electric
Philip Carey Mfg. Co., The, 1238-1239
Crane Co., 1148-1149
Electromode Corp., 984-985
General Electric Co., (Schenectady, N. Y.), 1088-1089
Ilg Electric Ventilating Co., 989, 1075
Westinghouse Electric Corp., Box 868, Pittsburgh, 1032-1039

HEATERS, Feed Water
Bell & Gossett Co., 1194-1195
Brownell Co., The, 1161
Condenser Service & Engineering Co., Inc., 1053
Foster Wheeler Corp., 1041
National Radiator Co., The, 1150-1151
Westinghouse Electric Corp., Box 868, Pittsburgh, 1032-1039
Worthington Pump & Machinery Corp., 1062

HEATERS, Fuel Oil
Airtherm Mfg. Co., 978
Automatic Burner Corp., 1177
R. W. Beckett Corp., 1178
Bell & Gossett Co., 1194-1195
Campbell Heating Co., 968-969
Carrier Corp., 952-953
Chicago Steel Furnace Co., 979
Combustion Equipment Div., (Todd Shipyards Corp.), 1186
Condenser Service & Engineering Co., Inc., 1053
Dravo Corp., 980-981
General Electric Co., (Schenectady, N. Y.), 1088-1089
National Heater Co., 983
National Radiator Co., The, 1150-1151
Petroleum Heat & Power Co., 1182-1183
York-Shipley, Inc., 1189

HEATERS, Gas
Airtherm Mfg. Co., 978
Aladdin Heating Corp., 1066
Bryant Heater Co., 966
Campbell Heating Co., 968-969
Chicago Steel Furnace Co., 979
Crane Co., 1148-1149
Dravo Corp., 980-981
Ilg Electric Ventilating Co., 989, 1075
Lee Engineering Co., 982
Meyer Furnace Co., The, 972-973
National Heater Co., 983
Pacific Steel Boiler Div., U. S. Radiator Corp., 1155
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086

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Air Devices, Inc., 1014, 1096
Aldrich Co., 1176
American Radiator & Standard Sanitary Corp., 1146-1147
Bell & Gossett Co., 1194-1195
Brownell Co., The, 1161
Burnham Corp., 1145
Condenser Service & Engineering Co., Inc., 1053
Crane Co., 1148-1149
Fitzgibbons Boiler Co., Inc., 1164-1165
Kewanee Boiler Corp., 1166-1169
H. C. Little Burner Co., 1184
L. J. Mueller Furnace Co., 974-975
Pacific Steel Boiler Div., U. S. Radiator Corp., 1155
Preferred Utilities Mfg. Corp., 1188
H. B. Smith Co., Inc., The, 1154
Taco Heaters, Inc., 1197
Trane Co., The, 1000-1001
United States Radiator Corp., 1156-1157
Weil-McLain Co., 1158
York-Shipley, Inc., 1189

HEATERS, Indirect
American Radiator & Standard Sanitary Corp., 1146-1147
Bell & Gossett Co., 1194-1195
Crane Co., 1148-1149
John J. Nesbitt, Inc., 997
Taco Heaters, Inc., 1197
H. A. Thrush & Co., 1198-1199

HEATERS, Storage
Bell & Gossett Co., 1194-1195
Brownell Co., The, 1161
Kewanee Boiler Corp., 1166-1169

HEATERS, Tank
American Radiator & Standard Sanitary Corp., 1146-1147
Bell & Gossett Co., 1194-1195
Bryant Heater Co., 966
Burnham Corp., 1145
Fitzgibbons Boiler Co., Inc., 1164-1165
General Electric Co., (Schenectady, N. Y.), 1088-1089
H. B. Smith Co., Inc., The, 1154
Taco Heaters, Inc., 1197
Weil-McLain Co., 1158

HEATERS, Unit
Airtherm Mfg. Co., 978
American Blower Corp., 948-949
Bayley Blower Co., 1067
Bishop & Babcock Mfg. Co., The (Massachusetts Blower Div.), 1068
Bryant Heater Co., 966
Buffalo Forge Co., 1069
Burnham Corp., 1145
Carrier Corp., 952-953
Chicago Steel Furnace Co., 979
Clarage Fan Co., 954
Dravo Corp., 980-981
C. A. Dunham Co., 1212-1216
Electromode Corp., 984-985
Fedders-Quigan Corp., 987
General Electric Co., (Schenectady, N. Y.), 1088-1089
Grinnell Co., Inc., 988, 1118-1119
Hastings Air Conditioning Co., Inc., 958
Ilg Electric Ventilating Co., 989, 1075
Jaden Mfg. Co., 990
Kennard Corp., 991
Lee Engineering Co., 982
McQuay, Inc., 992-993
Modine Mfg. Co., 994-995
D. J. Murray Mfg. Co., 996
National Heater Co., 983
National Radiator Co., The, 1150-1151
Herman Nelson Corp., The, 998-999
John J. Nesbitt, Inc., 997
New York Blower Co., The, 1080
Niagara Blower Co., 959
Refrigeration Economics Co., Inc., 1002
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
Warren Webster & Co., 1226-1229
Western Blower Co., 1087
Westinghouse Electric Corp., Sturtevant Div., 1032-1039
L. J. Wing Mfg. Co., 1003-1005
Young Radiator Co., 1006

HEATERS, Unit, Gas Fired
Airtherm Mfg. Co., 978
Aladdin Heating Corp., 1066
American Radiator & Standard Sanitary Corp., 1146-1147
Bryant Heater Co., 966
Buffalo Forge Co., 1069
Carrier Corp., 952-953
Chicago Steel Furnace Co., 979
Dravo Corp., 980-981
Hastings Air Conditioning Co., Inc., 958
Ilg Electric Ventilating Co., 989, 1075
Lee Engineering Co., 982
L. J. Mueller Furnace Co., 974-975
D. J. Murray Mfg. Co., 996
National Heater Co., 983
United States Air Conditioning Corp., 962
Utility Appliance Corp., (formerly Utility Fan Corp.), 1086

HEATING, PUMPING and STRAINING UNITS, Fuel Oil
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Aerofin Corp., 1050-1052
Airtherm Mfg. Co., 978
American Blower Corp., 948-949
Campbell Heating Co., 968-969
Carrier Corp., 952-953
Chicago Steel Furnace Co., 979
Clarage Fan Co., 954
Charles Demuth & Sons, 1099
Dravo Corp., 980-981
Electromode Corp., 984-985
Iron Fireman Mfg. Co., 1174-1175
Lee Engineering Co., 982
Marlo Coil Co., 1060
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
Niagara Blower Co., 959
Trane Co., The, 1000-1001
United States Air Conditioning Corp., 962
United States Radiator Corp., 1156-1157
Westinghouse Electric Corp., Sturtevant Div., 1032-1039

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Airtemp Div., Chrysler Corp., 970-971
Aladdin Heating Corp., 1066
Bahnson Co., The, 950-951
Bryant Heater Co., 966
Buffalo Forge Co., 1069
Burnham Corp., 1145
Campbell Heating Co., 968-969
Charles Demuth & Sons, 1099
Duo-Therm Div., Motor Wheel Corp., 967
Electromode Corp., 984-985
Fedders-Quigan Corp., 987
General Electric Co., (Bloomfield, N. J.), 956-957
Iron Fireman Mfg. Co., 1174-1175
H. C. Little Burner Co., 1184
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
Ray Oil Buner Co., 1185
Trane Co., The, 1000-1001
U. S. Radiator Corp., 1156-1157
Waterman-Waterbury Co., The, 976-977
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

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Airtemp Div., Chrysler Corp., 970-971
Airtherm Mfg. Co., 978
Aldrich Co., 1176
Barnes & Jones, Inc., 1208
Bell & Gossett Co., 1194-1195
Bryant Heater Co., 966
Burnham Corp., 1145
Campbell Heating Co., 968-969
Chicago Steel Furnace Co., 979
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Charles Demuth & Sons, 1099
Dravo Corp., 980-981
C. A. Dunham Co., 1212-1216
Duo-Therm Div., Motor Wheel Corp., 967
Electromode Corp., 984-985
General Electric Co. (Bloomfield, N. J.), 956-957
Hoffman Specialty Co., 1218-1221
Illinois Engineering Co., 1222-1223
Iron Fireman Mfg. Co., 1174-1175
Lee Engineering Co., 982
H. C. Little Burner Co., 1184
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
National Radiator Co., The, 1150-1151
Ray Oil Burner Co., 1185
Sarco Co., Inc., 1224-1225
Spence Engineering Co., Inc., 1141
Spencer Heater Div., The Avco Mfg. Corp., 1152-1153
Taco Heaters, Inc., 1197
Trane Co., The, 1000-1001
United States Radiator Corp., 1156-1157
Warren Webster Co., 1226-1229
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
L. J. Wing Mfg. Co., 1003-1005
York-Shipley, Inc., 1189

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Airtemp Div., Chrysler Corp., 970-971
Burnham Corp., 1145
Campbell Heating Co., 968-969
Iron Fireman Mfg. Co., 1174-1175
Lee Engineering Co., 982
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
National Radiator Co., The, 1150-1151
United States Radiator Corp., 1156-1157
Waterman-Waterbury Co., The, 976-977

HEATING SYSTEMS, Electric

Electromode Corp., 984-985

HEATING SYSTEMS, Furnace

Airtemp Div., Chrysler Corp., 970-971
Airtherm Mfg. Co., 978
Campbell Heating Co., 968-969
Crane Co., 1148-1149
Dravo Corp., 980-981
Iron Fireman Mfg. Co., 1174-1175
Lee Engineering Co., 982
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
National Radiator Co., The, 1150-1151
Waterman-Waterbury Co., The, 976-977
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Airtemp Div., Chrysler Corp., 970-971
Airtherm Mfg. Co., 978
Aladdin Heating Corp., 1066
Aldrich Co., 1176
Bryant Heater Co., 966
Burnham Corp., 1145
Campbell Heating Co., 968-969
Chicago Steel Furnace Co., 979
Crane Co., 1148-1149
Dravo Corp., 980-981
General Electric Co., (Bloomfield, N. J.), 956-957
Lee Engineering Co., 982
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
National Radiator Co., The, 1150-1151
United States Radiator Corp., 1156-1157
Waterman-Waterbury Co., The, 976-977

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Airtemp Div., Chrysler Corp., 970-971
Bell & Gossett Co., 1194-1195
Burnham Corp., 1145
C. A. Dunham Co., 1212-1216
Durant Insulated Pipe Co., 1241
General Electric Co., (Bloomfield, N. J.), 956-957
Hoffman Specialty Co., Inc., 1218-1221
Iron Fireman Mfg. Co., 1174-1175
Jas. P. Marsh Corp., 1232-1233
L. J. Mueller Furnace Co., 974-975
National Radiator Co., The, 1150-1151
Pan-L-Heat Corp., 1196
Ric-wiL Co., The, 1243
Sarco Co., Inc., 1224-1225
Taco Heaters, Inc., 1197
Trane Co., The, 1000-1001
H. A. Thrush & Co., 1198-1199
United States Radiator Corp., 1156-1157
Warren Webster & Co., 1226-1229
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

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Air Devices, Inc., 1014, 1096
Airtemp Div., Chrysler Corp., 970-971
Airtherm Mfg. Co., 978
Aldrich Co., 1176
Burnham Corp., 1145
Campbell Heating Co., 968-969
Chicago Steel Furnace Co., 979
Charles Demuth & Sons, 1099
Dravo Corp., 980-981
Duo-Therm Div., Motor Wheel Corp., 967
General Electric Co. (Bloomfield, N. J.), 956-957
Iron Fireman Mfg. Co., 1174-1175
S. T. Johnson Co., 1180-1181
Kewanee Boiler Corp., 1166-1169
Lee Engineering Co., 982
H. C. Little Burner Co., 1184
Meyer Furnace Co., The, 972-973
L. J. Mueller Furnace Co., 974-975
National Heater Co., 983
National Radiator Co., The, 1150-1151
Petroleum Heat & Power Co., 1182-1183
United States Radiator Corp., 1156-1157
Waterman-Waterbury Co., The, 976-977
Williams Oil-O-Matic Div., Eureka Williams Corp., 1187
York-Shipley, Inc., 1189

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Airtemp Div., Chrysler Corp., 970-971
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Chicago Pump Co., 1201
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Ingersoll-Rand, 1204
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Trane Co., The, 1000-1001
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PUMPS, Fuel Oil
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Buffalo Pumps, Inc., 1200
Chicago Pump Co., 1201
Jas. P. Marsh Corp., 1232-1233
Nash Engineering Co., The, 1202-1203
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PUMPS, Turbine
Chicago Pump Co., 1201
Nash Engineering Co., The, 1202-1203
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Allis-Chalmers Mfg. Co., 964-965
Chicago Pump Co., 1201
C. A. Dunham Co., 1212-1216
Hoffman Specialty Co., 1218-1216
Ingersoll-Rand, 1204
Nash Engineering Co., The, 1202-1203
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Aerofin Corp., 1050-1052
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McQuay, Inc., 992-993
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Refrigeration Economics Co., Inc., 1002
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Burnham Corp., 1145
Crane Co., 1148-1149
C. A. Dunham Co., 1212-1216
United States Radiator Corp., 1156-1157
Vulcan Radiator Co., The, 1056

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C. A. Dunham Co., 1212-1216
United States Radiator Corp., 1156-1157
Vulcan Radiator Co., The, 1056
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Burnham Corp., 1145
Crane Co., 1148-1149
D. J. Murray Mfg. Co., 996
National Radiator Co., The, 1150-1151
United States Radiator Corp., 1156-1157
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Airtherm Mfg. Co., 978
C. A. Dunham Co., 1212-1216
G & O Mfg. Co., The, 1054
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Airtherm Mfg. Co., 978
Burnham Corp., 1145
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C. A. Dunham Co., 1212-1216
Modine Mfg. Co., 994-995
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American Radiator & Standard Sanitary Corp., 1146-1147
Burnham Corp., 1145
Crane Co., 1148-1149
C. A. Dunham Co., 1212-1216
Modine Mfg. Co., 994-995
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Pan-L-Heat Corp., 1196
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Babcock & Wilcox Co., The, 1159
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Johnson Service Co., 1132-1133
Minneapolis-Honeywell Regulator Co., 1136-1137
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Barber-Coleman Co., 1098
Crane Co., 1148-1149
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Webster Engineering Co., The, 1173
White-Rodgers Electric Co., 1144
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Mercoid Corp., The, 1134-1135
Mueller Steam Specialty Co., Inc., 1234
Penn Electric Switch Co., 1139
Sarco Co., Inc., 1224-1225
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REGULATORS, Furnace
Automatic Products Co., 1123
Barber-Colman Co., 1098
General Controls, 1128-1129
Hart & Cooley Mfg. Co., 1102-1103
Minneapolis-Honeywell Regulator Co., 1136-1137
Penn Electric Switch Co., 1139
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General Controls, 1128-1129
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Barber-Colman Co., 1098
Clark Mfg. Co., 1210-1211
Crane Co., 1148-1149
C. A. Dunham Co., 1212-1216
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Vinco Co., Inc., The, 1190-1191

RUST AND SCALE REMOVER
Vinco Co., Inc., The, 1190-1191

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American Air Filter Co., Inc., 1018-1019
Dollinger Corp., 1022-1023
Mueller Steam Specialty Co., Inc., 1234
Penn Electric Switch Co., 1139
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SEPARATORS, Dust
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Dollinger Corp., 1022-1023
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Air-Maze Corp., The, 1016-1017
Baker Ice Machine Co., Inc., 1059
Clark Mfg. Co., 1210-1211
Crane Co., 1148-1149
Dollinger Corp., 1022-1023
Illinois Engineering Co., 1222-1223
Warren Webster & Co., 1226-1229
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Crane Co., 1148-1149
Farrar & Trefts, Inc., 1163
Illinois Engineering Co., 1222-1223
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Warren Webster & Co., 1226-1229
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American Rolling Mill Co., The, 1114
Carnegie-Illinois Steel Corp., 1115
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SHEETS, High Tensile
American Rolling Mill Co., The, 1114
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American Rolling Mill Co., The, 1114
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United States Steel Corp., Sub., 1115

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American Flange & Mfg. Co., Inc., 1249
American Rolling Mill Co., The, 1114
Carnegie-Illinois Steel Corp., 1115
United States Steel Corp., Sub., 1115

SHEETS, Steel
American Flange & Mfg. Co., Inc., 1249
American Rolling Mill Co., The, 1114
Carnegie-Illinois Steel Corp., 1115
United States Steel Corp., Sub., 1115

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Celotex Corp., The, 1252
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Insul-Mastic Corp. of America, 1255
Insul-Wool Insulation Corp., 1258
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Jos. A. Martocello & Co., 1047
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April Showers Co., 1040
Carrier Corp., 952-953
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Jos. A. Martocello & Co., 1047
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Babcock & Wilcox Co., The, 1159
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Hoffman Specialty Co., 1218-1221
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Mueller Steam Specialty Co., Inc., 1234
Sarco Co., Inc., 1224-1225
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Clark Mfg. Co., 1210-1211
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Alco Valve Co., 1122
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Illinois Testing Laboratories, Inc., 1131
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By reference to these indices, the manufacturers names and the page numbers, any item of equipment or materials, and the producers address, may be located quickly.

Air & Refrigeration Corporation

475 Fifth Avenue, **New York 17, N. Y.**

Atlanta, Ga. **Detroit, Mich.**

Air Conditioning, Humidifying, Dehumidifying, Cooling, Scrubbing, Air Washing and Purification Apparatus

Air & Refrigeration Corporation specializes in the design and manufacture of industrial and comfort-conditioning apparatus where maintenance of suitable humidity and temperature within closely controllable limits is essential. This specialization is based on technical knowledge and ingenuity born of extensive experience in the solution of the more difficult problems of air conditioning. A complete line of air conditioning equipment is available to contractors and owners for all phases of humidifying, dehumidifying, cooling and washing.

Capillary Air Washers provide a superior type humidifying, dehumidifying, air washing, cleaning and cooling unit for central station apparatus. For most purposes the Capillary Washer requires 1/3 the volume of water at 1/3 the pressure used by conventional spray equipment. They are available with factory insulated casings and tank for central station applications. *For complete data, see Bulletin G-3.*

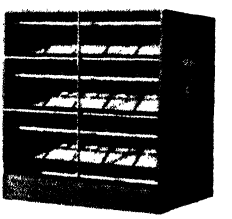
Capillary Unit Conditions are factory insulated and assembled, ready for use. They include fan, motor, drive, heating coils, Capillary Cells with suitable sprays, spray pump and mixing dampers. Units are designed for floor mounting or for ceiling suspension, and can be arranged for the reception of cooling coils, if required. *Complete description and engineering data will be found in Bulletin G-3.*

Spray Type Air Washers for washing, humidifying and dehumidifying air are all basically the same. A & R Spray Washers include special features of design developed to insure more efficient and dependable operation, lower maintenance costs, and, in many cases, lower installation costs. Such features relate especially to eliminators, collecting tanks, flooded baffles, nozzle arrangement, etc. Spray Washers can be supplied with factory insulated casings and tank for central stations applications. *For details, see Bulletin AW-1.*

Sprayed Coil Dehumidifiers for year-round treatment of air are complete with heating coils, sprays, circulating pump and glass mat eliminators. Sprayed coil dehumidifiers are factory insulated and complete, ready for assembly in the field. Special features in design insure continuous washing and cleaning of finned surfaces and easy accessibility to all parts. *For engineering information and detailed description, see Bulletin SC-1.*

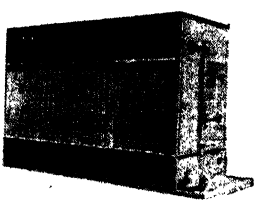
A & R Insulated Panels consist of insulation between metal sheet on one side and hard fiber board on the other, the three laminated and cemented together under pressure. This unique panel design includes the structural frame to form units which require *only bolting together* to make enclosures of any required shape for plenum chambers and many other purposes. Panels are available in widths from 3 in. to 48 in., and in lengths to 12 ft. Their use insures tremendous economies in field labor. *For details, see Bulletin P-1.*

Submit design and capacity for special recommendations; write for catalog and engineering data.

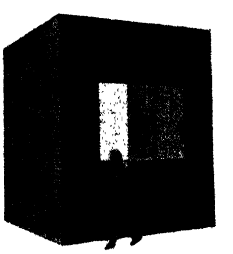


Factory Insulated Class 1 Capillary Air Washer—Capacity 33,000 cfm.

Factory Insulated Size #3-4 Capillary Unit Conditioner—Capacity 16,000 cfm.



Factory Insulated Prewasher for Lint Removal—Capacity 12,000 cfm.



Factory Insulated Plenum Chamber—Size 18 ft Long, 12 ft Wide x 15 ft High.

American Blower Corporation

Detroit 32, Michigan

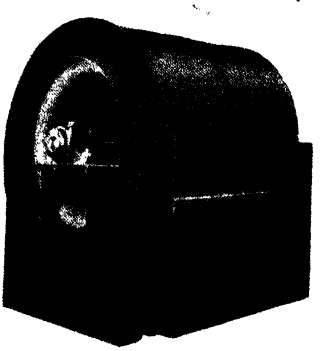
CANADIAN SIROCCO COMPANY, LTD.

310 Ellis Street, Windsor, Ontario

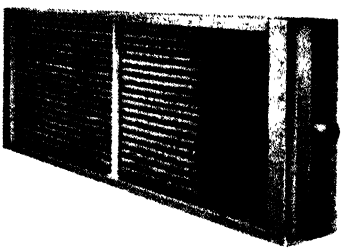
Branch Offices in Principal Cities

Division of AMERICAN RADIATOR & Standard Sanitary CORPORATION

AIR CONDITIONING — HUMIDIFYING — DEHUMIDIFYING — COOLING — VENTILATING — HEATING — VAPOR-ABSORPTION — DRYING — AIR WASHING AND PURIFICATION — EXHAUSTING EQUIPMENT AND MECHANICAL DRAFT APPARATUS



Double Inlet "ABC" Multi-blade Fan—above, is a heavy duty ventilating fan. The wheel has narrow, forward pitched blades. Low tip speeds assure quiet operation. Request Bulletin A-801. Bulletin A-603 describes backwardly inclined, non-overloading HS Fan.



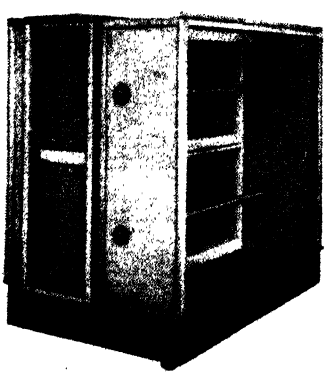
Heating and Cooling Coils—above, American Blower heating and cooling coils offer a number of improvements in design and construction. Available in a complete range of sizes and types, including:

Bulletin B-1218 { Type S steam coils; Type D double tube coils; Type U return blend coils; Type B booster coils

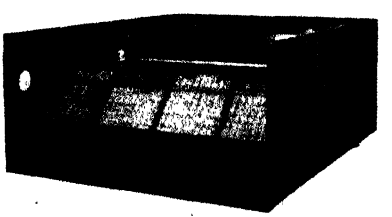
Bulletin 1521 { Type W water coils; Type C cleanable water coils; Type X direct expansion coils

Bulletin B-1318 Type H heavy duty coils

"ABC" Utility Sets—complete packaged units, direct connected or V-Belt short coupled drive for duct applications. Sizes for wide variety of ventilating problems. Quiet, compact. Bulletin 2814.



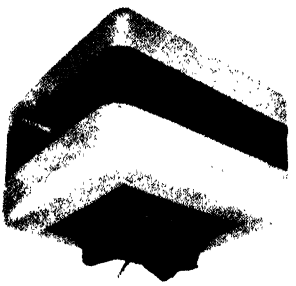
American Blower Air Washer—above, cleans, purifies and freshens air, removes dust, odors and bacteria, cools if desired and provides an effective method of controlling humidity. Bulletin 3623.



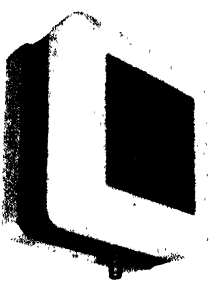
Capillary Air Washers—above, for high efficiency in cleaning, humidification, cooling and dehumidification of air. Air is forced at low resistance through long, irregular passages of small size formed by a large amount of thoroughly wetted glass surface. Write for Bulletin 3723.

TYPES OF AMERICAN BLOWER CORPORATION AIR HANDLING AND CONDITIONING EQUIPMENT

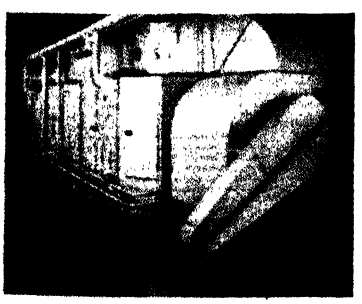
All types of air handling and air conditioning equipment for industrial applications, process work, drying, cooling; also equipment for stores, offices, shops, public buildings, power plants, etc., and attic and kitchen ventilation for homes.



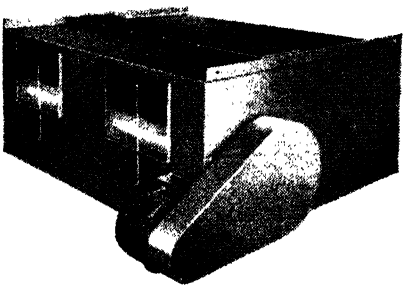
"ABC" Vertical Unit Heaters—for ceiling applications, give an even, wide floor area distribution of heat. For either steam or hot water heating systems. Variable speed, 2-speed and constant speed models. Write for Bulletin 6417.



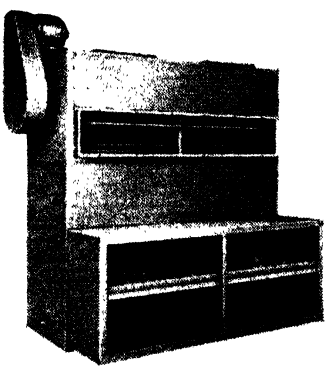
Venturafin Unit Heaters—for many general purpose heating jobs. Wall or ceiling mounted. Streamline construction. rugged heating elements. Steam or hot water. Request Bulletin 6317.



Air Conditioning Central Systems—provide an effective way of cooling, heating, humidifying, dehumidifying and purifying air in all classes of business and public buildings where a duct system is desirable. Write for special data.



Heating and Ventilating Units—with air filters and Aileron control. Ideal wherever attractive, quiet and economical heating and ventilating units are required. Wall, floor or ceiling mounting. Offer great flexibility of design and arrangement to meet specific needs. Bulletin 6017.



American Blower Air Conditioning Units—*Type A* for all normal unitary type commercial and industrial applications. Cooling, heating, humidifying. Capacities 1000 cfm—13,600 cfm. *Type S* for commercial and industrial applications desiring washed air or high relative humidities. Capacities 1000 cfm—13,600 cfm. *Type M*, large capacity for central system installation with separately mounted fan. Cooling, dehumidification, heating, humidifying. Capacities 1000 cfm—41,000 cfm. Bulletin 6527.

93 Worth St.
New York, N. Y.

703 Embree
Crescent
Westfield, N. J.

553 S. Figueroa St.
Los Angeles, Calif.

The Bahnson Company

Winston-Salem, N. C.

Bahnson System
AIR CONDITIONING ENGINEERS

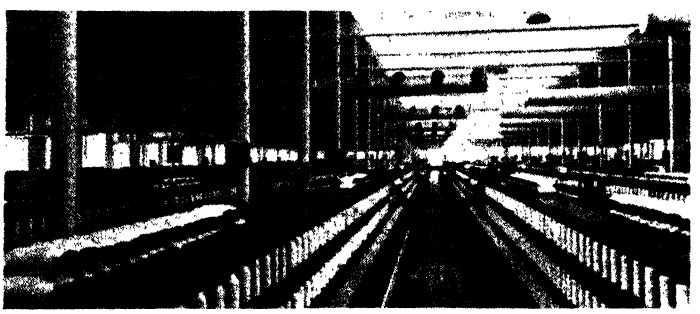
886 Drewry St.
Atlanta, Ga.

43 Virginia Apts.
Greenville, S. C.

1001 S. Marshall St.
Winston-Salem,
N. C.

HUMIDUCT

AIR CONDITIONING SYSTEM



The Bahnson Humiduct is a unit system of air conditioning for humidifying, ventilating, evaporative or refrigerative cooling, heating, filtering, electrostatic air cleaning, and dehumidifying, in any desired combination. Through the application of delivering saturated air plus entrained moisture, wherein part of the evaporation may take place in the room, supplementary evaporation is not required with the Humiduct. The use of this principle allows a more accurate control of humidity with a lower volume of air than is required with saturated air types of systems.

BAHNSON CENTRAL STATION AIR CONDITIONING

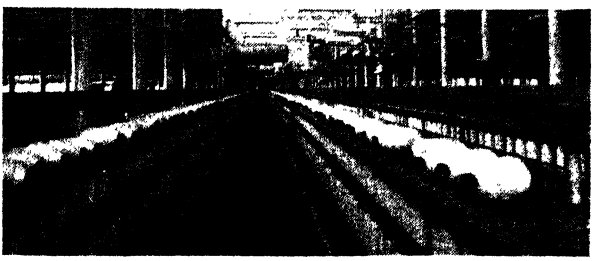
Air washers and other components for evaporative cooling or refrigerative cooling systems are designed, manufactured, and installed by Bahnson for applications requiring central station air conditioning. Conventional air washers of single or double bank sprays and the Bahnson Centrispray which utilizes the principle of centrifugal atomization of water are manufactured in required sizes.

Bahnson Central Station with Refrigeration

Bahnson System
AIR CONDITIONING ENGINEERS

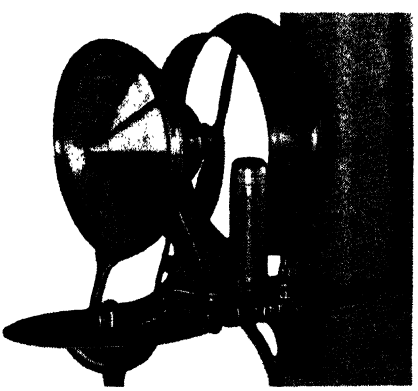
AIR-VITALIZER

The Bahnson Air Vitalizer air conditioning system employs a dry duct unit distribution system combined with the Bahnson Centrifugal Humidifier or the Bahnson Economizer Atomizer to obtain evaporation. Ventilation, humidification, evaporative cooling, heating and air filtering are combined with the flexibility of the Air Vitalizer system to permit any air handling or evaporative capacity. Positive circulation affords even distribution with additional sensible Cooling.



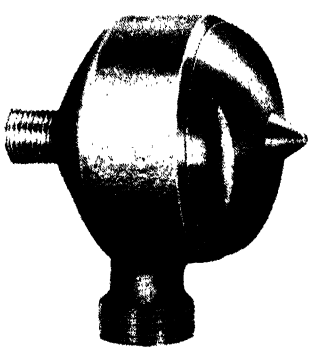
CENTRIFUGAL HUMIDIFIER

The Bahnson Centrifugal Humidifier is a completely self-contained unit humidifier requiring only water supply, drain, and electrical connection for installation. Evaporative capacity ranges up to 12 gal of water per hour dependent upon the size of the Humidifier and conditions under which it must operate. The Centrifugal Humidifier may be equipped with the Type J individual humidity control, or the highly sensitive Bahnson Master B control may be used to actuate an electric motor valve on the feed water line to a group of humidifiers.



Type H with J Control

1. **Atomizes water into a fine mist.**
2. **Diffuses the mist with room air until absorbed.**
3. **Distributes the humidified air uniformly.**
4. **Automatically controls evaporation for constant relative humidity.**



Type ESC
Pat. Pending

Economizer ATOMIZER

The Type ESC Bahnson Economizer is a pneumatic Atomizer employing air and water under pressure to produce a fine spray for humidification purposes. The Type ESC Atomizer is very simple in construction and dependable in operation. It includes a self-cleaning pin operating in conjunction with the water pressure to remove any dirt from the water line. The capacity of this Atomizer may be adjusted for amount of evaporation and quality of spray by regulating the pressure of the air and water supplying the unit. When operating at from 20 lb to 25 lb air pressure, the unit uses as little as one-half the amount of compressed air required for aspirating type Atomizers for comparable spray quality and evaporative capacity.

Carrier Corporation • Syracuse 1, N. Y.

MARINE DIVISION:
405 Lexington Ave.
New York 17, N. Y.

Carrier

INTERNATIONAL DIVISION:
122 East 42nd St.
New York 17, N. Y.

Offices and Dealers in principal cities—refer to your telephone directory.

Carrier AIR CONDITIONING

Room Air Conditioners—compact units in attractive cabinets; two sizes in window type models and two sizes in floor or console models. Built to provide summer comfort air conditioning, year round ventilation and air circulation for individual rooms, private offices and other similar small enclosures.

Self-Contained Air Conditioners—completely enclosed in neat cabinets, these units provide summer comfort for residences, retail shops, general offices, beauty salons, and other commercial spaces of medium size.

Assembled Air Conditioners—fully enclosed, compact units designed for installation outside the space to be air conditioned, and using ducts to distribute the air. Ideal for year round air conditioning of laboratories, offices, stores, and similar interiors.

Unitary and Central Station Air Conditioners—for groups of rooms such as offices and laboratories, and for large spaces such as stores, factories, theaters, industrial plants, and other interiors requiring year round air conditioning. Units available in floor or suspension models. Supplemented by refrigeration where cooling and dehumidifying is required.

"Weathermaster" Systems—for air conditioning of multi-story, multi-room buildings such as apartments, hospitals, hotels and office buildings. System consists of room units in decorative cabinets or for furring in under windows, each with individual control of temperature, and a central station apparatus. In one system the air is distributed through conduits requiring but little space—practical for new or old buildings. A special development of Carrier Corporation.

Blast Freezers and Cold Diffusers—for food freezing and storage, meat packing operations, and other industries requiring low temperatures. Units are available in suspension or floor models and can be used within the space to be refrigerated or remotely located and connected by ducts.

Write for descriptive literature on any of the above equipment

Carrier REFRIGERATION

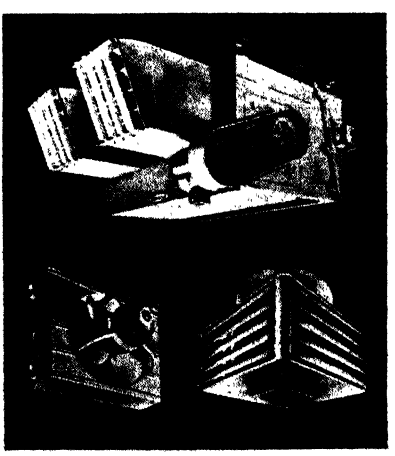
Centrifugal Refrigerating Machine—for large comfort and industrial air conditioning applications and for cooling processes down to below −100 F. These efficient machines operate with any standard drive, are simple in operation and require little maintenance. Uses safe refrigerant. Available in capacities from 100 to 1200 tons cooling

Reciprocating Refrigerating Machines—to provide refrigeration for industrial and comfort air conditioning of moderate size and for process cooling. These new 5 Series machines are available in direct connected or belt drive, water or evaporative cooled types and are job-assembled to give widest variety of capacities. Sizes from 5 to 100 hp.

Commercial Refrigerating Machines—for storage refrigerators, display cases, milk coolers, ice makers, farm and home food freezers in a wide range of capacities and temperatures. Units use "Freon" or Methyl Chloride refrigerants and are complete with compressor, drive, air or water cooled condenser, and controls mounted on a one-piece base.

Evaporative Condensers—for condensing refrigerants and cooling liquids by a process of blowing air over wetted coils. The evaporation of the water from the surface of the coils removes a maximum amount of heat with a minimum of water consumption. Can be used in place of a cooling tower. Afford savings wherever water costs are high. May be placed outdoors without protection. Capacities range from 6 to 75 tons condensing.

Carrier INDUSTRIAL HEATING



Unit Heaters—for commercial and industrial heating uses. Available in two suspended types: one horizontal discharge model for small space heating and one vertical 4-way discharge model for larger areas. Both models have adjustable louvres for directional control. Units consist of propellor type fan, coils for steam or hot water, and drive, all neatly encased. Available with manual or thermostatic controls. Capacities range from 15,600 to 502,000 Btu per hour at 2 lb steam pressure.

Heat Diffusing Units—for commercial and industrial buildings. Suspended or floor models with centrifugal type fan, coils for steam or hot water, and selective air distribution, all factory assembled for easy installation. Capacities are from 115,000 to 1,570,000 Btu per hour at 2 lb steam pressure.

Write for descriptive literature on any of the above equipment.

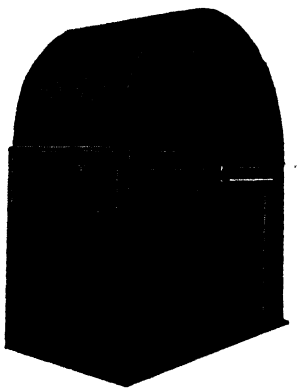
Clarage Fan Company

Kalamazoo, Michigan

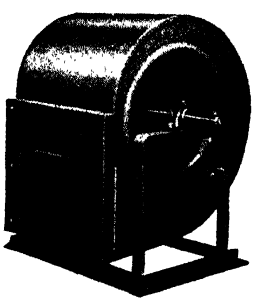
Application Engineering Offices — In Principal American Cities

(Consult Telephone Directory)

Clarage Air-Handling and Conditioning Equipment



Fans for ventilating and air conditioning. Capacities; 200 to 200,000 cfm.



Fans for warm air furnaces, oil burners, stokers, etc. 200 to 9000 cfm.

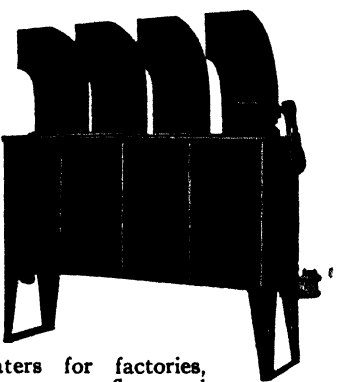
Fans for exhaust systems, pressure blowing, etc. 100 to 50,000 cfm.; built for a wide range of pressures.

Air Conditioning central systems and units to solve any temperature and humidity control problem.

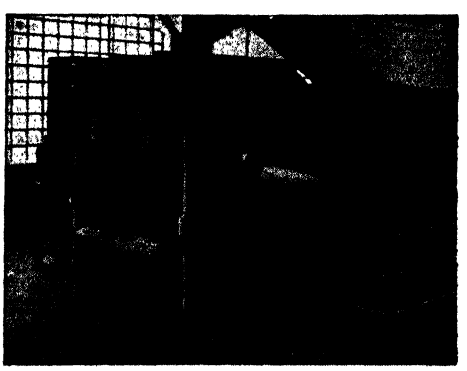
Fans • Blowers • Air Washers Air Conditioning Systems and Units • Unit Heaters & Coolers

For over thirty-five years Clarage has been a leading manufacturer of equipment for ventilating, heating, cooling, drying, air cleaning, humidifying, dehumidifying, complete air conditioning, exhausting, pneumatic conveying and mechanical draft. Clarage equipment is designed to meet all types of industrial, commercial, public building and power plant requirements. Whatever your air-handling or conditioning problem, Clarage is an excellent source of supply.

We build many other types of fans and allied equipment. Write for a Clarage catalog covering our complete line.



Unit Heaters for factories, stores, offices, etc.—floor and suspended type units. Offered in 19 standard sizes.



GENERAL REFRIGERATION

DIVISION

YATES-AMERICAN MACHINE CO., Beloit, Wisconsin

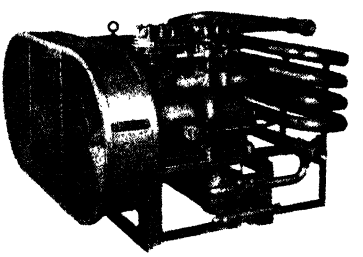
TWO GOOD NAMES TO REMEMBER

Lipman AUTOMATIC REFRIGERATION

GR AIR CONDITIONING

LIPMAN FOR REFRIGERATION

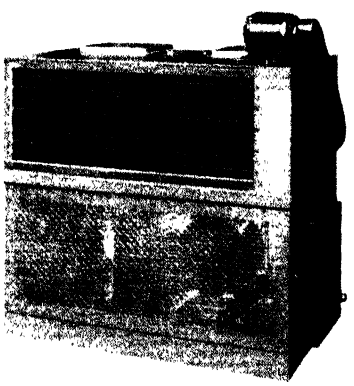
You can choose from a wide range of LIPMAN automatic refrigeration units —¼ thru 40-hp capacity—air or water-cooled - with ammonia, freon or methyl chloride refrigerant. Every unit is backed by more than a quarter century of LIPMAN service in every field of commercial refrigeration—your guarantee of dependable, economical performance.



MODEL F1509 WATER COOLED FREON—12 CONDENSING UNIT

A compact, self-contained 15-hp Freon-12 condensing unit.

GENERAL REFRIGERATION FOR AIR CONDITIONING



During its thirty years in the field, General Refrigeration has developed an outstanding line of air conditioning equipment, with a size and type for every requirement in theaters, hotels, factories, offices, shops, laboratories, etc.

MODEL 10-4000 DUCT-TYPE SELF-CONTAINED AIR CONDITIONER

Equipped with 10-hp condensing unit. Requires relatively small operating charge of refrigerant.

Let experienced GR-LIPMAN engineers study your refrigeration or air conditioning needs and recommend the correct unit for the job. No obligation. Write General Refrigeration Division, Yates-American Machine Company, Beloit, Wis., for descriptive literature and nearest distributor.

GENERAL ELECTRIC

AIR CONDITIONING DEPARTMENT

BLOOMFIELD NEW JERSEY

DISTRICT AND LOCAL OFFICES

ATLANTA 3, GEORGIA
319 Red Rock Building

BOSTON 15, MASS.
700 Commonwealth Ave.

CHICAGO 54, ILL.
The Merchandise Mart,
Room 1127

CINCINNATI 2, OHIO
617 Vine St., Room 1328

CLEVELAND 14, OHIO
925 Euclid Ave., Room 524

DALLAS 2, TEXAS
1801 North Lamar Street

DETROIT 2, MICH.
700 Antoinette St.

KANSAS CITY 6, KANSAS
Suite 2510, 106 West 14th St.

LOS ANGELES 54, CALIF.
212 North Vignes St.

MINNEAPOLIS 2, MINN.
12 South 6th St.

NEW YORK 22, NEW YORK
570 Lexington Ave.

PHILADELPHIA 22, PA.
1405 Locust St.

PITTSBURG 22, PA.
535 Smithfield St.

PORTLAND 7, OREGON
P. O. Box 909

ST. LOUIS, MISSOURI
Room 485 Arcade Building

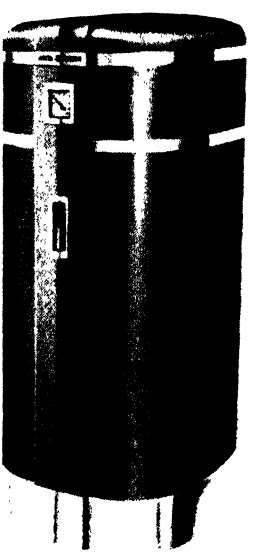
SALT LAKE CITY 9, UTAH
200 South Main St.

SAN FRANCISCO 6, CALIF.
235 Montgomery St.

WASHINGTON 5, D. C.
806 15th Street, N. W.

G-E AUTOMATIC HEATING EQUIPMENT

A COMPLETE LINE



G-E OIL-FIRED BOILER. Available in 7 sizes, from 75,000 to 450,000 Btu. Shipped with controls and jacket dismounted, to permit easy handling of the boiler. Assembly and installation on the site is a quick, simple job. Listed by Underwriters' laboratories.

G-E CONVERSION OIL BURNER. Attachment type. Comes in 2 sizes, 3 capacities (1 to 3 gal) with an input Btu range from 141,000 to 423,000 Btu. Listed by Underwriters' laboratories.

G-E WARM AIR OIL FURNACE. Small, packaged units, easily and economically installed. Two sizes, 60,000 and 85,000 Btu. Listed by Underwriters' Laboratories for 2 in. clearance on both sides and back.

G-E GAS-FIRED BOILER. Comes in 8 sizes, with Btu output ranging from 76,800 to 345,600. *A. G. A.* approved, Underwriters' Laboratory listed.

G-E GAS-FIRED WARM AIR FURNACE. Compact, packaged, easily and economically installed units in 5 sizes. Btu outputs ranging from 48,000 to 168,000. Listed by Underwriters' Laboratories for 2 in. clearance on both sides and back.

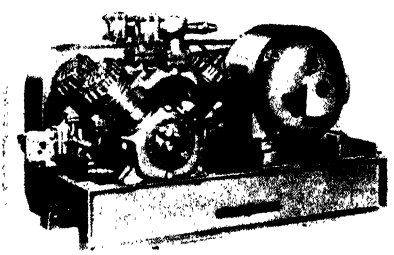
PACKAGED AIR CONDITIONING EQUIPMENT

G-E SELF-CONTAINED AIR CONDITIONERS to provide air conditioning directly in the space or remotely installed with simple ductwork, for stores, beauty shops, restaurants, large offices, office suites, or apartments. All parts accessible for service through easily removable front and side panels. Two new attractively styled models available, with 3-hp and 5-hp compressor motors, respectively.

WATER COOLERS

G-E WATER COOLERS—bottle type—designed to hold either 3 or 5 gallon water bottles and to cool 2.5 gal per hour, *A.S.R.E.* standard capacity rating. Extensively used in offices and small shops. G-E PRESSURE BUBBLER WATER COOLERS—FOOT PEDAL OPERATED—range in cooling capacity from 5.3 to 20.5 gph, *A.S.R.E.* standard capacity ratings. Wide variety of applications.

CENTRAL PLANT AIR CONDITIONING AND REFRIGERATION EQUIPMENT



REFRIGERATING CONDENSING UNITS 1/6 to 125-hp—A complete line of reciprocating type condensing units for use with "Freon" refrigerants. Air-cooled models available from 1/6-hp to 3-hp. Water cooled models available from 1/2-hp to 125-hp. Motor-compressor units for use with evaporative condensers or cooling towers available from 3-hp to 125-hp.

UNIT COOLERS—G-E "Conditioned Air" Unit Coolers can be applied to provide the essential, balanced combination of proper high humidity, gentle positive air circulation, and the correct temperature to maintain the quality, appearance, and weight of perishable foods.

CENTRAL PLANT AIR CONDITIONERS—for summer, winter, or year round air conditioning. Extra large, dynamically balanced multivane fans spring mounted for smooth operation. Panels on both sides, front, and top are easily removable. Practically all parts can be removed or serviced without disturbing frame or putting stresses on other parts.

Air cleaning by removable spun glass filters. Humidification actuated by drip screen humidifiers.

In sizes from 2.82 to 33.0 tons of refrigeration. Units are compact, thoroughly insulated internally, and finished in attractive gray so that they need not be concealed. No field fabrication is necessary.

FINNED HEAT TRANSFER SURFACE—G-E Electro-Thermal process causes intimate Thermal Bond, providing metal-to-metal contact (aided by generously proportioned die-punched collars themselves) for high efficiency.

Assembled in different tube sheets and headers to provide coils for wide variety of heating, cooling, or freezing applications. Designed for multiple mountings in housings or ducts, these coil assemblies can be bolted together to form unbroken surface. Single coils available in finned lengths to 12 ft, face areas up to 29.25 sq ft.

Coil assemblies equipped with truly cleanable "Freon" distributor of simple design. Any manufacturer's expansion valve can be used, or G. E. will select valve for application. Coils supplied with fin spacing 3, 4, 6, or 9 fins per inch.

COMPLETE AIR CONDITIONING SYSTEMS—Multiple unit systems for the air conditioning of hotels, office buildings, apartment houses, and hospitals. Attractive, compact room units make possible personal control of conditions in individual rooms. Refrigeration in central plant furnished by reciprocating type condensing units or centrifugal refrigeration units as requirements dictate.

Hastings Air Conditioning Co., Inc.

Hastings, Nebr.

Manufacturers of

AIR CONTROL AIR CONDITIONING

Air Conditioners.
Unit Heaters.
Utility and Package Blowers.

Dealers and Representatives in Principal Cities

A Complete Line of Highly Specialized Air Conditioners For DX, Cold City Water, Chilled or Well Water Operation.

All equipment may be used for combination cooling and heating.

Water coils are six rows deep and DX coils four rows deep. Developed and designed for utmost efficiency. Constructed of copper tubing expanded and metallically bonded to pure copper fins.

FLOWMETERS (to visually control flow) are standard on all water equipment.

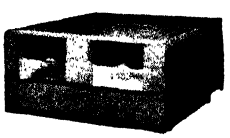
FLOOR MODELS

Floormasters — Unusual design and special features permit maximum installation possibilities with excellent results.

Cooling Capacity—
Water coils, 3 to 6 tons.
DX coils, 5 tons.
Air Delivery—2240 cfm.
Motor—½ hp Filters—three 16x25. Dimensions—Ht. 93 in., Width 48 in., Depth 25 in.

Royal—For offices, homes, hospitals, etc.
Cooling Capacity—
Water, 1 to 2 tons.
⅙ hp 590 cfm Filter 16x25.
Dimen. Ht. 40 in., Wd. 28 in., Depth 20½ in.

CENTRAL PLANTS



Sectional construction for ease of handling. Motors inside mounted to provide very neat appearing compact units.

SPECIFICATIONS

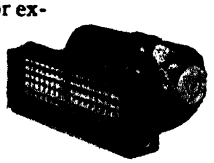
Size	CFM	Motor Hp	Filters	Capacity Tons
CP 30	3,000	1	5	4- 9
CP 40	4,000	1	8	6-12
CP 60	6,000	2	10	9-18
CP 80	8,000	3	12	12-24
CP120	12,000	5	20	18-36

STEAM UNIT HEATERS

Centrifugal Type for extreme quietness and efficiency.

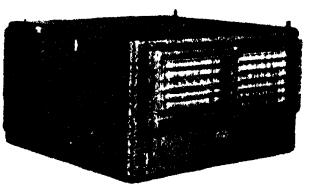
Steam pressure—to 150 lbs per sq in.

Finish—Brown wrinkle enamel and stainless steel louvers.



GENERAL UTILITY MODELS

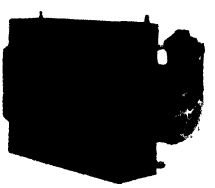
Master—Singly or in multiple are suitable for any business or space size. Large jobs handled without duct work by proper location of units.



Cooling Capacity—
Water coils, 3 to 6 tons.
DX coils, 5 tons.
Air Delivery—2,240 cfm.
Motor—½ or ¾ hp. Filters—four 16x23.
Dimen. Ht. 29 in., Wd. 49 in., Depth 50 in.

Majestic—Similar to Master except size. Cooling Capacity—Water 1½ to 3 tons. ¼ hp 1120 cfm Two 16x25 filters. Dimensions—Ht. 26 in., Wd. 28 in., Depth 40 in.

GAS UNIT HEATERS



These CENTRIFUGAL gas unit heaters present many fine and unusual features.

Squirrel-cage blowers provide SILENT operation and permit air delivery thru duct systems up to ¼ in. S. P.

Stainless steel ribbon burners result in quiet efficient combustion.

Dual directional, individually adjustable stainless steel louvers permit complete control of air delivery.

Write for Catalogs, Literature, or Information

Niagara Blower Company

General Sales Office: 405 Lexington Ave. **New York 17, N. Y.**

CHICAGO-5: 37 W. Van Buren St. BUFFALO-7: 673 Ontario St. SEATTLE-4: Fourth and Cherry Bldg.

District Engineers in Principal Cities

Over 30 Years' Experience in Industrial Air Conditioning, Liquid Cooling and Air Drying

NIAGARA AERO HEAT EXCHANGER

For cooling industrial liquids, water, oils, solutions, chemicals, compressed air and gases, with Niagara "Balanced Wet-Bulb" temperature control to improve efficiency and obtain precise results. Patented (U. S. Nos. 2,296,946 and R. I. 22,553). Ask for Bulletin 96.

NIAGARA AIR CONDITIONING SYSTEMS

For human comfort and for all industrial applications requiring controlled conditions of temperature, relative humidity, air purity and air movement.

NIAGARA AIR CONDITIONER, TYPE A

High precision apparatus using saturation to obtain control of R. H. to 1 per cent for laboratory work and control of hygroscopic materials. Ask for Bulletin 58.

NIAGARA AIR CONDITIONER, TYPE C

A year around air conditioning unit providing heating and humidifying or dehumidifying. Ask for Bulletin 80.

NIAGARA FAN COOLER AND DISK FAN COOLER

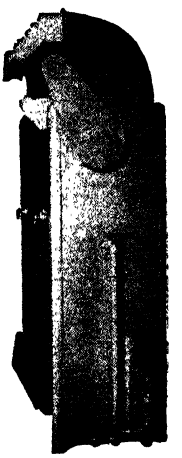
For comfort cooling, process cooling, low temperature storage for dairies, fruits, meats, food products, fur storage vaults, etc. Bulletin 72.

NIAGARA SPRAY COOLER

For all cooling applications requiring high humidity or high capacity in small space. Ask for Bulletin 72.

NIAGARA "NO FROST" SYSTEM

Using Niagara "No Frost" Liquid in spray coolers, prevents frosting of cooling coils, automatically keeps spray solution at proper concentration, gives freedom from brine troubles, corrosion. Constant, efficient operation. Temperature to −100° F. Ask for Bulletins 83 and 95.



Niagara "No Frost" Cooler

NIAGARA AEROPASS CONDENSER (Illustrated)

Saves power and water cost utilizing atmospheric air to remove heat of condensation. Patented Duo-Pass prevents scaling, saves power. "OILOUT" positively removes oil and dirt from refrigerant lines, assuring always full capacity. Ask for Bulletins 91 and 103.

NIAGARA "DUAL" COOLERS

Simultaneously cools a room and furnishes chilled water as a refrigerant. Saves equipment cost, operating expense. Patented. Ask for Bulletin 70.

NIAGARA INDUSTRIAL LIQUID COOLER

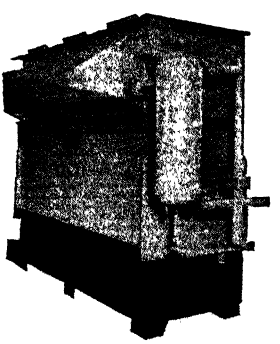
Furnishes refrigerated water or aqueous solution in any quantity up to 220 gpm. Positive control of temperature regardless of load variation. Delivers "sweet" water at 33° F without danger of freezing damage. Ask for Bulletin 100.

NIAGARA FAN HEATERS

For heating and ventilating large areas. Units of the highest quality in engineering, material and workmanship. Ask for Bulletin 73.

NIAGARA MOTOR BLOWERS

One, two and three-fan units. High and low static pressure models. Ask for Bulletin 89.



Niagara AeroPass Condenser with "Oilout"

Parks-Cramer Company

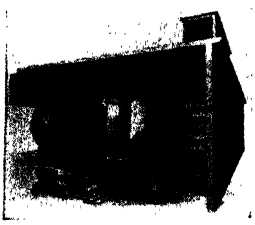
Fitchburg, Mass. **Charlotte, N. C.**

CERTIFIED CLIMATE

Complete Air Conditioning Systems including Heating, Cooling, Humidifying or De-humidifying, Air Changing, Refrigeration, Air Filtering, Air Washing

AUTOMATIC REGULATION

Merrill Process System of Hot Oil Circulation for Heating Industrial Materials
Jacketed Cocks, Fittings and Jacketed Piping

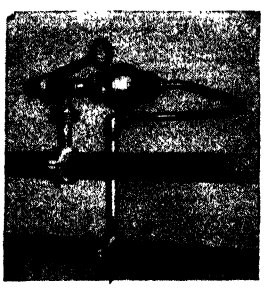


Central Station

Central Station Air Conditioning

A complete system of conditioning air, with positive circulation and controlled ventilation. One or more air washer and fan units. High humidifying and evaporative cooling capacity. Heating, filtering, and refrigerated cooling optional. Ducts with adjustable outlets distribute conditioned air uniformly. Slight air pressure also improves uniformity. No free moisture in room. Centralized maintenance.

Air Washer or Central Station Units.
Nozzles for Central Station Air Washers.



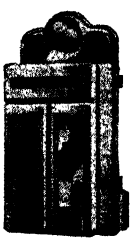
Turbomatic Humidifier

Turbomatic Humidifier

Efficient humidifier of the atomizer type. For direct humidification, as humidity boosters for Central Station systems of all makes. Self-cleaning, both air and water ports. Streamlined to prevent lint and dirt accumulation.

Parks Automatic Airchanger (not illustrated)

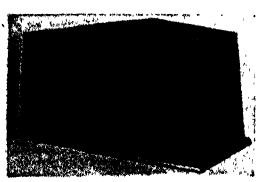
A patented system of forced air change used with a direct humidifying system. Insures fixed humidity and maximum evaporative cooling by controlling amount of air change and operation of humidifiers by a psychrometric humidity regulator. Designed for either complete new installations or for supplementing existing direct humidifying equipment.



Psychrostat

Automatic Regulation

The Psychrostat for accuracy, durability, sensitivity. Employs the principle of the Sling Psychrometer, used in all U. S. Weather Bureau Stations. Hygrostat (not illustrated) where requirements are not so exacting. An Air Conditioning System is no better than its Regulation.



Pettifogger

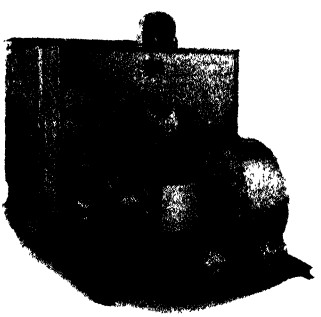
The Pettifogger

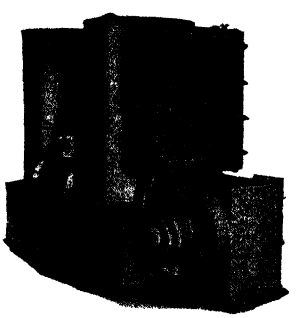
A compact humidifier for offices, stores, storerooms, laboratories, or other isolated departments. Self-contained in lacquered copper casing. Permanently though flexibly connected to water and electrical supplies. Automatic control. Adjustable capacity. Neutralizes drying effect of heating.

Pittsburgh Lectrodryer Corporation

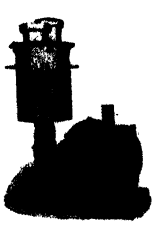
Foot of 32nd St. **Pittsburgh, Penna.**

Large **Lectrodryer** handling the make-up air for the altitude wind tunnel, National Advisory Committee for Aeronautics, Aircraft Engine Research Laboratory, Cleveland, Ohio.

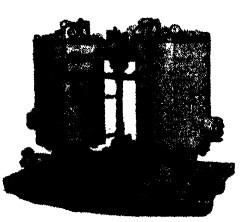




Lectrodryers are widely used for maintaining lowered relative humidities, using the activated alumina system of adsorbing water vapor from air. They are available in many standard sizes handling flows from 100 cfh up to 15,000 cfm in standard catalog units. Larger units can be designed for handling any desired flow. **Lectrodryers** are sturdy industrial type units suitable for years of efficient and reliable drying service with minimum maintenance. Reactivation is accomplished through the use of steam, gas or electricity, whichever the purchaser specifies. **Lectrodryers** can be used with or without aftercoolers.



The **Lectrobreather** shown at the left prevents the entrance of atmospheric moisture into oil and chemical storage tanks. The machine shown is mounted on a **Lectrobreather** reactivator. The dual adsorber **Lectrodryer** at the right continuously dries compressed air at 150 psig preventing the harmful effects of water and water vapor on air operated controls and instruments.



United States Air Conditioning Corporation

Heating, Cooling Ventilating and Air Conditioning Equipment

For Industrial, Commercial and Residential Applications

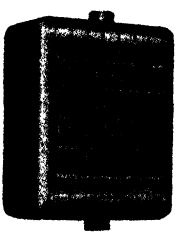
COMO AVENUE S. E. AT 33RD . MINNEAPOLIS 14, MINNESOTA
EXPORT DIVISION—GRAYBAR BUILDING, NEW YORK

Evaporative Condensers

A cooling unit that condenses refrigerants in one compact self-contained package. . Permits savings of 95 per cent in water costs, and by eliminating waste disposal problems, evaporative condensers provide unequalled economy in cooling refrigerant gases.

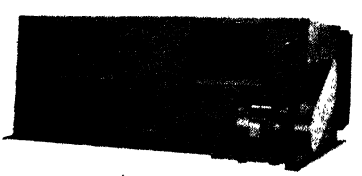
Upright Store Conditioners

A completely packaged unit designed for conditioning applications in stores, restaurants, beauty shops. 3 and 5 ton capacities.



Unit Heaters

Suspension type small area heater designed for supplementary heating in factories, garages, warehouses. Uses steam or hot water.

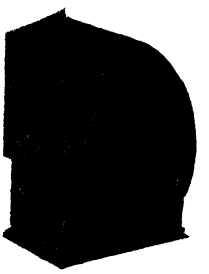


Unit Air Conditioners

Used for cooling and dehumidifying. Made in both single and double fan arrangements, and in 9 sizes from 1000 cfm to 12,000 cfm. Units available with special coils for mechanical cooling or heating.

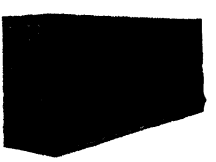
Blowers

Heavy and light duty blowers made in single or double inlet styles, and in a variety of sizes and capacities for all cooling, heating, ventilating and air conditioning requirements.



Unit Coolers

Cooling units designed by USAIR CO for industrial and commercial low temperature and comfort cooling needs.

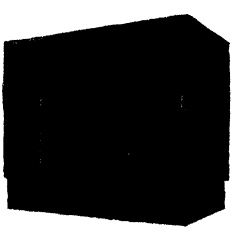


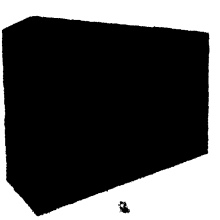
Coils

USAIRCO makes a complete line of coils for every air conditioning requirement—including steam coils for heating, standard and non-freeze type, water coils for heating or cooling, and direct expansion coils.

Air Washers

Single and double stage 2,500 to 100,000 cfm for cleansing, cooling by cold water or refrigerant, humidifying or dehumidifying.





Refrigerated Kooler-Aire

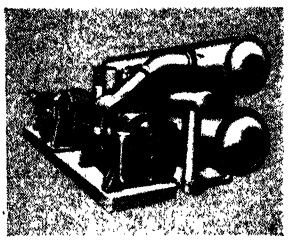
Unit combining cooling and dehumidifying units, refrigeration compressor and evaporative condenser all in one balanced assembly. 3 to 40 ton capacities.

York Corporation

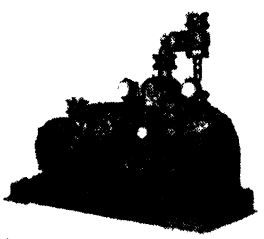
York, Pennsylvania

Factory Branches and Distributor Engineering and Sales Offices throughout the World.

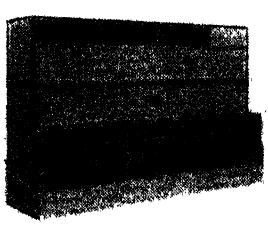
Air Conditioning and Refrigeration for maintaining proper atmospheric conditions for industrial processes or comfort requirements. Installations of unit and central systems in a complete range of capacities and types for every design requirement.



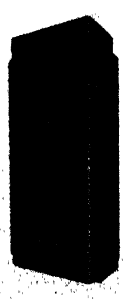
York Turbo Compressor



York V-W Condensing Unit



York Sectional Economizer



Yorkaire Unit Air Conditioner

Condensing and Water Cooling Systems—Turbo (centrifugal) brine and water cooling systems available over wide range of capacities—up to 1500 tons refrigeration for Freon-11 water cooling duty—suitable for steam turbine or motor drive.

Self-contained dynamically balanced, non-vibrating V/W type reciprocating compressors available in capacities up to 350 tons refrigeration in a single unit, with water cooled or economizer type condensers.

Efficient automatic capacity reduction available for economical operation at reduced load.

The York Economizer—A combined forced-draft cooling tower and refrigerant condenser, is available for installations where prohibitive water costs or inadequate drainage facilities preclude the use of a water cooled condenser. Standard factory constructed and built-up units may be used singly or in multiple for applications of any specified capacity. Economizers for use with Freon as the refrigerant are furnished, as standard, with a liquid sub-cooling coil. Economizers also designed for cooling of quench oil and other liquid coolants.

Air Conditioning Units: A complete line of finned coil, dry coil, wetted surface and spray type sectional air conditioners for horizontal or vertical applications, designed to facilitate installation and the distribution of air. Standard units can be equipped with by-pass feature and arranged for cooling and dehumidifying, heating and humidifying, for year-round processing.

Yorkaire Unit Air Conditioner—A compact, self-contained model occupying but 21 x 42 inches of floor space and requiring only water, drain and electrical connections to operate. Special features provide utmost flexibility to meet varying conditions. Temperature dial control provides both automatic and manual temperature control. Air volume and motion may also be adjusted by a special control and the directional grille provides ***directed air flow***—up, down or from side to side. May be used with ducts if desired.

Yorkaire Conditioners are ruggedly built, quiet in operation, equipped with standard fan and compressor motors for AC or DC.

Dehumidifiers—For central station systems where a large volume of air is to be handled and where control of humidity is an essential requirement, the York dehumidifier is especially applicable. Construction features insure a minimum space demand and maximum performance conditions. Standard washers are available in a full range of capacities for industrial installation.

ALLIS-CHALMERS MANUFACTURING COMPANY

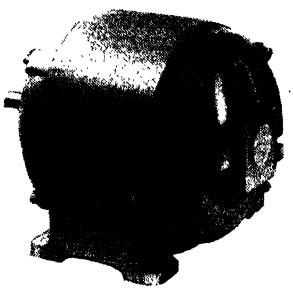
Milwaukee 1
Wisconsin

There is an Allis-Chalmers representative near you.

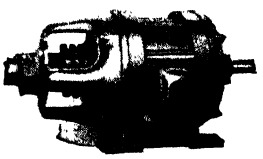
ALLIS-CHALMERS builds four major components for heating, ventilating and air-conditioning installations—in types and sizes for any requirement. A single source of supply means skilled sales service . . . coordinated installation . . . better unit responsibility. Bulletin 25B5170 describes Allis-Chalmers equipment for heating, ventilating and air-conditioning.

ALL-PURPOSE MOTORS

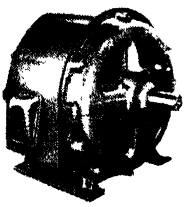
A complete line of ½ to 200 hp motors is built by Allis-Chalmers for any requirement of speed and torque. Strong, distortion-resistant construction adds to motor life.



SQUIRREL-CAGE

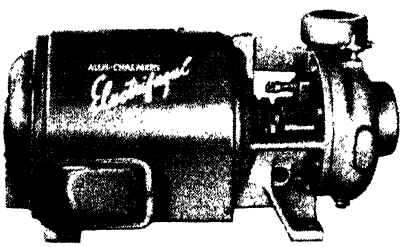


WOUND ROTOR



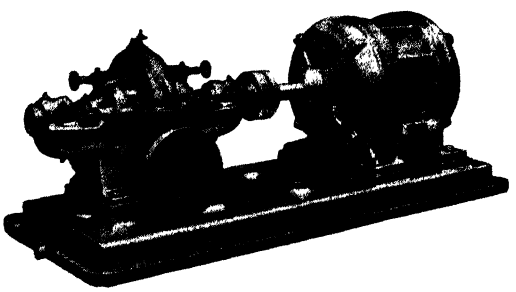
SYNCHRONOUS

CENTRIFUGAL PUMPS

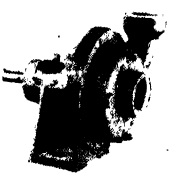


The Electrifugal

Motor and pump are built as one unit in the compact, efficient **Electrifugal** pump. Alignment is no problem. Has deep-groove ball bearings for all-position operation. Takes up ⅓ less space. 15 to 1600 gpm; heads to 500 ft. Bulletin 52B6059D.



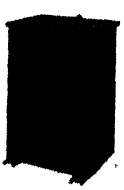
Double Suction Pumps



Low Cost Pedrifugal

Motor Controls

Allis-Chalmers supplies motor controls for every requirement of operation. Reversing and non-reversing, manual or magnetic, across-the-line or reduced voltage.



Dry Type Transformers

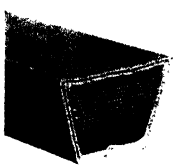
A compact, quickly installed Class "B" insulated transformer that has proved practical in large heating and ventilating systems. Serves all circuits; all system loads.

SALES OFFICES

Amarillo, Tex.	Amarillo Bldg.	Newark 2, N. J.	1060 Broad St.
Atlanta 3, Ga.	Healey Bldg.	New Haven 10, Conn.	157 Church St.
Baltimore 2, Md.	O'Sullivan Bldg.	New Orleans 12, La.	Canal Bldg.
Birmingham 3, Ala.	First National Bldg.	New York 7, N. Y.	50 Church St.
Boston 16, Mass.	Park Square Bldg.	Oklahoma City 1, Okla.	901 W. Grand
Buffalo 2, N. Y.	Liberty Bank Bldg.	Omaha 8, Nebr.	9th & Farnam St.
Charleston 1, W. Va.	Peoples Bldg.	Philadelphia 3, Pa.	Broad St. Sta. Bldg.
Charlotte 2, N. C.	Johnston Bldg.	Phoenix, Ariz.	Luhrs Tower
Chattanooga 2, Tenn.	Chat. Bk. Bldg.	Pittsburgh 19, Pa.	Koppers Bldg.
Chicago 3, Ill.	135 S. La Salle St.	Portland 4, Ore.	Public Service Bldg.
Cincinnati 2, Ohio	Cham. of Com. Bldg.	Providence 3, R. I.	Industrial Trust Bldg.
Cleveland 14, O.	Nat. Broadcasting Bldg.	Richmond 19, Va.	527 E. Main St.
Dallas 2, Texas	1800 N. Market St.	Rochester 4, N. Y.	Roch. G. & E. Bldg.
Davenport, Iowa	United Light Bldg.	Rockford, Ill.	Gas-Electric Bldg.
Denver 2, Colo.	Continental Oil Bldg.	St. Louis 3, Mo.	1205 Olive St.
Detroit 26, Mich.	Fisher Bldg.	Salt Lake City 1, Utah	Kearns Bldg.
Duluth 2, Minn.	Bradley Bldg.	San Antonio 5, Texas	Frost Nat'l. Bk. Bldg.
El Paso, Texas	Mills Bldg.	San Diego, Calif.	Bank of America Bldg.
Evansville, Ind.	125 Locust St.	San Francisco 8, Calif.	239 Yale Ave.
Fort Worth 1, Texas	Fort Worth Elect. Bldg.	Seattle 1, Wash.	Henry Bldg.
Grand Rapids 2, Mich.	Asso. of Com. Bldg.	Shreveport 23, La.	City Bank Bldg.
Houston 3, Texas	1719 McKinney Ave.	Spokane 8, Wash.	Old Nat'l. Bank Bldg.
Indianapolis 4, Ind.	Merchants Bk. Bldg.	Syracuse 1, N. Y.	935 Hiawatha Blvd. E.
Jackson, Mich.	297 W. Michigan Ave.	Tampa 6, Fla.	3602 Cleveland St.
Kansas City 6, Mo.	Waldheim Bldg.	Toledo 4, Ohio	Toledo Trust Bldg.
Knoxville 2, Tenn.	531 Gay St.	Tulsa 3, Okla.	320 East Archer St.
Los Angeles 13, Calif.	Rowan Bldg.	Washington 5, D. C.	Southern Bldg.
Louisville 2, Ky.	Ky. Home Life Bldg.	Wheeling, W. Va.	Hawley Bldg.
Memphis 3, Tenn.	Dermon Bldg.	Wilkes-Barre, Pa.	Miners Nat'l. Bk. Bldg.
Miami, Fla.	Pacific Bldg.	York, Pa.	42 East King St.
Milwaukee 2, Wis.	Mil. Gas Light Bldg.	Youngstown 3, Ohio	Mahoning Bk. Bldg.
Minneapolis 2, Minn.	Foshay Tower		

Distributors throughout the World

ALLIS-CHALMERS MULTIPLE V-BELT TEXROPE DRIVES



Texrope is the trade name and registered trade mark of V-belt drive products of Allis-Chalmers, pioneer in multiple V-belt drives. Texrope drives are compact, silent, easy on bearings . . . offer speed ranges of 7.1 . . . permit use of lower cost higher speed motors. Duplex-sealed cover protects Texrope V-belt internal cords against dirt, grit, moisture. Oil-Resisting, Static-Resisting, and Oil-Proof types. Bulletin in 20B6051G.

CONSTANT SPEED DRIVES

Texsteel Sheaves

Pressed steel construction. Fractional to 25 hp use.

Texdrive Sheaves

Integrally bushed for standard shafts. Of fine grain cast iron.

ADJUSTABLE SPEED DRIVES

Adjustable Sheaves

50 per cent speed change with movable threaded plate.

Vari-Pitch Sheaves

9 per cent to 28 per cent speed control for 1 to 300 hp.

Wide Range Vari-Pitch

Speed ranges up to 116 per cent, with wide section V-belts. ½ to 30 hp.

Easy To Put On . . . "MAGIC-GRIP" SHEAVES . . . Easy To Take Off

Sheave slides on shaft without forcing. *Easy "slide on" results in true alignment.* *Tightening 3 capscrews locks sheave to shaft.* *Use 2 capscrews as jackscrews in tapped holes.* *A twist of the wrist breaks bushing grip.* *Slide sheave off . . . no prying necessary.*

Let the pup be furnaceman

BRYANT HEATER COMPANY

17825 St. Clair Avenue - - - Cleveland, Ohio

Engineering, Sales and Installation information on Bryant Equipment available through Bryant Distributors, Dealers and Gas Companies in principal cities.

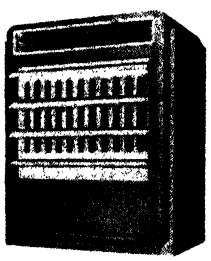
Vertical Winter Air Conditioner

Bryant Gas designed boilers include tubular cast iron sections, ribbed lower tubes, large steam liberating areas, all heating surfaces readily accessible for cleaning. Insulated metal jacketed covers and Bryant gas controls. Complete range of *AGA* inputs from 45,000 to 3,996,000 Btu/hr for steam and hot water heating systems, volume water heating and industrial process.

Bryant Vertical Winter Air Conditioners complete with blowers, humidifiers and filters are compactly designed for small housing, office or industrial use. Models available with heating sections made of either tubular cast iron or 12-gage steel. Quality controls are standard on all models. Capacities from 55,000 to 115,000 Btu/hr *AGA* input on cast iron and 45,000 to 145,000 on steel units.

Complete line of Forced Warm Air Gas-Fired Equipment from 60,000 to 375,000 Btu/hr *AGA* inputs. Efficient cast iron heating sections, large capacity blowers, humidifiers, filters and Bryant automatic controls are standard.

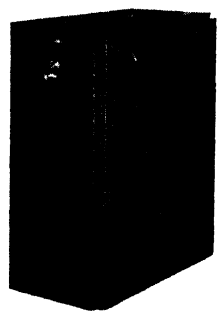
Bryant suspended type Gas-Fired Unit Heaters available in six sizes ranging from 60,000 to 210,000 Btu/hr *AGA* inputs. Efficient heat exchange of staggered vertical tube construction. Available in both cast iron combustion chamber, alloy steel tube and all steel types. Quick, clean, efficient heat for all types of industrial and commercial space. Flexible, automatic control and large volume air circulation produce ideal space heating results.



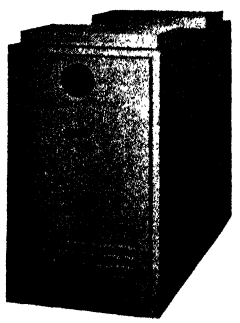
Suspended Type Gas-Fired Unit Heater

Bryant Dehumidifiers with rotary silica gel drum, is completely automatic in operation and finds application for exact humidity control in industrial processing, comfort air conditioning and the drying and storing of hygroscopic materials. They are available in three sizes, 800, 1300 and 2900 cfm. Standard units are reactivated by gas. Indirect units arranged for use with high pressure steam coils or electric strip heaters are available.

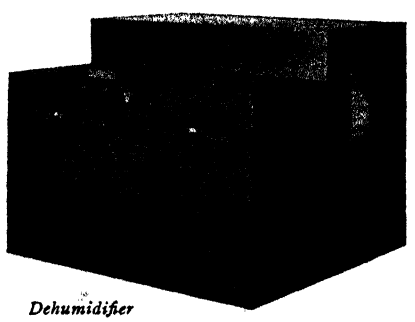
See your local Bryant Distributor or write for complete details and specifications.



Gas-Fired Boiler



Forced Warm Air Gas-Fired Equipment



Dehumidifier

DUO-THERM *Division of Motor Wheel Corporation*

Lansing 3, Michigan

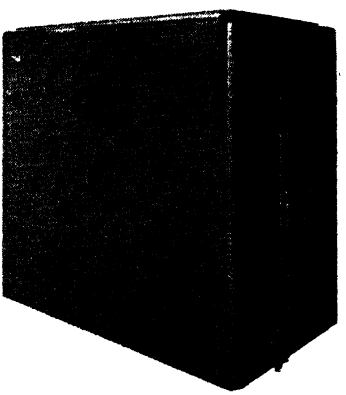
Duo-Therm Automatic Fuel Oil Furnaces are complete package unit cabinet models in baked enamel. They are designed to fit any type home of average size. Can be installed with ease in the basement or in the utility room. Listed as Standard by the *Underwriters' Laboratories* and Listed by the *Canadian Standards Association* for use with No. 1 or No. 2 fuel oil. Write for Engineering Manual on Duo-Therm Oil Burning Furnaces.

DELUXE MODEL WINTER AIR CONDITIONER in 3 sizes as follows:

330-DB— 52,000 Btu bonnet output— 800-1200 cfm blower output

340-DB— 78,000 Btu bonnet output— 1000-1700 cfm blower output

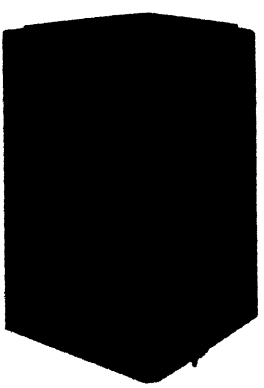
350-DB—108,000 Btu bonnet output—1500-2600 cfm blower output



UNDERNEATH BLOWER MODEL WINTER AIR CONDITIONER available in 2 sizes as follows:

330-UB—50,000 Btu bonnet output— 800-1200 cfm blower output

340-UB—75,000 Btu bonnet output—1000-1700 cfm blower output



GRAVITY MODEL FURNACE can be manually controlled or be equipped for automatic thermostatic control. Can easily be converted to either DeLuxe or Underneath blower types. Available in 3 sizes as follows:

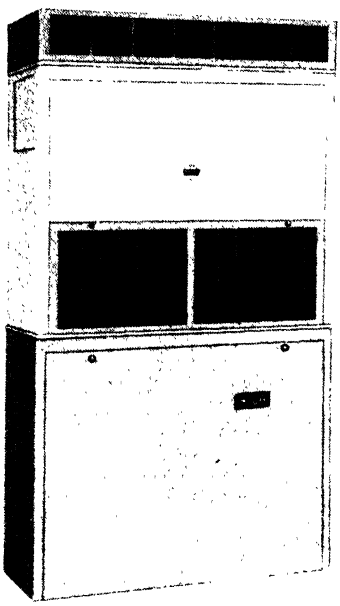
329-M—50,000 Btu bonnet output
330-T

339-M— 75,000 Btu bonnet output
340-T

349-M—104,000 Btu bonnet output
350-T

CHRYSLER AIRTEMP

AIRTEMP DIVISION OF CHRYSLER CORPORATION, DAYTON 1, OHIO



"PACKAGED" AIR CONDITIONERS

AVAILABLE IN 3 and 5 H. P.

COMPLETE—Cools, dehumidifies, filters, circulates the air. Free air discharge or duct distribution. Heating coil for year 'round service, optional.

COMPACT—Everything enclosed in a rust-resistant "Bonderized" cabinet of modern design with chrome hardware and trim. Occupies minimum of floor space—4.7 sq ft for 3 hp and 6.5 sq ft for 5 hp.

EASILY, QUICKLY INSTALLED—Tested and completely assembled at the factory. Needs only three connections; electric, water and drain.

SEALED RADIAL COMPRESSOR—Quiet, all moving parts balanced to eliminate vibration. Entire compressor assembly suspended from single rubber mounting. Long life because vital moving parts are "super-finished" and pressure lubricated.

FLEXIBLE—"Packaged" Air Conditioners can be installed singly or in multiple to meet almost any requirements. Can be moved easily.

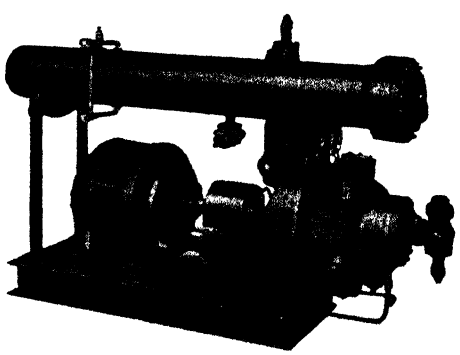
CHRYSLER AIRTEMP RADIAL CONDENSING UNITS

AVAILABLE IN 7½ TO 75 HORSEPOWER CAPACITIES

This heavy-duty Radial Condensing Unit, for use with Freon, is especially adapted for refrigeration, for industrial processes or air conditioning. Airtemp Radial compressors are direct connected and have force-feed lubrication. The automatic capacity-reduction device gives variable capacity . . . high operating efficiency. Light in weight and economical to operate, these condensing units are shipped ready to run. Vibrationless, they are very easy to install because special foundations are not necessary. Each pressure vessel approved by Underwriters Laboratories.

AUTOMATIC UNLOADER

The automatic cylinder unloading device permits starting the compressor under no load and keeps the compressor automatically adjusted to varying loads with no stopping and starting during operation.



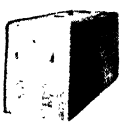
Automatic Capacity Regulation • Unloaded Starting • Direct Connected • Simplified Installation • Compact Design • Practically No Vibration • No Special Foundations Needed • Interchangeable Parts.

CHRYSLER AIRTEMP
AUTOMATIC HOME HEATING

VAPORIZING OIL-BURNING AUTOMATIC FURNACE . . . Models for forced-air—56,000 Btu output; gravity, 50,000 Btu output. Sure-Draft Fan assures highest overall efficiency. "Bonderized" and insulated jacket. Forced air model approved for closet installation, *Underwriters' Laboratories, Inc.*

OIL-FIRED AUTOMATIC FURNACE . . . Heats, humidifies, filters and circulates the air. Five models, from 70,000 to 160,000 Btu output. "Bonderized" and insulated jacket. Metal combustion chamber, seam-welded firebox of copper-bearing steel; large, slow-speed, rubber mounted fan. Airtemp oil burners on all models. Approved by *Underwriters' Laboratories, Inc.*

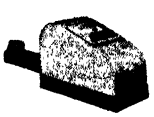
GAS-FIRED AUTOMATIC FURNACE . . . Heats, humidifies, filters and circulates the air. Steel Models 70,000 to 160,000 Btu output. Cast-iron Models 50,000 and 75,000 Btu output. "Bonderized" and insulated jacket. The Airtemp "Silent Flame" Gas Burner starts, stops and operates quietly, has many exclusive features—no popping or flash-backs. Approved, *A.G.A.* Laboratories.



OIL-FIRED STEEL BOILERS . . . Three models—BLF-110 rating 460 sq ft EDR, BLF-165 rating 690 sq ft EDR, BLF-220 rating 920 sq ft EDR, of steam at the boiler header. Combustion chamber of quality chrome steel. Boiler is combination of "Scotch Marine" and Locomotive types. Complete with Airtemp burner and all controls.

COAL-FIRED FURNACE, GRAVITY . . . Furnace body of heavy steel boiler plate—seams electrically welded. Front, heavy gauge pressed steel. Fire brick lining. Sizes 22 in., 24 in., and 27 in.; Btu at bonnet, 108,000, 119,700, and 154,200.

COMBINATION HEATING AND COOLING FOR THE HOME . . . Combination of a 3 hp Chrysler Airtemp "Packaged" Air Conditioner and any of the larger Chrysler Airtemp automatic furnaces. The same blower, filters and ducts of the automatic heating system are employed for cooling in the summer.



STOKERS . . . Domestic, available in both hopper and bin-feed models for anthracite or bituminous coal for burning 15 to 35 lb per hour. Powerful transmission, sectional retort and safety coupling . . . eliminates shear pins.

CONVERSION OIL BURNERS . . . Pressure-atomizing oil burner, 1.35 to 4.5 gallons No. 3 furnace oil per hour. All Airtemp Oil Burners are approved by *Underwriters' Laboratories, Inc.*

THE MEYER FURNACE COMPANY

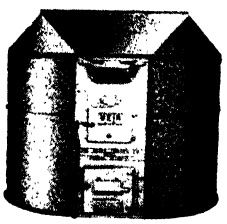
PEORIA, ILLINOIS

Manufacturers of Heating and Air Conditioning Equipment for Coal, Gas and Oil Burning

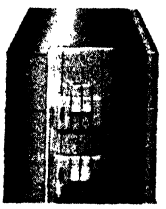
Branches and Distributors

ATLANTA, GA.
BIRMINGHAM, ALA.
CHICAGO, ILL.
COLUMBUS, O.
DES MOINES, IA.
FLORENCE, S. C.
GREEN BAY, WIS.
KANSAS CITY, MO.
LIMA, O.
MILWAUKEE, WIS.
NEW YORK, N. Y.
OMAHA, NEBR.
PHILADELPHIA, PA.
PITTSBURGH, PA.

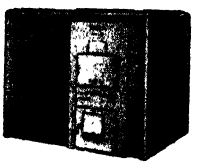
WEIR and MEYER Steel Warm-Air Furnaces, of welded-and-riveted gas-tight construction, have an 80-year reputation for efficiency, dependability and durability. They are available for small and large requirements and for all fuels in a wide variety of firing applications.



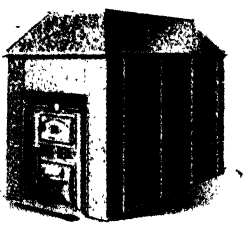
"R" Series Heavy Duty



U Series Gravity



U Series F-A



"500" Series Heavy Duty

WEIR COAL FIRED UNITS ("U" SERIES)

Available in Five Sizes For Both Gravity and Forced Air Domestic Heating

The "U" Series WEIR hand-fired coal furnace embodies a new construction principle (patent applied for) which when combined with its other time-tested WEIR features provides an outstanding heater. The gravity furnace as shown above ranges in register capacity from 50,000 to 170,000 Btu per hour. The rectangular-cased forced air furnace shown above ranges from 50,000 to 190,000 Btu per hour output at the register. This series may be stoker-fired or oil-fired though other designed furnaces are available for the particular fuels.

GRAVITY					FORCED AIR									
Fce. No.	Output at Bonnet	Drum Diam.	Casing Diam.	Smoke Collar Diam.	Fce. No.	Output at Bonnet	Cfm	L	W	H	R. A. Plenum	W. A. Plenum	No. & Size of Filters	Fan Size	Mtr. Size
20U	71,000	20	42	9	20UC	79,000	860	52	30	53	11x26	24x26	1 - 20x25x2	9	1/6
22U	115,000	22	46	9	22UC	130,000	1415	60	46	53	14x35	30x35	2 - 20x20x2	12-3	1/4
24U	120,000	24	48	9	24UC	135,000	1470	60	46	53	14x35	30x35	2 - 20x20x2	12-3	1/4
27U	144,000	27	50	9	27UC	161,000	1755	68	48	55	18x37	35x37	3 - 16x25x2	12-3	1/4
30U	170,000	30	54	10	30UC	191,000	2080	71	52	57	18x41	38x41	3 - 16x25x2	12	1/4

HEAVY DUTY

Manufactured in the Following Seven Sizes for Heavy Duty Service in all Types of Large Buildings

WEIR Heavy-Duty furnaces consisting of the "R" Series and the 500 Series illustrated above are ideal for industrial and commercial service and for schools, churches and other large spaces. Capacities range from 300,000 to 1,500,000 Btu per hour, designed only for forced air circulation but suitable for hand-firing or can be adapted for stoker, gas or oil firing.

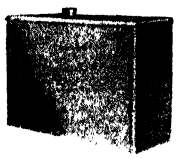
Furnace Number	Btu at Bonnet	Cfm	Fan Size	Motor Size Hp	No. & Size of Filters	Stoker Size	Oil Burner Gph	Smoke Collar Diam.	Overall		
									H	W	L
36R	400,000	6,000	21"	1½	8 - 20x20x2	63	4.5	10	70	80	119
38R	500,000	7,500	25"	3	12 - 20x20x2	75	5.5	2-10	70	80	119
540B	550,000	9,900	2-18"	3	15 - 20x20x2	100	6	12	80	92	108
544B	690,000	12,000	2-21"	3	15 - 20x20x2	100	7.25	12	80	106	108
544BS	700,000	15,300	2-21"	3	18 - 20x20x2	150	7.75	12	92	106	108
544B-2VR	850,000	18,000	2-25"	5	24 - 20x20x2	160	9.5	2-12	84	124	160
544B-2VRS	1,000,000	18,000	2-25"	5	24 - 20x20x2	200	11	2-12	96	124	160

THE MEYER FURNACE COMPANY

PEORIA, ILLINOIS

Manufacturers of Heating and Air Conditioning Equipment for Coal, Gas and Oil Burning

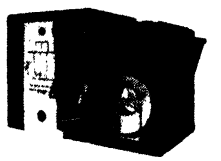
MEYER OIL AND GAS FIRED EQUIPMENT



"A" Series Oil Fired

"F" Series Gas Fired

"B" Series Hi-Boy



"K" Series Oil Fired

The MEYER oil-fired air conditioners are available in three types—the "A" Series suitable for basement installation in two sizes with outputs from 110,000 Btu to 165,000 Btu. The "B" Series Hi-Boy suitable for either basement or first floor installation in basementless houses available in two sizes with capacities of 93,500 Btu to 110,000 Btu. The "K" Series oil-fired air conditioners made in two sizes with outputs of 203,000 Btu and 294,000 Btu suitable for larger spaces.

"A" SERIES OIL FIRED AIR CONDITIONERS

Built For Fine Homes. Compact in Size. But Highly Efficient

Furnace Number	Input Btu/Hr	Gph	Output at Bonnet	Cfm	Fan Size	Mtr. Hp	No. & Size of Filters	Vent Diam.	L	W	H	W. A. Plenum	R. A. Plenum
A-100	140,000	1	110,000	1200	10	1/4	2 - 20x20x2	6	71	25	48	20x21	20x21
A-150	210,000	1.5	165,000	1800	12	1/4	4 - 16x20x2	8	81	32	48	26x28	24x28

"B" SERIES OIL FIRED HI-BOY

This Hi-Boy Handles Small Homes and Buildings Using A Minimum of Floor Space

B-85	119,000	.85	93,500	1000	10	1/6	1 - 25x20x1	6	28	26	65	22x24	
B-100	140,000	1.0	110,000	1200	10	1/4	1 - 25x20x1	6	28	26	70	22x24	

"K" SERIES OIL FIRED AIR CONDITIONERS

A Heavy Duty Type Unit That Has A Fine Background of Successful Service

K-175	258,000	2	203,000	2690	15	1/2	4 - 20x20x2	9	46	79	55	35x38	40x26
K-250	368,000	3	294,000	3890	15	3/4	4 - 20x20x2	9	52	82	55	41x41	40x26

The MEYER gas-fired air conditioner as illustrated above is available in five sizes from 110,000 Btu per hour to 495,000 Btu per hour input capacities.

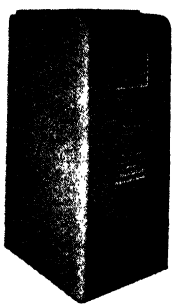
"F" SERIES GAS FIRED AIR CONDITIONERS

These Units are Unsually Compact and Can Be Equipped For Manufactured, Natural, or Liquified Petroleum Gas

Furnace Number	Input Btu/Hr	Output at Bonnet	Cfm	Fan Size	Mtr. Hp	Vent Diam.	No. & Size of Filters	L	W	H	W. A. Plenum	R. A. Plenum
F-10	110,000	88,000	960	10"	1/4	5	2 - 20x20x2	65	25	48	20x21	20x21
F-15	165,000	132,000	1440	12"	1/4	6	4 - 16x20x2	69	32	48	20x28	20x28
F-20	220,000	176,000	2400	2-10"	1/3	2-5	4 - 20x20x2	65	46	48	20x42	20x42
F-30	330,000	264,000	3600	2-12"	1/2	2-6	6 - 20x20x2	69	60	48	20x56	20x56
F-45	495,000	396,000	5400	3-12"	3/4	3-6	8 - 20x20x2	69	88	48	20x84	20x84

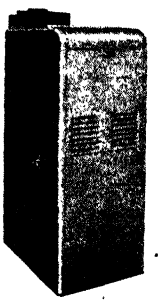
L. J. Mueller Furnace Co. - Milwaukee 7, Wis.

HEATING — MUELLER Climatrol REG. U. S. PAT. OFF. — AIR CONDITIONING



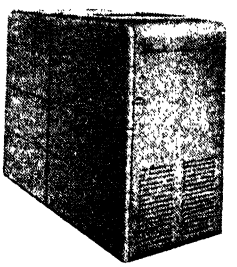
Series "SHP"

Gas-fired winter air conditioner. May be installed in basement or utility room. Available in three sizes, with *A.G.A.* input ratings from 60,000 to 100,000 Btu per hour. Provides wide range of air delivery capacities to meet specific needs.



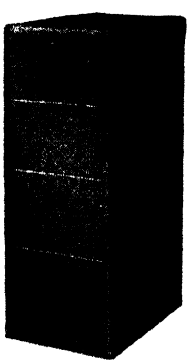
Type "107"

Gas-fired cast iron winter air conditioner for basement or utility room installation. Furnished in three sizes, with *A.G.A.* input ratings of 60,000, 90,000 and 120,000 Btu per hour. Also available for gravity operation in two sizes.



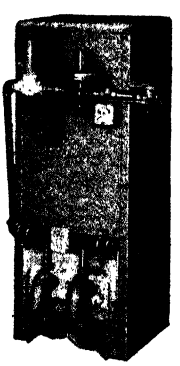
Type "102"

This gas-fired winter air conditioner is of sectional construction, with the blower compartment at the rear of the unit. It is available in three sizes with *A.G.A.* input ratings of 135,000, 180,000 and 225,000 Btu per hour.



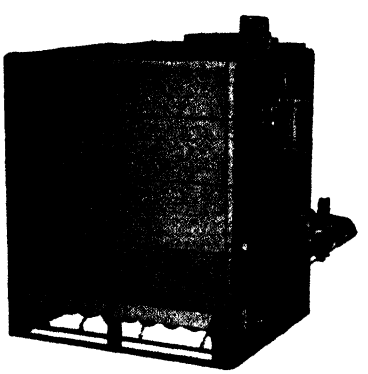
Type "10"

Gas-fired boiler, with enclosed controls, used primarily for residential installation. It has *A.G.A.* ratings of 290 to 2015 sq ft for hot water and 180 to 1260 sq ft for steam.



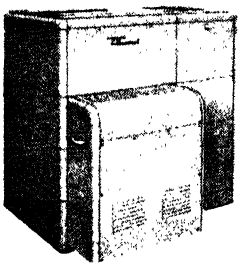
Type "11"

Gas-fired boiler, without enclosed controls, used primarily for home installation. It has *A.G.A.* ratings of 290 to 2015 sq ft for hot water and 180 to 1260 sq ft for steam.



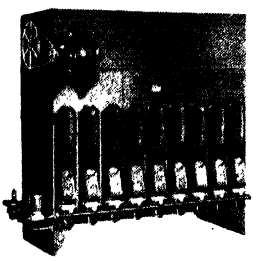
Type "20"

Gas-fired boiler used extensively for industrial installation. It has *A.G.A.* ratings of 1010 to 10,080 sq ft for hot water and 630 to 6300 sq ft for steam. Both this boiler and the Types "10" and "11" can be equipped for both direct and indirect applications.



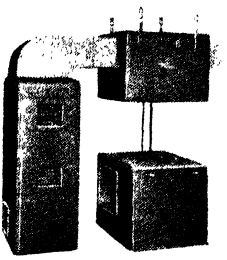
Type "105"

Gas-fired winter air conditioner with *A.G.A.* inputs of 100,000 and 150,000 Btu. Can be converted to oil. Also available for gravity operation.



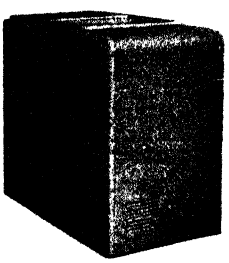
Series "UH"

Gas-fired unit heater for large space-heating requirements. Available in 4 through 12 sections, with *A.G.A.* inputs of 180,000 to 540,000 Btu per hour.



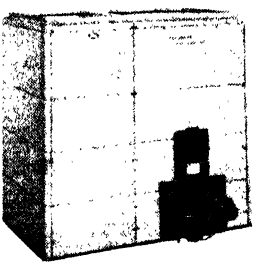
Type "900" and "SHP"

Type "900" Summer Air Conditioner is available in 3- and 5-ton sizes. It consists of a cooling coil and cabinet, compressor and cabinet, plus accessories.



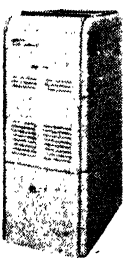
Series "50"

Oil-fired winter air conditioner with outputs at register of 100,000 to 225,000 Btu, with selection of blower sizes. Fired by pressure-atomizing burner.



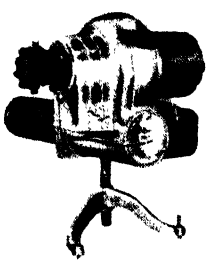
Type "202"

Oil-fired winter air conditioner available with inputs of 100,000 and 150,000 Btu. Unit may be converted to gas. Also available for gravity operation.



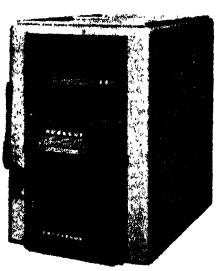
Type "209"

Oil-fired winter air conditioner with 90,000 and 120,000 Btu inputs with pressure burner; 60,000, 90,000 and 120,000 Btu with vaporizing burner.



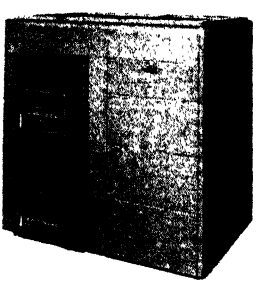
Type "450"

Oil-fired conversion burner of the pressure-atomizing type. Burner is available with inputs of 1 gallon through 5 gallons of oil per hour.



Series "FB"

Cast-iron, coal-fired winter air conditioner. Five sizes, with capacities at register from 94,400 to 198,900 Btu.



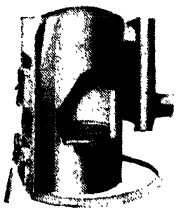
Type "702"

Steel, coal-fired winter air conditioner. 3 sizes, 20 in. to 24 in. drums, with capacities at register from 92,650 to 122,000 Btu per hour.

The Waterman-Waterbury Co.

Minneapolis 13, Minnesota

Manufacturers of WATERBURY Coal, Oil and Gas Fired Furnaces and Air Conditioning Equipment



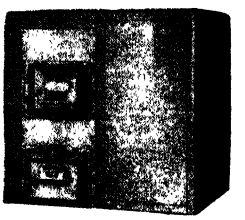
WATERBURY GAS-TITE FURNACE 700 Series

The welded steel furnace body keeps dust, smoke and fumes out of the air stream. A large combustion chamber and radiator with long fire travel insure efficiency and economy.

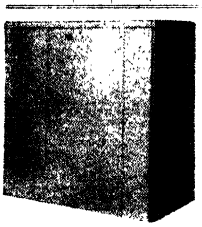
Also furnished in a complete home Air Conditioner.

Size Furnace	Diameter		Height		Steel Thickness			Diam. Smoke Pipe	Approx. Shipping Wt Lbs Furnace less Casing	Output Ratings	
	Furnace Body	Pipe Casing	Furnace Body	Pipe Casing & Hood	Body	Head	Radiator			Sq In. Leader Pipe	Btu at Bonnet
720	20″	39″	49″	64″	10 Ga.	10 Ga.	12 Ga.	8″	531	482	87,529
722	22″	41″	49″	64″	10 Ga.	7 Ga.	12 Ga.	8″	603	505	91,730
724	24″	44″	49″	64″	7 Ga.	7 Ga.	12 Ga	9″	730	541	98,056
727	27″	46″	55″	70″	7 Ga.	1/4″	12 Ga.	9″	866	672	121,856

Gastite Air Conditioner



Size	Width	Length	Height	Size Outlet Opening	Size Inlet Opening	No. of Filters	Size thru Unit Filter	Blower CfmRange	Btu Per Hour Output at Bonnet
720-10	36″	50″	55″	32x24	32x16	2	16x16	375 to 1050	87,963
722-10	40″	56″	55″	36x26	36x22	2	20x20	375 to 1050	94,011
724-10	40″	56″	55″	36x26	36x22	2	20x20	375 to 1050	100,193
724-12	40″	56″	55″	36x26	36x22	2	20x20	645 to 1677	100,193

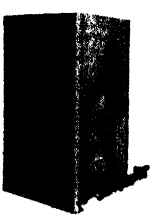


WATERBURY GAS FIRED AIR CONDITIONER

The latest achievement of Waterbury's engineers, designed specifically for gas. Completely automatic—filtered, humidified forced air—enclosed in a compact, baked enamel casing. Can also be furnished for Propane or Butane.

Size	Input Rating Btu per Hr	Output Capacity Btu per hour at Register	*Blower Cfm Range	Width In.	Length (Heater Casing Plus Blower Casing)	Height Overall In.	Size Outlet Opening	Size Return Inlet Opening	No. of Filters	Size each Filter	** Rec Flue Pipe Diam.	Size Gas Connection Required
6413-9	90,000	72,000	400 to 800	28		50	20x24	15 x24	2	16x25	5″	3/4″
6413-9 High	90,000	72,000	400 to 800	28	28	64	24x24		1	16x25	5″	3/4″
6415-10	120,000	96,000	600 to 1200	28		58	20x24	16 x24	2	16x25	6″	3/4″
									1	16x25		
6426-12	180,000	144,000	800 to 1800	55	52	50	24x51	19 5/8x26	1	20x25	2-5 to 7″	1″
6426-15	180,000	144,000	1000 to 2800	55	56	50	24x51	25 1/16x34 7/16	4	16x20	2-5 to 7″	1″
6430-15	240,000	192,000	1000 to 2800	55	56	58	24x51	25 1/16x34 7/16	4	16x20	2-6 to 8″	1 1/4″
6430-18	240,000	192,000	1232 to 3204	55	72	58	24x51	40 x36	6	16x25	2-6 to 8″	1 1/4″

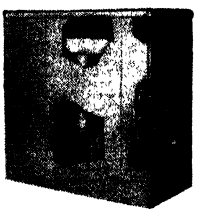
WATERBURY GAS GRAVITY FURNACE



Size Furnace	Input Rating Btu per Hr	Output Rating Sq In. Warm Air Pipe	Width In.	Length In.	Height Overall In.	Size Outlet Opening	**Rec. Flue Pipe Diam.	Size Gas Connection Required In.
6413	90,000	67,500	28	28	50	24x24	5″	3/4″
6415	120,000	90,000	30	30	58	26x26	6″	3/4″
6426	180,000	135,000	28	55	50	24x51	2-5 to 7″	1″
6430	240,000	180,000	30	58	58	26x54	2-6 to 8″	1 1/4″

The Waterman-Waterbury Co.

Minneapolis 13, Minnesota



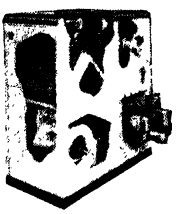
WATERBURY 6300 Series OIL FIRED AIR CONDITIONER

Completely automatic oil heat with forced, filtered, humidified air, all enclosed in one compact casing finished in baked enamel.

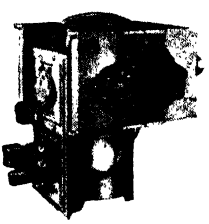
Size	Input Rating Gal Oil per Hr	Output Capacity Btu per Hr at Bonnet	Width Casing	Length Casing	Height Overall	Size Outlet Opening	Size Return Inlet Opening	Distance between Opening	No. of Filters	Size each Filter	Diam. Smoke Pipe
W-6315-10	1 gal	97,000	28″	58″	58″	24x20	24x16	3″	2	16x25	7″

2320-12 OIL FIRED AIR CONDITIONER

This unit has a side mounted burner and can be furnished with a burner hood at slight additional cost.



Size	Input Rating Gal Oil per Hr	Output Capacity Btu per Hr at Register	Width Not Incl. Burner Hood	Length	Height Overall	Size Outlet Opening	Size Return Inlet Opening	Distance between Openings	No. of Filters	Size Each Filter	Diam. Smoke Pipe	Dimens. Burner Hood Wdt. (Side-Side)	Dimens. Burner Hood Depth	Dimens. Burner Hood Hgt.
2320-12	1.20	120,000	30	60	61	26x24 1/8	26x24 1/8	6 7/8″	2	1-16x25 1-20x25	7″	23	17	28



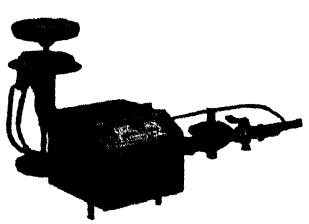
SEAMLESS OIL FIRED FURNACE BODY

Specially engineered for oil firing only, it may be used as a gravity circulating pipe furnace. It is the heating element of the Comfortrol Oil Fired Air Conditioners.

Specifications Comfortrol Oil Fired Air Conditioners

Size	Input Rating Gal per Hr	Btu per Hr at Register	Normal Cfm Range	Width Less Front Hood	Length Overall	Height	Size Outlet	Size Inlet	Filters No.	Filters Size	Smoke Pipe
1322-12	1.5	142,763	645 to 1677	44″	72″	64″	36x36	19 5/8x26	1	20x25	8
									1	16x25	
1322-15	1.5	142,763	922 to 2397	44″	74″	64″	36x36	25 1/16x34 7/16	4	16x20	8
1324-15	2.0	190,350	922 to 2397	48″	78″	64″	40x40	25 1/16x34 7/16	4	16x20	8
1324-18	2.0	190,350	1232 to 3204	48″	81″	64″	40x40	40 x36	4	20x25	8
1327-18	2.5	237,938	1232 to 3204	52″	85″	64″	44x44	40 x36	4	20x25	9
1327-21	2.5	237,938	1450 to 3770	52″	85″	64″	44x44	38 x44	6	16x25	9
1330-21	3.0	285,525	1450 to 3770	56″	89″	70″	48x48	38 x44	6	16x25	9
1333-24	3.5	333,113	1968 to 5118	60″	104″	72″	52x52	46 x48	6	20x25	9
1336-24	4.0	380,700	1968 to 5118	66″	110″	81″	58x58	46 x48	6	20x25	9

‡Burner hood all sizes is 24 in. wide, 10 in. deep.
*Add 140 lbs for oil burner and controls. Add 80 lbs for burner hood.



GAS CONVERSION BURNER

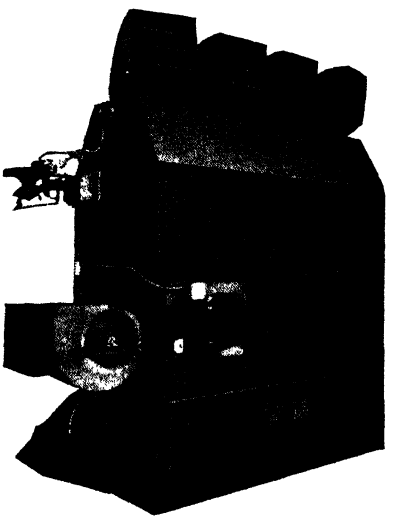
A real gas burner, the same as used in the Gas Air Conditioner. Can also be furnished for Propane or Butane.

Number	Maximum Btu Input	Maximum Cubic Feet of Mixed Gas	Maximum Cubic Feet of Manuf'd. Gas	Minimum Fire Pot Size
G-100	165,000	208	300	18 Inch

Airtherm Manufacturing Company

728 S. Spring Ave.
St. Louis 10, Mo.

THE ENGINEERED LINE OF UNIT HEATERS



AIRTHERM

Direct-Fired Warm Air Heaters

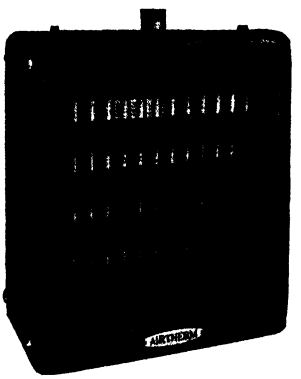
Offer You These Six Heating Advantages

1.—A complete factory heating unit.
2.—Comes to you ready to set in place.
3.—Control system wired at factory.
4.—Available in floor-mounted or suspended models.
5.—Oil burners or gas burners are interchangeable to meet future fuel conditions.
6.—Capacities from 650,000 to 1,950,000 Btu per hour.

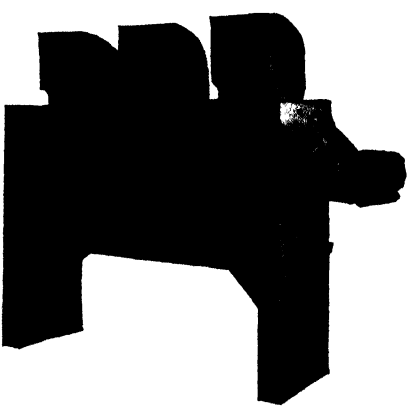
For detailed information, write for Bulletin 801-A.

AIRTHERM STEAM UNIT HEATERS

(Copper Coils)



Airtherm Horizontal Propeller Type Steam Unit Heater available in capacities from 26,000 to 274,000 Btu. Write for Bulletin 1206.



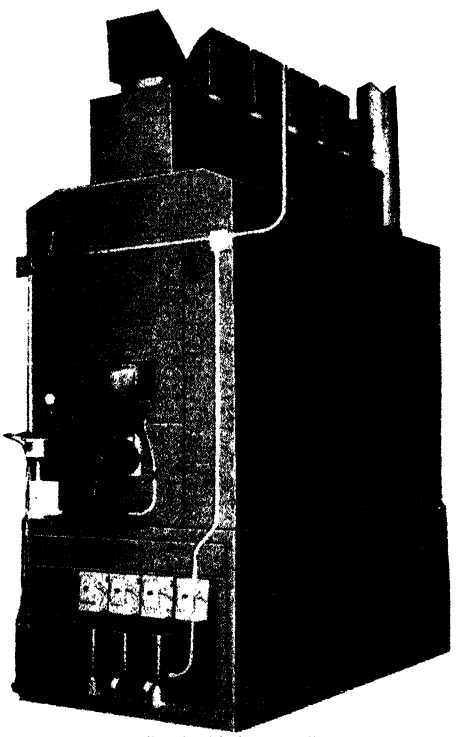
Airtherm Blower Fan Type Unit Heater available in capacities from 222,000 to 827,000 Btu. Floor, vertical or horizontal models. Write for Bulletin 401.

Chicago Steel Furnace Co.

9326 S. Anthony Ave., **Chicago 17, Ill.**

DIRECT-FIRED SPACE HEATERS

Standard Sizes Up to 1,500,000 B.T.U.



Fired with Gas or Oil

HEAT EXCHANGER—Designed and constructed in a near tear-drop shape which permits the air to flow with a minimum of friction. This design affords a maximum of both strength and area in its crown sheet, and reduces power consumption to the very minimum.

COMBUSTION CHAMBER—Fabricated from four way $\frac{3}{16}$ and $\frac{1}{4}$ in. floor plate. The chamber is of the correct size and shape to provide proper volumetric content for the complete combustion of oil or gas.

BLOWERS—Three standard up-blast discharge, multi-vane Blowers, each individually powered, are provided to supply the correct amount of air to properly cool the Heat Exchanger. Individually-driven Blowers are used because of the great flexibility of operation obtainable. Uniform bonnet temperature may be enjoyed by the simple expediency of increasing or reducing the amount of air driven around any particular section of the Heat Exchanger.

A Modern, Economical and Flexible Method of Heating Large Areas

TECHNICAL AND RATING DATA—Larger Sizes Available

SERIES "A"—MODEL NUMBERS		350-A	500-A	750-A	1000-A
Heat Delivery	Btu. per Hr.	350,000	500,000	750,000	1,000,000
Heating Surface	Sq. In.	26,152	34,152	46,330	59,124
Combustion Space	Cu. In.	82,264	119,416	182,232	243,524
Oil Firing Rate	G. P. H.	2.5—4.0	4.0—6.0	6.0—9.0	9.0—12.0
Air Delivery	C. F. M.	3,000 to 4,200	6,000 to 7,800	8,200 to 9,600	12,500 to 15,000
Blower Motor	3 Req'd. (ea.)	¼ H. P.	⅓ H. P.	½ H. P.	1.0 H. P.
Dimensions					
Height	overall	8'—0"	9'—6"	9'—10"	10'—6"
Width	overall	3'—0"	3'—6"	4'—2"	4'—8"
Length	overall	6'—10"	7'—10"	8'—4"	10'—0"
Cold Air Inlet	2 each	6'-10" x 2'-0"	7'-10" x 2'-3"	8'-4" x 2'-7"	10'-0" x 3'-0"
Warm Air Outlet		6'-0" x 1'-0"	7'-0" x 1'-8"	8'-0" x 1'-8"	10'-0" x 2'-0"
Flue Gas Outlet	Diam.	8"	10"	12"	14"

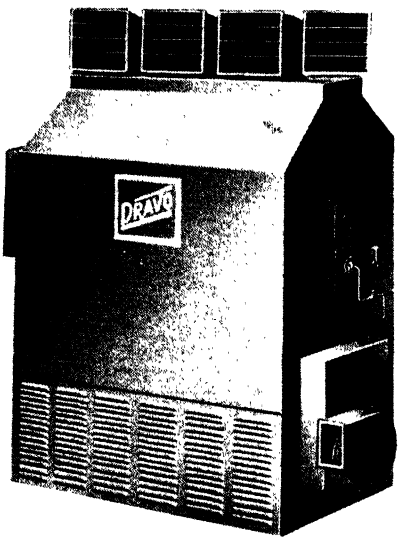
"TERRITORIES NOW BEING ASSIGNED"

DRAVO CORPORATION

HEATING SECTION

Dravo Bldg., PITTSBURGH 22, PA.

Sales Offices in Principal Cities



Gas-Fired Dravo Counterflo Direct Fired Heater

DRAVO COUNTERFLO DIRECT FIRED HEATERS

Dravo Counterflo Direct Fired Heaters are designed for open-space heating in factories, warehouses, terminals, garages, foundries, airport hangars, mills, machine shops, and similar establishments.

Each unit is a self-contained heating plant embodying burner, combustion chamber, supplementary heat transfer surface, motor-driven fans, louvred cowls, and automatic control system. Dravo Counterflo Direct Fired Heaters may be installed as single units, or in multiple, for buildings of any size.

Installation is simple and can be performed by any skilled mechanic. Only three connections need be made,—to fuel supply, electric power, and flue vent. This simplicity permits installation of Dravo Counterflo Direct Fired Heaters for temporary heating during building construction; permanent connections can be made when heater locations are established

Descriptive Bulletin FW-516, and specification sheets, are available on request. *Write Heating Section*, DRAVO CORPORATION, Pittsburgh 22, Pennsylvania.

DRAVO CORPORATION

Pittsburgh

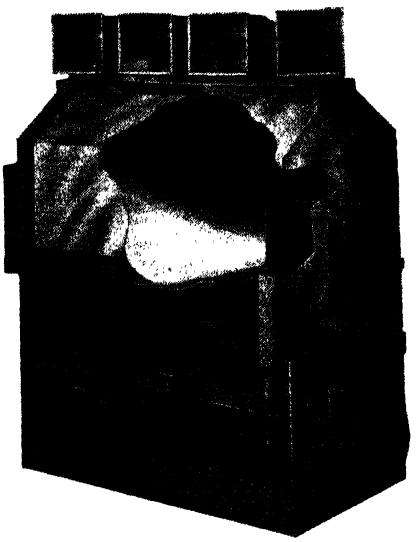
Philadelphia • Chicago
Cleveland • Detroit
New York • Atlanta
Wilmington

Distributors for Dravo Counterflo Direct Fired Heaters are located in key cities.

Features of Dravo Counterflo Direct Fired Heaters include:

- Stainless Steel Combustion Chamber.
- Counterflo Combustion and Heat Transfer.
- 80-85 per cent Sustained Efficiency.
- Effective Comfort-Zone Recirculation.
- Minimum Heat Loss Thru Roof.
- Simplicity of Installation.
- Flexibility of Application.
- Adaptability for Wide Range of Fuels.

Unit capacities of Dravo Counterflo Direct Fired Heaters range from 400,000 to 2,000,000 Btu per hour output. The following tables show the external dimensions and weights of the various units as well as the capacities of each size heater.



Cut-away view of heater showing counterflo principle of combustion and heat-transfer, as well as the four-pass gas-flow system

ENGINEERING DATA

Heater Number	Btu Output Capacity	Air at 70 Deg. Free Delivery		Fan Motor HP	No. Discharge Cowls	Approx. Shipping Weight
		Approx. CFM	Temp. Rise Deg. F			
40	400,000	4500	83	1½	3	1100
50	500,000	5500	84	2	3	1150
75	750,000	8500	81	3	4	2200
100	1,000,000	11000	84	5	4	2300
125	1,250,000	14000	83	7½	4	3000
150	1,500,000	17000	81	10	4	3100
175	1,750,000	19000	85	15	4	3900
200	2,000,000	22000	84	20	4	4000

Heater Number	FUEL CONSUMPTION—80 per cent Heater Efficiency Assumed			Approximate Overall Dimensions		
	Light Oil GPH (135000 Btu Oil)	Heavy Oil GPH (148000 Btu Oil)	Gas CFH (1000 Btu Gas)	Width	Length	Height
				Ft—In.	Ft—In.	Ft—In.
40	3.7	3.5	500	2—7	4—11	8—1
50	4.6	4.3	625	2—7	4—11	8—1
75	7.0	6.5	940	3—8	7— 3	10—0
100	9.3	8.6	1250	3—8	7— 3	10—0
125	11.5	10.8	1560	4—3	8—11	11—2
150	14.0	13.0	1875	4—3	8—11	11—2
175	16.2	15.0	2190	4—9	9— 5	12—9
200	18.5	17.2	2500	4—9	9— 5	12—9

Lee Engineering Company

Union National Bank Bldg., **Youngstown, Ohio**

LEE DIRECT WARM AIR HEATING

The Lee System of warm air heating generally costs less to install than steam or hot water; utilizes fuel with a high degree of efficiency; distributes the heat exactly where needed; responds promptly without lag; requires little or no maintenance; and needs no licensed attendant. Heaters for use with the Lee System are made in the four types illustrated and described briefly below.

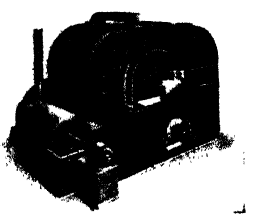
BRICK-SET TUBULAR HEATER

For use with central heating system in connection with duct distribution. Single heater capacities from 2,800,000 Btu per hour to 8,000,000 Btu per hour. Two heaters, installed as a battery serving as one unit, provide capacities over 10,000,000 Btu per hour.

Brick Set Tubular Heater

STEEL ENCASED TUBULAR HEATER

For use with central heating systems in connection with duct distribution over a capacity range of from 2,000,000 Btu per hour to 6,000,000 Btu per hour. Heater may be installed in heated area without enclosure, requires no foundation, and may be moved from one location to another by taking unit apart and reassembling.



Steel Encased Tubular Heater

TUBULAR UNIT HEATER

For use either as a central system in connection with duct distribution or with adjustable outlet nozzles as a unit heater. Capacity range from 2,000,000 Btu to 6,000,000 Btu per hour. In sizes up to 4,000,000 Btu heater is shipped as a completely assembled unit with all but mechanical equipment, refractory lining and controls in place. Heaters require no foundation and are equipped with crane hooks so that they may be moved from one location to another.

Tubular Unit Heater

SHELL UNIT HEATER

For use with or without distributing duct system. Heaters have capacity range of from 300,000 Btu to 2,000,000 Btu per hour. Available for gas, oil or combination gas-oil firing. All units are shipped completely assembled, wired and ready for operation. Units furnished with either refractory lined or stainless steel combustion chambers. Heaters may be floor mounted or suspended in any position. Also available in both hand and stoker fired models.

Shell Unit Heater

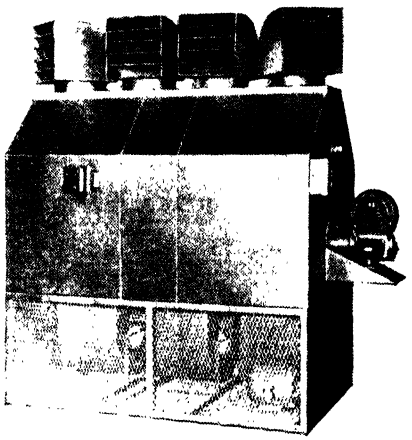
For further information write for Catalog HV-44.

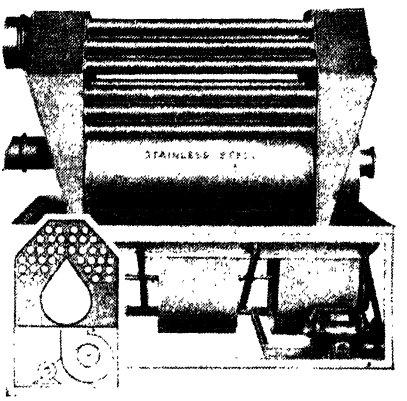
National Heater Company

2182 Cleora Avenue, **St. Paul 4, Minnesota**

NATIONAL CHAMPION

STEEL S-P-A-C-E HEATERS





GAS AND OIL FIRED UNITS

National Champion Heaters are available in both factory floor set units, as illustrated, and in quiet operating, resilient mounted models for convenient connection to duct distribution system. Skeleton view illustrates compactness of heat exchanger and blower section mounted on sturdy angle-iron base frame. Lifting eyes are provided for crane handling. Streamlined firebox of rust and heat resisting Stainless Steel requires no refractory and affords life far beyond that possible with mild carbon steel. Tear Drop combustion chamber design and convector tube arrangement assure complete efficient air impingement on all heating surface at a minimum of resistance. Induced draft blowers can be supplied when suitable chimney or stack is not available.

ENGINEERING RATING CHART—TEAR DROP DIRECT FIRED HEATERS

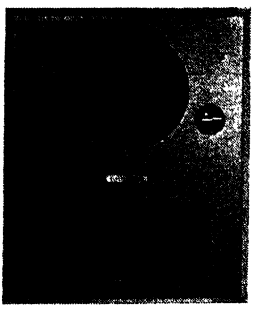
Heater Number	B.T.U. Output Capacity	½ S.P. C.F.M.	Sq. Ft. Heating Surface	Blowers D W D I	Maximum Firing Rate		Blower Motor		Stack Req'd. Minimum	
					Oil G.P.H.	Gas C.F.H.	H.P.	R.P.M.	Dia. Inches	Hgt. Feet
T.D. 25	250,000	3,600	120	14" Twin	2.5	330	¾	1750	10	20
T.D. 40	400,000	5,400	130	14" Twin	4.0	550	1	1750	10	20
T.D. 50	500,000	6,600	150	14" Triple	5.0	680	1½	1750	10	25
T.D. 70	700,000	8,800	175	14" Triple	7.0	940	2	1750	10	25
T.D. 80	800,000	10,200	200	16" Triple	7.5	1100	2	1750	12	30
T.D. 100	1,000,000	12,500	250	16" Triple	9.5	1400	3	1750	12	30
T.D. 125	1,250,000	15,300	315	18" Triple	11.5	1610	5	1750	14	35
T.D. 150	1,500,000	19,400	375	18" Triple	14.0	2040	5	1750	14	35

Heater Number	Tubes		Approximate Shipping Weight	Warm Air Plenum Opening	Overall Dimensions Inches			Gauge Material				
	No.	Dia.			Width	Length	Height	Tubes	Headers	Stainless Steel Comb. Chamber	Casing	Discharge Heads
T.D. 25	23	3	1,300	14 x 60	32	60	81	14	12	14	20	18
T.D. 40	23	3	1,350	14 x 60	32	60	81	14	12	14	20	18
T.D. 50	23	3	1,780	14 x 80	32	80	81	14	12	14	20	18
T.D. 70	23	3	1,855	14 x 80	32	80	81	14	12	14	20	18
T.D. 80	36	3	2,110	18 x 80	48	80	81	14	10	14	20	18
T.D. 100	36	3	2,200	18 x 80	48	80	81	14	10	14	20	18
T.D. 125	48	3	3,000	20 x 100	54	100	96	14	3/16	14	20	18
T.D. 150	48	3	3,250	20 x 100	54	100	96	14	1/4	14	20	18

ELECTROMODE CORPORATION

45 Crouch St. Rochester 3, N.Y.

FOR HOME • ELECTROMODE All Electric HEATERS • INDUSTRY • FARM



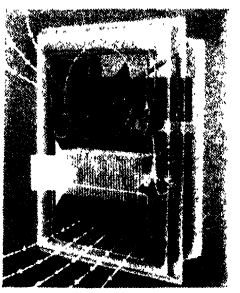
BILT-IN-WALL Heaters For Homes and Offices

These room heaters circulate warm air at floor level for greatest efficiency. No ductwork required. Economical to install as auxiliaries, or (where electric rates permit) as main heat sources. Manual or thermostatic control. Thermal cutoff prevents overheating. Electromodes are approved by *Underwriters' Laboratories;* fully guaranteed.

Model	Watts	BTU	Volts AC 60 Cycle	Shipping Wt. in Carton
W12-15S	1500	5,122	115 or 230*	40 lbs
W12-20S	2000	6,830	230	40 lbs
W12-20	2000	6,830	230	40 lbs
W12-30S	3000	10,245	230	40 lbs
W12-30	3000	10,245	230	40 lbs

*Specify which voltage

"S" denotes single heat control. All others equipped with variable heat switch. 2 KW and 3 KW sizes wired for 3-wire, S/N, 115/230 volt service. Dimensions (front plate): 21 in. high, 17 in. wide. Each heater shipped complete with wall box to fit standard 2 in. x 4 in. wall construction. Approximate wall opening required: 18¼ in. high, 14¼ in. wide. Finish: baked-on brown enamel.



X-ray View shows cast-aluminum Safety-Grid element (large arrow) which provides complete safety from fire, shock or burn. Small arrows illustrate "Down-Flo" heat circulation.

Bilt-in-SMALL-ROOM Heater

For baths, small bedrooms, dinettes, trailers, etc. Quickly installed; operates on usual 115 volt lighting circuit. Cast-aluminum Safety-Grid element, with safety thermal cutoff. Manual or thermostatic control. Two-way switch permits use of fan, without heat, when desired. White baked-on enamel finish. Approved by *Underwriters' Laboratories.* Guaranteed.

Model	Watts	BTU	Volts AC Only	Net Weight	Shipping Weight
WJ-13	1320	4508	115	13¼ lbs. including wall box	14 lbs in carton

Shipped complete with wall box, for standard 2 in. x 4 in. wall construction. Approx. opening required, 9⅞ in. x 11⅛ in. Toggle type fastener allows for various wall thicknesses. Heater front plate dimensions: 11½ in. high, 12⅞ in. wide.

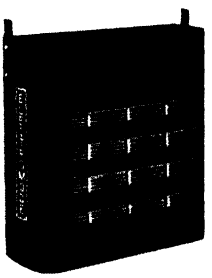
Write for Information

Specific literature is available on these and other Electromodes for domestic and industrial heating. See your electrical supplier, or write Dept. HV-18, Electromode Corporation.

ELECTROMODE CORPORATION

45 Crouch St. Rochester 3, N.Y.

FOR HOME • ELECTROMODE All Electric HEATERS • INDUSTRY • FARM



Unit Heaters For Auxiliary Warmth Cut Heating Costs; Easily Installed

SUSPENSION TYPE

For wall or ceiling mounting. 10 to 60 KW. Electromodes are approved by *Underwriters' Laboratories;* guaranteed.

No Exposed Hot Wires

Safety-Grid consists of a tubular element embedded in a finned aluminum casting. This patented design gives high thermal conductivity, safety, resistance to corrosion.

10 KW to 60 KW Heaters

For 230 or 460 volts—specify when ordering.

Model	KW	BTU	CFM Approx.	Shipping Wt. Approx.
[a]14-10	10	34,150	800	100 lbs
[a]14-12	12	40,980	800	100 lbs
[a]18-15	15	51,225	1500	180 lbs
18-20	20	68,300	1500	180 lbs
20-25	25	85,375	1800	200 lbs
20-35	35	119,525	1800	200 lbs
27-45	45	153,675	4000	360 lbs
27-60	60	204,900	4000	360 lbs

[a]Models 14-10, 14-12, 18-15 are for single or 3 phase. Other models for 3 phase only.

Heaters are furnished with 460-volt single or 3-phase heater elements; with 115 or 230-volt single-phase motor.

Thermostatic Control

Available with all models. A contactor is necessary on units above 5 KW capacity, on 3 phase and on DC, to operate safety switch, thermostat.

These all-electric units supply fan-forced warmth, directed as desired. As auxiliary heat sources, they replace the central heating system during changeable weather, or when only some departments need heat. As main heat sources (where electric rates permit), they eliminate the need for a central heating system. They require no plumbing or ductwork—only circuit wiring.

Combination Portable and Suspension Type

Contains a circular Safety-Grid element. Capacities, 1.5 to 7.5 KW. Electromodes are approved by *Underwriters' Laboratories*; guaranteed.

1.5 KW to 7.5 KW Heaters

Model	KW	BTU	CFM Approx.	Shipping Wt. in Carton
[a]AA-15	1.5	5,122	100	20 lbs
[b]AN-30	3	10,245	200	30 lbs
[c]BN-50	5	17,075	350	44 lbs
[d]CN-7.5	7.5	25,613	550	60 lbs

[a]AA-15 may be plugged into usual 115V branch circuit. Also available for 230V single phase.

[b]AN-30 is for 115V or 230V—specify which.

[c]BN-50 furnished with switch but without cord or plug. 230V single or 3 phase; 460V 3 phase.

[d]CN-7.5 furnished without switch, cord or plug. 230V single or 3 phase; 460V 3 phase.

Models AA-15 and AN-30 furnished with on-off switch, 10 ft heavy-duty cord, plug.

Heaters for Special Applications

Blower units, blast heaters for air ducts, mobile units on casters; others. Engineering help is at your disposal.

COMBUSTION CONTROL CORPORATION

Flame Failure Safeguards (fireye) *Boiler Feedwater Controls*

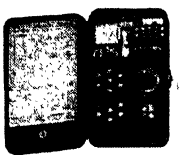
77 Broadway, **Cambridge 42, Mass.**

205 W. Wacker Drive, Chicago—765 Cordilleras Ave., San Carlos, San Francisco

District Offices in all Principal Cities

FIREYE PHOTOELECTRIC FLAME FAILURE SAFEGUARD AND PROGRAMMING CONTROL FOR OIL BURNERS

Type 45PH5



Type 24PJ8

Type 45JP1

Complete operating and starting protection for industrial and commercial oil burners with Flame Rod protection of gas pilot. Type 24PJ8 automatically starts burner and programs sequence of gas pilot, ignition, burner motor, oil valves, providing scavenging period, fuel valve delay, post ignition time. Flame Rod, Type 45JP1, monitors gas pilot flame, preventing opening of oil valve unless gas pilot is established. Scanner Type 45PH5 takes over monitoring of oil flame after pilot is established. Failure of either gas flame during ignition or main oil flame during normal operation results in immediate shutdown of burner system.

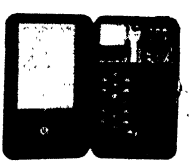
Fireye equipment is available in combinations providing one or all of these safeguard functions, depending on requirements of installation.

FIREYE ELECTRONIC ROD FLAME FAILURE SAFEGUARD AND CONTROL FOR GAS BURNERS

Operating protection for industrial and commerical gas burners. Flame Rod Type 45JQ1 constantly monitors gas pilot flame after its manual or electric ignition. Main gas valve cannot open until Flame Rod indicates pilot flame is established. Pilot flame failure after opening of main fuel valve is instantly signalled by Flame Rod to Electronic Control Type 24QJ5, which immediately shuts off Burner.

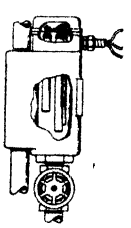
Fireye equipment is designed with completely fail-safe characteristics. Any circuit element failure results in system shutdown. A built-in low-voltage interlock completely checks system, internal and external to control, on each burner recycle.

Type 24QJ5

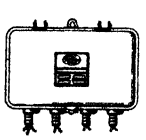


Type 45JQ1

FIREYE BOILER FEEDWATER CONTROL AND BOILER WATER CUTOFF



Type 65BF3



Type 15GK1

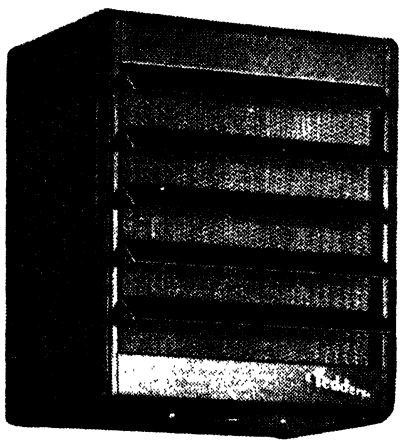
Electrically maintains desired boiler water level. When level drops dangerously low fuel supply instantly cuts off and alarm sounds. Fireye Boiler Feedwater control is alternating current control. Combines probe circuit and transformer to operate direct current relay through a rectifier. Using direct current in relay circuit increases contact pressure, makes possible use of low a-c voltages in probe circuit thereby eliminating electrolysis problems and probe sealing. Noncorrosive probe fittings, designed for pressures up to 300 psig mount parallel to boiler water control.

FEDDERS-QUIGAN CORPORATION

85 Tonawanda St.

Buffalo, New York

Heat Transfer Specialists Since 1896



Fedders Series 15 Horizontal Unit Heaters with Streamline Copper Tubes and Fins

Fedders UNIT HEATERS

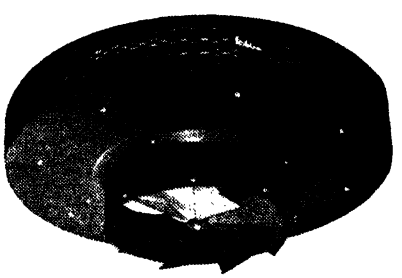
Horizontal Type

COPPER TUBES AND FINS

Fedders streamline tubes provide aerodynamic efficiency and the ample-area saddle of the fins gives generous bonded metal-to-metal contact between copper tubes and fins for high thermal efficiency. Handsome, rugged cabinets—complete relief of expansion stresses within the core as well as between core and cabinet—latest type broad blade fans provide large air volume, quiet operation and maximum efficiency. Large Btu capacity with low final temperatures assure ideal working conditions. Capacities, 100 to 1,000 EDR. Write for Bulletin 15C-3.

Fedders
DOWNBLOW
UNIT HEATERS

Used where requirements necessitate clearance for material handling equipment, tall machinery and other conditions requiring piping to be kept out of the way and for spot locations such as over frequently opened shipping room doors.



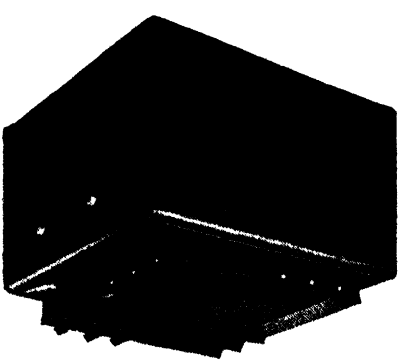
COPPER TUBES AND FINS

Straight downblow or diffusion of heat is accomplished by adjustable directional outlets to fit conditions.

Circular type for ceiling heights from 20 to 45 ft. 800 to 1800 EDR capacities.

Square models chiefly for medium ceiling heights of 15 to 25 ft.

Write for Bulletin 12C-3.



Grinnell Company, Inc.

Heating, Industrial and Power Plant Piping, Fittings, Hangers, Valves, Pipe Bending, Welding, Piping Supplies, Etc.

Executive Offices: **Providence 1, R. I.**

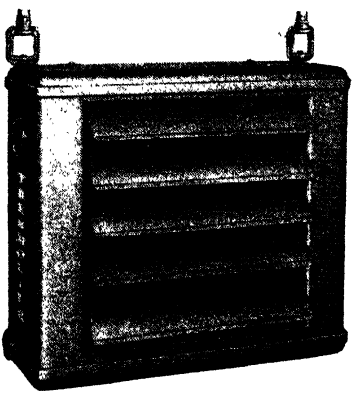
National Distributors of Thermoflex Traps and Heating Specialties

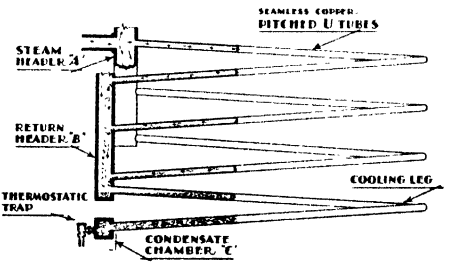
For data on other Grinnell Products, see pages 1118-1119

THERMOLIER

REG. U. S. PAT. OFF.

THE GRINNELL UNIT HEATER





Patented Construction of Internal Cooling Leg

In addition to its patented Internal Cooling Leg Thermolier has many other desirable features including its Single Header U-Tube construction which compensates for expansion and contraction strains. Radiation is from brass-finned seamless copper U-tubes rolled into a cast iron tube sheet.

Steam circulation and the removal of condensation in Thermolier are distinctly different than is usual in unit heaters. The actual cooling effect of this construction is equal to a run of more than 100 ft of ordinary, exterior cooling leg piping.

Steam is delivered into Chamber "A" of the header and circulates from there through the pitched U tubes, carrying its condensation with it into Chamber "B." By partitioning off the lower tube or tubes at the bottom of the Steam Supply Chamber "A" these tubes carry all condensation from Chamber "B" into Drain Chamber "C." In passage of this condensation through these tubes, the air from the fan is rapidly carrying off heat just as it does in the rest of the unit. The result is that these two bottom tubes form an efficient internal cooling leg, integral with the unit.

Thermolier is available in 9 Models. Catalog will be sent on request to Grinnell Company, Inc., 277 West Exchange Street, Providence 1, R. I., or to any branch office in principal cities listed on our page 1118.

CAPACITIES

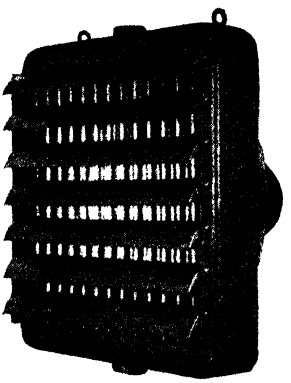
60 F Entering Air Temperature—2 Lb Steam Pressure

Model Nos.	Btu per Hour	Equivalent Direct Radiation	Model Nos.	Btu per Hour	Equivalent Direct Radiation
D21	35,600	148	D57	101,300	422
D31	48,700	203	D66	128,700	536
D37	62,200	259	D71	151,700	632
D44	84,100	350	D91	196,000	817
			D111	275,300	1147

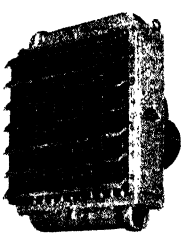
ILG Electric Ventilating Co.

2876 North Crawford Ave., **Chicago 41, Ill.**

Offices in More Than 40 Principal Cities

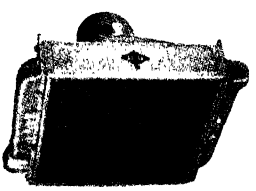


Horizontal Type Unit Heaters—have ILG-built Self-Cooled Motor which counteracts coil heat—never "slow roasts." Graduated, 2-piece, cast iron header gives "balanced" steam distribution. Brass orifice bushings expand tubes uniformly in header plate. Copper fins are *pressed* into round copper tubes for permanent union—no brazing, soldering, or welding. Bottom header "floats" to permit expansion and contraction of coil independent of casing. Tested and Rated according to codes of *I.U.H.A.* and A.S.H.V.E. Ratings certified by *I.U.H.A.*—"One-Name-Plate" Guarantee. Wide range of sizes and capacities.



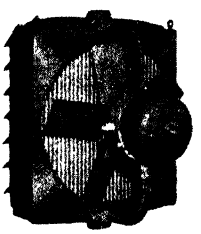
Low-Ceiling Type

For vertical mounting in buildings where headroom is at a premium. Side inlets and outlets at top and bottom assure extremely compact installation.



Vertical Type

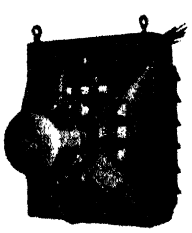
Recommended for installations with extremely high or extremely low ceilings. Air diffusers or deflectors available to direct flow of heater air.



Textile Type

More tubes, no fins—for textile mills and applications where lint or other material normally adheres to fin surfaces and clogs up coil.

ILG Electric Unit Heaters

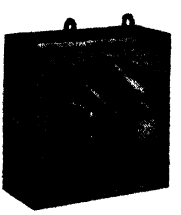


STANDARD TYPE

For instant, clean, safe, dependable heating. Coil is of black heat type which operates below 400 degrees. Protected against excessive temperature rise by patented automatic thermal cut-out and magnetic starter. Sizes 5 to 15 KW.

TYPE "HT"

For installations requiring a small volume of heat. Exceptionally efficient. Suitable for constant duty. Non-overheating black heat type coil with individually interchangeable elements. Sizes 1½ to 4 KW.



For ILG Propeller and Centrifugal Fans, see page 1075

Jaden

MANUFACTURING COMPANY

HASTINGS NEBRASKA

SINCE 1914

New and Improved Self Contained Air Conditioning Units—for use with cold water.

Capacities From 1 Ton to 20 Tons with Comparable Capacities for Heating.

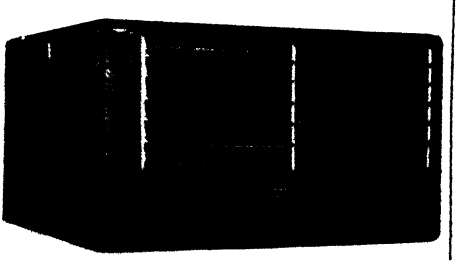
Models for Cooling Include Floor Type for Individual Rooms, Suspended Units and Central Plants for Duct Systems.

Centrifugal Unit Heaters, Package and Utility Type Blowers for Heating and Ventilating

• **Central Plants**—capacities from 3 tons to 24 tons. Air delivery from 1100 cfm to 10,000 cfm. All central plants are assembled in sections to simplify installation. All models available with steam coils for combination heating and cooling.

• **Suspended Models**—capacities from 1 ton to 4 tons. Air delivery 585 cfm to 2200 cfm. Especially adaptable to individual rooms where duct system is undesirable. Completely self-contained with motor, coils, blower and filters housed in sturdy steel cabinet with attractive featherweave finishes.

• **Floor Type Models**—capacities from 1 ton to 3 tons. Designed for use in individual rooms. All models self-contained with motor, blower coil and filters housed in well designed metal cabinets attractively finished or available in base coat for finishing in special colors.



• **Package Blowers**—capacities 1000 cfm to 4000 cfm. All models equipped with filters and available with or without fan controls. Cabinets of extra heavy steel construction with featherweave finish or with base coat for finishing in special colors.

• **Utility Blowers** both single—twin mounted double inlet type—capacity from 800 cfm to 10,000 cfm. Available in any discharge arrangement and with or without motors. Single blowers available in "base type" which includes heavy angle frame for special cabinet construction when necessary.

• **Unit Heaters**—capacities from 76,800 to 155,000 Btu/hr. std. rating, air delivery 1165 cfm to 2100 cfm. Centrifugal type for use with steam or forced circulated hot water. Unusually quiet in operation—highly efficient and easily adaptable to duct installation. Finished in attractive featherweave or base coat for special colors.

WRITE FOR CURRENT SPECIFICATION CATALOG

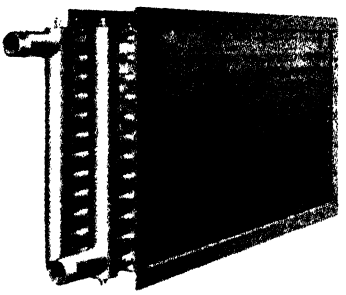
KENNARD Corporation

1819 So. Hanley Rd., **St. Louis 17, Mo.**

Manufacturers of

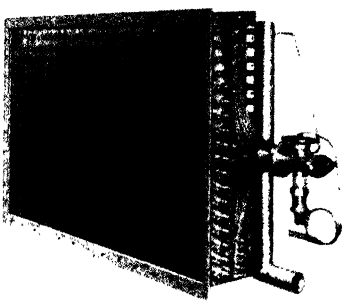
HEAT TRANSFER EQUIPMENT

AIR CONDITIONING BLOWER UNITS—HEATING AND COOLING COILS — EVAPORATIVE CONDENSERS — COOLING TOWERS — INDUSTRIAL COOLERS — UNIT COOLERS — UNIT HEATERS



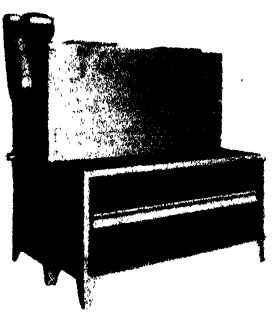
WATER COOLING AND HEATING COILS

For cooling with cold water and for heating with hot water.



DIRECT EXPANSION COILS

For freon. A complete range of sizes to meet all conditions and capacities.

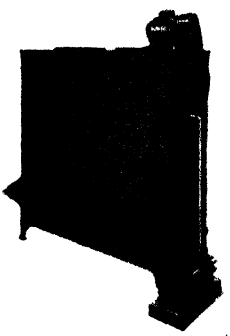


BLOWER UNITS

Ceiling and floor type air-conditioning units. 1 to 50 tons cooling capacity range and 24,000 to 1,125,000 Btu's range in heating. Various arrangements of discharge, filter box and motor drive.

EVAPORATIVE CONDENSERS

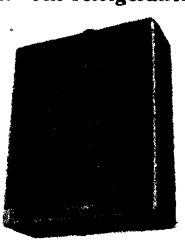
3 to 100 tons. All refrigerants. All prime surface coils. Indoor or outdoor units.



INDUSTRIAL COOLERS

(Not Illustrated)

1000 to 15,500 cfm. Floor type. Coils up to 12 rows in depth. All refrigerants.



UNIT HEATERS

Horizontal propellor fan type. Steam ratings 26,500 to 268,300 Btu's.

McQuay, Inc.

1602 Broadway, N.E., Minneapolis 13, Minn.

MANUFACTURERS OF AIR CONDITIONING EQUIPMENT

Sales Offices in all Principal Cities

- **Air Conditioners**
- **Air Conditioning Coils**
- **Blast Heating Coils**
- **Refrigeration Coils**
- **Unit Heaters**
- **Unit Coolers**

PROVEN McQuay PRODUCTS

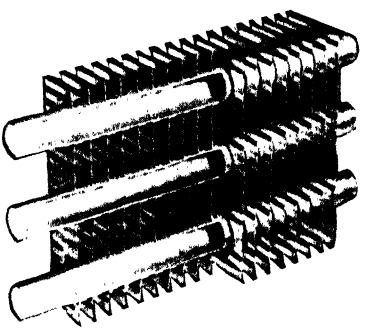
- **Comfort Coolers**
- **Blower Coolers (Suspended & Floor Type)**
- **Ice Cube Makers**
- **Icy-Flo Accumulators**
- **Zeropak Low Temp. Units**

THE EXCLUSIVE McQUAY RIPPLE-FIN RIPPLE-TUBE COIL ASSEMBLY

McQuay hydraulically expanded Ripple-Fin Ripple-Tube Coils effect permanent contact between tubes and the entire surface of the fin collars—that's the advantage of the hydraulic pressure method—to create the lasting mechanical bond without the use of any "low conductivity" bonding material.

This significant advantage is a typical example of how a seemingly small detail in engineering design plays an important part in making superior products.

McQuay construction means higher flexible strength with less air friction and cleaner operation. To provide greater flexibility, all headers are of non-ferrous tubes, elipted to compensate for any unequal expansions and contractions.

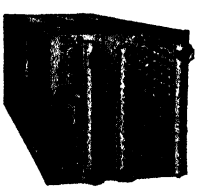


RIPPLE-FIN COIL

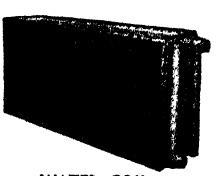
All secondary surface is of the aluminum ripple-fin continuous plate type, to give extra strength, and to provide heat transfer surface that remains clean for a longer period, thereby giving greater efficiency; all tubes are electro-tin plated for further protection and longer life.

The new standardized design provides 11 header sizes and 19 tube lengths, plus other intermediate header sizes and many other tube lengths. McQuay thus provides greater flexibility for sizing jobs.

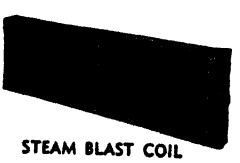
This careful attention to detail makes McQuay performance possible and establishes their preference among users. McQuay coils are available in a wider variety of styles and sizes, both standard and special coils for steam, hot water, cold water, brine, direct expansion and other applications.



COMBINATION COOLING COIL



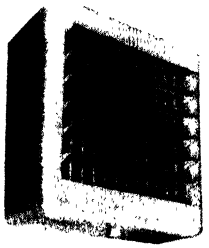
WATER COIL



STEAM BLAST COIL

MORE THAN 1,000,000 COIL TYPES AND SIZES

McQUAY manufactures a complete line of Standard Coils for the Industry.
Coils for Heating—1 to 10 rows deep using low or high pressure steam or hot water.
Jet-Tube (Non-Freeze steam inner tube) type coils 1 and 2 rows deep.
Cleanable Tube—(Removable plug) type coils 1 to 12 rows deep.
Water Coils for Cooling—1 to 12 rows deep.
Direct Expansion Coils—for cooling 1 to 10 rows deep.
Refrigeration Coils—all types and sizes.
Special Coils—of various materials furnished on order for special applications.



HORIZONTAL UNIT HEATER

HORIZONTAL UNIT HEATERS

Restyled in 1947 to provide up to the minute eye appeal. This renewed line of 12 sizes completely covers the range from 23,000 to 300,000 Btu. All sizes carried in stock. Write for Catalog 320.

DOWN FLOW UNIT HEATERS

Available with various air discharge arrangements for low, medium, or high suspension, these unit heaters fill a need on almost every job. Carried in stock in 16 sizes from 32,000 to 500,000 Btu. Write for catalog 746.

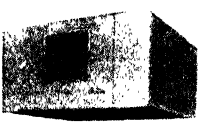
DOWN FLOW UNIT HEATER

BLOWER TYPE UNIT HEATERS

Made in 11 basic sizes covering the entire range from 1500 cfm and 125,000 Btu to 16,000 cfm and 1,136,000 Btu. Provision for handling external static; various outlet diffusers; also available with face and bypass dampers.

For long life, efficiency, and for eye appeal specify McQuay Unit Heaters.

BLOWER TYPE UNIT HEATER



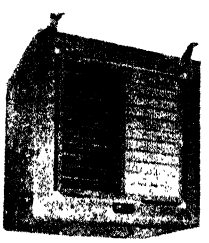
AIR CONDITIONER (YEAR-ROUND)

COMFORT COOLERS
For Small Commercial Applications

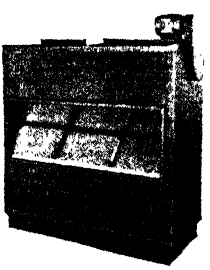
Made in two types—one for use with water or brine; another for Freon or methyl chloride. Five sizes (1, 1½, 2, 3, and 5 ton models) in each type—all with variable-speed motors. Write for catalog 81A.

SMALL AIR CONDITIONERS
Cold Water and Freon Types For Small Commercial Applications

Choice of recirculation of indoor air, entire intake of outside air, or a combination of both. Cold water or brine used in one type; Freon or methyl chloride in another. Modern "sound isolated" construction assures quiet operation. 2, 3, 5, and 7½ ton sizes. Write for Catalog 83A.



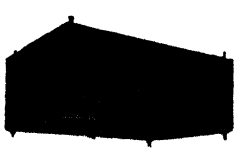
COMFORT COOLER



AIR CONDITIONER (YEAR-ROUND)

LARGE CENTRAL SYSTEM AIR CONDITIONERS
For Large Industrial and Commercial Applications

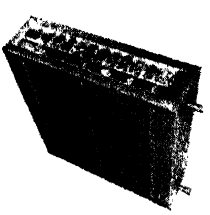
Suspended and floor types, cools, dehumidifies, filters, and circulates air in summer, heats, humidifies, filters and circulates air in winter. Extreme flexibility and accessibility "built-in." Cooling capacities from 5 to 50 tons in both Suspended and Floor Type. Write for catalog 85.



AIR CONDITIONER (YEAR-ROUND)

McQUAY
Icy-Flo Accumulators

The new practical "Storage-Battery" for refrigeration effect is now available for handling heavy loads of short duration. Ideal for churches, lodges, mortuaries, noon cafeterias, and many industrial applications. Write for catalog 105.



ACCUMULATOR

Modine Manufacturing Company

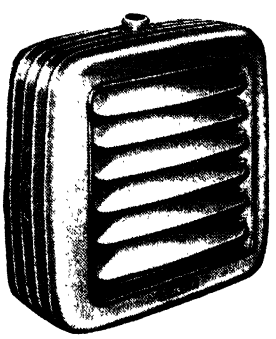
Heating and Air Conditioning Division

General Offices: 1500 Dekoven Ave., **Racine, Wis.**

Factories at Racine, Wis. and La Porte, Ind.

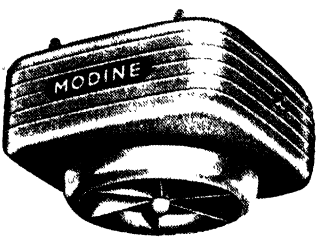
Branches in all Principal Cities

NEW MODINE UNIT HEATER LINE



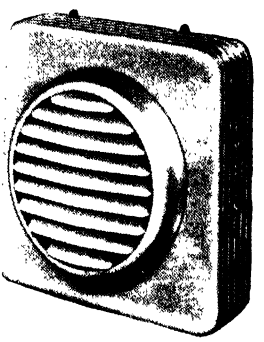
Horizontal Type

23 Models—for general industrial and commercial applications. Patented Modine center tappings permit direct-from-pipe-line suspension.



Vertical Type

16 Models—designed for overhead installation, up near ceilings of high bays to clear plant production equipment, or at low levels as in stores and offices.



New Power-Throw

8 Models—for specialized industrial applications. A new type of draw-through horizontal delivery unit heater with powerful, scouring jet action.

Three Distinct Types—47 Basic Capacities for Industrial and Commercial Unit Heater Applications

Modine's beautiful, new, integrated line of unit heaters offers new versatility in steam and hot water unit heater application. The three coordinated types may be used individually, or, where requirements indicate, in combination with each other. Thus, it is possible to meet varying heat, air delivery, mounting height, and location demands with the combined action of different unit heaters.

Condensers: Pure copper or copper alloy from inlet to outlet for maximum resistance to internal and external corrosion. Pure copper fins are metallically bonded to round, seamless, heavy-guage red brass tubes for permanent contact and to insure uninterrupted heat conduction from primary to secondary surface. Modine-patented expansion bend permits tubes to expand or contract individually as temperature requires. All steam and condensate carrying passages are brazed into an integral pressure-resisting unit.

Bonderized Casing: Attractive beige-gray casing with chrome trim protected from rust by Modine Parker Bonderizing.

Quiet Operation: Scientifically sound-silenced for quiet performance. Casing interiors are acoustically-insulated to muffle noises from within. Velocity generator eliminates air rush "peaks," subdues external air-rush noise.

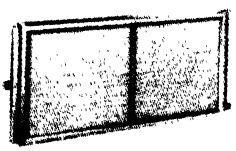
Efficient Motors: Nationally known makes of continuous-duty, totally enclosed fan type. Rubber mounted to prevent vibration noise from being transmitted to casings.

Safety Fan Guard: Staunch, steel safeguard protects against danger of unshielded fan.

WIDE NEW LINE OF HEATING COILS

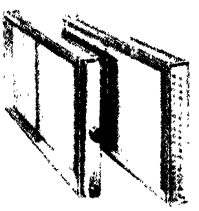
The new Modine line of Heating Coils now gives you over 1,236 coils to choose from in matching your specific performance and size requirements for heat transfer surface. But that's not all! Newly engineered and designed, Modine coils permit use of smaller duct sizes for increased convenience and efficiency! Available in four major types:

1. Standard Coil



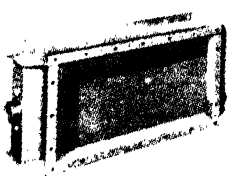
For all normal heating, ventilating, air conditioning and drying applications where steam is heating medium. 595 sizes and models.

2. Non-Freeze Coil



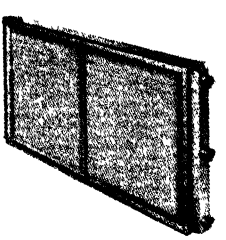
Incorporates steam distributing tubes for resistance to freezing and uniform face temperatures. Use where temperature is controlled by modulating steam supply . . . even with 32 deg F entering air. 510 sizes and models.

3. Booster Coil



For use where small volumes of air are handled. Ideal for controlling temperatures in branch ducts. Face areas as small as ½ square foot in standard and non-freeze types. 46 sizes and models.

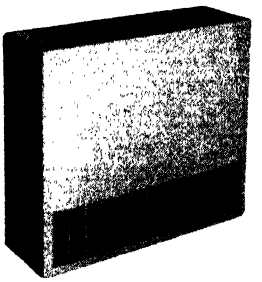
4. Hot Water Coil



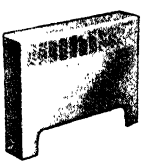
A serpentine coil for use on hot water. Exclusive Modine feature permits counterflow installation regardless of air flow direction with complete air venting and drainage provision. 85 sizes and models.

CABINET UNIT HEATERS

Designed for heating offices, lobbies, corridors, etc. . . . wherever quick, positive distribution of heat combined with quiet operation and gentle air movement are desirable. Has considerably greater heat output than convector of equivalent size. Employs copper heating coil for use on steam or hot water system. Mounted on wall or ceiling. Capacities: 105 EDR and 310 and 450 EDR.



CONVECTOR RADIATION



Floor Cabinet Type

Built to meet modern residential, institutional, and commercial heating requirements, Modine convectors operate on the principle of *natural convection*. Cooler, heavier air is drawn in through the enclosure's bottom opening; comes in contact with copper heating unit that carries steam or hot water. As air is heated, it rises; is then circulated out into room through grille at top of enclosure.

Concealed copper heating unit combines compactness with high heat capacity—to give room added floor space as well as fast, even heating. Use of copper makes the heating unit almost instantly responsive to automatic control.

Enclosures are streamlined for simplicity and harmonize readily with any type of interior. Parker-Bonderized before being prime painted, the enclosures are less vulnerable to the formation and spread of rust.

Manually installed enclosure fronts can be installed in 30 seconds without tools. Easy removal of fronts assures convenience in cleaning and gives ready access to the heating unit.

Available in recessed and cabinet types.

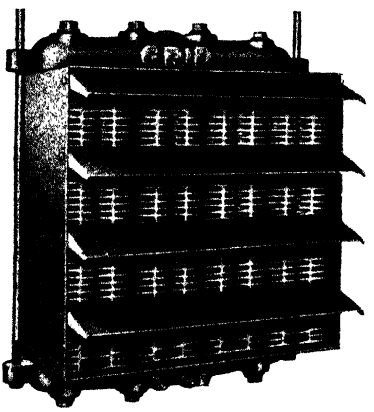
T. M. REG. U. S. PAT. OFF.

D. J. Murray Manufacturing Co.

Wausau, Wisconsin

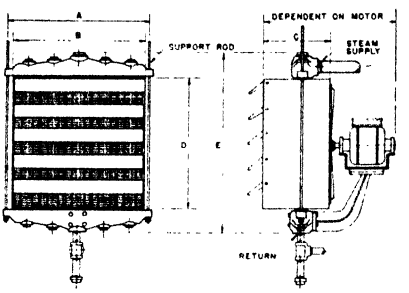
Offices in Principal Cities

MANUFACTURERS OF THE GRID UNIT AND GRID BLAST COILS



One piece construction "fin" heating sections of high test cast iron—no soldered, brazed, welded or expanded connections. Patented.

Designed and tested to operate with steam or hot water systems—for steam pressures from 2 lbs to 250 lbs. Engineered along the same lines as the standard GRID Unit which had aluminum heating sections and has been on the market since 1929.



Overall dimensions for installation of Cast Iron GRID Unit Heater

CI (CAST IRON) SERIES GRID UNIT HEATER DATA

Model No.	Dimensions					Motor		Vol. Fan CFM	Capacities 5 PSI Steam 60° F Air		Pipe Size		Support Rod Dia.	Approx. Ship. Weight Lbs.
	A	B	C	D	E	HP	RPM		Btu/Hr	Final Temp. °F	Supply	Return		
CI-1000	11 5/8	10 1/2	12 1/4	10 7/16	17 1/4	1/25	1550	572	29,080	106	1 1/4	1 1/4	1/2	150
CI-1200	14 1/8	13 1/8	12 1/4	13 5/16	21 1/2	1/15	1550	798	45,450	112	1 1/4	1 1/4	1/2	210
CI-1500	17 1/2	15 3/8	11 1/2	16	23 7/8	1/8	1750	1500	76,500	107	1 1/2	1 1/4	1/2	280
CI-1520	17 1/2	15 3/8	11 1/2	21	28 3/8	1/8	1750	1700	101,500	114	1 1/2	1 1/4	1/2	390
CI-2000	22 1/8	20 9/16	11 7/8	21 1/16	28 3/8	1/6	1150	2600	143,000	110	2	1 1/4	1/2	490
CI-2025	22 1/8	20 9/16	11 7/8	25 7/8	35 1/4	1/6	1150	2875	173,640	115	2	1 1/4	1/2	520
CI-2500	27 1/2	25 7/8	13	25 7/8	35 1/4	1/2	1150	4350	224,000	107	2	1 1/4	5/8	700
CI-2504	27 1/2	25 7/8	13	25 7/8	35 1/4	1/4	1150	3300	206,000	117	2	1 1/4	5/8	660
CI-2530	27 1/2	25 7/8	13	31	40 1/2	1/2	1150	4650	275,800	114	2	1 1/4	5/8	900
CI-3000	32 5/8	31	13	31	40 1/2	1/2	850	6300	332,000	108	2 1/2	1 1/4	5/8	1020
CI-3000	32 5/8	31	13	31	40 1/2	1 1/2	1150	8000	380,000	103	2 1/2	1 1/4	5/8	1070

NO ELECTROLYSIS TO CAUSE CORROSION

Low maintenance expense.
More air changes per hour.
Positive "directed" heat.
No leaks—no breakdowns.
Lower outlet temperature.
Larger air volume.
No soldered, brazed or expanded joints.
Open design that keeps units clean.

Send for complete catalog information

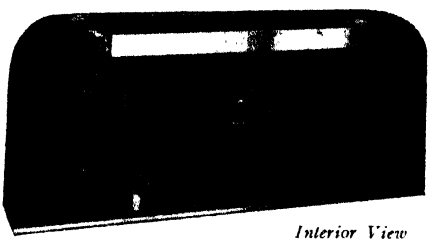
Send for information on Blast coils and radiation.

John J. Nesbitt, Inc.

Philadelphia 36, Pa.

Manufacturers of

THE NESBITT SYNCRETIZER Heating and Ventilating Unit, and
THE NESBITT PACKAGE, schoolroom ensemble consisting of the Syncretizer, Convector and storage units, sold by John J. Nesbitt, Inc., and American Blower Corporation;
NESBITT HEATING SURFACE with Dual Steam-distributing Tubes,
NESBITT SERIES H HEATING SURFACE, and
NESBITT SERIES W COOLING SURFACE,
sold by leading manufacturers of fan-system apparatus;
NESBITT CONVECTORS, sold by plumbing and heating wholesalers;
WEBSTER-NESBITT UNIT HEATERS (See page 1229),
distributed in U. S. A. by Warren Webster & Company.



Interior View

NESBITT SYNCRETIZER—Series 400

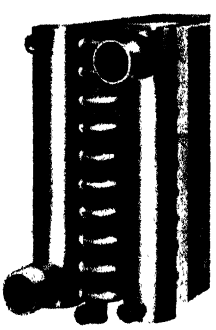
For heating and ventilating schoolrooms, offices, etc., where the continuous introduction of outdoor air is desired. For engineering data, get Publication 225-2; for "The Story of Syncretized Air," Publication 231-2. For data on The Nesbitt Package, schoolroom ensemble consisting of the Syncretizer, Convector, and storage units, get Publication 249.

Nesbitt Series B Thermovent

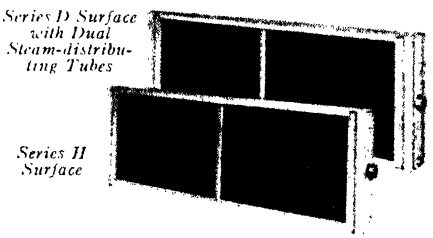
For heating and ventilating auditoriums, gymnasiums, assembly halls, and similar gathering places. Publication No. 227-2.

NESBITT COOLING SURFACE
Series W Surface

For air cooling and cooling and dehumidifying (with cold water) or air heating (with hot water). Constructed of copper tubes and plate-type aluminum fins. Available in either continuous or cleanable tube type, in single sections having one to eight rows of tubes deep, in three fin spacings, in eleven fin widths, and up to sixteen finned tube lengths. Sturdy galvanized casings. For engineering data send for Publication 246.



Uncased Surface Showing Drain Header



NESBITT HEATING SURFACES
Series D Surface
With Dual Steam-distributing Tubes

Copper tube and aluminum fin surface for low-pressure applications. Adapted to close, continuous automatic control with modulating steam valves. Steam-distributing tubes within condensing tubes carry the steam equally to the full section assuring *uniform* discharge temperatures even under throttled steam supply; eliminating temperature stratification; preventing tube freezing without preheaters.

Series D Surface is available in two types, Type DS and Type DD. Steam is supplied from one end of the surface in Type DS, which is recommended for lengths up to six feet. Steam is supplied from both ends of Type DD, which is recommended for lengths over six feet.

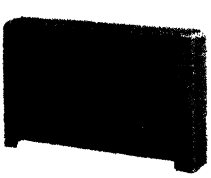
Cased or uncased units of many sizes and capacities. For engineering data, send for Publication No. 247-1.

Nesbitt Series H Heating Surface

A lightweight, enduring, highly efficient blast-coil heating surface designed for steam pressures up to 200 lb. gauge. Send for Publication 248.

NESBITT CONVECTORS

Designed for steam or hot water heating of residences, apartments, offices, etc. Send for Publication 252. Available in 20 stock sizes.



THE HERMAN NELSON CORPORATION

General Offices and Factories at Moline, Illinois

Branch Offices and Product-Application Engineers in the Following Cities:

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BOSTON, MASS.	DULUTH, MINN.	MINNEAPOLIS, MINN.	RICHMOND, VA.
BUFFALO, N. Y.	EL PASO, TEX.	MISSOULA, MONT.	SAGINAW, MICH.
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CHICAGO, ILL.	INDIANAPOLIS, IND.	NEW ORLEANS, LA.	SAN ANTONIO, TEX.
CINCINNATI, O.	JACKSON, MISS.	NEW YORK, N. Y.	SAN FRANCISCO, CALIF.
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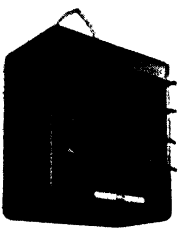
DALLAS, TEX.	LOUISVILLE, KY.	PHILADELPHIA, PA.	SYRACUSE, N. Y.
DENVER, COLO.	MEMPHIS, TENN.	PHOENIX, ARIZ.	WASHINGTON, D. C.

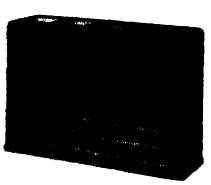


HERMAN NELSON HORIZONTAL SHAFT PROPELLER-FAN TYPE UNIT HEATERS

Designed for ceiling suspension, these unit heaters project warm air downward in an angular direction. Copper heating element for use with steam or hot water, incorporates patented stay tube which maintains proper relationship between headers without increasing strain on loops thus prolonging life of unit. A wide variety of models, sizes and arrangements.

HERMAN NELSON VERTICAL SHAFT PROPELLER-FAN TYPE UNIT HEATERS

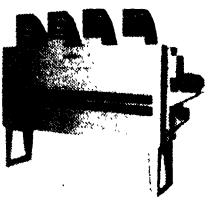
For high ceiling installations. Discharge air vertically downward, or at an angle to vertical in various directions. Long life copper heating element for use with steam or hot water incorporates patented stay tube. Units available with either high or low velocity discharge, each with a wide range of capacities.



HERMAN NELSON DE LUXE UNIT HEATERS

Efficient, economical, compact, quiet and attractive, these Unit Heaters provide the ideal method for heating offices, showrooms, corridors, markets, stores, etc. Copper heating element incorporates patented stay tube. Units may be placed on floor, wall or suspended from ceiling. Eighteen models, sizes and arrangements.

HERMAN NELSON CENTRIFUGAL FAN TYPE UNIT HEATERS

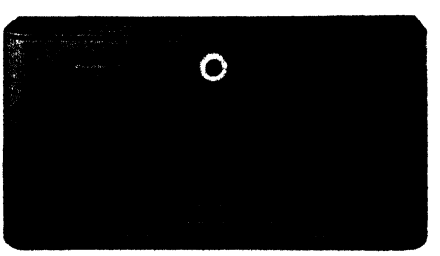


For efficient heating of large areas. Can be supplied with by-pass damper for introduction of indoor and outdoor air. Design of copper heating element assures durability and contributes to high velocity discharge. For floor, wall, ceiling or inverted wall mounting.

HERMAN NELSON UNIT VENTILATORS

Maintain desired air conditions for room or auditorium areas where large groups of people gather. Copper heating element for use with steam or hot water is sturdily constructed for long life and designed for greatest heating efficiency.

Exclusive "draw-through" design prevents unhealthful drafts and eliminates unnecessary overheating. Locating motor in end compartment provides additional space for fan assembly and use of larger fans running at slower tip speeds.



Herman Nelson Unit Heaters and Unit Ventilators are tested and rated in accordance with the Standard Test Code adopted jointly by the *Industrial Unit Heater Association* and the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS.

THE HERMAN NELSON CORPORATION

General Offices and Factories at Moline, Illinois

HERMAN NELSON DIRECT DRIVE PROPELLER FANS

Provide most economical form of quality ventilation obtainable for industrial buildings of all types. 7 standard sizes available with wheel diameters from from 14 to 36 in. and capacities from 655 to 12,400 cfm. There are 7 high powered models to operate against static resistance of ⅜ in., with wheel diameters from 14 to 36 in. and capacities from 1200 to 14,600 cfm. Can be obtained in acid and explosion resisting models. Also three models especially adapted to small store and office applications.

HERMAN NELSON BELT DRIVE PROPELLER FANS

For public and commercial building installations where slow speed, quiet operation are required. Twelve sizes of the standard model with wheel diameters from 24 in. to 54 in. Also six sizes of the High Powered model with the same wheel diameters. Capacities: 5650 to 36,150 cfm. Due to quiet operation of Herman Nelson Belt Drive Propeller Fans, use of two speed motor is unnecessary.

HERMAN NELSON DIRECT DRIVE UNIT BLOWERS

Designed for many applications, such as fume hoods, toilet ventilation, chemical laboratories, industrial processing and drying problems. Compact, direct connected, motor driven units have universal discharge and mount on floor, wall or ceiling. Available in four sizes with 9 speed combinations. Wheel diameters from 6½ in. to 11 in. and capacities from 360 to 2265 cfm.

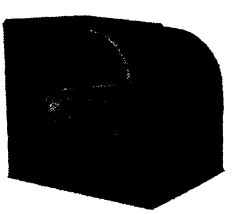
HERMAN NELSON BELT DRIVE UNIT BLOWERS

Fully self-contained unit including motor, drives and housing; forwardly curved or backwardly curved blade wheels available; adjustable motor pedestal with vibration dampers; universal discharge; nine sizes with 70 drive combinations. Available with any rotation and discharge. Wheel diameters from 11 in. to 30 in. and capacities from 980 to 16,892 cfm.

HERMAN NELSON TYPE "H" AND TYPE "HB" CENTRIFUGAL FANS

Especially suited for heating, air conditioning and ventilating systems. Type "H" has forwardly curved blade wheels. Type "HB" has backwardly curved blade wheels incorporating non-overloading power characteristics. Seventeen wheel diameters from 12¼ to 73 in.; single or double width; Class I or II construction; and any speed or discharge requirement.

Type HB



Type H

The Complete Line of Herman Nelson Propeller Fans and Blowers is tested and rated in accordance with the Standard Test Code adopted jointly by the *National Association of Fan Manufacturers* and the AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS.

The TRANE Company

2021 Cameron Avenue, **La Crosse, Wisconsin**

COMPLETE LINE OF HEATING, COOLING, AIR CONDITIONING AND AIR HANDLING EQUIPMENT

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A COMPLETE LINE

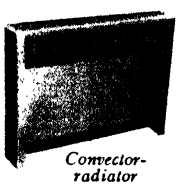
The Trane Company fabricates a complete line of heating, cooling, air conditioning and air handling equipment. Long years of experience with practical knowledge gained from close field contact, have developed products for every requirement.

Trane Systems—So comprehensive is the Trane Line that any number of complete heating and air conditioning systems can be designed in which all the major parts are made by Trane. Examples: Trane Custom-Air System of Air Conditioning for multiple-room buildings; central and unit systems of air conditioning for comfort and processes; steam and hot water heating systems. Products used in these systems are designed and made together for use together. Undivided responsibility.

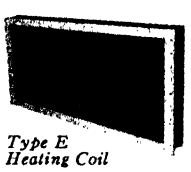
Trane Convector-radiator—The modern successor to the old-fashioned radiator, the Trane Convector-radiator is a compact, light-weight, easy-to-install unit. Available for either steam or hot water heating system. It combines attractive appearance with long life and economical service.

Currently easier to obtain and install than ever, new Type A Units are available from stock throughout the nation.

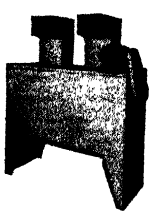
Trane Coils—There are Trane Extended Surface Coils for every heating or cooling, comfort or process application, in all types and sizes. Types include coils for steam, hot water or booster heating, direct expansion or water cooling.



Convector-radiator



Type E Heating Coil



Torridor Unit Heater

Projection Heater

Trane Blower Type Unit Heaters—Better known as Torridors, Trane Blower Type Unit Heaters are available for large space or duct work applications. Ideal for heating large spaces, exposed areas requiring a blanket of heat, and for process applications.

Trane Projection Heaters—A Trane development, the Projection Heater taps the usually wasted heat reservoir at the ceiling bringing it down where it is needed. Installed at 8 to 50 ft. heights, it projects warm air to the floor in a circular, vertical air stream. Ideal for low or high pressure systems in factories, warehouses, etc.

Trane Propeller Unit Heaters—Featuring a quiet operating, wide-bladed fan that pushes rather than bats the heated air through the coil, the Trane Propeller Unit Heater incorporates many unusual features, including adjustable louvers or grilled outlets directing heated air to the floor line, rugged motor supports, attractive appearance.

Trane Air Conditioning Manual—Trane offers the engineering profession a straight-forward and unbiased textbook covering the fundamentals of air conditioning, in a new enlarged edition. The Manual not only shows how to design every type of air conditioning system, but also clarifies underlying principles, enabling both student and engineer to reason out their own problems. Price—$5.00.

Trane Refrigeration Manual published primarily as an aid in understanding and correcting installation and service problems. Price —$1.50.

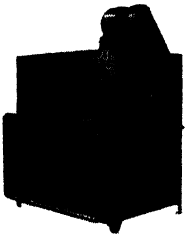
Trane Climate Changers —Trane Climate Changer, a unit type air conditioner, is designed for summer, winter, or year 'round air conditioning, commercial and industrial application, comfort or process installations. Available in various coil combinations with or without humidification equipment.

Trane Refrigeration Equipment — Outstanding in the refrigeration field is the Trane Turbo-Vacuum Compressor, a completely self-contained hermetically sealed centrifugal type water chiller, available in 50, 70, 100 and 200 ton sizes. Year 'round efficiency in constant operation with a minimum of maintenance is assured by the scientific simplicity of this machine.

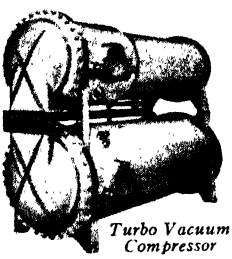
Trane also furnishes a complete line of Reciprocating Compressor and Condensing Units with capacities ranging from 3 to 100 tons. Also available are Trane Self-contained Air Conditioners for shop and office spaces.

Trane Roof Ventilators —The Trane Roof Ventilator can be used wherever an effective roof ventilator is required. This unit is available for either exhaust or supply purposes.

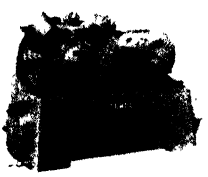
Trane Centrifugal Fans —Recommended for all types of heating, cooling, and air handling applications. In direct or belt-driven units, single or double widths, and all standard discharges in both backward and forward curved blade construction. Capacities 200 to 330,000 cfm.



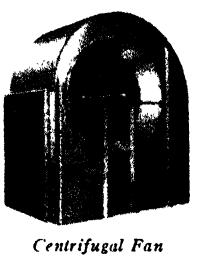
Climate Changer



Turbo Vacuum Compressor



Reciprocating Compressor



Centrifugal Fan

Lifetime Valve

Thermostatic Radiator Trap

Trane Steam Heating Specialties—There are over fifty valves, traps, vents, strainers, all allied specialties in the Trane Line. Among them are the famous Trane Hermetic Valve with the Lifetime Diaphragm that absolutely prevents steam leakage around the stem and the Thermostatic Radiator Trap which when used together provide an ideal combination for convectors and radiators.

Trane Hot Water Heating Specialties — Included among Trane Hot Water Heating Specialties are the Trane Circulator, Flo Valves, and Fittings. They combine with Trane Convectors or Unit Heaters to provide an ideal Warm Water Heating System for a great variety of applications.

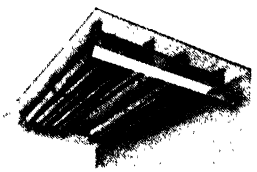
Other Trane Equipment —The complete Trane Line also includes—1. Trane Unit Ventilators for schoolroom air conditioning; 2. Trane Condensation and Centrifugal Pumps for a large variety of uses; 3. Trane Dry Type Water Chillers; 4. Trane Evaporative Condensers to condense refrigerants in the air conditioning system with a minimum use of water; 5. Trane Cooling Towers; 6. Trane Force-Flo Heater for quiet heat and neat appearance; 7. Trane Railroad and Bus Air Conditioning Equipment of all kinds; 8. Trane Shell and Tube Heat Exchangers for cooling and heating vapors or liquids in a closed system; 9. Evaporative Coolers for cooling fluids in a closed system; 10. Transformer Oil Coolers; 11. Air Washers.

Write today for Trane Condensed Catalog PB290 which describes completely all of the products listed here as well as providing sufficient data for their selection.

Refrigeration Economics Co., Inc.

1231 Tuscarawas St. E., **Canton 2, Ohio**

RECOY PRODUCTS

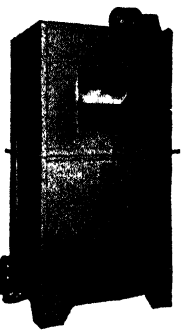


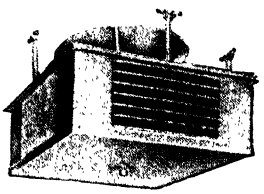
C. T. COILS

Continuous-tube down-draft fin-coils are still unsurpassed for meat coolers. Others available for practically any application.

EVAPORATIVE CONDENSERS

Evaporative condensers from 2 to 100 tons. Brine spray cooling to 25 tons.



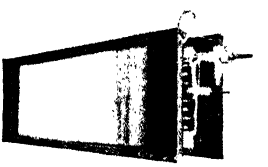


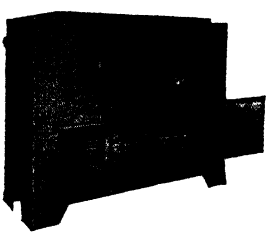
CEILING DIFFUSER

Ceiling diffusers distribute the cooled air across the ceiling, so the blast does not strike the products stored or occupants.

C. F. COILS

Continuous fin coils for unit coolers, blast heaters, air conditioning and condensers.



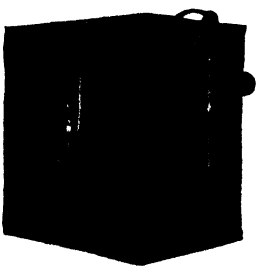


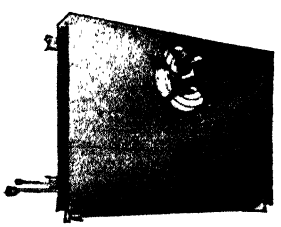
AIR CONDITIONING

Air conditioning units of ceiling or floor type in all capacities, for cooling, heating, or both.

COOLANT COOLING

Coolant coolers from 1 to 20 tons are a necessity for modern production of accurate machine parts.



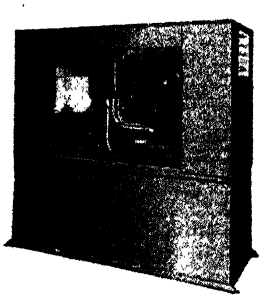


WALL UNITS

Recoy "All Seasons" wall units provide means of deflecting the cold air down along the wall or out horizontally into the room, thus providing proper air circulation for "All Seasons."

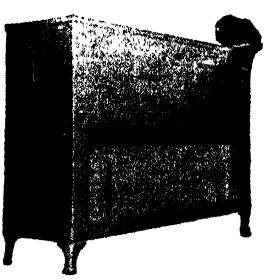
SHELL CONDENSER

Shell and tube, also shell and fin coil condensers. Both types have tubes arranged for cleaning with tube cleaner.



WATER COOLING

Self contained complete ice water and brine coolers complete with high and low sides, circulating pumps, controls, and insulation. 1½ to 50 hp.



FLOOR UNITS

Floor units with cooling surface exposed to view have a definite advantage over those with coils hidden. Design permits water defrosting.

Factories:
NEWARK, N. J.

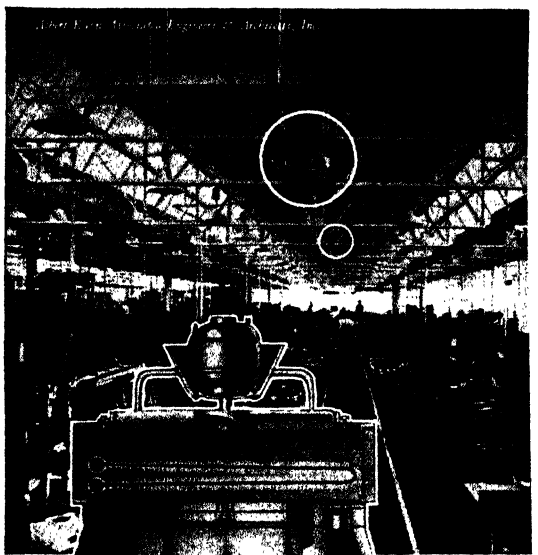
L. J. Wing Mfg. Co.

59 Seventh Avenue, **New York 11, N. Y.**

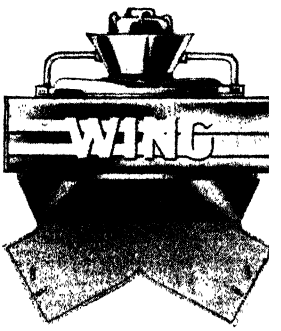
Canadian Factory:
MONTREAL

Branch Offices in **Principal Cities**

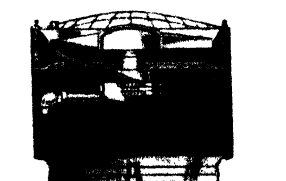
WING REVOLVING UNIT HEATERS



Cross-Section through heater showing motor, fan, heating section and revolving discharge outlet. Design No. 8.



Motor Driven Heater



(Right) Cross-section of Turbine Heater showing fan, turbine, heater section and revolving discharge outlet. Design No. 5.

Turbine Driven Heater

This innovation in the method of distributing heat produces a sensation in heating comfort never before attained—a sensation of fresh, live, invigorating air.

The fact that the outlets revolve assures uniform and thorough distribution of comfortably warmed air throughout the entire working area, without drafts, hot spots or cold spots.

Such an unprecedented high efficiency in distributing heat is the result of 25 years of constant study by Wing engineers to improve on the Floodlight System of heating pioneered by WING in 1921. This method projects the heated air vertically downward by means of light-weight, ceiling-suspended unit heaters.

It has needed only this latest refinement of slowly revolving discharge outlets to bring that method to perfection.

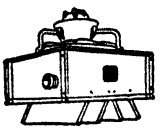
The WING Revolving Discharge type supplements the WING line of standard fixed discharge outlets, illustrated and described on the following page.
Bulletin HR-5.

The latest type of WING Unit Heater—with Revolving Discharge Outlets—is the WING TURBINE DRIVEN UNIT HEATER in which the steam used to drive the fan (instead of an electric motor) also supplies the heater section.

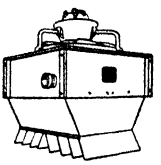
The Wing Turbine Revolving Unit Heater employs the new Wing Allsteel Steam Turbine which operates at *any* pressure. Condensate from the heater is never at a temperature exceeding 170 F. The entire unit is so designed that there is no back pressure on the turbine, assuring against leaks without the use of power-absorbing, troublesome packing. This also eliminates the need for traps and extra piping.

As in the motor-driven heater, the revolving discharge outlet distributes the heat continuously in constantly changing directions.

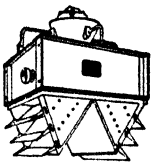
Type "HC" Fixed Discharge Design No. 7



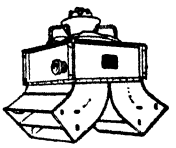
Design No. 1



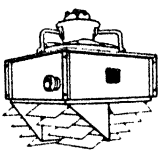
Design No. 1-HV



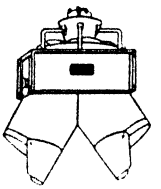
Design No. 3



Design No. 4



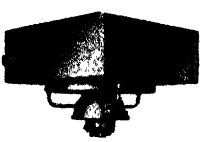
Design No. 6



Design No. 8

WING FIXED DISCHARGE UNIT HEATERS

The first light-weight, ceiling-suspended, unit heater. Eight different designs of outlets meet the requirements of every type, size and height of building or occupancy. Located near ceiling or roof, the accumulation of hot air in the upper spaces, with the accompanying costly waste of heat, is prevented. They project the air, comfortably warmed, downward to the working area. *Bulletin HR-5.*



DOOR HEATERS GARAGE HEATERS

WING developed this vertical cone-discharge heater in 1921 and today it is still applicable for heating the inrush of cold air at large doorways and for garage heating. Often cuts heating costs in half. *Bulletin HR-5.*

FOR LOW CEILINGS

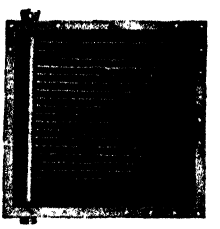
Type "LC"

In this type of WING Unit Heater the position of fan and motor are reversed to meet conditions of ceiling or roof height, form and shape of building, coverage, etc. *Bulletin HR-5.*

WING UTILITY UNIT HEATERS

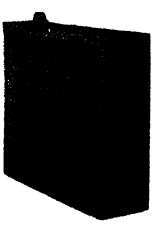
A lightweight suspended unit heater for delivering heated air in one general direction. Has the same powerful fan and rugged heating element as WING Featherweight Unit Heaters. This is the latest refinement of the original horizontal lightweight heater which was developed by WING. *Bulletin U-6.*

FEATHERFIN HEATER SECTIONS



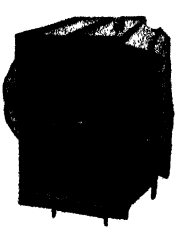
For heating or cooling air for any purpose by steam, hot or cold water or refrigerant. The heating element is extremely light and, for equal heat transfer, offers little resistance to air flow. Available for any desired final air temperature. *Bulletin HS-3.*

VARIABLE TEMPERATURE SECTIONS



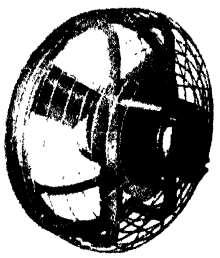
Invaluable in supplying fresh air for space heating or process work. Close control of the delivered air temperature is obtained without danger of freezing. Manual or automatic control. *Bulletin HS-3.*

WING INDUSTRIAL FOG ELIMINATORS



Eliminate fog, odor and fumes in dyeing, bleaching and finishing plants, creameries, pasteurizing, bottling, canning and packing plants, chemical works, paper mills, steel pickling plants, etc. No ducts are required. *Bulletin FE-12.*

WINGFOIL SAFETY VENTILATING FANS



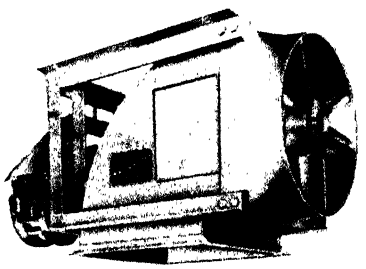
An axial flow fan that will deliver air against static pressure, quietly and efficiently.

Moves the air forward in straight lines with minimum eddy. Capacities to 100,000 cfm. *Bulletin F-9.*

WING FEATHERFIN PROCESS HEATING UNITS

For manufacturing processes such as drying, aging, etc., requiring the recirculation of the heated air. Motor or turbine located outside air current. *Bulletin P-2.*

WINGFOIL DUCT FANS



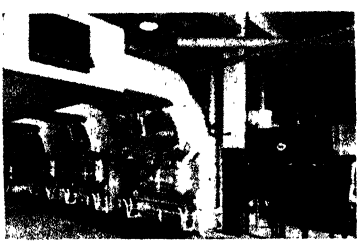
For economically moving air wherever ducts are used. It combines the efficient WINGFOIL AXIAL FLOW Fan with a housing which places the motor entirely outside the air duct. Motor and drive remain cool and clean and are easily accessible.

The powerful WINGFOIL Fan delivers high air volume with low power consumption against any pressures for which duct systems should be designed. V-belt or direct drive.

Light, compact and easy to install. *Bulletin F-9.*

WING SYSTEM OF CONTROLLED COMBUSTION

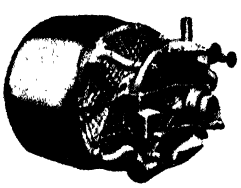
For low pressure heating boilers and small power boilers. Increases capacity and permits use of lowest cost fuel. Includes Type EM Blower equipped with fully enclosed dustproof motor with speed regulating rheostat and automatic control. Eliminates necessity of frequent firing, allowing intervals as great as 24 hours even in zero weather. *Bulletin M-96.*



Installation of Wing System of Controlled Combustion in a large school

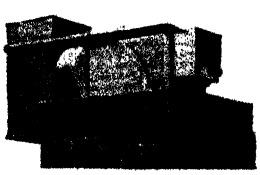
WING TURBINE-DRIVEN BLOWERS

Applied to hand, stoker, oil or pulverized fuel fired boilers, increase boiler capacity, maintain constant steam pressure and permit complete combustion of low-cost fuels. The exhaust steam, free from oil, can be used for heating or processes. *Bulletin T-98.*



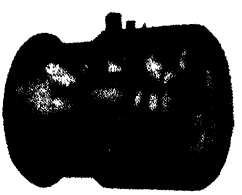
WING DRAFT INDUCERS

Installed in breeching or flue, or on chimney top; provide positive, exact draft regardless of weather conditions or inadequate chimney or breeching construction. Suitable for coal, oil, or gas-fired boilers; industrial furnaces and kilns. *Bulletin I-10.*



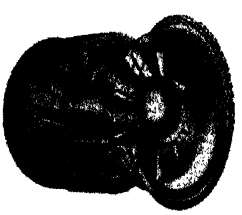
Chimney-Top Installation

WING MOTOR-DRIVEN BLOWERS



Type COM

Type COM for static pressures over 5 in. and volumes up to 35,000 cfm. Type EMD for moderate static pressures up to 5 in. Both blowers have fully-enclosed dustproof constant speed motor and built-in adjustable control vanes. Type COM has double-staged axial flow fan; Type EMD, single stage fan. Extremely compact; discharge can be vertical, horizontal or inclined. *Bulletin SW-1.*



Type EMD

Young Radiator Co.

Dept. 178, **Racine, Wis.**

Sales and Engineering Offices in Principal Cities

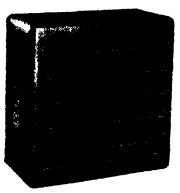
YOUNG

HEAT TRANSFER PRODUCTS

Oil Coolers • Gas, Gasoline, Diesel Engine Cooling Radiators • Heat Exchangers • Intercoolers • Engine Jacket Water Coolers • Gas Coolers • Unit Heaters • Convectors • Condensers • Evaporators • Air Conditioning Units • Heating Coils • Cooling Coils • Complete Line of Aircraft Heat Transfer Equipment.

"STREAMAIRE" UNITS

"Streamaire" units are a development of Young's quarter century of experience in building heat transfer products. Personalized, "on-the-job" engineering service by field men—backed by modern research and manufacturing facilities—assures the practical, economical installation as required in your plans.

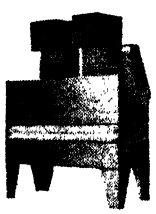


Type "SH" unit heaters for horizontal air discharge.

Available with capacities from 19,000 to 325,000 Btu per hour.

Type "V" or Vertiflow unit heaters for vertical air discharge.

Capacities from 52,600 to 552,000 Btu per hour.

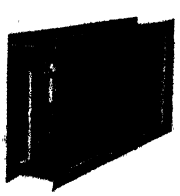


Type "BH" blower unit heaters for floor, wall or ceiling mounting.

Capacities from 109,400 to 1,047,000 Btu per hour.

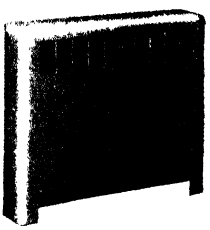
Type "W" water coils for cooling or heating with central plant systems.

Five widths, 11 to 35 in.; 2 to 8 rows of tubes; many lengths.



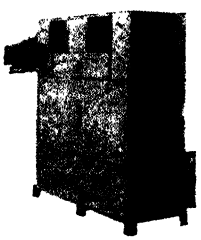
Type "E" evaporator coils for direct expansion cooling systems using Freon or Methyl chloride.

Four widths—one to six rows of tubes; many lengths.



"Streamaire" Convectors Standardized Types—circulate rather than radiate heat. Used with steam or hot water systems.

Cabinets blend with architecture and room furnishings.



"YAC" vertical or horizontal type air conditioning units provide "weather to order" year-round. A constant, quiet flow of evenly distributed clean, healthfully-fresh air at fingertips.

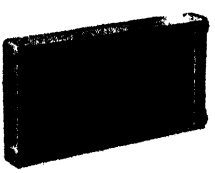
Also available in units for winter or summer conditioning only. Capacities from 400 to 16,625 cfm.

Types "B" and "A" blast coils for central plant heating and air conditioning systems.

Steam distributing tube type available.

Type "C" commercial heat transfer coils for use in factory built air conditioning units.

Steam distributing tube type available. One, two and three rows of tubes.



Revere Copper and Brass Incorporated

Executive Office: 230 Park Avenue, **New York 17, N. Y.**

MILLS—BALTIMORE, MD., NEW BEDFORD, MASS., ROME, N. Y., DETROIT, MICH., CHICAGO, ILL.

SALES OFFICES—BOSTON, MASS., PROVIDENCE, R. I., PHILADELPHIA, PA., ATLANTA, GA., NEW YORK, N. Y., PITTSBURGH, PA., CLEVELAND, OHIO, CINCINNATI, OHIO, GRAND RAPIDS, MICH., MILWAUKEE, WIS., ST. LOUIS, MO., INDIANAPOLIS, IND., MINNEAPOLIS, MINN., DALLAS, TEXAS, SEATTLE, WASH., SAN FRANCISCO, CALIF., LOS ANGELES, CALIF., HARTFORD, CONN., DAYTON, OHIO, HOUSTON, TEXAS

REVERE PIPE AND TUBE OF COPPER AND COPPER ALLOYS

For Heating, Air Conditioning, Plumbing, Fuel Lines, Compressed Air Lines, etc.

Revere Copper Water Tube, Types K, L, and M meets Federal and *ASTM* specifications.

Types K, and L furnished in hard and soft tempers.

Types M, 2½ in. and above, furnished in hard temper only.

Revere Type K Copper Water Tube in hard temper is not too hard to be bent with a hand bender.

Type K soft temper tube is recommended for underground water service or fuel lines.

Hot water lines of Copper Water Tube lose very little heat to ambient air, hence save fuel.

Revere Grade A Red-Brass Pipe or Copper Pipe (SPS) are recommended for piping systems where threaded connections are required.

For Radiant Heating

Revere Copper Water Tube, furnished in 60 ft coils is easily bent to form sinuous coils for heating panels.

Long, one-piece lengths of copper tube reduce the number of couplings or joints required.

Small diameters of copper tube require less thickness of embeddment.

For Refrigeration Systems, Air Conditioning, or general use **Revere Dryseal** copper tube is dehydrated and sealed.

Furnished in dead soft temper, it is easily bent and flared.

Suitable for fuel lines, compressed air lines and air control lines.

For Condensers and Heat Exchangers

Revere Cupro-nickel condenser tube has definitely been found superior for condensers, after coolers, and similar heat exchangers.

Similar tubes of Revere Admiralty Metal are widely used.

Revere Seamless Copper Tube is commonly used for finned tube coils.

For Industrial Piping and the Process Industry

Revere produces a wide range of pipe and tube made of copper and copper alloys for industrial use where high resistance to corrosion is required.

Solicitations for assistance in selecting piping material best suited to specific conditions are welcome.

Silver-brazed Joints

Revere Red-Brass Pipe or Copper Pipe is recommended where silver-brazed joints are required with standard pipe sizes.

Revere Copper Water Tube and standard soldered type fittings can also be silver-brazed with excellent results and generally at a saving in cost.

Technical Advisory Service

Revere maintains a staff of technical men to assist engineers, designers, and contractors in the selection of suitable Revere products for various applications. Their services are available without obligation.

Technical Literature

Literature relating to many fields of application for **Revere** pipe and tube products are available upon request.

Two booklets on Radiant Panel Heating cover the subject of design procedure and in the form of a non-technical and unbiased discussion for lay readers.

Revere Copper Water Tube
STANDARD DIMENSIONS AND WEIGHTS

Size In In.	Type K			Type L		Type M	
	O.D. in In.	Wall Thickness In.	Wt. Lb per Ft	Wall Thickness In.	Wt. Lb per Ft	Wall Thickness In.	Wt. Lb per Ft
¼	.375	.032	.134	.030	.126		
⅜	.500	.049	.269	.035	.198		
½	.625	.049	.344	.040	.285		
⅝	.750	.049	.418	.042	.362		
¾	.875	.065	.641	.045	.455		
1	1.125	.065	.839	.050	.655		
1¼	1.375	.065	1.04	.055	.884		
1½	1.625	.072	1.36	.060	1.14		
2	2.125	.083	2.06	.070	1.75		
2½	2.625	.095	2.93	.080	2.48	0.65	2.03
3	3.125	.109	4.00	.090	3.33	.072	2.68
3½	3.625	.120	5.12	.100	4.29	.083	3.58
4	4.125	.134	6.51	.110	5.38	.095	4.66
5	5.125	.160	9.67	.125	7.61	.109	6.66
6	6.125	.192	13.9	.140	10.2	.122	8.92

The American Brass Company

General Offices: Waterbury 88, Conn.

Offices and Agencies in Principal Cities

ANACONDA
from mine to consumer

IN CANADA: ANACONDA AMERICAN BRASS LIMITED, New Toronto, Ontario

PRODUCTS—Anaconda Deoxidized Copper Tubes and Fittings; Anaconda "85" Red Brass Pipe; Everdur Metal for storage heaters, storage tanks, ducts and air conditioning equipment

ANACONDA COPPER TUBES AND FITTINGS

For Heating, Plumbing and Air Conditioning

Anaconda Deoxidized Copper Water Tubes assembled with Anaconda Fittings offer an unusual combination of advantages in hot water heating systems at a cost only slightly higher than black iron and approximately the same as wrought iron pipe. These advantages may briefly be summarized as follows:

Low Friction Loss—Because the inside surfaces of copper tubes are inherently smoother than those of pipe and tubes made of ferrous materials and also because they do not become roughened by the formation of rust, these tubes offer a lower resistance to flow. In addition, the long radius turns of Anaconda Elbows and the smooth inside surface of Anaconda Wrought Copper Fittings further reduce friction losses.

These factors naturally increase the efficiency of the system, particularly when it includes a forced pressure circulator.

Ease of Installation—In many places the flexibility of copper tubes simplifies connections that ordinarily would be awkward and expensive to make with rigid pipe and threaded fittings. Anaconda Solder Fittings are compact. They can be installed in restricted space where the use of a wrench would be impossible.

Architects and builders naturally object to large holes and notches cut in the framing members of a building for the passage of piping. Anaconda Copper Tubes can be installed with a minimum of cutting in the structure—although holes should be large enough to permit movement of tubes due to expansion and contraction.

Temper and Thicknesses—Anaconda Copper Tubes are made in both hard and soft temper and in standard wall thicknesses.

They meet the requirements for these types of tubes in Federal Specification WW-T-799a and *A.S.T.M.* Specification B88. Type K, the heaviest, is recommended for heating lines and general piping.

Accuracy of Dimensions—Anaconda Deoxidized Copper Water Tubes are all finished to the close size tolerances required by the *A.S.T.M.* and Federal Specifications, which have been found essential for efficient assembly with solder fittings.

Anaconda Copper Tubes, in standard sizes are furnished soft in 60-ft coils; also hard and soft in 20-ft straight lengths.

The American Brass Company

REFRIGERATION TUBING

Anaconda Dehydrated Copper Refrigeration Tubes are manufactured in accordance with *A.S.T.M.* Specification B68, in all standard sizes up to and including ¾ in. O.D., in 50-foot coils. Other lengths are made to special order. These tubes are manufactured under exceptionally clean mill conditions and close technical control to assure clean, smooth inside surfaces, unusual accuracy in size and shape, and uniform softness. The tubes are cup-sealed immediately after annealing and dehydrating.

ANACONDA "85" RED BRASS PIPE

Anaconda "85" Red Brass Pipe, in standard pipe sizes, is considered the highest quality corrosion-resistant pipe commercially obtainable at a moderate price and is recommended for steam return lines.

Anaconda "85" Red Brass Pipe contains 85 per cent copper and conforms to Government specifications for Grade "A" water pipe. The mark "Anaconda 85" is stamped in the metal at one-foot intervals throughout each length.

EVERDUR*

Everdur Metal is the original copper-silicon alloy group. It is manufactured by The American Brass Company in five standard compositions and in practically all commercial forms.

This high strength engineering metal is resistant to a wide range of corroding agents. Because of a versatile combination of useful properties, Everdur has become standard as a material for equipment in many fields of engineering and industry.

In addition to their non-rusting properties and high strength, Everdur alloys possess many qualities not usually found in metals of this character. They are unusually resistant to general atmospheric conditions and other normally corrosive factors. Everdur alloys have excellent machining and working characteristics and can be fabricated into a variety of forms and shapes. Everdur alloys are available for oxy-acetylene or carbon arc welding.

*"Everdur" is a trademark of The American Brass Company registered at the U. S. Patent Office.

CORROSION RESISTANCE

The corrosion resistance of Everdur is equivalent to that of pure copper and in some cases, slightly superior.

However, like copper and all copper alloys, Everdur is not equally resistant to all corroding agents, nor to the same corroding agents under all conditions. As with copper, the resistance to corrosion may be substantially reduced in some instances by the presence of oxidizing agents. Nevertheless, Everdur does offer excellent resistance to the corrosive action of many solutions and atmospheres.

Everdur Tanks—Everdur copper-silicon alloy is an ideal material for durable, rustless water tanks of every description—from domestic range boilers to large storage heaters for hotels, laundries, hospitals, textile plants, schools or breweries.

Everdur is made in all commercial shapes including annealed tank plates which have physical properties as given in *A.S.T.M.* Specification B96.

Minimum specification requirements for hot rolled-and-annealed tank plates are: Tensile Strength, 50,000 psi.; Yield Strength (at 0.5 per cent elongation under load) 18,000 psi.; Elongation, 40 per cent in 2 inches.

Welds made with annealed Everdur tank plates meet the requirements for Class B and C vessels in the *A.S.M.E.* Code for Unfired Pressure Vessels.

For additional data and names of fabricators address our nearest office or agency.

EVERDUR FOR AIR CONDITIONING EQUIPMENT

Because of its strength and welding properties, Everdur may be substituted for steel and fabricated by substantially the same methods and with much the same equipment as steel.

Everdur metal has been used with marked success for fans and blowers, ducts, humidifiers, cast and wrought parts of other equipment items subject to corrosive influences.

EVERDUR LITERATURE

Descriptive literature containing much pertinent tabular data will be sent on request.

Mueller Brass Co.

Port Huron, Mich.

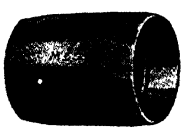
Branch Offices and Representatives in Principal Cities

ALBANY, N. Y.
ATLANTA, GA.
BOSTON, MASS.
CHICAGO, ILL.
CINCINNATI, OHIO
CLEVELAND, OHIO
ST. LOUIS, MO.
DALLAS, TEXAS
DETROIT, MICH.
FLINT, MICH.
HARRISBURG, PA.
INDIANAPOLIS, IND.
LOS ANGELES, CALIF.
MINNEAPOLIS, MINN.
NEWARK, N. J.
PHILADELPHIA, PA.
N. S. PITTSBURGH, PA.
SAN FRANCISCO, CALIF.
SEATTLE, WASH.
WASHINGTON, D. C.

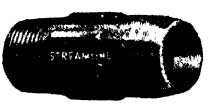
Canadian Sales and Manufacturer

MUELLER LTD., SARNIA, CANADA

PRODUCTS—STREAMLINE Copper Pipe and Seamless Tubes; STREAMLINE Hard Copper Pipe and Solder Fittings; Valves, Flared and STREAMLINE Solder Fittings for Mechanical Refrigeration; Forgings of Brass, Bronze and Copper; Castings of Brass and Bronze; Rod; Screw Machine Products; Fabricated Parts and Special Nickel and Chromium Plated Parts; Machined Formed Tubes.



Coupling Copper to Copper



Copper to Outside I.P.S.

45 Deg Elbow

Streamline Copper Pipe and Fittings for heating, plumbing, air conditioning and industrial use are made by the STREAMLINE PIPE AND FITTINGS Division, Mueller Brass Co., Port Huron, Mich.

The **Streamline** Solder Fitting is the original solder type fitting, introduced and manufactured by the Mueller Brass Co. of Port Huron, Mich. It incorporates many advantageous features and has proved to be the revolutionary advance of the age in the development of piping systems for plumbing and heating and for many industrial uses.

The **Streamline** Solder Fitting is not connected either by threading or flaring, but by soldering. The outside surface of the copper pipe and the inner surface of the **Streamline** fitting are cleaned with sandcloth, and solder flux is then applied to the cleaned surfaces to eliminate oxidation when the assembled joint is heated. The joint is then sufficiently heated with a blow or acetylene torch and the soldering operation is performed by feeding wire or stick solder through the feed hole in the fitting.

The **Streamline** Cast Bronze Solder Fitting alone has the solder feed hole. The solder feed hole, through which the solder is introduced, enters directly into an internal feed channel. The feed channel is located equidistantly between the internal shoulder against which the pipe rests and the outer edge of the fitting. When solder is introduced it is distributed by capillarity from the feed channel and distributed evenly and thoroughly between the bonding surfaces, traveling inward to the shoulder and outward to the edge of the fitting where it appears as a continuous solder ring around the full circumference of the pipe. This ring, and feed hole completely filled with solder, constitute positive visible proof to the operator that the joint is permanently leak-proof.

Streamline Pipe and Fittings Division

MUELLER BRASS CO.

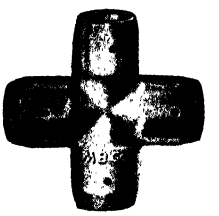
Port Huron, Mich.

Patents 1770852; 1770502

90 Deg Elbow

Tee

Tee
Copper to Inside I.P.S.



Crosses

The solder may be fed from any position, whether the feed hole is located at the top, side or bottom. Owing to the never failing phenomena of capillarity, the solder will flow up, down or laterally with equal facility.

Streamline Copper Pipe is a seamless cold drawn copper tubing conforming to *A.S.T.M.* B88. It is made in sizes ¼ in. to 12 in. and Types K, L, and M, of which Type K is the heaviest. The intermediate weight, Type L, is the preferred weight for plumbing, heating and refrigeration. Type M is manufactured only in sizes 2½ in. and larger.

For most purposes hard drawn pipe is used, though Types K and L can be furnished annealed when bending is required. Annealed Type "K" in sizes up to 2 in. is widely used for underground water "services."

Streamline Solder Fittings are furnished in all sizes to 6 in. inclusive. They are of the same thickness as Navy and MSS Fittings for 125 steam or 175 lb non-shock water pressure.

All fittings over 6 in. are flanged and may be had with either *A.S.A.* or riveted pipe standard flanges.

Mating flanges are soldered to the pipe—*A.S.A.* 125 standard flanges are available from 1 in. up.

During the last fifteen years architects and engineers have used **Streamline** Copper Pipe and Fittings successfully in every type of building construction and in thousands of installations throughout the United States and Canada.

In addition to its rust and vibration-proof qualities and long life, **Streamline** has many other advantages such as the reduction in size of pipe lines and radiator connections from those nominally used, a neat, compact installation requiring a minimum of space and important advantages in industrial and drainage applications. There is a **Streamline** product for every piping requirement.

Write Mueller Brass Co., Port Huron, Michigan, for complete information and catalog.

Atlantic Metal Hose Co., Inc.

112 West 64th St. **New York 23, N. Y.**

ATLANTIC SEAMLESS FLEXIBLE METAL HOSE
ABSORBS VIBRATION
on REFRIGERATING and AIR CONDITIONING EQUIPMENT

For standard pressures in a variety of metals

Type A

For high pressures and severe service

Type A-1

For refrigeration and air conditioning Freon Lines

Vibration Absorber

Throughout the Heating, Ventilating and Air Conditioning Industry—where the ability to control vibration and compensate for expansion must go hand in hand with the ability to take punishment and withstand pressure—Atlantic hose continues to break performance and economy records year after year.

Durable—the specially selected alloy and method of construction assures long life even under severest service.

Simplifies Installations—Both slip-on as well as pipe thread fittings can be provided in all commercial sizes for quick assembly.

We also manufacture hose for the conveyance of dust, air, exhaust, steam and all liquids.

Engineering Service—Our engineering department will cooperate with prospective users in the selection of suitable standard flexible hose, or in the design of hose to meet special requirements. Advise us of the details of the service and we will be pleased to offer our recommendation.

Chicago Metal Hose Corporation

Maywood, Illinois

PLANTS

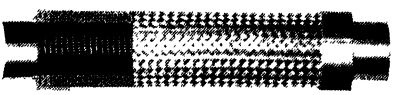
MAYWOOD, ROCK FALLS and ELGIN, ILLINOIS

OFFICES

NEW YORK CLEVELAND DETROIT CHICAGO GLENDALE, CALIF.
PITTSBURGH PHILADELPHIA

Distributing Outlets in Principal Cities

REX Vibra-Sorbers Noise and Vibration Control



Rex Vibra-Sorbers control vibration and reduce noise in refrigeration and air conditioning machinery. All-metal construction is liquid- and gas-tight, withstands high pressures, does not age, and has high corrosion resistance.

Available in copper bearing alloy for use with Freon or Methyl Chloride; or steel for Ammonia systems.

Write for detailed data.

SIZES: 3/16 in. to 4 in. inside diameters.

PRESSURES: 1,000 psi to 3,700 psi.

LENGTHS: Standard stock lengths. Special lengths available on order.

COUPLINGS: Stock units with male or female sweat fittings; also available with male pipe thread fittings.

REX-TUBE Flexible Metal Hose

Rex-Tube Convoluted Flexible Metal Hose Types have three basic formation patterns: square-locked, ball-bearing (or double-groove), and fully interlocked. Made of stainless steel, brass, steel, aluminum, bronze and other alloys. Packless and packed types. Sizes range from 3/16 in. to 12 in. inside diameters, and lengths to suit requirements.

FOR

Diesel engine exhaust lines
Refrigeration tubing armor
Air blower ducting
Ventilating ducts
Control wire casing
Wiring conduit
Suction hose
General utility hose

REX-WELD Flexible Metal Hose

Rex-Weld hose types are manufactured from uniform wall tubing by a special CMH corrugation-forming process. Metals used are steel, bronze, and other alloys. Rex-Weld sizes range from 3/16 in. to 12 in. inside diameter; with lengths and couplings to fit specific requirements. Especially designed for use under high temperatures and pressures, and where corrosive action is present.

FOR

Steam Hose
Reciprocating flexible connections
Oil burner connections
Pressure lubricating lines
Conducting searching gases and liquids
Diesel engine exhaust lines
Misalignment correction

FLEXIBLE METAL HOSE FOR EVERY USE

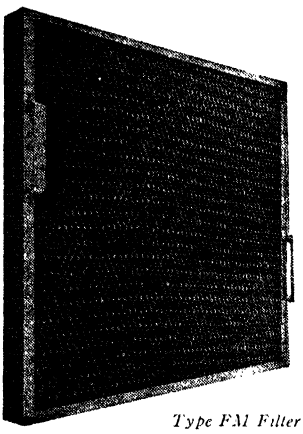
Air Devices, Inc.

Air Diffusers • Exhausters • Air Filters
Filter Holding Frames • Hot Water Generators

17 East 42nd St.
New York 17, N. Y.

AGITAIR PRODUCTS

Agents in All
Principal Cities



Type FM Filter

AGITAIR AIR FILTERS

HIGH VELOCITY • ALL METAL PERMANENT • CLEANABLE

Designed along entirely new air filtering principles, the high velocity Agitair Type FM permanent, cleanable air filter assures an amazingly high dust arresting efficiency and dust-holding capacity coupled with sustained low resistance to air flow. This permits the Type FM to remain in service from two to three times as long as ordinary 2 in. permanent, cleanable filters.

Although these new filters do not have to be cleaned as often, particular attention has been paid to their design to make cleaning easier and more thorough. They can be restored to top efficiency easily and quickly. Ruggedly constructed to withstand the mechanical abuse of cleaning. Panels and frames are accurately designed to prevent leakage around the filters.

HOW IT WORKS

High turbulence of many finely divided air streams is the keynote of Type FM air filter's new design. The media divides the air into countless fine streams and throws those streams into violent cyclonic turbulence. Each little "cyclone" centrifuges its dirt particles against countless viscous-coated "wiping surfaces" which virtually scrub the air clean by catching and holding the dirt. There is no straining action, hence no clogging.

HIGH VELOCITY

The Agitair FM Filter is designed to perform at highest efficiency at an approach velocity of 432 fpm—or 1200 cfm through a 20 x 20 in. filter panel. The efficiency of the FM is higher than conventional filters when operating at the lower design velocity of 288 fpm.

1/3 LESS SPACE REQUIRED

The ability of the FM to filter, with greater efficiency, 50 per cent more air at the high velocity of 432 fpm reduces the number of filter panels required. Now TWO FM's will do the work of THREE ordinary filters . . . ⅓ less space required . . . fewer units to be installed . . . fewer units to be serviced . . . overall installation and maintenance costs reduced to a minimum.

HIGHER EFFICIENCY

At the recommended velocities of other leading all metal viscous type filters, the Agitair FM has a higher dust arresting efficiency, which increases as velocities are stepped up.

LOWER RESISTANCE

The sustained low resistance of the Agitair FM means sustained peak volume of air for longer periods of time . . . no loss in air volume . . . no danger of unloading . . . clean filtered air at all times.

HIGHER DUST HOLDING CAPACITY

Employing a new formula for air filtration the new Agitair FM holds more dirt, from two to six times as much as ordinary 2 in. permanent, cleanable filters. No early clogging of air passages . . . less frequent servicing . . . lower maintenance cost.

LONGER SERVICEABLE LIFE

The Agitair FM Filter with its greater dust holding capacity, stays in service for longer periods of time; gives efficient performance for months instead of weeks or weeks instead of days.

Less frequent servicing—and rugged construction combine to give the Agitair FM Filter a much longer serviceable life.

TWO TYPES OF HOLDING FRAMES

Individual Type: Designed and constructed for easy handling in single unit installations, and to facilitate "on the job" assembly, into a multiple unit bank.

Pre-Fabricated Type: Delivered completely knocked down for easy assembly, this Agitair holding frame has been especially designed for installations requiring an unusually large number of filter panels and where cramped and unusual conditions place a limitation on available space.

GREASE FILTERS

An efficient, all-metal grease catching, grease holding media. Available in all sizes.

Air Filter Corporation

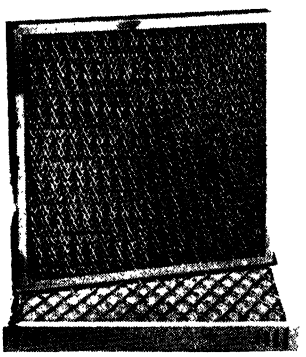
2514G W. Lisbon Ave. **Aircor** **Milwaukee 5, Wis.**

Canadian Representative
DOUGLAS ENGINEERING CO., LTD. MONTREAL

Manufacturers of AIRCOR AIR & GREASE FILTERS—the PERMANENT, CLEANABLE, VISCOUS TYPE Air Filters, designed for Heating, Ventilating, Air Conditioning and Industrial Use.

AIRCOR designers and engineers have contributed many of today's important developments in air filtration, dust, grit and grease elimination for domestic, commercial, and industrial use. **Aircor** Air Filters are well known for their high efficiency, low air resistance, great dust-holding capacity and low maintenance cost.

The specially designed **Aircor** filter core is constructed of multiple layers of crimped, electroplated wire mesh arranged to provide an exceptionally large contact area and impart a turbulent swirling action to the air passing through. Galvanized, crimped, expanded metal diffuser acts as a lint arrestor to prevent lint from imbedding in filter media. All units have heavy gauge galvanized steel frames with full welded corners.



AIRCOR AIR FILTERS—TYPE F_1 & F_2

For Air Conditioning, Heating and Ventilating

A permanent, cleanable viscous type air filter with special **Aircor** filter mesh design that traps more dust through complete depth while providing a minimum of air resistance. Dual purpose galvanized expanded metal screen deflects air stream, acts as lint arrestor—an aid in quicker, easier cleaning. Drain slots provided in filter frame. Bulletin 1245A.

Initial Resistance:	*Rated Efficiency*:
Type F_1 (1 in. thick) .060 in. w. g. at 288 fpm	98.5%
Type F_2 (2 in. thick) .065 in. w. g. at 288 fpm	98.5%

AIRCOR INDUSTRIAL FILTERS

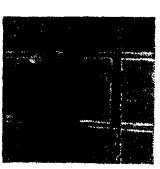
For Extra Heavy Duty

Specially designed for heavy duty service on industrial applications. Bulletin 146.

Initial Resistance:	*Rated Efficiency*:
Type D_2 (2 in. thick) .09 in. w. g. at 288 fpm	98.5%
Type D_4 (4 in. thick) .10 in. w. g. at 288 fpm	98.5%

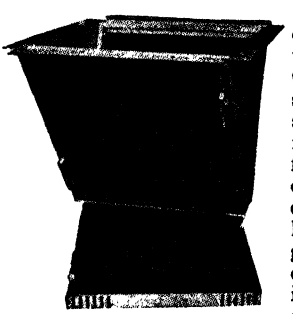
AIRCOR HOLDING FRAMES

For Flat and "V" Arrangements



Engineered holding frame design provides ample filtering capacity with a minimum of space. Compact, sturdy, extremely strong and rigid, this frame construction also simplifies filter removal and cleaning. Fireproof lining on back flange. Offers extra protection against air leakage. Available in V-type, or straight banks. Bulletin 600.

AIRCOR GREASE FILTER



Permanent, cleanable type **Aircor** Grease Filter specially designed to remove grease from exhaust ducts—a necessity in kitchens, galleys. Increases working comfort, decreases fire hazard, protects motors and brushes, and lengthens life of mechanical equipment. Assemblies for mounting on ceiling or wall, single or multiple units—includes holding frames, supporting angles and end seals. Bulletin 346.

I. *Resistance:* .07 in. w. g. at 216 fpm
Efficiency Rating: 98.5%. 2 in. Thick.

Write Air Filter Corporation for complete bulletins,

AIR-MAZE Corporation

5202 Harvard Avenue, **Cleveland, Ohio**

ENGINEERS AND MANUFACTURERS OF AIR FILTERS

DIRECT FACTORY REPRESENTATIVES IN ALL INDUSTRIAL AREAS

DISTRIBUTORS IN PRINCIPAL CITIES AND TOWNS THROUGHOUT THE UNITED STATES

Viscous Impingement Type Air Filter—Air-Maze viscous impingement cleanable type air filters are the result of nearly two decades of designing and building air filters exclusively. Air filter media consists of alternate layers of crimped galvanized screen cloth of various mesh, arranged to break up the air stream into minute, swirling currents. Dirt is impinged on the wire baffles, previously coated with an adhesive.

Progressive Density Provides Increased Dirt-Holding Capacity—An important feature of Air-Maze construction is the progressive density of the filter media, permitting lint and large particles to be collected on the upstream section of filter with little impedance to air flow. As shown in photos above, large quantities of dirt can be collected before filter requires cleaning. This design also lends itself to quick, thorough cleaning and recharging.

Dirt Arrestance—Efficiency of dirt arrestance varies, depending on filter design, type of test dust, dust feed, etc. Specific information on any type filter gladly furnished on request.

Resistances—Filters available with initial resistances as low as 0.045 in. water at 300 fpm. (Graphs showing resistance at various velocities are available for each type of filter.)

Face Velocities—Air-Maze offers air filters designed to operate efficiently at velocities from 106 fpm to 2000 fpm, depending upon application, pressure drop available, etc. Our representative will gladly furnish full information.

Sizes—Air filter panels made in rectangular shapes of any reasonable size and thickness. 1 in., 2 in. and 4 in. thicknesses are standard. Specially shaped filters also built to special order.

Holding Frames—Holding frames, complete with felt seal and choice of locking devices, are supplied when requested. For filter banks, Air-Maze furnishes either assembled frames or will drill frames for assembly on the job.

Cleaning Data—Filters easily cleaned with either hot water, steam or any commercial solvent. Charged by immersing in recommended adhesive or *S.A.E.* 30-50 oil. Complete instructions available upon request.

Write for Details—Write for name of nearest representative or information on any type of filter. Representatives in most principal cities. See classified section of your telephone directory.

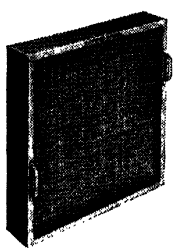
AIR-MAZE Corporation

5202 Harvard Avenue, **Cleveland, Ohio**

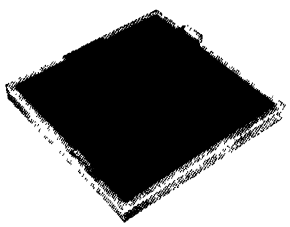
ENGINEERS AND MANUFACTURERS OF AIR FILTERS

Direct Factory Representatives In All Industrial Areas

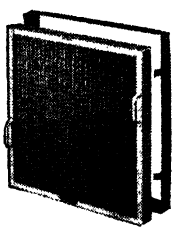
Distributors In Principal Cities And Towns Throughout The United States



Type "B" Industrial Filter



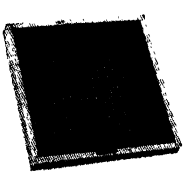
Type P-5 High-Velocity Filter



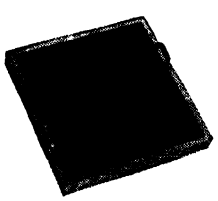
Type "A" Heavy Industrial Filter with holding frame

Air-Maze Corporation manufactures a complete line of viscous impingement type ventilating air filters to meet your requirements within a wide range of limits of pressure drop, velocity, dust-arrestance, weight, dirt-holding capacity and price. A few types are illustrated on this page.

These filters are all-metal—washable—fire-retardant.



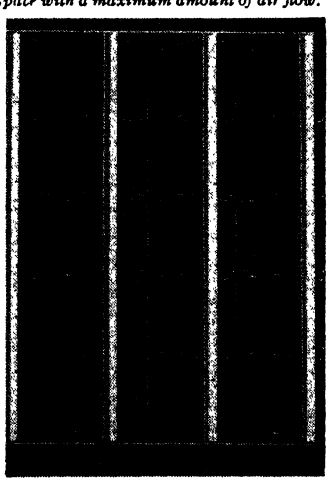
Kleenflo Filters for average applications*



Greastop Filters for kitchen canopies*

*Trade Mark registered.

Air-Maze panel filters arranged to save space with a maximum amount of air flow.



AIR-MAZE

The Filter Engineers

AMERICAN AIR FILTER COMPANY INC.

673 Central Avenue, **Louisville 8, Ky.**

In Canada: Darling Brothers, Ltd., Montreal, Quebec

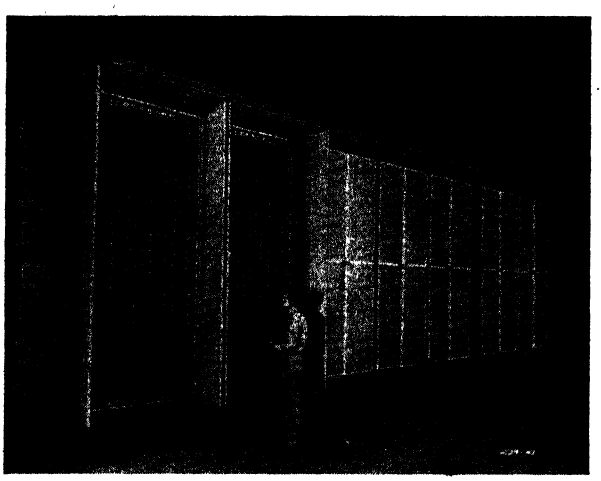
PRODUCTS: The American Air Filter Company, Inc. manufactures a complete line of Air Filtering Equipment including Electronic Air Filters, Automatic Self-Cleaning Filters, Viscous Unit Filters, and Dry Process Filters to be used for the removal of dust, soot, smoke, dirt, bacteria and other foreign matter from the air.

Because air filtration has proved to be the economical, practical and efficient method of cleaning the air, the modern air filter is now considered an absolute necessity in building ventilation or air conditioning, in the maintenance of health and personal efficiency, protection of interiors and furnishings and valuable merchandise and equipment. Shown here are but a few American Air Filter products in most general use.

The American Air Filter Company is recognized as an authority on dust problems and their satisfactory solution. Products offered embody the knowledge accumulated from twenty-six years of intensive research devoted exclusively to the study of dust problems and the development of air cleaning apparatus; the experience gained from designing, building and applying thousands of air filters; are backed by ample technical and financial resources; and may be relied upon as the most modern equipment in their field of service.

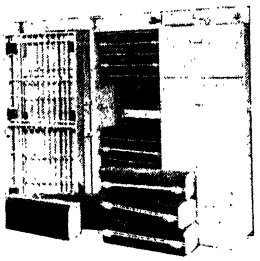
THREE TYPES OF ELECTRONIC AIR FILTERS

For more than ten years, research and experimentation with electronic air filtration have been in progress by AAF engineers. Today's complete line includes the self cleaning Electro-Matic introduced in 1939, the washable Electro-Cell with removable collector plates, and the Electro-Airmat with the replaceable Airmat paper medium. Here for the first time is high efficiency air cleaning in three types of electronic filters to meet any requirements for super clean air.

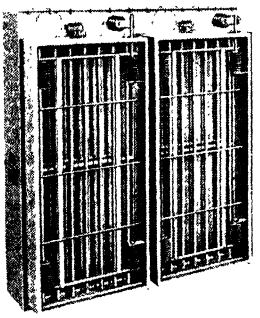


Electro-Matic Self-Cleaning Electronic Filter—The Electro-Matic filter is a self cleaning electric precipitator combining the most advanced principles of electronic air cleaning with notable improvements in construction details and method of operation. The self-cleaning feature is an exclusive advantage of the Electro-Matic filter. It eliminates the necessity of shutting down the filter for manual cleaning, minimizes the need for personal attention and permits continuous high-efficiency operation. It also allows the Electro-Matic filter to be built in standardized self-contained sections, easy to install and with all exposed parts of the filter casing electrically grounded for the protection of operating personnel. Send for Bulletin No. 250.

Electro-Cell Electronic Filter—Incorporates all of the new developments of major importance in electronic air filtration using collector plates. Installation has been simplified, performance improved and maintenance advantages provided. Built in vertical sections of two widths—2 ft and 3 ft over-all. Collector plate assemblies are removable; ionizers are hinged and extend the full height of the sections, preventing current loss. A choice of washing collector plate assemblies while in place, or removing assemblies for individual cleaning. Installation is simplified because filter is built in vertical sections rather than assembled of small units. Parts to be lifted and aligned are light in weight and electrical connections simplified. Write for Bulletin No. 252.

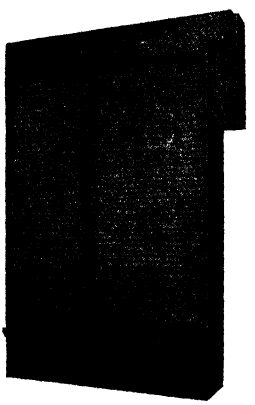


Electro-CELL Filter



Electro-AIRMAT Filter

Electro-Airmat Electronic Filter—The application of an electrostatic charge to a dielectric filtering material is an exclusive AAF research development which began early in 1934. Airmat paper is composed of a number of plys of porous tissue-like cellulose sheets. When electrically charged the plys tend to separate and each individual fibre becomes a collecting electrode which attracts and holds the dust and smoke particles. Ease and convenience of maintenance is a desired advantage of the Electro-Airmat. Requires neither water nor sewer connections for cleaning, nor spraying with oil to maintain its efficiency. When Airmat paper has accumulated its dust load it is removed and replaced with clean material by means of a mechanical loader. In case of power failure, filter media provides best mechanical air filtration known. Send for Bulletin No. 253.



American Multi-Duty Self-Cleaning Filter

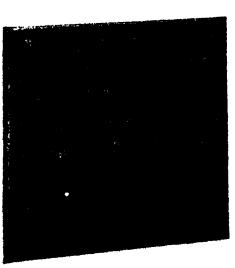
American Multi-Duty Automatic Filter provides outstanding features of performance and design and will accomodate either armored screen panels or die stamped louver panels available in three types. Offers advantage of uniformly constant air supply, fixed operating resistance and automatic operation. Ideal for ventilation and air conditioning service. Available in any size or capacity. Send for Bulletin No. 241-A.

AAF UNIT FILTERS

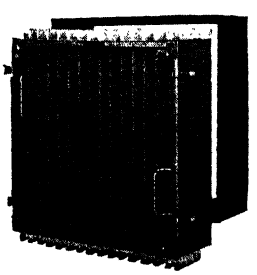
Throway Air Filter—Throway filters are inexpensive and designed to be discarded after accumulating dust load. Send for Bulletin No. 117-E.

Airmat Type PL-24—Airmat filters use standard Airmat medium, renewable after collecting dust load. Used both for comfort and industrial air conditioning. Available with unit frames to be set up to meet any capacity requirement or space condition. Send for Bulletin No. 230-C.

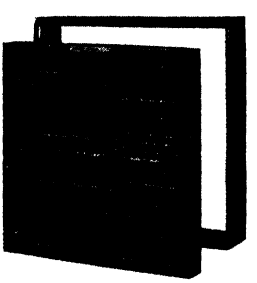
M/W Filters—The M/W comes in 2 in. and 4 in. thicknesses. Ideally suited to air cleaning problems encountered in general ventilation and commercial air conditioning. Permanent type, washable. Send for Bulletin No. 202.



Throway Air Filter



Airmat Type PL-24 Filter



M/W 2 Filter

W. B. CONNOR ENGINEERING CORP.

114 East 32nd Street
New York 16, N. Y.

Representatives in All Principal Cities

In Canada: Douglas Engineering Co., Ltd., Montreal, P. Q.

Air Recovery — **DOREX** — **Air Purification**

DOREX Activated Carbon Adsorbers recover the freshness of vitiated air by extracting air-borne odorous, gaseous and vaporous impurities. When applied to recirculated air in air conditioning, DOREX Adsorbers convert used, stale, *conditioned* air for ventilation thus reducing to a minimum the volume of *unconditioned* outdoor air make-up otherwise necessary.

With DOREX Air Recovery, the cooling and heating capacity of a proposed air conditioning system is decreased by the saving in outdoor air load.

With DOREX Air Recovery, an existing air conditioning system will serve a larger space or satisfy a greater conditioning load without increase in cooling or heating equipment or the consumption of more fuel or energy.

The highly active, specially processed and impregnated carbon employed will remove from the air passed through it and retain 95 per cent of all entrained gaseous impurities and maintain approximately this efficiency for from 6 months to 2 years depending upon the air contamination. Upon exhaustion the carbon is reactivated for re-use.

DOREX Air Recovery equipment is available in several types to suit individual requirements.

TYPE H—FOR COMPLETE DECONTAMINATION OF ALL AIR PASSED THROUGH IT

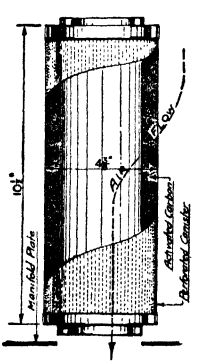


Fig. 1

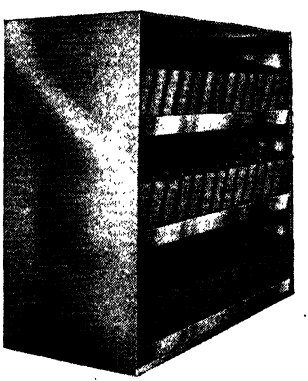


Fig. 2

Fig. 3

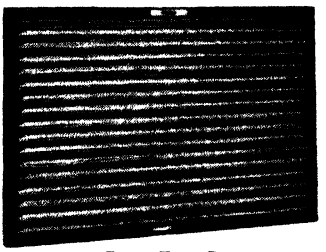
DOREX Type H Equipment consists of light-weight, removable, perforated, activated carbon-filled, adsorption canisters. These are mounted in multiple on one or more supporting manifold plates in such manner that all air to be treated will pass uniformly through the granular carbon media. The assembly arrangement is flexible to suit the space limitations. The resistance to air flow averages only 0.15 to 0.2 in. wg.

Fig. 1 shows a typical canister. It is closed at the top and the inner cylinder is open at the bottom, which opening registers with a corresponding hole in the supporting manifold plate. Fig. 2 is a photograph of a typical arrangement of canisters as installed. In this instance, three manifold plates each support 98 canisters arranged in 7 rows of 14 canisters each. Fig. 3 is a sectional view of this arrangement with the side removed and indicating direction of air flow. Each canister decontaminates from 25 to 35 cfm of air.

All Dorex equipment is covered by U. S. Patents Nos. 2,214,737; 2,303,331; 2,303,332; 2,303,333; 2,303,334 and others pending; Canadian Patents Nos. 383,986; 429,206; 395,611; 404,855; 410,088; 418,787; 443,235.

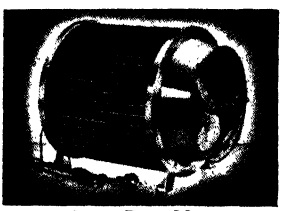
TYPE G—FOR CONTINUOUS DECONTAMINATION OF RECIRCULATED AIR

The DOREX Type G Air Recovery Panel is designed to remove accumulated odors and gaseous impurities from air recirculated by air conditioning units and systems. Its extremely compact design and the ease with which it can be installed makes it equally adaptable both to existing systems without requiring expensive alterations, and to newly designed systems, particularly where space is at a premium. It is also adapted to incorporation in *package* conditioners, railway cars, buses and airplanes, unit heaters and cold diffusers.



Dorex Type G

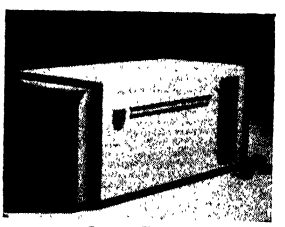
The Type G Air Recovery Panel consists of sturdy metal frames, each housing a battery of exposed perforated metal tubes which contain the granular carbon filter media. These panel units are available in stock sizes, suitable for arrangement in air ducts, or for attachment to standard dust filters, outlet or inlet grilles. They are designed to expose a maximum of carbon adsorption surface to the air stream with a minimum of resistance to air flow. Standard units are of one, two or three tube rows in depth, designated as G-1, G-2 and G-3, respectively.



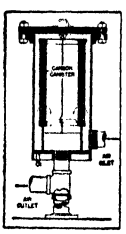
Dorex Type SQ

The DOREX Type SQ Odor Adsorber is an entirely self-contained unit suitable for either portable or stationary installation. It consists of a cage of closely spaced, perforated, granular activated carbon-filled tubes housing a quiet operating, circulating fan and motor. It is furnished assembled, equipped with starting switch and complete with extension cord and plug ready to connect to electric socket. **The DOREX Type SQ Unit** keeps the room air in continuous motion while, at the same time, completely purifying one-third of the total air circulated. It, therefore, provides both air circulation and ventilation without the use of outdoor air.

At the right is an illustration of the **Type A-100-B,** smallest of the DOREX self-contained *package* recirculating Odor Adsorbers. In its attractive enameled wood cabinet are contained a dust filter, four carbon gas adsorbing canisters, circulating fan and motor. It has a host of practical uses—in homes, offices, doctor's rooms, walk-in refrigerators, etc.



Dorex Type A



Dorex Type PL

The Type PL DOREX Vapor and Gas Adsorber is designed especially to extract oil vapors, fermentation odors and other gaseous impurities from compressed air. It is the only device which effectively removes air-entrained gaseous odors and impurities not eliminated by commercial filters, separators, after-coolers or receivers.

"AIR CONSERVATION ENGINEERING"

A complete and authoritative text book on the function, engineering and application of Air Recovery in air conditioning. Contains valuable tables and charts. Price $2.00. Complimentary copies available to recognized engineers upon request.

AMONG THOUSANDS OF DOREX USERS

American Tel. & Tel. Co.	General Motors Corp.	Radio Corp. of America
Anheuser-Busch, Inc.	Hammermill Paper Co.	E. R. Squibb & Sons
Boeing Aircraft Co.	Lever Bros.	Union Carbide & Carbon Corp.
Bristol Myers Co.	Monsanto Chemical Co.	Western Electric Mfg. Corp.
E. I. du Pont de Nemours Co.	Pennsylvania R.R. Co.	Western Union Telegraph Co.

(*See pages 1100 and 1101 for data on* KNO-DRAFT *Adjustable Air Diffusers*)

Dollinger Corporation

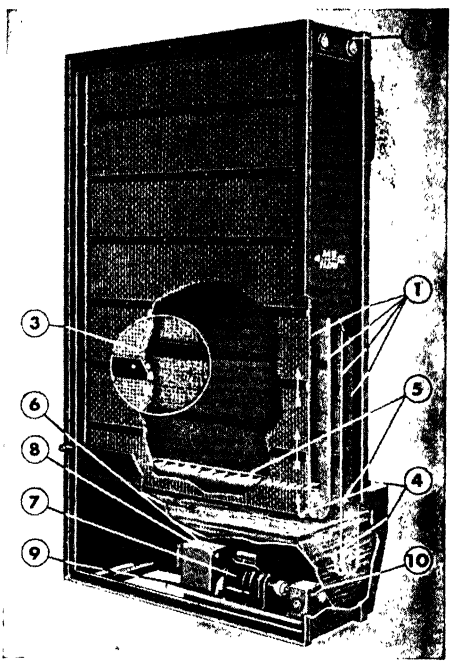
Filters for Building Ventilation, Air Conditioning, Engine Intake, Pipelines and Many Other Special Applications.

Representatives in Principal Cities

6 Centre Park — DOLLINGER PROTECTOMOTOR STAYNEW FILTERS — Rochester 3, N. Y.

STAYNEW MODEL A-3 AUTOMATIC FILTER

An endless curtain type oil-bath filter for handling large volumes of air at low cost plus exceptionally large dust-handling ability. The efficiency of Staynew Model A-3 is unsurpassed among mechanical self-cleaning filters.



Model A-3 Automatic Filter
(numbered features are referred to in accompanying description)

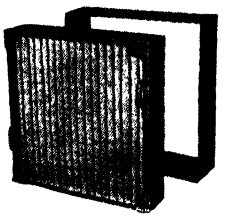
Operation and Features: *Double* filter curtains (1) carried on heavy roller chains driven by sprockets keyed to the shafts of the curtain rollers (2). These rollers float on ball bearings for quiet, frictionless operation. Curtains consist of removable panels (3) made of a single layer of bronze screen cloth to which are attached layers of woven copper mesh.

The first of the curtains is the denser, having about twice the impingement surface of the second or rear curtain. This first curtain acts as the filter and travels through the oil reservoir. The second curtain does not enter the reservoir, but acts only as a safeguard against oil entrainment. This design permits a direction of curtain travel such that cleaned panels (4) are always on the filtered air side. Therefore no dust can be carried across the back or return side of the front curtain to be blown off and carried on by the flow of air.

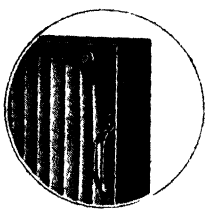
Patented, exclusive Staynew Air Brush Conditioners (5) prevent excessive amounts of oil being carried upward on the curtain panels and being entrained in the air stream.

Specifications

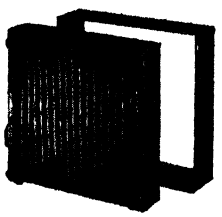
Model A-3 Filters are sectional and may be bolted together to obtain any required capacity. Sections come in two widths, 4 ft 3 in. and 2 ft 9 in. Curtain drive and control mechanism (6) arranged either as an integral part of filter unit or for remote mounting, includes a ⅙ hp motor (7) driving through a reduction gear and a momentary contact time switch (8) for testing and checking curtain travel and compressed air control. All are mounted on a common base plate (9) on clean air side of filter. Shear pin (10) is provided for protection of moving parts from accidental damage. The drive motor and the Air Brush Conditioners operate simultaneously for a few seconds at 15 minute intervals.



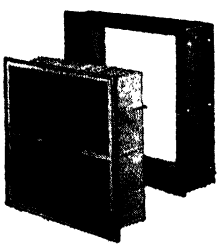
Model WKE Panel and Frame



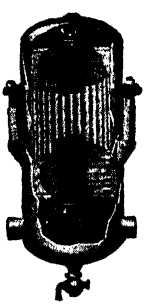
Handles and Latches



Viscous Model DPV Panel and Frame



Standard Panel Insert and Frame



Model ELS (Sectional View)

STAYNEW PANEL TYPE FILTERS

Model WKE: Dry-type finned panel filter for use in ventilation and air conditioning systems. Extremely large filtering area in relation to overall size. Adaptable to wide variety of filtering media—in fact, almost any medium obtainable in sheet form that can be crimped. Steel mesh on both sides of medium prevents sagging and makes the WKE *fire-resistant* (models available to meet Class I Fire Underwriters approval), and cleanable without possible damage from vacuum cleaning tool or cleaning nozzle. It may also be washed or dry cleaned when and if necessary. There are no cross bars, spacer bars, or other obstructions to interfere with the cleaning operation.

Filter cells are held in rigid box-type supporting frames of heavy gauge metal by spring-loaded cam-type locking latches. Two lifting handles are provided on each cell. Filtering medium supplied already crimped and cut to size. It may be inexpensively replaced in 2 to 5 minutes right at the filter bank—no special tools required.

Frames are drilled so that they can be riveted together to form a flat bank, or by the addition of angle uprights into a "V" or staggered arrangement.

Viscous Panel (Model DPV): A permanent type panel for air conditioning systems used in heavy duty industrial service. Filtering media consist of a series of layers of crimped galvanized screen cloth and woven mesh. These media when coated with PD-10 Pingene Filter Oil form an unusually efficient filter. Model DPV filters are cleaned easily with live steam or by washing in a suitable solvent. Spring-loaded locking latches and lifting handles are provided as in Model WKE.

Both Model WKE and DPV cells are furnished in 2 in. and 4 in. depths in various standard sizes.

Standard Panel: Dry-type Fin Construction, high filtering efficiency. Heavy steel Panel Insert and Frame. Cleanable. Forty-two square feet of filtering area. Thousands of Staynew Standard Panel Units have given satisfactory service for years. Available in 20 in. x 20 in. x 7 in. size only.

STAYNEW LIQUID FILTER

Model ELS: Widely used for the filtration of cooling water to prevent clogging of spray nozzles. Exclusive, low-cost SLIP-ON INSERT easy to remove, clean, replace. Radial Fin Construction provides all possible filtering area in smallest possible space. Standard models available to handle up to 1000 gpm.

Representatives in Principal Cities

Complete Information from Factory on Request

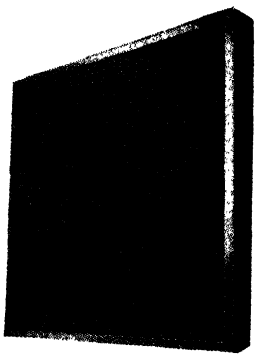
FILTERS FOR INTERNAL COMBUSTION ENGINES, COMPRESSORS, PIPE LINES; ALSO DUST COLLECTORS

Farr Company

Manufacturing Engineers

Los Angeles • California

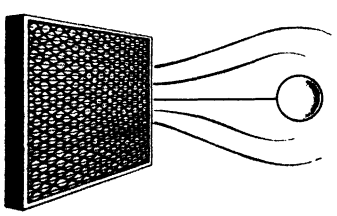
FAR-AIR FILTERS* FOR ALL TYPES OF INDUSTRIAL USE



FAR-AIR STANDARD PANEL FILTER
For Ventilation **For Grease**

Face velocity in f.p.m.	Capacity in c.f.m. per sq. in. of face area	Starting static pressure	C.F.M. CAPACITIES OF STANDARD FILTERS BASED ON VELOCITY USED			
			16"x20"	16"x25"	20"x20"	20"x25"
346	2.40	.06"	625	795	800	1020
390	2.70	.07"	700	895	900	1145
433	3.00	.09"	780	995	1000	1275
476	3.30	.10"	860	1095	1100	1400
519	**3.60**	**.12"**	**935**	**1195**	**1200**	**1530**
563	3.90	.14"	1015	1290	1300	1655
606	4.20	.16"	1090	1390	1400	1780
650	4.50	.19"	1170	1490	1500	1910
693	4.80	.20"	1250	1590	1600	2035

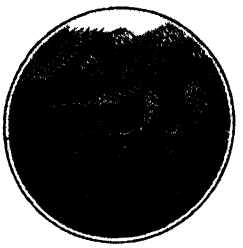
Based on our recommended face velocity of 519 fpm, Far-Air filters deliver 50 per cent more air with the same blower power. Filters are all metal, permanent construction . . . Installation of Far-Air Filters, effects a saving not only in initial costs but maintenance as well—you need only ⅔ of the filter area, with a Far-Air filter.



AIR FILTER TEST

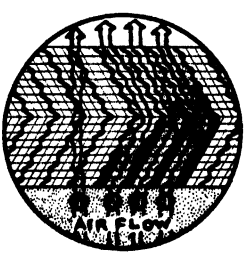
Farr Company has originated a simple procedure for testing air filter in place in order to determine the degree of efficiency. Write for information regarding this test.

*Trade Mark registered.



HERRINGBONE CONSTRUCTION

Far-Air filters' Herringbone design, which is a special cirmped wire type of construction, allows these filters to load progressively, which permits a dirt holding capacity two or three times greater. Each filter can handle 50 per cent more air with the same blower power, thus one-third fewer filters are needed to do the same job. No special equipment is needed for cleaning . . . a pressure hose and cold water. Far-Air filters can be cleaned in place. Of paramount importance to heating and refrigeration engineers is the fact that Far-Air Filters provide a filter area equal to the fin coil area. This special feature eliminates clumsy V-shaped additions on vent ducts usually necessary with other type filters.



PROGRESSIVE LOADING

As entering orifices of Far-Air Herringbone Construction Filters are loaded, air direction changes, flowing past the front loaded surface and progressively loading the clean screen mesh that remains. Greater free area permits a larger dust load with lower pressure drop. The small difference in pressure drop when a Far-Air Filter is loaded from when it is clean maintains a constant balanced air flow in the air distribution system.

For full information about other types of FAR-AIR FILTERS, write: FARR CO., Dept.H VG, 2615 Southwest Dr., LOS ANGELES 43, CALIF.

Raytheon Manufacturing Company

Commercial Products Division

Waltham 54, Mass.

RAYTHEON — *Excellence in Electronics*

RAYTHEON — *Excellence in Electronics*

Clean air as supplied by Electronic Air Cleaning reduces heating and cooling costs; reduces cleaning and redecorating costs; improves worker efficiency; improves product quality; and provides better conditions in which to work or relax. Only electronic air cleaning efficiently removes airborne particles as small as 1/250,000 in. in diameter.

RAYTHEON PRECIPITATORS

A COMPLETE LINE OF ELECTRONIC AIR CLEANERS

For industrial and commercial applications

INDUSTRIAL

Built up cell-type units for installation in ventilating and air conditioning systems.

Fully automatic, semi-automatic or manual washing.

Capacities 1200 cfm up.

See Bulletin DL-P-503.

RESIDENTIAL

The Raytheon Home **Precipitator**

Semi-automatically and fully automatically washed.

Capacities 1200 and 1800 cfm.

See Bulletin DL-P-509.

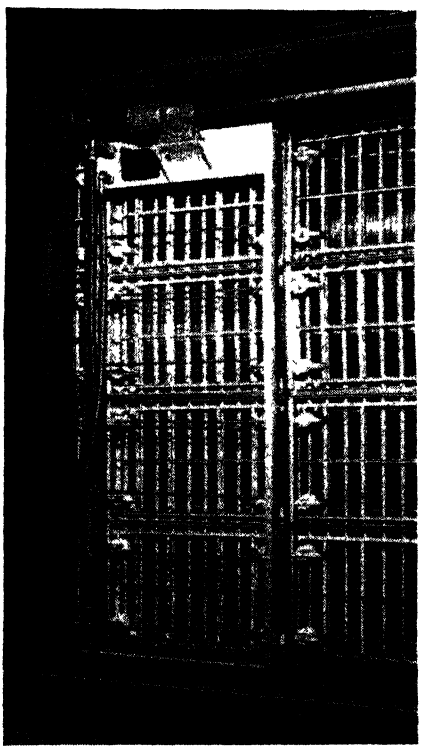
PACKAGED UNITS

For Industrial, Commercial and Residential Installations:—

Packaged, self-contained units. Fully automatic, semi-automatic, and manual washing.

Capacities 300, 1200 and 1800 cfm.

See Bulletin DL-P-505.



The new, fully automatic Raytheon Precipitator washes and dries all ionizers and collector plates, reapplies adhesive, shuts itself off. Operates without shut-down period—requires no cleaning maintenance whatsoever. In the picture above, baffle doors have been opened and louvres removed from the automatic washing unit to show construction details.

NOTE THESE IMPORTANT FEATURES

Ease of installation. Minimum maintenance. Minimum resistance to air flow. Economy of Operation. Flexibility—a size for every application. Quality products used throughout.

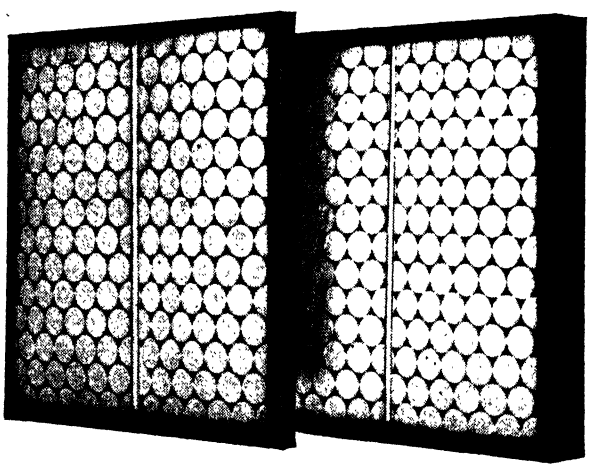
Owens-Corning Fiberglas Corporation

Toledo 1, Ohio

DUST STOP* **AIR FILTERS**

*REG. U.S. PAT. OFF.

—a FIBERGLAS* product



Dust-Stop Air Filters are replaceable impingement-type filters for use in all systems in which air is moved mechanically—central heating, ventilating and air-conditioning systems, and mechanically-circulated warm-air furnaces.

Dust-Stops provide high air filtering efficiency. They are constructed of packs of glass fibers (Fiberglas*), coated with an adhesive, faced with a metal grille, and bound on the edge with a fiberboard frame.

The Fiberglas fibers, packed to proper density, form an exceptionally effective medium for air filtration. Being glass, they are inorganic, chemically stable, resistant to heat and corrosive vapors. And being of glass, they do not absorb the nonodorous, nonevaporating adhesive with which they are coated. Each impinged particle of dust is quickly soaked, acting as a wick to carry adhesive to other particles. Thus, the adhesive remains effective until the filter is so heavily loaded with dust that resistance to air flow calls for replacement.

A minimum of manpower and time is required in replacing economical Dust-Stops—and they can be obtained quickly from near-by suppliers. Dust-Stops are made in two standard types: No. 1 (1 in. thick) and No. 2 (2 in. thick). Both are available in several sizes.

Owens-Corning Fiberglas Corporation Offices

ATLANTA, GA.
BOSTON, MASS.
BUFFALO, N. Y.
CHICAGO, ILL.
CINCINNATI, OHIO
CLEVELAND, OHIO
DALLAS, TEXAS
DETROIT, MICH.
HOUSTON, TEXAS
KANSAS CITY, MO.
LOS ANGELES, CALIF.
MILWAUKEE, WISC.
MINNEAPOLIS, MINN.
NEW YORK, N. Y.
PHILADELPHIA, PA.
PITTSBURGH, PA.
ST. LOUIS, MO.
SAN FRANCISCO, CALIF.
SEATTLE, WASH.
TOLEDO, OHIO
TULSA, OKLA.
WASHINGTON, D. C.

DUST STOP* AIR FILTERS AND FRAMES

*T. M. REG. U. S. PAT. OFF.

TWO TYPES OF FRAMES—

Dust-Stop Air Filters may be installed in banks of either "L" Type or "V" Type Dust-Stop Air Filter Frames. Both types of frames are designed, patented and manufactured by Owens-Corning Fiberglas Corporation for the convenient handling of Dust-Stop Air Filters.

The choice between "L" and "V" Type frames is determined by the frontal area available. The "L" Type frame requires less depth within the duct or plenum chamber but takes a larger face area than the "V" frame for the same cfm capacity. However, it can be set in various arrangements that reduce the required face area by increasing the depth.

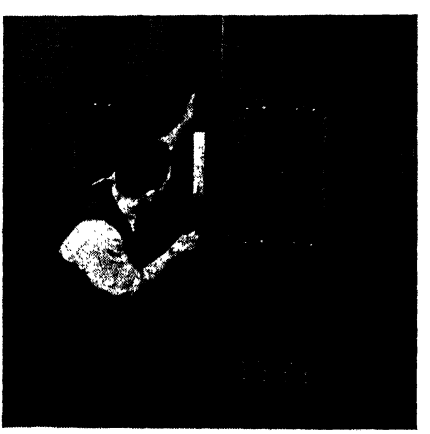
The "L" Type frame two filters deep is designed to hold two No. 1 Dust-Stop Air Filters in each cell. The "L" Type four filters deep holds four No. 1 Dust-Stop Air Filters (20 in. x 20 in.). "L" Type frames can be provided in any size from a single unit having one cell at a rated capacity of 800 cfm at a velocity of 300 lineal feet per minute to a unit consisting of 91 cells with a capacity of 72,800 cfm.

The "V" Type frame contains two "cells" each forming one side of the "V." Each cell will hold up to four No. 1 or two No. 2 Dust-Stop Air Filters. "V" Type frames take only the 20 in. x 25 in. filters. The "V" frames are available in any size from a single unit having a capacity of 2000 cfm to a 98 cell unit with a capacity of 98,000 cfm.

All frames are cold rolled steel and are shipped knocked down and crated, complete with all parts and instructions necessary for easy and rapid assembly.

Write for Catalog A5.2.1—"AIR FILTRATION IN CENTRAL SYSTEMS"

"L" Type Frame



"V" Type Frame

H. J. Somers, Inc.

6063 Wabash Ave., **Detroit 8, Mich.**

Agents in All Principal Cities

SOMERS Heavy Duty Industrial Filter

All Welded Vee Type
Patent No's. 2008800, 2130107

Somers Hair Glass Filters provide everything required in an efficient air-cleaning system.

Consider These Features:

- **High rating for dust, soot and bacteria separation.**
- **Require no adhesive, coating or impregnation.**
- **Indestructible in normal service.**
- **Minimum low-pressure drop.**
- **Odorless and non-absorptive.**
- **Fireproof.**
- **Washable.**
- **Permanent—Do not rot nor disintegrate.**
- **All welded zinc-plated 20 ga. steel frame.**
- **Metal protection strip on apex.**
- **Glass cloth between hot-dipped hardware cloth.**
- **Glass ribbon seal so air cannot short circuit.**

Somers Hair Glass Filters consist of a 20 gauge hot galvanized frame holding galvanized wire cloth packed with hair-spun glass strands. The glass strands are flexible, do not break up and cannot be drawn into air stream.

Hair Glass being chemically inert, has no facility of absorption; it cannot rust and lasts indefinitely in service. Water either hot or cold may be used to clean it, without impairing its efficiency.

These filters eliminate the necessity, the expense and the inconvenience of periodic replacement

SOMERS WASHABLE AIR FILTERS All Welded Vee Type Stock Sizes

Frame Size Height and Length	Frame Depth	Filter Surface Square Inches	For Average Dry Filter Installations	Wet Application
8″ x 12″	3 1/8″	288	288 C.F.M.	144 C.F.M.
12″ x 12″	2 7/8″	288	288 C.F.M.	144 C.F.M.
12″ x 20″	3 1/8″	720	720 C.F.M.	360 C.F.M.
15 1/2″ x 24 1/2″	3 13/16″	1023	1023 C.F.M.	511 C.F.M.
15 1/2″ x 24 1/2″	3 1/8″	1674	1674 C.F.M.	837 C.F.M.
15 5/8″ x 24 5/8″	2	480	480 C.F.M.	240 C.F.M.
15 5/8″ x 24 5/8″	3 1/8″	1110	1110 C.F.M.	555 C.F.M.
16″ x 20″	2	384	384 C.F.M.	192 C.F.M.
16″ x 21 1/2″	3	816	816 C.F.M.	408 C.F.M.
16″ x 25″	2	480	480 C.F.M.	240 C.F.M.
16″ x 25″	2 1/2″	624	624 C.F.M.	312 C.F.M.
16″ x 25″	3″	864	864 C.F.M.	432 C.F.M.
16″ x 25″	3 1/8″	1344	1344 C.F.M.	672 C.F.M.
16″ x 25″	3 1/8″	1440	1440 C.F.M.	720 C.F.M.
16″ x 25″	3 1/8″	1632	1632 C.F.M.	816 C.F.M.
16″ x 25″	3 1/8″	1056	1056 C.F.M.	528 C.F.M.
18″ x 18″	3 13/16″	864	864 C.F.M.	432 C.F.M.
18″ x 18″	3 1/8″	1134	1134 C.F.M.	567 C.F.M.
18″ x 24″	3″	1080	1080 C.F.M.	540 C.F.M.
19 1/2″ x 19 1/2″	2″	480	480 C.F.M.	240 C.F.M.
19 1/2″ x 19 1/2″	3″	819	819 C.F.M.	409 C.F.M.
19 1/2″ x 19 1/2″	3″	936	936 C.F.M.	468 C.F.M.
19 1/2″ x 19 1/2″	3″	995	995 C.F.M.	497 C.F.M.
19 1/2″ x 19 1/2″	3 1/8″	1053	1053 C.F.M.	526 C.F.M.
19 1/2″ x 19 1/2″	3 1/8″	1170	1170 C.F.M.	585 C.F.M.
19 1/2″ x 19 1/2″	3 5/16″	1696	1696 C.F.M.	848 C.F.M.
20″ x 20″	2″	480	480 C.F.M.	240 C.F.M.
20″ x 20″	2 1/2″	600	600 C.F.M.	300 C.F.M.
20″ x 20″	2 3/4″	780	780 C.F.M.	390 C.F.M.
20″ x 20″	2 3/4″	840	840 C.F.M.	420 C.F.M.
20″ x 20″	3″	960	960 C.F.M.	480 C.F.M.
20″ x 20″	3 1/16″	1020	1020 C.F.M.	510 C.F.M.
20″ x 20″	3 1/8″	1200	1200 C.F.M.	600 C.F.M.
20″ x 20″	3 1/8″	1320	1320 C.F.M.	660 C.F.M.
20″ x 20″	3 1/8″	1680	1680 C.F.M.	840 C.F.M.
20″ x 25″	2″	600	600 C.F.M.	300 C.F.M.
20″ x 25″	2 7/8″	1020	1020 C.F.M.	510 C.F.M.
20″ x 25″	3 1/8″	1560	1560 C.F.M.	780 C.F.M.
20″ x 25″	3 5/16″	1800	1800 C.F.M.	900 C.F.M.
20″ x 30″	3 1/8″	1800	1800 C.F.M.	900 C.F.M.
20″ x 30 1/2″	3 5/16″	2400x	2400 C.F.M.	1200 C.F.M.
23″ x 20″	3 1/8″	1656	1656 C.F.M.	828 C.F.M.
23 1/2″ x 23 1/2″	3 1/8″	1621	1621 C.F.M.	810 C.F.M.
23 3/4″ x 17 3/4″	3″	1068	1068 C.F.M.	534 C.F.M.
24″ x 25 1/2″	3 1/8″	1872	1872 C.F.M.	936 C.F.M.
25″ x 20″	3 1/8″	1800	1800 C.F.M.	900 C.F.M.
26″ x 23 1/2″	2 1/2″	936	936 C.F.M.	468 C.F.M.
26″ x 23 1/2″	2 5/8″	936	936 C.F.M.	468 C.F.M.
26″ x 34″	3 1/8″	2652	2652 C.F.M.	1326 C.F.M.
28″ x 33 1/2″	2 1/2″	1428	1428 C.F.M.	714 C.F.M.
29″ x 33 1/2″	3 1/8″	3045	3045 C.F.M.	1520 C.F.M.
30″ x 15″	3 5/16″	1800	1800 C.F.M.	900 C.F.M.
30″ x 20″	3 1/8″	1800	1800 C.F.M.	900 C.F.M.
30″ x 24″	3″	1800	1800 C.F.M.	900 C.F.M.
31″ x 23 1/4″	3 1/4″	3162	3162 C.F.M.	1581 C.F.M.

Other sizes also available. Send for complete stock size list.
Frames zinc plated for 100 hour salt water spray test. Refill may be inserted if necessary.
Quotations and further engineering data, including master holding frame drawings will be sent on request.

Just a *few* users of Somers Filters

Chemical Plants
American Viscose Co.
American Zinc & Chemical Co.
Davison Chemical Corp.

Automotive
Frederick Sterns Co.
Cadillac Motor Car Co.
Chevrolet Motor Car Co.
Chrysler Corp.
Fisher Body Corp.

Refrigeration and Air-Cond.
Frigidare Corp.
Norge Div.—Borg Warner
Kelvinator Corp.
York Ice Machine Co.

Ships
Amer. Shipbuilding Co.
U. S. S. Saratoga
U. S. N. Lake City, Fla.
U. S. N. Daytona Beach, Fla.
U. S. N. Vero Beach, Fla.
U. S. N. Jacksonville, Fla.

Utilities and Municipalities
City of Kenosha
Michigan Consolidated Gas Co.
Detroit Edison Co.
New York Edison Co.
Westchester Lighting Co.

Dep't. Stores
S. S. Kresge Co.
S. H. Kress & Co.

Food Processing
Awrey Bakeries
Gilbert Chocolate Co.
Kellogg Co.

Manufacturers
Buffalo Forge Co.
Burroughs Adding Machine Co.
Clarage Fan Co.
Curtiss-Wright Airplane Co.
Glensder Textile Co.
Hoover Co.
International Heater Co.
Kearney & Trecker Corp.
Killian Mfg. Co.
National Carbon Co., Inc.
Pittsburgh Plate Glass Co.
Rockford Machine Tool Co.
Sunstrand Machine Tool Co.

Research Products Corporation

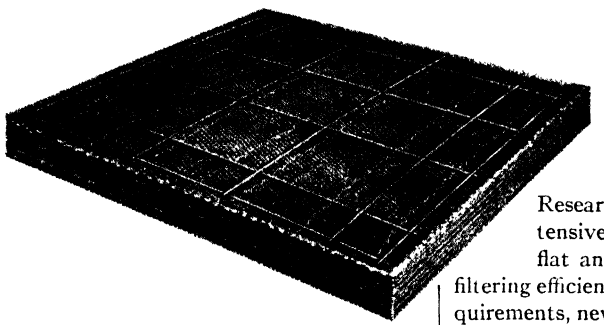
Madison 3, Wisconsin

RESEARCH AIR FILTERS FOR HEATING AND VENTILATING

U. S. Patent 2070073

U. S. Patent 2294478

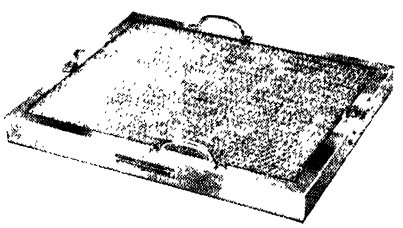
RESEARCH AIR FILTERS



Research Air Filters are widely used wherever air is moved mechanically in blown-air heating and air conditioning systems, in window ventilators and for protection of industrial equipment. Tests prove Research Air Filters have a 93 per cent dust removal efficiency (with 80-20 dust), 99 per cent ragweed pollen removal efficiency. The resistance build-up is very gradual.

Self-Seal Edge The time and labor saving **Self-Seal** edge is an exclusive Research Air Filter feature. The filtering media is a pad constructed of single sheets, cut, expanded and held together to form a honeycomb pattern of thousands of tiny baffles. This unique construction allows filter to be made slightly oversize, fitting snugly into place and eliminating all by-pass of air. When filter becomes dirt clogged, only the filter pad need be replaced.

Research Filter Banks. Research Air Filters are used extensively in filter banks—both flat and V types. For maximum filtering efficiency and minimum service requirements, new speedy **"Snap-in" grids** are used with filter pads, the removal of front grid only being necessary when changing pads.



Washable Alumaloy Filter. This filter has the same efficiency as the disposable type filter. It is about ⅓ lighter than most other washable type filters. Filter is cleaned by agitating in hot soapy water.

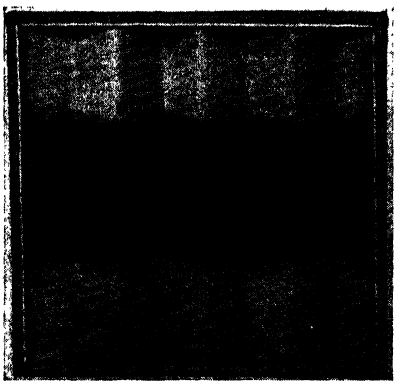
Alumaloy "Clean Duct" Grease Filter. All aluminum construction. Light weight. Easily cleaned. Retains high lustre appearance.

The Research Filter Watchman, a new automatic filter gauge, signals with light when filters are loaded to a maximum restriction to air flow; it may be set for any recommended resistance.

Supreme Air Filter Company

126 West 21st Street, **New York 11, N. Y.**

SUPREME WASHABLE DRY TYPE AIR FILTERS
AUTOMATIC OR MANUAL CLEANING



Supreme Air Filter (Before and after cleaning)

Supreme Air Filters are made of a spun glass filter media, annealed under a patented process, and covered with a galvanized or copper wire mesh 25-06, encased in a galvanized or copper frame.

Supreme Filters offer a low resistance to the free flow of air, are light in weight and easy to handle. All cells are equipped with handles and interchangeable in the same bank.

Supreme Filters are made in flat and sawtooth types: The flat filter is encased in a ½ in. frame, for convenience in ordering and lower cost production. The sawtooth type is corrugated the depth of the cell frame thereby increasing the filtering surface in a given area.

The spun glass in Supreme Filters is FIRE, ROT and VERMIN proof and not attacked by any chemical other than hydro-fluoric acid; it is approved by the Board of Fire Underwriters.

The important factor in rating a filter is generally not the removal of a certain per cent of dust by weight but rather the effectiveness for taking out certain objectionable constituents, which may be either the finest particles present or the coarser ones within a certain range. The lower number per cent of dust particles in buildings and out-of-doors occur just after air washing by rain or snow storm, and the greatest number in busy streets on dry days.

Supreme Filters can be washed in hot or cold water, adding a little soap powder or solvent, and spraying with not over 25 lb water pressure.

New mats can be supplied for all Supreme cell frames where mats become worn out or defaced, thereby saving the cost of a new frame, which has patent pending.

TABLE OF SUPREME AIR FILTER SIZES

Sizes	C.F.M.	Mat. SQ"	EFFY	Pd, W.G.	Sizes	C.F.M.	Mat. SQ"	EFFY	Pd, W.G.
1"					3"				
16" x 20"	480	480			16" x 20"	1500	1500		
16" x 25"	480	480	94.5	.14"	16" x 25"	1500	1500	97.1	.18"
20" x 20"	480	480			20" x 20"	1500	1500		
20" x 25"	480	480			20" x 25"	1500	1500		
2"					4"				
16" x 20"	800	800			16" x 20"	2000	2000		
16" x 25"	800	800	95.7	.16"	16" x 25"	2000	2000	98.0	.20"
20" x 20"	800	800			20" x 20"	2000	2000		
20" x 25"	800	800			20" x 25"	2000	2000		

Some Users of Supreme Air Filters

B. Altman Company
Bendix Radio Corporation
Bethlehem Steel Corporation
Christ Hospital
Colgate Palm Olive Peet Company
Commercial Bank & Trust Company
Conde Nast Company
Dime Savings Bank
E. I. DuPont deNemours & Co., Inc.
Fifth Avenue Hotel
Garment Capital Center
Geigy Dye Works
Koss Restaurant
Masonic Temple
Modern Industrial Bank
New Amsterdam Theatre
New York Central R. R.
New York Telephone Bldg. Corp.
New York Trust
Ohio Power Company
Pabst Air Condg. Corp.
Panama Steamship Line
Posi Print Works
Riegel Paper Corp.

Supreme Air Filters have been approved by the Maritime Commission for use on the C-2 ships.

Gulf Shipbuilding Co.
Moore Dry Dock Co.
Mantowac Shipbuilding Co.
U. S. S. A. So. Africa
International Tel. & Tel.
Colonial Trust Co.
Western Electric Company.

Write Supreme Air Filter Company for complete information and prices

Westinghouse Electric Corporation
Sturtevant Division

Air Conditioning, Heating, Ventilating, Dust Control and Fume Removal Equipment, Electronic Air Cleaners, Dryers, Compressors, Mechanical Draft Equipment

Hyde Park **Boston 36, Mass.**

Westinghouse-Sturtevant Division Manufactures a complete line of air conditioning, heating, ventilating and air handling equipment. Shown here is a selection of the complete line. Individual product catalogs are available where more detailed information is required on any item.

Sturtevant Puts Air to Work

Equipment designed to "Put Air to Work" is available for all commercial and industrial buildings, to improve comfort and efficiency and to provide industrial process air conditioning. Applications range from the small ventilation and air conditioning systems to the large specially engineered installations.

Engineering Assistance

Sturtevant offers unbiased engineering assistance in the selection of the correct product for the specific application.

Many years of experience in the design and manufacture of these products combined with the benefits of close co-operation with consulting architects and engineers, assure you of reliable recommendations.

Offices and Distributors are located in all principal cities. Refer to your local classified telephone directory.

REFRIGERANT COMPRESSORS

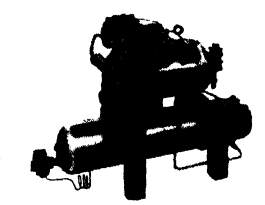
Hermetically-Sealed, Freon 12, Type CLS refrigerant compressors are designed for air conditioning and industrial refrigeration applications requiring suction evaporating temperatures ranging from 10°F to 50°F.

Westinghouse Special Features include:

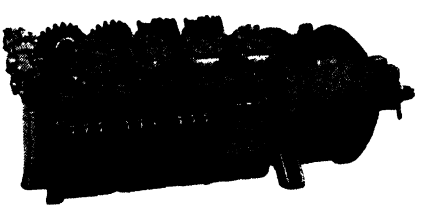
1. Shaft seals eliminated.
2. Direct drive—no belts, pulleys and couplings.
3. Sealed-in mechanism.
4. Refrigerant-cooled motor.
5. Compact size and light weight.

The hermetically-sealed compressors are reciprocating multi-cylinder, in-line type in sizes 7½ to and including 60 hp; 90 deg V-type on the 2, 3, 5, 75 and 100 hp sizes. They are protected by manually reset high and low pressure switch. Driving motors are polyphase, refrigerant-cooled induction type. Motors are protected by thermal overload protection in the De-ion magnetic linestarters.

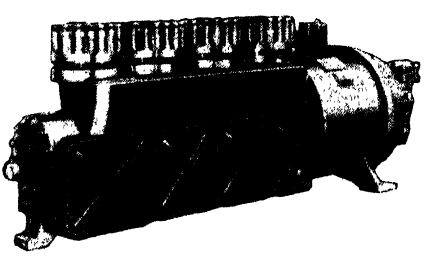
Mounting supports are available to permit mounting the compressor and suitable Westinghouse water-cooled condenser as a unit. Type CLS compressors are made in 12 sizes ranging in nominal capacities of from 2 to 100 tons refrigeration effect.



Two-Cylinder V-Type Compressor



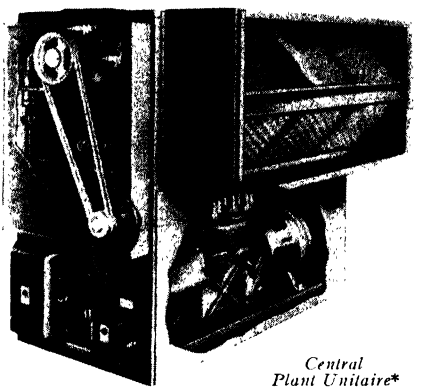
Sixteen-Cylinder V-Type Compressor



Six-Cylinder In-Line Type Compressor

Westinghouse Electric Corporation
Sturtevant Division

UNITAIRE*
AIR CONDITIONING UNITS

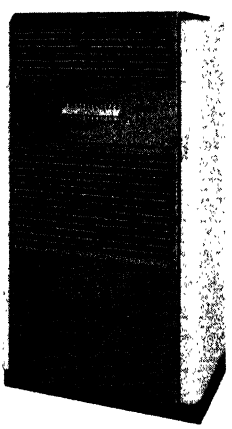


*Central Plant Unitaire**

Central Plant Type Unitaires are completely self-contained, with all the component parts of an air conditioning system, designed especially for installation with supply and return air ducts. Unitaires are completely assembled, piped, refrigerant-charged, wired and adjusted at the factory. Each is given a complete operating test to assure satisfactory performance when installed. All that is required is connection of water and electrical service and attachment to the duct system.

The condensing unit is a standard Westinghouse hermetically-sealed, direct-connected compressor, with water-cooled condenser, isolated from the supporting structure by rubber anti-vibration mountings.

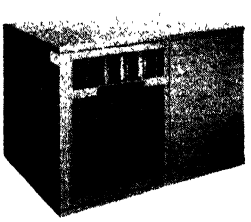
Central Plant Type Unitaires are available with 7½, 10, 15, 20 and 25 hp compressors.



Self-Contained Unitaire, Type SU*

Self-Contained Type Unitaires are widely used in small stores, restaurants, office suites and similar establishments. Usually they are installed in the room to be air conditioned, but in many cases they are remotely located with ducts supplying one or more spaces with air conditioned air. Available in sizes of 1, 2, 3 and 5 hp. Westinghouse Unitaires offer many important features:

1. Compact Size—Largest unit occupies less than 7 sq ft of floor space; smaller units often installed on shelves.
2. Attractive Appearance.
3. Completely Factory-Built.
4. Flexible Application.
5. Westinghouse Hermetically-Sealed Compressor.
6. Quiet Operation.



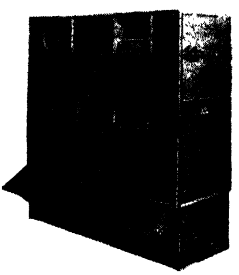
Self-Contained Unitaire, Type CU*

*Reg. U. S. Pat. Off.

Westinghouse Electric Corporation
Sturtevant Division

EVAPORATIVE CONDENSERS

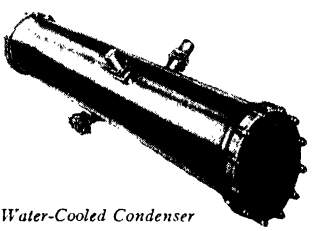
Where water is scarce or expensive, or its use or disposal restricted, the "Aquamiser" provides savings in water consumption. Westinghouse Aquamisers are available in sizes to give a range of capacities from approximately 5 tons to 100 tons each, net refrigeration effect.



"Aquamiser" Evaporative Condenser

WATER COOLED CONDENSERS

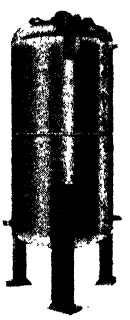
Where sufficient water is available from city water supply to cooling tower the water-cooled condenser is economical and efficient. To economically match refrigeration load requirements, Westinghouse water-cooled condensers are available in 14 sizes, ranging in nominal capacities from 2 to 100 tons net refrigeration effect.



Water-Cooled Condenser

WATER CHILLING UNITS

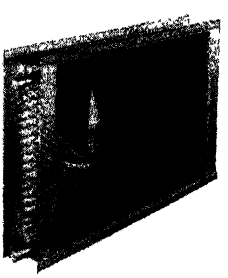
For the chilling of water for distribution to a number of cooling coils, for surface dehumidifiers and for use in industrial processes, these efficient water-chilling units range in size from 5 to 110 tons net refrigeration effect. The chiller, located close by the compressor, eliminates long refrigerant piping or long duct runs.



Water Chilling Unit

HEAT TRANSFER SURFACES

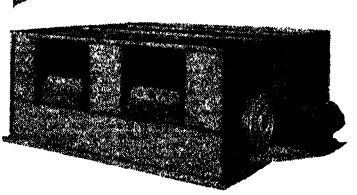
Direct expansion coils with patented refrigerant distributor, chilled water coils, steam and hot water coils are available in a great many sizes for all types of systems.



Heat-Transfer Surface

AIR CONDITIONING UNITS

Two types are available—a horizontal type for ceiling suspension and a vertical type for floor installation. In the horizontal and vertical types, year-round air conditioning is accomplished by the installation of cooling and dehumidifying surfaces for summer, and heating surfaces for winter air conditioning.



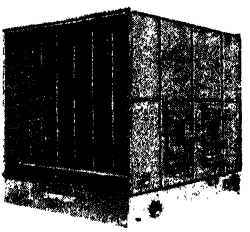
Air Conditioning Unit, Type AH

Westinghouse Electric Corporation
Sturtevant Division

AIR WASHERS

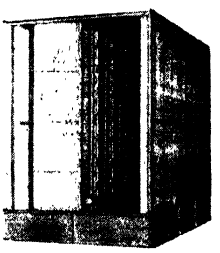
Three types are available—Type H, with one bank of nozzles, used primarily for humidifying; Type C, with two banks of nozzles, used for evaporative cooling. humidifying and dehumidifying; and Type S, with one bank of nozzles, used for humidifying, especially where space is limited.

Air Washer



FILTER-WASHERS

Self-cleaning filter-washers employ a bank of mineral wool, or glass fiber filter pads, in conjunction with water sprays to clean and humidify the air. Made in 72 standard sizes and to specifications.

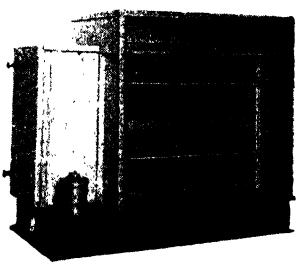


Filter Washer

SURFACE DEHUMIDIFERS

Available for either chilled water or directly expanded refrigerant, these wet surface units control accurately wet and dry bulb conditions in industrial and comfort air conditioning systems. Capacities range from 2000 to 50,000 cfm, with cooling capacities of 5 to 250 tons of refrigeration.

Unit Dehumidifier



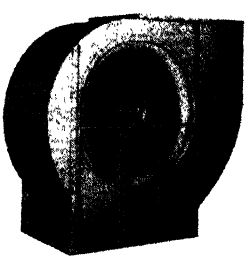
CENTRIFUGAL FANS

Silentvane*, Design 8, are high speed, exceptionally quiet heating and ventilating fans engineered for installations where fan noise cannot be tolerated. Made in 21 sizes with rotors from 12¼ in. to 87¾ in. in diameter, they operate from free delivery to 4 in. water gage static pressure, and at a maximum tip speed of 9000 feet per minute. Capacities range from 700 to 400,000 cfm.

Silentvane Centrifugal Fan Design 8*

Multivane, Design 6, high capacity, low speed fans, suitable for use in public buildings because of low tip speed, low outlet velocity, and small size for a given duty. With wheel diameters up to 87 in., they operate against static pressures up to 4 in. water gage, and at a maximum tip speed of 6000 fpm. Capacities range from 400 to 450,000 cfm.

Multivane Centrifugal Fan, Design 6

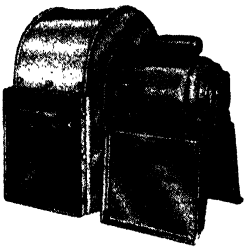


*Reg. U. S. Pat. Off.

Westinghouse Electric Corporation
Sturtevant Division

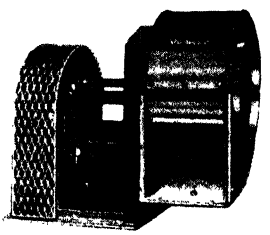
VENTILATING SETS

Rexvane* Ventilating Sets, with radial blade wheels designed for medium speed operation, are suitable for ventilating, fume exhausting and air conditioning. Rexvane Ventilating Sets are made in 7 sizes, wheel diameters from 6 in. to 17⅛ in. capacities to ¾ in. water gage static pressure, and air delivery to 4000 cfm.



Rexvane Ventilating Set*

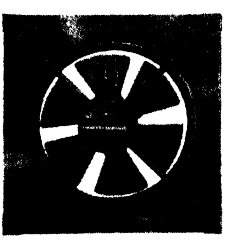
V-Belt Ventilating Sets are completely self-contained units consisting of Multivane fan and motor with V-belt drive. These sets are particularly suitable for a wide variety of heating, ventilating and air conditioning applications. Wheel diameters from 12 in. to 24 in., and air deliveries from 930 to 11,000 cfm.



V-Belt Ventilating Set

PROPELLER FANS

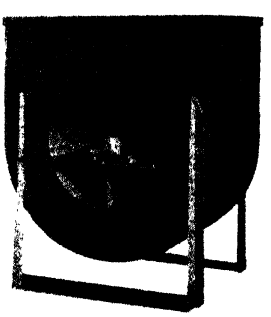
Propeller Fans, Design 7, with direct connected motors, are generally applicable to all air exhausting or ventilating problems when unit blows air directly outdoors or to another room, without ducts or high resistance to air movement. Motors are totally enclosed special fan duty type. Design 7 Propeller Fans are made in 7 sizes, from 12 in. to 36 in. diameter, and 815 to 11,050 cfm.



Elbow Axiflo Fan*

AXIFLO* FANS

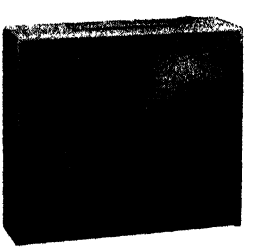
Axiflo pressure fans are axial flow type especially designed to meet industrial service requirements. They are available in straight through or elbow types, with either three-bladed aluminum or eight-bladed steel wheels. All designs or arrangements can be used in either vertical or horizontal position.



Air Blender

AIR BLENDERS

Widely used for central air conditioning and ventilating systems in commercial buildings, the Air Blender mixes cool dehumidified air or heated humidified air from a central system with predetermined quantities of recirculated air to maintain room temperatures for both winter and summer, air conditioning. It has no moving parts, and is equipped with a booster coil for winter operation. All units are built with 7 in. front-to-back dimensions, and in nominal lengths of from 18 in. to 60 in.



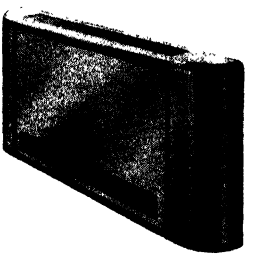
Propeller Fan, Design 7

*Reg. U. S. Pat. Off.

Westinghouse Electric Corporation
Sturtevant Division

UNIT VENTILATORS

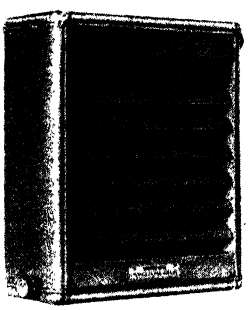
Unit Ventilators, filter, heat and circulate air through room areas. Each unit is equipped with heating coil, a fresh air inlet, motor driven fans, and controls, all enclosed in an attractive steel cabinet. Available in classroom models, or in auditorium type units for heating gymnasiums, auditoriums, and similar large room areas.



Unit Ventilator

SPEED HEATERS

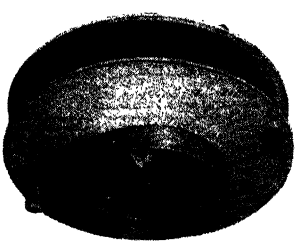
Sturtevant Speed Heaters, Design 14, are suspended type unit heaters adaptable to commercial and industrial installations to provide an even flow of heat over a large area. They are available in capacities of 25,800 to 300,500 Btu, and 398 to 5200 cfm. Attractive modern design makes Speed Heaters suitable wherever appearance is important. Their quiet, efficient operation fits them ideally for locations where economical, thorough speed heating is desired.



Speed Heater

DOWNBLAST SPEED HEATERS

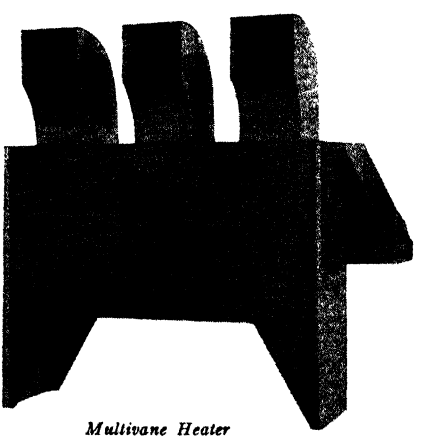
Downblast Speed Heaters are suspended type unit heaters for use with steam or hot water systems. They are designed for installation near the ceiling and are available in capacities of 40,000 to 400,000 Btu, and 695 to 5800 cfm. Downblast Heaters project the heated air downward to the working level, resulting in outstanding heating performance in buildings with high ceilings, or wherever it is necessary to project heated air downward between storage bins and other obstructions.



Downblast Speed Heater

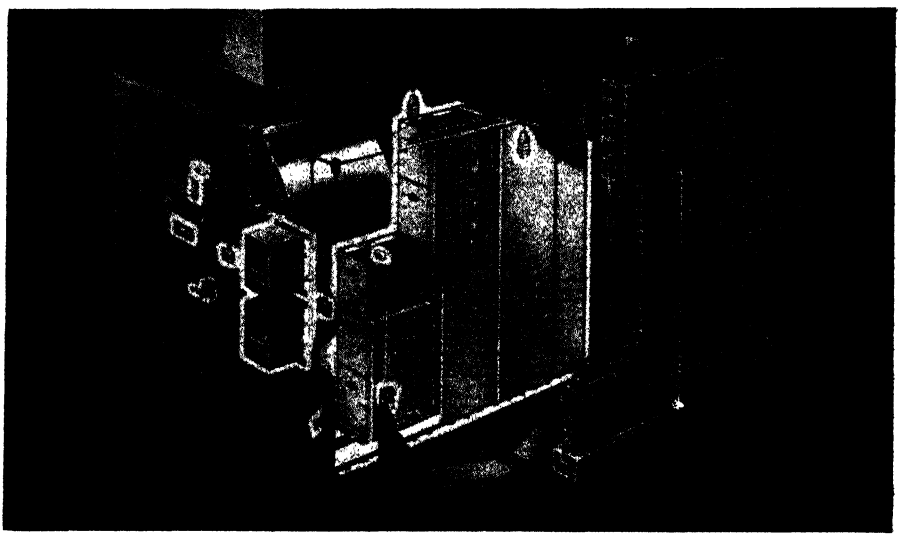
MULTIVANE HEATERS

Multivane Heaters are large capacity type for large area, severe heating jobs. They can be installed on floors, fastened to walls, hung from ceilings. Air motivation mechanism consists of multiple slow speed Multivane Fans, mounted on a common shaft—resulting in large volumes of air handled at low outlet velocity, low horsepower consumption, and quiet operation. Capacities range from 157,200 to 1,191,000 Btu, and 2100 to 18,000 cfm.



Multivane Heater

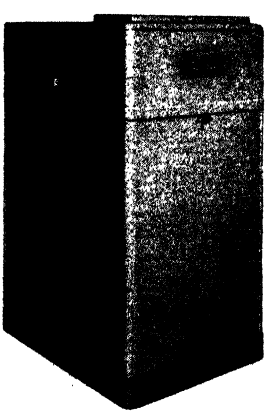
Westinghouse Electric Corporation
Sturtevant Division



PRECIPITRON*

Westinghouse Precipitron—the electronic air cleaner—makes possible greater efficiency in removing dust, dirt, smoke and other foreign particles from the air. The Precipitron cells are installed in the ventilating systems (see illustration above). Dust, smoke and soot pass through an electrostatic field, receive a charge, and are drawn to collector plates of opposite polarity where they remain until flushed down the drain.

Home Unit



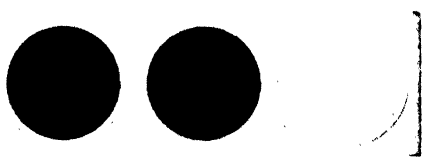
The Westinghouse Precipitron Home Unit is designed primarily for use in homes. It performs the same function, on a smaller scale, as the larger units do for commercial and industrial applications. No longer a luxury, the Westinghouse Precipitron electronic air cleaner minimizes the endless chasing of dust and dirt in the home.

It is comparable in size to a gas-fired furnace, and occupies about the same floor area. Provision is made on the unit for connection to the duct work of a forced air heating or air conditioning system. Placed in the air intake to the heating unit, the Precipitron removes more than 99.5 per cent of the dirt (by weight), and more than 90 per cent of all air-borne particles.

*Reg. U. S. Pat. Off.

Tests Prove Efficiency

Accepted testing methods previously conducted on a weight basis have been obsoleted since Precipitron entered the field of air cleaning. The Blackness Test reproduced here provides greater accuracy, approximates the actual particle count and is made without the addition of artificial dust. The efficiency of Precipitron by Weight Test showed over 99 per cent and by the Blackness Test as high as 90 per cent at air velocity of 300 fpm through the cells.



Uncleaned Air *Mechanically Cleaned Air* *Electrically Cleaned Air*

Test Comparisons Proving High Efficiency of Precipitron

Cells

The cell itself, known as the Collector, is composed of two duplicate sets of high voltage and ground plates mounted between two load-bearing end plates laced together by steel bars, angles and channels to form a rigid structure.

Precipitron is built in sizes to handle from 1200 cfm (for a single 24 in. cell) to any desired volume through multiple cell arrangements. Cells are available in two sizes: 24 in. x 24 in. x 26½ in. and 36 in. x 24 in. x 26½ in. For 90 per cent efficiency, the 24 in. and 36 in. cells are rated at 1200 and 1800 cfm respectively. For 85 per cent efficiency, ratings are 1500 and 2250 cfm.

Ionizers

Ionizing section is made of formed sheet steel, top, bottom and side plates welded together to form a rigid frame. The ground tubes run vertically between the top and bottom plates. Two sets of Ionizing wires are used; one, the usual vertical set, and another set stretching horizontal at the ends to prevent leakage around the ends of the vertical wires.

Power Packs

The Power Pack is employed to change the a-c supply to d-c of suitable voltage to charge the Ionizers and Collector Cells. They furnish approximately 6000 volts d-c to the plate circuit of Collector Cells and 13,000 volts d-c to the Ionizer circuit.

The Power Packs include an indicator system and safety device. Three types of Packs are available:

Type L—Suitable for 4 to 16-36 in. cells.
Type S—Suitable for 1 to 5-36 in. cells.
Type M—Suitable for 1-24 in., 2-24 in., 1-36 in., or 1-24 in. and 1-36 in. cell.

All Power Packs are designed to operate from 115 volts ±5 volts on single phase a-c systems.

AUTOMATIC WASHER

Traveling Header

The basic element of the automatic washer is a set of spray nozzles which spray either water, compressed air or adhesive on the Precipitron cells. Water nozzles are mounted on a horizontal header and a mechanism is provided to move this header vertically up and down over the face of the cells. The secondary element of the washer is the control of its automatic operation which is described under "Control Panel."

Illustration below shows complete header with back vanes closed, the washing being done with vanes in this position as air is prevented from going through this group and forced through the balance of the cells where it is cleaned.

Header is moved by means of roller chains driven through a gear reducer by a ½ hp 220-440 volt, 3 phase motor. A limit switch controls up and down travel of header.

Control Panel

This panel operates the two traveling headers of the washer automatically once they have been placed in position on either side of the cell group to be washed and the momentary contact push-button on the panel has been pushed.

Control Panel comes fully assembled, is internally wired and ready to be set in place. The control circuit requires 115 volts single-phase of sufficient capacity to carry a ¼ hp motor. The power circuit requires either 220-volt or 440-volt, 3-phase, power of sufficient capacity to handle two ½ hp motors in reversing service.

Control Panel

Travelling Header

April Showers Company

4126 Eighth Street, N.W. **Washington 11, D. C.**

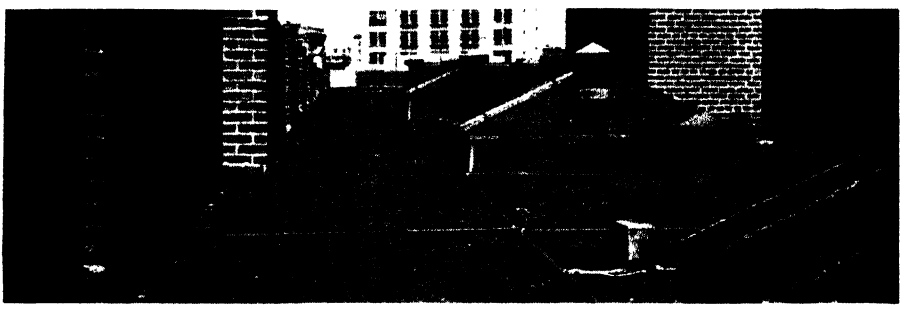
April Showers

(Trade Mark Reg. U. S. Pat. Office)

AUTOMATIC EVAPORATIVE ROOF COOLING

Distributors and Dealers in Principal Cities

SPRAY PROTECTION AGAINST SOLAR RADIATION



U. S. Government Office Building COOLED with APRIL SHOWERS

SURFACE COOLING has many converts. **THESE 1946** installations show the trend toward space cooling by the sprayed surface method. Hundreds of installations, from Boston to Los Angeles have been made. The systems are automatic, and very little water is required:

Victor Mfg. & Gasket Co., Chicago	103,000 sq ft of roof
Country Life Press Corp., Garden City, L. I.	90,000 sq ft of roof
Hallicrafters Co., Chicago	140,400 sq ft of roof
Lily Tulip Cup plant (Westinghouse air conditioned) Augusta, Ga.	104,000 sq ft of roof
Ponemah Mills, Taftville, Conn.	52,015 sq ft of roof
Harris Covington Hosiery Mills, N. C.	19,390 sq ft of roof
John E. Lucey Co., Bridgewater, Mass.	14,877 sq ft of roof
Gering Products Co., Kenilworth, N. J.	23,000 sq ft of roof
Aerojet Engineering Corp., Azuza, Calif.	22,000 sq ft of roof
Pennsylvania Central Airlines, D. C. Airport	22,500 sq ft of roof
Remington Rand Corp. Store, Washington, D. C.	8,500 sq ft of roof

and many others.

Write for Descriptive Literature *No Obligation for Estimate*

A FEW DEALERSHIPS STILL OPEN

APRIL SHOWERS is the trade name of an EFFICIENT fool proof method of preventing roof heat penetration or solar infiltration causing excessive heat in upper floors and in factories, stores, theatres, shops, etc.

City water under normal city pressure is usually adequate to serve your APRIL SHOWERS system. The sun operates it. Roofs LAST LONGER, greater comfort is assured, production during the summer's heat is kept apace, errors through fatigue are avoided, and MANAGEMENT acclaims APRIL SHOWERS a GOD-SEND.

Developed in 1933-34.

APRIL SHOWERS controlled roof cooling is protected by U. S. Patents; beware of imitators or infringers. USED BY AIR CONDITIONING ENGINEERS to cut solar load.

APRIL SHOWERS new residence heads now ready.

Foster Wheeler Corporation

165 Broadway, New York 6, N. Y.

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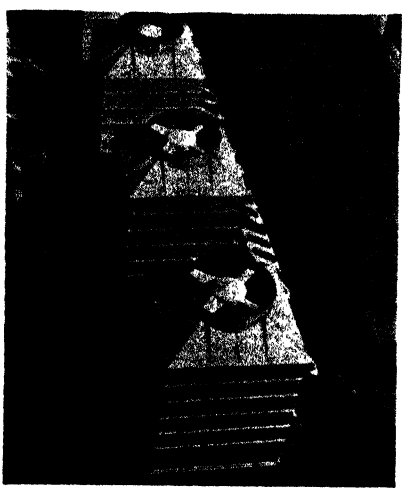
SAN FRANCISCO • WASHINGTON, D. C.

Cooling Towers

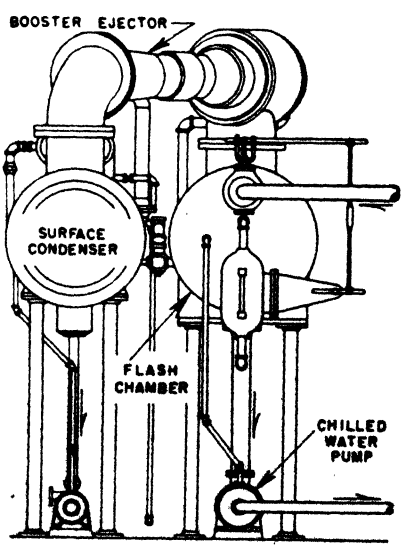
Foster Wheeler engineers have had wide experience in the design and construction of high-efficiency cooling towers for service under any climatic conditions. FW towers have been constructed all over the world to meet the cooling requirements of a variety of industrial needs, such as those encountered in chemical plants; public utilities; textile manufacture; office buildings and department stores; and oil refineries. Careful study of each proposed installation is undertaken before recommendations for the most suitable tower are given.



Left: Three of five induced draft towers installed in 1933 on the roof of the R. H. Macy department store in New York City. The first two towers cool circulating water for the condenser of a turbine; the other towers, only one of which is shown, cool water used in Macy's air conditioning system.

Vacuum Refrigeration

Schematic diagram showing arrangement of a typical vacuum refrigeration system. These systems, which cool water by subjecting it to high vacuum, supply chilled water for air conditioning or refrigeration. When a sufficient quantity of steam is available, vacuum refrigeration systems have several outstanding advantages—low initial cost; low maintenance cost; no toxic, explosive refrigerants; and, exclusive of pumps, no moving parts. Entire units designed and constructed by Foster Wheeler.



The Marley Company, Inc.

Fairfax and Marley Roads, **Kansas City 15, Kansas**

Representatives in All Principal Cities (Consult Classified Telephone Directory)

Water Cooling Towers of All Types and Capacities. Spray Nozzles

Marley Non-Clog Spray Nozzles

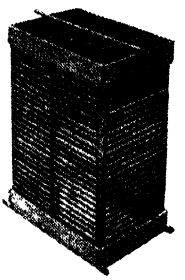
Low pressure tangential inlet with high speed whirl and uniform fine spray.

Two-Piece Nozzle for all cooling and spraying. Readily cleaned.

One-Piece Nozzle for cooling towers, spray ponds; large capacity.

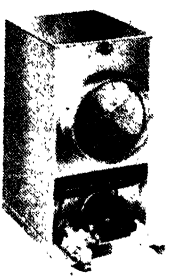
Atomizing Nozzle for humidifying, vaporizing; a "mist-like" spray.

ATMOSPHERIC SPRAY TOWERS



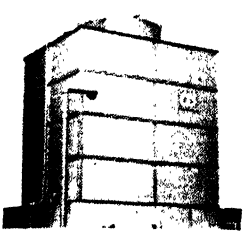
Marley Atmospheric Towers are designed for lowest cost, high efficiency installations on roof or ground where breeze is unobstructed. They are easily installed, simple and economical to operate. No fans, motors or other moving parts are employed. All are sturdily constructed from durable wood for long, trouble-free life. These towers owe their efficiency to the use of Marley low pressure spray nozzles and distribution systems. They are made in a wide range of closely graduated sizes and are shipped complete with necessary hardware, ready to erect.

MARLEY AQUATOWERS



Completely self-contained, these new "packaged-unit" cooling towers are the latest product of Marley's constant research and development program. Each Aquatower contains a built-in pump of ample capacity driven by the fan motor. Pump may be omitted if desired. Their small over-all space requirement permits installation in limited areas indoors or out. Aquatower capacities range from 3 to 15 tons of refrigeration. Shipped completely assembled, entire unit may be placed in operation by making electrical and hot, cold and make-up water connections.

SMALL SERIES VERTICAL STEEL



These attractive induced draft steel cased towers are specifically designed for medium capacity refrigeration and air-conditioning service. Small Series Vertical towers are equipped with Marley Triple Effect eliminators, Marley low pressure spray nozzles and distribution system. They are prefabricated and piece-marked for simplified field assembly. V-belt fan drive is standard equipment for all models. Marley Geareducers are available for larger capacity towers.

MARLEY DOUBLE-FLOW TOWERS

For large capacity installations, Marley patented Double-Flow Towers are designed to provide maximum efficiency and flexibility.

J. F. Pritchard & Co.

Fidelity Building, **Kansas City 6, Missouri**

New York, Pittsburgh, Houston, Tulsa, Los Angeles
Representatives in Other Principal Cities

Engineers—Constructors—Manufacturers for the Refrigerated Industries
Specialized Equipment for Use with Refrigeration and Air Conditioning

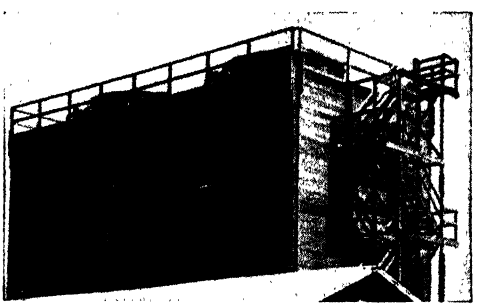
ENGINEERING-CONSTRUCTION

Many years of experience, covering large plants and small, all types of cold storage and refrigeration processing, qualify Pritchard to handle complete plants, revamps or additions, from plans to operation, on a full-responsibility turn-key basis that saves time and money. Any *part* of the complete Pritchard service (process designing, economic studies, plant layout, unit installations, etc.) is available separately.

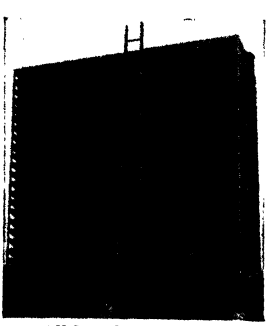
AIR TREATER—Renders Air Germicidally Pure—Removes Dust, Pollen, Smoke and Other Solid Particles and Microorganisms—Controls Humidity—A compact "package" unit for easy installation.

AIR & GAS DRYING EQUIPMENT—Total or Controlled Dehumidifying—Adaptable for Various Solid or Liquid Adsorbents—Standard units, all capacities, automatic or manual regenerating.

HEAT EXCHANGERS AND CONDENSERS—All types of heat transfer apparatus, high or low pressure, shell and tube, atmospheric or submerged, standard or special designs. Pritchard has facilities and application knowledge to meet any need.



Induced Draft Cooling Tower



All-Metal Spray Tower

Indoor Forced Draft

COOLING TOWERS—Pritchard has long been one of the foremost suppliers of cooling towers of all types and capacities. Specifications, prices, ratings and application recommendations furnished promptly.

Small Mechanical Draft Towers—Forced or induced, for indoors or out. Self-contained steel-cased units, easy to install, 2-ton capacity and up.

Natural Draft Spray Towers—With or without deck filling, with or without basins. Simple to assemble; slip-fit louvers; Redwood or all-metal; any capacity.

Natural Draft Deck Towers—Celebrated Pritchard "drift retrievers" minimize drift loss without restrictive secondary louvers. Free air flow gives higher efficiency. Rugged construction; low-pressure, uniform water distribution.

Induced Draft Towers—Extra-sturdy structural members and joints; double-wall casing. Valuable exclusive features include "Featherweight Fans" of wrought monel, superior air delivery per horsepower; trouble-free gear drives, either right-angle type with flex-coupled shaft to motor outside of fan ring or the famous "Sealdflow" unit streamlined to the fan hub, mounting motor and gears vertically on the fan shaft; low pumping head, uniform water distribution.

ALL-MONEL COOLING TOWER FANS—No gears, belts or couplings. Spherical hub houses slow-speed ball-bearing motor, lubricated for life, suspended in the fan ring by hollow vanes which ventilate the motor and guide the air stream. 36 in. to 96 in. diameters, avoid costly problems common to ordinary fans. Available as replacements, any make.

"AIRDFIN" AIR-COOLED HEAT EXCHANGERS—New efficiency and economy for many cooling and condensing functions, i.e., steam and other vapors, jacket water, oils, gases, quenching baths, etc. High-efficiency fan propels air through banks of finned tubes. No water problems.

Refrigerating Machinery Co.

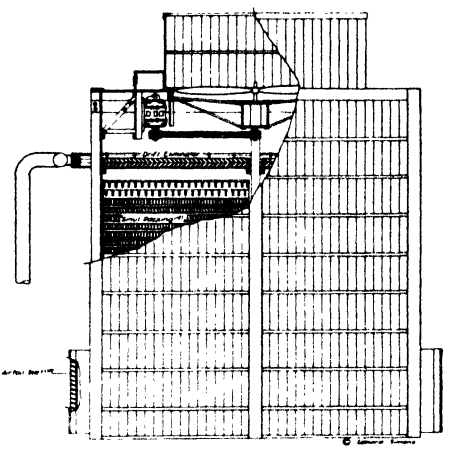
HEAT TRANSFER EQUIPMENT

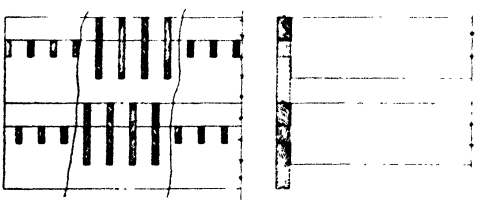
525 Market Street, **San Francisco 5, California**

Distributors in Principal Cities

INDUCED DRAFT TOWER

Designed for modern requirements in 50 stock sizes from 75 to 2,000 gpm capacity. Equipped with multiple fans and of cell type construction for simplicity in erection and maintenance. Exclusive features permit compactness, low pumping head and automatic control of off peak loads. Structurally engineered by timber experts. Metallic connectors and tie rods concealed. Double sheathed. Fabrication at Nulco plant in the Redwood Empire.





SINUL PACKING

(Pat's. Pending)

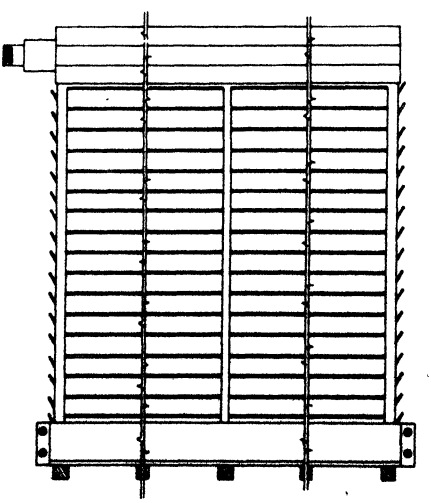
Constructed of California Redwood in stout self aligning mats, this efficient surface is responsible for the compactness and low pumping heads of R.M.C. Cooling Towers. Protected against warping and rigid enough to support workmen, it is a gravity packing not dependent on metal fastenings. When combined with Sinul Airfoil Inlet (Pat. Pend.) low static pressures are achieved.

ATMOSPHERIC COOLING TOWERS DECK TYPE

In 43 stock sizes from 4 ft x 4 ft x 6 ft to 6 ft x 28 ft x 20 ft. All units plant fabricated for k.d. shipment with hardware, drawings and erection instructions.

Recommendations and prices for unusual applications furnished promptly.

Write for "Handbook of Cooling Tower Selection"



Water Cooling Equipment Company

8613 New Hampshire Avenue

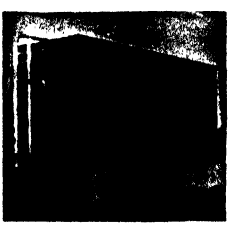
Affton Station, St. Louis 23, Missouri

MANUFACTURERS OF MECHANICAL DRAFT AND ATMOSPHERIC COOLING TOWERS

FORCED DRAFT COOLING TOWER

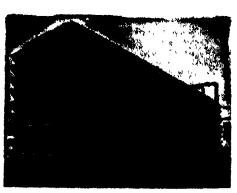
41,500 gpm, twenty-two cell, heavy duty, double forced draft cooling tower . . . equipped with twenty-two 12-foot diameter adjustable pitch, propeller type fans.

REDWOOD "WATERFALL" ATMOSPHERIC SPRAY COOLING TOWER



Factory fabricated and shipped knocked-down with all hardware, spray headers and spray nozzles. Complete erection instructions and drawings are furnished to assist in the assembly of the tower.

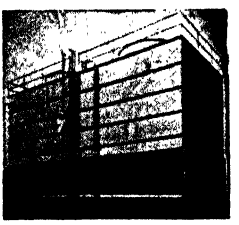
These towers are portable and can be knocked-down and moved simply by removing the louvres and bolts. Shipment can be made from stock. Write for Bulletin 125-A.



REDWOOD ATMOSPHERIC DECK TYPE COOLING TOWER

PRODUCTS

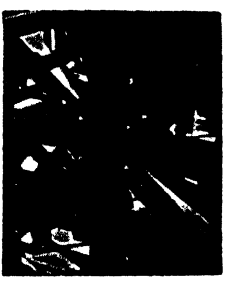
Heavy duty forced and induced draft cooling towers, standard induced and forced draft towers, induced draft coil towers, atmospheric deck cooling towers, atmospheric spray towers, spray ponds and spray nozzles.



INDUCED DRAFT

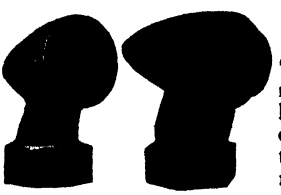
This type of cooling tower is recommended for installations where noise is a prime factor of consideration. The noise of the mechanical items is carried upward and discharged into the air. The mechanical draft cooling tower assures a positive cooling of the water to a specified temperature independent of wind velocity.

TIMBER JOINT CONNECTOR



Special cast iron timber joint connector used to develop the full strength of the timber joint, an accomplishment almost impossible to achieve by bolting.

Patent No. 2,280,121



Patent No. 2,123,697

SPRAY NOZZLES

"Whirlcone" non-clogging, low pressure, centrifugal type spray nozzles for spray ponds, spray towers and other uses. Write for Bulletin 76-A.

ENGINEERING

Design and construction are based on sound engineering principles to meet specific requirements for cooling performance and structural strength. Redwood, steel or other suitable materials are used.

American Moistening Company

ESTABLISHED 1888

Providence 1, R. I.

ATLANTA 2, GA. BOSTON 9, MASS. CHARLOTTE 1, N. C.

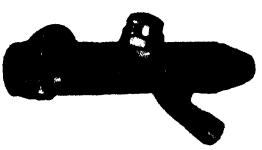
AMCO

UNIT HUMIDIFYING AND AIR CONDITIONING EQUIPMENT

A few of many AMCO products with a Long Record of Dependable Performance

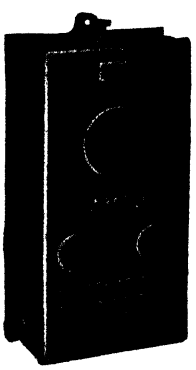
Self-cleaning Atomizers.
Sectional Humidifiers.
Ideal Humidifiers.
Amtex Humidifiers.
Hand Sprayers.
Fabric and Paper Dampeners.
Electro Psychrometers.
Sling Psychrometers.
Hygrometers.
Mine Sprays.

The Amco line of devices for the supply, maintenance and control of humidity is complete in its ability to meet any presented problem of applied humidification. Used independently or as an adjunct to Central Station equipment, these devices automatically maintain any required humidity condition in a capable uniform performance.



AMCO ATOMIZER—No. 5

Quality and quantity of spray are maintained even under adverse conditions because this atomizer is automatically self-cleaning. When the compressed air supply is shut off, either manually or in response to a humidity control, *both* air and water nozzles are thoroughly cleaned.



AMCO HUMIDITY CONTROLS

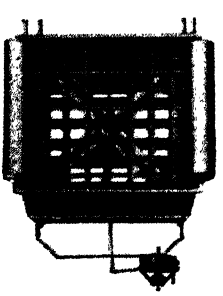
Compressed Air Operated

An extremely accurate and active device operated by compressed air which assures a regulation of humidity within exceedingly close ranges.

AMCO HUMIDITY CONTROL

Electrically Operated

Similar in principle to the Compressed Air Type except that the hygroscopic element operates electrical contacts which control the units.



AMCO EVAPORATIVE COOLING UNIT

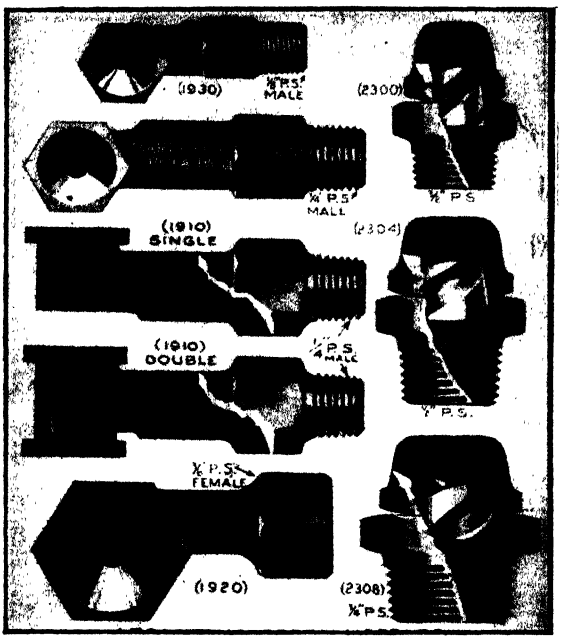
The Amco System of evaporative cooling contributes to smooth production at high speeds in two ways; it maintains the percentage of relative humidity best suited to the fibre and process involved, and at the same time promotes the comfort and efficiency of personnel by obtaining the maximum practical cooling effect from evaporation. It does this by introducing outside air into the room in varying amounts, regulated in accordance with climatic conditions and inside requirements.

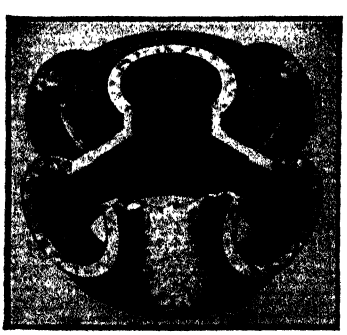
A ductless system—very flexible and portable. Can be applied in conjunction with an existing humidifying system.

Jos. A. Martocello & Company

229-31 North 13th Street, **Philadelphia, Pa.**

SPRAY POND AND ATOMIZING SPRAY NOZZLES





MARTOCELLO

Atomizing Spray Nozzles produce a uniform, good, wide spray with less friction and at minimum pressure requirements.

Nozzles illustrated at the right are manufactured with precision in Brass Forgings and Bar Stock. Their design has been thoroughly tested for results and durability and will give you satisfaction.

Successful, Efficient Results depend largely upon selecting the proper number and type of Nozzles with Brass or Monel cap suitable for your job. Therefore we suggest you send us your specifications as we also have several Types other than illustrated and we will gladly assist you to obtain the most efficient application.

MARTOCELLO

Spray Pond Nozzles of a sturdy one-piece construction —cast of High Grade Red Brass with Inlet and Outlet accurately machined, are less clogging, offer less friction and give unsurpassed overall efficiency.

MARTOCELLO CLUSTER CASTINGS

Sturdy Grey Iron Construction with large area for reduced friction and even distribution. They are Hot Dipped Galvanized after fabrication.

Furnished with **Nozzles** and continuous Standard Steel **Long Sweep** Galvanized Pipe **Spray Arms** and **Center Nozzle** Nipple in accordance with layout required.

Sizes Carried in stock for **Prompt Shipment** 1½ in. P. S. Outlet, 3 in. P. S. Inlet and 2 in. P. S. Outlets, 4 in. P. S. Inlet Cluster Castings.

WRITE, PHONE OR WIRE

For Bulletin listing Capacities and Prices. Prompt shipments from stock.

Monarch Manufacturing Works, Inc.

2509 E. Ontario St., **Philadelphia 34, Pa.**

SPRAY NOZZLES FOR WATER AND OIL

NON-CLOG AIR WASHER NOZZLES

produce an exceptionally efficient, evenly distributed hollow cone spray. Single large tangential inlet to swirling chamber minimizes any possibility of clogging. Also available in ⅜ in. to 1 in. pipe sizes inclusive, and of Brass, Stainless and Monel.

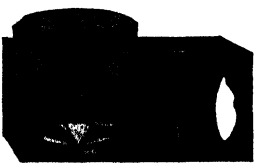


Fig. 631

Capacities: Gallons per Hour

Sizes		Lb Operating Pressure			
Pipe	Orifice	10	20	30	40
¼"	69			5.3	6.15
	61		6.25	7.5	8.3
	61 x 53	5.7	7.5	8.8	10.0
	53	6.4	9.0	10.7	11.8
	3/32	14.1	18.7	22.5	25.0
	⅛	23.2	32.0	40.	47.3
	11/64	31.0	43.9	54.5	63.0
	3/16 x 3/32	45.0	64.2	75.0	90.0
	7/32" S	73.4	105	137	155
	7/32	85.8	116	140	164

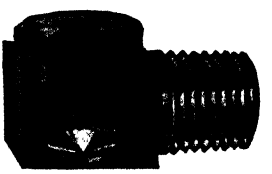


Fig. 629

AIR CONDITIONING AND OIL BURNER NOZZLES

Water Capacity in Gallons per Hour

Fig. F-80

Nozzle No.	Lb Operating Pressure				
	25	40	60	80	100
1.35		.57	.69	.83	.92
1.65		.75	.89	.99	1.12
2.00		.94	1.14	1.28	1.40
2.50		1.13	1.45	1.64	1.86
3.00	1.03	1.39	1.62	1.85	1.95
3.50	1.36	1.77	2.11	2.46	2.80
4.00	1.56	2.00	2.42	2.77	3.16
4.50	1.86	2.32	2.77	3.21	3.68
5.00	2.20	2.88	3.57	4.09	4.59
5.50	2.22	2.96	3.75	4.31	4.78
6.00	2.55	3.35	4.01	4.78	5.23
7.00	2.90	3.91	4.60	5.17	6.00

Produce finest breakup possible with direct pressure only. Capacities above are on water. "Nozzle No." is capacity on 34 second Saybolt viscosity oil at 100 lb pressure. Larger sizes up to Nozzle No. 60.00.

Furnished of all Brass for Water—Stainless Steel tip and disc for Oil. Standard with ⅛ in. or ¼ in. female pipe Brass adapter and Monel gauze strainer.

SPRAY POND NOZZLES

For recooling condenser water, etc. Operate on pressures from 5 lb upward. Made of Cast Red Brass and in pipe sizes 1 in., 1½ in., 2 in., and 2½ in. Capacities from 4.1 to 88 gpm at 7 lb pressure.

Write for Detailed Catalogs

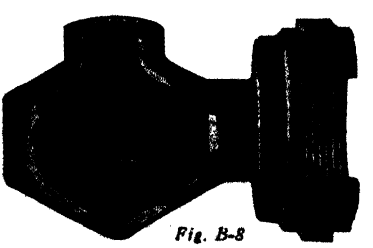


Fig. B-8

Acme Industries, Inc.

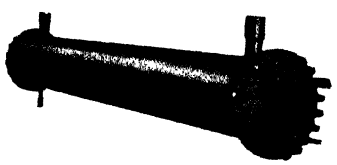
Jackson, Michigan

Representatives in Principal Cities

REFRIGERATION AND AIR CONDITIONING EQUIPMENT

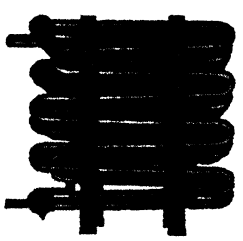
FREON CONDENSERS
AMMONIA CONDENSERS

Shell and Tube Type for use with Ammonia, Freon or other refrigerants. Standard or special designs to meet varying water temperatures available and condensing temperatures desired.



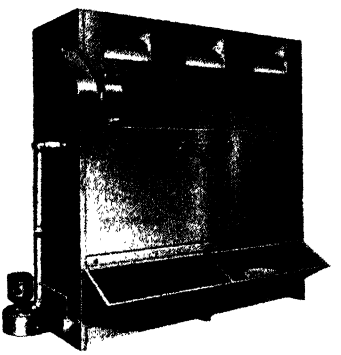
DRY-EX COOLERS

Refrigerant in tubes, solution baffled through shell. For cooling water, brine, glycols or alcohols by direct expansion of refrigerant.



PIPE COILS

Fabricated in all shapes and sizes from ½ in. IPS to 2 in. IPS. Special assemblies available for custom built evaporative condensers, raceway coils.

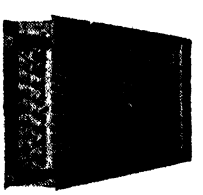


EVAPORATIVE CONDENSERS

All prime surface for Freon and Ammonia refrigerants. Heavy gage sheet metal casing, especially processed for maximum resistance to rust and corrosion. Capacities to 100 tons.

HEAT INTERCHANGERS

Shell and coil units for small capacities. Shell and tube units for large installations. 16 standard models from one ton to 180 tons capacity.



FIN COILS

Direct expansion coils with liquid distribution for Freon. Low temperature, wide fin spacing all steel coils hot dip galvanized for flooded ammonia.

Acme Industries, Inc. also manufactures flooded water and brine coolers, receivers, oil separators and lowside specialties.

WRITE FOR CATALOG ON ANY PRODUCT

AEROFIN CORPORATION

410 So. Geddes Street

Syracuse 1, N. Y.

AEROFIN

Standardized Light-weight Heat Exchange Surface

Branch Offices

CLEVELAND, CHICAGO, NEW YORK, PHILADELPHIA, DETROIT, DALLAS, TORONTO

Aerofin is the modern Standardized Light-Weight Encased Fan System Heating and Cooling Surface originated by *Fan Engineers* to meet the present and future requirements of this highly specialized field. All Standard AEROFIN Units are furnished as completely encased Units, ready for pipe and duct connections. The patented casings are built of pressed steel and are exceptionally strong and rigid, protecting the Unit from all the strains of pipe connections and expansion or contraction in service. The casings are flanged on both faces, top and bottom, and template punched for bolting together adjacent Units, or for duct connection.

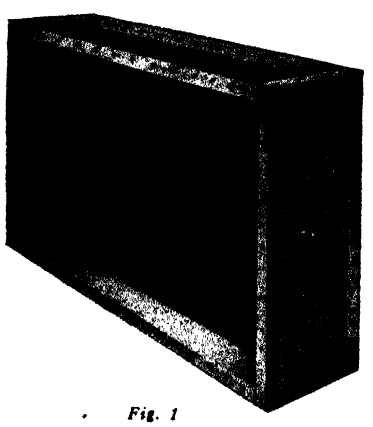


Fig. 1

Aerofin Non-freeze heater (Fig. 1) is non-freeze, non-stratifying spiral fin coil built into casing for air conditioning units or for installing in ducts. May be installed horizontally or vertically. Used on any two-pipe steam system for preheating or reheating. Modulating control on preheaters.

Available in 13 lengths and 3 widths, from net face area of 2.76 sq ft to 26.28 sq ft.

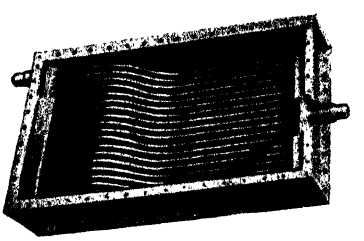


Fig. 2

Flexitube Aerofin (Fig. 2) is distinguished from all other developments by its off-set tubes, so arranged as to absorb all expansion and contraction strains.

Headers—Steel.

Tubing—⅝ in. O.D. copper, admiralty or aluminum.

Joints—Where admiralty or copper tubes are used together with bronze or steel headers tubes are brazed to headers. Where both aluminum tubes and headers are used tubing is welded to headers.

Casings—Copper, aluminum or galvanized iron.

Design—Constructed with headers on opposite ends making possible installation of units with tubes horizontal or vertical.

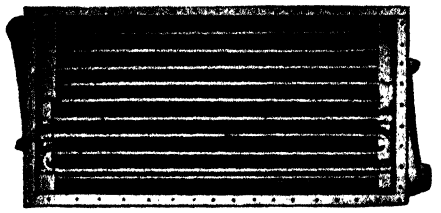


Fig. 3

Universal Aerofin (Fig. 3) is distinguished by its "S" bend construction of tubing, units designed with steel headers on opposite ends, the ends of the "S" bends being connected thereto by compression nuts, the bends taking care of the expansion and contraction of the tubing.

Recommended where close control is desired.

Headers—Pressed steel.

Tubing—1 in. O.D. copper or admiralty.

Casings—Copper, aluminum or galvanized iron.

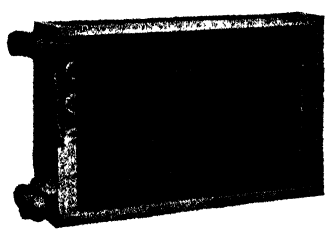


Fig. 4

Aerofin Heavy-Duty Industrial Heating Coil for use where extra-rugged coil is needed for close control. Steam pressures from 25 to 350 lb gauge; temperatures to 500 F.

Headers—Pressed steel.

Tubing—1 in. O. D. heavy copper.

Casings—12-gauge galvanized iron.

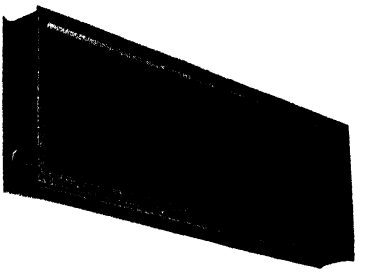


Fig. 5

Booster Aerofin—straight tube type, single pass construction for pressures from 1 to 200 lb gauge.

Headers—steel.

Tubing—$\frac{5}{8}$ in. O.D. copper.

Casings—copper, aluminum or galvanized iron. Recommended where small coils are needed or to raise the air temperatures in branch ducts.

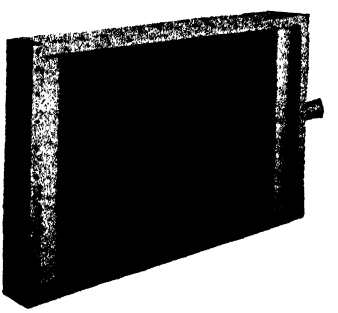


Fig. 6

Narrow Width Aerofin: (Fig. 6) recommended for water cooling or for flooded Freon systems. Made in straight tubes only with headers on opposite ends, joints between headers and tubing being brazed. Construction similar to Flexitube AEROFIN.

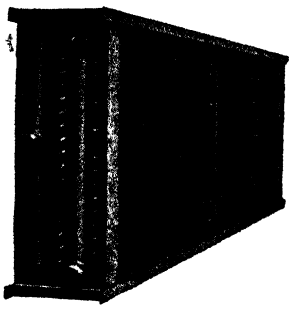


Fig. 7

Aerofin Continuous Tube Water Coils (Fig. 7) are designed for air cooling by circulating cold water through the AEROFIN and air over extended fin surface. Made for either horizontal or vertical air flow.

Tubes and fins are copper, completely tinned with permanent metallic bond between fin and tubes. Headers are made of steel and casings of heavy galvanized iron or copper.

Tested to 100 lb steam, followed by 450 lb air with coil submerged in water.

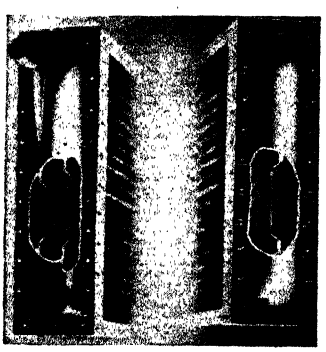


Fig. 8

Aerofin Cleanable Tube Units (Fig. 8) for cooling only made with headers removable to permit cleaning tubes. Recommended for use where sediment or scale forming chemicals are present in the cooling water.

Headers—Cast iron.
Tubing—Copper or admiralty.
Casings—Copper or glavanized iron.

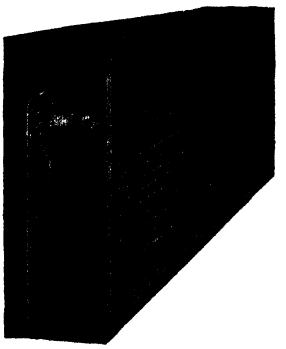


Fig. 9

Aerofin Direct Expansion Units: (Fig. 9) Centrifugal Header Type—For cooling air, using Freon expanded directly into the coil.

AEROFIN Sizes

Flexitube: 13 standard lengths, three widths, one and two rows deep.

Narrow: same as Flexitube.

Universal: 17 standard lengths, two widths, one and two rows deep.

Continuous Tube: 13 standard lengths, three widths, 2-3-4-5 and 6 rows deep.

Cleanable Tube: 17 standard lengths, one width, 2 and 4 rows deep.

Direct Expansion: Centrifugal Header—11 standard lengths, three widths, 2-3-4-5-6 rows deep.

Steel Supporting Legs: 18 in. and 24 in. high. Punched same bolt hole centers as standard casings. Quickly attached. No other foundation required.

Sale: AEROFIN is sold only by manufacturers of nationally advertised Fan System Apparatus. List upon request.

Write Syracuse for Heating Bulletin G-32; Direct Expansion Bulletin DE-34 on refrigeration type units; Continuous Tube Bulletin C. T. 34 for Water Cooling Coils; or phamplet on Cleanable Type AEROFIN for cooling.

Condenser Service & Engineering Co., Inc.

65 River Street
HOBOKEN, N. J.

ELIZABETH, N. J.
POTTSVILLE, PA. SCRANTON, PA.
EDGEMOOR, DEL.

DESIGNERS AND MANUFACTURERS OF

Steam Generators—Steam Condensers—Steam Jet Air Ejectors—Lubricating Oil Coolers—Feedwater Heaters—Fuel Oil Heaters—Evaporators—Distillers—Oil Refinery Heat Exchangers—Process Industry Heat Exchangers—Strainers—Feedwater Filters—Grease Extractors—Sewage Ejectors—Pumps—Oil and Water Separators—Wizard Condenser Injectors—Flowrites—Salinometer Cocks—American Ball Steam Engines.

Twenty years of specialized experience *designing*, building, fabricating and a special feature—a designing organization which also services heat exchangers—assures sound design, quality construction and economical operation. Conseco builds heat exchangers for all types of air conditioning systems using, Freon, CO_2, ammonia, methyl chloride and SO_2.

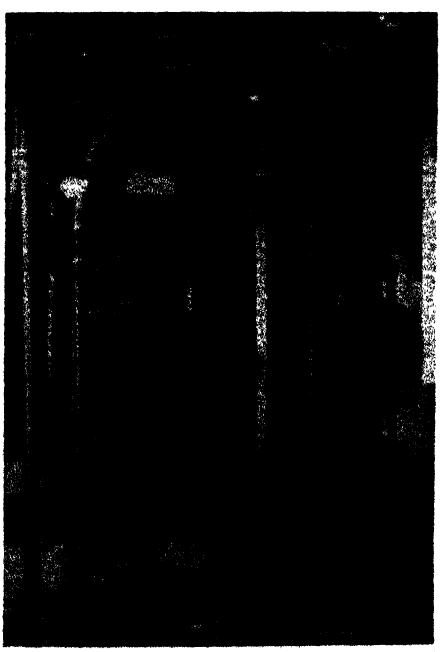
Conseco maintains a highly-trained service organization equipped with special tools developed by us to save time, labor and material, ready for action any time of day or night, anywhere on the continent. Heat exchangers are retubed or repaired in the shortest possible time, and at low cost. Tube sheets, tubes, ferrules, all types of packing, and other necessary materials are always stocked, ready for instant shipment.

The keynote of our service organization is fast, accurate, dependable service performed by competent, properly equipped men working under qualified engineering supervision.

Every detail of a Conseco heat exchanger is designed to profit from good and bad features uncovered by years of service work on units of every type and make. This has resulted in the production of simple, efficient units, low in original cost and inexpensive to maintain.

Conseco engineers will be glad to serve you. If you want fast action, write, phone or wire.

Conseco heat exchanger installation for ammonia service aboard ship.



Conseco CO_2 heat exchangers operating at 1900 psi replaced double tube type in various Sanger theatres.

Conseco CO_2 heat exchanger installation, Stanley Theatre, Philadelphia, replaced double tube unit shown above it.

The G & O Manufacturing Company

138 Winchester Avenue **New Haven, Connecticut**

G&O

SQUARE FIN TUBING

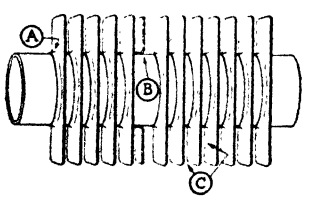
STRAIGHT LENGTHS—U-BENDS—CONTINUOUS COILS

THE use of INDIVIDUAL fins results in high efficiency in heat transfer from primary tube surface to secondary fin surface.

Fins of any size or shape may be obtained giving any desired proportion of primary and secondary surface.

A square fin has about 30 per cent greater surface than a round fin of a diameter equal to one side of the square.

Individual fins permit of any fin spacing; also, of using fins in groups at intervals along tubes.



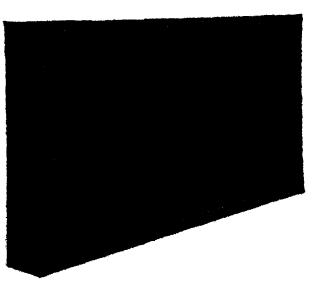
A—Generous Fin Collar provides large contact area between Tube and Fin.
B—Tube expanded against Fin Collar; insures mechanically tight joint, made permanent by bond of high temperature alloy—complete thermal contact.
C—Free air-flow passages; non-clogging.

STANDARD SIZES

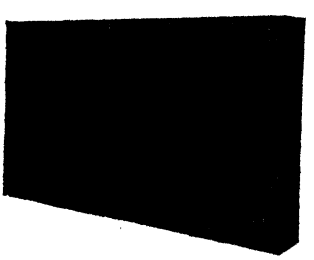
O.D. of Tube	Fin Size	Fin Spacing per Inch	Surface per Linear Foot
3/8"	7/8" sq.	6	0.80 sq. ft.
3/8"	7/8" r'd.	6	0.60 sq. ft.
5/8"	1 1/8" r'd.	6	0.87 sq. ft.
3/4"	1 1/2" r'd.	6	1.55 sq. ft.
3/4"	1 5/8" sq.	6	2.40 sq. ft.
1"	2 1/8" sq.	6	4.00 sq. ft.
1 3/8"	2 3/8" r'd.	4	2.33 sq. ft.

RADIATING ELEMENTS FOR ALL HEAT TRANSFER PURPOSES

G&O Finned Radiation Coils for industrial applications are available in a wide range of sizes.



Universal U-102



Standard No. 10

Send for Catalog and Price List

Shaw-Perkins Manufacturing Company

Pittsburgh 19, Pa.

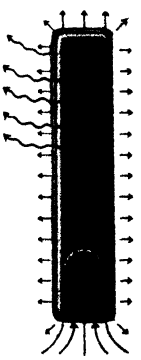
RADIATORS

Developed far beyond ordinary types of radiators and convectors, the Shaw-Perkins units have brought to radiation pleasing appearance and greater operating economy. Users have been particularly impressed by their highly efficient heat distribution. Installed in homes, ships, hospitals, office and industrial buildings.

The Shaw-Convector Radiators

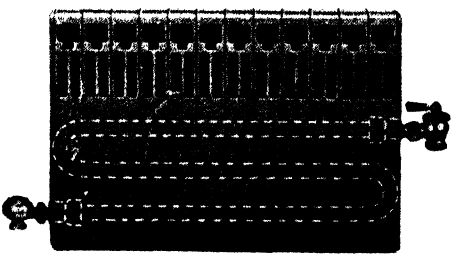
The Shaw Convector-Radiator is an attractive self-contained unit requiring no cabinet or expensive recessing. Occupies little floor space and harmonizes with modern decoration.

Designed to operate on high or low pressure steam or forced hot water. Frequently the high pressure steam feature alone justifies its selection for with such an installation smaller heating units and piping are required resulting in considerable installation and operating savings.



Wide air spaces between smooth steel fins induce the movement of large volumes of low temperature air thereby assisting in the fast and even distribution of heat through the room.

Because of its high heat output, it combines sturdy construction with a weight less than half that of ordinary exposed radiators of the same capacity.

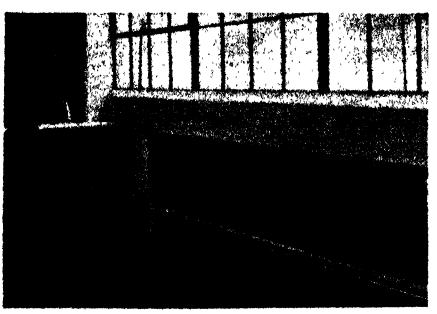


The Shaw Construction

The heat from the steam or hot water contained in the copper tube is conducted through all the steel radiating fins over which large quantities of low temperature air pass constantly and joins with the radiant heat from the exposed metal surfaces to produce a quick and economical form of comfortable warmth.

The Perkins-Convector Radiators

A Modern Industrial Heating Unit for High or Low Pressure Steam



Perkins Radiator installed in a Pittsburgh laboratory

This Advanced Radiator embodies a heavy copper tube arranged in the form of a continuous coil to which are mechanically bonded a series of steel plates, the whole assembly being locked into a rigid unit by a combination of tie rods and spacers.

The Perkins convector-radiator has been designed to move large volumes of low temperature air in order to produce quick, uniform, economical heating. The amount of air is greater than that of other types of radiators.

It is designed for operation on either high or low pressure steam. At high pressure the heat emission is greatly increased, so there is a reduction in the number of heating units and auxiliary equipment. Furthermore by modulating the pressure of the steam, the heat output of these radiators may be made to balance the heat loss of the building under varying conditions, resulting in a remarkable steam economy.

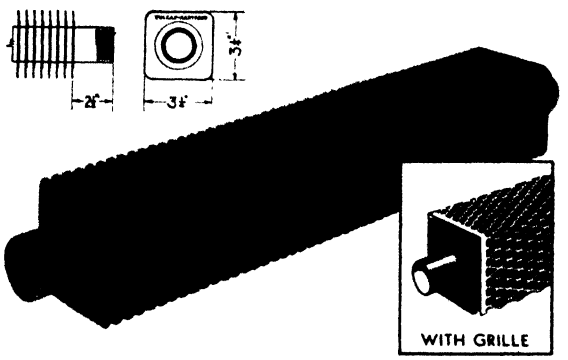
Representatives in principal cities. Send for catalog.

The Vulcan Radiator Company

26 Francis Avenue **Hartford 6, Conn.**

MANUFACTURERS OF FINNED TUBES FOR OVER TWO DECADES

Vulcan Radiation is used in railroad cars, ships, hospitals, schools, churches, homes and industrial plants. Available in steel or copper . . . easy to install . . . light in weight . . . requires few fittings and supports . . . pipe ends threaded or chamfered for welding. Heat distribution is uniform. Steel radiation comes in two sizes . . . 2 in. IPS, rated—5¼ sq ft per lineal ft at 1 lb steam and 70 deg air . . . for 1¼ in. IPS see illustration—this size also available in copper.

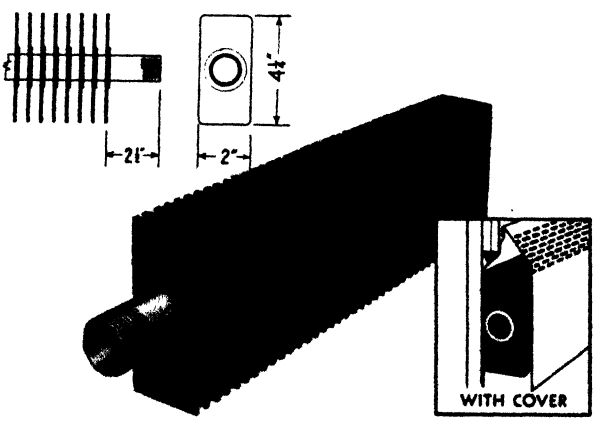


1¼ in. IPS, rated—4¼ sq ft per lineal ft.

Vulcan Radiation is fabricated by mechanically imbedding offset fins or plates on a tube or pipe. The patented offset fin construction gives complete rigidity to the entire assembly and extends the heating surface of the tube.

Because of its comparatively light weight and compactness, Vulcan Radiation responds quickly to thermostatic control. Full heat output is obtained almost immediately after steam is supplied. Since most of the heat is given off by convection, the result is EVEN, UNIFORM HEAT from floor to ceiling.

Vulcan Baseboard Radiation . . . fin - on - tube construction with grille covers combines radiant and convection heating. High safe working pressure . . . either hot water or two-pipe steam systems. Light in weight . . . easy to install . . . requires few fittings or supports. Comes in two sizes . . . 1¼ in. IPS . . . steel fins 2¾ in. wide by 3¾ in. high. Rated 4.0 sq ft per lineal ft. For 1 in. IPS see illustration.



1 in. IPS . . . steel fins 2 in. wide, 4¼ in. high. Rated—2.6 sq ft per lineal ft at 1 lb steam and 70 deg air.

Contact Representatives in Principal Cities or Send for Catalog.

Baker Ice Machine Co., Inc.

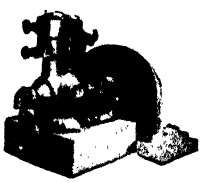
SALES AND SERVICE
IN PRINCIPAL CITIES

South Windham, Maine
Omaha, Nebraska
Cable Address: BAKERICE

BUILDERS OF DEPENDABLE REFRIGERATION EQUIPMENT SINCE 1905

● **PRODUCTS: Ammonia Compressors; Self-Contained Ammonia Units; Self-Contained "Freon-12" Units; Shell and Tube Condensers, Vertical or Horizontal; Refrigeration Valves and Fittings; Water or Brine Coolers, Shell and Tube or Multi-Unit Type; Coils and Cooler Units of all sizes; Automatic Refrigeration Controls and Accessories; Evaporative Type Condensers.**

BAKER AMMONIA COMPRESSORS

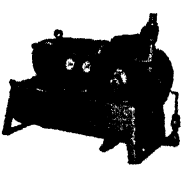


From 1 to 100 tons capacity. V-belt drive or direct connection to motors or engines. Vertical enclosed single-acting type. Duplex or multiple installations to obtain any desired capacity.

BAKER AMMONIA COMPRESSOR UNIT

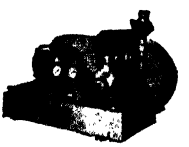
Model F6B from 7½ to 20 hp. Bore and stroke 3½ in. x 3½ in. Four cylinders, reciprocating single acting type. Force feed lubrication. Timken Roller Bearings. This model available in single or multiple compressor or condensing units as desired.

BAKER "FREON-12" UNITS



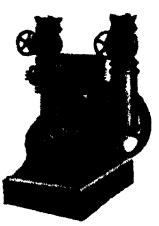
"Freon-12" Units of the self-contained automatic type from ¼ to 20 hp capacity in single units. Furnished in air-cooled type ½ to 20 hp and water-cooled type 3 to 20 hp.

"FREON-12" COMPRESSOR UNITS



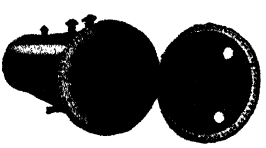
Arranged for use with evaporative type condenser or separately mounted shell and tube condensers. Sizes from 3 hp to 20 hp. Two and four cylinder types. Automatic controls.

BAKER AMMONIA BOOSTER COMPRESSORS



For sub-zero temperature work. Lubrication under pressure. Single or multiple compressor installations. V-belt or direct drive. Large gas manifold at compressor suction ports allows complete filling of cylinder at variable speeds.

BAKER SHELL AND TUBE CONDENSERS AND COOLERS



ASRE welded single units to 150 tons, multiple units any capacity. Shells 8 in. or 50 in. diameter. Removable heads. Vertical or horizontal, single-pass or multi-pass. Brine or water.

Baker Also Manufactures a Complete Line of Industrial-Type Cooling Units, Ammonia Valves, Screw-End Fittings, Capped Valves, Flanged-Type Fittings

Curtis Refrigerating Machine Division

of Curtis Manufacturing Company

1959 Kienlen Ave., **St. Louis 20, Mo., U. S. A.**

ESTABLISHED 1854

Full Line of Units from ¼ to 30-hp

CURTIS REFRIGERATION AIR CONDITIONING COMMERCIAL

Unit Coolers and Evaporator Coils

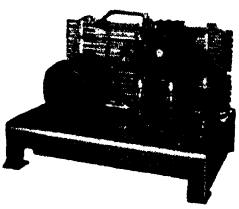
PRODUCTS: Complete Refrigerating Equipment for Dairies, Creameries, Ice Cream Cabinets, Ice Cream Making Plants, Cold Storage Locker Systems, Walk-in Coolers, Drinking Water Systems, Commercial and Low Temperature Cooling, Processing and Air Conditioning Installation, Packed and Remote Types.

Commercial Refrigeration

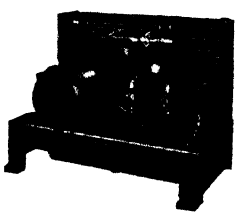
¼ to ½ hp Self-Contained Condensing Unit.

Air cooled condensing units from ¼ to 3 hp, inclusive, and water cooled units from ⅛ to 30 hp, inclusive. All models available for either Freon (F-12) or Methyl Chloride. Mechanical advantages include Timken Bearings, Centro-Ring Positive Pressure lubrication.

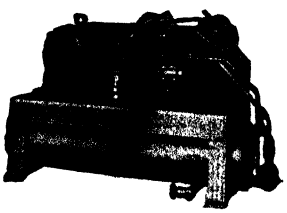
Special models are available for ice cream, frozen food cabinets and for the dairy industry.



5 hp Water Cooled (Counterflow) Condensing Unit. Other from sizes ¼ to 5 hp.



1½ hp Air Cooled Condensing Unit. Other sizes from ¼ to 3 hp.

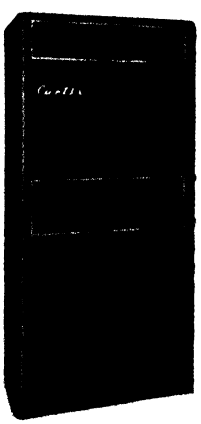


15 hp Cleanable Shell and Tube Condensing Unit. Other sizes from 3 to 30 hp.

Air Conditioning

For today's Air Conditioning requirements Curtis offers complete packaged, refrigerated air conditioning units, requiring only water and electrical connections to install. Cools, dehumidifies, circulates and filters the air. Eliminates costly installation expense. Adaptable for heating.

7½-10-15 ton Remote or Central Type Air Conditioner.



3 and 5 ton Packaged Type Air Conditioner.

ATLANTA
BOSTON
BUFFALO
CHARLOTTE
CHICAGO
CINCINNATI
DALLAS
DETROIT
KANSAS CITY
LOS ANGELES

Frick Company

(Incorporated)

Air Conditioning, Refrigerating and Ice-Making Equipment

Waynesboro, Penna.

MEMPHIS
NEW ORLEANS
NEW YORK
OKLAHOMA CITY
PALATKA
PHILADELPHIA
PITTSBURGH
ST. LOUIS
SEATTLE
WASHINGTON

Distributors in FRICK **Principal Cities**

AIR CONDITIONING

Ask for Frick Bulletins 502, 503, 504 and 505 on Air Conditioning

Complete Frick systems; also refrigeration for use with equipment supplied by others. Over 1000 installations attest the value of Frick equipment. Successful experience with exacting commercial and industrial jobs enable us to solve your air conditioning problems.

AMMONIA REFRIGERATION

Combined units and vertical enclosed compressors, with two or four cylinders, in sizes from ½-ton up. Widely used for air conditioning, with material savings. Ask for Bul. 503 on this subject.

Pratt and Whitney use Frick Ammonia Refrigeration for Precision Air Conditioning Service

FREON-12 REFRIGERATION

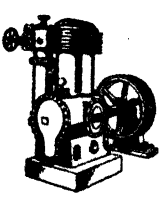
Frick "Eclipse" and the larger F-12 compressors provide a complete and efficient line. Coils, coolers, condensers and controls to suit. Patented Flexo-Seal at shaft, pressure lubrication from submerged pump, capacity controls, and other superior features make Frick machines your logical choice.

Frick Equipment Air Conditions Three Test Rooms for Bendix Radio at Towson, Md. Temperature and Humidity are Automatically Controlled between 194 and —76° F

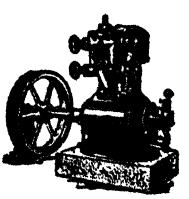
LOW-PRESSURE REFRIGERATION

Commerical and industrial units in sizes from ¼ hp. up. Charged with Freon-12. Air and water-cooled condensers. Coils, coolers, and air conditioners. Get in touch with your Frick Distributor; ask for Bul. 97. Our service includes estimates, layouts, manufacture, installation, maintenance.

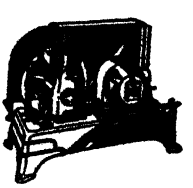
"Eclipse" Freon-12 Compressor. Bulletin 100.



Enclosed Freon-12 Machine. Bulletin 508.



Enclosed Ammonia Compressor. Bulletin 112.



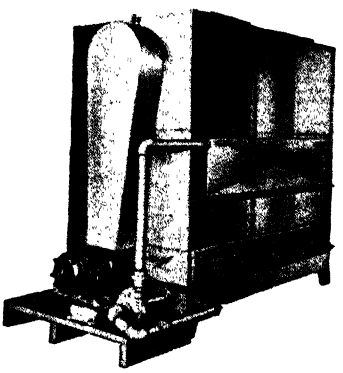
Low Pressure Refrigerating Unit. Bulletin 97.

Marlo Coil Co.

6135 Manchester Ave., **St. Louis 10, Mo.**

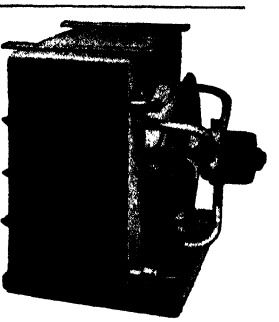
Manufacturers **MARLO-HEAT TRANSFER** Equipment
Since 1925

Industrial Coolers — Unit Coolers — Evaporative Condensers — Low Temperature Units — Air Conditioning Units — Heating and Cooling Coils — Cooling Towers — Diesel Engine and Oil Evaporative Coolers.



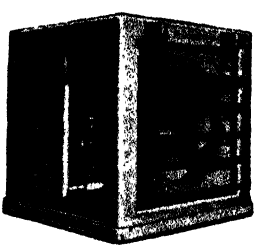
COOLING TOWERS

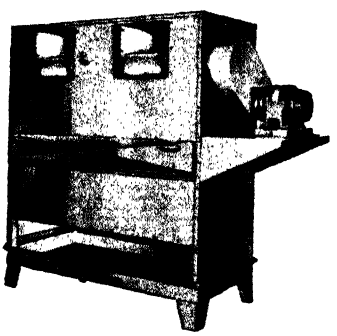
Triple-Type: Induced Air — Wetted Surface —Water Spray. Compact in space, weight and price. Outdoor—Indoor—3 to 50 tons—Built sectionally. Write for *Bulletin* 406.



EVAPORATIVE CONDENSERS

3 to 100 tons—All refrigerants — All prime surface coils—No fins —Quiet—Motor Unidrive. Indoor or outdoor units—Durable construction. Write for *Bulletin* 404.



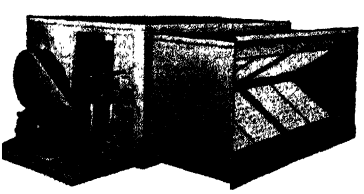


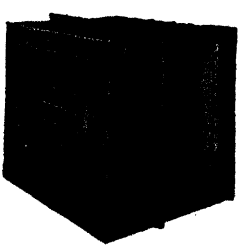
INDUSTRIAL COOLERS

15 unit sizes—1000 to 24,000 cfm—Floor type. Galvanized frame and pans—Sectionally built. Variables: (1) Rows of coil and fin spacing. (2) Circulating brine spray or dry coil. (3) Defrost sprays optional. (4) All Refrigerants. Write for *Bulletin* 403.

UNIT COOLERS

Pull-through (DUC) and Blow-through (UC) types —for all refrigerants. 11 unit sizes—4 and 6 row coils—full range of capacities. 675 to 4160 cfm—Venturi fan ring—Deflector louvers. Sturdy—Economical—Quiet. Also Wall Panel Type. Write for *Bulletins* 412 and 392.





AIR CONDITIONING UNITS

Cooling — Heating — Dehumidifying — Humidifying. 10 sizes—3 to 35 tons—900 to 13,000 cfm. Noise level ratings—Ceiling suspended or floor types. Write for *Bulletin* 409.

(U.S. Patent 2266373)

BLAST COILS

Air conditioning—Industrial Refrigeration —Heating. Any material—All refrigerants—Every application. "BALL-BONDED"—mechanically expanded tubes to fins. Write for *Bulletin* 396.

ELECTRIC DEFROST LT UNITS

Compact ceiling type—High capacity—Low cost. 7 sizes—Ammonia or Freon—½ to 2½ tons at 12 deg TD. Defrosted electrically. Quickly installed—Sectional doorway-sized. Write for *Bulletin* 408.

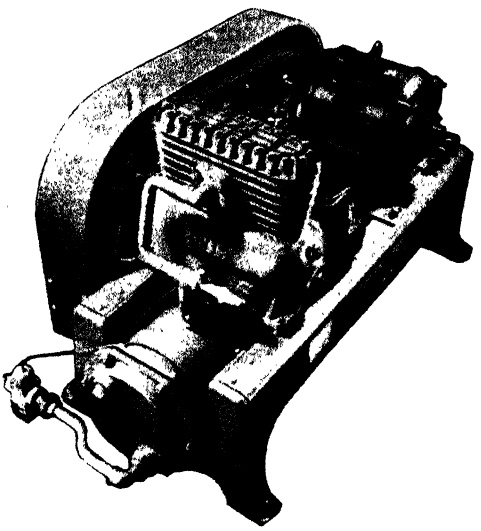
MILLS *Industries, Incorporated*

Refrigeration Division 4100 Fullerton Avenue · Chicago 39, Illinois

Mills Compression Equipment
for Air Conditioning • Commercial and Industrial Refrigeration

COMPRESSOR

2½ in. x 3 in. four cylinder, vertical, single acting, reciprocating type . . . heavy, one piece alloyed semi-steel cylinder block and crankcase . . . oil sight glass . . . alloy semi-steel pistons, two compression rings, one oil ring . . . hardened piston pins . . . drop forged steel connecting rods . . . bronze piston pin bearing . . . bronze main bearings . . . exclusive Mills design shaft seal.



CONDENSING UNIT

Base of cast iron ends and formed steel sides . . . shell and tube type receiver condenser with removable heads and leak alarm fittings . . . complete with automatic water valve, starting box, low pressure control with high pressure safety cut-out . . . complies with Underwriters' specifications . . . dynamically balanced and non-vibrating, light in weight, compact, requiring a minimum of floor space. Mills Condensing Units are economical to operate and maintain. Condensing units are shipped ready to operate. No special foundations are necessary.

APPLICATIONS

Refrigeration in air conditioning applications for comfort, food preservation, and industrial uses for processing and testing. Compactness of condensing units make them ideal for self-contained applications.

ENGINEERING

Mills Industries, Incorporated maintain an engineering test laboratory as a service to their customers, equipped with three hot rooms, calorimeter, indicating and recording, pressure and electrical instruments and all apparatus necessary for a thorough analysis of the use of condensing units to any manufacturer's product or field applications.

CAPACITIES AT 40° F SUCTION GAS

Size	RPM	Displacements CFM	Capacities in BTU	Width	Depth	Height	Net Weight
5 hp	480	16.37	65000	63"	29½"	32"	895 lb
7½hp	700	23 86	90500	63"	29½"	32"	945 lb
10 hp	890	30.34	125000	63"	30"	34"	1050 lb

Air cooled models from ¼ to 3 hp.
Water cooled models from ½ to 10 hp.

All models are designed for use with Freon-12 or Methyl Chloride refrigerants for low, standard, and high back pressures, for operation throughout the complete range of temperatures.

Compressors are designed for low head temperatures and high volumetric efficiency.

Condensers are matched to the performance ranges of each compressor.

A Member of the Mills Field Organization Is Near You
And at Your Service

Worthington Pump and Machinery Corporation

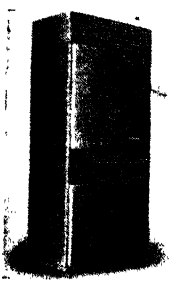
Air Conditioning and Refrigeration Division

General Offices: HARRISON, NEW JERSEY

ALBANY	CHARLOTTE	DETROIT	LOS ANGELES	PITTSBURGH	SAN FRANCISCO
ATLANTA	CHICAGO	EL PASO	MILWAUKEE	PORTLAND, ORE.	SEATTLE
BALTIMORE	CINCINNATI	FORT WORTH	NEW HAVEN	PROVIDENCE	SPRINGFIELD, MASS
BIRMINGHAM	CLEVELAND	GALVESTON	NEW ORLEANS	ST. LOUIS	SYRACUSE
BOSTON	DALLAS	HOUSTON	NEW YORK	ST. PAUL	TULSA
BUFFALO	DENVER	KANSAS CITY	PHILADELPHIA	SALT LAKE CITY	WASHINGTON, D.C.
					WILMINGTON, DEL.

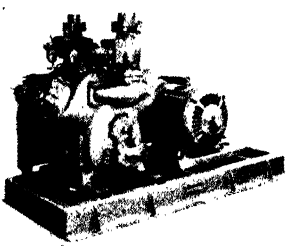
Representatives in all Principal Cities

Self-contained Air Conditioners



Cooling (or heating, if desired), dehumidification, ventilation, circulation and air cleaning for commercial and small industrial applications. 3 and 5 ton capacities. Compressor, finned copper tubing condenser, large-surface finned cooling coils, quiet low-speed fan, throw-away filters, concealed temperature and air volume controls. Freon-12.

Self-contained Units



Small sizes range from ¼ to 10 hp. Large sizes, capacities up to 100 tons. Freon-12 compressor units for use with evaporative condensers or water-cooled condensers. Automatic capacity control.

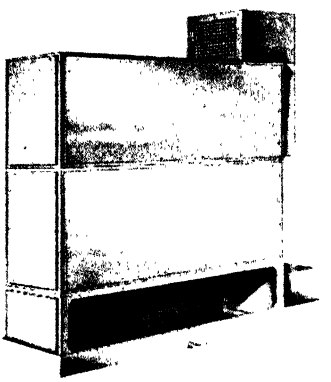
Centrifugal Refrigeration

Water Cooling Systems

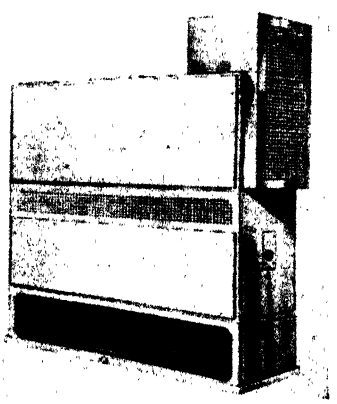
Freon-11 centrifugal compressor, water cooler and water-cooled condenser in compact unit assembly. Electric motor or steam turbine drive. 56 unit sizes . . . 150 to 1200 tons.

Air Conditioning Units

For Direct Expansion Freon-12 or Chilled Water Circulation



Vertical and horizontal; 1500 to 12,000 cfm; large air passages; slow speed, quiet rugged fans; separable sections; readily accessible. The design permits flexibility in installation arrangements.



Evaporative Condensers

A combined condenser, receiver and modified cooling tower, in one assembly, for Freon-12, methyl chloride, and ammonia systems; 10 to 60 tons refrigeration; all parts easily accessible.

Jacket Water Coolers

For cooling jacket water for Diesel and gas engines, air compressors, etc.

Air CONTROLS INC
Div. of
The Cleveland Heater Co.

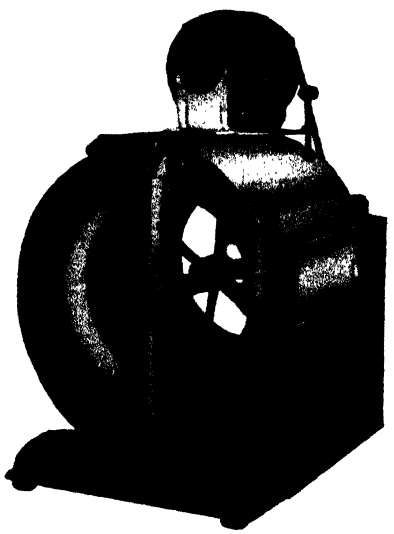
MEMBER NATIONAL WARM AIR HEATING AND AIR CONDITIONING ASSOCIATION — INDOOR COMFORT

2310 Superior Ave. **Cleveland 14, Ohio**

REX BLOWERS

DESIGNED and Engineered for MAXIMUM PERFORMANCE

Engineered to meet all modern needs and proof-tested for performance, **REX** Blowers set the pace for leadership by better design, smooth operation and trouble-free service. You can give your equipment an added sales feature by using **REX** Blowers—it's a feature you cannot afford to overlook.



Outstanding Features Of The REX Blower Line

Accessible, long-lasting oiling element . . .

The new streamlined bearing bracket with the sight-feed oil gage, and oil reservoir cap near the top of the blower, permits ease of lubrication. This revolutionary bearing holds 2 to 4 times as much oil as conventional bearings.

Adjustable cutoff . . .

Equally efficient against high or low resistances by simple adjustment.

Rigidity . . .

The extra heavy construction of the new **REX** Blower line, insures sturdiness. Cross-bracing maintains alignment and quiet operation.

Reliable . . .

The operating record of thousands of **REX** Blowers which are in actual operation on air conditioning equipment, is the best testimonial of their reliability.

For Complete Information, Write For Catalog No. 247 Which Contains Complete Performance & Specification Data.

American Coolair Corporation

3606 Mayflower Street, **Jacksonville 3, Florida**
Charter Member, Propeller Fan Manufacturers Association

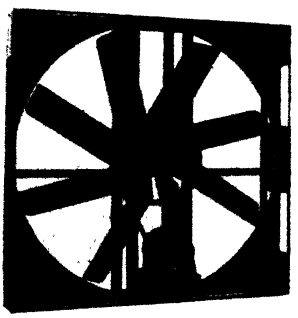
BUILDERS OF V-BELT DRIVE EXHAUST FANS FOR 20 YEARS

The principle of **Rapid Air Change** for the effective cooling of commercial and industrial buildings has been used by Coolair for 20 years, and the company specialized in the development of V-belt drive exhaust and home-cooling fans. Coolair manufactures a wide range of fan sizes and types to fill the ventilating and cooling requirements of all kinds of buildings.

In planning a Coolair installation, provide for a complete change of air once every 30 seconds to one minute. Select fan from table on opposite page to conform to cubic contents of space to be cooled. Write for FREE bulletins containing detailed information, or for the name of nearest Coolair dealer or distributor.

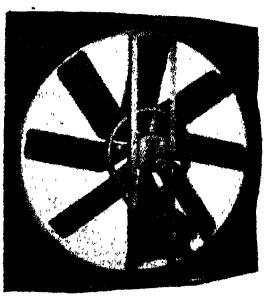
QUALITY FEATURES OF COOLAIR FANS

1. **Patented Spring Mountings on Smaller-motored Units.** All moving parts float on resilient springs, absorb noise.
2. **Compact Welded-steel frame.** Cannot warp or twist. Easy to install.
3. **Reversible Operation.** Fan will blow in or exhaust as desired when equipped with reversible motor.
4. **Oversize Ball Bearings in Fan Hub.** Eliminate chatter and thrust knock, assure long life. Permit operation in any position if ball bearing motor is used.
5. **Eight Steel Blades.** Up to 12 in larger fans. Multi-blade design means slower speeds, steadier air flow, quieter operation.
6. **V-belt Drive.** Small motors operate at most economical running speeds.
7. **Long Hour Service Motor.** Nationally known motors.
8. **Certified Air Ratings.** Set in accordance with ASHVE-NAFM Standard Test Code.
9. **Full Streamlined Orifice.** Avoids "spill-off" of air, reduces power consumption.



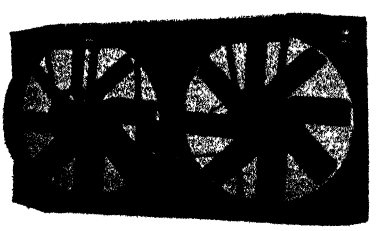
TYPE S—For Large Industrial Jobs

Especially designed for ventilating and cooling industrial plants, shops, power stations, warehouses and other large buildings. Heavily braced double frame, special pillow-block ball bearings on each side of fan wheel, 8 to 12 reinforced fan blades, multiple heavy duty V-belts. Lowest possible operating cost. Type S Fans range from six to nine feet with several motor sizes for each.



TYPE O—For Industrial, Commercial, Home Use

Patented built-in springs (on smaller motored sizes) and streamlined orifice combine to make this type extremely quiet in operation. Designed for reversible operation. Equally efficient in any position when equipped with ball bearing motor. Usually installed in window openings, walls, skylight openings, penthouses or attics. Available in seven fan sizes ranging from 26 to 62 inches with several motor sizes for each. U. S. Patents 1992112 and 2191418.



TYPE OT—Twin Unit

This unique Coolair Twin-unit is two fans of Type O specifications mounted side by side in one frame and operated by a single motor. For use where limited headroom or wall space will not permit the use of a single fan of ample size. Can be placed on end to fit into existing window and door openings. Covered by U. S. Patents 1992112, 2108738 and 2191418.

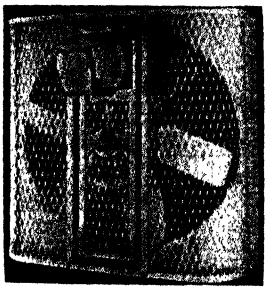
Dimensions in Inches

Fan Size	Overall Height	Overall Width	Overall Depth (Approx)
28-W	31	33	15
2-O	30⅝	30⅝	16
2½-O	36⅝	36⅝	18
3-O	42⅝	42⅝	18
3½-O	49	49	19
4-O	55⅛	55⅛	19
4½-O	61⅛	61⅛	19
5-O	67⅝	67⅝	19
6-S	75¼	75¼	30
7-S	87	87	32
8-S	99⅝*	99⅝*	49
9-S	112⅛*	112⅛*	54
2-OT	30⅝	61¼	18
2½-OT	36⅝	73¼	18
3-OT	42⅝	85¼	19
3½-OT	49	98	19
4-OT	55⅛	110¼	22

*These dimensions include five-eighths inch for bolt heads.

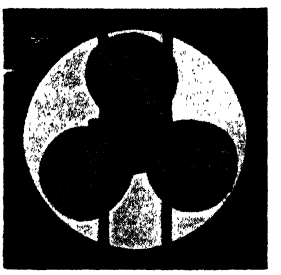
28-W FAN WITH SAFETY GUARD

Coolair's lowest priced belt-drive fan is equipped with built-in springs, adjustable diameter motor pulley and safety guard. This fan can be easily and quickly installed in upper or lower half of any standard window of work rooms or offices where proper ventilation is necessary for health, comfort and efficiency of workers. See tables for data.



DIRECT DRIVE FANS

Four sizes 16 to 24 inches in diameter. General purpose exhaust fan for most commercial and industrial uses. Data on sizes, performance and dimensions furnished on request.



COOLAIR AUTOMATIC CEILING & WALL SHUTTERS

Precision-built all-steel shutters that open and close automatically when fan is turned on or off. Ceiling shutters eliminate need of ceiling grille and trap door in attic installations. Wall shutters give weather protection for fans discharging directly to open air.

Performance Data—Coolair V-Belt Drive Fans

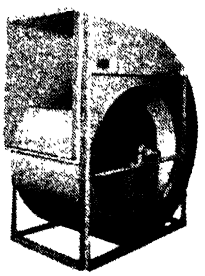
Fan Size		Horse Power	Fan R. P. M.	Cubic Ft. Air Per Min.
28-W	VL	¼	580	6000
2-O	VL	¼	570	6200
	D	⅓	630	6800
2½-O	VB	¼	411	8000
	VC	⅓	454	8800
	D	½	522	10100
	D	¾	600	11700
3-O	VB	¼	312	10000
	VC	⅓	345	11000
	C	½	398	12700
	D	¾	450	14400
	D	1	500	16000
3½-O	VB	⅓	261	13000
	VC	½	300	15000
	C	¾	345	17000
	D	1	380	19000
	D	1½	440	22000
4-O	VL	½	258	19000
	VC	¾	317	22000
	D	1	353	25000
	D	1½	405	28000
4½-O	VB	½	224	22800
	VC	¾	255	25000
	C	1	276	27000
	D	1½	319	32000
	D	2	355	35000
5-O	VB	½	200	27000
	VC	¾	225	30000
	C	1	245	33000
	C	1½	282	38000
	D	2	310	42000
	D	3	355	48000
6-S	B	1	155	35000
	C	1½	177	40000
	C	2	195	45000
	D	3	224	50000
	D	5	270	60000
7-S	B	2	170	58000
	C	3	195	67000
	D	5	230	76000
	D	7½	270	85000
8-S	B	3	150	80000
	C	5	178	95000
	D	7½	205	110000
	D	10	225	120000
9-S	B	5	150	110000
	C	7½	170	125000
	D	10	190	138000
	D	15	215	154000
2-OT Twin	VB	¼	455	9800
	VC	⅓	500	10800
	VC	½	570	12400
2½-OT Twin	VB	⅓	359	14000
	VC	½	411	16000
	VC	¾	470	18200
3-OT Twin	VB	½	312	20000
	VC	¾	360	23000
3½-OT Twin	VB	¾	272	27800
	VC	1	300	30700
4-OT Twin	VB	1	258	38000
	VC	1½	317	44000
	D	2	345	48000

B—Very Quiet (Homes, Theatres, Hospitals, etc.).
C—Quiet (Stores, Offices, Restaurants, Barber Shops, etc.)
V—Equipped with built-in springs.
D—Industrial (Laundries, Factories, Canneries Bakeries, Pressing Clubs, Garages, etc.).
L—Has adjustable diameter motor pulley for Very Quiet and Quiet performance.

Aladdin Heating Corporation

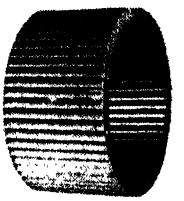
2222 San Pablo Ave., **Oakland 12, Calif.**

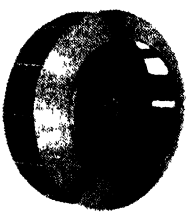
Manufacturers of Centrifugal Blowers, Heating and Ventilating Equipment.



FC Fan and Rotor

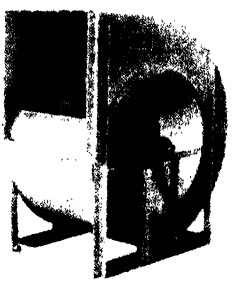
The Aladdin FC fan having a forward curved rotor is built in 14 standard sizes, single or double width, of 8 arrangements of drive and 8 directions of discharge. The low tip speed which is characteristic of this fan makes it ideal for general application where quiet operation is essential. Write for Bulletin No. 490.

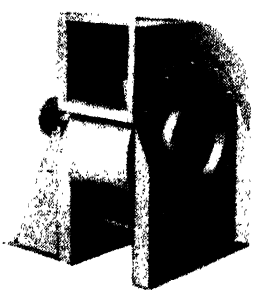




BB Fan and Rotor

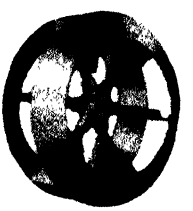
The BB fan is a backward curved fan with the non-overloading horsepower characteristic. This fan is built in 12 standard sizes, single or double width of 8 arrangements of drive and 8 directions of discharge. These fans are available in class I, II, III or IV and can be built for special application where required. Write for Bulletin No. 485.

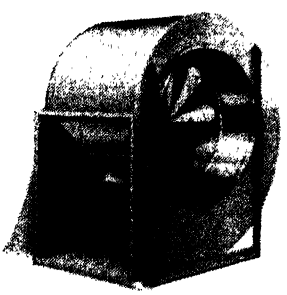




EX Fan and Rotor

The EX fan is used chiefly for the conveying of materials, fume exhaust etc. These fans are reversible and can be furnished in 13 standard sizes of 8 arrangements of drive and 8 directions of discharge. They can be designed for special applications such as for handling abrasive materials or for acid fumes. Write for Bulletin No. 460.





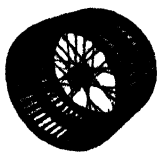
RB Fan and Rotor

The RB fan having a radial curved rotor is used chiefly for kitchen exhaust duty. They are well suited for handling grease and other sticky materials, also for exhausting fumes and vapors from tanks, hoods, etc. This fan is built in 12 sizes, single width only, of 8 arrangements of drive and 8 directions of discharge. Write for Bulletin No. 450.

Bayley Blower Company

1817 S. Sixty-Sixth Street **Branches in Principal Cities** **Milwaukee 14, Wis.**

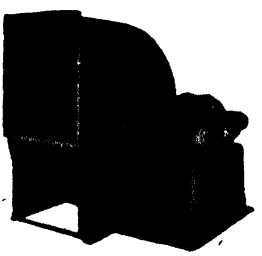
Builders of Heating, Ventilating, Cooling, Purifying, Humidifying and Air Washing Equipment; Exhaust and Drying Apparatus, Mechanical Draft and Blast, Fans and Blowers of all Types



TYPE "F" PLEXIFORM FANS AND TYPE "AP" AEROPLEX FANS

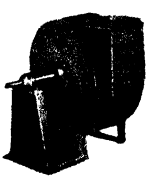
Plexiform and Aeroplex Fans are both designed for heating, ventilating and air conditioning service. The **Type "F"** fan is using a multi-blade wheel (see cut at left) while the type **"AP"** fan is built around a wheel of high speed design (see cut at right.)

The wheels determine the character of the performance or the fan "Characteristics," thus the Type "F" is a slow speed fan having a rising power curve, while the **"AP"** is a high speed design and has self-limiting power characteristics. Both fans are highly efficient and can be built single inlet, single width, or double inlet, double width in ten different arrangements of drive and eight directions of discharge. The standard fans range in capacity from 1200 to 300,000 cfm and these fans are readily available in Class I or II designs for various types of duty. Class III and IV can be furnished on special application.



Type "EX" Fans

For all exhaust problems, pneumatic conveying, fume exhaust etc. **"EX"** is highly adaptable, feasible and serviceable fan. It is sturdy in construction, easily installed and maintained. The design is reversible and standard sizes Nos. 15 to 80 inclusive are available.



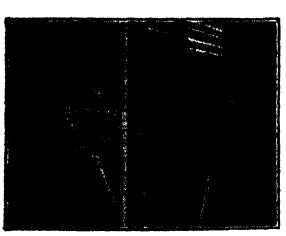
Type "H" Fans

For pressure applications from 6 in. to 42 in. for belt drive or direct connection to motor, **Type "H"** is a most practical design. Standard sizes Nos. 25 to 80 are listed but the design is suitable for modification of wheel diameters to meet various motor speeds.

Both **"EX"** and **"H"** fans can be designed to fit specific applications. The design permits easy modification of details and the fans can be used for induced, forced draft, cupola service, primary or secondary air supply to oil burners, etc. Special details, outlet and inlet, or mounting can be designed to suit your special assembly.

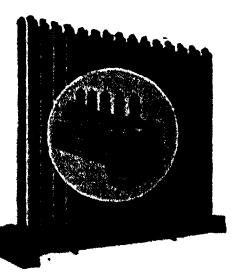
Turbo Spray

The Turbo Spray for industrial and comfort conditioning, cooling and humidifying, is a practical design as the atomization is by mechanical means, thus there can be no clogging or interruption of service even in atmosphere heavily laden with fibers or other foreign material. Single or multiple bank washer, one or two stage designs can be furnished from 2500 to 100,000 cfm capacity. To fit space requirements width and height can be modified to suit.



Chinook & Chinookfin

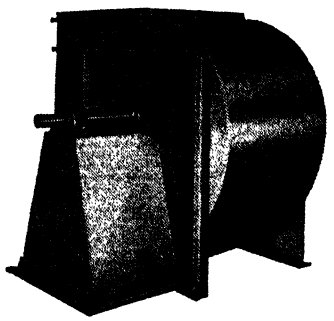
Both **Chinook and Chinookfin Coils** are based on the tube-within-a-tube design, originated by Bayley. The principle involved permits single header with all tube ends free expanding, thus eliminating the likelihood of freeze ups and cracking usually due to expansion and contraction strains. Both type coils are designed for usual hot blast heating and cover a wide range of capacities and applications.



The Bishop & Babcock Mfg. Co.

Massachusetts Blower Division

4901 Hamilton Ave. **Cleveland 14, Ohio**

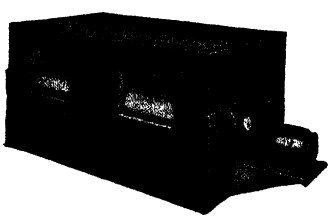


SQUIRREL CAGE AND POWER FIXED FANS

Squirrel Cage Fans, outstanding in performance, slow speed characteristics.

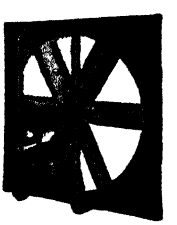
Power Fixed Fans are backward curve blade type, with non-overloading characteristics. Double width, double inlet, Class I or Class II construction, built in a wide range of sizes. Rating and dimension tables available. Write for catalogs.

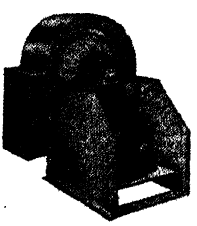
The new Design 2 Air Conditioning Furnace Blowers are now available, with a wide variety of stock combinations and discharge arrangements. They can be furnished in special widths or in multiples. Also available are wheel assemblies, housings and housing sides. Write for catalog.



Unit Heaters. Blower type. Floor and Ceiling type made in 13 standard sizes, with regular or non-freeze coils, filter and damper sections. Ratings from 50,000 Btu up. Propeller Fan type "H," Horizontal made in 16 sizes. Type "V" Vertical projection for ceiling mounting. Write for catalogs for full information.

Propeller Fans available with Belt drive with wheel sizes 24 in. to 48 in. Direct Drive with wheel sizes 12 in. to 36 in. Both types available with single or 2 speed motor. A complete line of Automatic Shutters and Fan Houses are obtainable. Write for catalog.





Ventilating Sets. Series MSV Design 2. Belt Driven, with or without motor and drive cover. Type "S" Design 2 are direct connected, designed for either supply or exhaust on small ventilation problems. Write for catalog.

Buffalo Forge Company

450 Broadway, **Buffalo, N. Y.**

Sales Representatives in These Cities:

ALBANY 7, N. Y.—Mr. R. B. Taylor, 966 Broadway
ATLANTA, GA.—Mr. J. J. O'Shea, 305 Techwood Drive
BALTIMORE 1, MD.—Machinery & Equipment Sales, Inc., 1014 Cathedral St.
BOSTON 76, MASS.—Mr. E. D. Johnson, 507 Main St., Melrose Station
CHICAGO 6, ILL.—Emmert & Trumbo, 20 N. Wacker Dr.
CINCINNATI 2, OHIO—Mr. F. W. Twombly, 626 Broadway
CLEVELAND 13, OHIO—Weager & Sherman 418 Rockefeller Bldg.
DALLAS 1, TEX.—Buffalo Forge Co.—Mr. T. H. Anspacher 1801 Tower Petroleum Bldg.
DAVENPORT, IOWA—D. C. Murphy Company, Inc., 305 Security Bldg.
DES MOINES 9, IOWA—D. C. Murphy Company, 214 Old Colony Bldg.
DENVER 17, COLO.—Hendrie & Bolthoff Mfg. & Supply Co., Box 5110 Terminal Annex D
DETROIT 16, MICH.—Coon-DeVisser Co., 2051 W. Lafayette Blvd.
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KNOXVILLE 21, TENN.—Mr. C. F. Sexton, P. O. Box 2224, 702 Empire Bldg.
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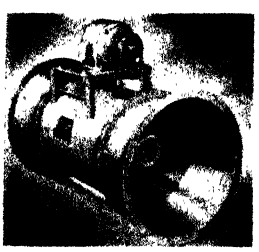
NEW YORK 7, N. Y.—Koithan & Johnson, 39 Cortlandt St.
NEWARK 2, N. J.—Mr. G. C. Norman, 27 Washington St., Room 203
OMAHA 2, NEB.—Wain Engineering Co., 375 Brandeis Theatre Bldg.
PHILADELPHIA 2, PA.—Davidson & Hunger, 1200 Cunard Bldg.
PITTSBURGH 22, PA.—Mr. H. Lee Moore, 345 Fourth Ave.
ROCHESTER 4, N. Y.—Buffalo Forge Co., Mr. R. Moyer, 846 Sibley Tower Bldg.
ST. LOUIS 3, MO.—Mr. J. W. Cooper, 2118 Pine St.
SALT LAKE CITY 1, UTAH—Lee Pace & Turpin, 142 S. Fifth West St.
SAN ANTONIO 6, TEXAS—Langhammer Rummel Co., 436 Main St.
SAN FRANCISCO 9, CALIF.—Buffalo Forge Co. Mr. C. W. Lockhart, 1214 Central Tower Bldg., Third and Market Sts.
SEATTLE 1, WASH.—A. T. Forsyth Company, 3150 Ellicott Ave.
TOLEDO 2, OHIO—C. M. Eyster Company, 1118 Madison Ave.
TUCSON, ARIZ.—Tidmarsh Engrg. Co., 23 N. Main St.
WASHINGTON 5, D. C.—Buffalo Forge Company, Mr. G. S. Frankel, 310 Woodward Bldg.
WILKES-BARRE, PA.—Power Engineering Co., 517 Brooks Bldg.
KITCHENER, ONT., CANADA—Canadian Blower & Forge Co.

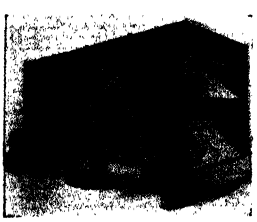
PRODUCTS—Equipment for all types of Heating and Ventilating, including: Unit Heaters, Multiblade Fans, Air Washers, Unit Air Washers, Unit Coolers, Drying Equipment, Mechanical Draft Fans, Air Preheaters, Blowers, Exhausters, Disc Fans, Spray Nozzles.



BUFFALO AXIAL FLOW FANS

High pressure ventilating fans with non-overloading characteristic, vibrationless operation and straight line air propulsion. The axial flow design cuts energy losses and power costs to a minimum.

BUFFALO AIR WASHERS



Where washing, tempering and purifying of air under changing atmospheric conditions is required, Buffalo Air Washers are available in designs to handle every plant problem. At left, above, a Buffalo Air Washer widely used in many plants.

BUFFALO LIMIT-LOAD CONOIDAL

Dynamically balanced, these fans are non-overloading regardless of operating conditions. Well suited to moving large volumes of air at low power cost. Sturdy rotor and housing construction throughout.

BUFFALO UNIT HEATERS

For throwing quick heat economically into desired areas of plant and public buildings, Buffalo "Highboy", "Lowboy" and "Breezo-Fin" unit heaters are available in floor, wall or ceiling installations.

VENTILATING INFORMATION ON REQUEST

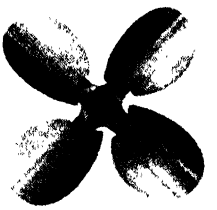
Buffalo fans and air conditioning units cover practically every air application. The Buffalo representatives above will gladly give you advice on your problem, or simply write us.

Burden Company

1000 North Orange Drive, **Los Angles 38, Calif.**

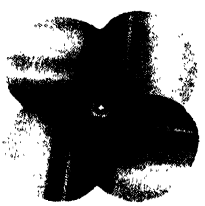
Manufacturers of Aluminum-Fan Blades
Aluminum and Steel Blower Wheels

Burden Blades and Blower Wheels are designed to operate smoothly and efficiently, on a minimum of horsepower, giving maximum volume of air flow. All Burden Blades and Blower Wheels are tested for dynamic and static balance by the patented Burden electronic Balancer. All blade hubs are standard for motor on suction side of blade. Burden products are outstanding for their low noise level, resistance to corrosive action, slight weight and great strength. For specifications of Blades and Blower Wheels and for types not listed, write factory.



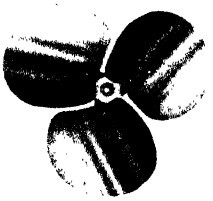
ATTIC

Balanced for quiet efficient operation. Full air volume affords greater cooling capacity. Built of polished aluminum with steel spider. Light weight. Sizes: 36, 42 and 48 in. diameters.



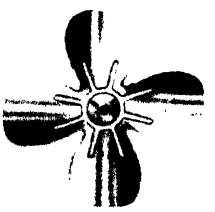
FULL PRESSURE

Four overlapping aluminum blades with plated steel hub and spider. Available in 8 in. through 24 in. sizes.



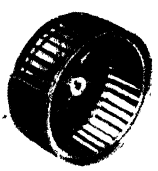
SEMI-PRESSURE

Three aluminum blades, with plated steel hub and spider. Available in 10 in. through 30 in. in diameter.



FREE AIR

A four bladed, one piece fan. Available in either stamped aluminum or plated steel. Made in sizes ranging from 6 in. through 12 in. Also available in colors.

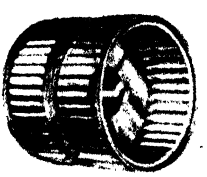


SINGLE BLOWER WHEEL

Light weight aluminum or steel construction. Anodized or plain finish. Rigid. Sturdily built. Cadmium plated steel hub. Sizes and widths according to needs.

SINGLE BLOWER WHEEL

Made of aluminum with choice of plain or anodized finish. Also may be had in steel. Strong, rigid wheel in wide variety of diameters and widths.



DOUBLE WHEEL

Constructed of aluminum or steel with double inlet and outlet. Rigidly mounted cadmium plated steel hubs. Available in wide variety of diameters and widths.

Champion Blower & Forge Co.

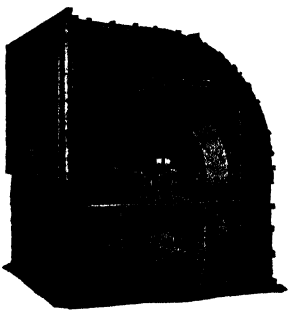
Manufacturers and Engineers

Plant and Offices: **Lancaster, Pa.**

Address Correspondence to Div. 9

Manufacturers of Blowers, Ventilating Fans and Exhaust Fans for Air and Material; and Blast Gates

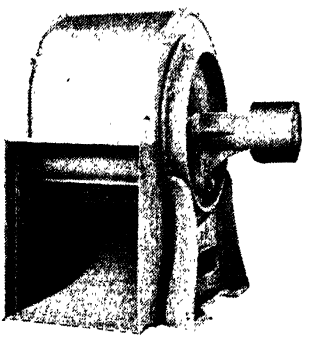
Representatives in Principal Cities



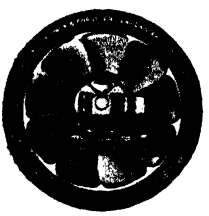
Type S

Type S Forward curve ventilating fans, single and double width, as well as direct motor drive.
Sizes 30 in. to 60 in. wheel dia.

Type S Forward curve ventilating fans, single and double width, and electric drive up to 36 in. wheel diameter.



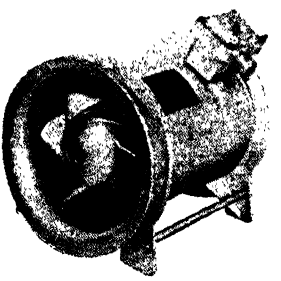
Type S



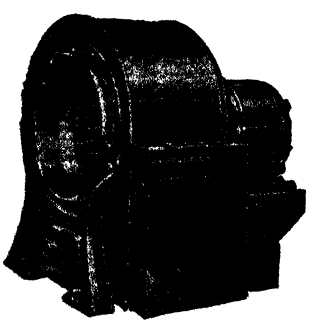
Type SV

Type SV Super Ventilating fans, direct motor drive up to 36 in. diameter. Motor belt drive up to 48 in. size.

Type M Axial Flow non-overloading fans for high and low pressures. Exhausting and Ventilating.



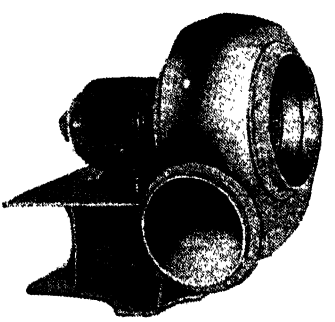
Type M



Type BC

Type BC Backward curve ventilating and exhaust fans, single and double width; belt driven and direct connected electric.
Sizes 12 in. to 60 in. wheel dia.

Type CE Electric cast iron exhaust and forced draft fans. Also volume control dampers.



Type CE

Chelsea Fan & Blower Co., Inc.

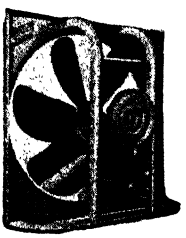
1206 Grove St., **Irvington 11, N. J.**

Charter Members Propeller Fan Manufacturers Association

Trade Mark Registered

EXPORTED TO ALL COUNTRIES OF THE WORLD BY WESTREX CORPORATION

(Western Electric Export Corporation)



THE INDUSTRIAL FAN (TYPE IND.)

Cat. No.	C.F.M.	Motor HP
IND24	5700	⅛
IND30	8300	½
IND36	11250	½
IND42	16600	¾
IND48	21500	1
IND54	27000	1½
IND60	32000	1½

Fans for corrosive fumes or excessive heat quoted on request.

This fan is one of the most efficient fans built today. Under static pressure, that is, operating in moderate length ducts or against automatic louvers, the Industrial fan can move more air with less power than most fans on the market. The carefully designed venturi orifice and blades make this efficiency possible.

The fan is belt-driven for three (3) reasons:—first, to reduce power consumption through increased efficiency of higher speed motors; second, to give more quiet operation through reduced fan speeds; third, to reduce original cost of fan to consumer.

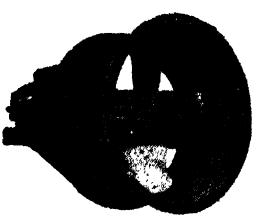
The frame is all steel, welded to a steel orifice. It is rigid, yet light in weight, simplifying installation.

On special order, these fans can be built to operate against static pressure up to 2 in.

TYPE OPJ—OCTOPUS JR.
Portable Exhauster and Blower

3-4" HOSES
CFM Per Hose
10' = 412 50' = 297

TYPE DXB—BOOSTER
Spray Booths, Fumes, Excessive Heat



16" to 36"
2000 to 9500 CFM

BB—ALL PURPOSE
Removes Smoke, Steam, Heat and Fumes

12" to 30"
1200 to 7000 CFM

Bulletins and Engineering Data furnished on request

Air Delivery Ratings of all Chelsea Products are in accordance with the *Standard Test Code* of the *Propeller Fan Manufacturers Assn.* and the A.S.H.V.E. INSIST ON CERTIFIED RATINGS. LOOK FOR THIS SEAL. ⟶

DeBothezat Fans Division

American Machine and Metals, Inc.

Main Office and Factory—East Moline, Illinois

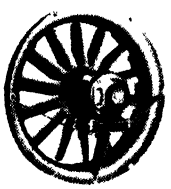
In Canada: AMERICAN MACHINE AND METALS (CANADA) LTD., 215 St. James St. West, Montreal 1, P.Q.

Foreign Sales Office: WOOLWORTH BUILDING, NEW YORK 7, N. Y.

SALES ENGINEERING OFFICES IN ALL PRINCIPAL CITIES

Certified Wind Tunnel Ratings • Non-Overload Power Characteristics

EFFICIENT AGAINST PRESSURE

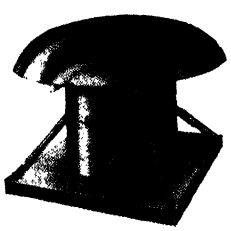


Axial-Flow Vent Set

DeBothezat Axial-Flow Fans are built in a wide range of sizes, from 16 inches through 12 feet in diameter. Volume fans (4 blades) are for low to moderate static pressures. Pressure fans (14 blades) are for high static pressures, up to 2 in. SP. Non-overloading power characteristic prevents motor burn-out and eliminates need for oversize motor. All DeBothezat Axial-Flow Fans have certified performance ratings. Catalog furnished on request.

DeBothezat Giant Fans, 5 feet through 12 feet in diameter, are suitable for gear, "V" belt or direct drive, for use with electric motor, steam turbine or gasoline engine. Catalog furnished on request.

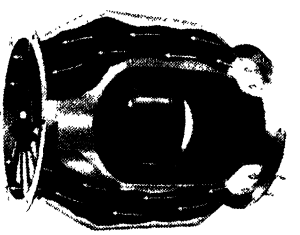
CONTROLLED VENTILATION



Power-Flow Roof Ventilator

Motor driven fan with weatherproof housing provides positive controlled ventilation at all times, independent of wind or weather. Streamlined appearance, low height. Operates efficiently with or without duct system. Hinged hood permits ready access to fan and motor. Available in four sizes, with fan wheels 16 in. through 36 in. in diameter. Catalog furnished on request.

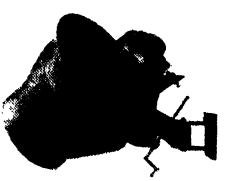
FUME REMOVAL



Bifurcator (Cut-away view)

For exhausting air that is abnormally hot, corrosive, flammable or explosive. Motor is mounted in separate, through-ventilated chamber completely isolated from air stream. Destructive fumes are by-passed (bifurcated) around motor. DeBothezat Bifurcators install directly in the duct, in any position from horizontal through vertical. Available in eight sizes, with fan wheels 18 inches through 48 inches in diameter. Catalog furnished on request.

SPOT COOLING



"Hy-V" Air Jet

DeBothezat "Hy-V" Air Jets are extraordinarily efficient man coolers, particularly for workmen who are exposed to radiant heat from ovens, furnaces, forges and molten metals. Arranged for either column or floor mounting, they are adjustable to blow a concentrated blast of cooling air in any direction to remote spaces without the aid of ducts. Available in 18 in. through 30 in. sizes. Catalog furnished on request.

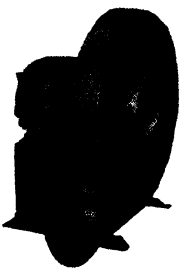
General Blower Company

8622 Ferris Ave., **Morton Grove 5, Ill.**

Engineering Offices in all Principal Cities

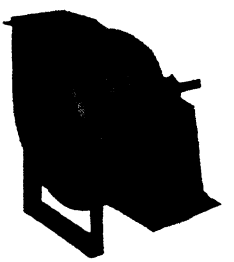
FOR BETTER AIR MOVING RESULTS USE GB LUNGS FOR INDUSTRY

Engineering • Manufacturing • Application of Blowers, Fans and Exhausters • for Blowing • Heating • Cooling • Conveying • Aerating • Separating • Agitating



A—Turbo Blowers

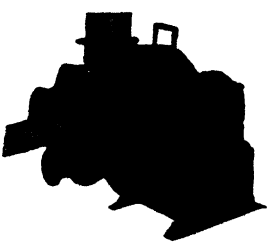
More than 20 years' experience in the construction of Blowers, Fans, and Exhausters for leading Industrial Users in widely diversified fields.



B—Steel Plate Exhausters

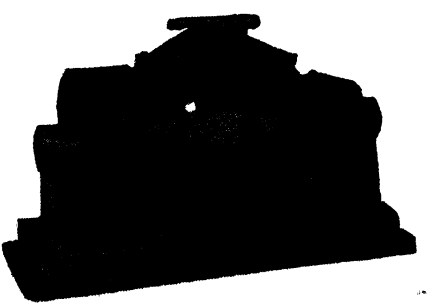
Engineering skill and integrity in the Building and supplying of Centrifugal and Rotary Positive types of Blowers, Exhausters and Gas Boosters enables us to supply you with the type of equipment best suited to your particular need, whether "standard" or "custom built."

We maintain Sales Engineering offices in all large cities. It is desirable and advantageous to consult with our local engineering representatives on all types of air-handling applications. They are at your service to help with your problems and to bring the engineering skills and resources of the General Blower Company to your organization.



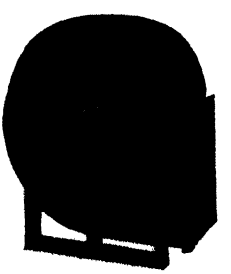
C—Welding Fume Exhausters

Write for our new, illustrated Products Bulletin
"LUNGS FOR INDUSTRY"



F—Rotary Positive Blowers

E—Exhaust Fans



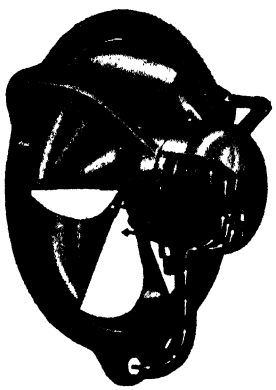
D—Multiblade Exhausters

ILG Electric Ventilating Co.

2876 North Crawford Ave., **Chicago 41, Ill.**

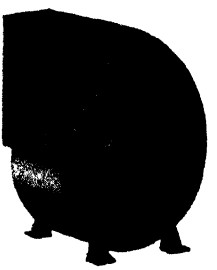
Offices in more than 40 Principal Cities

Propeller Fans, Centrifugal Fans, Unit Heaters, Kitchen Ventilators, Night Cooling Fans



ILG Direct-Connected Self-Cooled Motor Propeller Fans

Used for exhaust of stale air, fumes, heat, dust, odors, etc. Self-cooled motor combines protection of enclosed motor with low operating cost of open motor—constantly cooled by fresh, clean air, circulated internally—never "gums-up" from contact with foul air—saves 5 to 10 per cent on power costs. Rugged, heavy-duty framework. Dynamically-balanced fan wheel, direct-connected to motor. Smooth, quiet, effortless operation—economical, long lived. "ONE-NAME-PLATE" Guarantee. Certified ratings. Sizes, 8 in. to 54 in.



ILG Direct-Connected Centrifugal Fans

Type "BC"—Load-limiting type with backward curved blades. Motor load remains constant over wide range of air volume and change in static pressure. Wheel mounted directly on motor shaft with motor partially recessed in side of casing. No motor base required. Unobstructed inlet. 10 sizes. Also available for belt-drive in 12 sizes.

Type "B" Volume Blowers

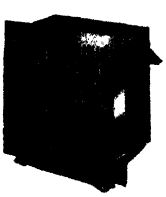
Small volume, low pressure, quiet running. Multi-blade wheel direct-connected to motor shaft. Cast iron base. Universal discharge. 12 capacities.

Type "P" Volume Blowers

For exhausting dust, fumes, removal of steam, vapors. Four discharge positions to avoid friction in short bends. 7 capacities.

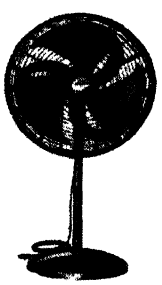
Type "6S" Utility Blowers

Designed for building into apparatus which requires ventilation or air movement. Extremely flexible in arrangement, furnished with or without inlet flange, outlet flange stand, etc.



Kitchen Ventilators

Built-in becomes permanent part of kitchen wall. Quiet high capacity, efficient, equipped with ILG Self-Cooled Motor. 3 sizes. Also models for window installation.



Night Cooling Fans

Portable model for use at attic or downstairs window. For permanent installation in attic, use ILG Self-Cooled Motor Propeller Fans (top of page).

JOY MANUFACTURING CO.

General Offices: Henry W. Oliver Building, **Pittsburgh 22, Pa.**

MANUFACTURERS OF VANEAXIAL FANS

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AND MORE THAN 500 DISTRIBUTORS THROUGHOUT THE WORLD

SERIES 1000 AXIVANE INDUSTRIAL AND COMMERCIAL FANS

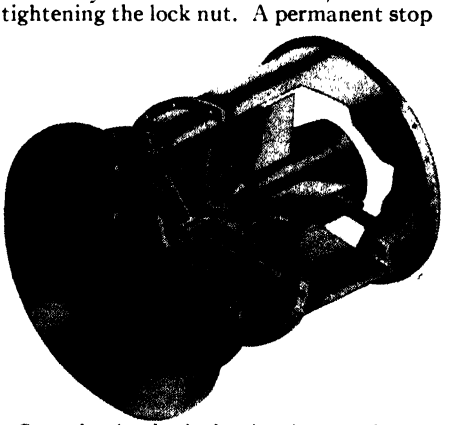
Joy Series 1000 adjustable blade **Axivane** Industrial fans are available in 124 sizes ranging in volume capacity up to 100,000 cfm with pressures up to 9.6 in. W. G. Housing diameters range from 18 in. to 60 in. For complete specifications, construction details, and selector charts giving pressure-volume range for each fan, write for bulletin number J-605.

Joy **Axivane** Series 1000 fans are efficient, quiet, compact, flexible, and easy to install.

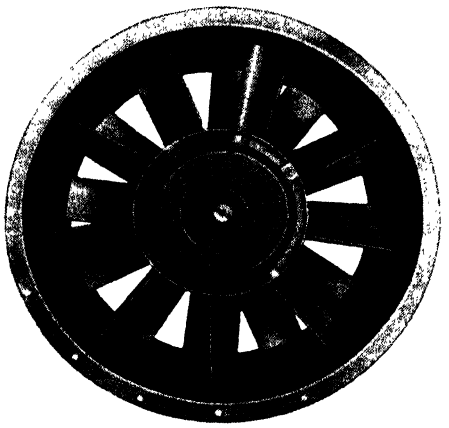
ADJUSTABLE BLADES

Joy **Axivane** Industrial Fans have the extra performance flexibility of adjustable blades. Adjustable blades, are standard equipment on all Series 1000 fans. The factory blade setting can be quickly changed to provide either a wide pressure range for any particular volume or a change in volume simply by loosening a lock nut with a wrench, setting the blades uniformly with the indicator, and re-tightening the lock nut. A permanent stop

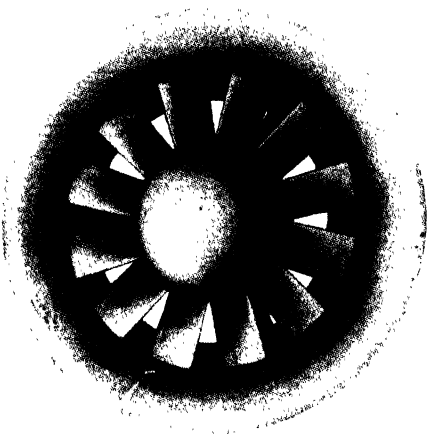
Blades are adjustable on the job by loosening one lock nut



Cutout drawing showing location of motor and compact construction



Rear view, showing vanes and motor



Front view, showing simplicity of construction

prevents setting blades in a position likely to overload the motor. Minimum blade settings are limited by the fan housing.

Adjustable blades permit on-the-job correction for unpredictable duct resistance or for poorly installed duct work.

MORE EFFICIENT

Stationary straightener vanes, located immediately behind the rotor, partially recover the rotative energy imparted to the air by the rotor, and re-establish axial flow to the air leaving the vanes. This eliminates excess turbulence at the point where the air enters the duct system and increases efficiency by decreasing pressure loss.

The Joy **Axivane** fan utilizes an aerodynamically efficient blade and stationary vane design.

QUIETER OPERATION

For equal weight and space the Joy **Axivane** fan is quieter than a centrifugal type fan of equal volume and pressure. The streamlined airflow from an **Axivane** fan makes sound insulation a simple and inexpensive operation when required for the ventilation and air conditioning of quiet spaces such as hospitals, auditoriums, radio stations, etc., where insulation against system noise must be used.

MORE COMPACT

Joy **Axivane** fans are built around the motor, the fan housing becoming an actual part of the duct system. This produces a more compact design than is possible with a centrifugal fan. An **Axivane** fan, installed on an in-line connection with ventilation ducts, parallel to and close by an overhead structure, may require 70 per cent less space than a conventional belt-driven centrifugal fan. The compactness of a Joy **Axivane** fan assures a maximum of net operating or rentable area. Fan rooms are virtually eliminated.

EASIER TO INSTALL

The Joy **Axivane** Series 1000 fan develops a greater volume and pressure per pound of fan and motor because of its compact, in-line construction. This light weight permits a simplicity of installation that minimizes installation costs and total weight by eliminating heavy foundations, complex duct offsets and elbows, drives, and guards. **Axivane** fans can be installed quickly and easily, even by relatively inexperienced or unskilled labor.

MATCHED ACCESSORIES

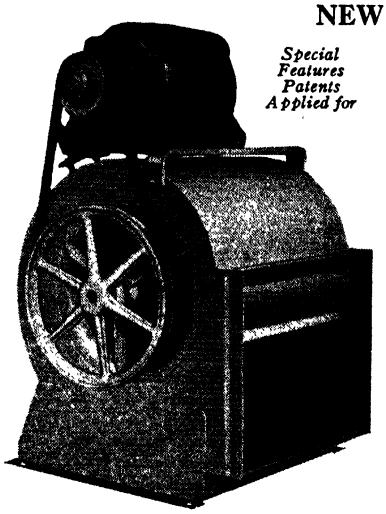
Inlet bells, screens, and fan supports are accessories designed to fit all **Axivane** Fan housings. In ordering, it is only necessary to state the model number with or without the accessories, as desired. If required with accessories these will be furnished to fit the fan model ordered without special number.

No matter how carefully a duct system is planned, an incorrectly selected inlet bell will reduce fan efficiency by increasing intake turbulence. This excess turbulence will also increase the noise level of the fan. When a fan takes its air directly from the weather, a plenum, a fan room, or from a duct system larger in circumference than the fan housing, a bell should be used.

The Lau Blower Company

2007 Home Avenue, Dept. H, **Dayton 7, Ohio**

Engineers and fabricators of general Air Handling Equipment
Blower Assemblies • Blower Wheels • Propeller Fans • Accessories

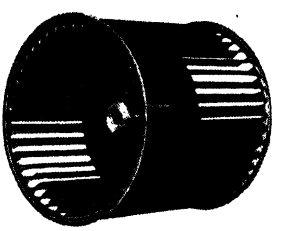


Special Features Patents Applied for

NEW Series "A" Blower Assemblies

The Lau Series "A" Blower Assembly—result of years of exhaustive tests of all types of blowers—years of research and design evolution—is the all-time, outstanding achievement in the blower field. Greater mechanical strength. Greater efficiency. A more compact unit (overall size considerably smaller than formerly). Will fit more jobs. Embodies many new and revolutionary features exclusive with Lau. Includes new 3-point suspension type bearing bracket—an integral part of the shroud—identical for various angles of discharge. New frictionless, self-aligning bearing—completely encased in Neoprene. New center suspension wheel (see below). New discharge outlet design and construction. Cut-off cannot set crooked on outlet. No wavy edges. Faster installations. New 1-piece motor mounting easily convertible, rear to top or vice versa, by simple use of two sheet metal screws. Many other features. Complete range of sizes. Every size tested and rated for performance in accordance with A.S.H.V.E. and *N.A.F.M.* Codes.

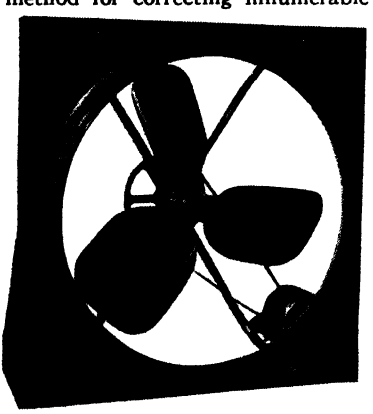
NEW Series "A" Blower Wheels

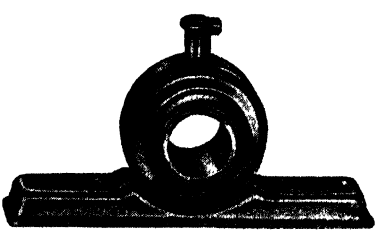


New center-suspension wheel *tested and proved* by us to have greater mechanical strength, truer concentricity, and far more efficient performance than ordinary types of wheel. Complete details supplied to interested parties upon request.

Propeller-type "Niteair" Fans

For a wide variety of applications where it is necessary or advantageous to exhaust undesirable air and provide fresh air from the outside. Equally applicable for industrial, commercial, residential and farm building installations. Efficient and economical method for correcting innumerable air-control problems—removing dust-laden, foul, contaminated, or excessively hot air, fumes, gases, smoke. Circulating cool night air through living and sleeping rooms for greater summer comfort. Venturi-type entrance housing reduces air "drag" and turbulence—eliminates most common cause of "air noise." 6 sizes—18 in. to 48 in.





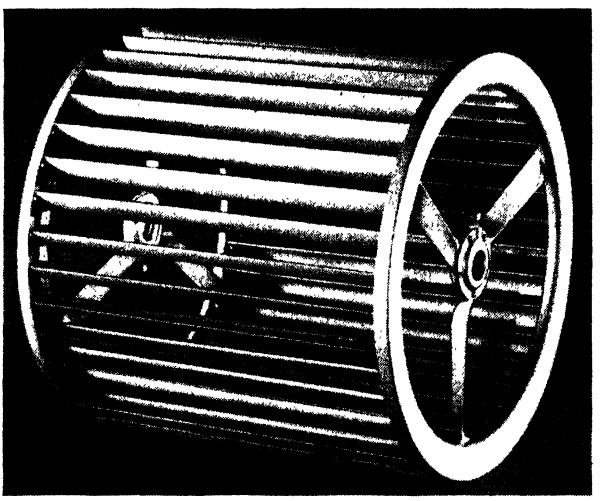
Self-aligning Pillow Blocks

Catalogs, performance data, specifications, and prices available on request on above and other air handling equipment. Inquiries solicited for any application. Our engineers will gladly assist you. *Write Dept. H regarding your requirements.*

Morrison Products, Inc.

A 25 Year Firm

East 168 Street and Waterloo Road, **Cleveland 10, Ohio**



BLOWER WHEELS

for

Manufacturers of Warm Air Heating and Air Conditioning

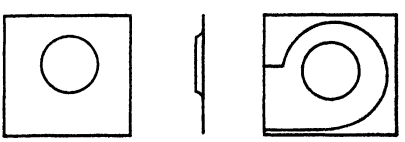
Morrison Airstream Blower Wheels are made exclusively for original equipment manufacturers in heating, ventilating and air conditioning. Wheels are double width—double inlet in standard diameters from 10 in. to 16 in. and in widths from 6 in. to 16 in.

One-Piece Blade Construction:—Blades made from single strips of steel on progressive die equipment. No possibility of blades coming loose.

Three-Piece Balanced Assembly:—Blower wheel consists of one-piece blade assembly and two pressed rings with integral hubs. These three pieces are spot welded together giving extra rigidity, strength and balance for smooth running.

Equalized Weight Distribution:—End mounting of blower wheels distributes weight closer to bearings. Smaller shafts and bearings therefore possible. Shaft whip eliminated. Shaft deflection reduced.

Available:—Complete engineering service including templates, shop drawings, tables, data, cost analysis, graphs, charts, sources of component parts.



- Housing Squares and Scroll Sides available for Low Cost Assemblies.

CATALOGS:

Morrison Blower Wheels
Morrison Engineering Service
Morrison Cost Analysis Estimate Book

Copies Mailed Upon Request

The NEW YORK BLOWER COMPANY
GENERAL OFFICES
3145 SOUTH SHIELDS AVENUE • CHICAGO 16
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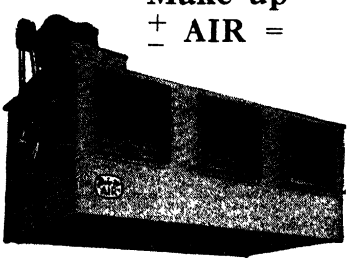
Representatives in Principal Cities

FANS • BLOWERS • UNIT HEATERS • MAKE-UP AIR UNITS
AIR WASHERS • HEAVY DUTY HEAT SURFACE

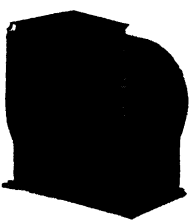
Make-up ± AIR =



M15—15,000 cfm

A unit that delivers, warmed, filtered, outside air to industrial spaces to replace exhausted air and balance minus pressure. Corrects drafty conditions and uncontrolled infiltration. Made in 4 sizes from 5,000 cfm to 20,000 cfm. Described in *Bulletin 453.*

Type ME Centrifugal Fans

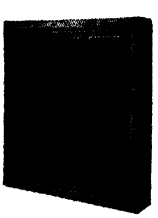


Capacities up to 101,000 CFM

Slow speed wheels offered from 7½ to 15 in. and 36 to 66 in. Capacities up to 70,000 cfm.

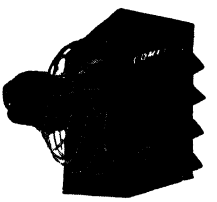
Quiet operating medium speed wheels with non-overloading horsepower characteristics for heating, ventilating and air conditioning or industrial applications. Wheel diameters from 18 in. to 66 in., with any speed or discharge required. Class I, II, III or IV construction. *Write for Bulletin 471*

Steelfin Hot Blast Heating Surface



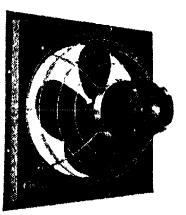
Extra heavy duty, fin-and-oval tube, all-steel, welded construction. A hot dip metallic coating over all, including headers, affords perfect bonding and conductivity. Suitable for continuous heating service on steam pressures up to 150 lb.

Comet Unit Heaters



Heavy duty, welded steel, fin-and-tube heating element. Suitable for continuous heating service on steam pressures up to 150 lb or more. 9 sizes with capacities from 31 Mbh to 300 Mbh. *Bulletin 454.*

Comet Exhaustair



Delivers large volumes of air at low resistance and low current consumption. All wheels are machine balanced for smooth, vibrationless operation. Made in two types and eight basic sizes. Wheel diameters from 12 in. to 60 in. Direct or belted drive. Capacities from 400 cfm to 22,000 cfm. *Ask for Bulletin 462.*

Type GI Industrial and Heat Fans

For dust and gas removal, conveying of materials and handling hot gases. Housings, drives, and discharge arrangements to meet any requirement. Wheel diameters from 14 in. to 66 in. Capacities from 450 cfm to 60,500 cfm.

Details and engineering data in Bulletin 461.

General Purpose Fans

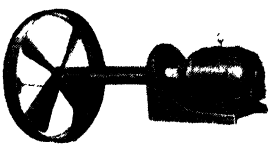
Portable, self-contained units for Class I industrial and ventilating applications. Recommended for ease of installation, low maintenance and space saving features. Made in three types and eight basic sizes. Capacities 400 cfm to 18,000 cfm. *Bulletin 482.*

PROPELLAIR Div.

ROBBINS & MYERS, INC.
1947 Clark Boulevard
SPRINGFIELD, OHIO

VENTILATING SPECIALISTS IN ALL PRINCIPAL CITIES

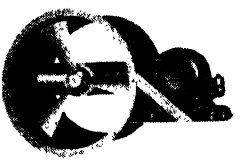
For Ducts, Walls, Windows, Hoods, Roof Ventilators



PROPELLAIR DIRECT-CONNECTED FANS

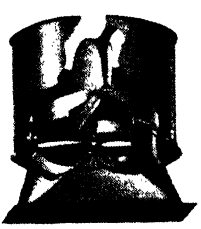
For use wherever motors may operate within the air stream, from free air to medium and relatively high resistance. A compact, durable design with fan having two to six blades. Sizes: 12 in. to 60 in. Capacities: 800-85,000 cfm. Type "CD."

For Heat, Acids, Alkalies—Fumes, Gases, Dust



BELT-DRIVEN PROPELLAIR DRUM-TYPE

A complete fan unit in short duct section ready for installation in lines from 20 in. to 48 in. diameter. Type "CS" may be used for severe acid or alkaline conditions, explosive fumes and gases. Type "CSV," for excessive temperatures, circulates outside air through belt and fan shaft tubes to keep drive and bearings cool. Also furnished without duct section. Capacities: 4100 to 43,000 cfm.



For Roof Ventilation

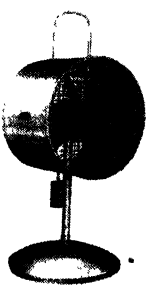
PROPELLAIR VERTI-STACK

Dependable and economical power roof ventilators. Butterfly dampers open wide the instant fan is started, close automatically as fan coasts to a stop, offer virtually zero resistance as heat, fumes, moisture, dust shoot high into air. Rain is prevented from entering by fan when operating. Drainage gutter prevents leakage when dampers are closed. Sizes: 20 in. to 60 in. Capacities: 3700 to 77,000 cfm.

For Heat, Moisture, Fumes, Dust, and Gases

PROPELLAIR EXTENDED-SHAFT FANS

This design locates motor outside air stream when fan is installed in duct at right angle turn, elbow, "Y," or offset. Simple installation usually can be supported by duct without auxiliary bracing. Drive shaft is enclosed and sealed within steel tube. Sizes: 12 in. to 60 in. Capacities: 2000 to 68,000 cfm. Type "CE."



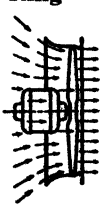
For Cooling Men and Materials

PROPELLAIR PEDESTAL & CRADLE-MOUNTED FANS

Pedestal-type Man Coolers have sturdy steel drum protected front and rear, formed steel base, rigid support, and crane hook. Also made with adjustable cradle mounting (Type "CU"). Capacities to 20,650 cfm.

AIRFOIL-SECTION Blades

Airfoil Principle Entrance Ring



Propellair fans have airfoil-section blades with variations of pitch, curvature, and thickness to compensate for different lineal speeds of points at various radii. Air movement is uniform over whole fan area. The Propellair curved entrance ring eliminates eddy currents; helps efficient Propellair blades deliver highest pressure and volume.

Schwitzer-Cummins Company

1145 East 22nd Street

Indianapolis 7, U.S.A.

Engineers and Manufacturers of Centrifugal Blowers and Blower Wheels—Attic Fans—Exhaust Fans—Ventilating Fans of All Types

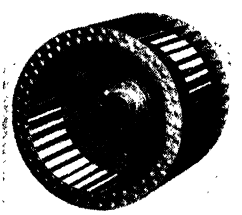
PRODUCTS OF THE VENTILATING DIVISION

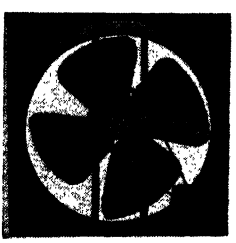
HY-DUTY BLOWERS SINGLE INLET AND DOUBLE INLET

Ruggedly built and designed for fine performance and quiet operation. Double inlet models, four outlet positions—single inlet models, eight outlet positions. Wheel diameters 8½ in. to 25 in.—200 cfm to 15000 cfm. *N.A.F.M.* code tested.

HY-DUTY BLOWER WHEELS

Large range of size, single and double inlet. Diameters 4½ in. to 50 in. Can furnish our standard wheel or to your specifications. Wheels for Hy-Duty Blowers are the center disc, wide blade type, accurately balanced.



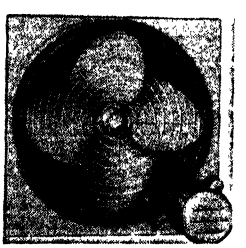


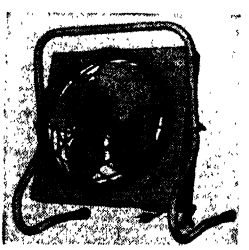
FRESH-AIR MAKER VENTILATORS

An all welded, light weight, low cost, high delivery, ball bearing ventilator with unusual flexibility for installations in homes, apartments, factories, business establishments.

←FIVE FAN DIAMETERS

24 in., 30 in., 36 in., 42 in. and 48 in. 4200 cfm to 20,500 cfm.





FRESH-AIR MAKER EXHAUST FANS

12 in., 16 in. and 20 in. arranged also for portable floor use or window mounting.

WINDOW OR ATTIC FAN

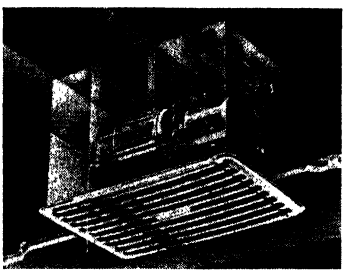
A handsome Fresh-Air Maker for universal application. Ideal for inexpensive installation in apartments and small homes. Air delivery 4200 cfm, very quiet. 24 in. fan diameter.

Trade-Wind Motorfans, Inc.

5725 So. Main St.
Los Angeles 37, Calif.

Representatives In All Principal Cities. Carried In Stock By Many Electrical Jobbers

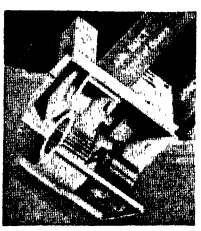
CLIPPER BLOWERS



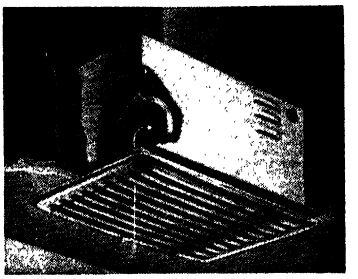
Phantom View of Model 1301 shows partition which isolates motor from air stream, increasing motor life.

The Trade-Wind Clipper Blower is a small capacity centrifugal blower, primarily used for exhaust application. While used extensively for home kitchen ventilation, it is widely used for other applications. Many thousands of these units have been in service ten years or more in school toilets, therapy and treatment rooms in hospitals and clinics, dental laboratories, ticket booths, offices, x-ray and photographic dark rooms, and hundreds of kindred desirable uses.

This is a "Unit Package" assembly, complete with ceiling grille and proper electrical connections. It is Underwriters approved and listed and carries a (prorata) five year guarantee, made possible by the use of the highest quality electrical motor component. The installation requires only the application of a discharge duct of the same dimension as the outlet collar and the optional addition of an automatic shutter for the end of the duct.

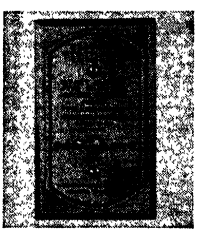


Motor and blower assembly easily removed without tools.

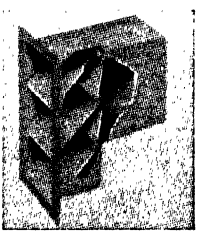


Model 1401 Clipper Blower, single wheel, vertical discharge, with "dripless" grille.

The assembly is inherently quiet and is installed rigidly in the structure without need for resilient mountings or flexible duct connections. Variable speed controls are available on single wheel models for the purpose of controlling variable air capacity. The blower is normally quiet at its maximum speed. The motor and wheel unit is removed easily without tools through the ceiling inlet opening. The patented construction of the Clipper entirely isolates the motor from the air stream. This exclusive feature adds to the service life of the motor and keeps the motor free from contaminated air.



Two-speed control unit fits standard single switch box.



Automatic shutters available for single and double blowers.

Selection Chart and Specifications
CLIPPER BLOWERS—110 Volt, 60/50 Cycles, A.C.

Cat. No.	Description	Type Blower	Net Air CFM*	Recommended Max. Room Size Cu Ft	Duct Size	Motor Watts	H.P.
1301 B Clipper	Horizontal Discharge Complete with Grille	Single Wheel	275	1500	7" x 4½"	100	1/30
1401 B Clipper	Vertical Discharge Complete with Grille	Single Wheel	275	1500	7" x 4½"	100	1/30
2501 Duplex Clipper	Horizontal or Vertical Interchangeable Discharge Complete With Grille	Two Wheels	425	2500	10½" x 5¼"	90	1/20

*This rating is based on ⅛ in. S.P. (W. G.) or the approximate resistance of 30 ft of duct the same size as outlet on Blower. The Blower will operate against a maximum of 3/10 in. S.P. with a reduction of approximately 4070 rated air capacity.

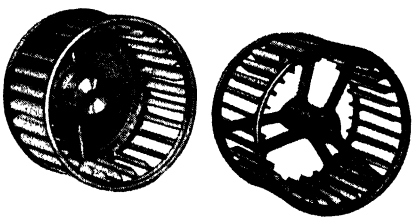
The Torrington Mfg. Co.

50 Franklin Street, **Torrington, Conn.**

Manufacturers of Blower Wheels and Propellor Type Fan Blades.

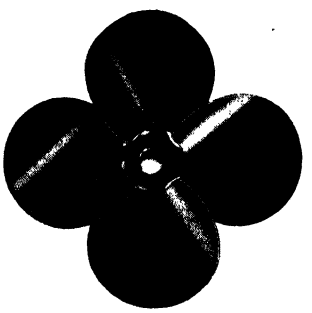
AIRISTOCRAT Quiet Propeller Fan Blades

AIROTOR Blower Wheels

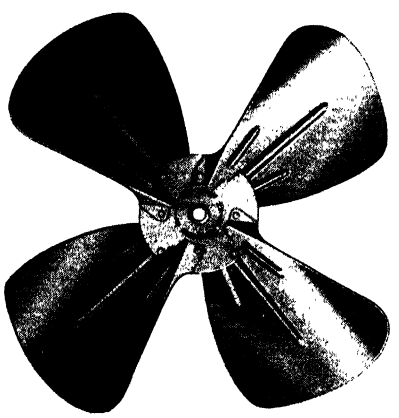


Left—Airotor Blower Wheel—Single Width—Single Inlet Patents 2,231,062; 2,272,695 Des. 126,043

Right—Airotor Blower Wheel—Double Inlet—Spider End Plates



Airistocrat "Standard" Series Pats. 2,072,322 and 2,021,707



4-Blade Airistocrat Attic Fan "M" Series

Torrington Airotor Blower Wheels are light, sturdy and inexpensive—incorporate new principles of design and construction, which insure rigidity and concentricity. **Single Width—Single Inlet** wheel is of simple four-piece construction. **No rivets or welds are used;** concentric rib serving as backing for blade strip is formed at same time as hub socket, insuring trueness of wheel. Rigid radial ribs prevent deflection by thrust. Three thicknesses of metal in rims make for maximum strength. Excellent for many heating and ventilating uses. Manufactured in both aluminum and steel in 1½ in., 2, 3, 3⅝, 4½, 5, 6, 7½, 9 and 10½ in. diameters. Clockwise or counterclockwise rotation. Same sizes available in DA type double width, double inlet wheels.

Torrington Airotor Blower Wheel—Double Width—Double Inlet—Spider End Plates. Has blades punched and formed in a single strip, rigidly held by flanged single piece end rings. Hubs are rigidly mounted by peening. Wheels of 2½ in., 3⅝ in., and 10½ in. diameter are available at present. Additional sizes now being developed.

AIRISTOCRAT Quiet Propeller Fan Blades are widely recognized for their all-around excellent performance. The unique, patented construction embodies entirely new principles in the art of fan design—produces a blade unsurpassed for quiet operation, rugged construction and attractive appearance. Every **Airistocrat** unit is carefully built and the blades are hand gauged for correct contour and alignment. Statically balanced, these blades deliver full air volume with a minimum of noise. Aluminum alloy blades and steel spiders are standard except where otherwise noted.

Available in a variety of finishes. Catalog gives detailed dimensions and guaranteed performance curves recorded under *NEMA* and *NAFM* code tests at various speeds for each of the **Airistocrat** models described.

New Blower Wheel Catalog charts capacities, gives detailed dimensions, suggests housing dimensions for all above wheels. Valuable "Tips" for designing air impelling units are also included.

"Standard" Series—Has blades mounted on a steel spider. Sturdy, attractive steel or aluminum blades which have withstood extreme laboratory breakdown tests. Sizes 8 in., 10, 12, 14, 16, 18, 20 and 24 in. diameters in a variety of pitches to meet every need.

AIRISTOCRAT "M" Series Attic Fan Blades—Three outstanding features of this new design are: (1) Extremely high efficiency, which gives maximum cfm per horsepower; (2) knockdown construction which drastically lowers shipping costs; (3) quiet operation—a point of major interest to the consumer.

This all steel four-blade fan is manufactured for attic use exclusively, in 36 in. and 42 in. diameters, in 40 deg pitch only.

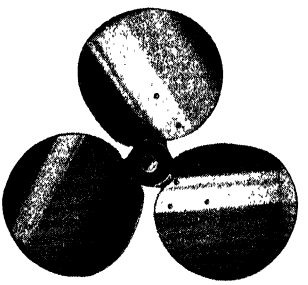
Three Blade "Y" Series—The design of this blade is the result of two years of laboratory experiment to produce a better air circulator blade. At recommended speed these blades produce a high velocity air stream effecting deep penetration with unusual quietness. Sizes 10 in., 12, 14, 16, 18, 20, 24 and 30 in. diameters, steel or aluminum blades.

Pressure "P" Series—Similar in construction to "Standard" Series but with blades especially designed for higher pressures. Sizes 10 in., 12, 14, 16 and 18 in.

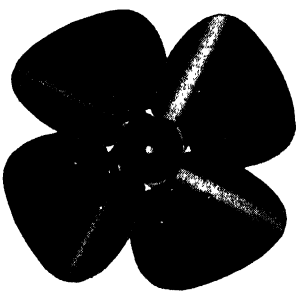
Pressure "U" Series—Four blade models of steel designed for pressure operation. Sizes 20 in., 22, 24, 26, 28 and 30 in. diameters.

AIRISTOCRAT "B" Series Attic Fan Blades have the same proportions, proved aerodynamically correct, in all diameters. New larger center disc and heavier spider arms increase strength and a new blade shape adds to the appearance of this carefully designed product. Available in 3, 4 or 5 blades in standard diameters 24, 30, 36, 42 and 48 in. All steel construction. Available in the following finishes: 1. Plain. 2. All one color lacquer.

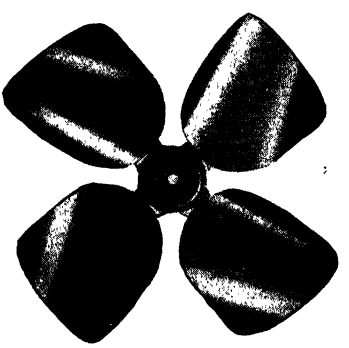
"One-Piece" Airistocrat Fan Blades—Exceptionally rigid models blanked from one piece of metal. Made in both steel and aluminum. Sizes 3 in., 4, 4½, 5, 5½, 6, 6½, 8, 9, 10, 12 and 16 in. diameters, all four blades; also 5½, 7, 8, 9, 10 in. 5-blade. Available in the following finishes: 1. Plain. 2. Lacquered. 3. Zinc or cadmium plated (steel only).



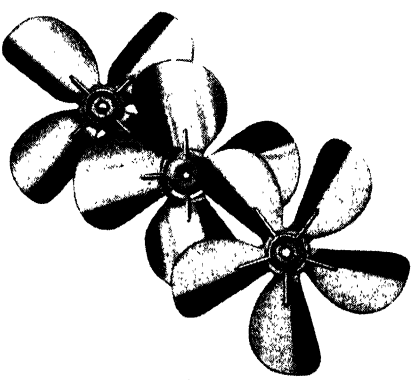
3-Blade Airistocrat "Y" Series



4-Blade Airistocrat Pressure Fan "P" Series



4-Blade Airistocrat Pressure Fan "U" Series



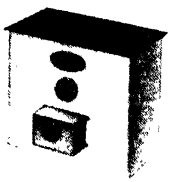
"One Piece" Airistocrat Fan

Utility Appliance Corporation

FORMERLY UTILITY FAN CORPORATION

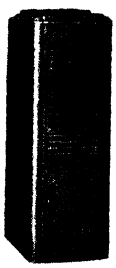
4851 S. Alameda St., Los Angeles 11, Calif.

Utility Gas-Fired Heating Equipment, Evaporative Coolers, Blowers and Fans



FLOOR FURNACES

Dual and flat register models . . . all-welded construction . . . vented . . . manual or thermostat control . . . draft diverter . . . die-stamped steel grille.



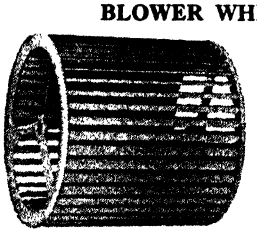
FORCED AIR FURNACES

Compact design permits use in basement or closet . . . dynamically-balanced blower rubber mounted . . . Fiberglas Dustop filters . . . heavy guage steel, die-formed and welded . . . baked enamel finish.

WALL-O-MATIC BUILT-IN CIRCULATING HEATERS

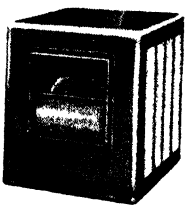
Delivered ready for installation, locked to 2 in. x 4 in. mounting studs . . . fits standard 4 in. stud wall without added furring. Single and dual discharge models. Thermostat or 3-position manual control. Vented.

BLOWER WHEELS



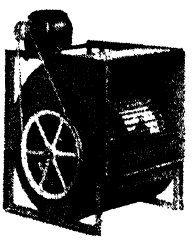
Improved five-piece welded construction . . . blades stamped from strip steel . . . certified air delivery ratings . . . dynamically and statically balanced . . . dual drive . . . venturi design end ring.

EVAPORATIVE AIR COOLERS



Comfort cooling . . . residential, commercial, industrial . . . dynamically balanced centrifugal blower . . . uniform water distribution to "No-Sag" cooling pads.

STANDARD BLOWERS



Dynamically balanced, multiple-vane centrifugal blowers. Four-side angle iron frame increases rigidity, eliminates vibration . . . permits installation with any of four discharge positions.

HEAVY DUTY BLOWERS

For increased air deliveries at higher static pressures. Dynamically balanced. Rigid construction. Single and double width.

PROPELLER FANS

Direct or belt drive . . . panel-mounted . . . streamline ring permits smooth air flow . . . resilient mounted motor . . . low speeds . . . 16 in. to 30 in.

Utility Blowers and Coolers are tested in accordance with the A.S.H.V.E. Code.

Utility heating appliances are *A.G.A.* approved.

Write for complete information, catalogs and price.

Western Blower Company

Founded in 1908

Manufacturers of Heating, Cooling and Ventilating Equipment for Public Building, Industrial, Commercial and Residential applications.

Main Office and Plant
1800 Airport Way
Seattle 4, Washington

Sales Offices in the principal cities West of Rocky Mountains.

TURBINE MULTIBLADE FANS—forward curved blade, Type TR, for heating, ventilating, drying, mechanical draft, etc. Bulletin No 31.

TURBINE STREAMLINED FANS—backward curved blade, Type S, with non-overloading horsepower characteristics, for same general purposes as Multiblade Fans. Bulletin No. 30.

TURBINE ELECTRIC VENTILATING UNITS—direct connected, and **PULLEY DRIVEN UTILITY SETS**—V-belt driven. For general utility duct ventilating systems. Bulletin No. 31.

WESTERN FURNACE FANS and BOOSTER FANS—for forced circulation of air in modern home heating and light ventilating duty. Bulletin No. 60.

RB VOLUME AND PRESSURE FANS—of the radial blade type, either direct connected or belt driven for varied ventilating and conveying applications. Bulletin No. 39.

SLOW SPEED PLANING MILL EXHAUSTERS—single or double for shaving exhaust systems. Bulletin 32-3.

MILL EXHAUSTERS—motor dirven, furnished single or double to suit motor speeds. Bulletin No. 32-3.

SPIROVANE PROPELLER FANS—furnished either direct connected or V-belt driven, for commercial or industrial ventilation. Bulletin No. 50.

WESTERN UNIT HEATERS—vertical and horizontal, for general heating and drying applications. Bulletin No. 53.

VOLUME HEATERS—with one or more centrifugal fans for heating, ventilating and air conditioning, available in veritcal and horizontal cabinet units with or without filters. Bulletin No. 54.

OLYMPIC Heat Exchangers, Converters, Side Arm Heaters, Immersion Heaters, Oil Heaters, and Condensate Coolers.

AIR WASHERS—for cleaning, cooling, humidifying and dehumidifying.

Bulletins as listed above furnished upon request.

APPARATUS DEPARTMENT

GENERAL ELECTRIC

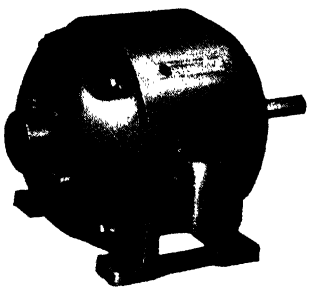
SCHENECTADY, N. Y.

Sales Offices, Warehouses, Service Shops, and Distributors in Principal Cities

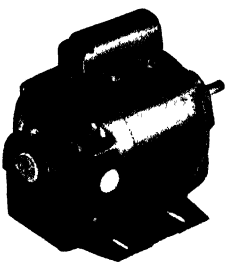
MOTORS FOR HEATING, VENTILATING, AND AIR CONDITIONING

General Electric offers a complete line of motors for compressors, fans, and pumps, from which you can select easily the motors with electrical and mechanical characteristics best adapted to your equipment. Many of the most common applications are listed below. Information on other motors—vertical, enclosed, etc., with various electrical and mechanical modifications—can be obtained at a G-E office near you.

For additional information, ask for Motor Catalog GEA-42S1.



Tri-Clad induction motor, Type K, polyphase*



Fractional-horse-power capacitator-motor, Type KC

SOME G-E MOTORS AND THEIR USES

Application	Speed	Type Winding	Type	Horsepower Range	Power-supply Classification
Fans and Centrifugal Pumps	Constant or Adjustable	Shunt	B & CD	1/8—200	Direct-current
		Compound	B & CD	1/8—200	
Reciprocating Pumps and Compressors	Constant	Capacitor, Normal torque	KC	1/4—3	Single-phase Alternating-current
		Capacitor, High-torque	KCJ	1—3	
Small Direct-connected Fans	Constant	Resistance, Split-phase	KH	1/40—1/3	
		Shaded-pole	KSP		
	Constant or 3-speed	Capacitor, Low-torque	KCP	1/50—5	
Belted Fans, Centrifugal Pumps	Constant	Capacitor, Normal-torque	KC	1/4—3	
		Repulsion-induction	SCR	5—10	
Reciprocating Pumps and Compressors	Constant or Multispeed	Squirrel-cage, Normal-torque	K	1/4—1000	Polyphase, Alternating-current
		Squirrel-cage, High-torque	KG	5—200	
Pumps, Compressors, Fans	Constant or Adjustable-varying-speed	Wound-rotor	M	1/2—1000	
	Constant	Synchronous	TS	25—2000	

Types of Enclosures: Open (dripproof)—protected from falling objects or dripping liquids. Splashproof — where wetness is a factor. Totally enclosed — for complete protection. Explosion-proof—for inflammable gases. Dust-explosion-proof—for combustible dusts.

*Trade-mark reg. U. S. Pat. Off.

APPARATUS DEPARTMENT

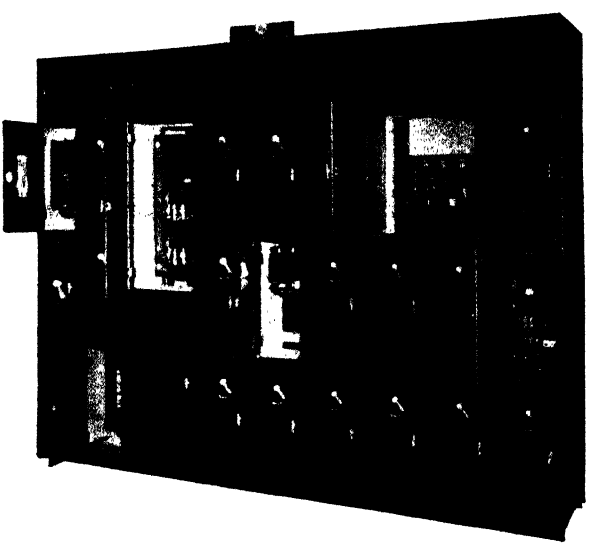
GENERAL ELECTRIC

SCHENECTADY, N. Y.

Sales Offices, Warehouses, Service Shops, and Distributors in Principal Cities

CONTROL FOR HEATING, VENTILATING, AND AIR-CONDITIONING MOTORS

General Electric offers a complete line of standard manual and automatic controls for all types of motors driving compressors, fans, pumps, etc. Publications describing these items, as well as such control accessories as pressure governors, pressure switches, float switches, electrically operated valves, and indicating selsyns, are available on request. For special applications, G-E control to meet your exact requirements can be designed. Most frequently, however, the needs of the air-conditioning industry are best served by one of the many possible G-E "packaged" control combinations designated as Cabinetrol* equipments.



Typical Cabinetrol unit, showing open motor-starter panels

The Cabinetrol system of motor control is based upon the use of standardized enclosures equipped with standard control devices. General Electric can build quickly most air-conditioning control systems—simple or complex—by properly combining standard control units and accessories into the required number of basic Cabinetrol sections. If future expansion should require further control equipment, additional Cabinetrol units can easily be added to the basic system.

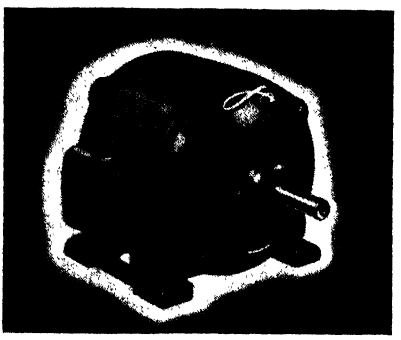
The standard enclosures used in the Cabinetrol system will mount standard motor-starting devices up to and including NEMA Size 4. Ample space is provided for incoming-line, feeder, and metering equipment. Bulletin GEA-3856 details more fully the advantages of this new system of centralized low-voltage control.

The General Electric Company will gladly assist in the solution of any electrical problem related to air conditioning.

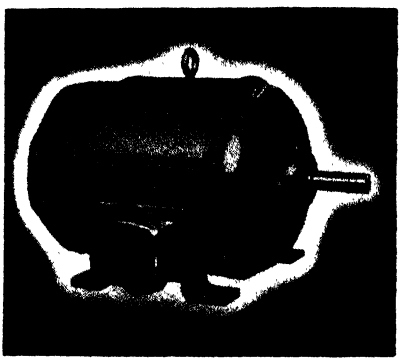
*Trade-mark reg. U. S. Pat. Off.

The Louis Allis Co.

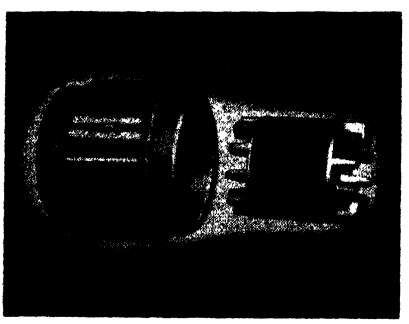
Milwaukee 7, Wisconsin



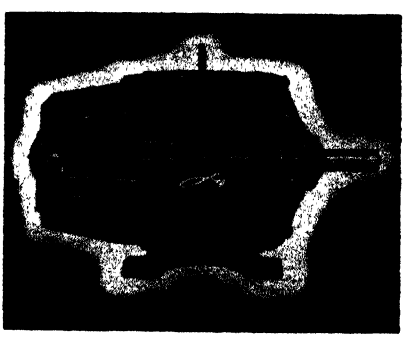
Louis Allis protected type Squirrel Cage motors (Type OG) are specially engineered and designed for applications requiring greater protection.



These Direct Current motors are correctly engineered and precision built—available in a very wide range of both electrical and mechanical modifications. The extra rugged construction of these motors assures long life to dependable performance.



The wide-spread experience of our engineering staff will be placed at your disposal to assist in powering your product with these compact efficient Shaftless motors. Available in a wide range of sizes and electrical modifications.



Wound Rotor (slip ring) motors are ruggedly constructed throughout. A wide range of speed variations are obtainable with comparatively simple control. Available with mechanical modifications for every industrial use.

We manufacture a size and type electric motor for every industrial requirement.

Wagner Electric Corporation
EST. WE 1891

6464 Plymouth Avenue
St. Louis 14, Mo., U.S.A.

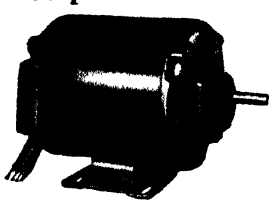
Sales Offices in 29 Principal Cities

SINGLE-PHASE
POLYPHASE
DIRECT-CURRENT
MOTORS

For Heating, Ventilating and Air Conditioning Equipment

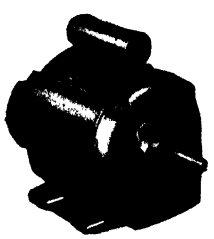
SINGLE-PHASE MOTORS

Repulsion-Start Induction



1/6 to 15 hp, all standard frequencies and voltages; sleeve and ball bearings; open or totally enclosed; horizontal and vertical; rigid, flange, or resilient mounted (in smaller ratings).

Capacitor-Start Induction

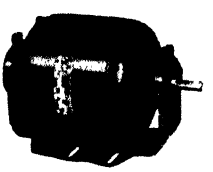


1/6 to 3/4 hp, all standard frequencies and voltages; sleeve and ball bearings; dripproof and totally enclosed; horizontal and vertical; rigid, resilient and flange mounted.

Permanent Split-Capacitor

1/20 to 3/4 hp, constant speed, two-speed, or adjustable-speed, all standard frequencies and voltages; sleeve bearings; totally enclosed; round frame with rubber rings.

Shaded-Pole Fan Duty



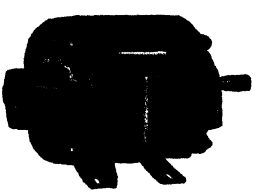
1/125, 1/80, 1/40 and 1/30 hp, 50 or 60 cycles, 115 or 230 volts; sleeve bearings; totally enclosed; rigid, round frame and resilient mountings; with or without 3-speed regulator.

POLYPHASE MOTORS

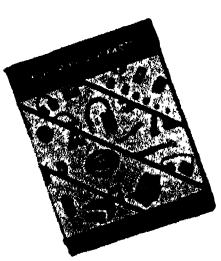
Squirrel-Cage Induction

1/6 to 400 hp, 2 and 3 phase, all standard frequencies and voltages; sleeve and ball bearings; open or totally enclosed; horizontal and vertical. Built in several electrical types.

DIRECT-CURRENT MOTORS



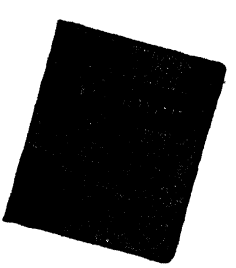
1/20 to 3 hp, all standard voltages, sleeve or ball bearings, dripproof frames, rigid mounted. Wagner direct-current motors in the 44 frame are shunt-wound, all others are compound wound.



Write For These Bulletins

MU-40—Lists part numbers and prices of Wagner motor repair parts, arranged for quick reference.

MU-185—Describes and illustrates all types of Wagner motors.

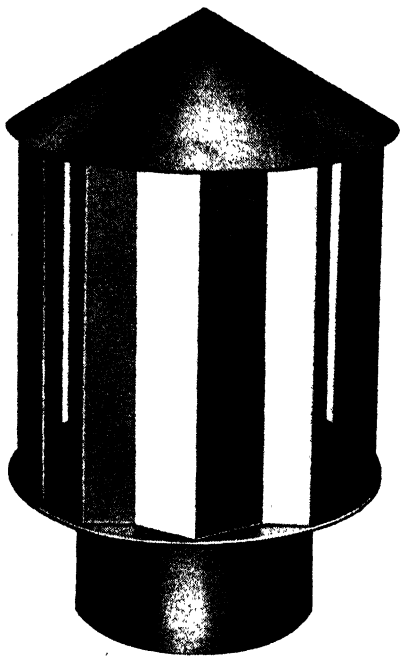


G. C. Breidert Co.

3129 San Fernando Road, **Los Angeles 41, Calif.**

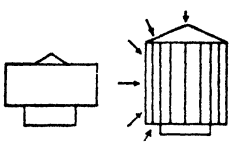
Representatives Located in Principal Cities of the U. S.

BREIDERT AIR-X-HAUSTERS FOR ROOF VENTILATING, VENT FLUES & CHIMNEY TOPS



Type B

The Breidert Air-X-Hauster introduces a new principle in ventilator design. Because of the revolutionary, aerodynamically-correct design of the Breidert Air-X-Hauster, wind currents striking it from *any* angle are converted into a powerful suction force that rapidly exhausts stale air from the interior of the house, kitchen or building. The Breidert remains stationary, has no moving parts. *Back-drafts are eliminated where there is no interior negative pressure!*



Old Method *Breidert Method*

The Breidert ventilator offers *certified* capacity ratings based on tests made with wind blowing at *all* angles (as shown). These high capacities were proved and certified by Smith, Emery Co., Pacific Coast branch of Pittsburgh Testing Laboratories. *Insist* on certified ratings based on directional wind tests at various vertical angles as shown in considering *any* ventilator. Breidert Air-X-Hausters were used extensively during the war on many types of combat and cargo ships, war housing, military barracks, and other government buildings. They also are widely used on all types of factories, commercial buildings, and residences.

For Kitchen Ventilation . . . The Breidert system provides a continuous, silent, effective circulation of air that exhausts heat and odors *at their source*, with no operating or maintenance expense. There are no "hang-over" cooking odors because the exhaust action of the Breidert is continuous. The neat, compact appearance of the "Type A" Breidert especially recommends it for residences.

For Vent Flue Caps . . . The Breidert does not have the defects of conventional types of caps and accessories. It eliminates the necessity for down-draft diverters, with accompanying dangers of explosion in case unburned gas accumulates or is blown into the room.

For Chimney Tops . . . By stopping all down-drafts (interior negative pressure excepted), a Breidert Air-X-Hauster on the chimney absolutely prevents the fireplace from smoking and damaging furnishings. *It provides positive "draw" regardless of wind direction!*

Write for Free Engineering Data Book . . . contains specifications and installation data, certified capacity ratings, etc. Address Dept. HV.

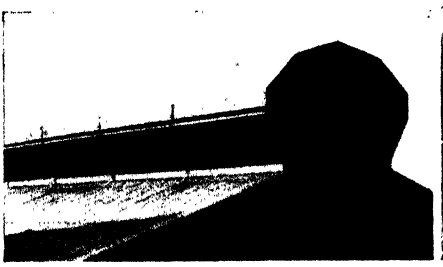
The Swartwout Company

18511 Euclid Avenue, **Cleveland 12, Ohio**

Representatives in Principal Cities

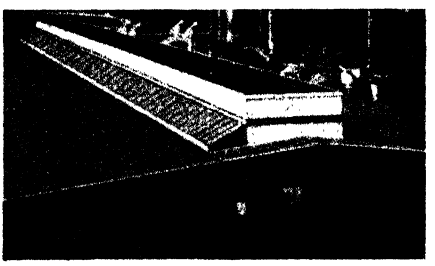
Gravity and Powered Industrial Roof Ventilators

GRAVITY ROOF VENTILATORS



Swartwout-Dexter Heat Valve

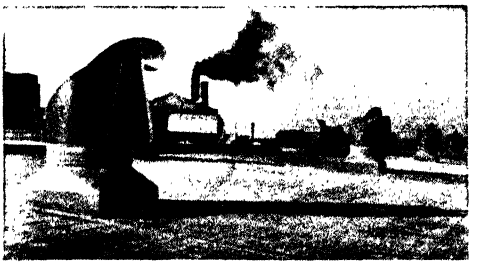
Continuous opening natural draft ventilator particularly effective for ridge of peaked roof, saw-tooth construction or skylights; adaptable to flat or slant roofs. Air takes but one turn, flows directly upward. Made in throat opening sizes 4 in., 6 in., 9 in., 12 in., 15 in., 18 in., 24 in., 30 in., 36 in. and 42 in. Ten foot lengths may be assembled continuously for any roof length. Adjustable damper.



Swartwout AIRMOVER

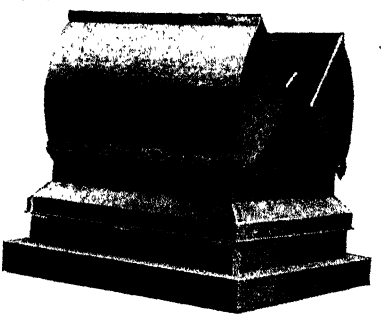
A horizontal type multiple heat valve featuring exceptionally short air travel, built in units 10 ft x 7 ft 6 in. x 32 in. high; 30 sq ft of opening per unit. Large scale ventilation achieved by use of continuous runs, or can be used as single units over heat concentration centers. Installed on curbs of wood, steel or concrete. Can be adapted to any type of roof.

POWERED ROOF VENTILATORS



Swartwout AIRJECTOR

Streamlined rotary head type roof ventilator using propeller type fan. Curved head turns with wind—outlet points away from wind to take advantage of suction effect. Made in 13 throat sizes, from 12 in. to 72 in., with wide range of capacity ratings. Adaptable to special conditions where high temperatures or fumes are a problem. Available without fan as a rotary gravity unit.



Swartwout JECT-O-VALVE

Powerful exhauster of the straight-through type, particularly effective over vats, furnaces, foundry pouring floors, etc. Air stream opens top dampers, which return to closed position when fan is off. Completely weathertight in either open or closed position. Hinged top section permits easy access for servicing. Made in 28 in., 36 in., 40 in., 44 in., and 48 in., throat size, in a variety of cfm capacities.

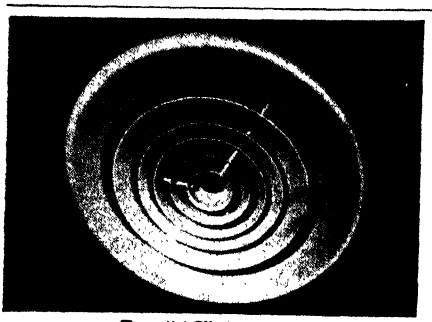
All of the above made in galvanized steel as standard; can be supplied in copper, aluminum, A.P.M. or stainless steel.

See *Sweets Architectural File* for further data, or send for complete Swartwout catalog, Bulletin 324.

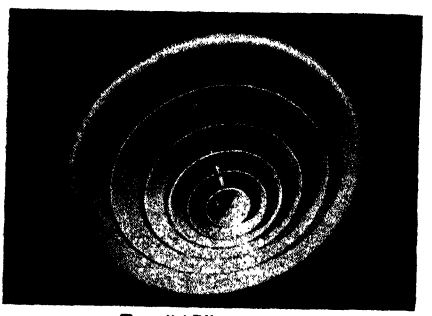
Anemostat Corporation of America

10 East 39th Street, New York 16, N. Y.

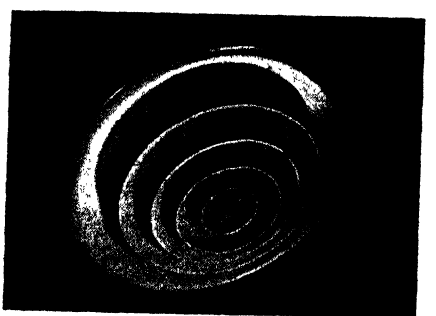
The Anemostat Draftless Aspirating Air-Diffuser



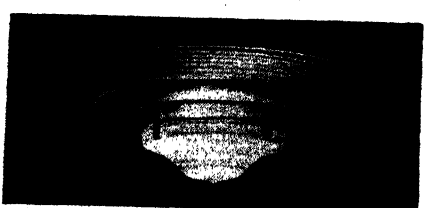
Type "AC" Anemostat



Type "AR" Anemostat



Type "B" Anemostat



Type "NL" Anemo-Light

THE ANEMOSTAT PRINCIPLE

ANEMOSTATS produce unparalleled results because of their unique design which operate on the following interdependent principles:

1. Air expansion within the device, which reduces velocity instantly.
2. True "Aspiration," which causes room air—equal to from 25 to 35 per cent of the supply air—to be drawn into the device, where it is mixed with the supply air. The percentage of aspiration depends on the type of Anemostat used.
3. Creation of a multiplicity of air currents and counter-currents at low velocities which cause slow but adequate secondary air motion.

CEILING OR WALL TYPES

TYPE "AC" ANEMOSTAT is a combination device for diffusing supply air and exhausting room air. It is designed to exhaust 75 cfm of room air for every 100 cfm of supply air. Furthermore, it has an aspiration effect of 30 per cent. The Type "AC" may be used with velocities up to 2500 fpm and wherever both supply and exhaust are required through the same unit. The Type "AC" Anemostat should not be used with ceiling heights exceeding 16 ft.

•

TYPE "AR" ANEMOSTAT is a diffuser for supply air only and aspirates a volume of room air equal to 35 per cent of the supply air. Type "AR" Anemostat is used in enclosures where temperatures to be maintained require a high rate of air changes.

•

TYPE "B" ANEMOSTAT is a diffuser for supply air only. It has 35 per cent aspiration. Type "B" may be used with velocities up 4000 fpm and is suitable for industrial and commercial installations. It can be used on either exposed or concealed duct work.

"NO AIR-CONDITIONING SYSTEM IS BETTER THAN ITS AIR-DISTRIBUTION"

NEW TYPE C-1 Anemostat is an *adjustable* diffuser for positive control of heated, cooled, or ventilating air. It may be used flush with ceilings or on exposed duct work. Any desirable air pattern may be obtained by simply turning the regulating knob.

An entirely new simplified method of installation is employed for the first time on this unit.

Complete technical data available.

•

TYPE "HU-3" and TYPE "HU-4" ANEMOSTATS are diffusers for the draftless, uniform and economical distribution of heat from vertical-discharge Unit Heaters. Both types provide approximately 25 per cent aspiration. "HU" Anemostats offer very little resistance to the air discharged from the heater. "HU" Anemostats may be combined with practically all sizes and types of vertical-discharge heaters on the market.

"HU" Anemostats are efficient and inexpensive diffusers for use also with general heating installations. They will function equally satisfactorily attached to either concealed or exposed hot air ducts.

•

TYPE "W" ANEMOSTAT is a diffuser of supply air from the wall-outlet. It has an aspiration effect of 35 per cent. Excessive air motion from the floor to well above the breathing level is eliminated . . . and the temperature differential, both horizontally and vertically between points in the occupied zone, is reduced to a minimum. The effective diffusion covers an area within a radius of 180 F. This result cannot be obtained by any other method which introduces air from a wall outlet.

•

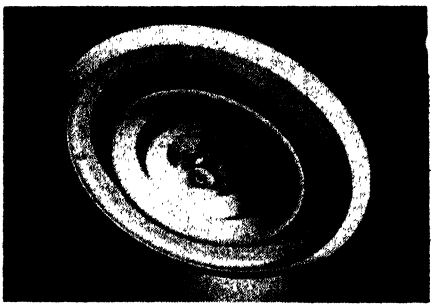
TYPE "NL" ANEMO-LIGHT is a combination diffuser and a built-in lighting unit . . . attractive in appearance . . . efficient in air-diffusing and lighting.

•

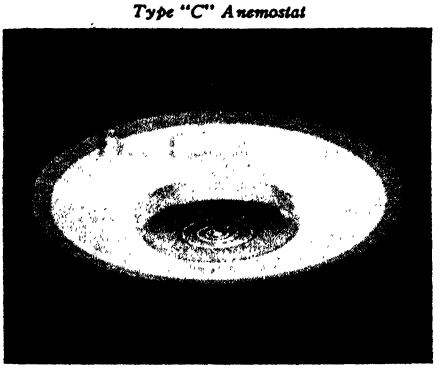
TYPE "CSL" COVE-LIGHTING COMBINATION is an indirect cove-lighting unit with a Type "CSL" Anemostat, particularly suitable for use in theatres and auditoriums . . . and wherever varied and unusual lighting effects are desired.

•

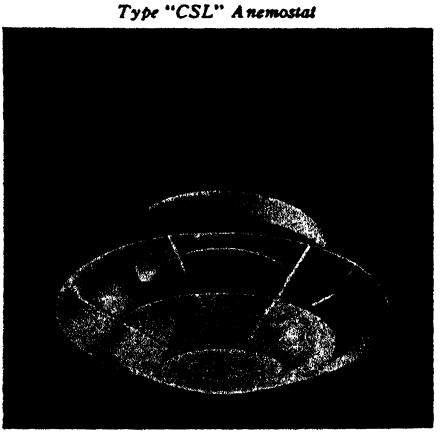
PENDANT LIGHTING FIXTURES of all types, standard or special, can be hung from the center of the ceiling-type Anemostat.



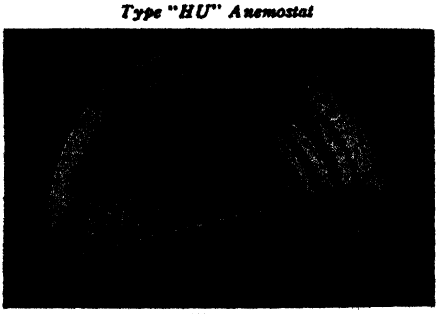
Type "C" Anemostat



Type "CSL" Anemostat



Type "HU" Anemostat



Type "W" Anemostat

"NO AIR-CONDITIONING SYSTEM IS BETTER THAN ITS AIR-DISTRIBUTION"

Air Devices, Inc.

Air Diffusers • Exhausters • Air Filters
Filter Holding Frames • Hot Water Generators

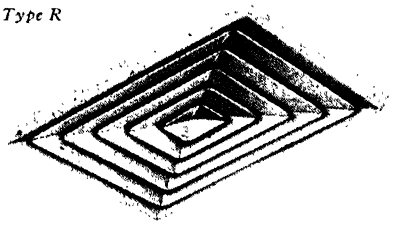
17 East 42nd St.
New York 17, N. Y.

AGITAIR PRODUCTS

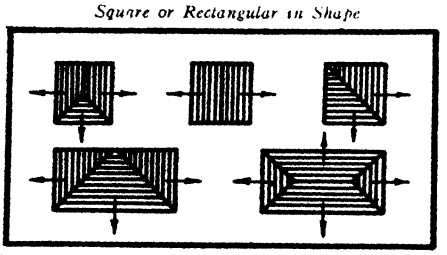
Agents in All Principal Cities

AGITAIR DIFFUSERS

Type R

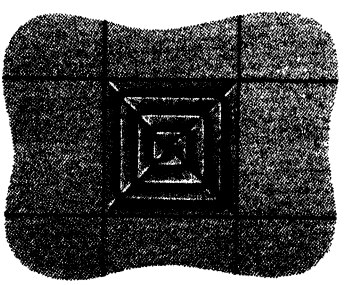


Square or Rectangular in Shape



Type R AGITAIR is the only diffuser that offers the higher efficiency of the square or rectangular shape in diffusing air quietly, draftlessly and with rapid temperature equalization throughout any shaped room. Its patented construction can be assembled into patterns which discharge the required amount of air in one to four directions.

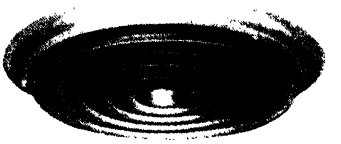
Each side delivers a quantity of air proportional to the areas served. Thus the engineer or architect can select an attractive diffuser that fits his design—rather than make his design fit the diffuser.

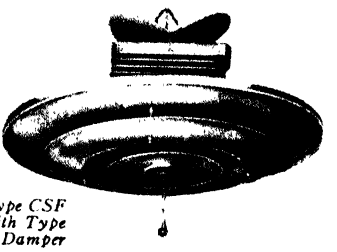


ACOUSTICAL CEILINGS

An improved, re-styled air diffuser known as the AGITAIR **Type RTC,** square or rectangular in shape, especially designed for installation in acoustical ceilings. Made in sizes to comform to standard tile dimensions.

Type A





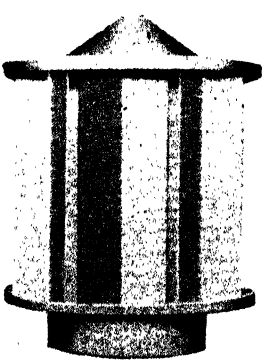
Type CSF with Type B Damper

Circular AGITAIRS combine beautiful design with finest operating features to give rapid temperature equalization and draftless diffusion of air. Model CSF is quiet, easy to install. Pressure losses at minimum. Type A diffusers are smaller, weigh less, are easy to install. Type CM is for marine use. In all sizes for all types of mounting and with lighting combinations. Dampers are provided where needed.

The AGITAIR Diffuser Data Book, available to architects and engineers, will help you design and install air distribution systems. Consult our engineers.

AGITAIR WIND-ACTUATED EXHAUSTERS

Provide proper ventilation regardless of wind direction, and with positive elimination of down-draft. Functions at peak efficiency at average low wind velocities. Will not restrict the flow of air or gases when there is no movement of outdoor air across the head. Fan-equipped units also for higher ratings. ***Bulletin EX-101.***



The Auer Register Co.

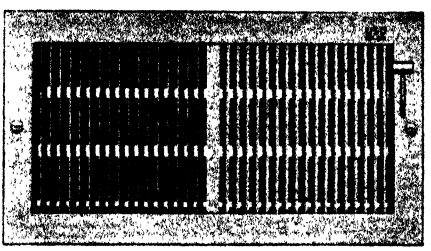
3608 Payne Avenue, **Cleveland 14, Ohio**

Manufacturers of Registers and Grilles for Gravity and Air Conditioning Systems; Metal Grilles for Radiator Enclosure, Ventilation, Concealment

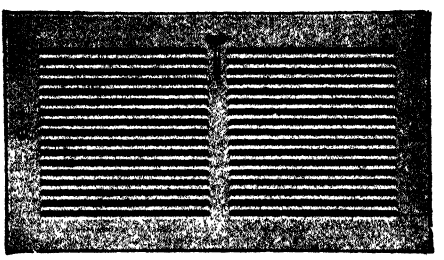
AIR CONDITIONING REGISTERS AND GRILLES

The Auer line of registers and grilles for all warm air heating and air conditioning systems is complete and modern, with a wide choice of styles for every purpose. Only a few are shown here. For gravity systems, the Auer Heat-Rite is a popular, streamline model adjustable for up-or-down flow. For extra strength, also for floor furnaces, use Dura-Bilt Registers and intake, with cross-bars set edgewise and all joints inter-locked and mortised. All Auer models are designed with due regard for air capacity, and supplied in all standard sizes and finishes. Latest Auer Register Book showing entire line sent on request.

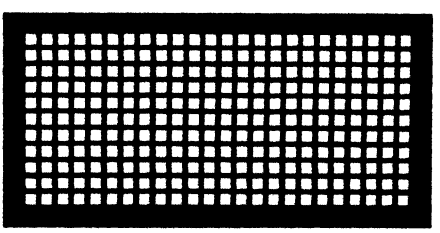
Auer flat stamped metal grilles are made in many designs, all sizes, for all purposes. Furnished in steel (or stainless), aluminum, brass, or bronze, and finished in prime coat, special finishes or platings. Send us your specifications. Ask for special Auer Grille Catalog "G," with full scale details and tables of openings and free areas.



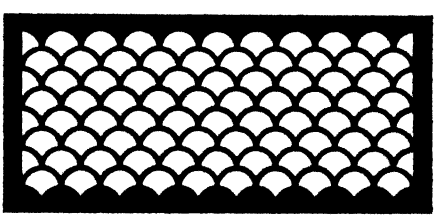
Airo-Flex No. 4432 Register—Multi-louvres adjustable up, straight or down. Grille bars adjustable for right or left flow. Grille to match.



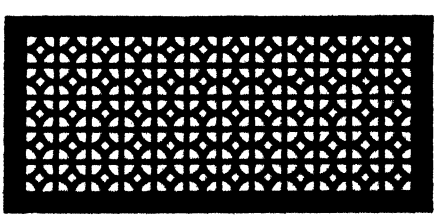
Airo-Flex No. 7032 Register—Grille bars set to direct air downward at 22½ deg, but adjustable for other angles. Single louvre. Grille to match.



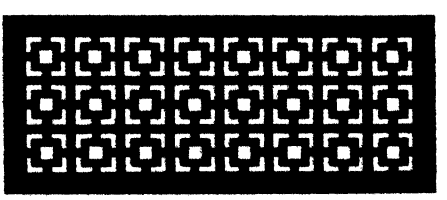
6A—Square Lattice Grille



32A—Shell Grille



4A—Moorish Grille



35A—Square Link Grille

Barber-Colman Company

Rockford, Illinois

ENGINEERED AIR DISTRIBUTION OUTLETS

VENTURI-FLO
Overhead Air Diffusers

Venturi-Flo overhead air diffusers have flow characteristics similar to those of the well known fluid-flow measuring device—the Venturi Meter. The relationship between the neck area of the unit proper and the Venturi-Flo throat area is so proportioned as to create a slight back pressure in the neck at all times, thereby automatically insuring uniform distribution around the entire periphery of the unit.

Three types of overhead diffusers are available, the recessed, the surface, and the thermostatically controlled types. A wide range of sizes permits handling air volumes up to 15,000 cfm per unit. Fittings for attaching any standard light fixtures to the outlets may be obtained for all designs. The surface and recessed types can also be furnished as combination supply and exhaust units and with adjustable dampers.

Uni-Flo Grilles and Registers are especially designed for air conditioning applications. They are engineered and prefabricated with directional flow fins for each individual application. Proper air distribution is assured and the necessity for adjustment after installation obviated.

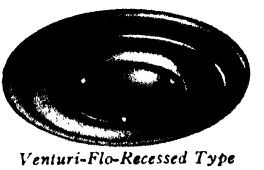
Uni-Flo Grilles and Registers can be furnished in a variety of shapes and sizes for plain and curved surfaces.

Registers are similar in construction to grilles but with the addition of spring loaded positive closing fan or key-operated dampers.

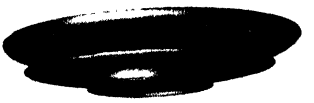
Electroplated Finishes: Gunmetal, brushed bronze, plain zinc, and satin copper; also available in gray prime coat and satin aluminum.

Uni-Flo Air Distribution Accessories: Include the Volocitrol and the Airturn. The Airturn is a scientifically designed and highly efficient air turning member. The aero-dynamically correct vanes reduce losses caused by eddies, reverse air flow and low pressure areas at the turn to a minimum. Airturns are prefabricated and are available in units of one piece construction in sizes up to and including 48 in. x 48 in.

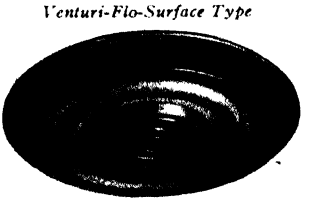
The Volocitrol has been designed to noiselessly provide positive and adjustable control of air volume, pressure and distribution across a supply outlet. They are available in two models, one for use with side wall and the other for overhead systems of air distribution.



Venturi-Flo-Recessed Type



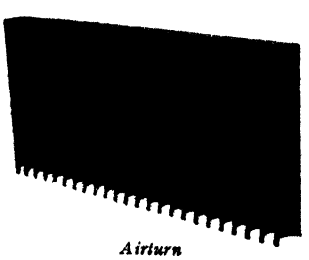
Venturi-Flo-Surface Type



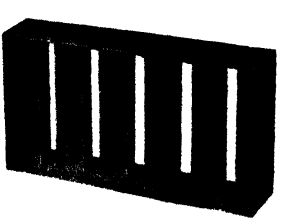
Venturi-Flo-Thermostatically Controlled Type

Uni-Flo Grille Model "M"

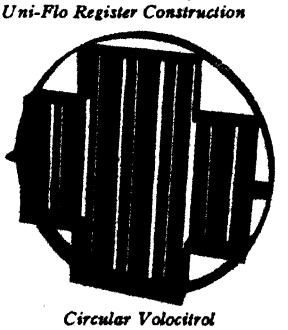
Uni-Flo Register Construction



Airturn



Volocitrol



Circular Volocitrol

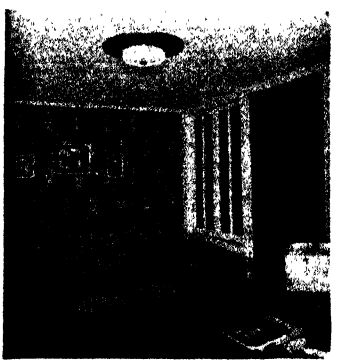
SEE OUR COMPLETE CATALOG IN SWEETS

Charles Demuth & Sons

Mineola, N. Y.

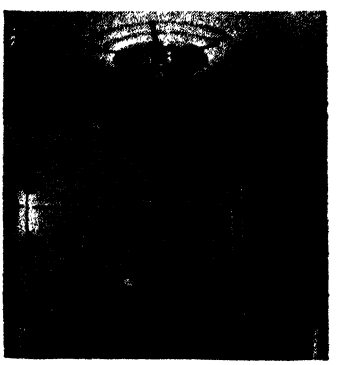
Air Distributors—Oil-Fired Conditioners

THE DEMUTH AIR DISTRIBUTOR is known to the Air Conditioning industry as the Distributor with Curved Vertical Vanes. Operates without any special attachments or devices. This special design imparts a series of turbulent air streams, resulting in a noiseless and positive 360 deg circulation and recirculation of the air—without a draft. Turbulent air streams plus an injector principle provides complete air mixture.



Type S-L

Type S



Special Type

FURNISHED in Polished or Satin Aluminum, Galvanized iron Stainless Steel and Enameled steel, as standard finishes, with sizes from 4 to 30 in.

Features a practical and simple installation method.

Available with lighting fixtures as shown in the left photograph.

All spinning operations required in the production of Demuth distributors are performed in the manufacturer's own shop.

Heavy Duty Industrial Oil Fired Forced Air Unit

Demuth "Samoyede" Oil Fired Furnaces

Heats, humidifies, filters and circulates the air. Domestic and Industrial models from 100,000 Btu to 2,500,000 Btu. Steel welded construction of Demuth patented design. Gun type oil burner, high temperature refractory combustion chamber. Large heating surface providing long flue passage, offers high efficiency and fuel economy.

Quick heating and troublefree performance. Enameled finish, with polished aluminum trim. All large sizes for industrial use made to order.

W. B. CONNOR ENGINEERING CORP.

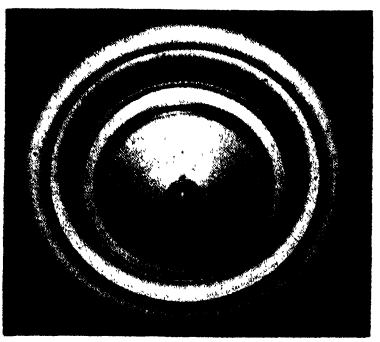
114 East 32nd Street, New York 16, N. Y.

Representatives in All Principal Cities

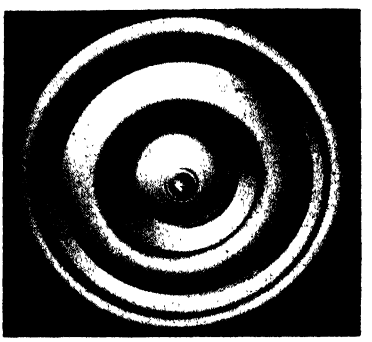
In Canada: Douglas Engineering Co., Ltd., Montreal, P. Q.

KNO-DRAFT *Adjustable* AIR DIFFUSERS

KNO-DRAFT Adjustable Air Diffusers insure efficient air distribution, maximum secondary air induction, noiseless and draftless diffusion, and uniform temperature throughout the occupied zone, *regardless* of season or ventilation requirements. Every KNO-DRAFT unit is easily and quickly adjustable for individual or seasonal requirements. The same KNO-DRAFT Diffuser is equally effective to expel chilled air **parallel** to the ceiling or eject heated air downward to prevent stratification.



TYPE KDA FOR SUPPLY AIR—Attractive—light, yet sturdy—for high or low ceilings or attachment to exposed ducts. Anti-smudge rim prevents streaked ceilings. Sizes 4 in. to 36 in. neck diameter for capacities from 50 to 15,000 cfm per unit.



TYPE SRD FOR SUPPLY AND RETURN AIR—To simplify duct work. Sizes 6 in. to 24 in. supply-air neck diameter for supply capacities from 50 to 2,500 cfm per unit, with central, return neck area 75 per cent of supply neck area.

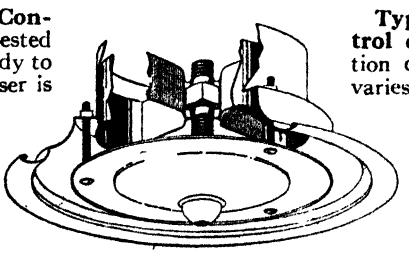
The KNO-DRAFT Diffuser will effectively distribute large volumes of air—premixing room and supply air. It permits the use of higher duct velocities—resulting in smaller ducts and lower costs. Duct designs are simplified and fewer outlets are required. KNO-DRAFT Diffusers are simple in construction, light in weight, and easily installed.

KNO-DRAFT Diffusers are geometrically proportional, size for size, insuring like resistance at like neck velocity for any size—and balanced static pressure throughout the system.

THE TYPE D AIR VOLUME CONTROL is designed for application exclusively to KNO-DRAFT ADJUSTABLE CEILING AIR DIFFUSERS. It is furnished already assembled within the diffuser and requires neither field assembly nor attachment to ducts, angle rings or other external appurtenances.

Type D Air Volume Control is adjusted and tested before shipment and ready to function when the diffuser is installed.

Its operation is entirely independent of the air direction adjustment which is part of all standard KNO-DRAFT Air Diffusers.



Type D Air Volume Control complements the function of the air diffuser. It varies only the *quantity*, not the *characteristic* of the air distribution. With it, a series of diffusers may be balanced without affecting the air diffusion efficiency.

With KNO-DRAFT TYPE KD ADJUSTABLE CEILING AIR DIFFUSERS the desired air pattern for any room or zone is AT YOUR FINGER TIPS

Kno-Draft Diffusers are covered by U. S. Patents Nos. 2,365,867; 2,369,119; 2,432,280 and others pending; Canadian Patents Nos. 429,206; 443,235.

APPEARANCE

The **KNO-DRAFT** Adjustable Air Diffuser lends itself well to any architectural or industrial requirement. Its simple, unobtrusive appearance and functional design make it an attractive air conditioning accessory in any commercial or manufacturing area.

UTILITY

An air diffuser is the sole "point of contact" between the conditioning system and the people it serves. If the diffuser is not adjustable *after installation* everything about that "point of contact" must be decided in advance. This can impose an often difficult, and always unfair, limitation on the designer. Air diffusion, especially in a room not yet built, can be a hazardous element to predict with complete accuracy. Air movement requirements, in a structure already built, may sometimes change with relocation of heat-producing equipment, people, or partitions. The advantage of adjustment *after installation* offers a new approach to this phase of the system design problem. With KNO-DRAFT Adjustable Air Diffusers, the behavior pattern of an air distribution system can, within fairly wide limits, be controlled, hence altered, after installation.

ECONOMY

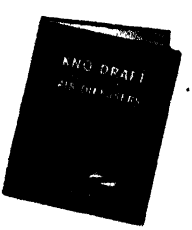
The economy of the KNO-DRAFT Adjustable Air Diffuser is a combination of three distinct economies, each contributing an added control over costs.

INSTALLATION—The self-contained removable inner assembly can reduce installation time by as much as 50 per cent. Where ceilings already exist the outer cone is attached to duct or collar quickly and easily.

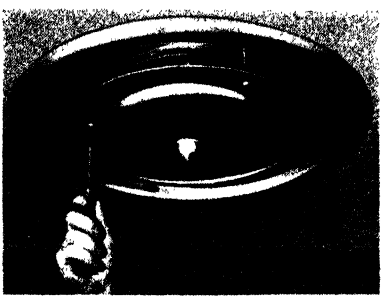
BALANCING—A minimum of time and effort is required to balance a KNO-DRAFT air distribution system. The single annular air stream permits immediate and accurate velometer reading. Desired air supply ratios may be rapidly obtained by adjusting the volume control dampers.

ADJUSTMENT — By simply raising or lowering the inner cone the diffuser is adjusted for any direction of air discharge from vertical to horizontal. By adjusting the volume control damper the air supply may be increased or decreased at will at individual points or zones.

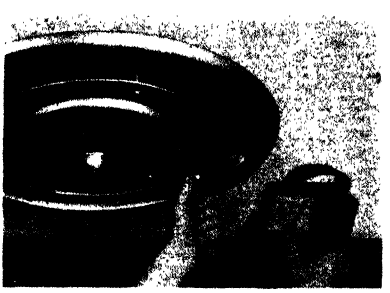
NEW CATALOG AND HANDBOOK—This new catalog contains in one complete and concise manual all the data necessary for the proper selection of air diffusers. Much information on air diffusion in general is included. *Write for Bulletin K-20.*



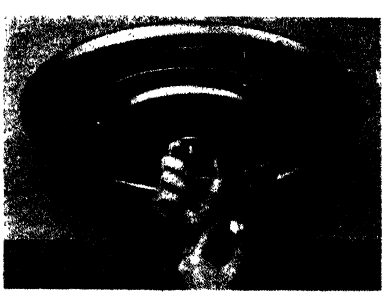
***INSTALLATION**—Removable self-contained inner assembly cuts installation time and costs.*



***AIR DIRECTION ADJUSTMENT**—Raising or lowering inner assembly provides any air direction angle—after installation.*



***BALANCING**—Single air stream allows direct velometer reading of volume immediately.*



***AIR VOLUME ADJUSTMENT**—Twist of wrist regulates air volume instantly after installation.*

(*See pages 1020 and 1021 for data on* DOREX *Air Recovery Equipment*)

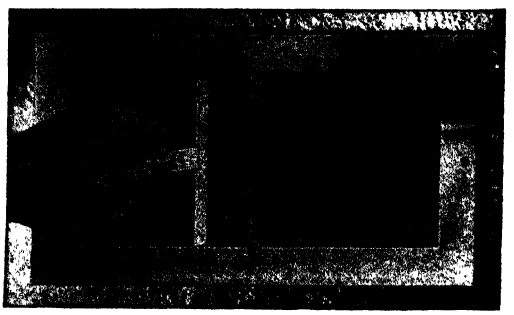
Hart & Cooley Manufacturing Co.

Established 1901

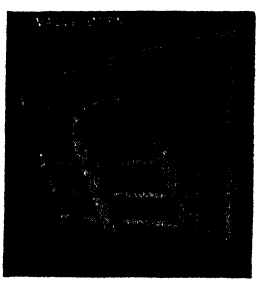
Air Conditioning Registers and Grilles - Warm Air Registers
Damper Regulators - Furnace Regulators - Pulleys - Chain

Holland, Mich.

NO. 75 DESIGN—FLEXIBLE FIN TYPE with TURNING BLADE VALVE to provide DOUBLE DEFLECTION. Also without Valve as Grille or Intake



CONTROL OF AIR FLOW IN TWO PLANES



Instant Adjustment of Air Flow (Up, Straight or Down)

Is obtained by turning the regulator on the register face to the proper setting with a key furnished with each register. When the valve is opened, as shown at the left, the individual valve louvres automatically stop in position to provide the proper air flow—Up (Fig. 1) for cooling systems to avoid drafts; Straight (Fig. 2) for ventilating systems; Down (Fig. 3) for heating systems to prevent stratification. When the valve is closed, as shown at the left below, it completely stops the flow of air.

Air Flow Can be Quickly Adjusted Sideways

No. 75 Design has a flexible fin-type face. Each fin may be twisted individually with a wrench furnished, to provide any desired sideway deflection of air flow.

Greatly Reduced Turbulence and Resistance

Figs. 1, 2, and 3 show the air flow with No. 75 Design; Fig. 4, with the conventional register. Compare the turbulence in the stackhead of the latter with the smooth flow obtained with No. 75 Design.

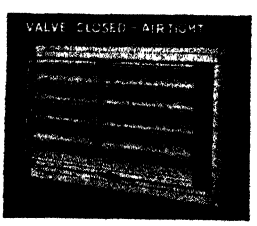
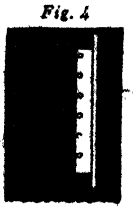


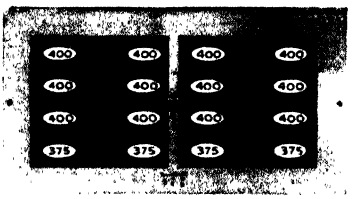
Fig. 1

Fig. 2

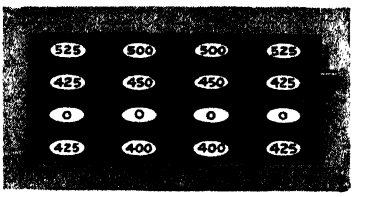
Fig. 3

Fig. 4





Velocities with No. 75 Design



Velocities with Conventional Register

EVEN DISTRIBUTION OF AIR OVER ENTIRE FACE

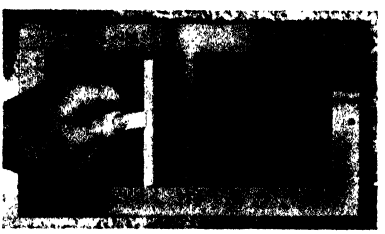
The turning blade valve distributes the air evenly with a uniform velocity over the entire face, as shown in Figs. 1, 2, and 3 on the preceding page. Note how the air rushes through the upper part of the face with a conventional register, as shown in Fig. 4. Since the entire face of No. 75 Design register is utilized for discharge of air, smaller and in some cases fewer registers can be used without causing excessive velocities.

Prevention of Streaked Ceilings—With either UP, STRAIGHT, OR DOWN deflections the air does not strike the ceiling immediately in front of the register; streaked ceilings are thus avoided.

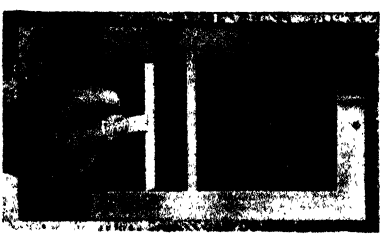
Excellent Concealment of Duct—The depth and close spacing of the vertical bars, combined with the valve, provide almost complete concealment of the duct, adding considerably to the pleasing appearance of the register face.

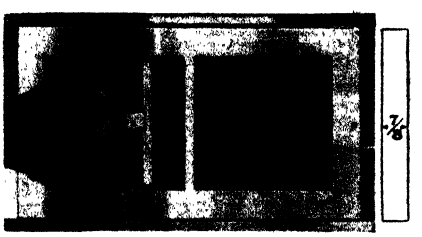
Special Settings—No. 75 Design functions equally well when located at the end of a horizontal duct or, by installing it upside down, when the air is delivered to it from above.

AVAILABLE IN FOUR TYPES



With Turning Blade Valve—No. 751 Register (Left) has Sponge Rubber Gasket and 3/16 in. turndown. No. 754 Register (Right) is similar except has 7/8 in. projection and is furnished without gasket.





Without Valve—No. 750 Grille (Left) has 3/16 in. turndown. No. 757 Intake (Right) has 7/8 in. projection

FOUR TYPES OF INSTALLATION FRAMES AVAILABLE

No. 75 Design items can be used with or without installation frames. No. 3 Sidewall Stud Frame (illustrated), fastens directly to stud, forming a solid, streak-proof foundation for register. No. 8 Frame is similar for baseboard use. No. 5 Baseboard Stack Frame provides inexpensive, streak-proof installation. No. 2 Band Iron Frame provides for connecting register to stackhead.

CATALOG 48 showing the complete H & C line, available upon request.

Hendrick Manufacturing Company

48 Dundaff Street, **Carbondale, Pa.**

Sales offices in principal cities—consult telephone directories

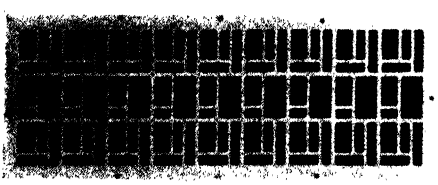
Hendrick Bulators; Hendrick Perforated Metal Grilles; Hendrick Mitco Open Steel Flooring, Armorgrids, Shur-Site Treads

HENDRICK BULATOR*

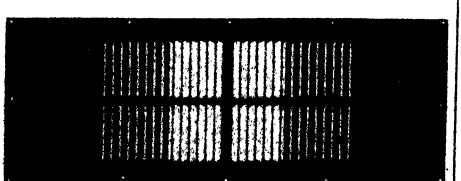
Recently developed by Hendrick, and tested at the Case Institute of Technology, Cleveland, the Bulator* Grille meets every requirement of architect and engineer for attractive appearance with proper air throw and spread.

Hendrick Bulator* is a practicable combination of an ornamental grille and a deflecting vane grille. The architect may select from a wide variety of Hendrick ornamental metal grilles a design that harmonizes with the decorative motif. Properly placed behind the ornamental grille, the deflecting vanes of the Bulator give the air throw and spread specified by the engineer. But the deflecting vanes are not noticeable behind the grille; only the decorative grille catching the eye.

The deflecting vanes are so constructed that the air flow can be deflected to right or left, up or down, or in a combination of directions.



Photograph taken with deflecting vanes less than an inch behind grille, shows that vanes are not noticeable.



Vertical deflecting vanes, showing how the vanes may be set to produce any desired air stream pattern.

The tests made under the direction of Prof. G. L. Tuve, at the Case Institute of Technology, Cleveland, show that correctly designed ornamental metal grilles, properly mounted in front of the deflecting vanes, have little effect on the air stream pattern and air throw.

Using a 24 in. wide by 8 in. high combination of control louvers, vertical deflecting vanes, and a metal grille with 65 per cent open area, the test showed the following resistance pressure in inches of water:

Cubic feet of air per minute				
400	600	800	1000	1200
with grille attached				
0.03″	0.08″	0.13″	0.21″	0.29″
with grille removed				
0.02″	0.05″	0.09″	0.14″	0.20″
Total throw of air stream, feet				
5.5′	8.2′	10.9′	13.6′	16.4′

The report states: "In the series of tests, we found that at a given air volume the presence or absence of the 'Mosaic' (pattern) grille made very little difference on either the air stream pattern or the throw, but the resistance was changed by the presence of the grille, as shown by the table."

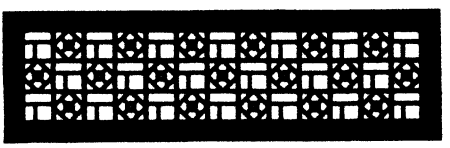
Hendrick's engineering department will be glad to cooperate with architects and engineers in the selection and installation of Bulator Grilles, incorporating any type of control desired.

*Beauty+Ventilator

HENDRICK PERFORATED METAL GRILLES

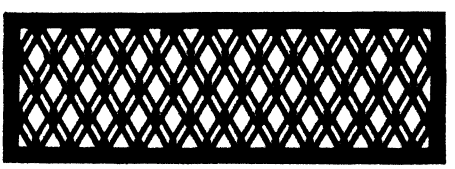
Hendrick decorative grilles are furnished in over a hundred patterns, and in a wide variety of overall dimensions, bar sizes, and number and size of perforations.

Many exclusive Hendrick designs, originally produced to meet an architect's specifications for some particular project, are now available as standard numbers, and facilities for making special designs to specifications make the Hendrick service even more complete. The wide range of patterns permits the choice of a grille that will harmonize with any style of architectural design or period construction.

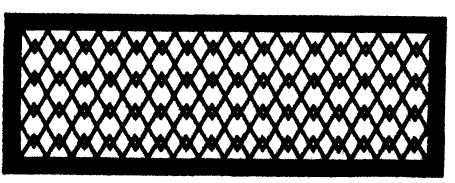


Arglin—63 per cent Open Area

Grilles are fabricated in heavy-gauge aluminum, bronze, copper, Monel, steel, stainless steel, and other commercially rolled metals. With ample open areas and accurate sizes, Hendrick grilles are characterized by clean-cut perforations, fine finish, and freedom from burrs and other imperfections.

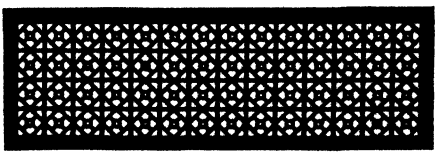


M–No. 8—57 per cent Open Area

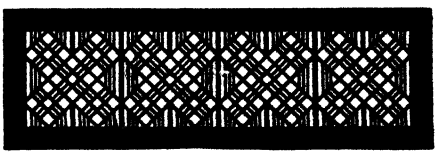


M–No. 9—67 per cent Open Area

They are easy to install, and always lie flat because of a special flattening operation in their manufacture.



Argive—60 per cent Open Area

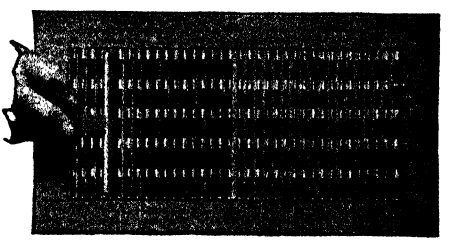


La Crosse—55 per cent Open Area

AIR CONDITIONING GRILLES AND REGISTERS

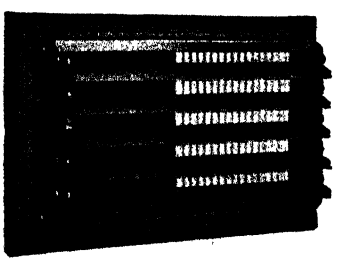
Hendrick air conditioning grilles and registers for directed air flow are made in various meshes, the standard having 3/8 in. opening between face bars. All types are furnished with either horizontal or vertical directional bars.

The standard mesh can either be furnished with grille bars permanently set at the factory for straight or directional air flow, or furnished so that the grille bars may be individually adjusted on the job to direct air flow to any desired degree.



Front View

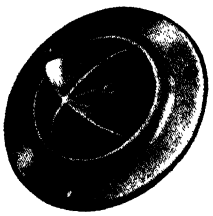
Rear View



Etablissements NEU

47 rue Fourier—Lille

Nord **France**



Vega

Any of the three following functions may be obtained with **Vega** ventilation outlet, invented by J. Fourtier:

—delivery of a direct air vein,

—diffusion of the delivered air,

—no delivery at all.

An adjustable device, formed by 4 semi-circular blades set in a circular opening, may change the direction and the diffusion of air delivered by the ventilation outlet.

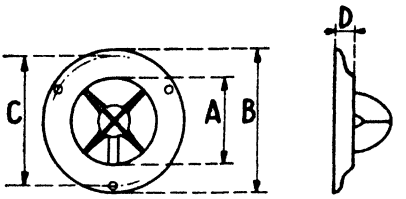
The **Vega** ventilation outlet is of a very reduced size, because the adjustable device is placed in the delivered air vein. Of very light weight, it is easily fitted up; it can be placed on a receiver supporting one or several devices, or on the ventilation duct itself, either vertical or horizontal. Its working is simple and rapid.

The various working settings and the numerous applications of this ventilation outlet place the **Vega** on a universal standard.

Ventilation outlet

Patent Applied for No. 665,689

Main Dimensions

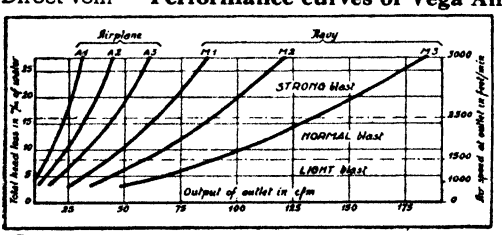


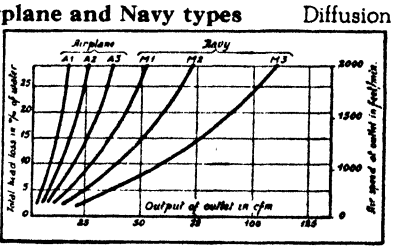
Type No.		Nominal Capacity cfm	A mm	B mm	C mm	D mm
AIRPLANE	A1	20	37.5	80	70	10
	A2	30	45	80	70	10
	A3	40	53	80	70	10
NAVY	M1	60	65	132	116	17
	M2	90	75	132	116	17
	M3	135	90	132	116	17

The special design and fitting of the device enable the quick adjustment of any outlet from one number to another.

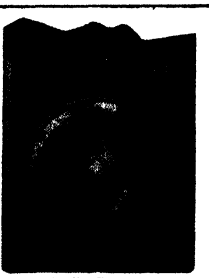
Vega ventilation outlet is made of cast metal or cast material; its finish is made to suit all applications and to be in harmony with any kind of decoration.

Direct vein **Performance curves of Vega Airplane and Navy types** Diffusion



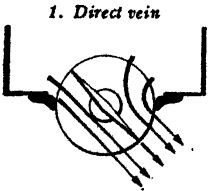


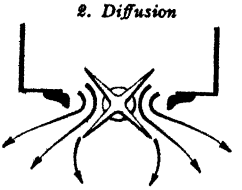
1. Direct vein

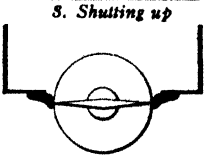


2. Diffusion

3. Shutting up







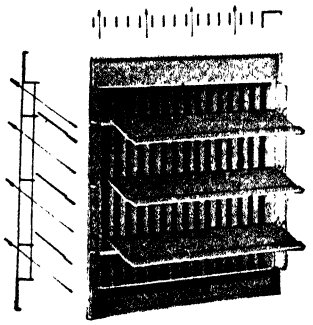
Main Position of Adjustable Device

The Independent Register Co.

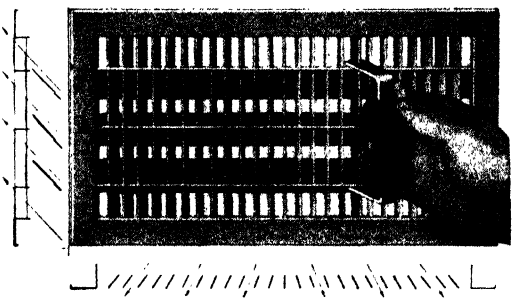
ESTABLISHED 1898

3747 East 93rd Street, **Cleveland, Ohio**

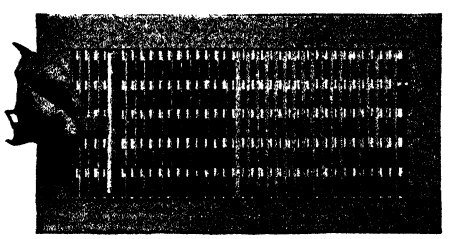
AIR CONDITIONING REGISTERS AND GRILLES



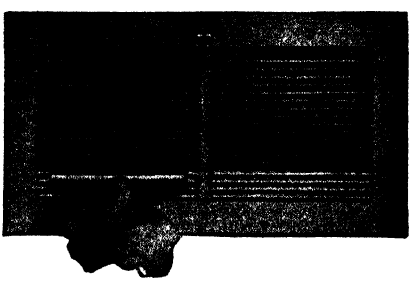
Rear View
Showing Adjustable Deflecting Vanes



No. 321A Grille with Deflecting Vanes—With vertical grille bars and horizontal deflecting vanes. The grille bars may be individually adjusted to direct air flows to right or left; and the vanes are made individually adjustable to deflect air flows up or down.



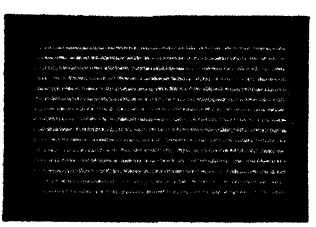
No. 238 Wrought Steel—4-way adjustable direction of air flow. Flexible vertical grille bars, multiple valves.

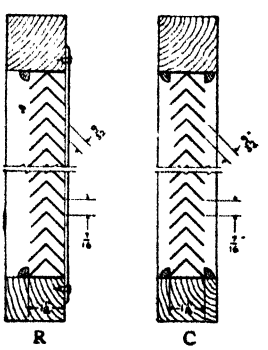


No. 139 Wrought Steel—Flexible horizontal grille bars, bendable for up, down or straight air flow. Single valves.

Independent No-Vision Grilles—No. 1312 for Doors, Walls and Partitions

The grille bars are "V" shaped; it is impossible to see through the grille from any viewpoint.





R C

No. 1312R—With overlapping rim ⅝ in. wide, on all four sides.

No. 1312C—With grille core only, installed with moulding.

The Pyle-National Company

1334-58 North Kostner Avenue, **Chicago 51, Illinois**

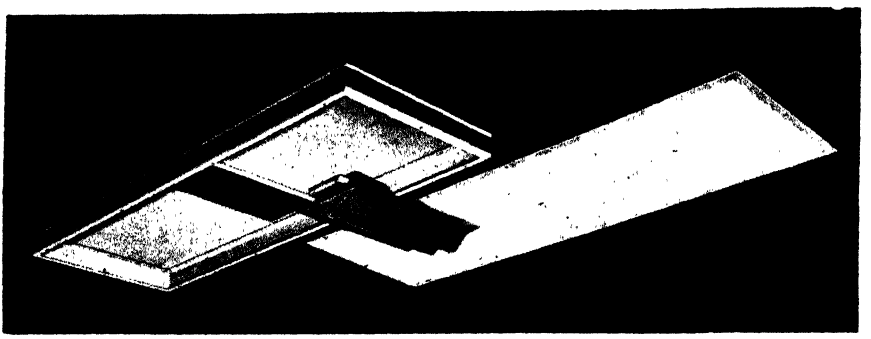
Representatives in Principal Cities

Manufacturers of

MULTI-VENT

Panels

for Heating • Ventilating • Air Conditioning



Control Plate *Valve* *Distribution Plate*

MULTI-VENT Panels are used for the even distribution of warm, cool or fresh air within room spaces. The control plate frame is inserted in the overhead duct at the ceiling. The orificed adjustable air valve provides absolute displacement of static head, and may be set for varying quantities of air to enter the conditioned space, and at varying velocities or speed of entry, producing the comfort zone rate of air motion and degree of temperature desired by the occupant (provided the system includes the required auxiliaries). The perforated distribution plate, of large area, located in the ceiling, accomplishes a wide, gentle, uniform spread and dilution of the conditioned air and simultaneously provides panel heating or cooling. When used with the other correct auxiliaries Multi-Vent results in uniform temperatures and comfort.

Application data will be furnished on request

REGISTER & GRILLE MFG. CO.

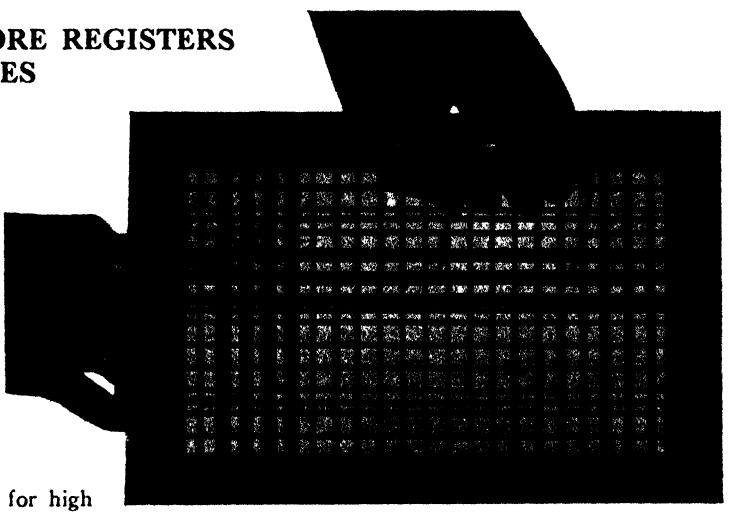
Incorporated

70 Berry Street, **Brooklyn 11, N. Y.**

Headquarters for all types of Registers and Grilles

RESIDENTIAL AND COMMERCIAL

DOUBLE CORE REGISTERS AND GRILLES



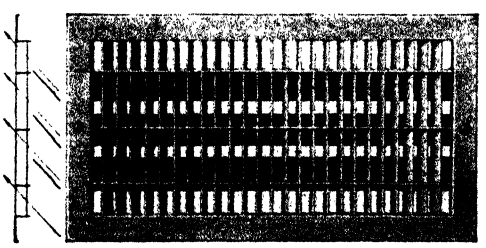
Designed only for high grade work where appearance and performance are the first consideration.

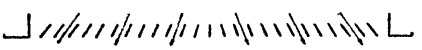
Style 620—Six-Way Adjustable Deflection

When used as a grille only, style 620 gives complete control of directional throw, and, when fitted with one of our many types of shutter, permits control of volume as well.

Can also be had with outside adjustable bars running horizontally (Style 610).

FOUR-WAY ADJUSTABLE DEFLECTION

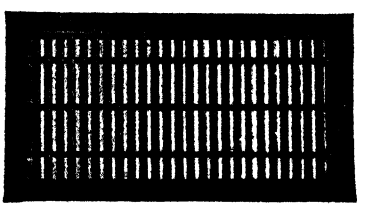




Style 20 Grille and HMV deflecting vanes

Front bars vertically adjustable, rear vanes horizontally adjustable; *or* Front bars horizontally adjustable, rear vanes vertically adjustable.

TWO-WAY ADJUSTABLE DEFLECTION



Use No. 20 Grille for adjustable right and left deflection. Style 10 has horizontal adjustable bars for up and down deflection.

Ask for our catalog which shows other types of air controls; also 81 different Stamped Metal designs and over 100 designs in Cast Metals—Iron, Brass or Bronze.

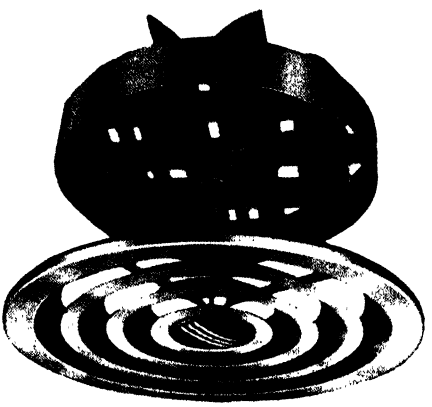
TUTTLE & BAILEY

Engineered Products for Residential, Commercial and Institutional Air Conditioning, Heating, Ventilating

NEW BRITAIN, CONNECTICUT

AEROFUSE

Diffuser and Damper



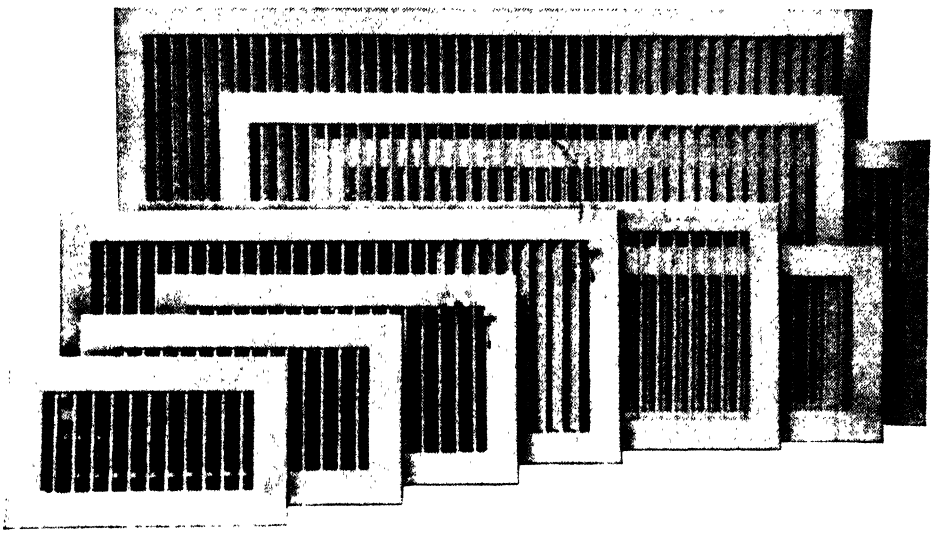
The satisfactory, efficient performance of an air conditioning installation depends largely upon the design of the units which provide distribution. The combination of Tuttle & Bailey AEROFUSE Diffusers and Dampers specified *at the vital point of air delivery* assures that this much of the system will do the job it is intended to do . . . provide the proper amount of supply air, delivered as you want it, where you want it, evenly distributed and without drafts.

Aerofuse Diffuser — Five standard types in a range of sizes—plus special adaptations for specific applications—means meeting the requirements of every air conditioning, heating or ventilating installation regardless of type or size of building. Rigid, one-piece construction facilitates installation . . . attractive appearance assures a design that will harmonize with any style interior.

Aerofuse Damper No. 4—An improved multi-louvre damper with exclusive designed-in features that provide positive volume control. Adds real efficiency when installed with AEROFUSE Diffusers. Minute adjustment of volume for accurately balanced system . . . multi-louvres divide supply stream, mean uniform distribution over diffuser, minimum turbulence and quiet operation. In open position, damper provides effective area greater than that of corresponding size diffuser . . . closed, it assures 100 per cent shut-off. Tamperproof, louvres may be locked in any position.

Tri-Flex SUPPLY AIR GRILLES AND REGISTERS

26 Standard Sizes for Quick Specifying, Easy Installation



T60 Grille—Full control of air deflection in horizontal plane. Individually adjustable bars, pivoted at front assure alignment regardless of setting.

T64 Double Deflection Grille—Combines T60 and deflector unit. Individually adjustable face bars and deflector blades.

T62 Multi-Shutter Register—Multi-Shutter unit attached to T60 Grille. Horizontal damper blades interlock when closed, eliminate air leakage. Lever or key operator.

T642 Double Deflection Multi-Shutter Register—Combines grille, deflector unit, multi-shutter damper. Provides 4-way air control. Face bars and deflector blades individually adjustable. Damper blades lever or key operated.

AEROVANE RETURN AIR GRILLES AND REGISTERS

T70-T80 Return Air Grille—Horizontal bars (T70) set for straight flow or 22 deg upward or downward deflection. Vertical bars (T80) set for straight flow.

T72-T82 Return Air Register—Combines AEROVANE Grille and multi-shutter unit as used with TRI-FLEX supply register. Same bar settings as T70 or T80.

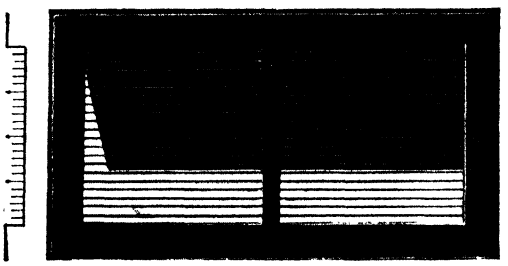
For detailed engineering data, write Tuttle & Bailey, New Britain, Conn.

United States Register Company

General Offices: **Battle Creek, Mich., U.S.A.**

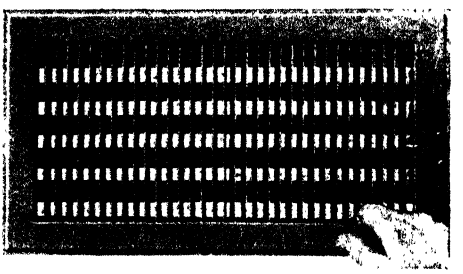
Branches: MINNEAPOLIS, MINN., KANSAS CITY, MO., ALBANY, N. Y.

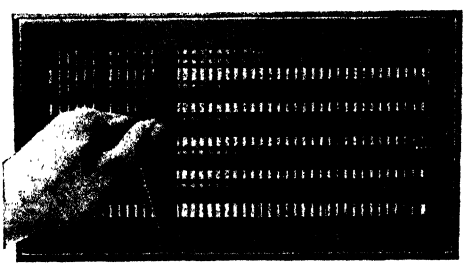
Air Conditioning Registers, Vents and Grilles



No. 153—Single-Valve Air Conditioning Register-Bars ¼ in. deep—Spaced 4 openings to the inch affords Non-Vision. Can be supplied in Directional Flow in either Horizontal or Vertical Bar Styles. Can be furnished with all styles of Setting Frames.

No. 249—Multiple-Valve Air Conditioning Register. Gives complete Air Control. Vertical Front bars—Key-pin adjusted to provide 45 deg Right and Left or Two-way Side Flow. Lever operated Horizontal Back-valves give from Full Closed to any degree of Up-flow and to 45 deg Down-flow. FULL FACE COVERAGE. Can be supplied with any style of Setting Frame. Fits all Stack Heads of Standard Size Dimensions.



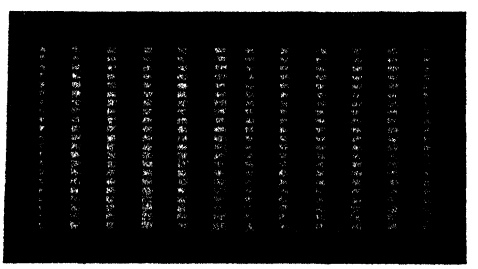


No. 256—Multiple-Valve Flex-bar-Air Conditioning Register. Vertical Front Bars set 22 deg Right and Left. Side Flow Deflection attained by setting of Grille Bars with bending wrench to accommodate room condition. Back-valves give same Up and Down control of air flow as No. 249 above. FULL FACE COVERAGE. Can be supplied with any style of Setting Frame. Fits all Stack Heads of Standard Size Dimensions.

All of above Styles can be supplied with either Lever or Individually adjusted Multiple Valves or Louvers. *i.e.* 177VVI—Vertical Valves Individually adjusted. 145VVL—Lever operated Vertical Valves.

Grilles and Vents in Matching designs are available.

For Complete Information Write for Latest Catalogs with Engineering Data.



No. 153-VVL Horizontal Bar Non-Vision Design-Vertical lever operated rear valves.

Complete Gravity and Air Conditioning Register, as well as Fitting Catalogs furnished on request.

Young Regulator Company

5209 Euclid Avenue, **Cleveland 3, Ohio**

DAMPER REGULATORS; REMOTE CONTROLS; VOLUME CONTROL GRILLES; DAMPERS

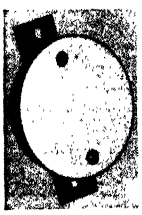
Manually and Automatically Controlled

Sales Representatives in Principal Cities

Young Regulators meet practically every condition where damper regulators are required for controlling air volume.

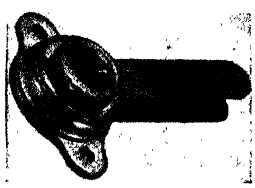
No. 1A—For installation in finished wall. May be locked in position.
No. 301 A and 201 A—For imbedding in plaster. Cover plate flush with finished wall.
No. 403 A—For mounting on duct lever adjustment. May be locked in position. Sizes ¼, 5/16 and 3/8 in.
No. 401 A—For mounting on duct. Key adjustment. May be locked. Sizes ¼, 5/16 and 3/8 in.
No. 900 A—For operating a splitter damper or deflecting vanes.
No. 656—End bearing provides a bearing for the damper rod at side away from regulator.

No. 1 A

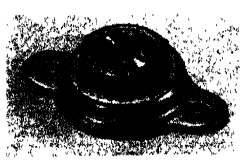


No. 301 A

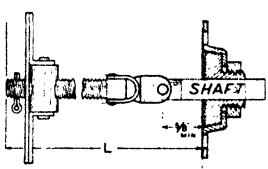
No. 201 A



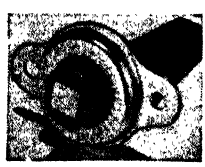
No. 403 A



No. 401 A



No. 900 A



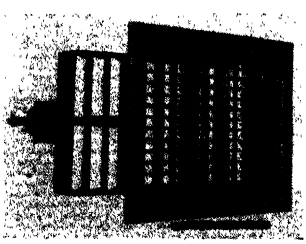
No. 656

Young Remote Control and Dampers.

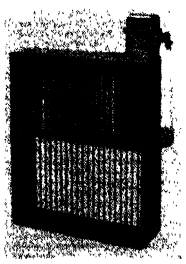
No. 700 A—For remote control of one or more dampers at distances up to 250 ft or more.
No. 704—Corner pulley eliminates friction on long rung or where there are many turns.
No. 915—Volume control grille gives equal distribution of air over entire grille and directional flow.
No. 815—Relief damper controls temperature in individual rooms. Remote bulb thermostat regulates dampers to give desired temperature in each room.

No. 700 A

No. 704



No. 915



No. 815

The American Rolling Mill Company

Executive Offices, Middletown, Ohio

ATLANTA 3, GA., 1437 Citizens & Southern Natl. Bank Bldg.
BALTIMORE 13, MD. ..... 3400 E. Chase St.
BERKELEY 2, CALIF. ..... Seventh and Parker Streets
BOSTON 16, MASS. ..... 439 Park Square Bldg.
BUFFALO 2, N. Y. ..... 504 Seventeen Court St. Bldg.
CHATTANOOGA 2, TENN. ..... 409 Chattanooga Bank Bldg.
CHICAGO 4, ILL. ..... 310 S. Michigan Ave.
CINCINNATI 8, OHIO..24 Cooper Bldg., Hyde Park
CLEVELAND 15, OHIO..... 1516-20 B. F. Keith Bldg.
COLUMBUS 15, OHIO ..... 724 Atlas Bldg.
DALLAS 1, TEXAS..... 2112 Tower Petroleum Bldg.
DAYTON 2, OHIO ..... 1802 Mutual Home Bldg.
DETROIT 2, MICH. ..... 5-261 General Motors Bldg.
HOUSTON 2, TEXAS ..... 1640 Commerce Bldg.

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SOUTH BEND 21, IND. ..... 3202 W. Sample St.
TULSA 3, OKLA. ..... 501 Mayo Bldg.

Choose the Correct ARMCO Grade

There is a grade of ARMCO sheet steel especially suited to every air conditioning application. For detailed information get in touch with the nearest district office or write direct to The American Rolling Mill Company, 390 Curtis St., Middletown, Ohio.

ARMCO Ingot Iron
(Galvanized)

Ducts
Washer Chambers
Plenum Chambers
Steam Line Casings
Spray Towers
Drip Pans
Housings
Machine Guards
Unit Conditioners
Roof Ventilators
Eliminator Blades

ARMCO PAINTGRIP
(Galvanized)

A special mill-Bonderized galvanized sheet that can be painted without pretreatment. Preserves life and beauty of paint and enamel.

ARMCO Cold Rolled PAINTGRIP: A zinc-flashed sheet with a special mill-Bonderized surface that takes and holds paint.

Hot Rolled
(Sheets and Strip)

Fan Blades
Blower Casings
Fuel Oil Tanks
Unit Conditioners
Stoker Hoppers

ARMCO ZINCGRIP

A special zinc-coated sheet that can be severely formed without peeling or flaking of the tightly adherent zinc coating. Also available with a mill-Bonderized finish for immediate painting.

Cold Rolled
(Sheets and Strip)

Furnace Casings
Room Unit Casings

Plates
(ARMCO Ingot Iron)

Smoke Stacks
Coal Hoppers
Breeching
Unfired Pressure Vessels
Low-fired Boilers
Tanks

Stainless Steel
(Sheets, Strip, Bars, Wire and Plates)

Oil Burner Nozzles
Worm Gears for Stokers
Combustion Chambers
Heat Flues and Tubes
Humidifier Pans
Pre-heaters
Furnace Parts and Supports
Fan and Blower Blades
Spring Wire
Welded Wire Fabric

Special grades have excellent resistance to destructive heat-scaling up to 2000°F.

ARMCO ALUMINIZED Steel

An aluminum-coated sheet steel with exceptional resistance to heat and corrosion. Resists heat discoloration up to approximately 900° F, and will withstand heat scaling at even higher temperatures. Also offers exceptional heat reflectivity where this is desirable.

United States Steel Corporation Subsidiaries

Carnegie-Illinois Steel Corporation, Pittsburgh and Chicago
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U·S·S COPPER STEEL

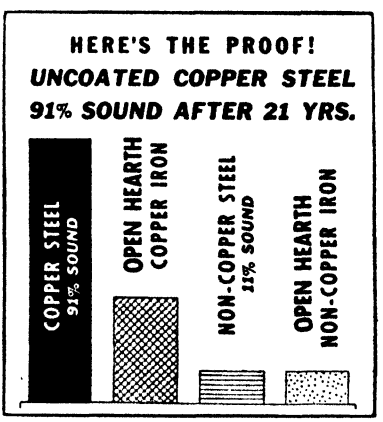
For Superior Rust Resistance at Low Cost

Corrosion resistance and cost are two determining factors of the type of metal to be used for various air-conditioning jobs.

Copper Steel has 2 to 3 times the atmospheric corrosion resistance of plain steel or pure iron as shown in the results of unbiased tests made at Pittsburgh, Ft. Sheridan and Annapolis by the American Society for Testing Materials.

The cost of U·S·S Copper Steel is less than that of pure iron or copper-bearing pure iron and only slightly more than plain steel. Thus there often is a dividend of 200 per cent to 300 per cent longer life and a saving in the first cost as well.

When galvanized, U·S·S Copper Steel produces a sheet that is rust resistant all the way through—not just on the surface. It should be used for all ducts carrying humidified air or placed in damp locations such as basements, shower rooms, etc.



Corrosion test of A.S.T.M. on 28 gage black sheets exposed at Annapolis, Md., October, 1916. The copper steel sheets outlasted all others in the test.

U·S·S PAINTBOND

U·S·S PaintBond should be used whenever galvanized steel is to be painted. This special Bonderized sheet can be painted immediately, offers a much better surface for painting, lessens danger of the paint flaking and retards corrosion. It is used for ductwork, furnace housings and outdoor metal work.

Send for our PaintBond booklet.

U·S·S GALVANNEALED

U·S·S Galvannealed has a tight, matte-surface zinc coating that withstands severe forming operations without peeling or cracking. Suitable for immediate painting without aging or other surface preparation.

U·S·S DUL-KOTE

U·S·S Dul-Kote is a specially treated non-spangled galvanized sheet which also can be painted immediately without aging or otherwise preparing the surface. It is available in the South and in the West.

Send for our Dul-Kote booklet.

OTHER U·S·S PRODUCTS INCLUDE:

Black Sheets—All grades, hot rolled, cold rolled in a number of different finishes.

Stainless—Heat resisting steel for various uses where temperatures are high and corrosion severe.

Cor-Ten—High strength steel—greater strength, greater atmospheric corrosion resistance for smokestacks, hoods, etc.

E. B. Badger & Sons Co.

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NEW YORK 18, N. Y.
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PRODUCTS AND SERVICES

BADGER "PACKLESS" CORRUGATED EXPANSION JOINTS

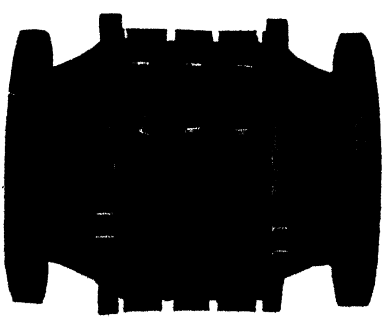
Engineers and Manufacturers of Chemical, Petro-Chemical and Petroleum Refining Equipment; Process Engineers, Designers and Constructors of Complete Plants.

BADGER "PACKLESS" CORRUGATED EXPANSION JOINTS

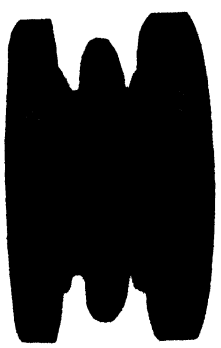
Protect equipment; eliminate costly shut-downs; prevent loss of materials flowing through pipe lines. The Badger "Packless" Corrugated type of expansion joint has been used for many years to relieve stresses, absorb vibrations between connected equipment, and compensate for changes in pipe lines due to temperature differentials.

BACKED BY FIFTY YEARS OF EXPERIENCE

Badger engineers pioneered the corrugated "packless" joint and brought it to its present high state of dependability and usefulness. To meet the increasingly severe conditions in industry, the more recent developments are included in the following brief descriptions.



Standard Flanged-End Badger Directed Flexing, Self-Equalizing "Packless" Corrugated Expansion Joint. ***Also made with standard welding end. (Double units available.) Bulletin No. 100.***



Badger Non-Equalizing "Packless" Corrugated Expansion Joint, Single Corrugation. ***Also made in multiple corrugation and special shapes. Bulletin No. 200.***

FLANGED AND WELDING ENDS. Badger "Packless" Corrugated Expansion Joints can be furnished with either flanged or welding ends.

TELESCOPING SLEEVES. Badger "Packless" Corrugated Expansion Joints can be furnished with telescoping sleeves if required.

INSTALLATION, OPERATING, MAINTENANCE ECONOMIES

• ***"Packless"***—Since this type of expansion joint is made from a *single tube*, no packing is required—hence no servicing. This is particularly advantageous in underground installations, because the expense of manholes and tunnels can be eliminated.

• ***Flexible***—This type of joint is readily flexed, thus reducing to a minimum the thrust on adjacent equipment or fittings.

• ***Wide Range of Traverses***—By varying the number of corrugations, the Badger "Packless" Corrugated Expansion Joint can be made to take care of traverses ranging from small fractions of an inch up to any practical limit.

• ***Wide Range of Pressures***—Standard joints are constructed for normal operating pressures; special joints for higher pressures.

• ***Compactness***—Outside diameter of Badger "Packless" Corrugated Expansion Joint is about that of a flanged fitting.

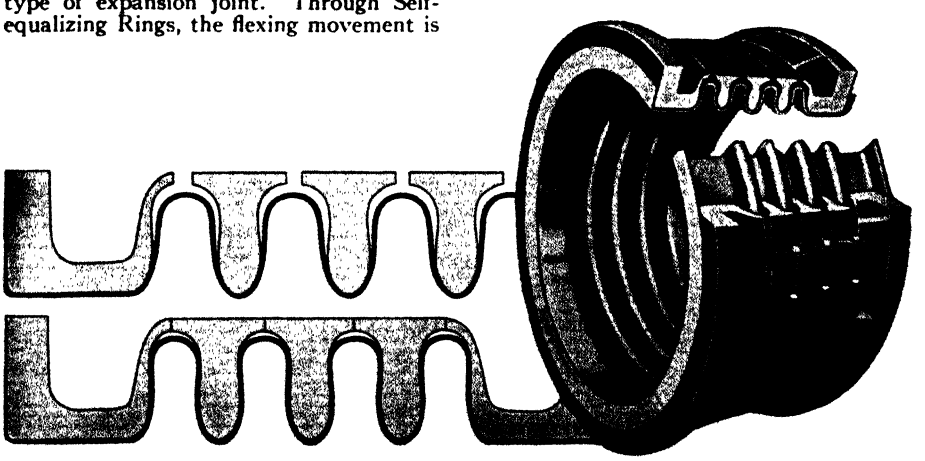
• ***Ease of Installation***—The Badger "Packless" Corrugated Expansion Joint is as easily installed as any fitting.

COPPER AND STAINLESS STEEL. Badger "Packless" Corrugated Expansion Joints are made in self-equalizing or non-equalizing types; and are made of copper, stainless steel, or other metals to meet varying conditions with respect to temperature, pressure and corrosion.

HEAT TREATMENT. Every Badger "Packless" Corrugated Expansion Joint is scientifically heat-treated during the process of manufacture to remove forming stresses. This Badger process increases resistance to flexing stresses, lengthening the life of joint.

DIRECTED FLEXING—SELF-EQUALIZING

This feature, *exclusive* with Badger "Packless" Corrugated Expansion Joints, greatly lengthens the life of the corrugated type of expansion joint. Through Self-equalizing Rings, the flexing movement is not only limited but is progressively controlled throughout the movement. Flexing stresses are kept distributed.



GRINNELL COMPANY INC.

Heating, Industrial and Power Plant Piping, Fittings, Hangers, Valves, Pipe Bending, Welding, Piping Supplies, Etc.

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PRODUCTS AND SERVICES—

Complete Service on materials to Specification on Power Plant Piping, Industrial Piping, and Industrial Heating Systems; Prefabricated Piping including Pipe Cutting and Threading, Pipe Bends, Welded Headers, Welded and Welding Fittings, Lap Joints and the Grinnell line of products for Super Power.

Grinnell Equiflo Valves for forced hot water heating systems; Grinnell Adjustable Pipe Hangers and Supports; Grinnell Cast Iron and Malleable Iron Pipe Fittings; Grinnell Flared Tube Fittings; Grinnell Malleable Iron Unions; Grinnell Welding Fittings; Grinnell Thermoliers (Unit Heaters); Thermoflex Traps and Heating Specialties.

Also Humidifying Systems; Piping for acids and other special materials.

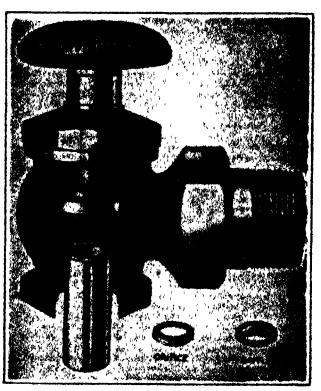
Malleable Iron, Brass, Bronze and other Castings; Brass, Cast Iron, Wrought Iron and Steel Pipe; Seamless Steel Tubing in Iron Pipe Sizes.

Valves: Check, Diaphragm, Globe, Pressure Reducing and Regulating, Quick Opening, Safety and Y.

Automatic Sprinkler Systems; Stand Pipes; Underground Supply Mains; Hydrants; Fire Pumps; Pressure and Gravity Tanks.

Grinnell Equiflo Valves

For Forced Hot Water Heating



Equiflo Valve

The designing of forced circulation hot water heating systems is so simplified by the Grinnell Equiflo Valve that they can be laid out and installed as easily as vapor or steam systems. This valve consists of a regular type packless radiator valve with a cartridge or tube made up of a series of orifices and baffles capable of setting up any required frictional resistance. This method of establishing any desired resistance does away with elaborate calculation of pipe sizes. Grinnell guarantees perfectly balanced circulation to each and every radiator where these valves are installed throughout the system.

Equiflo Data Book sent to interested parties.

GRINNELL ADJUSTABLE PIPE HANGERS AND SUPPORTS

One of the chief advantages of Grinnell Adjustable Hangers is that they permit adjustment of pipe lines after installation, thus obviating the necessity of turnbuckles or the removal of hangers. Their time and trouble-saving qualities during installation are equally exceptional. Below are shown a few Grinnell Hangers and Supports of particular interest to heating engineers. Send for Hanger Catalogue showing complete line.

Adjustable Swivel Rings (Patented)

Fig. No. 101
Solid Ring

These Malleable Iron Adjustable Swivel Rings can be used with Coach Screw Rod or Machine Threaded Rod in connection with practically any type of Ceiling Flange, Expansion Case, Insert, etc.

Adjustment of at least 1½ in. is secured by turning Swivel Shank. Swivel Shank automatically locks, preventing loosening due to vibration in the pipe line.

The Split Ring permits adjustment either before or after Ring is closed. A wedge type pin is loosely but inseparably cast into the hinged section for fastening this section after pipe is in place.

Fig. No. 104
Split Ring

Adjustable Swivel Pipe Rolls (Patented)

An adjustable type of pipe roll using a single hanger rod. Swivel Shank allows vertical adjustment and automatically locks, preventing loosening from vibration.

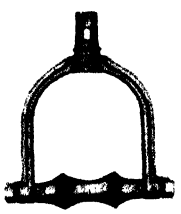


Fig. No. 174
Swivel Pipe Roll

CB-Universal Concrete Inserts (Patented)

Made of malleable iron, in one body size, to take a special removable nut, tapped for ⅜ in., ½ in., ⅝ in., ¾ in. or ⅞ in. rod as required. Nuts automatically lock by means of V-type teeth on both insert and nuts.

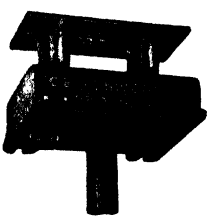


Fig. No. 282
CB-Universal Insert

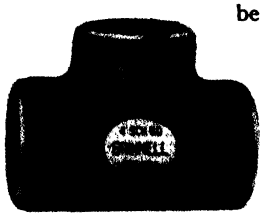
GRINNELL WELDING FITTINGS

Grinnell Welding Fittings are made from Seamless Steel Pipe or tubing and possess the same physical characteristics as standard, extra strong and o.d. steel pipe or seamless steel pipe of comparable size. They can be used under the same conditions, pressures and temperatures as the pipe itself.

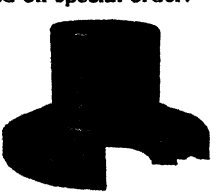
All Grinnell Welding Fittings have welding faces for all plain circumferential butt welds scarfed or beveled as follows: For wall thicknesses 3/16 to ¾ inch inclusive, 37½ deg. ± 2½ deg., straight bevel. Angles of bevel other than 37½ deg. can be furnished on special order.

90° Elbow, Long Radius

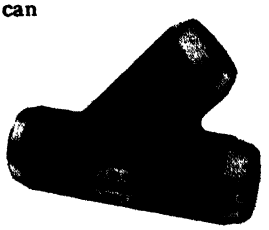
45° Elbow, Long Radius



Welding Tee



Lap-Joint Stub End with Lap Flange attached



Welding Lateral

Arthur Harris & Co.

210-218 N. Aberdeen Street **Chicago 7, Ill.**

ENGINEERS AND BRONZE FOUNDERS—FABRICATORS
OF NON-FERROUS METALS AND STAINLESS STEEL

Metals Fabricated—Aluminum, Block Tin, Brass, Bronze, Copper, Everdur, Monel, Nickel, Inconel, Stainless Steel and KA2 SMO. Bulletin on request.

Bends

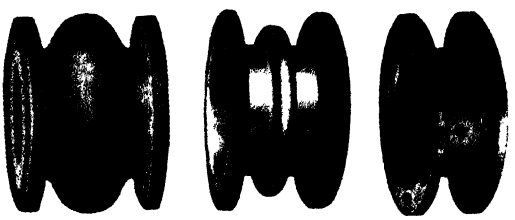
We make bends in every shape from all sizes of copper water tube, pipe and tubing in copper, brass, aluminum, stainless steel, monel, tin and nickel. Standard or special connections. U-bends for storage water heaters.

Also special pipe work for industrial installations, plumbing, heating and brewing.

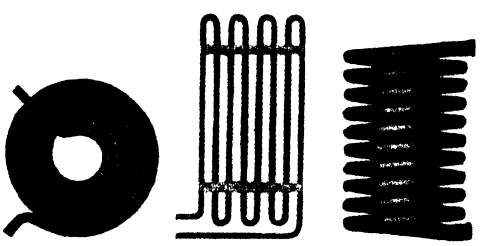
Non-Ferrous Castings—"Dairywhite" nickel silver for Process Industries Equipment. Suitable for milk and food products machinery. Castings also of 88-10-2, 80-10-10, 85-5-5-5, silicon bronze and manganese bronze, and special mixtures.

Copper Expansion Joints

For low pressure and vacuum. Made in two styles—convex and concave. Sizes 4 in. to 60 in. diameter. Cast iron or steel flanges. Flanges drilled to American standard unless otherwise ordered: B-290 available only in sizes 4 in. to 15 in. inclusive.



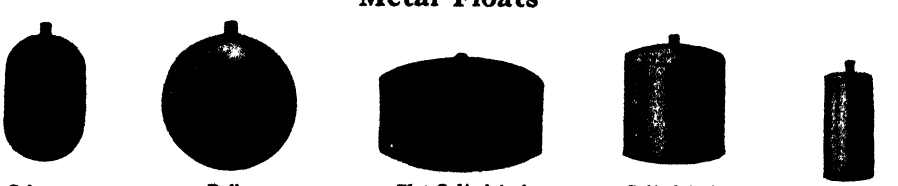
B-280 Convex *B-290 Convex* *B-281 Concave*



Coils

For heating, cooling and condensing. All shapes made from any size pipe or tube—standard or special connections, of copper, brass, aluminum, stainless steel, KA2 SMO, monel, inconel, nickel, block tin, and Everdur.

Metal Floats



Column *Ball* *Flat Cylindrical* *Cylindrical* *Cylindrical*

Made of copper, plain steel, stainless steel, KA2 SMO, aluminum, brass, Monel, pure nickel, Admiralty and Everdur, for open tank and all pressures.

Seamless copper ball floats carried in stock in diameters of 3 in., 4 in., 5 in., 6 in., 7 in., 8 in., 10 in., 12 in. for open tank and pressures of 25, 50, 100 and 150 lb. Floats in special sizes and pressures—made to order. Stainless steel ball floats 2½ in. to 12 in. for high pressure and corrosion carried in stock—special stainless steel floats made to order—stainless steel ball floats larger than 12 in. diameter can be made up specially. Float catalog sent on request.

Tube Turns

INCORPORATED

General Offices and Factory: **Louisville 1, Ky.**

TRADE MARK | TRADE MARK

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NEW YORK, 150 Broadway..........Rector 2-7844
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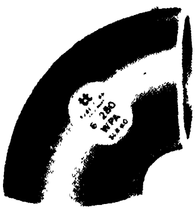
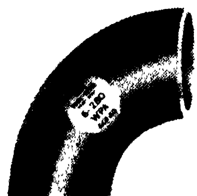


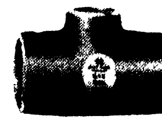
90° Short Radius Elbow



90° Long Radius Elbow

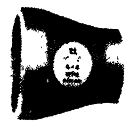
45° Long Radius Elbow

Straight Tee



Reducing Outlet Tee

In addition to carbon steel welding fittings listed here, the complete **Tube-Turn** line embraces many alloys—types 304, 347 and 316 stainless, carbon moly and chrome moly steels, copper, aluminum, brass, Monel, Inconel, nickel and wrought iron. Dimensions and engineering data are included in the **Tube-Turn** *Stainless Steel Catalog* and *Catalog No. 111*, sent on request.



Concentric Reducer

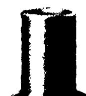
Eccentric Reducer

TUBE-TURN WELDING FITTINGS—RANGE OF SIZES

Type of Fitting	Description	Standard Weight	Extra Strong	Schedule 160	Double Extra Strong	Light Gauge: Nominal Pipe Size	Light Gauge: Iron Pipe Size
Elbows	90° Long Radius	½"-24"	½"-24"	1"-12"	¾"-8"	4"-24"	3"-12"
Elbows	90° Short Radius	1"-30"	1½"-30"				
Elbows	45° Long Radius	½"-30"*	½"-30"*	1"-12"	¾"-8"	4"-24"	3"-12"
Returns	180° Long Radius	½"-24"	½"-24"	1"-12"	3"-8"	4"-24"	3"-12"
Returns	180° Short Radius	1"-30"	1½"-30"				
Returns	180° Extra Long Radius	1"-2½"	1"-2½"				
Tees	Straight	½"-24"	½"-24"	½"-12"	½"-8"		
Tees	Reducing Outlet	½"-24"	½"-24"	½"-12"	½"-8"		
Reducers	Concentric & Eccentric	1x¾-24x20	1x¾-24x20	1x¾-12x10	1x¾-8x6		
Caps		1"-24"	1"-24"	1"-12"	1"-8"		
Stub Ends	Lap Joint	1"-24"	1"-24"				
Nipples	Shaped, 90° to Header	1¼"-12"	1¼"-12"				
Nipples	Shaped, 45° to Header	1¼"-12"	1¼"-12"				
Saddles		2"-24"**					
Laterals	Straight	1¼"-24"	1¼"-24"				
Laterals	Reducing-on-Run	1¼"-24"	1¼"-24"				
Crosses	Straight	¾"-24"	¾"-24"				
Rings	Welding	¾"-24"	¾"-24"				
Sleeves	Welding	2"-24"**					

SUPER Tube-Turn 45° long radius elbows, 90° long radius elbows, and 180° long radius returns available in both Standard weight and Extra Strong in sizes from 3" to 12". Tube-Turn welding fittings and flanges conform to applicable ASA and ASTM Standards. For further details please refer to Tube Turns catalog and data book No. 111.

*30 in. size short radius. **Do not conform to iron pipe thicknesses.



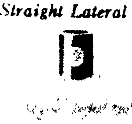
Lap Joint Stub End

180° Long Radius Return

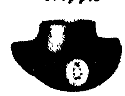
Cap

Straight Lateral

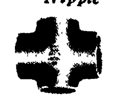
45° Shaped Nipple



90° Shaped Nipple



Saddle



Straight Cross

TUBE-TURN FORGED STEEL FLANGES—RANGE OF SIZES

	150 Lb.	300 Lb.	400 Lb.	600 Lb.	900 Lb.	1500 Lb.	2500 Lb.
Welding Neck	½"-24"	½"-24"	½"-24"†	½"-24"	½"-24"*	½"-24"	½"-24"
Slip-On	½"-24"	½"-24"	½"-24"†	½"-24"	½"-24"*	½"-24"	½"-24"
Lap Joint	½"-24"	½"-24"	½"-24"†	½"-24"	½"-24"*	½"-24"	½"-24"
Threaded	½"-24"	½"-24"	½"-24"†	½"-24"	½"-24"*	½"-12"	½"-12"
Blind	½"-24"	½"-24"	½"-24"†	½"-24"	½"-24"*	½"-24"	½"-24"
Socket Type	½"-24"	½"-4"		½"-3½"			
Reducing-threaded or slip-on	½"-24"	½"-24"	½"-24"†	½"-24"	½"-24"*	½"-24"	½"-12"

†Dimensions on sizes thru 3½ in. same as for 600 lb. flanges.
*Dimensions on sizes thru 2½ in. same as for 1500 lb. flanges.

Blind Flange

Welding Neck Flange

Welding Ring

Socket Flange

Lapped Flange

Threaded Flange

Alco Valve Company

ENGINEERED REFRIGERANT CONTROLS

851 Kingsland Avenue, **St. Louis 5, Mo.**

NEW YORK OFFICE: 122 EAST 42nd STREET

THE COMPLETE LINE OF REFRIGERANT CONTROLS

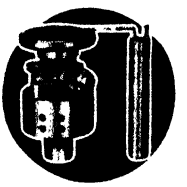
ALCO THERMO EXPANSION VALVES

THERMO EXPANSION VALVES: for automatic control of liquid refrigerant on all types of refrigeration and air conditioning systems. *Capacities*—from fractional tonnage to 100 tons Methyl Chloride, 50 tons "Freon-12."

Thermo-Limit—with pressure limiting feature and capacity change

Type TK—"3 valves in 1"

Type TCL

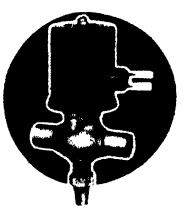


Type TR—Multi-Outlet

ALCO SOLENOID VALVES

SOLENOID VALVES: for all types of service. *For Liquid:* "Freon"—up to 75 tons. Methyl Chloride—up to 150 tons. *For Suction:* "Freon"—up to 8.8 tons. Methyl Chloride—up to 17 tons.

Type S1

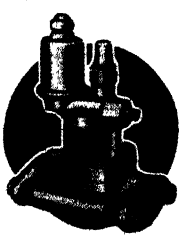


Type M3

Type R2

ALCO AMMONIA CONTROLS

AMMONIA CONTROLS: *Solenoid Liquid Valves*—up to 172 tons. *Solenoid Suction Valves*—up to 28 tons. *Thermo Expansion Valves*—from fractional tonnage to 60 tons.



Type EPR1S

Type M9F

Type TG

ALCO ALSO MAKES: ***Evaporator Pressure Regulators* for "Freon", Methyl Chloride and Ammonia with connection sizes up to 6 in.—*Solenoid Valves* for brine, water, gas, air and steam—*Float Switches*—*High Pressure Float Valves*—*Constant Pressure Expansion Valves*—*Liquid and Suction Line Strainers.***

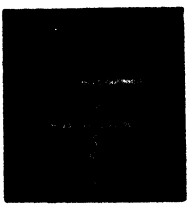
AUTOMATIC PRODUCTS COMPANY

2450 NORTH THIRTY — SECOND STREET

MILWAUKEE WISCONSIN

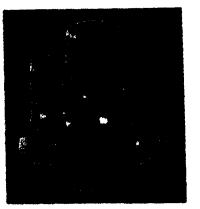
A-P DEPENDABLE CONTROLS

For Heating, Refrigeration and Air Conditioning



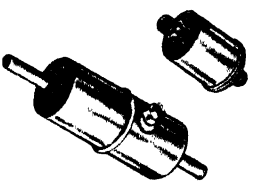
• **A-P Thermostatic Expansion Valves.** Several models and sizes, for capacities up to 16 tons Freon or 32 tons Methyl Chloride. Also available with pressure limiting feature in capacities to 1 ton.

• **A-P Solenoid Operated Water Valve.** Made especially for Deep Well Cooling.



• **A-P Thermostats**
For Cooling or Heating

• **A-PSolenoid Refrigerant Valves.** Capacities up to 50 tons Freon.

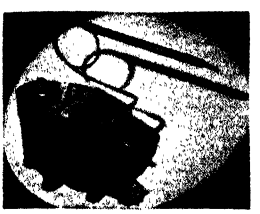


• **A-P Water Regulating Valves.** Capacities up to 1200 Gallons per hour.

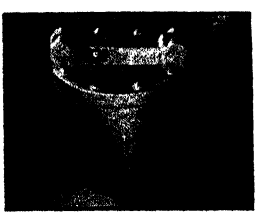
• **A-P "Trap-Dri"**
Combined Filter-Strainer-Drier
Traps dirt, scale, moisture in refrigeration systems.

A-P Controls for Oil Burning Gravity-Feed Heating Plants.

A-P Constant Level Oil Control Valve—With Fuel Compensator. Used on Gravity Oil Burning Appliances.



A-P Complete Furnace Control Set—Made in variety of types for Gravity-Feed Oil Burning Furnaces.



A-P Fuel Oil "Trap-It"—Traps dirt and water in fuel systems. Improves operation of all oil burning devices.

A-P Valve DEPENDABILITY
is widely recognized in Refrigeration, Air Conditioning and Heating. This reputation is born of close adherence to a rigid standard of perfection—in materials used, careful testing, inspection and simplicity of construction.

Detroit Lubricator Company

Division of American Radiator & Standard Sanitary corporation

General Offices 5900 Trumbull Ave., **Detroit 8, Michigan, U. S. A.**

New York 18, N. Y., 40 West 40th Street — Chicago 5, Ill., 816 S. Michigan Avenue

Export Department—Box 218, Ridgefield, N. J.

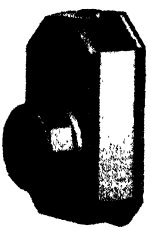
Canadian Representative:

Railway and Engineering Specialties Limited, Montreal, Toronto, Winnipeg

Automatic Controls

Detroit Lubricator Company manufactures a very complete line of electrical controls, designed to open or close an electrical circuit with changes of temperature or pressure. The No. 411 Thermostat (illustrated) is a low voltage model and is made in plain and Day and Night types. All No. 411 Thermostats are available with heat compensation to provide smooth, accurate temperature control. The No. 855 Mercoid Room Thermostat (illustrated) is a line voltage type—available in heating, air conditioning and refrigeration ranges.

No. 411



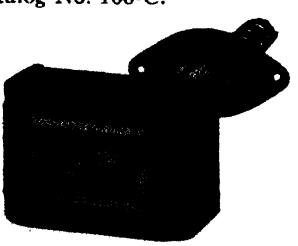
No. 855

For industrial use the No. 250 and No. 450 line of pressure and temperature controls is available, in pressure ranges from 20 in. vac. to 350 lbs. and in temperature ranges from −30° F to 495° F. Write for Catalog No. 100-C.

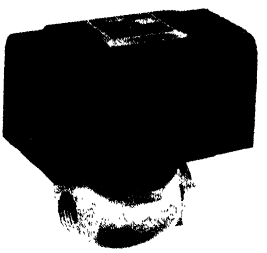
Furnace Controls

Also available is a full line of blower controls, combination blower and limit controls, such as the CA-815 illustrated.

There is a "Detroit" control available for practically every application where a dependable device is required to open or close an electrical circuit with changes of pressure or temperature. Write for complete information. Our Engineering Department is always ready to make recommendations on any specific problem. Write for Catalog No. 100-C.



No. CA815

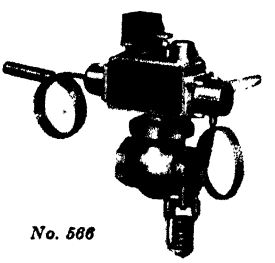


No. V-570

Gas Valves

The No. V-570 Electric Gas Valve is an electrically operated valve for control of gas lines from ½ to 1¼ in. It provides partial opening upon initial operation, permitting quiet ignition of gas. Inexpensive, compact, and attractive in appearance, it employs an easily serviceable bimetal strip motor for actuating force. Write for Bulletin 201.

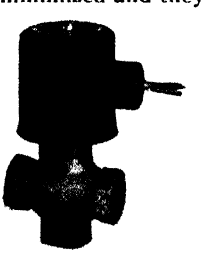
The No. 566 Valve combines in one compact unit all of the functions of a control system for gas heating. All safety functions are mechanical and operate independent of electric current. Adjustable for full snap or any degree of throttling action. Limit control closes valve with a snap action. Valve may be manually operated in case of current failure. Applicable to all gases, natural, manufactured, or mixed. Write for Bulletin No. 80.



No. 566

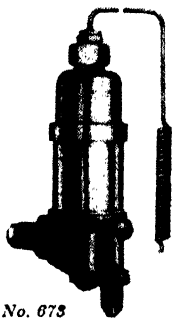
Solenoid Valves

"Detroit" Solenoid Valves for control of water, air, oil, gas, or refrigerant, embody many desirable features. A.C. hum is minimized and they will open against high pressures. Available in all standard voltages and cycles A.C. or D.C. No. 683-3 (illustrated) is a small size valve with ⅜ in. connections. No. 681 is a pilot operated, intermediate size valve, and the No. 686 is a large pilot operated valve with

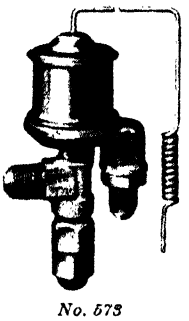


No. 683-3

capacity up to 17 tons Freon-12. No. 686 valve available with flanged connections. No. 681 and 686 are furnished with manual opening feature to permit opening in case of current failure. All models may be taken apart and cleaned in the field without removing from pipe lines. Write for Bulletin No. 199.



No. 673

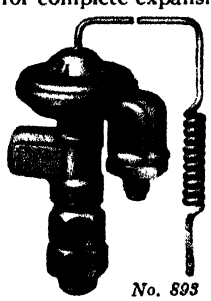


No. 573

"Detroit" Thermostatic Expansion Valves

"Detroit" Thermostatic Expansion Valves are designed to keep the evaporator in a refrigerating system completely refrigerated. Power elements are "gas charged" to a definite pressure, for motor overload protection; providing quicker response and more sensitive control. Capacities from ½ to 20 tons Freon-12. All needles and seats are made of Delubaloy, a very hard, corrosion resistant alloy to insure long, trouble-free service.

No. 673, the "standard of the industry," has a long record of dependability. It is sensitive and accurate in operation. No. 573 has the quality and operating characteristics of the 673 for smaller installations. It has a *single* power element with double diaphragm. Write for catalog No. 200B for complete expansion valves listings.

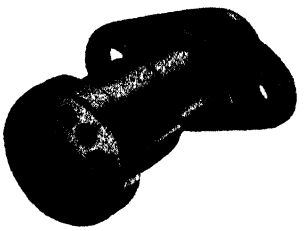


No. 893

"Detroit" Expansion Valves

These valves are of single diaphragm construction. The diaphragm is made of special alloy, carefully tested for flexibility to assure uniform capacities and smooth operation. Power elements are gas charged for protection against motor overload and for maximum sensitivity. Needles and seats are hard, corrosion resistant Delubaloy.

Automatic and thermostatic types in capacities from ½ to 20 tons Freon-12 and .9 to 36 tons methyl chloride. Write for Catalog No. 200-B.



Refrigerant Distributors

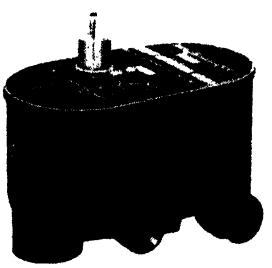
"Detroit" No. 790 Refrigerant Distributors insure a uniform supply of refrigerant to all sections of multiple circuit evaporators and are attached directly to the expansion valve by means of a flanged connection. These corrosion-resistant distributors are available for "Detroit" Thermostatic Expansion Valves No. 786, No. 787, No. 788 and No. 899.

They are made in five types of 2 to 18 passes for the above valves.

All distributors are designed for use with ¼ in. O.D. copper outlet tubes.

For complete capacity tables write for Bulletin No. 207.

"Detroit" Float Valves for Vaporizing Oil Burners



CRC-246 Single Metering Float Valve. The Greatest Improvement in Float Valve Design in Many Years.

For space heaters, furnaces, floor furnaces, water heaters, ranges, etc., the CRC 246 mounts directly on the burner nipple, eliminating tee, fittings and tubing. Low flows are extremely accurate, assuring exact control of fuel delivery for low pilot burners. Rate of flow constant for inlet heads from 2 inches to 84 inches—eliminates dying fire when fuel is low. Automatic temperature compensation assures even fuel flow regardless of fuel temperature—an important "Detroit" feature. Magnetic trip mechanism is positive—will not trip from vibration. Valve may be tilted a reasonable amount without affecting flow. Leveling by eye is satisfactory. So simple to clean that servicing is no problem. Write for Bulletin No. 217.

Fulton Sylphon Div.

ROBERTSHAW-FULTON CONTROLS CO.

Knoxville, Tenn.

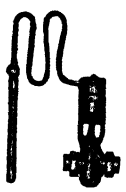
Sales Representatives in Principal Cities

Manufacturers of

Sylphon Automatic Temperature Controlling Instruments and Packless Expansion Joints

HOT WATER SUPPLY

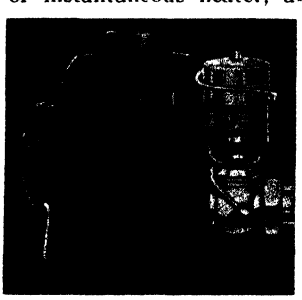
No. 923 Temperature Regulator—For controlling water temperature in heaters, open or closed tanks and other equipment. Operation unaffected by temperature fluctuations at the valve, either above or below bulb temperature. All parts, except steel adjustment spring, made of non-ferrous metals. May be installed in any position. Ranges from 40° —80° F to 290° —330° F. Bul'n HVG-20.



No. 923 Temperature Regulator

Sylphon Thermostatic Water Mixers

Utilize hot water from any storage tank or instantaneous heater, and effectively regulate the amount of cold water required to temper it to the desired degree, actually mixing the hot and cold water together before delivery. Temperature remains constant in spite of fluctuations in supply water temperatures or pressures. Four sizes with capacities ranging from 5 to 131 gpm. Bulletin HVG-20.



No. 902 Sylphon Thermostatic Water Mixer—1¼ to 131 gpm depending on water pressure

REFRIGERATION CONTROLS

Adapatable wherever brine is used as the refrigerant. Latest development is a "freeze-proof" valve (illustrated at left on the popular Sylphon No. 945-Z Regulator). Bulletin HVG-20.

No. 945-Z Regulator

PACKLESS EXPANSION JOINTS

The Sylphon Packless Expansion Joint eliminates useless building height, expensive construction, non-revenue producing space. No leaks or repairs, no repacking, always tight; heating system operates at full efficiency. Bulletin HVG-140.

No. 110 Sylphon Expansion Joint

SPACE HEATING CONTROL

No. 885 Automatic Radiator Valve—For exposed radiation. Small, neat, attractively finished, adjustable to room temperature desired. Simply replace ordinary radiator valves with these Sylphon Automatic Valves—no wiring, piping or auxiliary equipment is required. These valves answer the demand for an inexpensive means of providing accurate, dependable space temperature control in rooms, sections or throughout large buildings, new or old. Similar type valves for concealed radiation—get Bulletin HVG-80.

Sylphon No. 885 Automatic Radiator Valve

No. 890 Radiator Control Valve—For either exposed or concealed radiation. Similar in appearance and action to other Sylphon Automatic Valves, but operated by an electric wall thermostat. The closing of the thermostat circuit energizes a low voltage electric heater coil surrounding a bulb containing a volatile liquid. This liquid expansion causes pressure on a bellows in the valve head operating the valve. This provides radiator valve control from a remote location, permits regulation of several radiators from a single thermostat, enables a time switch to be installed, if desired, offers effective zone control of large areas at a fraction of the cost of conventional motor-operated valve systems. Bulletin HVG-70.

Sylphon No. 890 Electric Control Valve

No. 7 Temperature Control—A self-contained, self-powered regulator for controlling unit heaters, wall or ceiling type radiators, heating coils in duct-type heating systems, etc. Quickly installed, holds temperatures within close limits. Valve placed in steam line to one or a battery of heaters, thermostat mounted on wall or column. For use on regular heating pressures up to 15 lb. Similar regulators, Nos. 7-2 and 7-3 for 50 and 75 lb. Pressure and temperatures up to 170°F. Bulletin HVG-220.

Sylphon No. 7 Temperature Control (Self-operating)

HEATING AND AIR CONDITIONING CONTROL

Almost any type of heating, ventilating or air conditioning system can be advantageously controlled wholly or in part by Sylphon Regulators. Basic advantages of Sylphon Controls are:

Modulating—Maintains ideal conditions —not continually correcting too hot, too cold, too humid or too dry conditions.

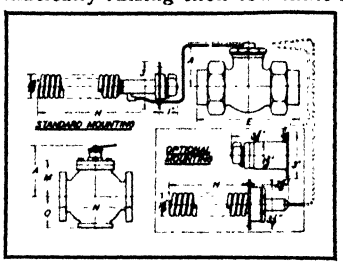
Compensating—Many Sylphon Regulators offer compensating control, automatically raising their low limit setting at a predetermined rate as outside temperatures fall.

Sensitive—Close operating temperature differentials. Quick response.

Simple—in design.

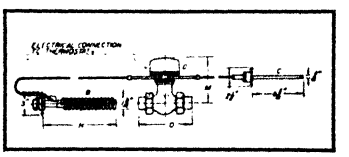
Rugged Construction—To give years of satisfactory service.

Adapatable—Any one of many combinations of Sylphon Instruments can be arranged to control any air conditioning system and to provide exactly the conditions desired. *Write for Bulletin SA C—220.*



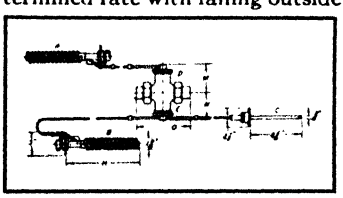
Regulator 928-C

The No. 928-C Regulator—Simple, compact yet highly sensitive. Suitable for modulating control of air temperatures in ducts. Bulb is constructed of numerous coils of copper tubing giving sensitivity to the slighest temperature variation. Packless valve eliminates service problem and makes this regulator ideal for installation in inaccessible locations. Suitable for steam pressures up to 15 lb; other types available for pressures up to 75 lb.



Regulator 928-ECC

The No. 928-ECC Sylphon Regulator—Room control and low-limit control in a single valve regulator for modulating control of ventilating systems. Main control from an electric room thermostat operating through the electric head "D" on the valve. Low-limit control by Bulb "B" located in discharge duct from the heater. Bulb "C", located in inlet side of the duct to the heater, compensates Bulb "B". Compensating thermostat can be furnished to raise low-limit setting at predetermined rate with falling outside temperature. Suitable for steam pressures up to 15 lb.

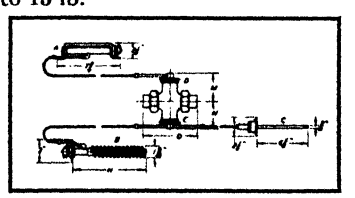


Regulator 829-C

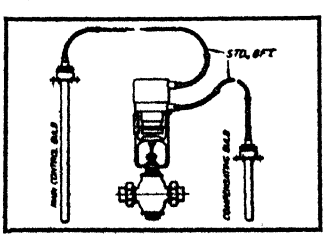
The Sylphon No. 889-C Regulator—A modulating, dual-function regulator for control of duct heating and ventilating systems—two independent valves in a single body.

Adjustable Thermostat "A" governing Valve "D" functions to maintain room temperature from temperature of recirculated air. Adjustable Thermostat "B" acts as a low-limit ductstat controlling Valve "E" to maintain minimum discharge air temperature. Bulb "C" compensates Bulb "B" to maintain even discharge air temperature irrespective of demand. Compensated Thermostat "B" can also be furnished to raise its setting at a predetermined rate with falling fresh air temperatures, if desired. Suitable for steam pressures up to 15 lb.

The Sylphon No. 889-C7 Regulator—The No. 889-C7 regulator has a wall type adjustable thermostat that is placed in the room or space to be controlled. This thermostat "A" operates upper half of the regulating valve. Otherwise, same as No. 889-C regulator described above.



Regulator 889-C7



Regulator 971

Sylphon No. 971 Differential Regulator—For controlling room temperature on the cooling cycle, where chilled water or brine is used as cooling medium and where it is desired to have a gradual increase in room temperature as outside temperature increases. This regulator is modulating in action, thereby affords better control over humidity than is procured when usual on-and-off type control is employed.

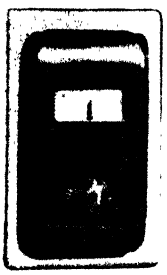
GENERAL CONTROLS

FACTORY BRANCHES: Boston • Chicago • Cleveland • Dallas • Denver • Detroit • Houston • Kansas City • New York • Philadelphia • Pittsburgh • San Francisco • Seattle

DISTRIBUTORS IN PRINCIPAL CITIES

HOME OFFICES AND FACTORY: 801 Allen Ave. Glendale 1, California

AUTOMATIC TEMPERATURE—PRESSURE—FLOW CONTROLS



The Trimtherm

THERMOSTATS

Trimtherm provides accurate, remote control of desired temperature. Streamlined, compact—extends only ⅞ in. from wall, yet sensitive to slightest temperature change (Differential ½ F.) Chrome cover, natural ivory base.

MAGNETIC GAS VALVES

Type K-3B

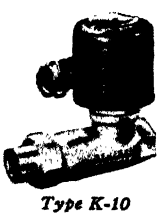
Versatile, two-wire, straight magnetic current-failure valve. Packless. Insures tight shut-off indefinitely. Humless. Size range, ⅛ in. to 6 in. I.P.S Operating pressures up to 5 lb. Voltages and frequencies, A.C. or D.C. Quiet, positive, trouble-free. Available in explosion-proof housing.

SLOW OPENING GAS VALVES

Type B-55

For industrial and commercial burners and furnaces. Adjustable opening time, 5 to 50 secs. Wide pressure range up to 5 lb. Size ¾ in. to 6 in. I.P.S. Ample power for louvre control. Damper arm easily rotated. Packless.

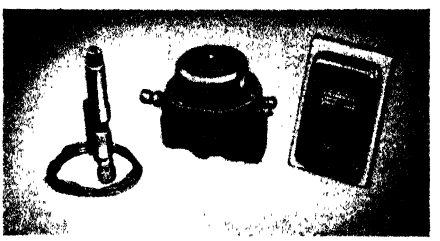
MAGNETIC VALVES



Type K-10

Provides six times more power than ordinary solenoid valves. Controls air, gas, water, light, heavy oils, steam. Positive opening, complete shut-off, packless, hum-free. Available for any voltage, A.C. or D.C., in sizes up to 1¼ in. I.P.S., port sizes up to ⅝ in. K-20 Series is designed for applications where single needle port sizes provide sufficient flow capacity. W-3 Series are magnetic 3-way valves for controlling fluid to piston and diaphragm operators on valves, doors, gates, etc.

B-60 GAS ACTUATED PACKAGE SETS



Everything needed in a convenient package for remote gas control—B-60 Valve, Trimtherm Thermostat, Pilot Burner Generator and 25 ft of wire. No outside current required. Safe, quiet, dependable. Applicable to gas furnaces, floor furnaces boilers, circulators, gas radiators. Operates on all types of gases.

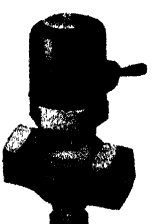
*hi-g MAGNETIC VALVES

Type PV (AV)-3

Designed for positive operation on aircraft, trucks, tractors, tanks, graders, ships, and other moving equipment. Handle all fluids, vapors and gases on anything that rolls, floats or flies at pressures up to 3000 lb or more. Packless, two-wire, current-failure type, available normally open, normally closed for intermittent or continuous duty.

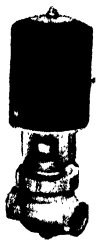
*Trade Mark—"hi-g" indicates positive ability to function in any position, regardless of vibration, change of motion or acceleration.

REFRIGERANT CONTROLS



Type K-18

Magnetic piloted, two-wire, current failure, high pressure, packless. Handle large capacities with minimum pressure drop and loss. Tight shut-off. Operates on wide variety of fluids and gases.

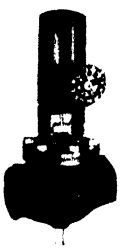


Type G-1-7

HYDRAMOTOR VALVES

Simplify valve control installations. Two-wire, current failure, electric-hydraulic operation. Ample motor-driven power, slow opening and closing movement. Operator drives against a spring in one direction; power failure or opening of circuit causes spring to operate in other direction.

MANUAL RESET VALVES



Type MR-1-2

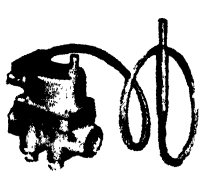
Equipped with manually-reset electromagnetically-held valve operator. Current flowing to operator permits manual opening by turning valve wheel at side. Current failure releases operator allowing valve to close. Trip-free mechanism cannot be opened under unsafe conditions. Once closed, valve is re-opened manually because applying current has no effect.

STRAINERS

Type S-5-1

Actual tests prove importance of strainers in prolonging operating life and reducing leakage of flow controls. S-5 Series STRAINERS come in 8 types; meshes 3/16 in. diam. to 120-per-inch.

THERMOPILOT (Valve Model)



Type MR-2

Manually-reset, electromagnetically-held-open valve with current generated by single couple subject to heat of pilot flame. Available 3/8 in. to 1½ in. I.P.S.

THERMOPILOTS

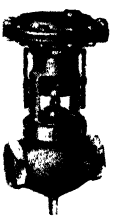
Type A-100

Proven principles of operation insure dependability. Flame applied to thermocouple maintains electrical contact, allowing electrical gas valve to open. When flame fails, Thermopilot opens circuit to main gas valve. Flexible, armored, asbestos-covered cable detachable from relay. 2 or 3-wire control. Electrical rating, 2 amp., 24 volt; 1 amp., 115 volt; 0.5 amp., 230 volt.

THERMAL EXPANSION VALVES

Type V-200 provides unmatched sensitivity and dependability. Handles freon, methyl chloride, sulphur dioxide. Quickly removed orifice cartridges eliminate need for stocking several sizes for low tonnage installation.

GAS FUEL GOVERNORS



Type V-25-1

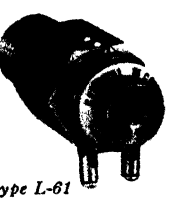
Throttle gas lines according to boiler pressure applied to diaphragm. Ball bearing thrust adjustment, ground and polished non-corrosive stems, low friction packing gland seal, multiple calibrated springs, high lift for maximum capacity. Suitable for butane, natural or manufactured gas. Available 3/8 in. to 3 in., I.P.S.

RELAYS AND TRANSFORMERS

Type RS-100

Type RS-100 handles single phase motor loads up to 1 hp or heating loads up to 1.1 kw. Combines double-break relay and integral transformer. Normally open; large double-break contacts. Two-wire control circuit; maximum holding current 0.4 amps. Furnished with ½ in. conduit connections and low voltage outlet. A.C. only.

TANK THERMOSTATS



Type L-61

Averages 6 to 10 degrees effective differential on water heater. Saves fuel by eliminating overheating due to large differentials. Temperature range, 60 to 170 F. Also to 230 F.

LOW PRESSURE GAS REGULATORS

Type V-300

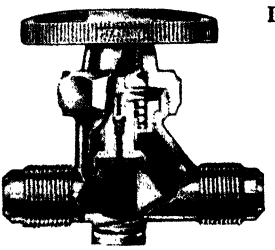
New V-300 Series are reliable, trouble-free valves with high capacity, close regulation, yet small and compact. Regulator sizes range from 3/8 to 2 in. I.P.S. Internal parts, corrosion-resistant. Cast iron regulator bodies, ong life calibrated springs, properly fitted all-metal valves.

GENERAL CONTROLS manufactures a complete line of Automatic Temperature, Flow and Pressure Controls. For complete specifications write for *Catalog 52B*.

Henry Valve Company

3260 W. Grand Avenue., **Chicago 51, Ill.**

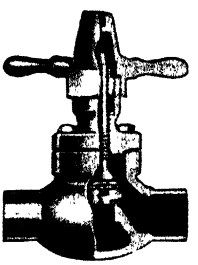
HENRY PRODUCTS FOR REFRIGERATION, AIR CONDITIONING, AND INDUSTRIAL APPLICATIONS: CONTROL DEVICES, VALVES, STRAINERS, DRIERS, FITTINGS, AND ACCESSORIES.



DIAPHRAGM PACKLESS VALVES

Line shut-off, branch shut-off, and angle types; flare, solder, or pipe connections. Hand expansion types also available. Forged brass body and bonnet, ports-in-line, non-directional, stainless steel diaphragm and working parts. Stock sizes ¼" to 1⅛" S.A.E., ¼" to 1½" solder, ¼" to 1" F.P.T.

WING CAP PACKED VALVES



Globe and angle, types, bronze with solder connections, semi-steel with solder and pipe connections. Floating, replaceable stem disc, back-seating to permit repacking under pressure, wrench socket in top of wing cap operates valve. For "Freon" or methyl chloride. Sizes: Bronze globe, ⅞" to 4⅛" solder; bronze angle, ⅞" to 3⅛" solder; flanged semi-steel globe with tailpieces for ⅞" to 5⅛" solder and for ¾" to 5" I.P.S. butt weld.

SOLENOID VALVES

Made in a wide range of sizes for refrigeration and industrial applications. Details furnished on request.

RELIEF VALVES

Diaphragm Type (Illustrated): For low-pressure refrigeration.

Approved under safety codes. Diaphragm actuated. Sizes, ½" F.P.T., ⅝" solder. Solder extensions provided to protect internal parts from heat. Smaller relief valves also available. See Catalog 97.

Ferrous Type: For ammonia, "Freon," or methyl chloride. Approved under safety codes. Sizes ⅜" to 2" F.P.T. See Catalog 65 for illustrations and details.

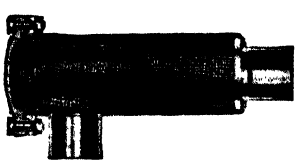
DRIERS

Henry Abso-Dry Driers are charged with dehydrated air. When seal caps are opened at time of installation, hiss of escaping air proves dehydrant is moisture-free. Perforated dispersion tube prevents channelling. Complete line of refillable and non-refillable types for air conditioning and refrigeration. See Catalog 97.

Type 756 (Illustrated): Cartridge-type drier with side outlet, compression spring, dispersion tube, and distortion-proof access flange. Dehydrant volume capacity 12 to 300 cu in. Sizes ⅜" to 1⅝" O.D.S.

STRAINERS

Henry strainers feature large capacity, large screen area, easy cleaning, all-brazed construction. Sizes and designs for all applications. See Catalog 97.



Type 866: Angle strainer with solder connections, reinforced monel metal screen, drawn brass shell, distortion-proof access flange. Screen area 23 to 275 sq in. Sizes ¼" to ⅝" O.D.S.

Type 895: Steel "Y" type strainer. Welded construction, distortion-proof access flange, protective baffle on inlet. Screen area 23 to 175 sq in. Capacity and connections for ⅝ "to 4⅛" O.D.S.; 1" to 3" pipe.

Sold and Recommended by Leading Refrigeration Jobbers in 130 Cities

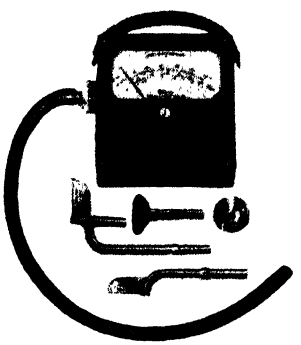
Illinois Testing Laboratories, Inc.

Room 516, 420 N. La Salle St., **Chicago 10, Ill.**

Alnor

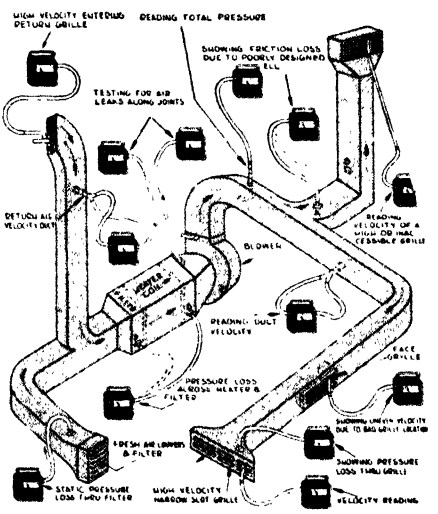
Precision Instruments for *Every* Industry

The direct-reading ALNOR VELOMETER



The Alnor Velometer is an instantaneous, direct-reading air velocity meter designed for convenient, rapid determination of air velocities in air conditioning, heating and ventilating, and exhaust systems. It gives instantaneous direct readings in feet per minute, without timing, calculations, or reference to tables or charts. Accurate information on performance of equipment, duct systems, etc., can be obtained with a few moments' inspection with the VELOMETER. It can be effectively used to locate drafts and leaks around windows and doors, or in duct systems.

The Alnor Velometer is built in several standard ranges from 20 fpm to 6000 fpm, and up to 3 in. static or total pressure. Special ranges available as low as 10 fpm and up to 25,000 fpm velocity and 20 in. pressure.



TYPE 4-F Standard minimum set for heating and air conditioning air velocity measurements.

ALNOR PYROMETERS

Alnor Pyrometers include a wide range of portable and wall mounting types, both single and multi-point instruments, for a variety of industrial temperature measurements. Temperature readings of molten metals, industrial furnaces, and similar equipment, and temperatures of surfaces, either metallic or non-metallic, moving or stationary, are readily obtained with standard ALNOR Pyrometers.

Johnson Service Company

AUTOMATIC TEMPERATURE AND AIR CONDITIONING CONTROL

General Office and Factory

Milwaukee, Wis.

Direct Branch Offices in Principal Cities

JOHNSON TEMPERATURE REGULATING CO. OF CANADA, LTD., 113 SIMCOE ST., TORONTO, ONT.
HALIFAX, N. S. MONTREAL, QUE. WINNIPEG, MAN. CALGARY, ALTA. VANCOUVER, B. C.

PRODUCTS AND SERVICES

Manufacturers, Engineers and Contractors for automatic temperature and humidity control systems applied to all types of heating, cooling, ventilating, air conditioning and industrial processing installations.

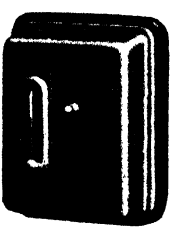
Space Control—Automatic control of room temperatures and humidities, applied to radiators, radiant heating, unit ventilators, unit heaters and heat delivery ducts. Johnson "Duo-Stats" maintain proper relationship between outdoor and heating system temperatures for groups of radiators, or "heating zones." A complete line of controllers for air conditioning systems, heating, cooling, humidifying, dehumidifying.

Process Control—Automatic temperature and humidity control for every range required in manufacturing and industrial processing. Thermostats, valves and dampers applied to tanks, dryers, vats, kettles, curing rooms, coolers, kilns, etc., in textile, rubber, pulp and paper, petroleum refining, meat packing, dairying, baking, sugar refining, brewing and distilling, tanning, candy making and other industries.

Nation-wide Service—Johnson sales engineers, and trained installation men available at all branches listed above. None is an agent, jobber, or part-time representative. All are salaried employees, devoting their efforts to the interests of the Johnson Service Company and its customers.

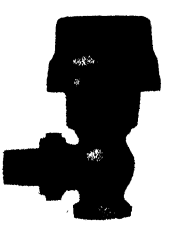
Send for Bulletins describing Johnson controllers.

Single Room Thermostat T-401



"Dual" Room Thermostat T-460

Room Humidostat H-107



"Sylphon" Radiator Valve V-111

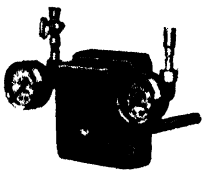
JOHNSON THERMOSTATS

Room Thermostats—Proportional (gradual) or two-position (positive) action, maintaining temperatures within one degree above or below point of setting. Various covers, allowing wide selection of adjusting features, guards and method of mounting. Red-reading thermometers with magnifying tube attached to covers.

Insertion and Immersion Thermostats—Rigid stem or capillary. Liquid or vapor-filled capillary systems for temperatures which are measured at point remote from location of operating mechanism. Various types of bulbs. Standard connecting tubing lengths: 8, 15 or 25 ft. Up to 50 ft on special order.

Thermometers—High grade insertion or immersion thermometers to measure temperatures in ducts, tanks, etc., with red-reading mercury column in heavy lens glass tube and 9-in. scale. Insertion thermometers have patented adjustable tilting feature.

Special Controllers—For applications encountered in industrial processes. "Record-O-Stat," combination capillary temperature controller and recorder. 12-in. chart and liquid or vapor-filled capillary systems. Single or duplex type, the latter controlling and recording wet and dry bulb temperatures . . . **Pressure Regulators**—Pressure ranges 27 in. of vacuum to 150 lb pressure. Bourdon tubes of types and sizes for required pressure range and for medium to be controlled: Air, water, steam or freon. Other regulators for pressures between ¼ lb and 200 lb . . . **Liquid Level Regulators** (Float type)—Control within extremely close limits. Mounted through wall of containing vessel by stem with 1 in. pipe thread. Floats of copper, stainless steel or special alloys . . . **Static Pressure Regulator**—Measures variations in pressure from .009 in. to 3 in. of water. Also used as differential regulator, measuring difference in pressure between two chambers.



Rigid Stem Insertion Thermostat T-860

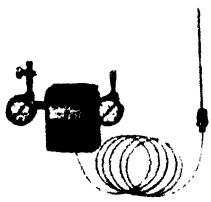
Sub-Master Thermostats—An important development for industrial applications and air conditioning. Applied to various controllers where readjustment must be made from a remote point.

Johnson Sensitivity Adjustment—A distinctive feature affording convenient means of adjusting the sensitivity of thermostats and humidostats, on the job, balancing "time-lag" with respect to capacity of conditioning apparatus. "Hunting" and temperature fluctuations prevented. Available on Johnson proportional action insertion and immersion thermostats, insertion humidostats, and certain room thermostats and humidostats.

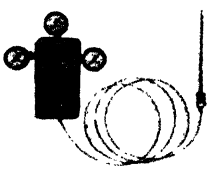
JOHNSON HUMIDITY CONTROL

Johnson Humidostats—Automatically control supply of moisture delivered to air by a humidifier or other means, maintaining constant relative humidity. Available in room and insertion patterns with various elements, the most sensitive controlling within 1 per cent at relative humidities as high as 95 per cent at 100 F. Humidostatic elements are wood cylinder, by-wood strip, bow-wood, horn, hair or animal membrane.

Johnson Humidifiers—"Steam grid" type (perforated pipe supplied with low pressure steam) or pan type with copper evaporating pan, brass heating coils and float control.



Capillary Thermostat T-860

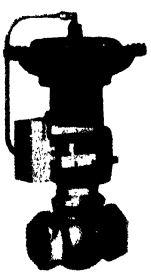


Sub-Master Capillary Thermostat T-901

JOHNSON VALVES

Johnson Diaphragm Valves—Simple and rugged. Diaphragms of special molded rubber, resistant to age and oxidation, operate valve stems against pressure of dependable springs. Available also with Sylphon seamless metal bellows. Made in standard sizes and patterns. Normally open (direct acting) or normally closed (reverse acting). Three-way mixing and by-pass valves, for steam, water, brine and other gases and liquids.

Johnson "Streamline" Diaphragm Valves—With modulating discs and special internal construction. Superior proportional control . . . Where maximum power is required for repositioning at slightest demand of controlling instruments. Johnson molded rubber diaphragm valves are fitted with pilot positioner, independent of friction and pressure variations.



Globe Valve with Pilot Positioner V-103

JOHNSON DAMPERS AND SWITCHES

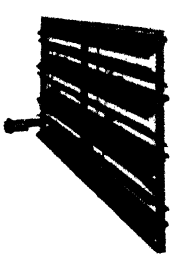
Standard Johnson Dampers—Steel blades in flat steel frames with adequate bracing to form rigid assembly. Black lacquer or special corrosion-resisting finishes. Angle iron frames optional.

Special Dampers—Galvanized iron, monel metal, aluminum, copper, rust-resisting steel, etc. Brass pins in steel bearings or ball bearings.

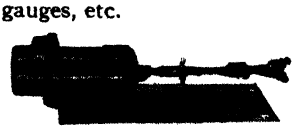
Johnson Damper Operators—Similar in principle to valves. Seamless metal or specially molded rubber diaphragm operates damper through suitable linkage. Johnson "Piston" damper operators afford long travel at full power. With or without pilot mechanism, as described for "Valves."

Johnson Pneumatic Switches—For operation of dampers and to place controllers in and out of service, from remote points. Oiled slate is standard. Ebony asbestos, polished oak, and genuine or imitation marble on order. Various apparatus, at central control points, is mounted on special switchboards, including lever type switches, gradual and multiple-step switches, clocks, air pressure gauges, recording gauges, etc.

3-Way Mixing Valve (Rubber Diaphragm) V-108



Proportioning Louver Damper D-225



Piston Damper Operator D-251

The Mercoid Corporation

Main Office and Factory, 4201 BELMONT AVENUE, **Chicago 41, Illinois**
NEW YORK OFFICE, 205 EAST 42ND ST. PHILADELPHIA OFFICE, 3137 N. BROAD ST.

AUTOMATIC CONTROLS FOR HEATING, AIR CONDITIONING, REFRIGERATION AND VARIOUS INDUSTRIAL APPLICATIONS

FOR PRESSURE & TEMPERATURE

These controls have a wide range of applications. They are noted for their accuracy and dependable performance. The outside double adjustment feature and visible dial eliminate all guesswork when setting the operating range.

VISAFLAME

The Mechanical Eye Actuated by Light. A positive safety control system for domestic and industrial oil burners. Operates direct from the light of the flame instead of from heat in the stack. Tried and proven to be the most practical method for dependable oil burner performance. (See next page.)

OIL BURNER SAFETY CONTROLS

Type JMI provides positive protection against flame or ignition failure on intermittent ignition oil burners. This control insures having ignition circuit closed before every starting operation of burner. Type JM is used for constant ignition burners.

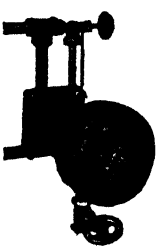
THE ONLY 100% MERCURY SWITCH EQUIPPED CONTROLS

The distinguishing feature of Mercoid Controls is the exclusive use of Mercoid hermetically sealed mercury switches. These switches are not subject to dust, dirt or corrosion, thereby assuring better performance and longer control life. The items shown below are but a few miscellaneous items. See Catalog No. 700 for complete line.

MERCOID THERMOSTATS

Mercoid low voltage room thermostats are known by their trade name SENSATHERM. They operate on a total differential of 1 degree F. Type H is the regular popular room thermostat. Type DNH is a hand wound day and night Sensatherm. Type HBH is the two-stage type for control of high-low oil or gas burners. Recommended also for stokers. Type 855 is designed for direct line voltage applications recommended for unit heaters, air conditioning, etc.

LOW WATER CONTROLS



Available also as a combined low water and pressure control to prevent firing into a dry boiler or building up excess pressure. There are a number of different types for various requirements. The illustration shows type provided with quick-hook-up fittings designed in accordance with the *A.S.M.E.* code.

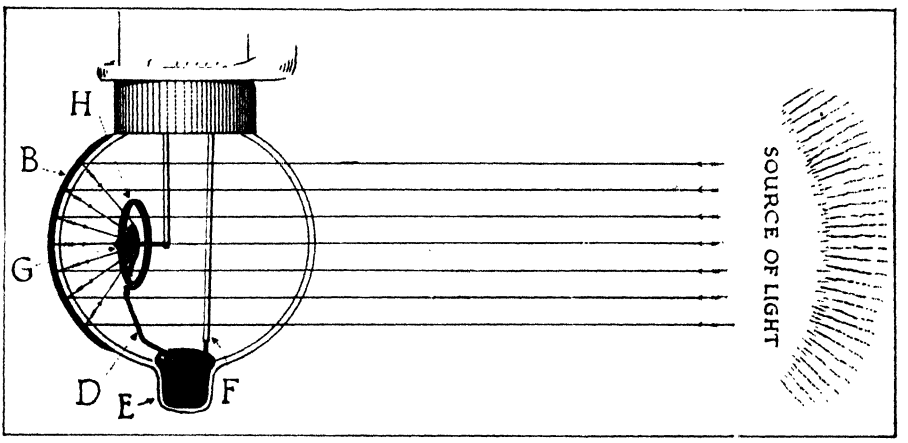
STOKER TIMER CONTROLS

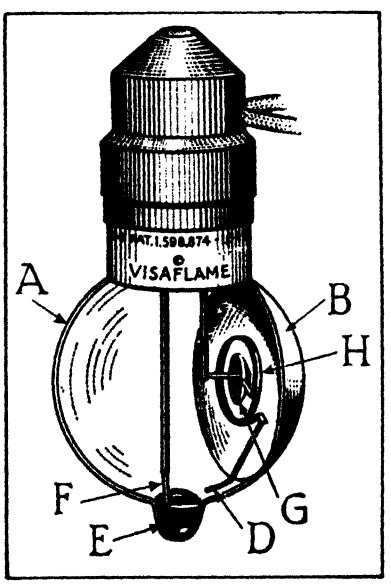
Type TV2 Stok-A-Timer combines a Mercoid Transformer-Relay and a synchronous motor timer mechanism for maintaining the stoker fire during periods when thermostat is not calling for heat. Interval adjustment can be set for ½ hour or 1 hour merely by moving a lever.

MERCOID VISAFLAME CONTROL SYSTEM

(Actuated by Light)

FOR DOMESTIC AND INDUSTRIAL
OIL BURNER APPLICATIONS





The Visaflame is a departure from the usual oil burner control operation. Instead of having a safety control on the stack, actuated by the heat from combustion, the Visaflame is located within or adjacent to the oil burner where it uses the light of the flame as a means of actuating the control system. This permits a more direct and positive method for protection against flame failure, power failure, or low line voltage.

The Visaflame System lends itself to streamline burner design as it can be built into the burner unit by the manufacturer, thereby making it possible to test the complete burner with safety device at the factory which also simplifies and reduces the cost of installation in the field.

MANNER OF OPERATION

The Visaflame, when properly focused, closes its circuit in the presence of light and opens its circuit when the light is absent. The light of the flame passes through bulb "A" and is picked up by the concave reflector "B" which concentrates the light waves on the small bimetal coil "G". This bimetal coil is opaque and therefore transmutes the light waves into heat, which causes it to move the attached electrode "D" into the pool of mercury "E." The electric circuit is then closed between the fixed electrode "F" and the movable electrode "D." The outer bimetal coil "H" to which the movable electrode is attached, compensates for varying ambient temperatures.

The Visaflame is available for Intermittent Ignition or for Constant Ignition oil burners. Also for manually operated industrial burners. Adaptable to high-low flame operation.

Minneapolis-Honeywell Regulator Company

2958 Fourth Ave., S., **Minneapolis 8, Minn.** Cable Address: MINNREG, MINNEAPOLIS

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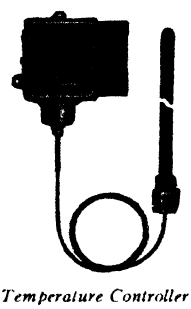


Temperature Controller

AUTOMATIC CONTROLS FOR EVERY APPLICATION

Minneapolis-Honeywell manufactures a complete line of electric, pneumatic, and self-contained control units and regulators designed for every type of heating, ventilating, and air conditioning installation. Indicating, recording, and controling instruments manufactured by Honeywell's Brown Instrument Division have wide application in the control of industrial processes.

Line Voltage Thermostat

RESPONSIBILITY FOR ENTIRE CONTROL SYSTEM

Minneapolis-Honeywell can supply a complete line of both electric and pneumatic controls. You can place full responsibility for **all** phases of automatic control with Honeywell. And you gain the advantage of unbiased advice about every type of control—advice based on Honeywell's 60 years of specialized engineering knowledge and experience.

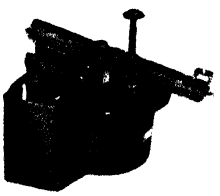
"Modutrol Valve"

THE MODUTROL SYSTEM OF ELECTRIC CONTROL

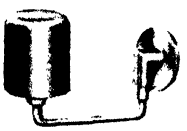
The Modutrol System designation is applied to any combination of Minneapolis-Honeywell Automatic Electric Controls or Self-contained Automatic Valves used to govern the operation of air conditioning or heating systems other than the small domestic installations. A wide variety of both modulating and two position motors, controllers and valves are available thus making the Modutrol System extremely flexible as to the selection of control equipment to produce the desired results.

Gradustat

Grad-U-Trol Valve

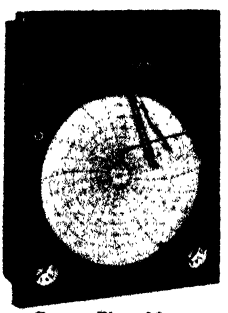


"Grad-U-Motor"—Pneumatic—for modulating control of dampers



Outdoor Weatherstat

Weatherstat Panel



Brown Flow Meter

THE GRADUTROL SYSTEM OF PNEUMATIC CONTROL

The Gradutrol System designation is applied to any combination of Minneapolis-Honeywell Automatic Pneumatic Controls used to govern the operation of air conditioning or heating systems. Such features as infinite positioning with the Gradutrol Relay and accurate graduation of valve and damper motors makes the Gradutrol System a truly remarkable advance in pneumatic control of commercial air conditioning and space heating installations.

COMBINATION ELECTRIC AND PNEUMATIC SYSTEMS

The outstanding advantages of both the electric Modutrol System and pneumatic Gradutrol System of control may be combined in a single installation. Thus maximum flexibility and low installation cost are obtained. Minneapolis-Honeywell can offer either an electric or pneumatic system, or a combination of the two. This is your guarantee of an unprejudiced recommendation.

WEATHERSTAT HEATING CONTROL SYSTEM

Heat Metered to the Weather

The outdoor control system that responds to wind, sun, and temperature conditions. Saves fuel, offers greater comfort to occupants by keeping a building in proper heating balance with all types of weather. Has wide usage on apartments, hotels, and other commercial and industrial buildings. The Weatherstat system is designed for direct control of the heating plant, or for zone applications. Zone systems are available in modulating or on-off control.

BROWN INSTRUMENTS

The extent to which air conditioning equipment is being used in office buildings, theatres, stores, industrial buildings, etc., has opened up a wide demand for indicating and recording resistance thermometers. To obtain uniform conditions and maximum economy from modern equipment, it is necessary that the engineer in charge have a visual picture of actual temperatures throughout the system.

Brown Resistance thermometers are available for indicating, recording, and controlling service and are applicable to all types of air conditioning and space heating installations.

In addition to Resistance Thermometers, The M-H Brown Instrument Division manufactures:

Thermometers
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Moeller Instrument Company

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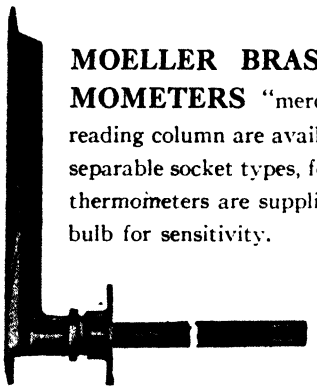
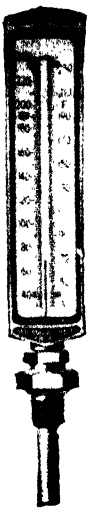
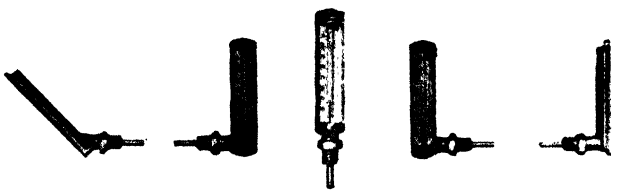
INSTRUMENTS FOR HEATING AND VENTILATING

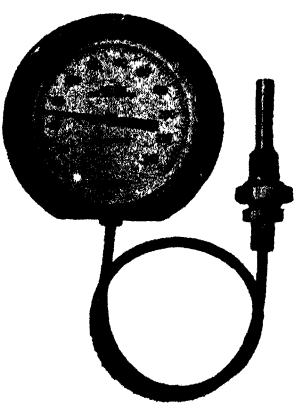


MOELLER BRASS CASE INDUSTRIAL THERMOMETERS "mercury filled" with MOELLER glass red reading column are available in 7, 9 and 12 in. cases, fixed, union or separable socket types, for pipe line and tank applications. Air duct thermometers are supplied with flanged union connection and bare bulb for sensitivity.

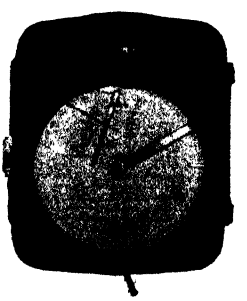




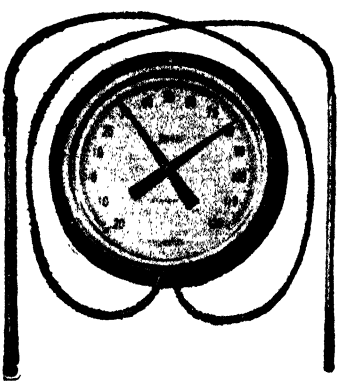
MOELLER DIAL AND RECORDING THERMOMETERS are mercury actuated, built for accuracy and long life. Dials are available in 4½, 6 and 8 in. sizes, single or duplex type. Recorders in 10 and 12 in. sizes, in 1, 2, 3 and 4 pen types.



Remote Reading Type, mercury actuated with separable socket connection. Back connection or flush mounting.



Single and multiple pen. Remote Reading types in rectangular or round cases.



Duplex mercury actuated, plain bulb type indicates temperatures at two separate points.

Send for catalogs and literature on

INDUSTRIAL • LABORATORY AND RECORDING THERMOMETERS THERMOSTATS • HYGROMETERS • HYDROMETERS • PSYCHROMETERS and MARINE SPECIALTIES

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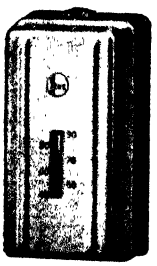
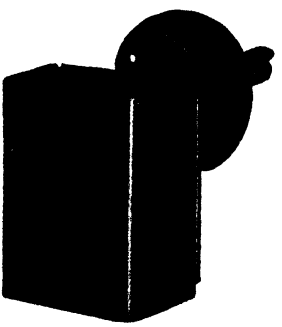
Automatic Controls for Heating, Refrigeration, Air Conditioning, Engines, Pumps and Air Compressors

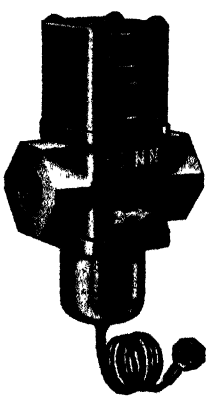


Thermostats

Stoker Timers



Oil Burner Stack Switches



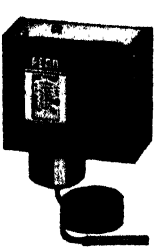
Water Valves

HEATING CONTROLS

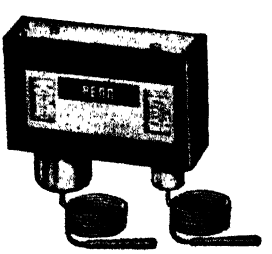
The Penn line of controls includes models for every type of heating service on steam, vapor, hot water or warm air systems whether gas, oil or coal fired. In this complete line there are: Low and line voltage Room Thermostats—Stoker Timers—Oil Burner Stack Switches—Hot Water and Warm Air Temperature Controls—Vapor Controls—Steam Pressure Controls—Relays—Humidistats—Day-Nite Tem Clocks—Damper Motor Controls—and Solenoid Valves. Condensed description and specifications are given in Bulletin 1508. *Write for your free copy.*

REFRIGERATION CONTROLS

Whatever your need may be in refrigeration controls—choose the exact type to fit the job from Penn's complete line of automatic controls. New series "270" pressure and temperature controls feature two-pole construction and direct reading calibrated scales. Also: Cooling Room Thermostats—Humidistats—Relays—Solenoid Valves—and Water Regulating Valves. All of these controls are described and illustrated in condensed Bulletin 1487. *Write for your free copy.*



New Series "270" Low Side Pressure Control



New Series "271" Dual Pressure Control

THE POWERS REGULATOR CO.

Over 55 Years of Temperature and Humidity Control—Offices in 47 Cities

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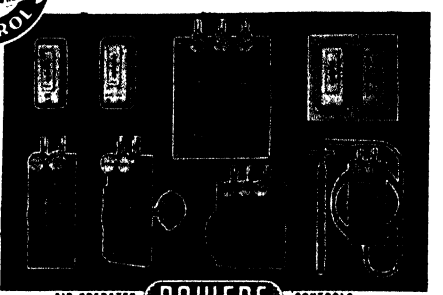
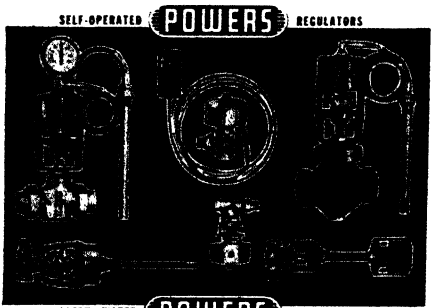
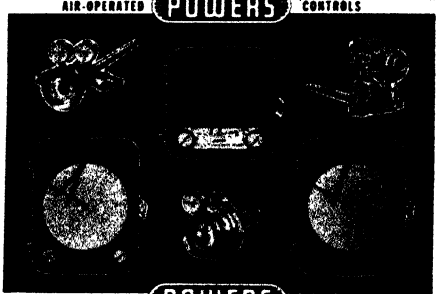
A very complete line of Temperature, Humidity, Pressure — indicating, controlling, and recording regulators — for heating and air conditioning systems, industrial processes and all types of hot water heaters.



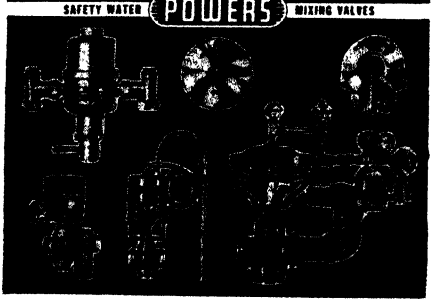
SELF-OPERATED POWERS REGULATORS



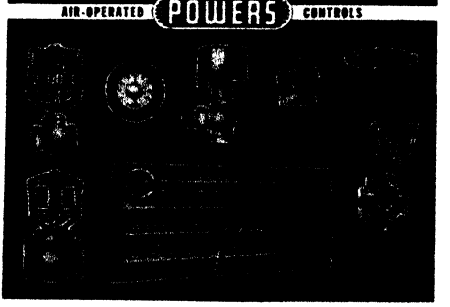
AIR-OPERATED POWERS CONTROLS



SAFETY WATER POWERS MIXING VALVES



AIR-OPERATED POWERS CONTROLS



Over 55 years of experience in furnishing and installing temperature and humidity control for every conceivable purpose in all types of buildings have given us a wealth of experience from which you can draw in selecting the proper type of control for any purpose.

Catalogs and Bulletins describing any or all of our products furnished upon request. Phone or write our nearest office. See your phone directory.

Spence Engineering Company, Inc.

28 Grant Street, **Walden, N. Y.**

SPENCE METAL DIAPHRAGM "DEAD END" REGULATORS

Advantages of Spence Regulators

Dead-end Shutoff—Spence Regulators are guaranteed to hold a dead-end.

Single Seat—Spence design makes possible a balanced single seat even in large sizes.

Metal Diaphragms—Under normal conditions never require replacement.

Accurate Regulation—Regardless of fluctuations in either load or initial pressure.

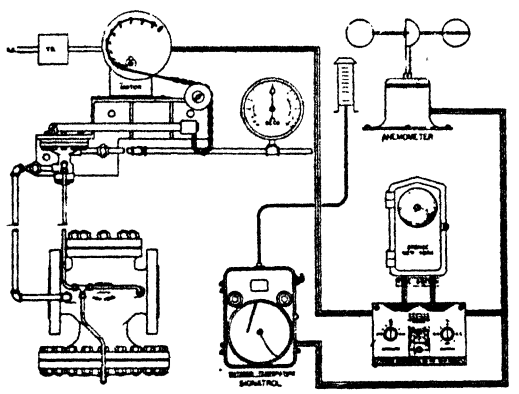
SECO Metal—Guaranteed to resist the wiredrawing action of steam.

Interchangeable Pilots—Any type of pilot will fit any size main valve.

Accessibility—Pilot is connected to main valve with unions.

No Stuffing Boxes—All main valves and most pilots are packless.

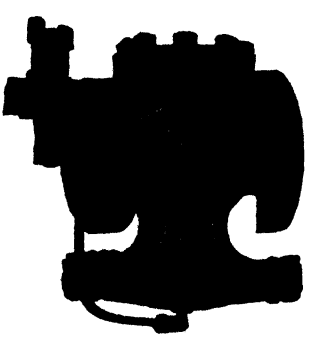
Spence Weather Compensator and Orifice Zone Control System



This simple, dependable Control, when installed on a properly designed orificed heating system, will show a substantial degree-day steam saving, at a low maintenance cost.

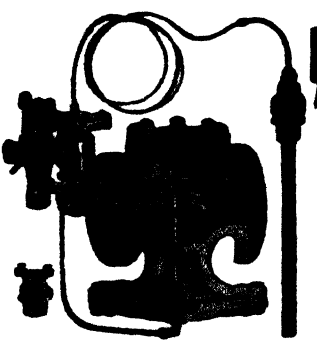
The delivery pressure of the Regulator is automatically adjusted in direct proportion to the building heat losses. In other words, as the losses become greater, steam pressure on the system is automatically increased.

Any number of zones can be controlled by one automatic Signatrol, automatic Wind Loss Compensator (Anemometer), Time Switch and Master Control Panel equipped with Manual and Automatic Dials for each zone. In this way each zone can be set individually and at the same time be under the Master Control.



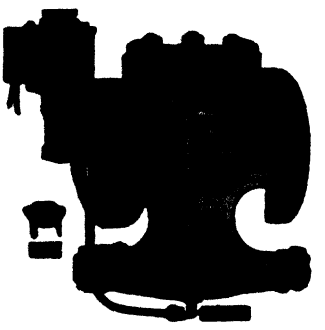
Pressure Regulator—Type ED

Designed to regulate a steady or varying initial pressure so as to maintain a constant, adjustable, delivery pressure. Applicable to heating systems, power plant operations, or manufacturing processes.



Combined Temperature and Pressure Regulator—Type ETD

Self-contained, pilot operated, dead-end. Designed to control flow of fluid to a heating or cooling element, so as to maintain a constant, adjustable temperature, and protect the element against excessive pressure.



Electrically Operated Valve—Type EM

Can be opened or closed independently by an electrical switch.

Type ET—Same as ETD except pressure control is omitted.

Order a SPENCE Regulator for 40 days' free trial.

Fall-O-Matic Universal Pipe Intersection Cutter.

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Manufacturing Distributors in Great Britain, Short & Mason, Ltd. London

Taylor Instruments for Indicating, Recording and Controlling Temperature, Pressure, Humidity, Flow and Liquid Level

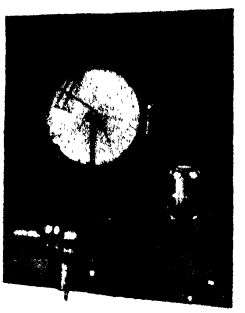
Taylor Industrial Thermometers—with new "BINOC" Tubing—Includes many styles and scale ranges with bulbs for every application. These thermometers contain a new and radical development of tremendous importance—*"BINOC" Tubing*. This newly designed and optically correct glass tubing assures an ease of reading that has been generally lacking in industrial thermometers. *"BINOC" Tubing* more than doubles the angle of vision within which readings can be made. Because of the patented Triple-lens construction its broad mercury column can be read easily and accurately with both eyes. Bore reflection is absent.

Taylor Biram's Anemometer—For measuring air velocities with fan revolutions indicated on dial. Various models for a wide range of air speeds and registration limits.

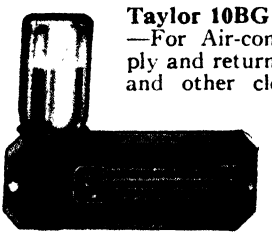
The Taylor "Fulscope" Recording Controller—An air-operated controller that gives practically any character of process control regardless of *time lag* in apparatus.

Available for controlling temperature, pressure, humidity, rate of flow, liquid level. Where extreme load changes or badly balanced operating conditions exist, precision control can be maintained by the automatic reset feature. For applications where a record is not needed, Taylor supplies an Indicating "Fulscope" Controller.

Taylor Recording Hygrometer—Records both wet- and dry-bulb temperatures on the same chart in different colored inks, making comparison very easy.



Type shown has motor-driven fan for conditioned rooms or passages where circulation is poor. Furnished without fan for installations where circulation across bulb is good.



Taylor 10BG Hygrometers—For Air-conditioning supply and return ducts, dryers, and other closed compartments where temperature and humidity readings are desired. Combines the accuracy of an etched-stem thermometer and ruggedness of an industrial thermometer. Easily installed. Available with bottle or constant automatic water supply.

Taylor Sling Psychrometer—Two accurate etched-stem thermometers mounted on die-cast frame, with the bulb of one covered with a wick to be moistened. Whirling bulbs subject this hygrometer to complete air contact to produce extreme accuracy of temperature and humidity measurement.

Taylor also offers a complete line of the famous Taylor Recording and Dial Thermometers; Ratio, Pneumatic Set, Self-Acting and Type "P" Controllers; Indicating Hygrometers and many types of Humidiguides.

United States Gauge

Sellersville 44, Penna.

Division of American Machine and Metals, Inc.

MANUFACTURERS OF PRESSURE, TEMPERATURE, FLOW AND ELECTRICAL MEASURING INSTRUMENTS

OFFICES AND DISTRIBUTORS IN PRINCIPAL CITIES

MOST COMPLETE LINE OF ITS KIND

You will probably find in the U. S. Gauge line, the instrument you need for indicating or recording pressure, temperature, flow or electrical values.

USG Instruments have a reputation for performing accurately, uniformly over a long period—as evidenced by the choice of experts—the manufacturers who install U. S. Gauges on over 6 out of every 10 pieces of original equipment. The **USG** system of quality control and 40 years of instrument manufacturing experience is your guarantee of dependable service from instruments that always "TELL THE TRUTH."

COMBINATION THERMOMETER AND ALTITUDE GAUGE

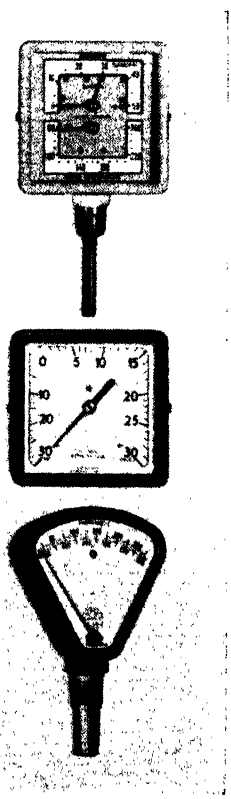
For use on hot water heating systems. Indicates on one dial: water temperature, head of water above gauge and pressure in system. Rugged construction with easy-to-read dial. Available in round or square case.

COMPOUND PRESSURE AND VACUUM GAUGE

Designed for installation on boilers, steam pressure, refrigeration, air conditioning and house heating systems, where it is desired to read pressure and vacuum on one dial. Available with or without an internal syphon, it has a sturdy corrosion resistant movement and a bronze bourdon tube. Furnished in dial sizes from 2 in. to 4½ in. Ranges from 15 to 300 lbs per sq in.

BI-METAL THERMOMETER

Attractive fan shaped dial thermometer, for installation on hot water boilers in house heating systems or other apparatus where sensitive bi-metallic element mounted in bulb can be used. Can be supplied in black, satin, chromium or nickel-finished case. Temperature range 60-260 F. Also made with back connection.



White-Rodgers Electric Company

1209 Cass Avenue, **St. Louis 6, Mo.**

AUTOMATIC CONTROLS

for

HEATING • AIR-CONDITIONING • REFRIGERATION

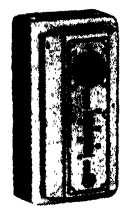
White-Rodgers controls with Hydraulic-Action have many features that assure complete accuracy and dependability in all applications—

- Maximum Sensitivity.
- Positive Settings.
- Full Range Accuracy.
- Consistant Differential.
- No Temperature Drift.
- Easily Adjusted.
- Extra Sturdy Switch.
- High Electrical Ratings.
- Versatility.
- Protected Switch.
- Not affected by Ambient Temperature or Atmospheric pressure.

THERMOSTATS

Series 120

Series 150



Series 130

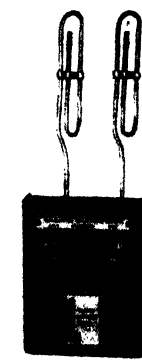
Series 120 and 130 light-duty, low-voltage thermostats are smartly designed with visible touch temperature adjustor. Unusually sensitive with powerful snap action that assures long life. Series 150, with Hydraulic-Action, are heavy-duty, line-voltage thermostats . . . for unit heaters, unit coolers, display cases, walk-in boxes and similar applications.

WARM AIR, STEAM AND HOT WATER CONTROLS

These controls are recommended wherever maximum flexibility must combine with extreme accuracy: Series 1100, Hydraulic-Action hot water controls designed for strap-on installations or with vertical or angle immersion wells; single or dual open and close-on-rise in compact case. Series 500, Hydraulic-Action warm air fan and limit, single or dual. Series 1200, steam or vapor pressure controls; short bellows movement insures long life.

Series 1200

Series 1100



Series 500

GAS CONTROLS

Series 3000

Series 2500

Series 2600

White-Rodgers Diaphragm Gas Valves, Series 2600, are readily applicable to all types of domestic and small industrial heating installations including boilers, conversion burners and floor furnaces. Light weight, easy to install, provided with manual operation switch in case of power failure. Also available with built-in mechanical limit control.

Series 2500 Solenoid Gas Valves, are desirable on installations requiring small overall dimensions. Especially designed centering springs eliminate chattering and magnetic hum. Each valve and seat individually ground and lapped for perfect fit. Series 3000 Gas Safety Pilots, made completely of stainless steel, employ a principle of differential expansion to close the main valve when pilot flame is extinguished. Economical . . . use less than 2 cu ft per hour at a line pressure of 3½ inches.

Burnham Corporation

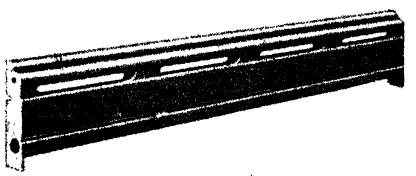
BOILERS and RADIATORS

Irvington-on-Hudson, N. Y.

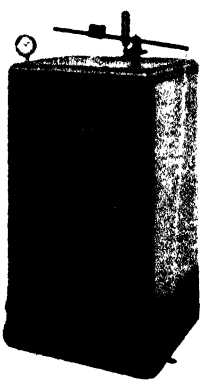
***There's a Burnham for Every Purpose*—Catalog No. 80 Sent on Request**

BASE-RAY Radiant Heating with Radiant Baseboards

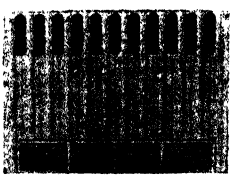
STANDARD Model BASE-RAY—Ratings—1.25 sq ft per lineal foot. Tappings—¾ in. at bottom only of both end panels. Sections are 7 in. high, 1¾ in. thick and in 12 and 24 in. length.



HY-POWER Model BASE-RAY—Ratings—2.08 sq ft per lineal foot. Tappings—¾ in. at bottom only of both end panels. Sections are 7 in. high, 2 in. thick and in 12 and 24 in. length.

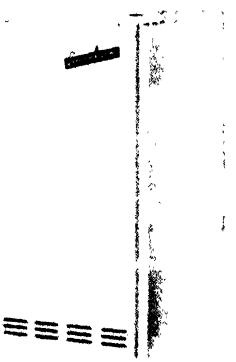


No. 1, 2, 3 and 36 in. Series—All Fuel. 230 to 4920 sq ft Steam and 370 to 7880 for Water.

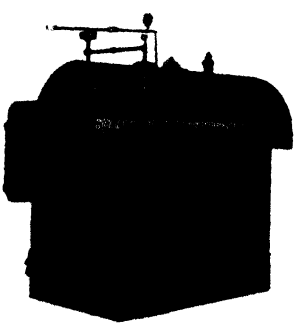


Burnham Radiant Radiator—Two heights. 20 and 23 in.

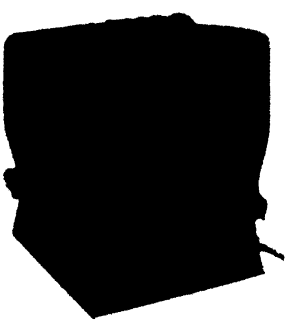
Burnham Slenderized Radiators (not shown) made in three to six tubes in all heights from 19 in. to 33 in.



YELLO-JACKET Boiler (with extended Jacket)—All Fuel Convertible. 305 to 935 sq ft for Steam and 490 to 1495 sq ft for Water.



Welded Steel Boiler—Capacities from 2500 to 35,000 sq ft for Steam and 4800 to 56,000 sq ft for Water. Furnished for coal, oil or stoker firing.



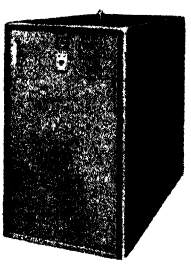
50 In. Twin-Section—4500 to 14,600 sq ft for Steam and 7200 to 23,360 sq ft for Water.

AMERICAN RADIATOR & Standard Sanitary CORPORATION

Pittsburgh 30, Pa.

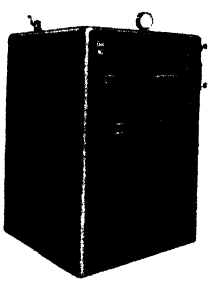
SEVERN BOILER FOR Coal (hand fired or stoker), or Oil

An efficient Boiler with many new features for convenience and economy. *Ratings:* Steam—350 to 780 sq ft, Water—560 to 1250 sq ft, installed radiation.



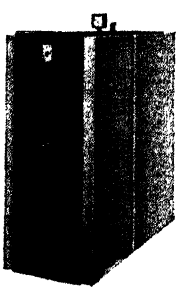
OAKMONT OIL BOILER

Exclusively for oil firing. Also supplied as complete boiler-burner unit with Arcoflame Burner. *Ratings:* Steam—390 to 810 sq ft, Water—625 to 1295 sq ft, installed radiation.



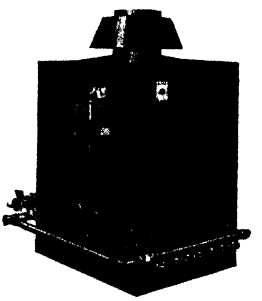
EXBROOK BOILER—For Oil or Stoker

A new boiler in sizes adapted for larger than average homes and buildings. *Ratings:* Steam 775 to 1650 sq ft, Water 1240 to 2640 sq ft installed radiation.



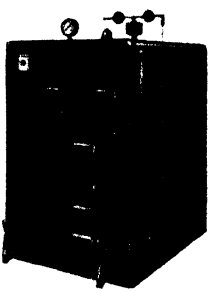
ARCOLINER OIL BOILER

A boiler of advanced design for smaller homes. Wet base construction *Ratings:* Steam—260 to 520 sq ft, Water—420 to 835 sq ft, installed radiation.



STANDARD GAS BOILER

Designed by experts to burn gas efficiently, and economically. *Ratings:* Steam — 400 to 12,420 sq ft, Water — 135 to 19,860 sq ft, installed radiation.

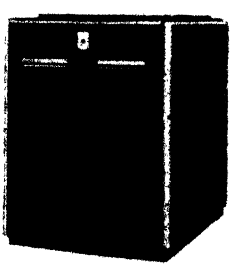


REDFLASH BOILERS For All Fuels

Economical heat for any size or kind of building. Ingot red jacket, fully insulated. *Ratings:* Steam—770 to 9900 sq ft, Water—1230 to 15,840 sq ft, installed radiation.

WATER TUBE BOILERS Stoker or Oil

For medium to large buildings. Efficient and economical. *Ratings:* Steam—930 to 4600 sq ft, Water—1490 to 7360 sq ft, installed radiation.



MOHAWK Winter Air Conditioner Gas-Fired

Provides automatic gas-fired Winter Air Conditioning in homes of any size. Capacities range from 43,200 to 216,000 Btu input per hour.

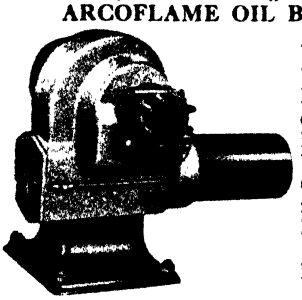
AMERICAN RADIATOR & Standard Sanitary CORPORATION

Pittsburgh 30, Pa.

YOU CAN FILL EVERY HEATING NEED FROM THIS COMPLETE LINE

From AMERICAN-Standard come Boilers, Warm Air Furnaces and Winter Air Conditioners of all types and sizes for Coal—stoker or hand-fired—Oil, or Gas, and a full line of Radiators, Convectors, Oil Burners, Domestic Water Heaters, and Accessories—all backed by the undivided responsibility of one of the world's largest manufacturers of Heating and Plumbing Equipment.

ARCOFLAME OIL BURNERS

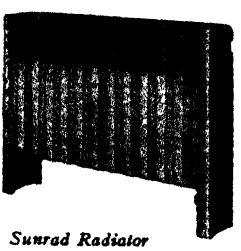


The Model "C" Arcoflame has a capacity of up to 3 gallons per hour. The Model "L" (not shown) from 3 to 7 gallons per hour. Both are highly efficient.

Arco Radiator

ARCO RADIATOR

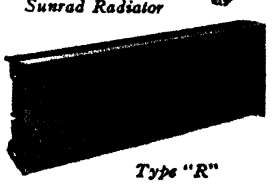
The modern, slim type radiator that occupies less space and gives more heat. It comes in four narrow widths and in four heights —19, 22, 25 and 32 inches.



Sunrad Radiator

SUNRAD RADIATOR

Installed recessed or free-standing. Requires no enclosure. Two sizes: 20 in. high x 5 in. wide = 2 sq ft, and 23 in. x 7½ in. = 3 sq ft.



Type "R"

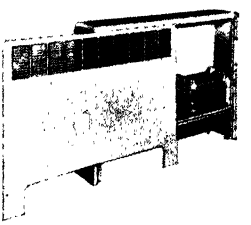
Type "RC"

BASE-BOARD RADIANT PANELS

Made to replace ordinary baseboards. Available in two styles: Radiant type 1.25 sq ft per lineal foot. Convertor type 2.08 sq ft.

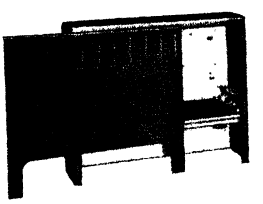
ARCO CAST IRON CONVECTOR

For convection heating. Available in four widths and in virtually any desired length.



ARCO MULTIFIN CONVECTOR

For all systems except one-pipe steam. Made in five widths. Non-ferrous.



BUDGET GAS FIRED WATER HEATER

Heats water automatically, stores it for instant use. Jacket finished in white enamel, black trim. Thrifty and dependable. Four sizes —15, 20, 30, and 40 gallons.

Budget Gas Fired

EXCELSO INDIRECT WATER HEATER

A complete line ranging from 30 to 2500 gal capacity.

No. 861 Hurivent Valve (for mains)

No. 800 Multiport Adjustable Valve (for radiators)

No. 999 Arco Packless Steam Radiator Valve

Crane Co.

BOILERS, RADIATORS, FURNACES, VALVES, FITTINGS, PIPE, WATER AND STEAM SPECIALTIES, CONTROLS AND PLUMBING MATERIALS

General Offices: 836 South Michigan Avenue, **Chicago 5, Illinois**

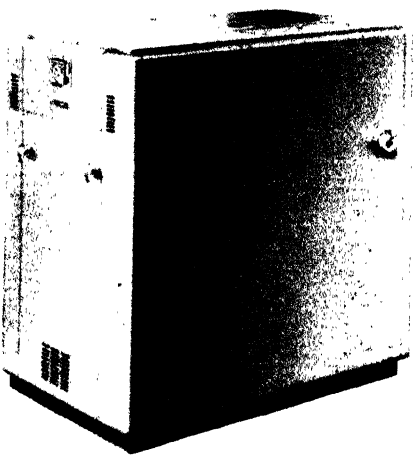
Nation-Wide Service Through Branches, Wholesalers, Plumbing and Heating Contractors

CRANE OFFERS EVERYTHING IN HOME HEATING

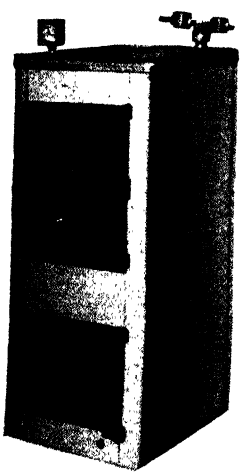
There's a Crane Boiler to fit any home—regardless of its size—whether coal, coke, oil or gas is the preferred fuel or whether the owner wants steam or hot water heating. These boilers are styled for beauty, dependability and simplicity, and they incorporate many new engineering features that assure greater fuel economy and operating efficiency.

Crane also builds boilers for many types of non-residential buildings. In addition, the Crane line includes everything else needed for heating systems—furnaces, stokers, oil burners, radiators, convectors, controls, water and steam specialties, pipe, valves and fittings.

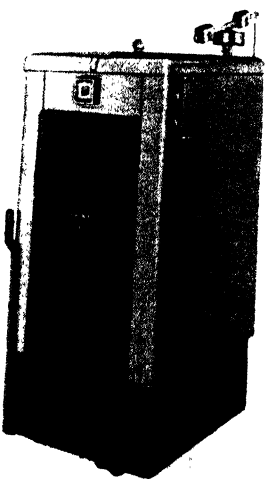
For full information on Crane Boilers and other heating equipment, consult your Crane Branch or Crane Wholesaler.



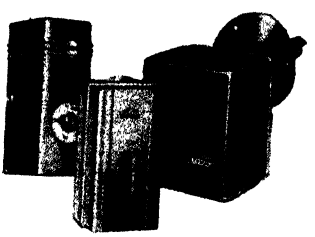
CRANE SIXTEEN BOILER—BURNER UNIT



CRANE FOURTEEN BOILER



CRANE TWENTY BOILER



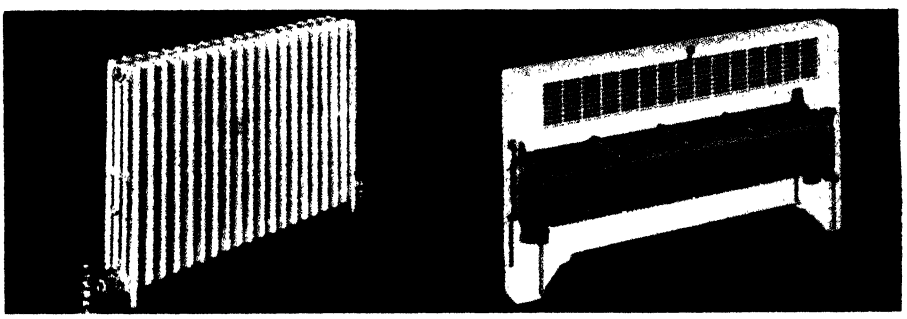
CONTROLS

The complete line of controls includes thermostats, stack switches, limit switches, aquastats, damper controls—everything necessary for a heating system.

COMING! CRANE RADIANT BASEBOARD HEATING

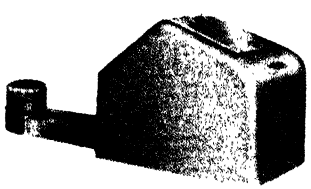
Steam or hot water is circulated through the baseboard panel — no radiators or grilles are necessary. Will give many advantages: more room space; more uniform distribution of heat; easier cleaning. Recommend it to customers who are planning new homes or remodeling.

CRANE RADIATORS AND CONVECTORS



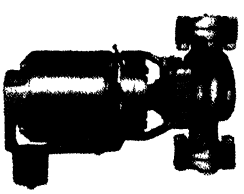
COMPAC RADIATORS: Slender in line—modern in design—give more heat —use less space. For free-standing or recessed installation, steam or hot water.

CONVECTORS: For attractive installations that harmonize perfectly with room decorations. Recessed or free-standing types for new construction or remodeling.



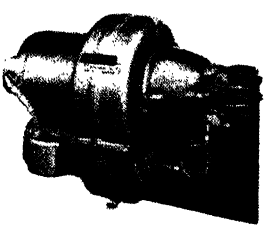
STOKERS

Newly designed and engineered. Assure uniform heating with minimum fuel consumption and minimum attention. Wide range of sizes.



WATER SPECIALTIES

Crane hot water specialties are made to suit every installation. They include water heaters, circulators and flow control valves—all top-quality equipment.



OIL BURNERS

Newly engineered. Crane oil burners provide heating comfort at low fuel costs. Simplified design and sturdy construction reduce maintenance to a minimum.

THE NATIONAL RADIATOR COMPANY

MODERN DESIGN HEATING EQUIPMENT

Johnstown Pennsylvania

Branch Offices:

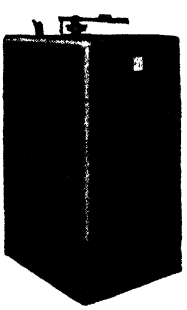
BALTIMORE.....2100 St. Paul Street
BOSTON.....620 Newbury Street
CHICAGO.....400 West Madison Street
NEW YORK.....60 East 42nd Street
PHILADELPHIA.....401 North Broad Street
PITTSBURGH.....Fourth and Wood Streets
RICHMOND.....12 South Third Street
WASHINGTON.....4034 Georgia Avenue, N.W.

"100" Series

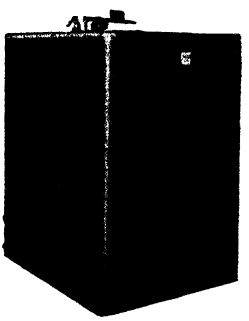
NATIONAL HEAT EXTRACTOR CAST IRON BOILERS. The distinguished family of National Heat Extractors was designed with an appreciation for the requirements of automatic heating. National Heat Extractors are provided with many features to insure high operating efficiency and maximum fuel economy. These include extended heating surface, multiple-flue section construction, effectively insulated jacket and doors and heat conserver baffles. Convertible from hand to automatic firing after installation and readily adaptable to any desired fuel or method of firing. Wide range of both storage and tankless domestic water heaters available.

NATIONAL OIL HEATING UNITS, cast iron or steel, provide complete "one package" equipment designed for maximum efficiency and top performance with this fuel. Complete automatic controls, prefabricated combustion chamber of proper proportions, quiet burner for rear firing and an attractive all-enclosing jacket.

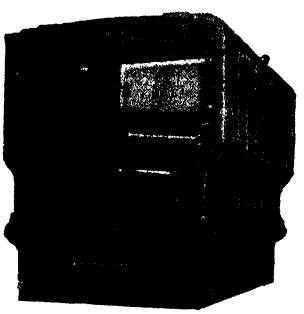
NATIONAL GAS BOILERS are modern, compact and designed exclusively for gas firing. Cast iron sections for long life and dependability. Tapered flues, long zigzag fire travel and heavy insulation insure efficiency and economy.



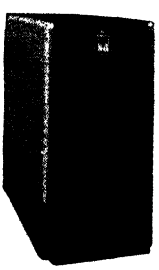
"200" Series



"300" and "400" Series



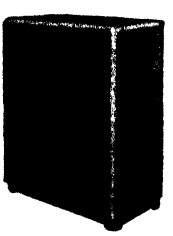
"500" Series



Oil Heating Unit

HEAT EXTRACTOR BOILERS

Boiler Series	Net I-B-R Ratings, Sq Ft	
	Steam	Water
100	170 to 410	270 to 660
200	350 to 880	560 to 1410
300	700 to 2300	1120 to 3680
400	2500 to 6000	4000 to 9600
500	4000 to 10300	6400 to 16480



Gas Boiler

OIL HEATING UNITS

Type of Unit	Net Ratings, Sq Ft	
	Steam	Water
100 Series Cast Iron	230 to 410	370 to 660
200 Series Cast Iron	400 to 880	640 to 1410
Residential Steel	275 to 700	440 to 1120

GAS BOILERS

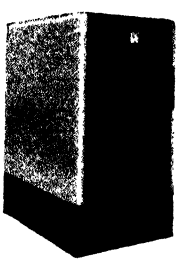
Boiler Series	Net Ratings, Sq Ft A.G.A. Approved	
	Steam	Water
20	109 to 390	174 to 624
30	353 to 983	565 to 1570
40	445 to 1920	711 to 3070

18"-23" Steel Boiler

NATIONAL STEEL BOILERS meet all the requirements of the *SBI* Testing and Rating Code and the *ASME* Boiler Construction Code. All are inspected and approved by a representative of the *Hartford Steam Boiler Inspection and Insurance Company.* The 18 in. and 23 in. Series RESIDENTIAL STEEL BOILERS are designed for smaller homes. The 26 in., 29 in., and 39 in. Series RESIDENTIAL STEEL BOILERS are designed specifically for large homes, apartments, and commercial installations. Can be furnished unjacketed, or with modernly styled heavily insulated jacket.

RESIDENTIAL STEEL BOILERS

Boiler Series	SBI Net Ratings, Sq Ft	
	Steam	Water
18" and 23"	275 to 700	440 to 1120
26", 29", and 39"	700 to 3000	1120 to 4800

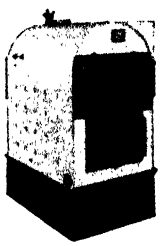


26"-29"-39" Steel Boiler

NATIONAL COMMERCIAL STEEL BOILERS are designed to supply the heating needs of larger buildings. Their firebox proportions conform with the recommendations of the *Stoker Manufacturers' Association.* Hand fired boilers may be converted to stoker, oil, or gas firing at any time after installation.

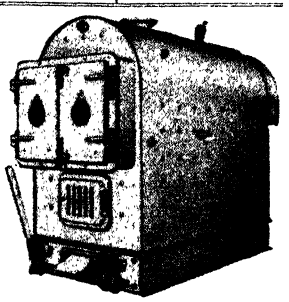
COMMERCIAL STEEL BOILERS

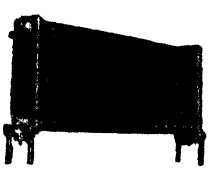
Boiler Type	SBI Net Ratings, Sq Ft	
	Steam	Water
Automatically fired	3000 to 35000	4800 to 56000
Hand fired	2500 to 29170	4000 to 46670



26"-29"-39" Steel Boiler Unjacketed

Commercial Steel Boiler

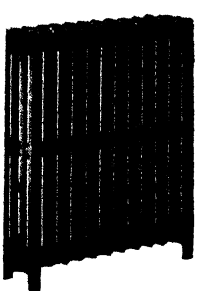




Aero Convector

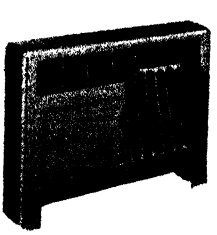
NATIONAL AERO CONVECTORS are of compact cast iron design with fins cast integral with tubes. Adaptable to any type of heating system and can be used with direct radiation.

NATIONAL ART RADIATORS blend inconspicuously with most decorative schemes. Compact proportions require minimum floor space. A wide variety of sizes and ratings can be furnished.



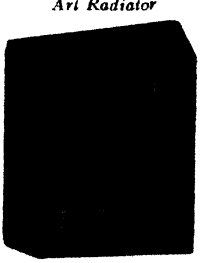
Art Radiator

NATIONAL CONVECTOR ENCLOSURES are made in several different types applicable to modern structural or decorative requirements. They were designed to develop maximum output of the convector.



Convector Enclosure

NATIONAL UNIT HEATERS are designed for quiet, economical operation with steam or hot water. Available in both Horizontal and Vertical delivery types in a number of sizes.



Unit Heater Horizontal Delivery

Spencer Heater

Division—The AVCO Manufacturing Corporation

Williamsport, Pa.

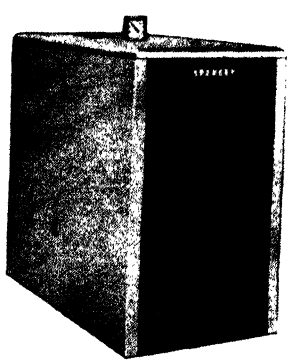
NEW YORK	SAN ANTONIO	WASHINGTON	GREENSBORO	CINCINNATI	INDIANAPOLIS
PHILADELPHIA	HARRISBURG	DALLAS	NASHVILLE	LOS ANGELES	CHICAGO
BOSTON	ALLENTOWN	RICHMOND	COLUMBUS	CLEVELAND	ST. PAUL
BINGHAMPTON	BALTIMORE			DETROIT	PORTLAND

Since 1888 Spencer has been manufacturing quality automatic magazine feed heaters—and has pioneered other outstanding developments in the heating industry. The Spencer line today includes a series of steel tubular boilers of proven design, quality and workmanship.

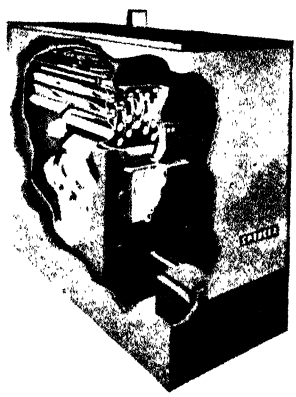
SPENCER STEEL HEATING BOILERS for Oil, Stoker or Hand-firing.

SPENCER SERIES "K" Net S.B.I. 320 to 550

A star performer in the Spencer line for small and medium homes for steam, vapor or hot water heating. Its beautiful two-tone jacket makes it easy to add another room in the basement. It is delivered with standard or extended jackets. A steel tubular heating boiler that can be oil or stoker-fired. Easily converted to a hand fired unit, it will give efficient, economical performance for many years. Here are a few reasons why the Spencer "K" performs so well: Insulated precision-ground doors —heavy duty uniform wall thickness steel tubes—square fire box and fire tube turbulators insure high temperature combustion —low stack loss.



Spencer Series "K"



Spencer Series "C"

SPENCER SERIES "C" Net S.B.I. 700 to 3000

The ideal boiler for homes and smaller commercial buildings. The "C" boiler's amazing economical efficient performance is the result of Spencer's 59 years' experience. It is fitted with beautiful standard or extended jackets. Its many exclusive Spencer features make it easy to install—easy to clean—a safe, practical boiler that gives long, trouble-free service. Spencer hot water heating service can be readily installed for year-round hot water. The "C" boiler is designed for oil or stoker firing but also available with specially designed grate equipment for hand firing.

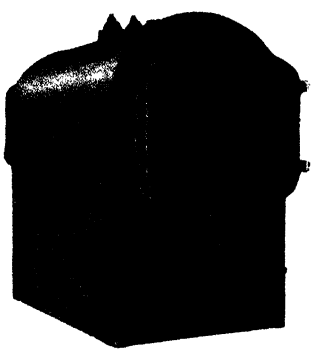
All Spencer "K" & "C" Series Boilers are manufactured in accordance with the *ASME Codes* and are fully approved by the *Steel Boiler Institute.*

SPENCER SERIES "A"
1800 to 42,500 Square Feet EDR Steam

For large homes, commercial buildings or apartments. The many features of the Spencer Series "A" are essentially the same for hand firing, oil, gas or stoker types.

The series "A" is of proven design—in use in thousands of installations. Spencer's peaked firebox design affords rapid natural circulation of boiler water and provides a self cleaning action. Maximum heating surface assures quick steaming with efficient low cost operation. All its internal units are easily accessible—easy to clean, keeping boiler at peak efficiency—resulting in economical performance. The "A" boiler has either rear or top smoke box outlet and you can readily install the Spencer year-round hot water system.

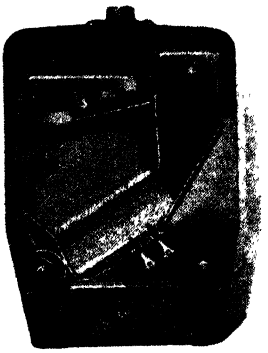
All sizes available with either mechanical (oil, gas or stoker) or hand fire bases. Smokeless Arch supplied on special order.



Spencer Series "A"

SPENCER SERIES L-2 L-3
Capacities 690 to 4510 EDR (Steam)

Designed for quick, economical heat with minimum service requirements for larger homes, apartments or churches. Fuel feeds by gravity, automatically, constantly—needs little attention in 24-hour period. No mechanical parts—burns No. 1 buckwheat and pea size anthracite at substantial saving.



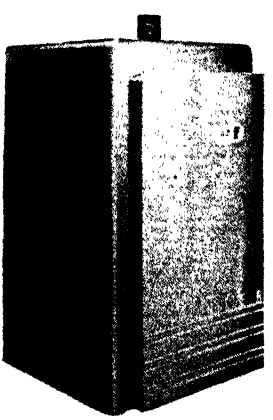
Spencer Series L-2

CAST IRON MAGAZINE FEED BOILERS

SPENCER SERIES "F"
From 290 to 740 EDR (Steam)

For the small home or building, you can't beat Spencer's "F" heater. Note clean design of Spencer's "F" series boiler. Jacket available in harmonious two-tone blue of highest quality steel . . . fully insulated. Its many features include easy accessibility for cleaning heating surfaces . . . no variance in combustion space and fire bed . . . no mechanical parts. The home owner really gets safe, trouble-free, economical performance with Spencer "F" heater.

The series "F" is one of the famous line of cast iron sectional magazine feed boilers especially designed to burn the small economical, buckwheat and pea size anthracite and coke fuels.



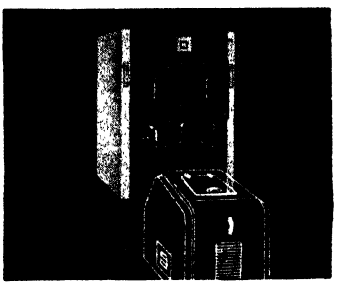
Spencer Series "F"

The H. B. Smith Company, Inc.

Westfield, Mass.

Branch Offices and Sales Representatives in Principal Cities

A complete line of modern cast iron sectional boilers for residential, commercial and industrial heating and for domestic hot water supply



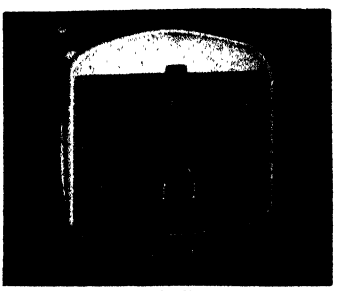
20 Mills

15-20-25 SMITH-MILLS BOILERS

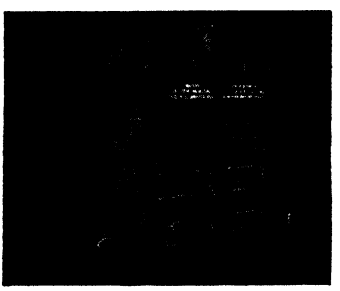
Capacities 200 sq ft to 2275 sq ft steam radiation. This complete line of modern push nipple boilers is available in models for oil, gas, stoker and hand firing. Provisions have been made for built-in domestic hot water heaters and controls.

MILLS WATER TUBE BOILERS
Series 24-34-44

Capacities 900 sq ft to 13,380 sq ft of steam radiation. Independent header type construction—tens of thousands of these famous Mills Boilers are installed in schools, hospitals, apartment houses, stores, and other commercial and public buildings. Models for hand and all types of automatic firing.



44 Mills



60 Smith

42 AND 60 SMITH BOILERS

May be used in batteries for heating loads up to and over 100,000 sq ft steam radiation. Many of these large units installed in industrial plants furnish steam for process requirements as well as for heating and domestic hot water.

SMITH HY-TEST BOILERS

Smith Hy-Test Boilers for hot water supply, are available in several models and many sizes for tank capacities to 20,000 gal. Constructed of the finest quality grey iron castings, these Hy-Test units are carefully tested at high pressures before shipment. The No. 17 series, for example, is tested at 350 lbs hydrostatic pressure—the highest test pressure of any cast iron boiler made.

17 HY-Test

Complete catalog information describing Smith boilers is filed in current issues of Sweet's "Architectural" and Domestic Engineering Catalog Directory

MEMBER

STEEL BOILER INSTITUTE · SBI · HEATING · PROCESS · POWER

Reg. U. S. Pat. Off.

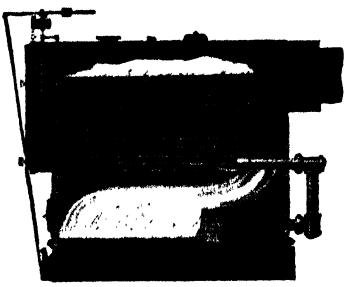
Pacific Steel Boiler DIVISION

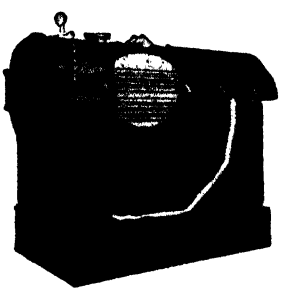
United States Radiator Corporation

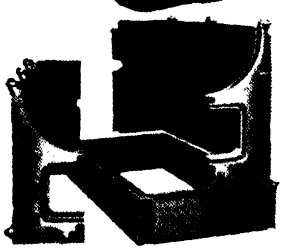
General Offices: **Detroit 31, Michigan**

Sales Offices in Principal Cities

A Complete Line of Low Pressure Steel Heating Boilers







All Pacific Boilers are built using the *A.S.M.E.* Boiler Code Standards as minimums, and rated in accordance with Steel Boiler Institute code.

DIRECT DRAFT AND SMOKELESS SERIES FOR COAL FIRING

Built in the following capacities for steam 2200 to 35,000 sq ft and in corresponding capacities for water.

All Pacific Boilers are built, inspected, and tested under the supervision of the Hartford Steam Boiler Inspection and Insurance Company.

HIGH FIRE BOX SERIES FOR MECHANICAL FIRING, STOKER, OIL OR GAS

Built in the following capacities for steam: 2680 to 56,830 sq ft and in corresponding capacities for water.

All Pacific Boilers are made of flange-quality steel, electrically welded—built to last.

PACIFIC THREE-PIECE CONSTRUCTION

All commercial sizes of Pacific Boilers are built in three sections—shell, firebox and base—and require minimum building opening. Where necessary, Pacific fireboxes can be split (as illustrated) to allow the boiler to be taken into the building in four sections. No cutting, no welding is required in assembling any Pacific Boiler.

PACIFIC RESIDENTIAL SERIES FOR COAL, STOKER, OIL OR GAS

Built in the following capacities for steam: 400 to 3000 sq ft and in corresponding capacities for water.

PACIFIC "*Plate Flue*" BOILER

For oil or gas—built in 4 sizes ranging from 400 to 900 sq ft steam and from 640 to 1440 sq ft water.

Descriptive Bulletins on Pacific Steel Heating Boilers will be mailed on request.

United States RADIATOR CORPORATION

Member I-B-R REG U. S. PAT. OFF.

GENERAL OFFICE, DETROIT 31, MICH. BRANCHES AND SALES OFFICES IN PRINCIPAL CITIES

US-CAPITOL*

THINTUBE RADIATORS

3-Tube

Heights In.	Per Section Heating Surface
25	1.6 Sq Ft

4-Tube

22	1.8 Sq Ft
25	2.0 Sq Ft

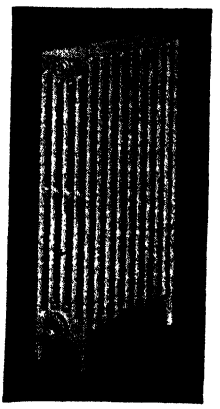
5-Tube

22	2.1 Sq Ft
25	2.4 Sq Ft

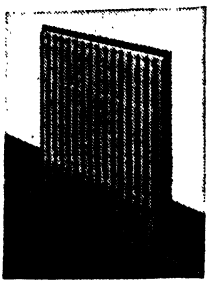
6-Tube

19	2.3 Sq Ft
25	3.0 Sq Ft
32	3.7 Sq Ft

*1¾ in. Centers.



US-SUNRAY RADIATORS



19 in. height is standard, 21 in. and 22½ in. heights can be furnished by use of higher legs.

No. 5—Depth 5¾ in.

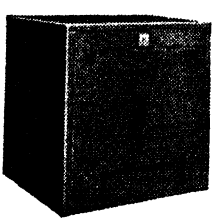
Heights In.	Per Section Heating Surface
19	1.8 Sq Ft

No. 6—Depth 6¾ in.

Heights In.	Per Section Heating Surface
19	1.8 Sq Ft

Boiler No.	A.G.A. Rating Sq Ft Water	A.G.A. Output Btu Per Hour	*Direct C. I. Radiator Load Sq Ft 150 Btu Per Sq Ft Emission	*Direct C. I. Radiator Load Sq Ft of Water Accelerated (200 Btu Per Sq Ft Emission)	Input Btu Per Hour	Water Inlets No. and Size	Water Outlets No. and Size	Flue Outlets No. and Size	Minimum Chimney Size	Size of Main Gas Valve
3-11	240	36,000	155	115	45,000	2-2½"	2-2½"	1-4"	4"	¾"
4-11	360	54,000	230	175	67,500	2-2½"	2-2½"	1-5"	5"	¾"
5-11	480	72,000	310	230	90,000	2-2½"	2-2½"	1-5"	5"	¾"
6-11	600	90,000	385	290	112,500	2-2½"	2-2½"	1-6"	6"	1"
7-11	720	108,000	470	350	135,000	2-2½"	2-2½"	1-7"	7"	1"
8-11	840	126,000	550	410	157,500	2-2½"	2-2½"	1-7"	7"	1"

* The Amount Allowed for Piping and Pickup Capacity for Each Boiler is Based on I-B-R Selection Factors.



US-22 "COMFORT LINE"

GAS BOILER

Data below

US-11 "COMFORT LINE"

GAS BOILER

Data above

Boiler No.	A.G.A. Rating Sq Ft Steam	A.G.A. Rating Sq Ft Water	A.G.A. Output Btu Per Hr	*Direct C.I. Radiator Load Sq Ft Steam	Sq Ft Water	Sq Ft of Water Accelerated	Input Btu Per Hr	Steam or Water Inlets No. and Size	Steam or Water Outlets No. and Size	Flue Outlets No. and Size Inches	Water Line Inches	Flue Size to Chimney Inches	Size of Main Gas Valve Inches
7-22	800	1280	192,000	530	850	635	240,000	2-3"	2-4"	1-9"	34"	9"	1¼"
9-22	1120	1790	268,800	750	1200	900	336,000	2-3"	2-4"	2-7"	34"	10"	1¼"
11-22	1440	2300	345,600	980	1570	1175	432,000	2-3"	2-4"	2-8"	34"	12"	1½"
13-22	1760	2820	422,400	1210	1940	1450	528,000	2-3"	2-4"	2-9"	34"	13"	1½"
15-22	2080	3330	499,200	1450	2320	1740	624,000	2-3"	2-4"	2-10"	34"	15"	2"
17-22	2400	3840	576,000	1690	2710	2030	720,000	2-3"	2-4"	3-9"	34"	16"	2"
19-22	2720	4350	652,800	1935	3100	2320	816,000	2-3"	2-4"	3-9"	34"	16"	2"
21-22	3040	4860	729,600	2170	3470	2600	912,000	2-3"	2-4"	3-10"	34"	18"	2"
23-22	3360	5370	806,400	2425	3880	2910	1,008,000	2-3"	2-4"	4-10"	34"	20"	2½"
25-22	3680	5890	883,200	2675	4280	3210	1,104,000	2-3"	2-4"	4-10"	34"	20"	2½"
27-22	4000	6400	960,000	2930	4690	3520	1,200,000	2-3"	2-4"	4-10"	34"	20"	2½"

*Based on I = B = R Piping and Pickup Allowances; Emission Btu per Sq Ft Steam 240, Water 150, Water Accelerated 200.

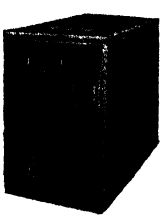
United States
RADIATOR CORPORATION
GENERAL OFFICE, DETROIT 31, MICH. BRANCHES AND SALES OFFICES IN PRINCIPAL CITIES

US-2
CAPITOL SUNRAY
OIL FIRED BOILER

Boiler No.	Net Sq Ft Direct Cast Iron Radiation		Net Btu Per Hr.	Gross Output Btu Per Hr.
	Steam	Water		
2-03	350	560	84,000	129,000
2-04	500	800	120,000	182,000
2-05	650	1040	156,000	234,000
2-06	800	1280	192,000	285,000

US-3
"THRIFT MODEL"
SUNRAY BOILER

Boiler Number	Sq Ft Direct Cast Iron Radiation					
	Hand Fired		Stoker Fired		Oil Fired	
	Steam	Water	Steam	Water	Steam	Water
R43-S or W	300	480	400	640	400	640
R53-S or W	450	720	550	880	550	880
R63-S or W	600	960	700	1120	700	1120



US-25
OIL FIRED BOILER

Boiler No.	Net Sq Ft Direct Cast Iron Radiation		Net Btu Per Hr.	Gross Output Per Hr.
	Steam	Water		
US-25-3	545	875	131,000	197,000
US-25-4	905	1450	217,000	320,000
US-25-5	1265	2025	304,000	439,000
US-25-6	1625	2600	390,000	555,000
US-25-7	1985	3175	476,000	669,000

RED TOP
CAPITOL BOILERS

"A" Series—All Fuels

Boiler No.	Sq Ft Direct Cast Iron Radiation	
	Steam	Water
A-7	340	545
A-8	440	705
A-9	540	865
A-10	640	1025
A-11	740	1185

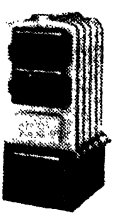
"B" Series—All Fuels

B-7	740	1180
B-8	920	1470
B-9	1110	1770
B-10	1275	2040
B-11	1440	2300
B-12	1580	2530
B-13	1730	2770
B-14	1880	3000

"C" Series—All Fuels

Boiler No.	Sq Ft Direct Cast Iron Radiator	
	Steam	Water
C-12	2250	3600
C-14	2715	4345
C-16	3180	5090
C-18	3645	5830
C-20	4110	6575
C-22	4575	7320
C-24	5040	8065
C-26	5450	8720
C-28	5800	9280
C-30	6110	9775

"DEEPFIRE"
HOT WATER
SUPPLY BOILERS
COAL OR OIL
100 lb Working Pressure



Capacity—Gallons
100° rise in 1 Hour

Coal Fired		Oil Fired	
Boiler No.	Gallons	Boiler No.	Gallons
30	132	030	115
40	252	040	165
50	360	050	215
60	450	060	265

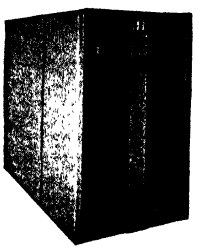
Weil-McLain Company

Manufacturing Division: **Michigan City, Ind. and Erie, Pa.**
General Offices: **641 W. Lake Street, Chicago 6, Ill.**
NEW YORK OFFICE: **501 Fifth Avenue**

Weil-McLain Boiler and Radiator service is made conveniently available through local stocks carried by Weil-McLain Distributors in most of the important distributing centers.

No. 68 Boiler for Automatic Firing

Boiler is completely jacketed and insulated. Has an integral front burner extension. Net I-B-R Ratings: Steam 390 to 690 sq ft, Water 625 to 1,100 sq ft.



No. 78 Boiler for Automatic Firing

Boiler has insulated enameled de luxe jacket. Front or rear jacket extension available. Net I-B-R Ratings: Steam 530 to 1,130 sq ft, Water 850 to 1,810 sq ft.

"RO Series" Boiler for Automatic Firing

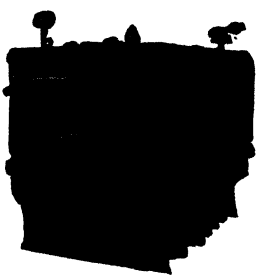
Jacketed and insulated round boiler for small homes. Connected Load Ratings: Steam 420 and 520 sq ft, Water 630 and 790 sq ft.

Nos. 57, 67, 77 All-Fuel Boilers

Conversion type boilers for hand or automatic firing. Connected Load Ratings: Steam 210 to 1000 sq ft, Water 340 to 1600 sq ft.

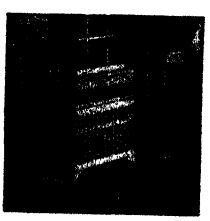
Round-Type Boiler

Unjacketed Round Boiler with corrugated heating surfaces for economical home heating. Connected Load Ratings: Steam 310 to 900 sq ft Water 490 to 1440 sq ft



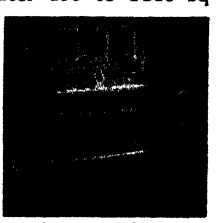
Square-Type Boilers

Sectional boilers for larger installations. Complete range of sizes. Connected Load Ratings: Steam 1,815 to 11,300 sq ft, Water 2,900 to 17,900 sq ft.



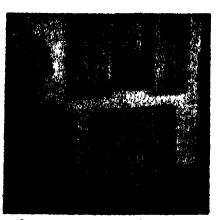
Raydiant "Concealed"

A Radiant convector type all cast-iron Radiator. Made in "Concealed," also Partially Recessed types.



Solray Radiator

Free standing all cast-iron Cabinet type Radiator with metal cover top. Available in three depths in 21, 24 and 27 in. heights.



Junior Radiator

Smaller Tubular type Radiation which conserves space. Available in 1¼ in. centers in 3, 4, 5 and 6 tube widths and 19 to 32 in. heights.

THE BABCOCK & WILCOX COMPANY

85 Liberty Street **New York 6, N. Y.**

Manufacturers of

Water-Tube Boilers
Oil Burners

Chain-Grate Stokers
Seamless Steel Tubing and Pipe

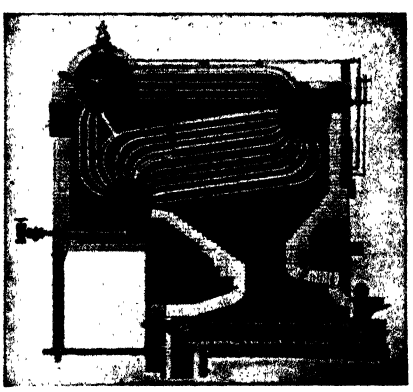
Branch Offices and Representatives in all Principal Cities

Type H Stirling Boiler

The Babcock & Wilcox Type H Stirling Boiler is a highly efficient unit built for moderate pressures at moderate prices. . . . and is designed to occupy minimum floor space and head room for the heating surface required.

This boiler is built in four classes and 36 sizes ranging from 691 to 6225 sq ft of heating surface, and can be designed for operation with any fuel and every method of firing.

The moderate price is due only to the simplicity of design, efficient production methods and superior shop equipment.



Type H Stirling Boiler with Babcock & Wilcox Chain-Grate Stoker

ADVANTAGES OF THE BABCOCK & WILCOX TYPE H STIRLING BOILER:

Unusual steaming capacity for the floor space and head-room required.

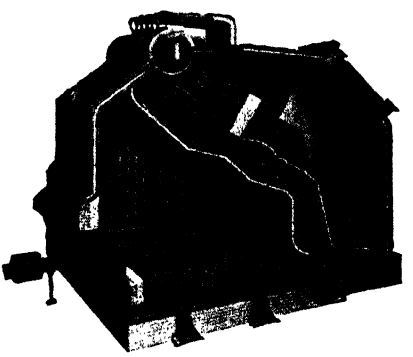
The choice of three locations for gas exit reduces cost of flues and breeching.

Distribution baffles make effective all of the heating surface.

Tube renewal is facilitated by correct tube spacing, and a tube removal door.

The boiler is supported by a structural-steel framework entirely independent of the brickwork.

A complete table of sizes and dimensions will be sent upon request. Simply ask for Bulletin G-8-C.



B&W Integral-Furnace Boiler, Type FF

Many of the advantageous features incorporated in large B&W central-station boilers are now available for the first time in the B&W Integral-Furnace Boiler, Type FF, which is offered in sizes ranging from 1353 to 6506 sq ft heating surface.

DISTINGUISHING FEATURES INCLUDE:

A completely water-cooled furnace. The construction provides water cooling for front and rear (or bridge) walls, as well as side walls and roof.

A furnace arrangement in which the primary combustion zone is followed by an open pass, thus making use of a principle of combustion that was first developed and used successfully in the B&W Open-Pass Boiler for central stations. This design insures mixing of the gases while at high temperatures, thereby aiding efficient and smokeless combustion.

Cyclone Steam Separators, which provide dry steam at high boiler-water concentrations independently of normal variations in water level, and increase circulation by eliminating steam from the water.

These, with related features, result in a boiler that is outstanding for economy of fuel and maintenance and for ease of operation. Write for Bulletin G-34.

The Bigelow Company

105 River Street, **New Haven 3, Connecticut**

MANUFACTURERS OF

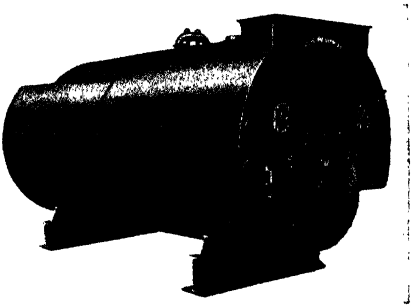
FIRE TUBE BOILERS **WATER TUBE BOILERS**

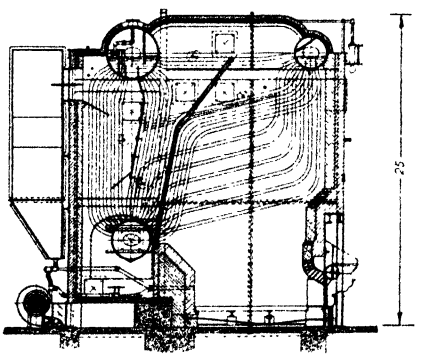
SALES REPRESENTATIVES IN PRINCIPAL CITIES

Catalog Furnished on Request

BIGELOW SCOTCH TYPE HEATING BOILER

A compact, self contained, highly efficient oil fired boiler that requires low head room and has low water line. All parts internally and externally are readily accessible. The boiler is of welded construction and contains no water leg or stay-bolted surfaces. Built in units with steam rating from 1,820 to 42,500 sq ft.



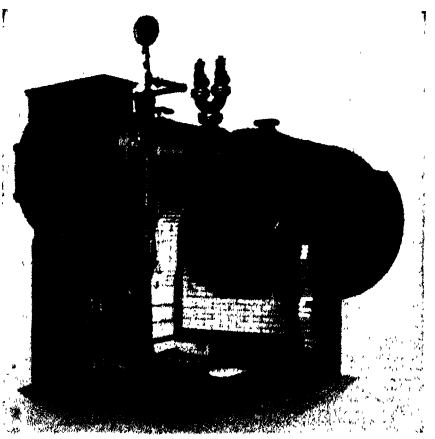


BIGELOW TYPE F WATER TUBE BOILER

Cut shows boiler equipped with spreader type stoker. The flexibility of design permits oil and other type stoker firing. Partial water wall surface is provided without extra headers, downcomers and circulating tubes. The Type F Steam Generating Unit is built in sizes ranging from 10,000 to 60,000 lb of steam per hour.

BIGELOW TWO-PASS BOILER

This boiler is designed to meet heating and power requirements, especially where space limitations prevail. The unit may be oil, stoker or hand fired. The elimination of special brick shapes and stay-bolts reduces the cost of maintenance to a minimum. The Two-Pass boiler is built in standard sizes from 25 hp to 250 hp.



The Brownell Company

ESTABLISHED 1855

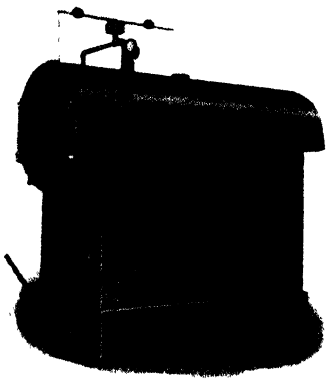
452 N. Findlay St.

Dayton 1, Ohio

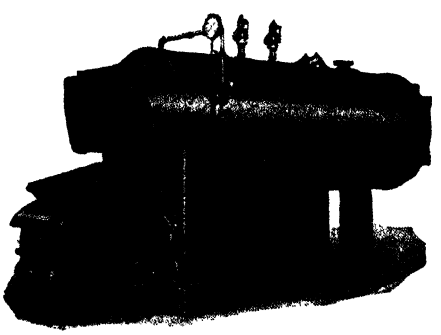
Manufacturers of

BROWNELL BOILERS, STOKERS, AND HEAT EXCHANGERS

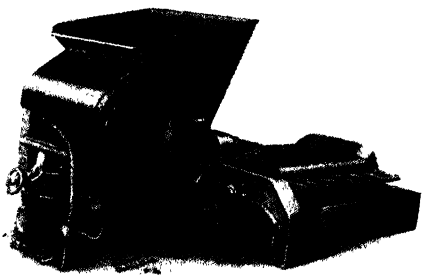
Representatives in All Principal Cities



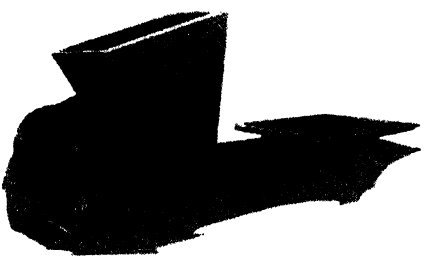
Welded Triple Pass Heating Boilers built in either high leg or low water line types. Hand fired ratings 500 to 35,500 sq ft steam, 800 to 56,800 sq ft water radiation. Stoker, Oil or Gas fired up to 43,100 sq ft steam or 69,000 sq ft water radiation. *A.S.M.E.* Code construction.



High or Low Pressure Double Pass Boiler with Type LR Stoker. Designed and manufactured as a matched unit steam generating plant. Furnished in working pressures from 15 to 150 lb and sizes up to 300 hp. For power, heating, and process steam. Steam ratings 3,600 to 42,500 sq ft. Water rating, 5,800 to 68,000 sq ft when used with stoker, oil, or gas. *A.S.M.E.* Code construction.



Type LR (Low Set) Underfeed Ram Type Stoker. Ideal where height of setting is limited. Sizes to 300 hp; "R" models up to 700 hp. Automatic air volume control. Can be furnished with Brownell exclusive, fully automatic intermittent coal feed control.



Type C Screw Feed Stoker, proved by years of service to be sturdy, reliable and efficient. Illustration shows dead plates; can also be furnished with dump plates in the larger sizes. 30-300 hp.

Heat Exchangers, Generators, Converters. Hourly capacities from 60 to 4,400 gal; storage capacities 25 to 1,904 gal.

The illustrations show only a part of the complete Brownell line. We shall gladly send literature describing Brownell equipment. Our field organization is ready to assist in problems of steam generation and heating.

Combustion Engineering Company, Inc.

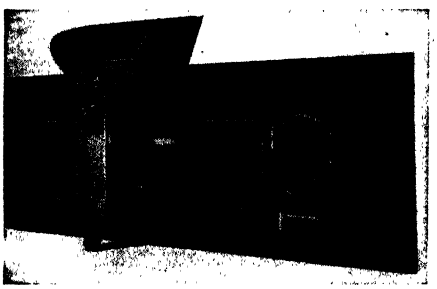
All Types of Fire Tube and Water Tube Boilers
Mechanical Stokers

Complete Steam Generating Units
Pulverized Fuel Systems

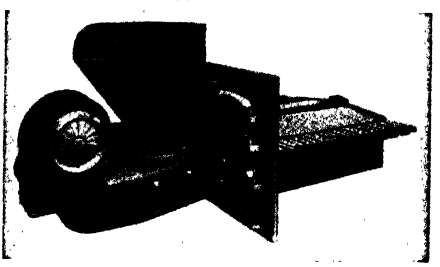
200 Madison Avenue, **New York 16, N. Y.**
Offices in all principal cities of the United States and Canada

More than 19,500 C-E Stokers purchased to date

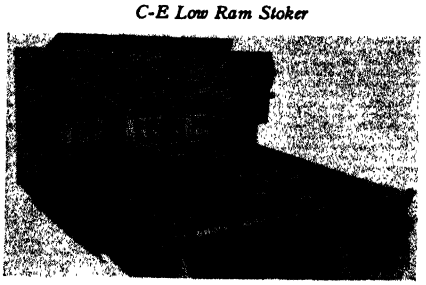
C-E Skelly Stoker



Type E Stoker



C-E Low Ram Stoker



C-E Spreader Stoker

C-E Skelly Stoker—A compact, self-contained unit with integral forced-draft fan, adapted to burn either anthracite or bituminous coal. Alternate fixed and moving grate bars assure lateral distribution of fuel Automatic control is standard equipment. Approximate application range—20 to 200 rated boiler hp.

Type E Stoker—A single-retort, underfeed stoker with an established reputation of many years' standing for dependable service. Designed to burn a variety of bituminous coals under boilers up to about 600 rated hp. Available with steam, mechanical or electro-hydraulic drive.

C-E Low Ram Stoker—A single-retort, stationary-grate underfeed stoker for burning bituminous coals under boilers in the upper size range of the C-E Skelly Stoker.

C-E Spreader Stoker—A simple, rugged overfeed stoker designed to burn a wide variety of coals. Fines are burned in suspension and the coarser coal on a grate which may be of either stationary, dumping or continuous discharge type. Rate of coal feed and air supply may be regulated over a wide range and are readily adaptable to automatic control. Applicable to boilers from about 100 boiler hp up.

C-E Multiple Retort Stoker—For burning bituminous and semi-bituminous coals under boilers up to the largest sizes.

C-E Traveling Grate and Chain Grate Stokers—Including both Coxe and Green types. Available with grate surfaces suitable for anthracite, coke breeze, lignite or bituminous coal, as required. Traveling grates are all forced-draft types; chain grates are either forced draft or natural draft types.

C-E Boilers—All fire tube and water tube types in sizes ranging from 25 hp up to the largest. Standard and special designs to suit all conditions of fuel, load and space. Included are all types formerly known by the trade names "Heine," "Walsh & Weidner," "Casey-Hedges," "Ladd" and "Nuway."

Separate Catalogs describing each of these products are available. A-331-E

Farrar & Trefts

Incorporated

ESTABLISHED 1863

20 Milburn Street, **Buffalo 12, N. Y.**

FARRAR & TREFTS SALES OFFICES

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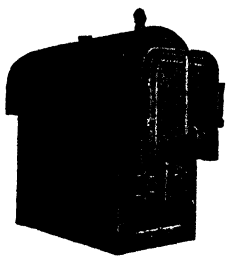
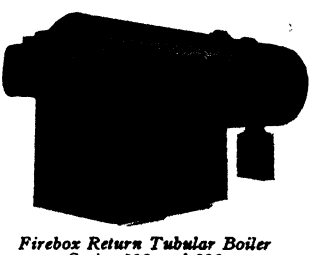


The Bison Compact Boiler Series 100 and 900

The F&T Bison Compact Welded Heating Boiler is more than just another boiler. It has been designed carefully so as to have a large furnace volume, the proper volume of water, just the right amount of steam liberating surface, the correct volume for steam storage and a balanced circulation. The result is a remarkably steady water line—**A Balanced Boiler.**

This boiler requires a minimum amount of floor space and is easy and inexpensive to install. It is reasonable as to first cost and economical in operation. Construction is in accordance with the *A.S.M.E.* Code for 15 lb working pressure and boilers are designed for hand firing with anthracite or bituminous coal or for mechanical firing with oil, gas or stoker. There are various sizes available from 1,800 to 35,000 sq ft of steam radiation, all ratings as required by the *Steel Heating Boiler Institute.*

The Bisonette Compact Boiler has the same characteristics as the larger Bison Compact Boiler. It has been designed for installation in large residences and small business establishments where the advantages inherent in a Steel boiler are desired.



Firebox Return Tubular Boiler Series 500 and 600

Firebox Return Tubular Heating Boilers are **Quality Boilers.** They are constructed to measure up to the high standards set by Heating Engineers and will give unfailing service under all conditions. Being economical to install and operate, they are highly favored by Architects and Engineers for heating Schools, Hospitals, etc.

There are two types of Firebox Boilers, the Up-Draft Type and the Down-Draft Type. Both types are made of welded or riveted construction for heating purposes at 15 lb working pressure and riveted, or, Class 1 fusion welded x-rayed and stress-relieved for power purposes at 100, 125 and 150 lb working pressure in accordance with the *A.S.M.E.* Code. Sizes from 4.500 to 35,000 sq ft of steam radiation, as rated by the *Steel Heating Boiler Institute,* are designed for hand firing with coal or for mechanical firing with oil, gas or stoker.

Scotch Wet Top Back Boilers are designed so that no refractory tile are required at the top of the rear combustion chamber. The steam space extends the entire length of the boiler and the furnace is entirely surrounded by water which permits immediate maximum heat transfer and absorption. This special design results in a boiler that is extremely efficient to operate and is maintained at a minimum cost.

The Scotch Wet Top Back Boiler is a self-contained unit. It can be moved easily and can be installed on two saddles. No expensive foundation or pit is required. No external brickwork is needed. Because of its short length, low height and low water line, this compact boiler unit can be installed in small spaces where there is lack of headroom and where no other type will fit.

Designed for oil, gas or mechanical firing, in accordance with the requirements of the *A.S.M.E.* Code for 15 lb working pressure, ratings of these boilers conform to *S.B.I.* Sizes range from 5160 to 42500 sq ft of steam radiation.

"Catalogs on Request"

Fitzgibbons Boiler Company, Inc.

Established 1886

General Offices: Architects Bldg., 101 Park Avenue

New York 17, N. Y.

Manufactured at: OSWEGO, N. Y.

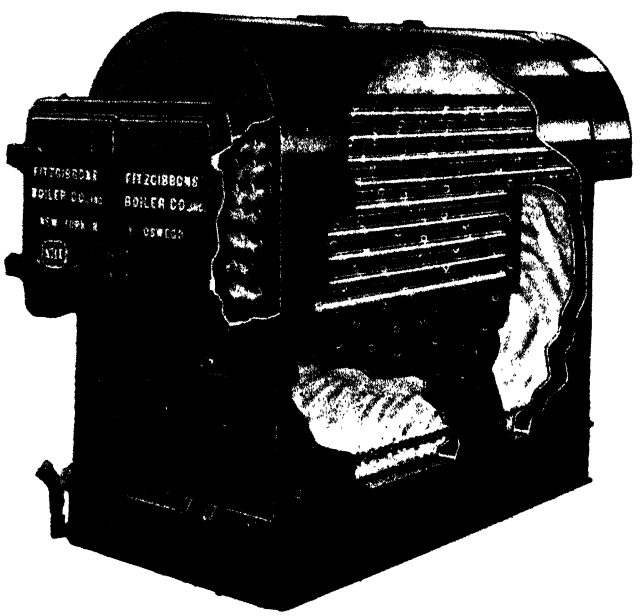
Sales Branches in Principal Cities

Member, Steel Boiler Institute

Member

Reg. U.S. Pat. Off.

PRODUCTS—STEEL HEATING and POWER BOILERS for all fuels and all heating systems. Capacities to meet requirements of any building. Built and rated according to *A.S.M.E.* and *S.B.I.* Codes.—AIR CONDITIONERS for Direct-Fired installations in residences of all sizes.



FITZGIBBONS

"D" TYPE

Welded Steel

Firebox Boilers

For 15 lb W.S.P.

***A.S.M.E.* Built**

***S.B.I.* Rated**

Hartford Inspected

The boiler for apartments, office buildings, theatres, schools, hospitals—capacities from 1800 to 42,500 sq ft steam EDR.

Full and complete combustion is a feature of the Fitzgibbons "D" Type steel boiler. In the oil or gas fired type, the generous combustion area insures the liberation of every Btu.

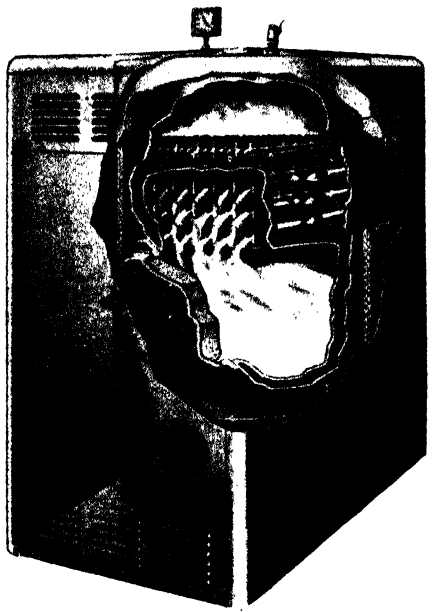
In the coal burning type, grate apertures and secondary air intake are correct for admitting the right amount of air. Flue gases make several passes over the length of the boiler.

Positive water circulation—a rapid continuous surging sweep induced by the concentration of heat at the crown sheet. This powerful circulation is further helped by the absence of convolutions or distorted forms which might impede it.

Ample domestic hot water is provided with no storage tank by the Fitzgibbons "Tanksaver."* Where a storage tank is used, the "Tankheater" may be furnished.

Hand-fired, Coal Type—1800 to 35,000 sq ft steam Oil, Gas, Stoker—2190 to 42,500 sq ft steam 18 sizes.

*Reg. U.S. Pat. Off.



FITZGIBBONS 400 SERIES
***A.S.M.E.* Built—*S.B.I.* Rated**
Hartford Inspected.
5 Sizes—320 to 900 sq ft steam net radiation load.

FITZGIBBONS "400" SERIES

the Steel Boiler for residences

A boiler that brings to the home every advantage of Fitzgibbons steel boiler construction. Electrically welded in a one-piece unit, it combines strength and durability with leak-proof, crack-proof construction.

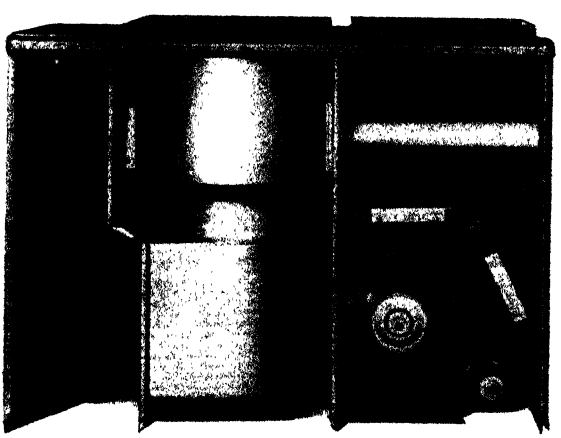
The 400 Series is a particularly quick heating boiler, giving immediate response to thermostat control. This reduces the periods of burner operation and is the reason for outstanding fuel savings and comfortable temperature uniformity enjoyed by the thousands of 400 Series heated homes. Abundant domestic hot water for kitchen, laundry and baths is provided by the Fitzgibbons Tanksaver* summer and winter, with no storage tank required.

This boiler is available in types for all mechanical firing methods, and for hand firing with coal, the latter type supplied with complete grate equipment.

*Reg. U.S. Pat. Off.

FITZGIBBONS "DIRECTAIRE"*

The winter air conditioner for residential comfort



FITZGIBBONS "DIRECTAIRE"
6 Sizes—65,000 to 200,000 Btu/hr.

With a notable degree of economy in fuel, Directaire winter air conditioner tempers the air in response to thermostatic action, humidifies the air automatically to the degree correct for comfort, cleans the air of dirt, dust and foreign matter, and circulates the air quietly, and without drafts. The Directaire is notable for fuel economy, due to the Fitzgibbons "Contra Flo" principle, in which the passage of air through the unit is opposed to the flow of combustion gases. A further advantage is the variable pitch pulley which increases blower capacity, for summer circulation of cool basement air.

Fitzgibbons "Weld-Seal" crack-proof construction, prevents all chance of combustion gas leakage into the air stream. Installation is quick and easy.

*Reg. U.S. Pat. Off.

Won for the 5th time

KEWANEE BOILER CORPORATION

Division of AMERICAN RADIATOR & Standard Sanitary CORPORATION

Kewanee, Illinois

BRANCHES IN 64 PRINCIPAL CITIES

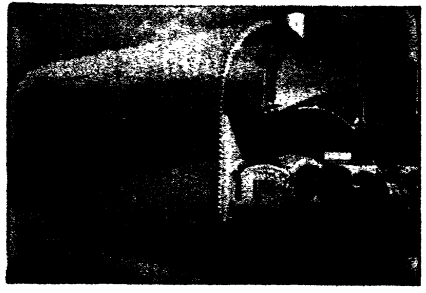
SBI Reg U S Pat Off MEMBER

Steel Heating and Power Boilers, Water Heating Garbage Burners, Tabasco Heaters and Tanks

KEWANEE STEEL HEATING BOILERS

Kewanee offers a dependable line of Steel Boilers built for heating every size building with high efficiency burning any kind of fuel. Standard sizes and types of Kewanee Boilers are kept in stock ordinarily for immediate delivery.

Almost eighty years of intensive study and effort are back of Kewanee Boiler designs. They are all constructed in our extensively equipped factory at Kewanee, Illinois, in conformity with these Codes: American Society of Mechanical Engineers for construction, and for rating with the Steel Boiler Institute Simplified Practice. The Kewanee series include:

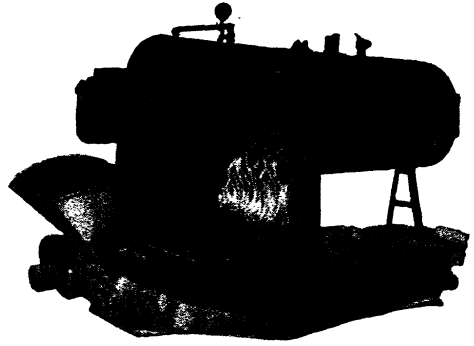


Firebox Boiler Portable Up-draft Type "400" and "500" Series, Hi-Pressure

HEAVY DUTY RIVETED FIREBOX TYPES: 1,380 ft to 42,500 ft. 10 to 304 Horsepower. Steam Working Pressures 100, 125 and 150 lbs. Single-pass tubes for rear smoke outlet; Two-pass tubes for front smoke outlet.

WELDED BOILERS: 2,200 ft to 42,500 ft. Direct Draft Type "C" with Corrugated Crown Sheet, rear Smoke outlet, and welded firebox two-pass for front Smoke outlet.

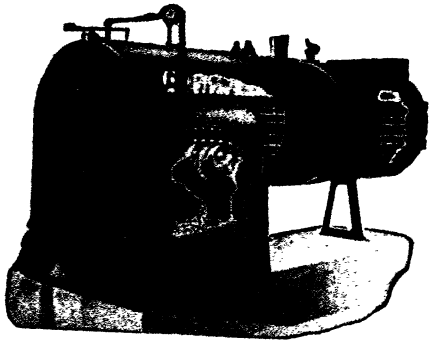
RESIDENCE STEEL BOLIERS: 225 ft to 3,000 ft. Square and Round Type "R" with and without Jackets and Hot Water Heating Coils for Storage Tank or Instantaneous flow.



Firebox Boiler for Oil, Gas or Stoker "500" Series

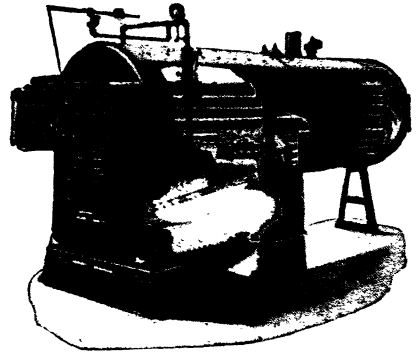
SPECIFICATIONS—PORTABLE UP-DRAFT BOILER

Boiler No.	576	577	578	579	580 480 1	581 481	582 482	583 483	584 484	585 485	586 486	587 487	588 488	589 489	590 490
SBI Rating Steam, Coal ..... Sq Ft	3500	4000	4500	5000	6000	7000	8500	10000	12500	15000	17500	20000	25000	30000	35000
Horsepower ..... Hp	25	29	32	36	43	50	61	72	89	107	125	143	179	214	250
SBI Rating Oil, Gas, Stoker ..... Sq Ft	4250	4860	5470	6080	7290	8500	10330	12150	15180	18220	21250	24290	30360	36430	42500
Horsepower ..... Hp	30	35	39	44	52	61	74	87	109	130	152	174	217	261	304
Width and Length ..... In. x Ft In.	42x8-7	42x9-6½	48x8-11½	48x9-8	54x9-2½	54x10-6	60x11-1	60x12-9	66x12-10	66x14-9	72x14-9	78x14-9	78x17-7½	84x17-9½	84x20-0½
Overall Height Shell ..... In.	80½	80½	86½	86½	94½	94½	102	102	108	108	114	116	116	126	126
Height of Water Line ..... In.	73	73	76	76	83	83	88	88	93	93	97½	100	100	108	108
Shipping Weight Coal ..... 125 Lb	8500	9000	10500	11000	12500	14000	16000	18000	20500	23500	26000	29000	33500	37500	41500
Oil, Gas or Stoker ..... 125 Lb	7980	8510	9590	10100	11700	12760	14930	16530	19230	21940	24100	26840	31210	35000	38820



Type "K" Up-draft Boiler for Hi-Pressure

Smokeless Boiler Portable Down-draft Type "300" Series for Hi-Pressure

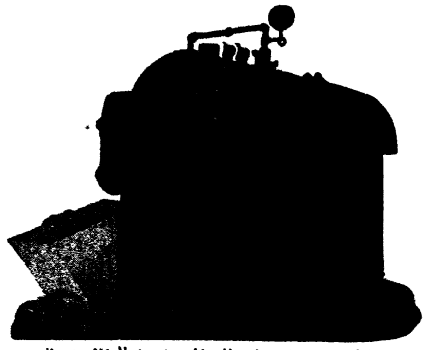


SPECIFICATIONS—TYPE "K" PORTABLE UP-DRAFT BOILER

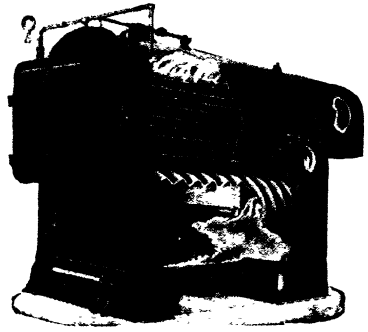
Boiler No.	4K	5K	6K	8K	9K	10K	11K	12K
SBI Rating Steam, Coal ..... Sq Ft	1380	1800	2200	3000	3500	4000	4500	5000
Horsepower ..... Hp	10	13	16	22	25	29	32	36
SBI Rating Oil, Gas, Stoker ..... Sq Ft	2020	2190	2680	3650	4250	4860	5470	6080
Horsepower ..... Hp	14	16	19	26	30	35	39	44
Width and Length ..... In. x Ft In.	36x8-10	36x10-4	36x11-10	42x11-4	42x12-10	48x11-10½	48x13-4½	48x14-10½
Overall Height Shell ..... In.	65½	65½	65½	71½	71½	77½	77½	77½
Height of Water Line ..... In.	57	57	57	60½	60½	63	63	63
Shipping Weight Coal ..... 125 Lb	4800	5000	6500	7500	8500	9000	10500	11000
Oil, Gas or Stoker ..... 125 Lb	4440	4710	5820	6880	7980	8510	9590	10100

SPECIFICATIONS—SMOKELESS DOWN-DRAFT BOILER

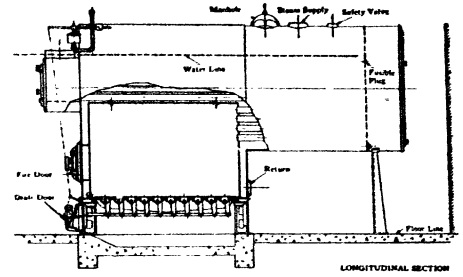
Boiler No.	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390
SBI Rating Steam, Coal ..... Sq Ft	3500	4000	4500	5000	6000	7000	8500	10000	12500	15000	17500	20000	25000	30000	35000
Horsepower ..... Hp	25	29	32	36	43	50	61	72	89	107	125	143	179	214	250
SBI Rating Oil, Gas, Stoker ..... Sq Ft	4250	4860	5470	6080	7290	8500	10330	12150	15180	18220	21250	24290	30360	36430	42500
Horsepower ..... Hp	30	35	39	44	52	61	74	87	109	130	152	174	217	261	304
Width and Length ..... In. x Ft In.	42x8-3	42x9-3	48x8-9	48x9-6½	54x9-4	54x12-11	60x12-8½	60x14-9	66x14-11	66x17-4	72x16-5	78x17-0½	78x20-7½	84x19-11	84x22-8
Overall Height Shell ..... In.	80½	80½	86½	86½	94½	94½	102	102	108	108	114	116	116	126	126
Height of Water Line ..... In.	73	73	76	76	83	81	88	88	92½	92½	98	98½	98½	110	110
Shipping Weight Coal ..... 125 Lb	8000	9000	10000	10500	12000	15000	17500	19500	23000	26500	29500	32000	38500	44500	49500
Oil, Gas or Stoker ..... 125 Lb	7400	8510	9010	9520	11130	13910	16080	18260	21530	24820	27550	30290	36380	41900	46870



Type "C" Boiler Hi-Firebox Series 7L70 for Oil, Gas or Stoker



Type "C" (cut-away View) 27L70 for Hand-fired Coal



"5000" Series Diagram
Welded Firebox Boilers Updraft 5176-5190 Mechanical rating same dimension as 5076-5090 Hand-fired. Smokeless Downdraft 6177-6190 Mechanical rating same dimensions as 6077-6090 Hand-fired.

SPECIFICATIONS—TYPE "C" HI-FIREBOX WELDED BOILERS — 7L70 Series & 27L70 Series

Boiler No. Oil, Gas, Stoker	7L73	7L74	7L75	7L76	7L77	7L78	7L79	7L80	7L81	7L82	7L83	7L84	7L85	7L86	7L87	7L88	7L89	7L90
SBI Rating Steam..Sq Ft	2680	3160	3650	4250	4860	5470	6080	7290	8500	10330	12150	15180	18220	21250	24290	30360	36430	42500
SBI Net Rating....Sq Ft	2200	2600	3000	3500	4000	4500	5000	6000	7000	8500	10000	12500	15000	17500	20000	25000	30000	35000
Width x Lgth., In. x Ft In.	36x5-10½	36x6-4½	36x6-10½	36x7-9	42x7-10½	42x8-6½	42x9-2	48x9-4½	48x10-7	54x9-11	54x11-2½	60x11-6½	66x12-3½	72x12-1½	72x13-4½	78x14-9½	84x14-2½	84x15-11½
Overall Height Shell...In.	84	84	84	84	88½	88½	88½	92½	92½	105½	105½	115½	120½	130½	130½	138	162½	162½
Height of Water Line..In.	75	75	75	75	76½	76½	76½	79½	79½	90	90	100½	103	113	113	119	141½	141½
Shipping Weight.....Lb	3100	3500	3900	4400	4900	5400	5800	6700	7600	8800	10000	11800	13600	15300	17000	20100	23200	26100
Boiler No. Hand-fired Coal	**27L73**	**27L74**	**27L75**	**27L76**	**27L77**	**27L78**	**27L79**	**27L80**	**27L81**	**27L82**	**27L83**	**27L84**	**27L85**	**27L86**	**27L87**	**27L88**	**27L89**	**27L90**
SBI Rating Steam..Sq Ft	2200	2600	3000	3500	4000	4500	5000	6000	7000	8500	10000	12500	15000	17500	20000	25000	30000	35000
SBI Net Rating....Sq Ft	1830	2170	2500	2920	3330	3750	4170	5000	5830	7080	8330	10420	12500	14580	16670	20830	25000	29170
Shipping Weight.....Lb	3600	4000	4500	5100	5600	6200	6700	7800	8800	10200	11500	13600	15700	17600	19500	23200	26700	30200

SPECIFICATIONS—WELDED FIREBOX BOILER — "5000" Series & "6000" Series

Boiler No. Updraft	5076	5077	5078	5079	5080	5081	5082	5083	5084	5085	5086	5087	5088	5089	5090
SBI Rating Steam Coal.....Sq Ft	3500	4000	4500	5000	6000	7000	8500	10000	12500	15000	17500	20000	25000	30000	35000
SBI Net Rating.....Sq Ft	2920	3330	3750	4170	5000	5830	7080	8330	10420	12500	14580	16670	20830	25000	29170
SBI Rating Steam: Oil, Gas, Stoker.....Sq Ft	4250	4860	5470	6080	7290	8500	10330	12150	15180	18220	21250	24290	30360	36430	42500
SBI Net Rating.....Sq Ft	3500	4000	4500	5000	6000	7000	8500	10000	12500	15000	17500	20000	25000	30000	35000
Width x Length.....In. x Ft In.	42x7-3	42x8-0	42x8-11	42x9-10	48x9-9	48x11-1½	54x11-1	54x12-9	60x13-2½	60x15-3	66x14-5½	66x16-0½	72x16-8½	78x17-5½	78x19-8½
Overall Height.....In.	81	81	81	81	86½	86½	92½	92½	100½	100½	105	105	112	117	117
Height of Water Line.....In.	70	70	70	70	73½	73½	78	78	84	84	86	86	94½	96	96
Shipping Weight, Coal.....Lb	5100	5600	6100	6600	7500	8400	9600	10800	12600	14400	16100	17900	21200	24400	27500
Boiler No. Downdraft		**6077**	**6078**	**6079**	**6080**	**6081**	**6082**	**6083**	**6084**	**6085**	**6086**	**6087**	**6088**	**6089**	**6090**
Shipping Weight, Coal.....Lb		5800	6300	6800	7700	8600	9900	11200	13100	14900	16600	18300	21500	24500	27300

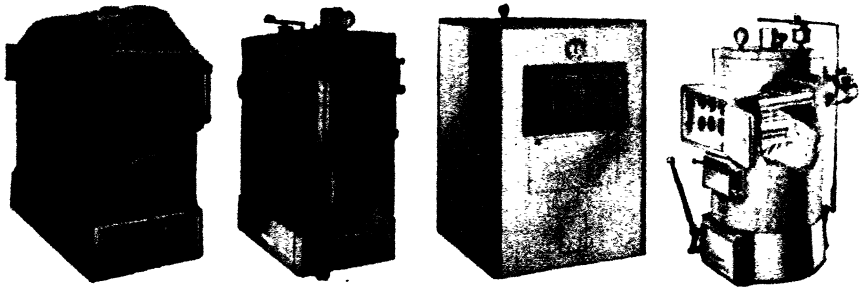
Rated Capacity for Water Boiler is 60 per cent greater than Capacity for Steam Boiler.

Table for two series of Boilers lists maximum dimensions only.

KEWANEE TYPE "R" RESIDENCE BOILERS

Kewanee Type "R" Boilers are especially designed and constructed to meet all heating and hot water requirements for homes and small buildings. Every kind of solid fuel, coke, all grades of hard or soft coals and their briquette or treated forms are burned with excellent results. Also, any liquid fuel, oil, and natural or commercial gas can be used with high efficiency.

Standard jackets will be available for Round "R" and Square "R" Boilers. Hot Water Copper Coil may be ordered for Round and Square "R" Boilers, 55 to 720 gallons capacity for storage tank operation, also 135 to 700 gallons instantaneous flow.



SPECIFICATIONS—RESIDENCE BOILERS SQUARE "R" ROUND TYPE "R"

Boiler No.	3R1	3R2	3R3	3R4	3R5	3R6	3R7	3R8	733	734	735	736	1737
Net Load Steam, Hand-fired..Sq Ft	740	910	1080	1230	1480	1810	2140	2480	225	330	450	570	.....
Water.....Sq Ft	1180	1450	1720	1970	2370	2890	3430	3970	360	530	720	910	.....
Btu per Hour.....1000's	178	218	261	295	355	434	514	595	54	79	108	137	.....
Net Load Steam, Mechanical.Sq Ft	900	1100	1300	1500	1800	2200	2600	3000	275	400	550	700	900
Water.....Sq Ft	1440	1760	2080	2400	2880	3520	4160	4800	440	640	880	1120	1440
Btu per Hour.....1000's	216	264	312	360	432	528	624	720	66	96	132	168	216
Heating Surface.....Sq Ft	53	65	77	88	106	129	153	177	16	24	32	41	53
Grate Area.....Sq Ft	4.2	4.9	5.7	6.3	7.2	8.4	9.4	10.5	1.6	2.2	2.9	3.7	.....
Furnace Volume.....Cu Ft	8.2	10.0	11.8	13.6	16.4	20.0	23.6	27.3	3.1	4.4	6.4	8.9	8.9
Width and Length.....In x In.	30x30½	30x36½	30x42½	30x48½	34x42½	34x50½	34x58	34x67	.....	.....	.....	.....	.....
Diameter Firebox Inside.....In.	.....	.....	.....	.....	.....	.....	.....	.....	17	20	23	26	26
Overall Height from Floor.....In.	65	65	65	65	72½	72½	72½	72½	54	54½	58	60½	61
Height of Water Line.....In.	55½	55½	55½	55½	62½	62½	62½	62½	46	44	47	49	49
Shipping Weight, Hand.....Lb	1775	1975	2175	2350	2600	2900	3200	3500	700	880	1040	1280	.....
Mech.....Lb	1500	1650	1800	1950	2250	2475	2725	3000	600	800	920	1130	1400
Outside Surface to Cover....Sq Ft	38	43	48	53	58	65	73	82	17	24	35	41	47

KEWANEE STORAGE WATER HEATERS

Kewanee Storage Heaters—use exhaust or live steam. 15 standard Coil Elements in 29 standard size storage tanks. Capacities 95 to 2240 gals per hr.

KEWANEE SCOTCH MARINE BOILERS

Kewanee Scottie Junior for High Pressure Steam in small industrial usage. 6 sizes 6 to 30 hp at 100 lbs steam pressure.

Kewanee Welded Scotch Marine, Low Pressure Steam. 11 sizes, 5470 to 30360 sq ft, mechanically fired.

KEWANEE HI-TEST BOILER

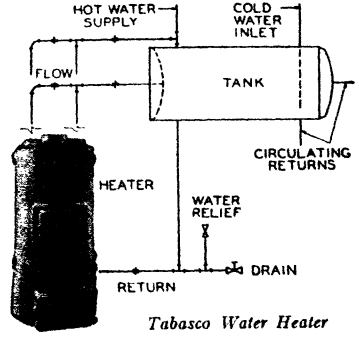
Kewanee Hi-Test Fusion Welded Series for High Pressure Steam in power or industrial process. 6 stock sizes, 50 to 150 hp, 125 and 150 lbs steam working pressure. All *A.S.M.E.* Code.

KEWANEE WATER HEATERS AND TANKS

All-Weld Water Heaters, Tabasco or Garbage Burning, 5 sizes to heat 165-700 gal 50 deg per hour. Extra Heavy W. P. 100 lb per sq in. 150 lb Test.

Water Heating Garbage Burner

Tanks 85 to 450 Gal



Tabasco Water Heater

The Titusville Iron Works Company

Division of Struthers Wells Corp.

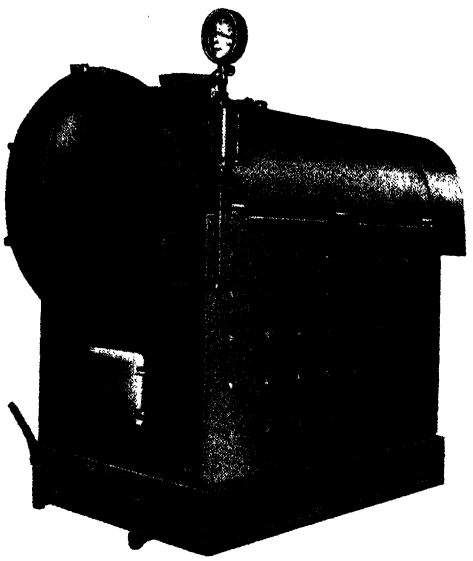
Titusville, Penna.

PLANTS AT TITUSVILLE, PA. and WARREN, PA.

Designers and Builders of Heating and Power Boilers for every purpose since 1860—Water Tube Boilers—Scotch Marine Boilers—Oil Country Units.

TITUSVILLE COMPACT STEEL HEATING BOILERS

19 sizes in Hand Fired, Mechanical Fired, using any type fuel. Constructed to *ASME* Code, Hartford Inspected *S.B.I.* rated.



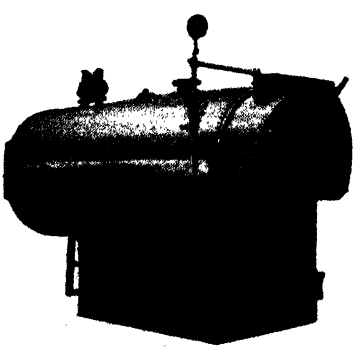
Working pressures — 15 lb Steam; 30 lb Hot Water. Extra large combustion chambers, two-piece construction, rear smoke box, full width flue doors—designed for new operating economy.

Hand Fired Coal, 1800 to 35,000 sq ft steam, 2880 to 56,000 sq ft Hot Water.

Mechanical fired 2190 to 42,500 sq ft Steam, 3500 to 68,000 sq ft Hot Water.

TITUSVILLE SERIES "R.P." PORTABLE FIREBOX BOILERS

13 sizes in Hand Fired, Mechanical Fired, using any type fuel Constructed to *ASME* Code, Hartford Inspected, *S.B.I.* rated.



An ideal "all around" boiler for high pressure steam generation. Two pass, 3 in. Firetubes, Front Smoke Outlet, 100, 125 lb working pressures.

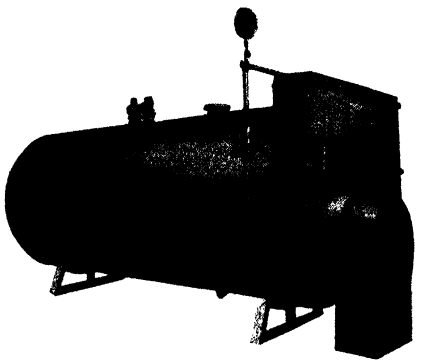
Hand Fired Coal 25 to 250 hp 3500 to 35,000 sq ft Steam Radiation.

Mechanical Fired 30 to 304 hp 4200 to 42,500 sq ft Steam Radiation.

The Titusville Iron Works Company

TITUSVILLE "SOH" LOW PRESSURE SCOTCH BOILERS

Mechanical Fired, Hand Fired, using any type fuel. Constructed to *ASME* Code. Hartford Inspected, *S.B.I.* rated.



Completely self contained, compact, low water line, low head room, no pit or brick base, 3 inch boiler tubes. Extra large steam volume and disengaging area.

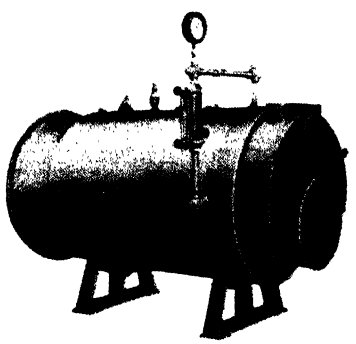
Hand Fired Coal 2366 to 33,950 sq ft Steam. 3786 to 54,320 sq ft Hot Water.

Stoker Fired Coal 3160 to 42,500 sq ft Steam. 5050 to 68,000 sq ft Hot Water.

Oil, Gas Fired 2190 to 42,500 sq ft Steam. 3510 to 68,000 sq ft Hot Water.

"WEE SCOTT" WELDED SCOTCH MARINE BOILERS

Mechanical Fired for Oil, Gas or Stoker. Constructed to *ASME* Code, Hartford Inspected, *S.B.I.* rated.

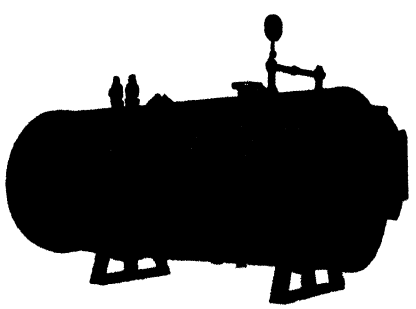


9.7 to 50 hp, 125 lb working pressure—due to extra large combustion volume and large flue areas—higher ratings than shown are available. Can be adapted to hand coal firing. Noted for economy, efficiency, easy installation, low maintenance costs.

Steam Rating 1650 to 8483 sq ft.

TITUSVILLE "SPO" HIGH PRESSURE SCOTCH MARINE BOILERS

Mechanical Fired, Hand Fired using any type fuel, constructed to *ASME* Code, Hartford Inspected *S.B.I.* rated.



All welded construction, working pressures 125 lb and 150 lb. Titusville Scotch Marine Boilers are the ultimate in economy and durability—the results of 86 years of progressive engineering and experience.

Hand Fired Coal 58 to 292 hp.

Mechanical Fired 60 to 300 hp.

The International Boiler Works Company

350 Birch St., **East Stroudsburg, Pa.**

SALES OFFICES IN PRINCIPAL CITIES

FOR years "Fuel-Saver" Boilers Type C have met the requirements for low cost heating in office and apartment buildings, hotels, schools, theatres, industrial plants, etc.

Their design and construction makes them especially suitable for modern heating requirements:

QUICK STEAMING

Due to rapid and positive internal water circulation.

MAXIMUM HEAT ABSORPTION

Due to effective distribution of heated gases.

EASE OF CLEANING

Due to accessibility of heating surfaces.

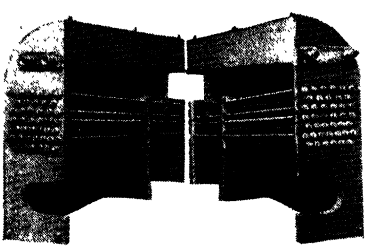
"FUEL-SAVER" Boilers have cut fuel costs in thousands of heating installations.

Complete range of standard sizes rated in accordance with *S.B.I.*-15 lb *A.S.M.E.* standard—for hand, stoker, oil or gas firing.

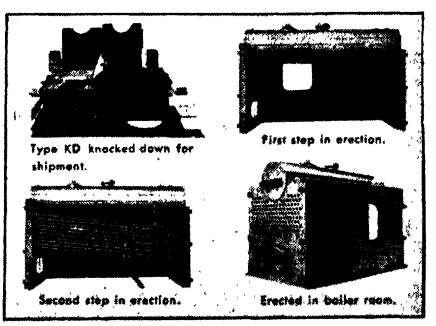
Type C twin section—a heating boiler in halves. For installation where Type C one piece cannot be carried through existing passages.

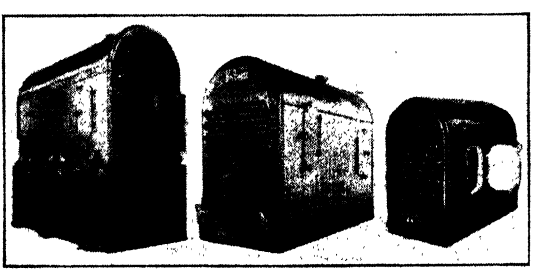
Type KD—knocked down—a heating boiler designed for shipment so that sections can be carried through a door or window. Eliminates expensive cutting or patching of building. Reduces time out when in need of steam.

Typical Type C Installation



Halves of twin section ready for bolting





Type CR water-tube power boiler for processing and power. 100-125-150 s.w.p. *A.S.M.E.* standard.

Complete range of sizes—10 to 300 hp for hand, stoker, oil or gas firing.

BOILER BUILDERS FOR 62 YEARS.

Write for bulletins

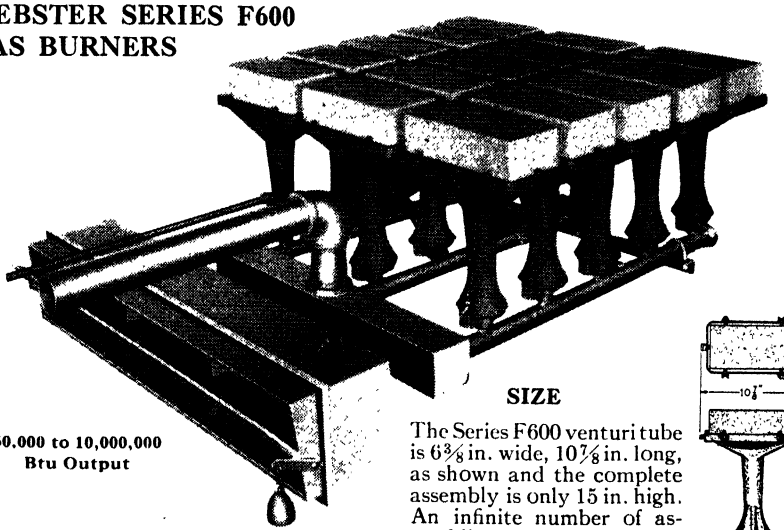
The Webster Engineering Co.

419 West 2nd St., **Tulsa, Oklahoma**

Division of

SURFACE COMBUSTION CORPORATION, TOLEDO, OHIO

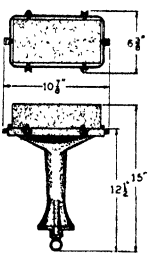
WEBSTER SERIES F600 GAS BURNERS



50,000 to 10,000,000 Btu Output

SIZE

The Series F600 venturi tube is 6⅜ in. wide, 10⅞ in. long, as shown and the complete assembly is only 15 in. high. An infinite number of assemblies are possible by proper arrangement of the individual tubes. For complete sizing information write for bulletin.



For Use in Any Steel Firebox or Sectional Boiler

Improved venturi and greater port area insure much higher capacities at lower pressures.

Unique baffles at the outlet of the mixing tube make possible perfectly even distribution of flame completely around the baffle brick. As a result the maximum flame length is greatly reduced.

Interchangeable grills with multiple ports can be varied to suit the combustion characteristics of various gases. The proper sizing of these grills prevents any possibility of flash back.

In addition to the above major improvements the F600 possesses the same desirable features that made the 600 so popular.

1. Simple installation requiring no expensive insulated combustion chamber and having no furnace radiation loss.
2. Extreme quietness due to low rate of combustion over a large area.
3. Flexibility from infinite number of possible combinations varying both size and shape to meet load and firebox conditions at various gas pressures.
4. High radiant transmission rate due to radiant temperature of the standard firebrick baffles on the top of the burner tubes.
5. Low draft loss because of ample secondary air openings.
6. Plain gas pilots of heat resistant material and of a design that will not allow flame to pull off.
7. Safety pilot applied in a cool zone in a manner that insures perfect direct ignition of the burner yet allowing the the thermal element to cool quickly upon flame failure.
8. Guaranteed vibrationless under all conditions.

CAPACITY OF SINGLE F600 VENTURI TUBE—No. 17 MTD ORIFICE

Manifold Gas Pressure	2.0" W.C.	3.0" W.C.	4.0" W.C.	5.0" W.C.	6.0" W.C.	4 oz.	6 oz.	8 oz.
Input—Cu Ft, 1 hr.	58.0	72.0	84.0	94.5	104.0	112.0	138.0	159.5
Output—Sq Ft, St. Rad	178	222	258	289	318	343	423	488
Output—Boiler H.P.	1.28	1.59	1.85	2.07	2.28	2.46	3.04	3.4

Iron Fireman Manufacturing Company

Automatic Firing Equipment for Coal, Oil, Gas

Portland, Oregon **Cleveland, Ohio**

Address inquiries to 3166 West 106 St., Cleveland 11, Ohio

Retail Branches or Subsidiaries: CHICAGO, ILL.; MILWAUKEE, WIS.; ST. LOUIS, MO.; NEW YORK, N. Y.; BROOKLYN, N. Y.; TORONTO, CANADA

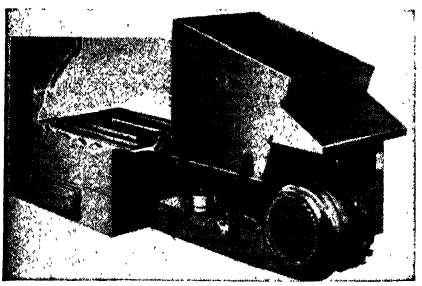
Dealers in Principal Cities and Towns in the United States and Canada

Representation in numerous foreign countries

COMMERCIAL AND INDUSTRIAL STOKERS

STANDARD HOPPER MODELS

This series of stokers is the standard of value in equipment for automatically firing boilers ranging in size up to 350 hp. Available in a wide range of coal feeding capacities, lengths and grate arrangements, to fit varied requirements.



Commercial Installation—Hopper Model

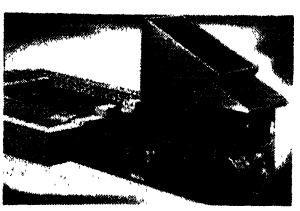
Hopper Model Iron Fireman in Operation in Horizontal Return Tubular Boiler

STANDARD COAL-FLOW MODELS

Commercial-Industrial Installation Coal-Flow model that carries coal direct from main bin or bunker to fire

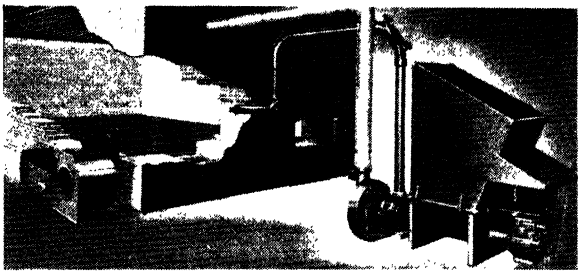
A heavy duty stoker which combines Iron Fireman's well known firing efficiency with the automatic conveying of coal direct from bunker to fire. An integral coal conveying mechanism eliminates the labor and expense of manual coal handling. The IRON FIREMAN COMMERCIAL-INDUSTRIAL COAL-FLOW stoker fires boilers developing up to 350 horsepower. PNEUMATIC SPREADER STOKERS also available in Coal-Flow models.

POWERAM STOKERS



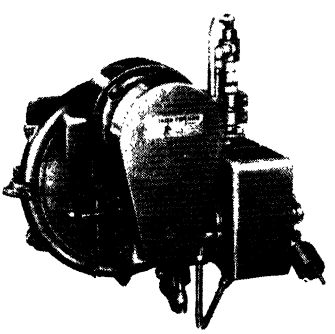
Combines ram-type coal distributor system in retort with free-running worm conveyor from coal supply, and has these advantages: Delivers the fuel to the fire bed in a loose, easily aerated condition; the reciprocating pusher blocks insure proper fuel distribution, and make possible the successful and efficient burning of many types of coal which otherwise are impractical to fire automatically with underfeed stokers. Designed for boilers developing up to 400 hp.

PNEUMATIC SPREADER STOKERS



As shown in the illustration above, the IRON FIREMAN PNEUMATIC SPREADER STOKER meters steam size coal from hopper or main coal bunker to transfer housing, where coal is picked up by pneumatic conveyer and delivered to furnace. The conveyor nozzle accurately spreads the larger particles of coal over the entire grate in a shallow, uniform fuel bed. The preheated fines burn in suspension, reducing the cinder carry-over and greatly improving the combustion efficiency and responsiveness, as compared with other stokers which do not preheat fuel. The conveying air provides the overfire air which is essential for efficient combustion. Entering at right angles to the flow of burning gases from the fuel bed, the conveying air produces *maximum turbulence; another requisite of efficient and smokeless combustion.* THE IRON FIREMAN PNEUMATIC SPREADER STOKER was designed to burn efficiently such economical fuels as the lower rank bituminous, and sub-bituminous coals and also lignite. It provides reliability of operation, physical adaptability, ease of operation, and low maintenance which is not afforded by other types of automatic coal burning systems. Pneumatic Spreader stokers are particularly adaptable to operation at high ratings, and as a result are greatly stepping up steam output in many plants throughout the United States and Canada. IRON FIREMAN PNEUMATIC SPREADER STOKERS are made in both hopper and Coal-Flow models; the latter carry coal direct from the bunker to the fire. Available in capacities up to 1000 hp per nozzle. Multiple units for larger boilers.

INDUSTRIAL OIL BURNER



Oil Volumeter accurately regulates oil regardless of its temperature or viscosity

This industrial oil burner brings new precision and dependability to the firing of high viscosity oils. Accurate adjustment of the fuel feed rate, eliminating pulsating fires and difficult "cold boiler room" starting, is achieved by a principle of multiple-piston feeding. This positive feed control produces a steady flame even when burner is throttled down to low capacity. Any fuel oil, from the lightest to the heaviest, will operate without need for special adjustments. Models available for manual, semi-automatic, or fully automatic operation. Control combinations can be provided to meet individual requirements. Available in capacities from 8 to 125 gph., to develop up to 425 hp.

RESIDENTIAL STOKERS, OIL AND GAS BURNERS—OIL AND COAL SELF-FIRING DOMESTIC BOILERS AND FURNACES—RESIDENTIAL GAS FURNACES.

Write for new general Catalog No. 1396, illustrating and describing the complete line of Iron Fireman automatic heating equipment for industrial, commercial and domestic use.

Aldrich Company

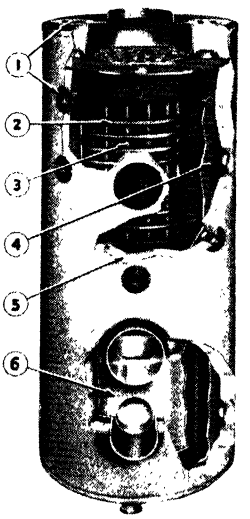
121 E. Williams St., **Wyoming, Illinois**

Boiler-Burners, Domestic and Commercial Oil Burners

BOILER-BURNER UNITS

Sizes—Specifications—Dimensions

Size of Boiler-Burner	100	150	250	400	642	700
Rating—Sq Ft Hot Water EDR	750	1000	1500	2100	3300	5000
Rating—Sq Ft Hot Water Standing	500	650	1000	1400	2200	3333
Rating—Sq Ft Steam EDR	500	630	935	1275	2025	3000
Rating—Sq Ft Steam Standing	333	420	620	850	1350	2000
Rating—BTU per hour (Max.)	118000	160000	224800	315000	514000	808500
Water Heater Delivery—GPH @ 100° Rise	125	190	280	475	610	850
Storage Capacity—gallons	26.5	38	53.5	82	116	140
Firing Rate GPH—Maximum	1.3	1.7	2.7	3.6	5.7	9.0
Firing Rate GPH—Minimum	.9	1.2	1.7	2.4	3.7	6.0
Firing Rate GPH—Best	1.2	1.35	2.0	2.5	4.5	7.5
Model Aldrich Burner furnished	AX-1	AX-2	AX-3	AX-3	BX	BX
Sq Ft of Heating Surfaces	20.6	26.6	42.5	69	96	145
Outside Diameter	20″	23″	26″	29½″	34½″	41″
Height from Floor	50″	54″	62″	70″	70″	72″
Smoke Pipe Diameter	7″	8″	8″	9″	10″	12″
Riser and Return Size—NPT (2 ea.)	2″	2″	2½″	2½″	3″	3″
Shipping Weight lbs—Boiler only	575	770	1080	1500	2400	2500
Shipping Weight lbs—Burner only	85	85	85	85	140	140
Shipping Weight lbs—Total	660	855	1165	1585	2540	2640



Aldrich Boiler-Burner Units—available in a range of 6 sizes for Hot Water Heating, Steam Heating, and Hot Water Supply—are designed for home, apartment, garage, club, restaurant, hotel, and factory installations. Gages, covers, and trim are furnished to suit model and type of unit ordered. Coils are factory-installed and tested in WC and SC models. Matched Aldrich Oil Burner furnished with each unit. Standard equipment includes full set of basic automatic controls.

Models Available

W—Water Boiler (universal tapping)

WC—Water Boiler (with coil)

S—Steam Boiler (universal tapping)

SC—Steam Boiler (with coil)

HSG—Hot Water Heater (galvanized, with dress jacket)

Models W, S, and HSG available in all sizes.

Models WC and SC come in 100, 150, 250, and 400 sizes only.

1. *Universal tapping on all models provides openings for necessary gages, valves, controls, 2 risers, 2 returns.*
2. *Built-in tankless heater is copper tube coil in WC or SC models. It provides adequate supply of hot water; no external storage tank or indirect heater is needed.*
3. *Correctly proportioned, seamless, steel fire tubes are easily cleaned; spirals inserted within tubes increase heating efficiency.*
4. *Main shell is heavy steel, welded to top and bottom plates. Entire assembly is tested under 150 lbs hydrostatic pressure.*
5. *A 2 in. thick blanket of rock wool insulation, between main shell and outer jacket, minimizes heat loss and reduces running time of burner.*
6. *Welded steel fire box is surrounded by water leg for high efficiency. Cast refractory lining has high resistance to chipping or deterioration.*

ALDRICH OIL BURNERS

Capacities from .75 gph to 19 gph

Models AX-BX-JU

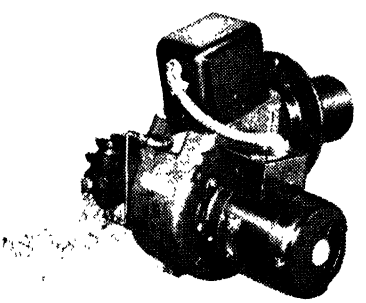
Aldrich Oil Burners are designed for domestic or commercial installations on warm air, steam, or hot water systems. Capacities range from .75 to 19 gph in 3 sizes and 5 models. Model AX (illustrated) has interchangeable draft tube assemblies and air cones, thereby permitting quick change through 3 firing ranges. Capacities: AX-1, 0.75 to 1.35 gph; AX-2, 1.35 to 2 gph; AX-3, 2 to 5 gph. Model BX, for large homes or apartments, comes with two-stage pump and firing range of 4 to 9 gph. Model JU, a heavy-duty burner for commercial and industrial use, has a capacity of from 5 to 19 gph. It is equipped with a ¾ hp motor, duplex nozzles and ignition, a two-stage pump. All models feature a well-designed fan housing, steel draft tubes, large inspection openings. Aldrich Oil Burners and Boilers are U. L. approved.

Automatic Burner Corp.

1823 CARROLL AVE.
Chicago 12, Ill.

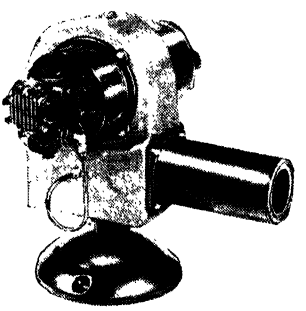
THE TRADE MARK OF QUALITY OIL BURNERS FOR 26 YEARS

PRESSURE TYPE OIL BURNER
Model 51



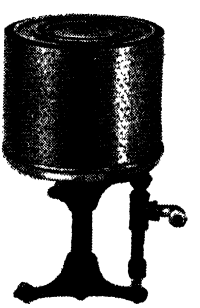
Here is the burner which meets every demand of the complete range of domestic heating needs. It combines beauty of design: excellence of engineering; precision production, to deliver guaranteed performance. The Model 51 mounts directly to the boiler by means of a flange, accurately machined for precise fit. Its 1/8th horse power motor insures trouble-free, amazingly quiet operation. It is attractively finished in the non-rusting, wear-resistant beauty of Hammerloid. Available in standard and odd cycles and voltages.

PRESSURE TYPE OIL BURNER
Model 52



The gun type oil burner has the famous ABC Oilairator mechanism that atomizes the fuel, mixes it with air, and delivers it with correct twist and velocity to insure complete combustion. The ABC nozzle combined with the proper choke and turbulator guarantees precise control and flexibility . . . guarantees a thoroughly satisfactory economical home heating unit. Capacity 0.6 to 6.0 gallons per hour.

RANGE BURNER



This ABC oil burner offers the advantages of all-steel construction, complete interchangeability of parts, and precision manufacture. Tight joints insure constant efficiency of the flame. Easy to clean . . . easy to operate . . . ideal for stoves, ranges, water heaters. Uses kerosene as a fuel.

Makers of . . .

Domestic Boiler and Furnace Units. Range Burners...Water Heaters...Special Products.

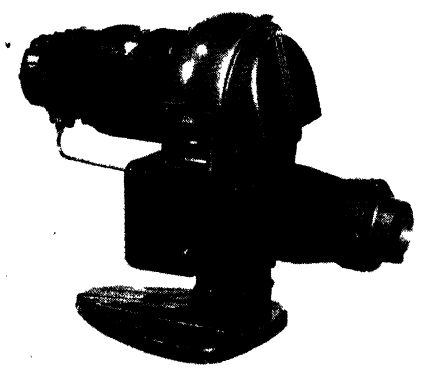
R. W. Beckett Corporation

Elyria, Ohio

Manufacturers of

Beckett Commodore Oil Burners

For all types of heating systems . . . steam, hot water, and warm air. For homes, apartments, business blocks, churches, schools and other applications.



Protected in the United States and Canada by 16 issued patents. Other patents pending.

Approved by Underwriters', and meets the specifications of the U. S. Dept. of Commerce, N. Y. C., Board of Stds. and Appeals, Canadian Stds. Ass'n.

Each time the Beckett COMMODORE starts operating, peak combustion efficiency is attained **immediately**. The air for combustion is violently rotated and mixed with atomized oil **before** the mixture is ignited resulting in a clean, quiet, uniform flame held in suspension.

The special **automatic air shutter** of the COMMODORE opens only to admit measured air for combustion while the burner operates. When the burner stops, the air shutter **closes**, preventing gravity air flow through the heating plant and up the chimney.

The complete power assembly of fuel unit, motor and fan is removable as a single unit. Electrode assembly and all current-carrying parts are enclosed in the air tube. Accurate center to center alignment of motor and pump shafts and **dynamic** balancing of all rotating parts assure vibrationless, noiseless operation.

Every Beckett COMMODORE Oil Burner is given an actual **test under fire** before shipment from the factory.

SPECIFICATIONS

CAPACITIES	Series "OB"	Series "M"	Series "L"
Maximum Oil Rate (G.P.H.)	3.5	6.00	13.00
MAXIMUM CONNECTED LOAD:			
Steam Sq. Ft.	1,600	2,700	5,850
Hot Water Sq. Ft.	2,500	3,240	9,350
Warm Air B. T. U.	350,000	600,000	1,300,000

ELECTRICAL REQUIREMENTS

110 Volts, 60 cycle A.C.
110 Volts, 25 cycle A.C.

IGNITION REQUIREMENTS

Electric Ignition by integral transformer.

CONTROLS

Underwriters' Listed Constant or Intermittent.

FUEL REQUIREMENTS

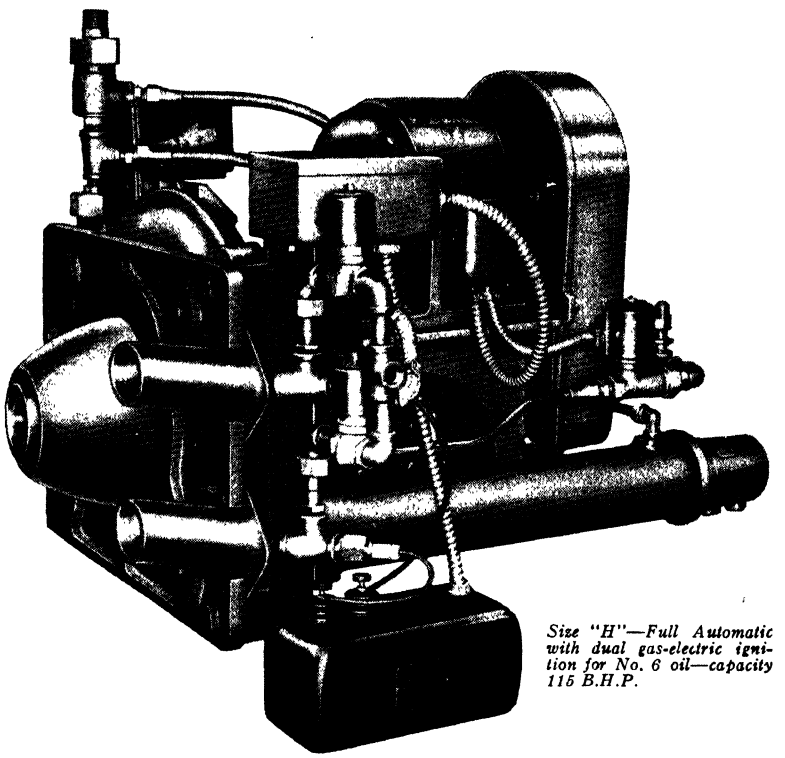
"No. 3 Fuel Oil" . . . Commercial Standard Specifications.

ENTERPRISE
ENGINE & FOUNDRY CO.

18th and Florida Streets • **San Francisco 10, Calif.**

Combustion Equipment Division

Distributors in all Principal Cities



Size "H"—Full Automatic with dual gas-electric ignition for No. 6 oil—capacity 115 B.H.P.

Enterprise Rotary Oil Burners are designed for efficient utilization of No. 3 and No. 5 oils, and when furnished with electric pre-heaters for No. 6, or Bunker oils. Approved by the Underwriters' Laboratories, the sizes range from 12 to 330 boiler hp in the pump type and to 650 boiler hp for gravity feed or with independent pumpset. By addition of a multi-jet gas head in the burner front plate, standard Enterprise Oil Burners can be converted to a combination unit where natural, manufactured, or process gas is available.

Enterprise Burners are available with manual, semi-automatic and full-automatic controls, and low fire, two-position or modulating controls.

Enterprise engineers have developed many applications for these burners where heat is required for industrial processing. The burners are designed for firing high or low pressure boilers of all types for commercial and industrial uses.

One of the features of the Enterprise Burner is the V-Belt Drive which offers a wide range of burner flexibility and makes possible the use of standard and modern type motors. The Enterprise design features durability, simplicity, quiet and economical operation.

Watch for Early Announcement of New Enterprise Oil Burner Models.

S. T. Johnson Co.

Builders of Domestic and Commercial Oil Burners

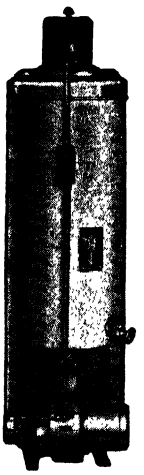
940 Arlington Ave., **Oakland 8, Calif.**

401 No. Broad St., **Philadelphia 8, Pa.**

Self-storage water heaters, separate burner units, burner-boiler units, conditioned air units, range burners and various specialized items comprise the line-up of Johnson light-oil Burners.

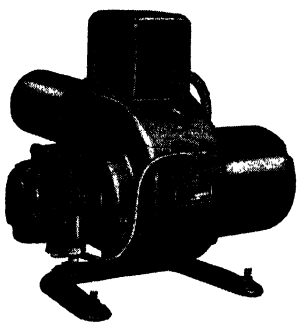
There is a wide range of sizes and capacities in each classification with which heating engineers and contractors can successfully meet every type of problem.

Every Johnson Burner is backed by an unbroken 44-year record of fine engineering and excellent craftsmanship.



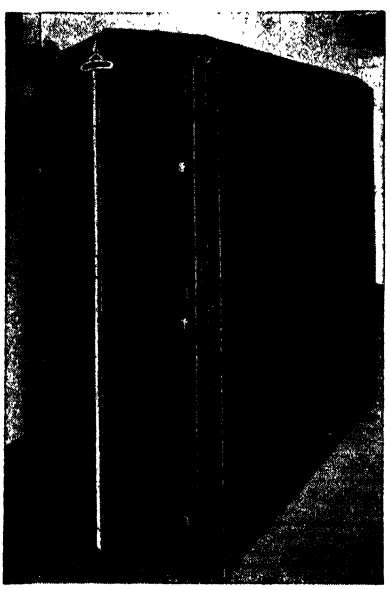
AQULUX WATER HEATERS →

Fully automatic, self-storage. Capacity: 100 to 540 gph.



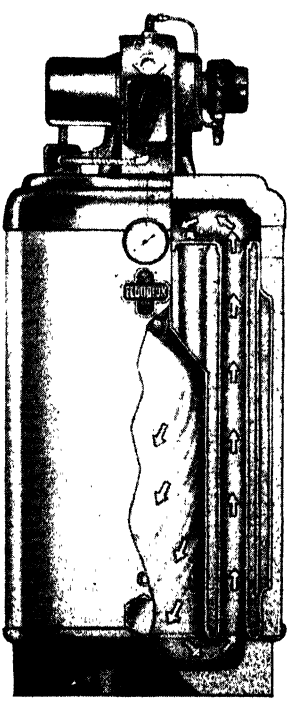
← **BANKHEAT BURNERS**

Fully automatic, pressure atomizing type. Sizes up to 20 gph.



← **SELECTAIR HEATERS**

Hot air, hot water or steam heat. 3 sizes. Bankheat Burners.



→ **ECONOLUX HEATERS**

Heat and hot water. Fully automatic Bankheat Burners.

S. T. Johnson Co.

Builders of Heavy-Duty Industrial Oil Burners

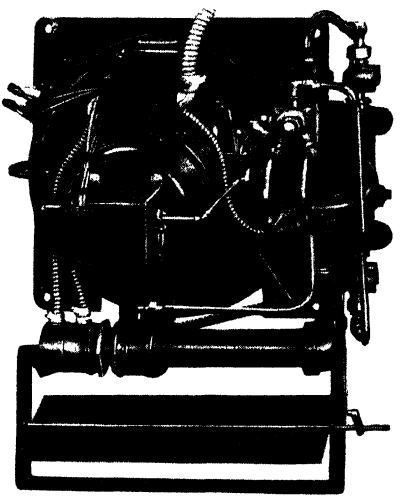
940 Arlington Ave., **Oakland 8, Calif.**

401 No. Broad St., **Philadelphia 8, Pa.**

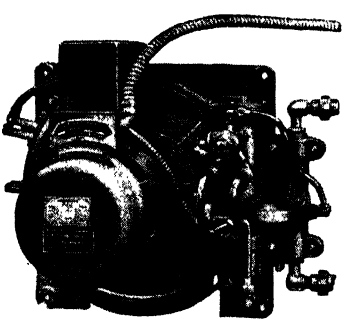
Johnson Industrial Burners are designed to operate on Heavy Oils which produce extra heat at low cost. They increase the capacity of equipment formerly fired with coal and produce desired steam pressures more quickly. Automatic regulation permits the boiler to operate with maximum efficiency at any specified steam pressure, without watching, care or attention, thus reducing labor costs.

They have been installed with marked success in hotels, hospitals, factories, office buildings and other large structures all over America because they provide heating engineers with a wide range of capacities and with every desired feature of economy, performance and automatic control.

In their design and in their construction, Johnson Burners represent the new and advanced engineering and building techniques backed by 44 years of practical experience.

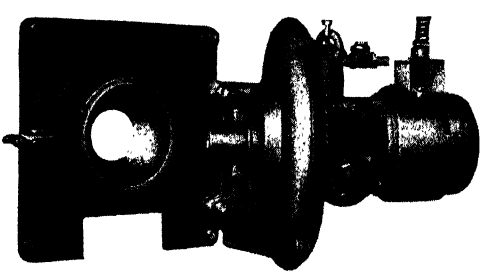


TYPE 30 AVH
Fully automatic. Pre-heater type. Burns No. 6 Oil. Six sizes, 20 to 300 horse power output.



TYPE 30 AV
Fully automatic. Burns No. 5 Oil. Six sizes, 2 to 100 gph.

TYPE 28
Manual and semi-automatic. With or without built-in pumps. Burns No. 5 and No. 6 Oils. Seven sizes, 2 to 135 gph. Illustration shows burner swung away from fire-hole-plate for easy inspection.



Petroleum Heat & Power Company

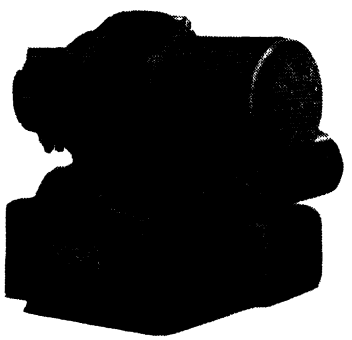
Main Office and Factory: **Stamford, Conn.**

Good Oil Burning Equipment . . . "Since 1903" . . . Fuel Oils

PETRO
REG. U S. PAT. OFF

DOMESTIC OIL HEATING EQUIPMENT

PRESSURE ATOMIZING DOMESTIC BURNERS



Petro P 20 Burner

Burner Model Number	Nozzle Size Gal. per Hr.	Total Capacity		App. Shpg Wgt.
		Steam Sq. Ft.	Hot Water Sq. Ft.	
P-20-A	1.00	350	560	155
P-20	1.25 To 2.50	435 To 875	695 To 1400	155
P-21	2.00 To 4.50	700 To 1575	1120 To 2520	160
P-22	3.00 To 6.00	1050 To 2100	1680 To 3360	170
P-12	6.00 To 10.00	2100 To 3500	3360 To 5600	215
P-13-A	9.00 To 12.00	3150 To 4200	5040 To 6720	285
P-13	12.00 To 18.00	4200 To 6300	6720 To 10080	285

Models P 20-A, P 21, P 22

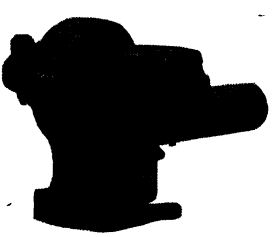
In domestic heating this group of Petro burners has wide and general application to steam, hot water, or warm air systems.

Burns No. 3 fuel oil (or lighter), heaviest and lowest priced fuel oil approved by Underwriters for domestic use. They are precision-built atomizing (or "gun" type) burners, with constant electric ignition for reliable, safe operation. May be installed with inside or outside fuel storage tanks without adding auxiliary pumping facilities. Order or inquiry should specify the type, size and rating of boiler or furnace to be fired, together with the total load.

Models P 12, P 13-A, P 13

Have wide application in heating large residences, stores, garages and other commercial buildings.

Approved for No. 3 (or lighter) fuel oil.



Petro P 13 Burner

Petro Boiler Units—both cast iron sectional and steel—in a range of five sizes covering normal domestic needs, and Petro Water Heaters and forced warm air furnaces are planned for production in late 1947. Information on this equipment available at that time. Send for catalog of Petro Domestic Oil Heating Equipment.

Petroleum Heat & Power Company

Main Office and Factory: **Stamford, Conn.**

Good Oil Burning Equipment . . . "Since 1903" . . . Fuel Oils

PETRO REG. U. S. PAT. OFF.

INDUSTRIAL AND COMMERCIAL OIL BURNING SYSTEMS

FOR AUTOMATIC . . . SEMI-AUTOMATIC . . . OR MANUAL OPERATION

For Unheated No. 5 or Lighter Oil

Model WA—Automatic ignition and operation with synchronized control of oil and air.

Model W-SA—Semi-automatic, *i.e.;* automatic variation of firing rate with manual ignition; or for manual variation and manual ignition.

For Heated Oils: Heavy No. 5, No. 6 (Bunker "C") oil

Model W-AH—Automatic ignition and operation with synchronized control of oil and air, and of oil heaters.

Model W-SAH—Semi-automatic with oil heaters, i.e.; automatic variation of firing rate with manual ignition; also available for manual variation and manual ignition.

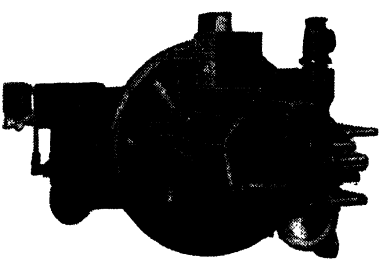
CAPACITIES

Model	Motor H.P.	Max. Gals. per Hour	Rated Cap. B.H.P.	Sq. Ft. C.I. Steam Rad.
W-2½	⅓	11	37	5,150
W-3	½	15	50	7,030
W-4	½	25	84	11,720
W-5	1	33	110	15,470
W-6	2	45	151	21,100
W-7	2	62	208	29,100
W-8	3	100	336	46,600
W-9	3	145	487	68,000

These burners are available for all electrical current characteristics.

PETRO'S THERMAL VISCOSITY CONTROL

The only dependable and accurate control of viscosity—and hence delivered combustion efficiency—is through the heat applied to the oil. Petro's Thermal Viscosity System controls this heat-application at its source. Has been used successfully for years, without any need for frequent manual adjustment.



Model W—Direct Driven, Rotary Cup Type Burner. Illustration Shows Modutrol Mounted on Burner.

This burner is a self-contained assembly of motor, fan, pump, rotary cup atomizer and all air and oil adjustment apparatus.

Interlocking air and oil control mechanism permits any minimum or maximum operation required within the burner's range of operation. Counter-flow Angular Air Vanes at nozzle increase air and oil turbulence and aid efficient combustion of heavy fuel oils.

Special oil adjustment valve meters oil to rotary cup, yet permits manual operation without disturbing permanent burner adjustment.

Removable rotary cup and nozzle permits changing shape of flame to suit requirements of any boiler and prevent flame impingement.

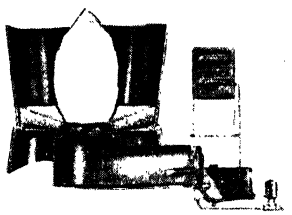
Send for catalog of Petro Commercial and Industrial Oil Burners

TRADE MARK

H.C. Little Burner Co.

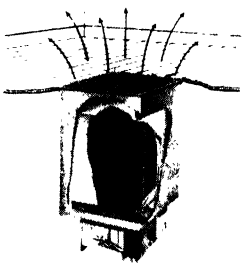
Head Office: **San Rafael, Calif.**

Factory Representatives in 18 Principal Cities



Natural Draft, Automatic, Vaporizing Burner

Natural draft vaporizing burner, specifically designed for low cost furnace oil and listed by the *Underwriters' Laboratories*. Cutaway model shown in typical conversion installation (with controls attached) is fully automatic, with electric ignition (no pilot light) and thermostatic control. Manually operated models, which do not require electricity, are also listed for low cost oil. Seven sizes: 1.45 qts to 2½ gal per hour.

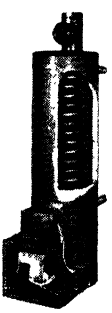


Fully Automatic Oil Burning Floor Furnace

These low cost units are factory assembled, including all controls, ready to hang in floor. Easy installation, no basement needed. Natural draft vaporizing burner, automatic operation, with electric ignition and thermostatic control. Inexpensive to operate. Listed by Underwriters' Laboratories for low cost furnace oil. Two sizes: No. **70-47**—47,250 Btu output (22 in. wide x 28 in. long x 44 in. high); No. **100-47**—75,000 Btu output (22 in. wide x 40 in. long x 45½ in. high).

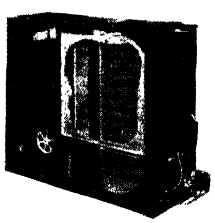
Utility Room Furnace

Ideal for modern homes without basement. Compact, fits neatly in small utility room or closet. Overall size: 20 in. wide x 32 in. deep x 73½ in. Very high efficiency. Two filters, 16 in. x 20 in. x 2 in.; 9 in. blower, 1000 cfm capacity at ¼ in. SP. Cold air return bottom or sides. 84,000 Btu output.



Coil Water Heater

For camps, auto courts, apartments or small hotels. Uses separate hot water storage tank. Also makes excellent boiler for hot water installations in home heating. Two sizes: No. 150—106,960 Btu output, 150 gph (80° rise); No. 250—160,440 Btu output, 250 gph (80° rise).

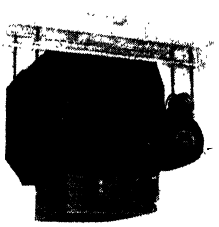


Winter Air Conditioner

Size A, 85,000 Btu output. Size B, 125,000 Btu output. Multivane blower, filters, vaporizing burner.

Ceiling Furnace

Industrial overhead heating saves floor space. Units are factory assembled, including vaporizing oil burner (no refractory brick saves much weight), thermostatic control, high capacity heat distributing blower with ¼ hp motor. Conforms to requirement of the Underwriters' Laboratories for use in garages. 140,000 Btu output.



A complete line of oil-fired small home heating units —plus special industrial units of moderate capacity.

Ray Oil Burner Co.

405 Bernal Avenue
San Francisco 12,

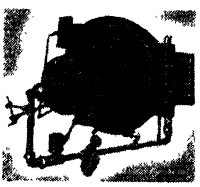
Distributors in all Principal Cities

Since 1872

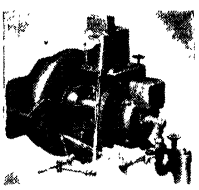
629 Grove Street
Jersey City 2, N. J.

Consult your local Telephone Directory

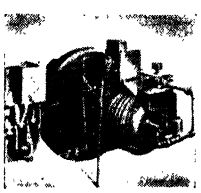
Products: **A complete line of Horizontal Rotary and Pressure Atomizing Oil Burners; Combination Oil-or-Gas Burners; Industrial Gas Burners; Oil Burning Water Heaters; Winter Air Conditioning Units, Commercial Ranges.**



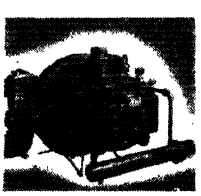
1 to 1000 hp Type AG, Manual, Semi-Auto.



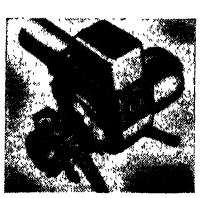
Semi-Automatic, Type AP-14, for No. 5 oil.



Fully Automatic Type AR-134, for No. 5 oil.



Fully Automatic Type AR-144, for No. 6 oil.



Fully Automatic Type JP, # 3 or lighter oil.

RAY HORIZONTAL ROTARY OIL BURNERS

Built in fully automatic, semi-automatic and manual types; in sizes from 1 to 1000 Boiler hp; to burn all grades of fuel oil.

Standard models include both direct and belt drives—the latter being recommended for use where other than 50 or 60 Cycles AC, or only DC is available. Types for straight electric or straight gas ignition; pump or gravity feeds. Direct drive types include a steam turbine driven model.

All fully automatic types for heavy oil incorporate the Ray Dual Pump and Reservoir, with the Ray VISCOSITY Valve, a patented, exclusive feature which automatically meters the correct amount of fuel at all times, regardless of changes in viscosity. All larger sizes employ dual ignition, for maximum reliability.

RAY PRESSURE ATOMIZING OIL BURNERS

Fully automatic, for No. 3 oil or lighter. AC or DC; capacities to 18 gal/hr.

RAY COMBINATION OIL-or-GAS BURNERS

Operate on any grade of fuel oil, any grade of natural or manufactured gas. Oil burner sizes to 1000 boiler hp; maximum gas capacity: 43,600 cu ft/hr. Changeover may easily be made in a few minutes.

RAY INDUSTRIAL GAS BURNERS

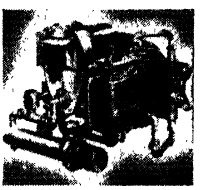
For gas pressures above 1 lb/sq in. May be used alone or in combination with a Ray Oil Burner. Built in eleven sizes; in capacities to 43,000,000 Btu/hr.

RAY WINTER AIR CONDITIONING UNITS

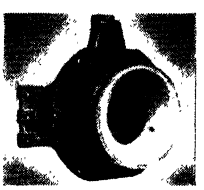
Built in four sizes, with input capacities of 140,000, 230,000, 350,000, 450,000 Btu.

RAY OIL WATER HEATERS

Two sizes. *Capacities:* 45 and 75 gal. *Maximum recovery rates:* 154 and 240 gph.

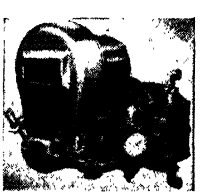


Belt Drive Automatic Type BR-141, # 6 oil.

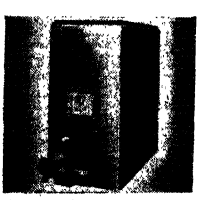


Gas Burner, Type HN, for high pressure gas.

Steam Turbine Drive, Type TG, all grades oil.



Small Capacity (¼ to 2½ gph) rotary burner.



Ray Oil Furnace, Winter Air Conditioning Unit.

Combustion Equipment Division

TODD SHIPYARDS CORPORATION

81-16 45th Avenue, **Elmhurst, Queens, N. Y.**

NEW YORK, BROOKLYN, ROCHESTER, CHARLESTON, S. C., CHICAGO, BOSTON, WASHINGTON, DETROIT, GRAND RAPIDS, TAMPA, GALVESTON, MOBILE, NEW ORLEANS, LOS ANGELES, SAN FRANCISCO, SEATTLE, MONTREAL, TORONTO, BARRANQUILLA, BUENOS AIRES, LONDON. HOBOKEN, NEWARK, PHILADELPHIA, SPRINGFIELD, MASS., BALTIMORE,

THE TODD HEX-PRESS REGISTER in combination with the **TODD "VEE-CEE" VARIABLE CAPACITY BURNER** . . . makes possible increased combustion efficiency under almost any type of boiler of 100 hp. capacity or larger, operating at 50 lb. steam pressure or higher.

It provides equal efficiency under either forced or natural draft conditions. The Hex-Press Register assures the most intimate mixture of oil and air as well as quicker, more complete combustion . . . with minimum draft loss at high capacity . . . effecting great economy in maintenance and materially reducing fuel costs.

Through the exclusive "variable range" feature of the "Vee-Cee" Burner, practically unlimited firing range is assured . . . without change of burner tips, oil delivery pressure or angle of spray.

Constant steam pressure can be maintained regardless of demand . . . changing load requirements are met instantly under manual or fully automatic control.

COMBINATION GAS AND OIL BURNERS

For Natural or Refinery Gas and/or Fuel Oil. Available in wide range of capacities. Quickly adjustable for the combustion of either fuel alone, or both in combination. Of special value where fluctuating comparative costs of these fuels call for equipment suited to change-over without time-consuming structural changes.

Maintenance and operation are reduced to a minimum by compactness and simplicity of design . . . accessibility of all parts . . . rugged construction and positive overall efficiency.

Design features eliminate possibility of escaping gas due to structural distortion . . . prevent stratified combustion resulting from improper air distribution and high gas pressure.

Providing sufficient flexibility to care for varying loads, these units assure high furnace temperature and radiant heat transfer with low stack temperature . . . thorough mixture and optimum air-fuel ratio with utmost ease of adjustment.

ROTARY FUEL OIL BURNERS

For firing high or low pressure steam or hot water boilers of all types . . . in smaller factories and industrial plants, laundries, dryers and cleaners, office buildings, hotels, apartment houses. Also applicable to industrial ovens, kilns, etc., where furnace and general physical conditions permit.

Available with manual, semi-automatic or fully automatic control . . . in varying sizes and types . . . for burning light or heavy oil.

Horizontal atomizing cup is rotated by direct-connected electric motor, assuring constant firing as long as motor is in operation. Motors are of extra large frame size, air-cooled and built to withstand long, hard service. Positive air-oil interlocking device automatically shuts off oil supply following any burner stoppage.

Of rugged construction . . . with all parts easily accessible for cleaning or renewing . . . these burners provide a flexible capacity range, with complete and efficient combustion under widely fluctuating loads.

TODD MANUFACTURES: Mechanical Pressure Atomizing Oil Burners—VEE-CEE Variable Capacity Burners—Horizontal Rotary Oil Burners—Oil Burning Air Registers for Natural, Assisted, Induced or Forced Draft—Inside Mixing Steam Atomizing Oil Burners—Combination Gas and Oil Burners—Furnace Doors and Interior Castings for Converting Howden Type Furnace Fronts to oil firing—Oil Burning Galley Ranges—Oil Heating, Pumping and Straining Equipment—Heated Air Generators.

All installations of Todd Equipment are always *individually engineered* to fulfill specific requirements. *Send for descriptive literature.*

Todd engineers are always available for consultation and analysis of combustion problems—without obligation.

Williams Oil-O-Matic Division

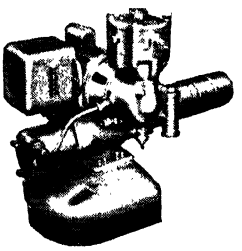
EUREKA WILLIAMS CORPORATION, BLOOMINGTON, ILLINOIS

WILLIAMS OIL-O-MATIC HEATING COOLING PRODUCTS

Manufacturers of Automatic and Manually Controlled Fuel Oil Burners

OIL BURNERS

Williams Oil-O-Matic Lo-Pressure burners are offered in 4 sizes ranging in capacity from ½ to 7 gallons of fuel oil per operating hour. Easily installed in any type heating plant. Patented Thrift Meter premeters oil to exactly meet heating plant needs. Wide, non-clogging orifice handles even the heaviest oils.



Williams Hi-Pressure precision-built burners are available for those who want high quality at minimum cost. 3 sizes with capacities from 1.00 to 7 gallons per hour.

How to Decide Size of Burner

For low pressure domestic boilers, 1 gal of fuel oil per hour (140,000 Btu) is required for approximately 300 sq ft of steam radiation or its equivalent, or for 480 sq ft of hot water radiation or its equivalent. 70,000 Btu when using hot air furnace ratings. 24 sq ft steam boiler heating surface (or 2.2 hp). For exact data, see Oil-O-Matic Installation and Service Manual.

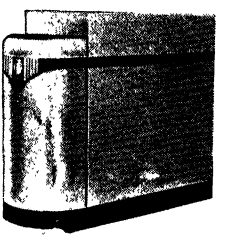
Oil-O-Matic Lo-Pressure Burners Leg or Flange Mt.

Model	Oil Capacity		Motor		Atom. Pressure
	Min.	Max.	Hp	Rpm	
K-150	.50	1.50	1/10	1800	2 lbs
K-3	1.00	3.00	1/10	1800	2 lbs
K-4.5	1.35	4.50	1/5	1800	2½ lbs
K-7	4.00	7.00	1/5	1800	3 lbs

Williams Hi-Pressure Burners Leg or Flange Mt.

HP-1	1.00	1.50	1/16	1725	100 lbs
HP-3A	1.35	3.00	1/12	1725	100 lbs
HP-7	3.50	7.00	1/5	1800	100 lbs

WINTER AIR CONDITIONERS

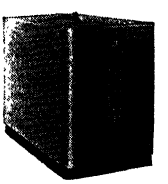


Williams Oil-O-Matic Winter Air Conditioners automatically draw in air, filter, heat and humidify it, and gently circulate the conditioned air to all rooms. 2 sizes fill all needs. Choice of Lo-Pressure or Hi-Pressure Burner.

Oil-O-Matic Winter Air Conditioners

Model	Btu at Bonnet	C.F.M. (a) ⅜" S.P.	Oil Input G.P.H.	Filters Sq In	Blower Motor
10	100,000	1300	1.00	1000	¼ hp
15	150,000	1800	1.50	1920	¼ hp

BOILER BURNER UNITS



Williams Oil-O-Matic Boilers are available in 3 models: Lo-Boy (illus.) in 4 sizes for steam, 4 for hot water; Water Base in 3 sizes for steam, 3 for hot water; Residential Steel in 4 sizes for steam, 4 for hot water. All units furnished complete with either Lo-Pressure or Hi-Pressure burners.

Oil-O-Matic Cast Iron Boiler Burner Units

Model	Net Load Ratings I.B.R.			Gross I.B.R.	
	Steam Sq Ft	Water Sq Ft	Btu	Oil Input G.P.H.	Output Btu
LB-5S or 5W	360	580	86000	1.35	130000
LB-6S or 6W	450	720	108000	1.65	162000
LB-8S or 8W	620	990	149000	2.20	222000
LB-10S or 10W	780	1250	187000	2.75	278000

Oil-O-Matic Cast Iron Water Base Boiler Burner Units

16S or 16W	290	460	69000	1.05	105000
20S or 20W	350	560	83000	1.25	126000
24S or 24W	410	660	98000	1.50	147000

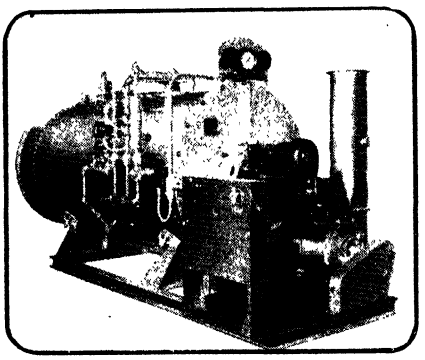
Oil-O-Matic Steel Boiler Burner Units

320S or 320W	320	510	76800	1.10	118000
400S or 400W	400	640	96000	1.40	146500
540S or 540W	540	860	129600	1.90	195000
680S or 680W	680	1090	163200	2.30	244000

Preferred Utilities Manufacturing Corporation

Executive Offices
1860 Broadway, **New York 23, N. Y.**
FACTORY—**DANBURY, CONN.**
BRANCH OFFICE: BOSTON, MASS.

Representatives in Principal Cities



Unit Steam Generator

PREFERRED UNIT STEAM GENERATORS

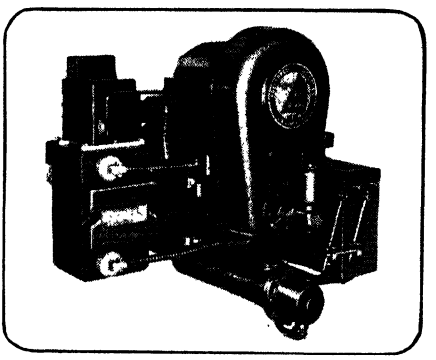
The Preferred Unit Steam Generator is a heavy duty, oil-fired, portable, automatic steam plant with all the equipment necessary to produce steam—economically—with a minimum overall thermal efficiency of 80 per cent.

Induced Draft — Induced or "pull through" draft requires only a small vent to the outside air—no large, expensive stack is necessary. Induced draft operation automatically controls air volume to meet the requirements of complete combustion and also eliminates the danger of forcing the products of combustion into the boiler room.

Heavy Oil Types—Preferred Unit Steam Generators are made in all sizes, up to and including 500 hp (pressures up to 200 lb psi) for use with the heavier grades of bunker oils, including the new catalytic residual oils—for either fully or semi-automatic operation.

Light Oil Types—For use with lighter oils, the Preferred Unit Steam Generator is made in all sizes up to and including 80 hp (pressures up to 200 lb psi).

For further details write for Bulletin No. 1000.



Oil Burner

PREFERRED OIL BURNERS

Preferred oil burners are made in both the horizontal rotary and pressure atomizing types. Each type is suitable for manual, semi-automatic or fully-automatic operation.

Horizontal Rotary Type—The rotary-cup burner is suitable for use with either light or heavy oil as well as the new catalytic residual Oils. A throttle control which includes the patented Voluvalve automatically delivers the correct mixture of oil and air for efficient combustion at all rates of firing, regardless of variation in temperature, pressure or viscosity of the oil.

The sizes range from 5 to 150 gph for residual oils (see Bulletin 175) and ⅛ to 3 gph for Diesel or lighter oils (see Bulletin 100).

Pressure Atomizing Type—Preferred pressure atomizing burners are designed to burn light oil only. Made in conversion models from 1 to 3 gph and unit steam generator models from 3 to 30 gph. (Bulletin in preparation)

Other Preferred Products

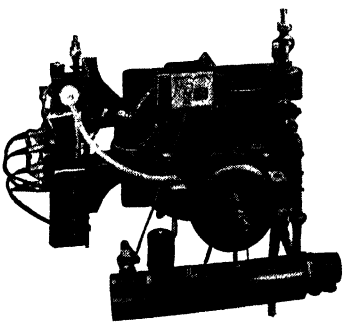
Water Heaters ..... Draft-A-Justors
Oil Burner Accessories ..... Boiler Room Compounds

York-Shipley, Inc.

Main Office and Plants—**York 16, Pennsylvania**

OIL-FIRED EQUIPMENT FOR INDUSTRY

HORIZONTAL ROTARY BURNERS



Model AHPM direct-drive fully automatic pump-type burner with full modulating system, for heating or process work. Uses No. 6 oil.

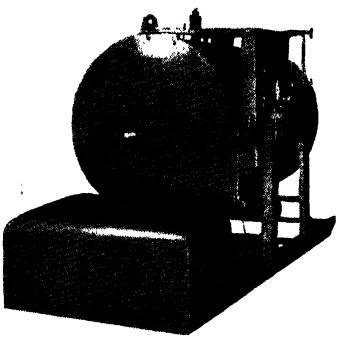
York-Shipley Horizontal Rotary Burners cover the range from 45 to 400 boiler hp, and are built in direct-drive and belt-drive types. Models are offered for use of fuel oils No. 1 through No. 6 (light distillate to most viscous bunker oils), for manual, semi-automatic, or full modulating control, with or without pumps.

The extremely wide range of models and sizes, high efficiency, and adaptability of this line assures easy selection of the *right* unit to fit *any* type or shape or make of boiler, with long life and low operating cost.

Three exclusive engineering developments provide *precision combustion* to an unparalleled degree: *The Iris Shutter*, which gives absolute control of burner air, causing metered volume of burner air to remain constant; *The Flame-Former*, which shapes the flame to fit combustion chambers of any type; and *The Automatic Torch Lighter*, a pressure-type igniter for smooth and positive automatic starting.

All York-Shipley Industrial products are sold, engineered and installed by local distributors who have been selected because of their knowledge of engineering and of equipment using heavy oils. These local distributors have well-trained staffs and will aid in solving any heating or power problems.

STEAM-PAK GENERATORS



Model SPL-30-3 low-pressure boiler for heating applications. A three-pass, downdraft, horizontal fire tube design. Uses No. 3 oil.

Steam-Pak Generators are built *both* for low-pressure heating load and for high-pressure process load, in sizes from 15 to 100 hp. Using fuel oils No. 3, 5, and 6, they require only a low-cost vent to remove products of combustion.

With about half the size, weight, and installation cost as compared to brick-set boilers of comparable capacity, Steam-Pak Generators require only four simple service connections, feature "one-man maintenance," are completely wired, piped, and pre-tested at the factory. Ready to operate when delivered.

The Steam-Pak Generator is an efficient unit, combining the oil burner and boiler in one package. It is designed to operate at peak efficiency through the entire firing range. This is accomplished with the Iris Shutter and modulating pump.

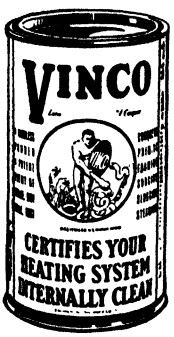
A COMPLETE LINE OF INDUSTRIAL COMMERCIAL AND RESIDENTIAL EQUIPMENT

York-Shipley, Inc. builds one of the widest range of oil-fired units. Beside the Horizontal Rotary Burners and Steam-Pak Generators for industrial and commercial use described here, we offer the famous *York-Heat* boiler-units, winter air conditioners, water heaters, vaporizing warm air furnaces and conversion burners.

The Vinco Company, Inc.

305 East 45th Street **New York 17, N. Y.**

Only a clean boiler can be an efficient boiler. A clean boiler means saving fuel, as well as safeguarding boiler metal.



Boiler Cleaner
3 and 5 lb. cans

A positively harmless insoluble powder cleaner for new, remodeled and old heating systems. A unique, scientifically processed compound on a special formula not to be confused with other powder boiler cleaners.

What Vinco Boiler Cleaner Does

VINCO removes oil, grease, scale, rust and dirt from the internal surfaces and from the boiler water *without the labor, expense, and uncertain results of blowing boilers over the top or of wasting returns.*

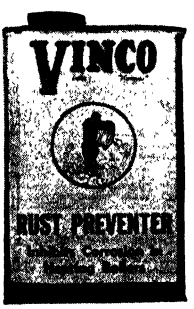
By this thorough cleaning Vinco prevents or cures foaming, priming, surging, and slow steaming.

How Vinco Boiler Cleaner Works

Each minute grain of VINCO powder adsorbs several times its own weight of oil, grease, rust and dirt. These larger grains of adsorbed impurities then settle and are drained through the bottom according to directions on each can.

Vinco Guarantees

1. VINCO contains no potash, lye, soda of any kind, oil, acid, or other harmful ingredients.
2. Purchase price is refunded if results are not as claimed when VINCO has been used according to directions.



Rust Preventer
1 qt. cans only

VINCO RUST PREVENTER

When used after VINCO Boiler Cleaner has removed oil, grease, rust, scale and dirt, it will add and keep the rust inhibiting factors at the optimal constant for a year or more. (Test kit below has complete instructions and chart.)

Vinco Field Test Kit No. 10

VINCO FIELD TEST KIT No. 10

for Testing and Treating Heating Boiler Waters

The kit enables the layman to make simple, rapid tests to diagnose and prescribe correct treatment of boiler waters right on the job.

A new time saving method that permits valid conclusions heretofore requiring complicated and often lengthy laboratory analysis and technique.

Each kit has sufficient material for complete tests on 100 jobs.

Refills cost about 2 cents for testing each job.

SPECIFICATIONS FOR COMPLETE VINCO TREATMENT OF NEW OR REMODELED STEAM, VAPOR, OR HOT WATER SYSTEMS

Do not use as a cleaning agent soda or any alkali, vinegar or any acid. Use Vinco.

1. AFTER THE SYSTEM IS TESTED AND TIGHT, USE THE PROPER QUANTITY OF VINCO LISTED.

After this first clean-out of any new or remodeled heating system, Vinco Boiler Cleaner need be used only if more piping, radiation, or another boiler is added to the original installation, or if the system is fouled by unwise cleaning or leak-sealing experiments.

2. After using Vinco Boiler Cleaner, Vinco Field Test Kit should be used to determine and apply the proper quantity of Vinco Rust Preventer. Vinco Rust Preventer should be applied annually or whenever the boiler water is drained for necessary repairs to the system.

SPECIFICATION FOR OLD HEATING SYSTEMS THAT DO NOT PERFORM PROPERLY

Diagnose and treat according to Vinco Field Test Kit. If a test kit is not available, consult table of quantities on this page and follow directions on Vinco cans.

SPECIFICATION FOR HOT WATER SYSTEMS

Use half quantities listed for treatment of steam systems to remove impurities. Then use test kit to determine proper quantity of Vinco Rust Preventer.

CONSULT THIS TABLE FOR NEW AND REMODELED HEATING SYSTEMS AND When a Vinco Field Test Kit No. 10 is not available if cleaning old heating systems.

QUANTITIES OF VINCO (IN POUNDS) REQUIRED FOR HEATING SYSTEMS

(Note that quantities are based on actual installed radiation, not on boiler capacity.)

Sq Ft of Radiation	For Steam or Vapor Systems, to prevent or cure priming or foaming. Also for Hot Water Heating Systems Maintained at approx. 200 F or above.	Annually, to remove rust scale, dirt and for Hot Water Systems below 200 F.
up to 350	3	1½
351 " 600	5	2½
601 " 1100	8	4
1101 " 1400	10	5
1401 " 1800	13	6½
1801 " 2100	15	7½
2101 " 2700	18	9
2701 " 3100	20	10
3101 " 3700	23	11½
3701 " 4200	26	13
4201 " 4600	28	14
4601 " 5000	30	15
5001 " 5300	31	15½
5301 " 5600	32	16
5601 " 5900	33	16½
5901 " 6200	34	17
6201 " 6500	35	17½
6501 " 6800	36	18
6801 " 7100	37	18½
7101 " 7400	38	19
7401 " 7700	39	19½
7701 " 8000	40	20
8001 " 8300	41	20½
8301 " 8600	42	21
8601 " 8900	43	21½
8901 " 9200	44	22
9201 " 9500	45	22½
9501 " 9800	46	23
9801 " 10100*	47	23½

*Above 10100 sq ft use an additional pound Vinco for each additional 300 sq ft of actual installed radiation.

Soot-Off—1 lb. cans 60 and 100 lb. drums

VINCO SOOT-OFF

Safely and thoroughly removes the insulating blanket of soot on fire pot, flues and chimney. It also insures against external corrosion (caused by dampness and soot forming sulphuric acid during summer layoff.) No dangerous chemicals.

REMOVE SOOT WITH VINCO SOOT-OFF SEVERAL TIMES A YEAR

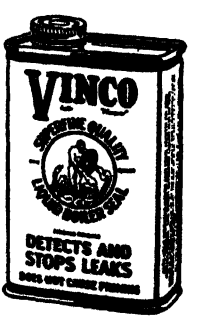
VINCO SUPERFINE LIQUID BOILER SEAL

A different liquid seal. Unique in that it does not induce priming and foaming. It has no unpleasant smell. Makes speedy and permanent repairs of boiler and heating system leaks. Fine to tighten up new jobs. Directions simple.

Quantities

Steam and Vapor Systems—Use 1 quart VINCO Liquid Boiler Seal to each 6 sq ft *grate* area.

Hot Water Systems—Use 2 quarts VINCO Liquid Boiler Seal to each 6 sq ft *grate* area.



Liquid Boiler Seal 1 qt. cans only

McDonnell & Miller, Inc.

Safety Devices for Steam and Hot Water Boilers and Liquid Level Controls

General Offices: Wrigley Building, **Chicago 11, Illinois**

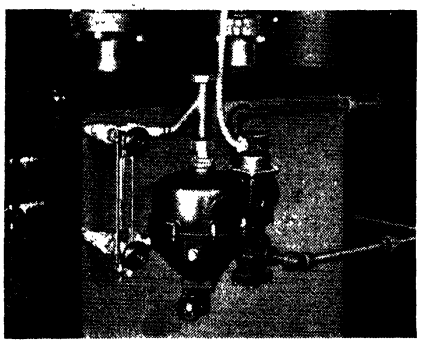
"Doing one thing well"

PRODUCTS:

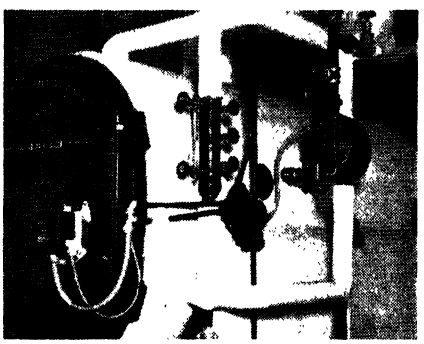
Boiler Water Feeders; Feeder Cut-off-Combinations; low Water Fuel Cut-offs; Pump Controls; Low Water Alarms; Humidifier Water Level Controls; Safety Relief Valves for hot water heating boilers and storage tanks; High and Low Oil Switches and Liquid Level Controllers for a wide range of services.

The service range and types of installations covering most common applications of McDonnell Boiler Water Level Controls are described here. For facts concerning protection of process boilers, or any special information, consult our engineering department.

McDonnell Combined Boiler Water Feeder and Low Water Cut-off



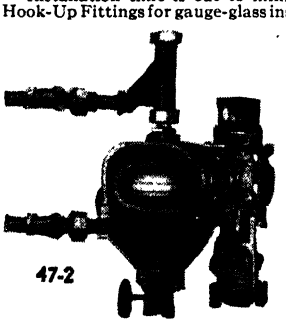
McDonnell No. 47-2 for heating boilers under *5000 sq ft capacity. Maximun steam pressure, 25 lbs.*



McDonnell No. 51-2 for heating boilers over *5000 sq ft capacity. Maximum steam pressure, 35 lbs.*

A typical installation of the McDonnell No. 47-2 Combined Boiler Water Feeder and Switch is illustrated above. The water feeder maintains safe level by feeding when water line drops. In case of foaming and priming or failure of water supply, causing water level to drop to ¼ in. in the water glass, low water switch comes into action. For automatically fired boilers switch may be wired to cut current to burner. For hand fired boilers switch may be wired to complete alarm bell circuit. Also furnished for hand fired boilers without switch—designated No. 47.

Installation time is cut to minimum by Quick-Hook-Up Fittings for gauge-glass installation. Valve mechanism is isolated from the heat of the float chamber. Large area straight-through blow-off valve is standard equipment.



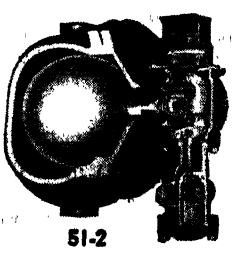
47-2

The McDonnell No. 2 Switch used in the No. 47-2 is Underwriters' approved. Electrical rating: a-c ¾ hp 110-220 V.; d-c 10 amp. 115 V.

The illustration above shows a typical installation of the McDonnell No. 51-2 Combined Boiler Water Feeder and Switch used for larger boilers. This combination functions the same as the No. 47-2, the feeder taking care of normal requirements and the switch safeguarding against emergencies by cutting off the burner in automatically fired boilers or completing a low water alarm circuit for hand fired installations. The feeder is also furnished for hand fired boilers (as No. 51) without low water cut-off and alarm switch.

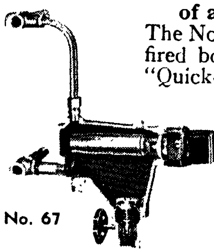
Basic features of the No. 51-2 are the same as in the No. 47-2, except that it is installed with 1 in. equalizing pipe instead of the McDonnell "Quick-Hook-Up" and has the larger feeding capacity required for larger boilers.

For boiler operating at pressures from 35 lb to 75 lb use the McDonnell No. 53-2 (with switch) or No. 53 (without switch). Electrical rating of switches used in No. 51-2 or 53-2 is the same as previously given for the No. 47-2.



51-2

McDonnell No. 67 Low Water Cut-off for automatically-fired steam boilers of any size. Maximum steam pressure, 25 lb

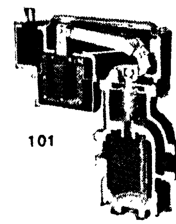

No. 67

The No. 67 takes care of low water cut-off requirements of automatically fired boilers with steam pressure below 25 lbs. It has the McDonnell "Quick-Hook-Up" for quick, easy and trouble-proof installation in the gauge glass tappings; deep sediment chamber with large quick-opening blow-off; packless, non-binding construction; adjustable terminal box to make wiring neat and easy; dependable, snap-action, twin switches.

One switch **closes** on small drop without stopping burner. It can be used to complete an alarm bell circuit, warning of approaching low water, or can be used to complete circuit to the McDonnell No. 101 Electric Water Feeder described below. Second switch cuts current to burner if water level drops to ¼ inch in gauge glass.

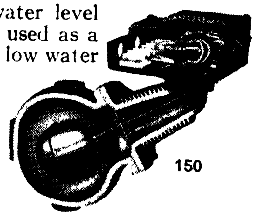
Underwriters' ratings for both switches: a-c ¾ hp, 110-220 V.; d-c ¼ hp, 115-230 V.

McDonnell No. 101 Electric Boiler Water Feeders for boilers up to 5000 sq ft capacity


101

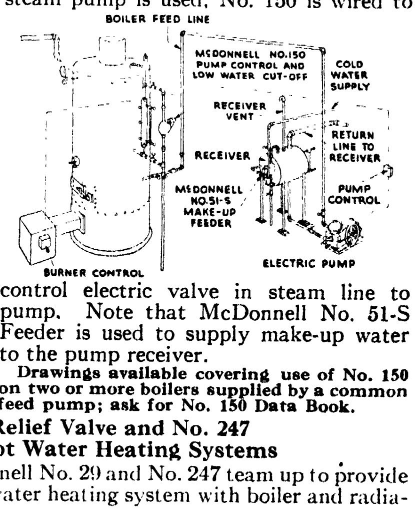
The No. 101 is an electric water feeder for use with No. 67 Low Water Cut-off or with McDonnell "built-in" Low Water Cut offs which are standard equipment on many modern heating boilers. It converts the cut-off into a combination boiler water feeder and low water cut-off as described on the opposite page.

McDonnell No. 150 Pump Control, Low Water Cut-off and Alarm Switch for boilers of any size. Maximum steam pressure, 150 lb


150

This boiler water level control may be used as a pump control, a low water cut-off, a low water alarm switch, or for any combination of these functions. Electrical ratings are: a-c 1 hp, 110-220 V., d-c ¼ hp, 110-220 V, as pump control or cut-off; 1 amp. 110 V, a-c or d-c—as low water alarm. No. 150 has automatic reset low water cut-off switch but may be ordered with manual reset as No. 150-M.

A typical hook-up of the McDonnell No. 150, controlling an electric pump and providing low water cut-off, is shown opposite. When water level drops ¾ in. below normal, No. 150 starts pump and then stops it when normal water line has been restored. If emergency occurs and water level falls to arrow mark on body of control, cut-off switch stops burner. If steam pump is used, No. 150 is wired to



control electric valve in steam line to pump. Note that McDonnell No. 51-S Feeder is used to supply make-up water to the pump receiver.

Drawings available covering use of No. 150 on two or more boilers supplied by a common feed pump; ask for No. 150 Data Book.

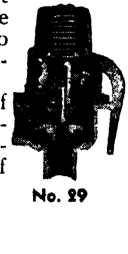
McDonnell No. 29 Safety Relief Valve and No. 247 Float Operated Feeder for Hot Water Heating Systems

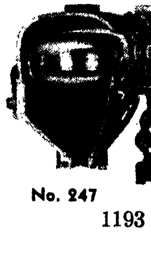
The drawing below illustrates how the McDonnell No. 29 and No. 247 team up to provide good operation as well as protection of a hot water heating system with boiler and radiation on the same level.

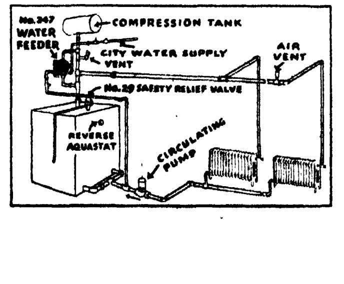
The No. 247 float operated feeder maintains the proper level above the high point in the supply main, eliminating the chance of separation of the water and loss of connected load.

The No. 29 Btu rated safety relief valve protects the boiler against excessive pressure when matched to the gross Btu output of the boiler.

This team of controls gives flexibility and protection to this type of system.


No. 29


No. 247

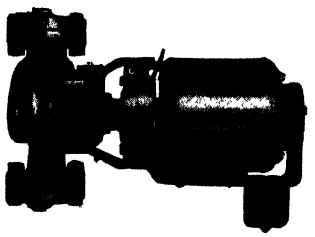


Bell and Gossett Company

Morton Grove, Illinois

HYDRO-FLO HOT WATER SYSTEMS AND SPECIALTIES

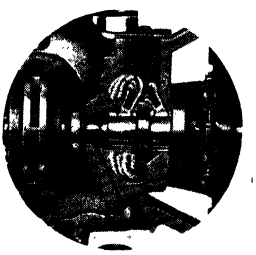
B & G Booster Pumps



The B & G Booster is the basic unit of a B & G *Hydro-Flo* Forced Hot Water Heating System. It is built as a horizontally driven unit for sound engineering reasons which have demonstrated their practical value in the thousands of installations now in operation. This construction makes possible many desirable and exclusive features.

For example, the patented water-tight Seal eliminates the need for a stuffing box. This Seal positively prevents entry of water into the bearings. The shaft is of highly polished, hardened machine steel and the close-fitted Impeller makes every revolution count by holding water slippage to a minimum.

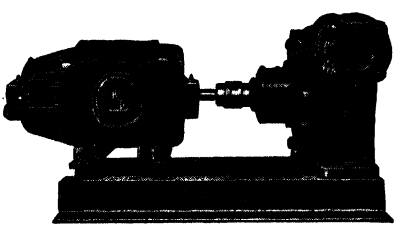
B & G Boosters have a genuine oil-circulating lubrication system—one of the greatest reasons for the quiet, dependable and economical operation of this pump. Oil is drawn up from the oil well by wool fibre wicking and dropped on the horizontal bearing surfaces. Medium grade motor oil is used and only a few drops at infrequent intervals required.

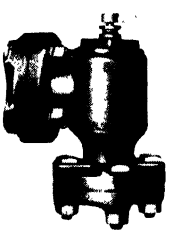


Oil Lubricated Bearings

B & G Universal Pumps ⟶

The B & G Universal Pump is designed for large forced hot water heating systems in apartment buildings, office buildings, factories, schools, etc. The installation can be operated as a large single zone or divided into several zones in which circulation of the pumped water in each circuit is controlled by a B & G Motorized Valve, operated by a zone thermostat.





B & G Angle Flo-Control ⟵ Valves

This valve, installed in the main, shuts off circulation to radiators when heat is not needed, permitting summer operation of a B & G Indirect Water Heater. It also helps maintain a uniform room temperature during the heating season.

B & G Motorized Valves ⟶

Thermostatically operated valves used for controlling boiler water flow through the individual circuits of zoned heating systems.

⟵ B & G Monoflo Fittings

B & G Monoflo Fittings permit the use of a *single* pipe main instead of the conventional flow and return lines. It is installed at the junction of the radiator risers to the single main and assures the diversion of the proper amount of heated water into each radiator. Savings in space, labor and materials are obviously effected.

SEE THE B & G HANDBOOK FOR COMPLETE DESIGNING DATA

HOT WATER SYSTEMS AND SPECIALTIES

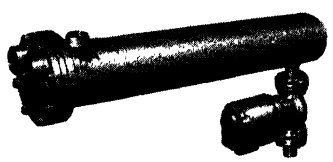
B & G Relief Valves

For relieving excess boiler pressures in hot water heating systems, and in the lines of service water systems. B & G Relief Valves have the design features which assure dependable service.

B & G Reducing Valves

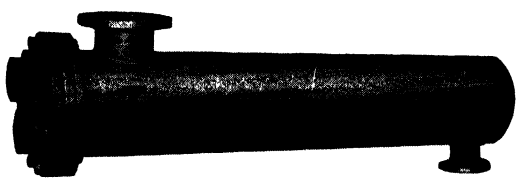
Fast operating valves for keeping hot water heating systems properly filled. Easily adjusted to meet varying building heights. Also high pressure reducing valves for protection of plumbing fixtures.

B & G Type "CWU" Radiation Heater



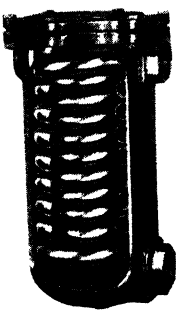
The B & G Radiation Heater is a "shell and tube" heat exchanger and is installed below the water line of a steam boiler. Hot boiler water is pumped by a B & G Booster through the shell, thereby heating the water for the heating system, which is pumped through the tubes of the Heater.

Pumping the water through both the heater and the heating system not only affords excellent temperature control, but also permits the use of much smaller pipe and fittings.



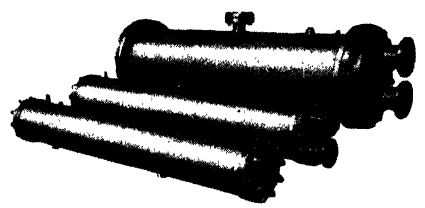
B & G Type "SU" Instantaneous Water Heaters

For heating water with steam. Ideal for industrial plants or wherever large volumes of hot water are required continuously for service water supply or process work. No storage tank required—the large heat transfer surface in these units heats water instantly as needed. Available in a wide range of capacities.



B & G Indirect Water Heaters

Any steam, vapor or hot water heating boiler can be equipped with a B & G Indirect Water Heater. With the proper electrical controls, the Heater will furnish an ample supply of hot water, *winter and summer*, at very low operating cost. Heater must be used with a storage tank of suitable capacity.

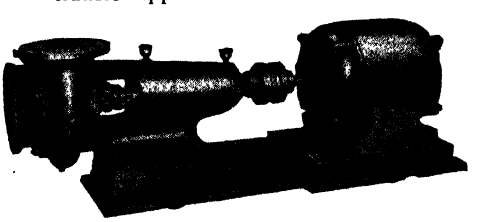


←≪ B & G Refrigeration Components

A very flexible line of direct expansion evaporators, condensers, liquid receivers, combination liquid receivers and subcoolers for refrigeration purposes are now available. Special alloys may be incorporated in the units for those critical heat transfer applications.

B & G Centrifugal Pumps ≫→

Design and construction based on years of experience in the industrial field. Rugged, compact units—built to stand up under the strain of continuous operation. Available with semi-open or enclosed impellers —motors flexible coupled or integral with pump. Send for Catalog.

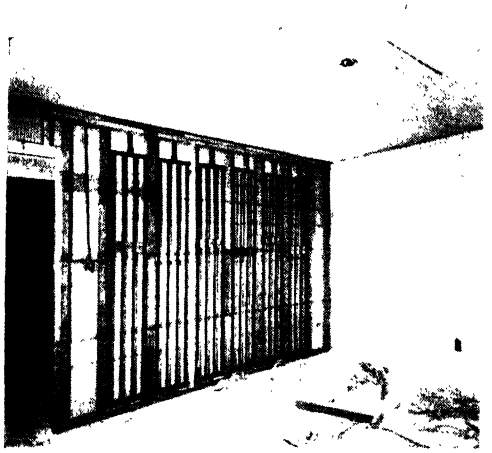


Pan-L-Heat Corporation

Manufacturers of **PAN-L-GRID** *for Radiant Heating*

2838 N. E. Columbia Blvd., **Portland 11, Oregon**

Factory Representatives in SEATTLE, WASH.; SPOKANE, WASH.; SALT LAKE CITY, UTAH; SAN FRANCISCO, CALIF.; LONG BEACH, CALIF.; AND PORTLAND, OREGON.



Inside Walls

Outside Walls

TYPICAL PAN-L-GRID INSTALLATIONS

4-7 or 4-6 Grids for 16 in. Stud and joist spacing.

3-7 for 12 in. stud and joist spacing.

4-10-2 and 4-10-3 developed for concrete installation.

Engineers, Architects and Contractors are specifying **PAN-L-GRIDS** because they are less costly and more applicable to installations for warm water heating systems.

PAN-L-GRIDS are being used with equal satisfaction in ceiling, wall or floor radiant heating and cooling systems.

Capacity ratings for each size of **PAN-L-GRIDS** have been determined by laboratory tests conducted by licensed Engineers. 8,000 PAN-L-GRIDS have been installed and are producing very satisfactory results based on these ratings. PAN-L-GRIDS are installed in various types of buildings and in climatic conditions ranging from design temperature of plus 30F. to minus 20F.

The **PAN-L-GRID** incorporates an orificing principle which insures equal distribution of flow through the grid.

PAN-L-GRIDS are BONDED for the users' protection. **PAN-L-GRIDS** are manufactured in sizes to fit standard building construction.

Tube—½ in. Standard Black Steel Butt-weld Pipe. Headers—1 in. Standard Black Steel Butt-weld Pipe. These sizes apply to the 6 ft and 7 ft models of the Grid. On the 10 ft Grid the tubes are either ½ in. or ¾ in. and the headers 1 in. or 1¼ in. respectively. The Grid is an all electric-weld unit furnished with standard ½ in., female I.P.S. screwed end connections. We can furnish all of these Grids in Byers genuine wrought iron pipe at a higher price if so desired by customer.

STANDARD GRID DIVISIONS

Grid Size	Nominal Length	Overall length	Overall Width	Overall Thickness	Shipping Weights
4 x 7′	7′–0″	7′–4″	1′–1¼	0′–1 5/16″	28 lb 10 oz
3 x 7′	7′–0″	7′–4″	0′–9¼″	0′–1 5/16″	20 lb 9 oz
4 x 6′	6′–0″	6′–4″	1′–1¼″	0′–1 5/16″	24 lb 11 oz
4 x 10′ x ½″	10′–0″	10′–4″	2′–2″	0′–1 5/16″	43 lb 10 oz
4 x 10′ x ¾″	10′–0″	10′–4″	3′–2½″	0′–1⅝″	59 lb 13 oz

For further information, ratings, engineering data, catalogs and installation details—write **PAN-L-HEAT CORP.** *or contact your nearest representative.*

Taco Heaters, Incorporated

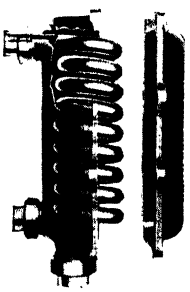
342 Madison Avenue, **New York 17, N. Y.**

TACO HEATERS OF CANADA, LTD., 24 Adelaide St., W., **Toronto**

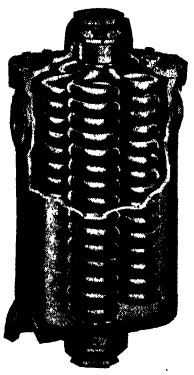
THERE is a storage or tankless, Biltin or external, type Taco indirect water Heater for every job.

Biltin Taco Heaters, which are standard equipment on leading heating boilers, are catalogued only in the boiler catalogs. For additional information on Biltin Tacos write boiler manufacturer or Taco.

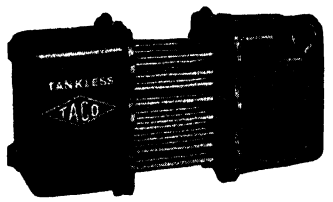
Complete catalog information on external Taco Heaters is also available for home, apartment house, hotel and housing projects.



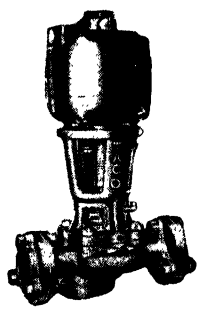
Domestic Tacos



Multi-coil Taco ←



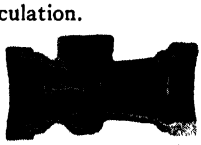
Tankless Taco Nos. 12, 14, 15, 18 and 23



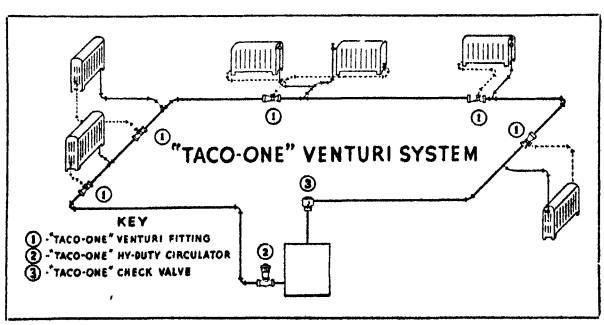
"Taco-One" Venturi System

A forced circulating warm heating system using a single pipe main from boiler to radiators and back again. Small pipes and one pipe main make a neater job, reduce installation costs. Radiators can be placed above and below main. 85 per cent of residential jobs need only one circuit which requires no balancing valves. This revolutionary heating system is made possible by the Taco Venturi Fitting and remarkable Taco Hy-Duty Circulator.

Taco Venturi Fitting—Acts as a suction pump in which the only moving part is water. Water does the trick by producing a vacuum pull that draws water through each radiator, giving positive uniform circulation.



Taco Venturi Fitting (Cross Section)

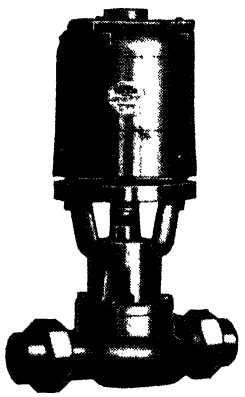


H. A. Thrush & Company

Peru, Indiana

Representatives in Principal Cities

FORCED CIRCULATING THRUSH FLOW CONTROL SYSTEM OF HOT WATER HEATING AND HEATING SPECIALTIES

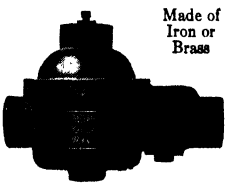


Patent Nos. 2,054,009, 2,111,441, 2,137,791, 2,207,183, 2,207,208, 2,257,867, 2,356,482 2,358,670

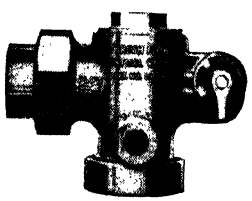
Flexible, economical of fuel, forced circulating Thrush Summer-Winter System of Hot Water Heat is the most satisfactory way to heat buildings. Thrush Systems, Water Circulators, Water Heaters, Pressure Relief and Pressure Reducing Valves and other fuel-saving heating specialties are available. Write today for information or engineering assistance.

THRUSH WATER CIRCULATORS

Five sizes, 1 in., 1¼ in., 1½ in., 2 in. and 3 in., for forced circulation in Hot Water Heating and Domestic Water Systems. Save fuel, insure uniform heating.



Made of Iron or Brass



Patent Reissue No. 19,873

THRUSH FLOW CONTROL VALVES

For use with Thrush Water Circulators

This patented valve prevents circulation when not required. Six sizes, 1 in., 1¼ in., 1½ in., 2 in., 2½ in. and 3 in. Work automatically by pressure head, generated by Thrush Circulator.

Number 4 Illustrated

THRUSH LOW PRESSURE WATER RELIEF VALVES

Protect heating boilers from excess pressures. Made in angle or straight types, of iron or brass, sizes ½ in., ¾ in. and 1 in. Unfailing dependability has been proved by over a quarter of a century of successful operation.

THRUSH PRESSURE REDUCING VALVES

Types for High and Low Pressures

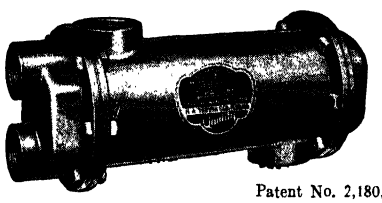
Sizes, ½ in., ¾ in. and 1 in. Low pressure reducing valves to reduce pressure of water entering heating system and maintain water supply in system automatically. High pressure reducing valves for protecting house plumbing and heating equipment from excessive city line pressures.

THRUSH AIR-TIGHT PRESSURE TANKS

An essential part of every hot water heating system. Conserves water and fuel, because the heated water expands into the Thrush Pressure Tank and returns to the system as it cools. Adds to the continued operating efficiency of the heating system over a long period of time.

THRUSH HIGH PRESSURE WATER RELIEF VALVES

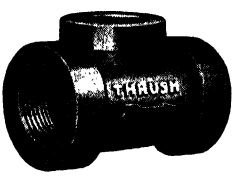
Protect water supply or range boilers and gas or electric water heaters from excess pressure and temperature (some types). Made in angle or straight types, of iron or brass, sizes, ½ in., ¾ in. and 1 in., for pressure relief only or combination pressure and temperature relief.



Patent No. 2,180,020

THRUSH WATER HEATERS

Highly efficient heat exchangers or converters. Sixteen sizes, for Hot Water or Steam. Pressure up to 150 lb water, 75 lb steam. Straight tubes readily cleanable. Provide Domestic Hot Water at low cost. Also used industrially for heating or cooling liquids.

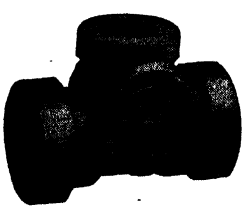


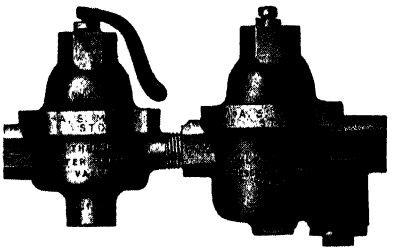
THRUSH SUPPLY TEES FOR ONE PIPE SYSTEMS NON-ADJUSTABLE

Assure positive diversion to radiators. Cast iron sizes, 1 in., 1¼ in., 1½ in. and 2 in., with branch outlets of ½ in., ¾ in. or 1 in. Also sweat copper sizes ¾ in., 1 in., 1¼ in. and 1½ in. all with ½ in. branch.

THRUSH ADJUSTABLE SUPPLY TEE FOR ONE PIPE SYSTEMS

Balances flow of water through each radiator, resulting in uniform heating. When branch flow is cut down, main flow is increased not retarded. Easily adjusted. Sizes in cast iron, 1 in., 1¼ in., 1½ in., and 2 in., with branch outlets of ½ in., ¾ in., and 1 in.

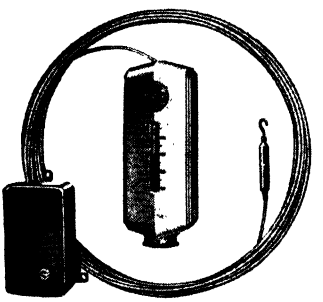




THRUSH DUAL CONTROL UNITS

Provide automatic pressure relief, reduce line pressure, automatically fill and maintain water supply in hot water heating system. Built-in strainer. Made in four types, brass or cast iron, ½ in. or ¾ in.

No. 201 THRUSH RADIANT HEAT CONTROL



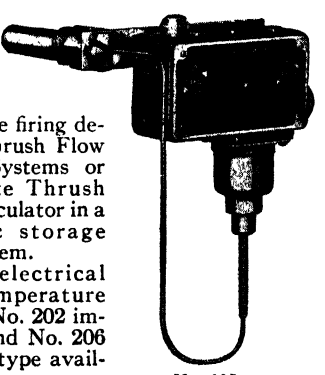
No. 200 *No. 201*

Automatically maintains room temperature within a fraction of a degree. Controls both room and water temperature in the radiators, compensating to prevent variation in room temperature or a lack of radiant heat. Requires No. 200 Thrush Relay Transformer for low voltage.

No. 205 THRUSH BOILER WATER TEMPERATURE CONTROL

No. 205 immersion control is used to operate the firing device of Thrush Flow Control Systems or to operate Thrush Water Circulator in a domestic storage water system.

Other electrical water temperature controls, No. 202 immersion and No. 206 clamp-on type available.



No. 205

WRITE FOR COMPLETE CATALOG

Buffalo Pumps, Inc.

450 Broadway, Buffalo, N. Y.

Sales Representatives in These Cities:

ALBANY 7, N. Y.—Mr. R. B. Taylor, 966 Broadway
ATLANTA 2, GA.—Mr. J. J. O'Shea, 305 Techwood Drive
BALTIMORE 2, MD., Mr. C. A. Conklin, III, 1014 Cathedral St.
BOSTON 76, MASS., Mr. E. D. Johnson, 507 Main St., Melrose Station
CHICAGO 6, ILL., Emmert & Trumbo, 20 N. Wacker Drive
CINCINNATI 2, OHIO, Mr. F. W. Twombly, 626 Broadway
CLEVELAND 13, OHIO, Mr. T. A. Weager, 418 Rockefeller Bldg.
KITCHENER, ONTARIO, Canada Pumps, Ltd., Mr. A. S. Capwell
DALLAS 1, TEXAS, Mr. T. H. Anspacher, 1801 Tower Petroleum Bldg.
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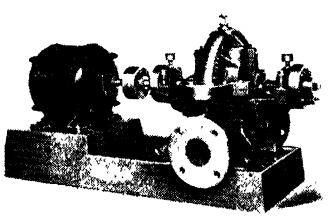
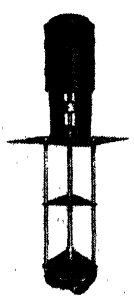
OMAHA 2, NEB., Wain Engineering Co., Mr. M. E. Wain, 375 Brandeis Theatre Bldg.
PHILADELPHIA 2, PA., Davidson & Hunger, 1200 Cunard Bldg.
PITTSBURGH 22, PA., Mr. H. L. Moore, 345 4th Ave.
SAN ANTONIO 6, TEXAS, Langhammer Rummel Co., 436 Main St.
SAN FRANCISCO 11, CALIF., Harry W. Parsons, Inc., 1214 Central Tower Bldg
SEATTLE 1, WASH., A. T. Forsyth Company 3150 Ellicott Ave
ST. LOUIS 3, MO., J. W. Cooper, 2118 Pine St.
TOLEDO, OHIO, Mr. C. M. Eyster, 1118 Madison Ave.
WASHINGTON 5, D. C., Mr. G. S. Frankel, 310 Woodward Bldg.

PRODUCTS—A Complete Line of Centrifugal Pumps For Use in All Types of Heating and Air Conditioning Installations. For Complete Information, Contact Your Nearest Buffalo Representative or Write Us.



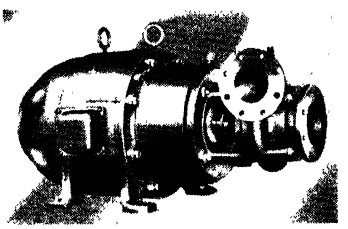
Buffalo Single-Stage Double Suction Pumps

Where installations require handling of 10 to 50,000 gpm, clear water, these pumps afford excellent service at low power cost and very little maintenance. They incorporate all accepted features of modern centrifugal pump design.



Buffalo Automatic Sump Pumps

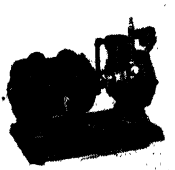
Distinct power savings are made possible with these Buffalo pumps, because their unusual efficiencies enable use of very small motors. A compact unit with ball bearing thrust and enclosed shaft.



Buffalo Close-Coupled Single Suction Pumps

Especially suited to handling hot water with low submergence on suction, these Buffalo pumps exert a high suction life. An important advantage in this type is its close coupling to the electric motor. This dispenses with bearings, assures permanent alignment and saves space. Easily serviced.

Buffalo Self-Priming Single and Double Suction Pumps



These centrifugal pumps provide a constant, positive prime without foot valves, with a primer under license from Nash Engineering Co. Featuring typical Buffalo design, the pumps have quiet, vibrationless rotors and fully accessible parts. Moving parts are above the liquid pumped.

Chicago Pump Company

2330 Wolfram Street **BRUnswick 4110** **Chicago 18**

PRODUCTS—Return Line Vacuum Heating and Boiler Feed Pumps, Condensation, House, Booster, Fire Pumps, Circulating, Brine, Sewage, Bilge, Sludge, Pneumatic and Tankless Water Supply Systems and Automatic Alternator for Duplex Sets of Pumps.

"CONDO-VAC"

Return Line Vacuum and Boiler Feed Pump for Heating Systems

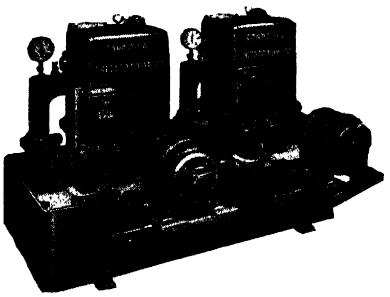


Fig. 2102—Duplex "Condo-Vacs" with Duplex Double Automatic Control

No vacuum on stuffing boxes, ample clearance in rotating member. It costs less to operate a "Condo-Vac." "Condo-Vac" reduces corrosion in piping and boiler to minimum—because pump does not take in air from atmosphere and entirely eliminates all air coming back from system. "Condo-Vac" is quiet, has a low inlet, entirely automatic, fool-proof, easy to maintain. *Ask for bulletin 270.*

Close-Coupled Pumps

Boiler Feed, Circulating, Tank Filling, Water Supply

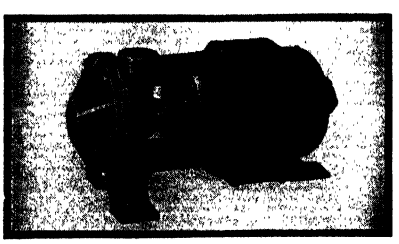


Fig. 2130—Close-Coupled, side suction pump

Capacities range from 3 to 600 Gpm against heads up to 189 ft. Motors from 1/6 to 20 Hp. Discharge 1 to 3 in. Closed and open type impellers. *Bulletin 108.*

"Sure-Return" Condensation Pump

for Low and Medium Pressure, and Systems up to 75,000 Sq Ft Radiation

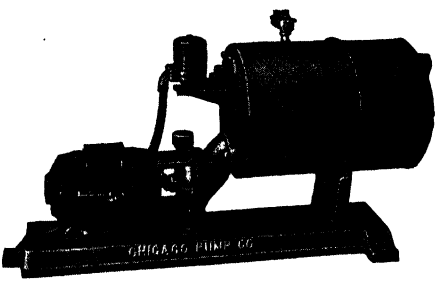


Fig. 1946

"Sure Return" Condensation Pumps and Receivers are built for systems up to 75,000 sq ft of direct radiation and for low and medium pressures. Built in either single or duplex units. Duplex units are alternated in their operation by the Automatic Alternator. *Complete data in Bulletin 250.*

Vertical Condensation Pumps

for Low and Medium Pressure for Systems from 500 to 100,000 Sq Ft Radiation

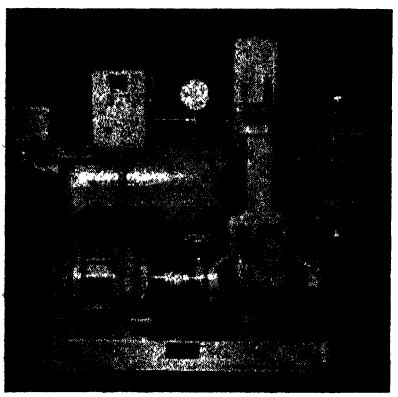
Fig. 1940 Vertical Condensation Pump

The vertical condensation pump is designed to receive returns from lowest radiation. The receiver is placed underground—an ordinary hole sufficing if necessary — and requires very little floor space. Unit is shipped complete, easy to install, assembled so as to prevent steam leaks. Special bearings will stand up under hot water for several years. A special float mechanism is guaranteed not to leak or stick in stuffing box. *Complete data and description in Bulletins 245, 253 and 255.*

The Nash Engineering Company

234 Wilson Road **South Norwalk, Conn., U. S. A.**

Sales and Service Offices in all Principal Cities

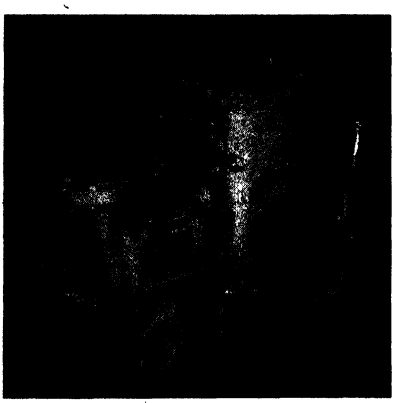


Return Line Vacuum Heating Pump

Standard with the heating industry for over eighteen years. Removes air and condensation from return lines of vacuum steam heating systems, discharging air to atmosphere and returning water to the boiler.

Two independent units are combined in a single casing—an air unit and a water unit. Impellers of both are mounted on the same shaft. Pump is bronze fitted throughout.

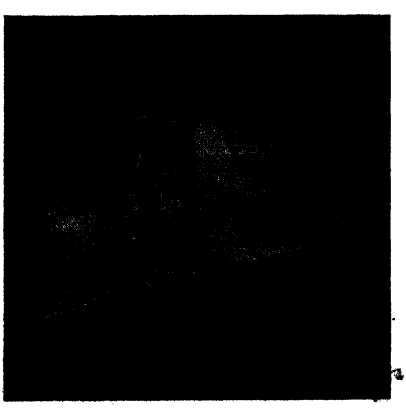
Supplied direct connected to standard electric motors, for belt drive, or for steam turbine drive. For continuous or automatic operation. Standard in capacities up to 300,000 sq ft E.D.R. Larger units special. Bulletins Nos. 307, 308, 309, and 310 on request.



Vapor Turbine Vacuum Heating Pump

Jennings Vapor Turbine Heating Pumps combine all advantages of the standard return line heating pump with a new type of drive, a specially designed low pressure turbine which operates directly on steam from the heating mains on any system, requiring a differential of only 5 in. of mercury, and returns that steam to the heating system with practically no heat loss.

This pump affords the safety and economy which goes with continuous condensation return and steady vacuum, and at no cost for electric current. Furnished standard in capacities up to 65,000 sq ft E.D.R. Larger units special. Bulletin No. 290 on request.



Condensation Pump and Receiver

Removes the condensation from radiators in return line steam heating systems, particularly radiators set below the boiler water line level, and pumps the condensation back to the boiler. Pump is bronze fitted with enclosed centrifugal impeller of improved design. By making the pump casing a part of the return tank, and bolting the motor base to the tank, floor space is conserved. The rectangular construction permits installation in a corner against the wall.

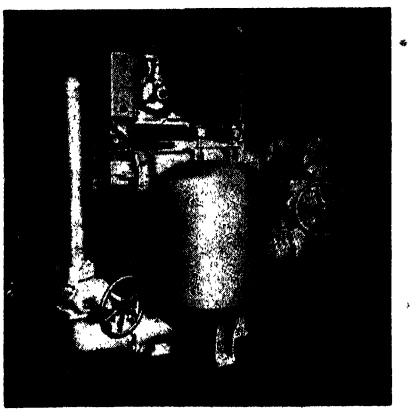
These pumps are furnished in standard sizes with capacities ranging from 1½ to 225 gpm of water. For serving up to 150,000 sq ft of equivalent direct radiation. Bulletin No. 319 on request.

The Nash Engineering Company

234 Wilson Road **South Norwalk, Conn., U. S. A.**

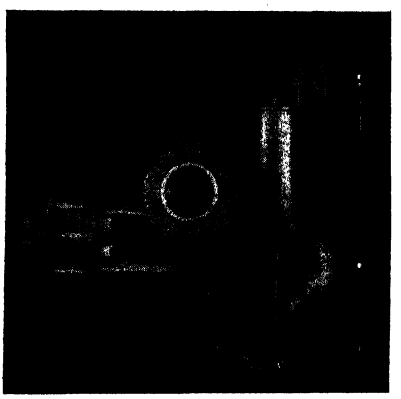
Sales and Service Offices in all Principal Cities

SEWAGE EJECTOR



For pumping unscreened sewage or drainage from basements below the street sewer level, handling crude sewage from low level districts, pumping effluent, sludge and other heavy liquids. The Jennings Sewage Ejector is of the pneumatic type. Air, compressed only to the pressure at which it is used, by a Nash Hytor Air Compressor, is motive power to pump the accumulated sewage from a pot to the sewer. There are no air storage tanks, reciprocating air compressors or screens, no air valves. Furnished in several standard sizes up to 1500 gpm against heads up to 100 ft. Bulletins on request.

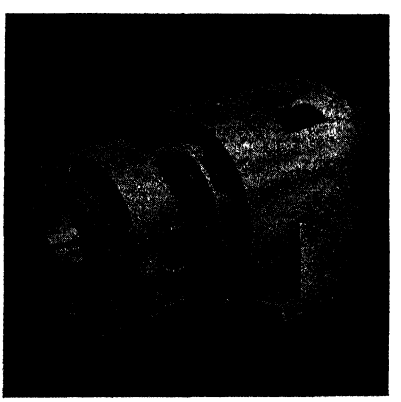
Suction Sump and Sewage Pumps



Jennings Sump Pumps are self-priming centrifugals for handling seepage water and liquids reasonably free from solids. Sewage Pumps are equipped with non-clog type impeller for liquids containing solids. Suction piping only is submerged. Centrifugal impeller and vacuum priming rotor are mounted on same shaft that carries rotor of the driving motor, forming a single moving element, rotating without metallic contact.

Will handle air or gas with liquid being pumped, and because of self-priming feature are installed entirely outside of pit, affording perfect accessibility for inspection or cleaning. Capacities to meet all requirements. Bulletins Nos. 159, 161, and 338 on request.

Air Compressor and Vacuum Pump



Nash Air Compressors operate on a unique and different principle. The one moving part rotates in casing without metallic contact. There is nothing to wear, and no internal lubrication.

Nash Compressors deliver absolutely clean air; ideal for agitation of liquids, pressure displacement, and handling gases. Vacuum pumps ideal for priming pumps, blood sucking pumps in hospitals, and wherever non-pulsating vacuum is required.

Pressure 75 lb or vacuum 27 in. of mercury. Furnished for any capacity; special for higher vacuums and pressures. Bulletins Nos. 282, 325, 331 and 337 on request.

Ingersoll-Rand

11 BROADWAY, NEW YORK 4, N. Y.

BIRMINGHAM, BOSTON, BUFFALO, BUTTE, CHICAGO, CLEVELAND, DALLAS, DENVER, DETROIT, DULUTH, EL PASO, KNOXVILLE, LOS ANGELES, NEWARK, NEW ORLEANS, NEW YORK, PHILADELPHIA, PICHER, PITTSBURGH, SALT LAKE CITY, SAN FRANCISCO, SCRANTON, SEATTLE, ST. LOUIS, TULSA, WASHINGTON

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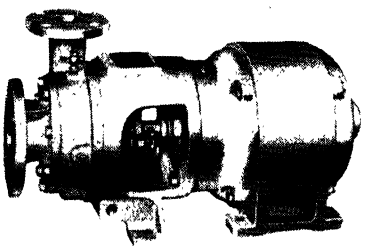
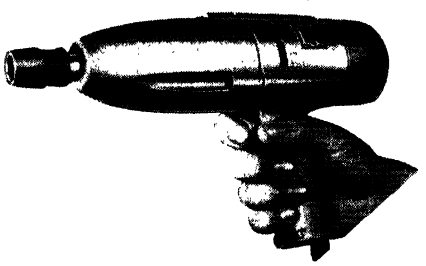


CENTRIFUGAL PUMPS

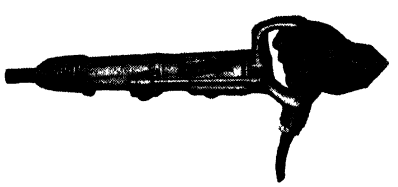
The MOTORPUMP is a compact, "package" unit, mounted integrally with motor on a rigid, oversize shaft and oversize bearings. It is highly adaptable to many services, needs no special foundation, and operates equally well in any position. It is available in several materials for pumping various liquids. Capacities from 10 to 1800 gpm, heads to 600 ft.

Other I-R pumps are offered for all hydraulic services, with any type of drive.



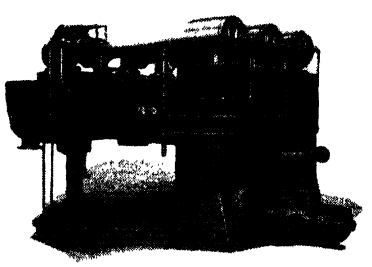
ALL PURPOSE PORTABLE TOOL

The 4U Electric Impact Tool is a lightweight, portable, tool for running and removing nuts, screws and studs, drilling, reaming, tapping, wire brushing, drilling brick and masonry, driving wood augers, hole-saw work, and the 101 jobs encountered in installation work. Plugs into any wall outlet. Capacities: ¼ in. drills, step-reaming to ½ in., running nuts to ⅜ in. thread size. 110 and 220 volts, 25 to 60 cycles universal motor.



LIGHT-WEIGHT JACKHAMER

The J-10 Jackhamer is the smallest of the self-rotating, rock-drill line, weighs 14 lbs. and is especially designed for maintenance and installation work. Its uses include drilling masonry for conduit, sprinkler hangers, foundation bolt holes, pipelines and drains as well as tearing out brickwork for doors and windows and similar demolition jobs. The J-10 is air-powered.



STEAM-JET REFRIGERATION

Where refrigeration is needed down to 35F, and a supply of steam is available, the I-R system of water-vapor refrigeration with Steam-Jet Coolers is offered. In this system water is the only refrigeration medium. It is cooled by direct evaporation in a high vacuum created by steam-jet booster ejectors. There are no moving parts, no vibration nor noise. Sizes run from 20 to 1200 tons of refrigeration and can be built to operate at any one of a wide range of pressures down to 2 lb per sq in.

I-R COMPRESSORS OF ALL TYPES AND SIZES

I-R Compressors are offered in all sizes and types from ½ to 3000 hp, in pressures from a few ounces to 15000 lbs, and in stationary or portable models. Air-cooled units range from ½ to 90 hp. I-R Water systems are available for industrial and domestic uses.

INTERNATIONAL HEATING & VENTILATING EXPOSITION
THE AIR CONDITIONING EXPOSITION

Permanent Address—Grand Central Palace, **New York 17, N. Y.**

EXPOSITIONS HELD

New York, 1948; Cleveland, 1947-1940; New York, 1938; Chicago, 1936; New York, 1934; Cleveland, 1932; Philadelphia, 1930.

1949 IN CHICAGO

The Ninth Air Conditioning Exposition will be held at the International Amphitheatre, Chicago, Ill., January 24 to 28, 1949. This promises to be one of the largest ever held and is in accordance with previously announced plans to hold the Exposition annually through 1950.

These Expositions continue to provide a valuable service to the industry by offering common meeting places where newest developments may be personally demonstrated and problems may be discussed with technical personnel. Every phase of air conditioning is covered—heating, cooling, piping, ventilation, humidification and dehumidification for industrial and commercial establishments as well as homes.

UNDER AUSPICES OF A.S.H.V.E.

These Expositions have been and will be held co-incident with the annual meetings of the American Society of Heating and Ventilating Engineers and under their auspices. Management is by International Exposition Company with permanent headquarters at Grand Central Palace, New York 17, N. Y.

EXHIBITORS

Comprise leading firms in each phase of the industry; number has varied from 150 to 400 exhibitors.

EXHIBITS

These range from and comprise all the types of articles discussed or advertised in this copy of THE A.S.H.V.E. GUIDE.

1. *The* COMBUSTION *Group:* Furnaces, burners (coal, oil and gas), grates, stokers, boilers, radiators (various types), refractories and auxiliaries.
2. *The* OIL BURNER *Group.*
3. *The* HYDRAULIC *Group:* Water feeders, water heaters, pumps, traps, valves, piping, fittings, expansion joints, pipe hangers, etc.
4. *The* STEAM HEATING *Group:* Vapor heating and steam specialties.
5. *The* HOT WATER HEATING *Group.*
6. *The* AIR *Group:* Warm Air furnaces and stoves, registers and grilles, cooling towers, air filters, motors, fans, blowers, conditioning equipment, ventilators (room and industrial types), unit heaters, etc.
7. *The* AIR CONDITIONING *Group:* Equipment which circulates and filters the air, in summer dehumidifies and cools; in winter heats and humidifies, and does all these in proper season for complete, all year-round air conditioning.
8. *The* CONTROL *Group:* Instruments of precision for indicating, controlling or recording temperature, pressure, volume, time, flow, draft or any other function to be measured.
9. *The* REFRIGERATING *Group:* Compressors, condensers, cooling apparatus, contingent apparatus and refrigerants.
10. *The* CENTRAL HEATING *Group:* Apparatus and materials especially designed or adapted to the uses of central heating and central heating station supplies.
11. *The* INSULATING *Group:* Structural insulators (refractory and cellulose materials), asbestos, magnesia clays and combinations thereof, pipe and conduit covering, etc., weather-stripping, etc.
12. *The* MISCELLANEOUS *Group:* Electric Heaters, boiler and pipe repair alloys, liquids and compounds, tools of all kinds, and equipment not specifically included in the above groups, but related thereto.
13. *The* MACHINERY AND GENERAL EQUIPMENT *Group.*
14. BOOKS AND PUBLICATIONS.

VISITOR ATTENDANCE

Attendance is by invitation and registration only, thereby presenting a selected audience. Included are contractors, dealers, jobbers, supply houses, home owners, industrial users, professional and service organizations, public utilities, real estate management concerns, etc. A detailed analysis of registered attendance is available on request. In 1948 at New York, there were 50,000 registered visitors.

Industrial Expositions in America lead the expositions of the world in style, business effectiveness, industrial influence and educational value. This Exposition stands among the leaders in Industrial Expositions in America. It is an educational institution which brings together the research developments and improvements in equipment and materials for use in heating, ventilating and air conditioning all types of buildings.

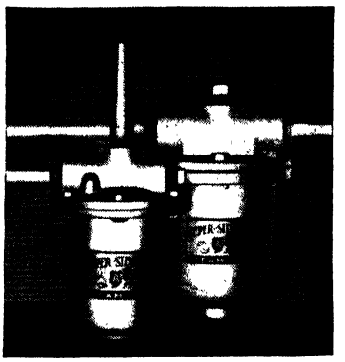
The V. D. Anderson Company

1942 West 96th Street, **Cleveland, Ohio**

Representatives in all principal cities

SUPER-SILVERTOP STEAM TRAPS

Are inverted bucket steam traps of an improved, thoroughly tested design. These steam traps automatically remove both condensate and air from the steam system—no manual operations are necessary.



Shows how trap is installed either as an elbow or straight in-line, using a minimum of fittings.

APPLICATIONS

Super-Silvertops are used on any steam-using equipment where it is desired to remove condensate and air automatically in order to produce maximum heating efficiency.

FEATURES

Simplified Piping—Connected either as an elbow or straight-in-line—only one nipple needed since the U-tube is inside the trap. Saves as much as three elbows, three nipples and 60 minutes of time, compared to other inverted bucket steam traps.

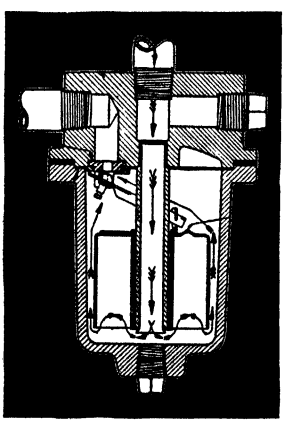
Precision Parts Alignment—The bucket does not swing free. It is controlled in true engineering fashion, guided on a hexagonal tube. This makes a knife-edge contact, eliminating almost all friction. The unusual guide arrangement keeps all parts in proper alignment and prevents the bucket from hitting the sidewalls of the case. Positive closing of the valve is insured.

Self-Cleaning—The reversing of the condensate flow on entering the trap produces a scrubbing action. This stirs up any sediment and dirt which is then carried away in the discharging condensate.

No Restricting Passages—Even in the smallest sizes there are no narrow cored passages to become clogged with scale.

Cannot Air-bind—As the air is automatically discharged ahead of the condenaste in each cycle of operation.

Vacuum or Pressure—These traps do not leak steam. No danger of vacuum being destroyed—trap is recommended for vacuum operation.



Materials: Case and head are of nickel semi-steel, bucket is copper, guide tube of admiralty bronze, valve and seat of special chrome alloy, all other parts of stainless steel. All interior parts can be furnished in stainless steel when so ordered.

INSTANT HEAT

Anderson Super-Silvertops can be equipped with Thermal Air Eliminators where instant heat is desired. **Other Anderson products are:** combination open float and thermostatic steam traps, float-type steam traps, air release valves, and pipeline strainers.

SIZES, LIST PRICES AND CAPACITIES

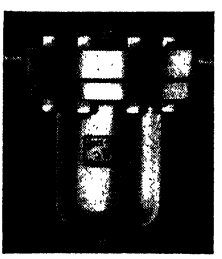
No. of Trap	10	19	20	21	22	23	24	25
Code Word for Telegrams	Val.	Vys.	Vyt.	Vol.	Vil.	Viz.	Vet.	Vas.
Pipe Connections, In. (See Note)	½ only	½ or ¾	½ or ¾	½ or ¾	¾ or 1	¾ or 1	1 or 1¼	1½ or 2
Shipping Weight, Lb'.	2¾	6	7	8	14	16	38	75
Diameter, In.	3 7/16	3 3/8	3 3/8	4 15/16	5½	5½	8 6/16	9¾
Height, In.	3 15/16	5 3/4	6 9/16	6 3/4	8 1/16	10 3/16	13 11/16	17 5/8
Maximum Gauge Pressure	125	200	200	200	250	250	250	250
List Price	$ 8.00	$10.00	$12.00	$14.00	$23.00	$32.00	$45.00	$60.00
Chrome Plated	10.00	12.00	.....	.....	.....	.....	.....	.....

WITH THERMAL AIR ELIMINATOR

Code Word for Telegrams	Valel	Vysel	Vytel	Volel	Vilel	Vizel	Vetel	Vasel
List Price	$9.60	$11.60	$13.60	$15.60	$26.20	$35.20	$49.80	$66.40

Differential Pressure	CAPACITY IN POUNDS OF WATER PER HOUR							
1	200	215	390	775	1050	1500	2400	9200
2	285	305	535	1100	1500	2100	3300	13200
3	320	340	665	1350	1800	2500	4100	16000
4	410	440	815	1500	2100	2900	4500	18500
5	475	505	970	1700	2300	3200	5274	21000
10	600	640	1125	2000	3200	4600	7500	29650
15	330	745	1380	1750	3300	5400	10000	30475
20	375	800	1500	2000	3500	6000	11100	40300
30	450	550	1060	1300	3500	4500	6200	48600
40	400	600	1115	1500	2800	5000	7000	23400
50	450	700	1275	1600	3100	4500	7500	26000
60	325	640	1040	1300	3250	4900	8000	20000
70	350	670	1115	1375	2700	3541	8000	21500
80	375	700	1150	1500	2800	3750	8600	23000
90	255	645	1120	1550	2900	3950	9100	24000
100	275	675	1200	1600	2450	4200	10000	25300
125	300	700	1275	1700	2900	3400	8000	19100
150	....	550	970	1200	2000	3700	8600	20500
200	....	630	1000	1300	2200	4150	8900	16800
225	....	....	....	....	1800	4400	9200	13300
250	....	....	....	....	1900	4500	9600	13750

Capacities based on continuous flow. When ordering be sure to specify maximum steam pressure.
Note: Pipe sizes shown in **heavy type** are standard and traps will be shipped tapped standard unless otherwise specified. Pipe sizes shown in light type furnished at no additional, cost but only from Cleveland stock.



SUPER-SILVERTOP STEEL SERIES

. . . for higher pressures and temperatures —come complete. No need for extra, expensive fittings, no pipe to bend, and no labor cost for making up extra pipe joints. Installation may be straight-in-line or as an elbow. Only two threaded joints required in either installation. The case and head are made of steel; and the gasket joints are of the recess type, preventing any possibility of gasket blowouts; all interior parts are stainless steel, except the valve and seat which are special chrome alloy.

CAPACITIES AND LIST PRICES

	No. of Trap		
Size	33	34	36
List Prices	$77.00	$120.00	$230.00
Code Word	FSH	FSB	FSC
Pressure, Lbs.			
150	2800	6000	11000
200	3100	5500	9000
250	3500	6000	10000
300	2500	6400	11000
350	2800	4500	8300
400	2500	4500	8700
500	2800	4750	9000
600	3000	4900	8500
700	2000	4500	8500

Barnes & Jones
INCORPORATED

129 Brookside Avenue **Boston 30, Mass.**

New York Office: 101 Park Avenue

Barnes & Jones Vapor and Vacuum Systems of Steam Heating; Modulation Valves; Adjustable-Orifice Radiator Valves; Packless Quick-Opening Radiator Valves; Thermostatic Radiator Traps; Thermostatic Trap Replacement Units; Condensators (Boiler Return Traps); Float and Thermostatic Traps; Strainers; Damper Regulators; Gages; Systems of Zone Control for Steam Heating. Complete Catalog on Request

Series K

The Series K valve is of the modulating type equipped with dial and pointer to indicate whether the valve is open or shut or in an intermediate position. Lever or wheel handle.

Series F

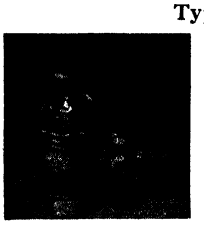
The Series F valve has no dial or pointer and is therefore furnished only with wheel handle or lock shield. Of same quality as Series K but lower priced.

Both Series K and Series F valves are quick opening, non-rising stems, renewable disc seats, of packless design. Made angle pattern in ½, ¾, 1 and 1¼ in. sizes; straightway (globe) pattern in ¾ and 1 in. sizes. For use in vapor or vacuum systems.

Capacities—Sq Ft E. D. R.

Size valve	½"	¾"	1"	1¼"
2 ounces pres.	25	50	90	160
8 ounces pres.	45	90	160	280

Type H



The Type H valve is of the adjustable orifice type so arranged that the dial indicates at all times the size of the radiator for which the valve is adjusted.

May be adjusted with steam on the system. Noiseless in operation.

Lever or wheel handle, unauthorized tampering virtually impossible. Made for pressure differentials of 1, 2, 3, 4 and 5 pounds, ¾ in. valve up to 100 sq ft. 1 in. valve over 100 sq ft.

Thermostatic Radiator Traps

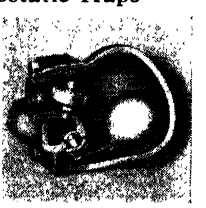
The B & J precision made thermostatic trap contains the unique, patented cage unit which is a complete operating unit in itself. The cage assembly contains the double thermostatic element calibrated in the factory, and locked in correct adjustment with the trap seat, which is also an integral part of the cage unit. Suitable for pressures up to 15 lb.

Capacities—Sq Ft of E. D. R.

Size	No.	Pres. Diff.—Lbs. per Sq In.					
		⅛	¼	1	2	5	15
½	122	70	92	168	228	320	610
¾	134	120	152	320	450	710	1260
1	147	200	300	590	760	1200	2200

Medium and High Pressure traps suitable for pressures between 15 lb and 100 lb can be furnished.

Float and Thermostatic Traps



Made in five sizes for handling large and sudden loads of condensate that are greater and more variable than can be handled efficiently by thermostatic traps. Suitable for pressures up to 15 lb.

Capacities Lbs Water per Hour

Size	No.	Pres. Diff.—Lbs. per Sq In.				
		¼	½	2	5	15
¾	T41	70	100	200	210	230
1	T42	175	250	500	525	575
1¼	T43	425	600	1200	1260	1380
1½	T44	850	1200	2400	2520	2760
2	T45	1775	2500	5000	5250	5750

Medium pressure F. & T. traps in ¾ in. and 1 in. sizes can be furnished for pressures up to 65 lb.

Barnes & Jones, Inc., manufactures a complete line of control systems operated either manually from a central station or automatically from an outdoor thermostat.

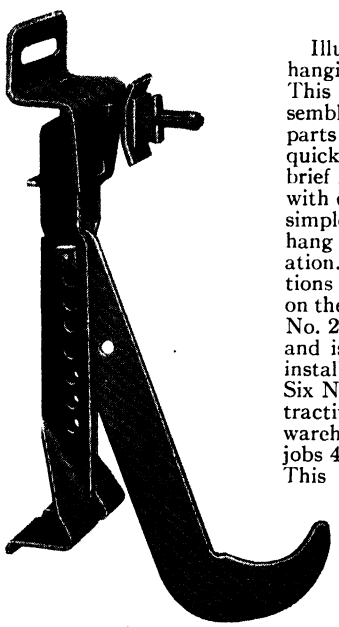
Carty & Moore Engineering Co.

Established 1919

511 West Larned Street **Detroit 26, Mich.**

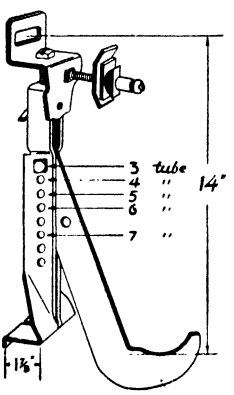
STEEL RADIATOR BRACKETS **STEEL CONCRETE INSERTS**

For over a quarter of a century Carty & Moore Brackets have been recognized by engineers and contractors as a superior product and there are nearly a million in use today. Specify them on your next job and watch labor costs drop because of quick and easy installation—they won't let you down!



MODEL NO. 22 BOTTOM HUNG RADIATOR BRACKETS

Illustrated is the No. 22 Universal Radiator Bracket for hanging all types of wall, tube or slender-tube radiation. This bracket is completely assembled when shipped and all parts are furnished, ready for quick and easy installation. A brief instruction card is enclosed with each bracket to explain the simple adjustments required to hang any particular type of radiation. Roughing-in specifications are shown by the drawing on the right. Because the Model No. 22 is completely assembled and is so simple to adjust, it cuts installation time to a minimum. Six No. 22's packaged in an attractively labeled carton for warehouse purposes—for specific jobs 40 brackets to a burlap bag. This bracket is also available with double hook and reinforced frame for double row wall radiation—specify No. 222.

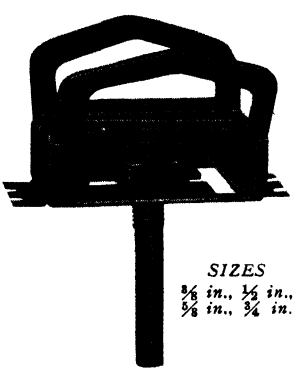


MODEL NO. 33 TOP HUNG BRACKETS

A completely assembled top hung hanger with 1¾ in. outset from the wall, especially approved for government jobs. Also available with 2⅞ in. outset for hospitals, institutions, etc. where frequent cleaning behind the radiator is required—specify No. 333. When ordering top hung brackets, specify model number and the type of radiation to be hung.

MODEL NO. 44 CONCRETE INSERTS

Carty & Moore No. 44 Concrete Inserts have long been used by leading heating contractors and are designed to meet the most exacting requirements. The C & M Insert is made of heavy gage pressed steel stampings and is strong and dependable. A long travel slot permits ample adjustment yet the nut cannot pull out and the wide wingspread allows the insert to become deeply imbedded in the concrete so it cannot tear out or loosen even under a heavy strain. Packed in nicely labeled cartons, 50, ⅜ in. or ½ in. to a box; 25, ⅝ in. or ¾ in. Sheets giving complete specifications will be sent on request.



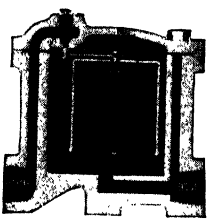
SIZES
⅜ in., ½ in., ⅝ in., ¾ in.

The Clark Manufacturing Company

1830 E. 38th St., **Cleveland 14, Ohio**

Established 1908

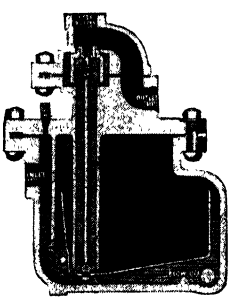
Clark, manufacturers of steam specialties for 39 years, produces a complete line of fluid controls. They are engineered for the jobs required of them, such as heating and air conditioning and wherever air, steam or gas is used.



(Series 70)

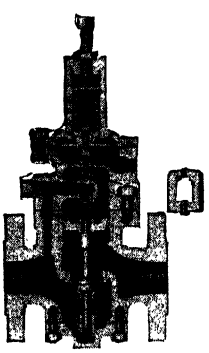
Inverted Bucket Traps are of three general sizes: (1) small, for general drainage service (2) for greater capacity (3) for high pressure and temperatures. The combination inverted bucket and blast type (Series 70-T) has a built-in thermal-by-pass to rapidly bring systems up to operating temperature by fast elimination of air and condensate.

The Clark Patented Bucket Venting Device provided in top of bucket furnishes the means of relieving the accumulated steam and air within the bucket.



(Series 80)

Open (Upright) Bucket Type used for general drainage—are available in Semi-Steel to 250 psi and Cast Steel to 400 psi. The discharge value is located at the top of the trap for easy inspection and can be replaced without removing trap from the line or breaking pipe connections.Th ey are equipped with "Clark-loy" ball type disc and seat.



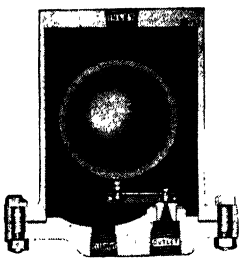
(Series "CRV")

"CRV" Pressure Regulator is integral pilot controlled—piston operated single seated type. It is suitable for operation at initial pressures and temperatures up to 250 psi and 450 F for cast semi-steel construction; 400 psi and 600 F for cast steel construction wherever steam, air or gas is used.

Steam Capacities (In Lbs. per Hour) of Clark "CRV" Regulators, at Various Initial Pressures

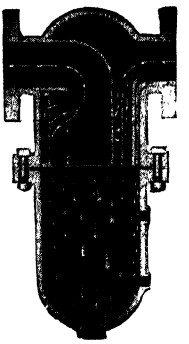
Initial Pressure	½ in.	¾ in.	1 in.	1¼ in.	1½ in	2 in.	2½ in.	3 in.
30	100	210	345	580	1000	1500	2500	4000
50	120	295	500	815	1120	2000	3500	5000
100	190	500	1000	1500	2500	4000	6000	8000
150	270	910	1180	2000	3500	5000	8000	10000
200	500	1500	1525	3000	4000	7000	10000	15000
250	560	2000	2200	3500	5000	8000	12000	20000

Air Traps—Automatically drains water from air lines, air receivers, drip pockets, aftercoolers, etc. Also adaptable for draining non-corrosive liquids from lines or equipment carrying vapors, such as steam and various kinds of gases.



No. 440

Separators—Effectively separates, collects and removes condensate and entrained moisture from lines conveying steam, air or other gases. This saves fuel. For there is more energy per pound in dry steam than in wet.

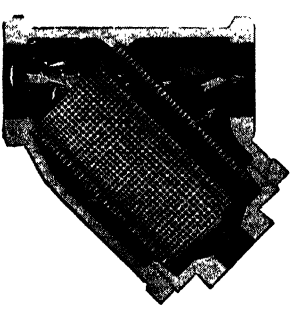


Horizontal HCT & HCT-S

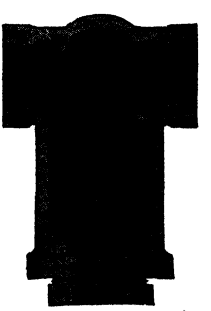
Trap Nos.	Std. Pipe Conn.	Opt. Pipe Conn.	List Price	Wt. Lbs	Continuous Flow Capacities of Condensate in Lbs per Hour For Various Sizes at given Differential Pressure Ratings.										
					10	30	50	75	125	150	200	250	300	400	600
70	1/2	3/4	$ 8.00	6	760	1290	1060	775	685	515	375				
72	1/2	3/4	10.50	9	945	1760	1615	1250	955	730	580				
73	3/4	1	15.50	10 1/2	1600	2600	2230	1900	1230	1025	850				
70T	1/2	3/4	11.00	7		1290	1060	775	685	515					
72T	1/2	3/4	13.50	10		1760	1615	1250	955	730					
73T	3/4	1	18.50	11 1/2		2600	2230	1900	1230	1025					
80	1/2	3/4	17.00	15		3800		1900	1560	1330		900			
81	3/4	1	22.50	26		8100		5900	3300	2940		2070			
82	1	1 1/4	30.00	39		1600		8800	6100	5320		3700			
83	1 1/4	1 1/2	37.00	48		21200		14000	10200	9430		6500	*Cast Steel		
84	1 1/2	2	55.00	77		35950		21700	15400	12875		11000	Series		
85	2	2 1/2	73.00	117		76000		42000	32000	29300		20000			
30	1/2		22.50	42	3000	2600			1230			625			
31	3/4		28.00	48	4200	4300			1560			900	680*	485*	
32	1		34.00	75	11080	6900			2750			1250	1335*	1080*	
33	1 1/4		47.00	175	21000	14500			6100			3750	3400*	2460*	
34	1 1/2		60.00	150	28000	19200			8700			5000	6900*	3145*	
35	2		85.00	210	48000	27500			12100			7350	14600*	5100*	
36	2 1/2		120.00	330	6000	54200			27300			14500	14600*	11500*	
800**	1/2	3/4	55.00	34					1230		850		680	485	
801**	3/4	1	68.00	57					2750		1900		1335	1080	860
802**	1	1 1/4	90.00	93					5500		4600		3400	2460	1730
803**	1 1/4	1 1/2	125.00	150					9500		6700		5700	4200	2820
804**	1 1/2	2	150.00	215					14300		10600		7800	6000	4200

**The 800 series shown here are the screwed type. Information on the flanged and extra heavy models is available upon request.

Strainers—Both the "T" and "Y" can be installed in steam, air, water and other fluid lines to remove dirt, scale, grit from fluid flow, protecting working parts of control valves. There is no appreciable pressure drop because of the straight thru flow. The blow-off connection at the bottom permits easy removal of collected dirt. Screen area is considerably greater than that of the pipe.



"Y" Strainer



"T" Strainer

C. A. Dunham Company

Administrative and General Offices

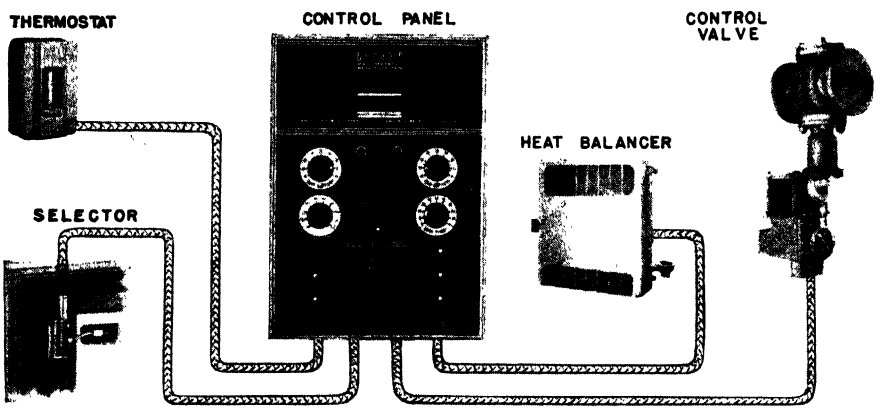
400 W. Madison Street, **Chicago 6, Ill.**

Factories: MARSHALLTOWN, IOWA; MICHIGAN CITY, IND.; TORONTO, CANADA; LONDON, ENGLAND
TORONTO 4, 1523 DAVENPORT ROAD. **LONDON,** LOMBARD RD., MERTON, S.W. 19

THE DUNHAM DIFFERENTIAL VACUUM HEATING SYSTEM

Fully Automatic

"Dunham Heating Service," as close to you as your telephone in most principal cities, see classified telephone directory. Expert heating engineers are available to architects and engineers for counsel at every one of these offices.



The Control Panel is the centralized operating station at which all control adjustments and settings are made and from which remote readings of room temperatures, control valve openings and percentage of heat output as measured by the Heat Balancer may be obtained. The Temperature Control Equipment appraises the heat demand of the building utilizing the resistance thermometer principle of operation. The Resistance Thermometers comprise coils of metal conductors whose electrical resistance varies with variations in their temperature connected in a Wheatstone Bridge circuit. Such temperature sensitive elements have no moving parts. All moving parts are contained in the Panel and in the Control Valve.

The basic control of the Differential Temperature Control Equipment balances the heat supply (measured by the Heat Balancer) with the heat demand (measured by the Selector). Compensating or limiting features are provided by the room Resistance Thermometer units. Since this room thermometer is not depended upon to perform the function of the conventional room thermostat, it is not as limited in its application. It can be used to register room temperatures from any location regardless of the type of occupancy of the room.

DUNHAM THERMOSTATIC TRAPS

For Operating Pressures up to 15 lb psi gage

The ½ in. trap is available in AP, RH, LH, SW, and vertical patterns. The ¾ in. in AP, SW only. The 1 in. in AP only.

Construction—Bodies, covers, nut and nipple are of brass, valves and seat are cast bronze. The trap is non-adjustable, permanent adjustment for correct operation is built into the element. The thermostatic elements for traps of the same size are interchangeable without adjustment. The disc is made from Monel Metal sheet. The cor-

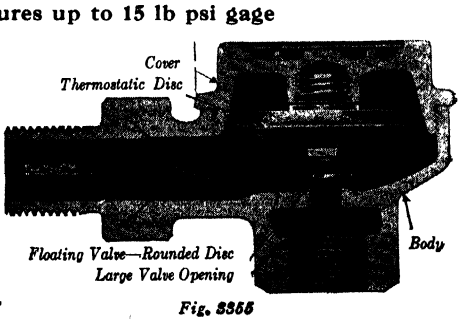


Fig. 8556

rugations are shaped to reduce hinge action at the rim of the disc and to distribute disc motion uniformly. The filling nozzle and the valve assembly are attached to their respective halves of the disc by threaded nuts making tight screwed joints which are further reinforced, locked and sealed by sweating with solder. The valve is flat and is attached to the disc by a ball swivel joint to insure its seating squarely and tightly. Valve opening is exceptionally large and the passage of water or dirt out of the trap is not obstructed by a guide as none is necessary with the Dunham design. Valve seat is raised slightly and rounded to minimize the depositing of incrustants.

DUNHAM THERMOSTATIC STEAM TRAPS—TYPE TH

For Working Pressures 25 Lb to 100 Lb

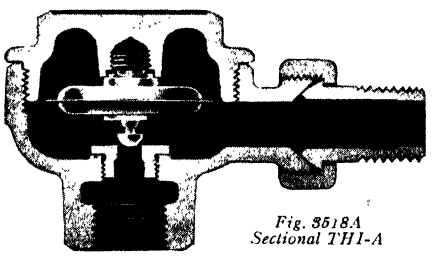


Fig. 3518A
Sectional TH1-A

Construction—Type TH traps are the thermostatic fluid expansion type.

The trap consists of two principle parts, a body with renewable valve seat and a cover containing the thermostatic element. Permanent adjustment for correct operation is built into the element. The covers may be removed from the trap body while hot without danger to the thermostatic element. The valve is swiveled to insure its seating tightly without causing localized stresses on the element. Body, cover, nut and nipple are of brass; valve and seat are of special heat treated stainless steel; thermostatic element is formed from monel metal sheet. Capacity lbs condensate per hour Type TH1A 1200 to 2600; Types TH2A and TH3A 1800 to 4500.

DUNHAM RADIATOR VALVES

"ORIFLEX" PACKLESS RADIATOR VALVE

Type 175 Oriflex self-contained adjustable orifice valve combines the conveniences of both lever and wheel handle valves. The adjustable orifice within the valve controls the steam flow. Oriflex eliminates the time consuming operations of disconnecting and re-connecting the valve in order to balance a system. Merely remove the handle, insert the key on the adjustment stem thus made accessible, adjust the orifice (calibrated guide surrounds stem) to the exact setting needed for perfect balance. Instead of being limited to orifices calibrated in steps of five square feet, Oriflex provides for adjustments in increments of one square foot.

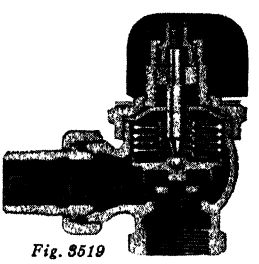


Fig. 3519

PACKLESS RADIATOR VALVE, SERIES 1140

Wheel Handle

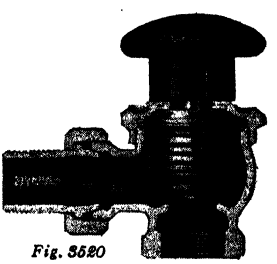


Fig. 3520

Suitable for all types of low pressure steam heating systems. The bellows construction, the non-rising stem, low bonnet, heat-resistant composition handle requiring less than one turn to open the valve fully, recommend this valve for services in which long-wearing quality, absolute tightness and attractive design are desired.

Bodies and bonnets are brass castings, rough finish. The valves are furnished with heavily constructed brass union nuts and nipples. The expansion member is the built-up type of bellows, fabricated from tinned phosphor bronze giving maximum resiliency and wear. The expansion member not only prevents leakage of steam, air and water, but also prevents steam, water and dirt from clogging and corroding the spindle nut and screw.

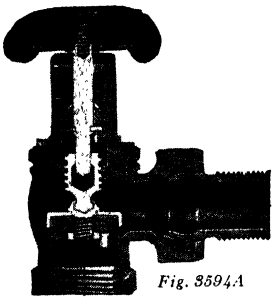
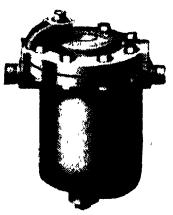


Fig. 3594A

740 SERIES DUNHAM RADIATOR VALVE

(Spring Packed)

Designed for low pressure steam heating service. Bodies are brass castings, rough finish. The valves are equipped with heavily constructed brass union nuts and nipples. All pipe threads and tappings are carefully machined and checked to standard gages. Non-rising stem, requires less than one turn of handle to open the valve fully. Dial shows direction and amount of opening. Heavy steel spring keeps a constant pressure on a special graphited asbestos composition ring to maintain a tight seal around the valve stem.



DUNHAM INVERTED BUCKET TRAPS

Type OB For Operating Pressures up to 250 lb
Type OBS For Operating Pressures up to 150 lb

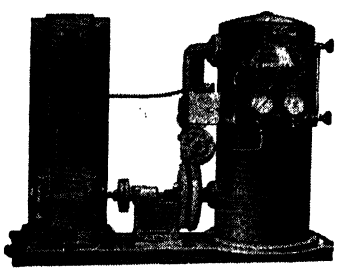
Type OB sizes are ½ in. to 1¼ in. inclusive, Type OBS made only ½ in. and ¾ in. sizes, right hand female tappings. Body and cover are of high test semi-steel castings and are provided with a plugged opening at the lowest point of the body. The valve and seat, which are renewable and interchangeable, are constructed of especially hardened, corrosion resisting steel. Bucket is formed from sheet copper. Cover cap screws are steel.

DUNHAM FLOAT AND THERMOSTATIC TRAPS

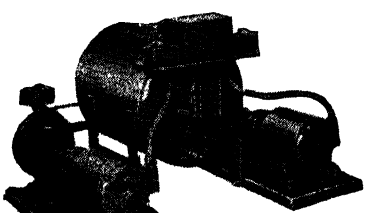
30 Series—For Operating Pressures up to 15 lb Gage

Trap is comprised of a cover and mechanism assembly and a body. Thermostatic disc and valve controls flow through a cored passage between the trap body and the discharge tapping for the release of air. The float is copper alloy. The float valve and seat are monel metal. Thermostatic elements are interchangeable. The trap body can be readily removed without disturbing piping connections to fully expose the working parts for inspection. Covers and disc Assemblies are interchangeable. Capacities, based on a rate of ¼ lb condensate per sq ft of EDR per hour, at a pressure difference between inlet and outlet of 2 lb gage, 800, 2000, 4800, 9600, 20000. Female right-hand threaded inlet and outlet. Connections ¾ in., 1 in., 1¼ in., 1½ in. and 2 in.

Dunham Closed Float Traps In Same Capacities



Type VR



DUNHAM PUMPS

Tested and Rated with A.S.H.V.E. Code.

Vacuum Pumps

Made in 9 sizes from 2500 to 65,000 EDR to be applied in accordance with EDR load, no allowance necessary for piping. Furnished as single or duplex units with a separate accumulator tank to take care of low returns. Each automatic pump has its own control panel wired through to motor. Selector switch on panel permits pump to operate on full vacuum and float control.

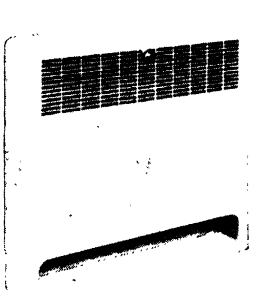
Pump and motor assembled on rigid cast iron base. Bronze fitted centrifugal pump has non-corrosive shaft. Enclosed type Impeller. Liberal size ball bearings.

Type CH-Model C, Single and Duplex—Capacities 2000 to 50,000 sq ft EDR discharge pressures 20 to 50 lbs; 60 cycle d.c. or a.c. 1750 rpm; 25 or 50 cycle a.c., 1450 rpm.

Type CHH-Model C, Single and Duplex—Capacities same as type CH. Discharge pressures 20, 30, 40, 50 and 70 lb. 60 cycle d.c. or a.c. 3450 rpm; 25 or 50 cycle a.c., 2850 rpm.

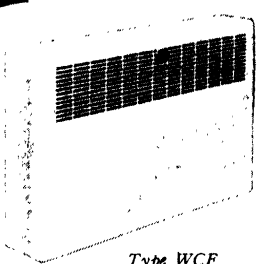
DUNHAM CABINET CONVECTORS
With Non-Ferrous Heating Element

Dunham Convectors can be used on steam or vapor, and gravity or forced hot-water heating systems. EDR capacities with 1 lb steam, 65° F entering air range from 12 to 108 sq ft EDR. Made in 4 in., 6 in., 8 in. and 10 in. widths; 20 in., 24 in., 32 in. enclosure heights; casing lengths from 18 in. to 64 in. Casings are constructed of No. 18 gage steel with removable fronts having rounded corners for pleasing appearance. The outlet grille consists of horizontal openings punched in the casing front. Dampers can be furnished when so ordered. Heating element is constructed of non-corrosive materials, copper or aluminum fins on seamless drawn, round copper tubes brazed to bronze headers. The tubes are expanded after assembly to assure intimate contact between fin and tube for permanent heat transfer. Heavy side plates protect the fins from damage. The elements are tested at a hydrostatic pressure of 400 lb per sq in. and are suitable for operation on 150 lb steam or water working pressure. Either end or top and bottom tapped headers (¾ in. I.P.S.) can be supplied.



Type FCF Convector

Heating Element



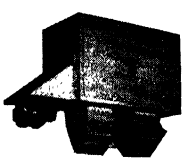
Type WCF Convector

DUNHAM UNIT HEATERS

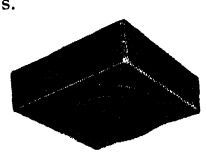
Types C and R are essentially industrial type units designed for heating large spaces. Type C, discharging large volumes of heated air downward to working levels, distributes heat evenly over large areas.

Type R—Wall Type

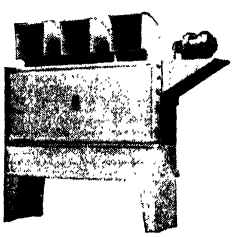
Type R—Ceiling Type



Type R—Inverted Wall Type



Type C—Built in various sizes up to 2000 sq ft EDR.



Type R—Floor Type with mixing damper also furnished with elongated nozzles

Type R is available in various types of mounting as shown. All units have belt driven centrifugal type fans using constant speed 1750 rpm motors. Complete heating element and complete fan and shaft assembly can be removed through either end of casing. Heating element is replaceable copper tube type.

Type V—Horizontal propeller fan type. Built in various sizes from 65 up to 1500 sq ft EDR.

DUNHAM AIR CONDITIONING UNIT

This single unit, when correctly installed, supplies heated air in winter and cooled and dehumidified air in the summer, with filtering, ventilation and circulation of air the year 'round. These combined services are rendered with a minimum requirement of space and a high functional efficiency which guarantees genuine satisfaction and genuine economy.

DUNHAM TYPE OTS HEATING ELEMENT

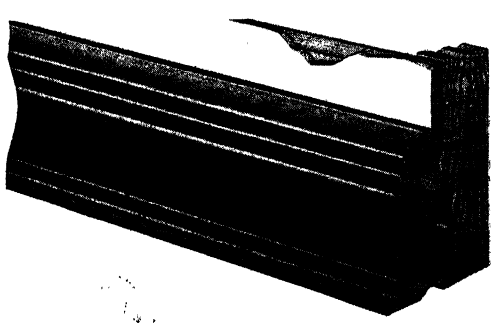
An extended surface heating element made of steel or copper. Light in weight, and has unusual heating capacity. Each element is made up of 1¼ in. pipe with heavy fins mechanically attached, eliminating the use of a solder bond without sacrifice of heat transfer. Each fin, when pressed on the pipe, interlocks with the preceding fin—forming an exceedingly tight and permanent mechanical joint. The complete unit is painted with heat-resisting zinc chromate black enamel. Lengths from 18 in. up to 144 in. can be supplied in 6 in. increments. Standard units are threaded at each end with standard pipe threads.

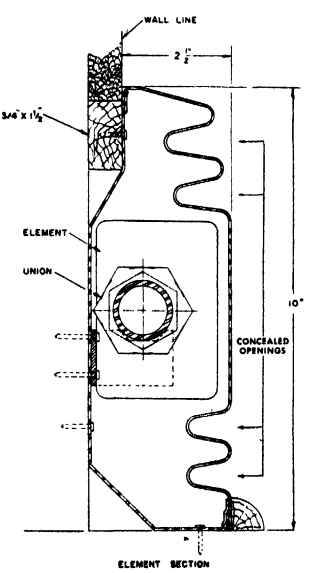
DUNHAM BASEBOARD

The Dunham Baseboard Simplicity Heating System is completely automatic. A room thermostat starts and stops the water circulator to provide just the right amount of heat. An aquastat starts and stops the heating device on the boiler to maintain a minimum water temperature and provide adequate hot water for washing, bathing and other domestic purposes. This automatic operation, plus the high efficiency and complete simplicity of the Dunham System, cuts installation and operation costs to a *fraction* of what you pay for old-fashioned heating systems.

Smart design and easy maintenance are combined in the Dunham Baseboard Simplicity Heating System. The specially engineered baseboard comes in an attractive style with completely hidden louvres to provide a decorative note that doesn't detract from the layout of your rooms as does an ordinary radiator heating system. It's easy to keep clean, too, because the Dunham Baseboard has no outside openings to catch dirt—and as it goes completely to the floor there is no hard-to-clean pocket of accumulated dust. The baseboard cover is easily removed and all parts are readily accessible. Attractive in appearance—easy to install—simple to operate and gives clean, comfortable, satisfying, healthful warmth . . . from wall to wall . . . from floor to ceiling.

This completely concealed heating system surrounds the entire house with a one inch pipe inside the outside walls (lengths of finned radiation are installed as required) to provide a wall of warmth, to keep out the cold. It wraps a house in a blanket of warmth. Designed and tested at odd moments during the long war years, an independent laboratory says, "Its performance was better in a basementless house than any other device that has been tested."





ELEMENT SECTION

William S. Haines & Company

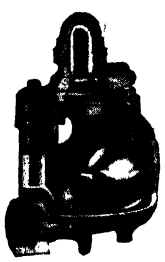
1010-12-14 Wood Street, **Philadelphia 7, Pa.**

Manufacturers of

EQUIPMENT FOR VAPOR AND VACUUM HEATING SYSTEMS

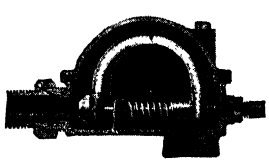
PRODUCTS—Haines Vento Radiator Traps, Medium Pressure and Blast Type Traps, Combined Float and Thermostatic Traps, Air Eliminators, High Pressure Thermostatic Traps, Boiler Return Traps, Radiator Valves.

HAINES F & T TRAPS



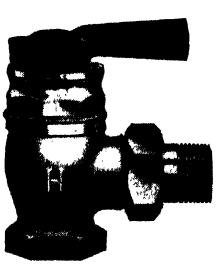
Designed to handle large quantities of condensation. For dripping steam mains, unit heaters, hot water generators. etc. Cannot become air bound as it has a thermostatically controlled air by pass. Sizes ¾ in., 1 in., 1¼ in. For pressures to 30 pounds.

HAINES MEDIUM PRESSURE TRAPS



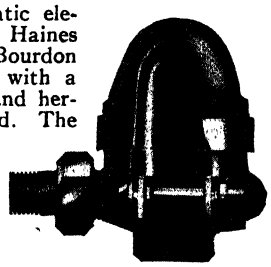
A ruggedly constructed bolted case trap. Ideal for hospital and kitchen equipment and all process work operating on pressure up to 100 pounds.

HAINES MODULATING VALVES



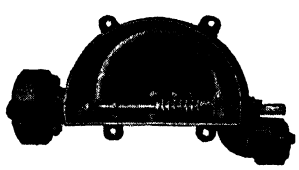
A packless valve assuring positive and leak proof performance. Completely opens or closes on less than a full turn of handle. Can be furnished with wheel or lever handle or lock-shield.

HAINES RADIATOR TRAPS



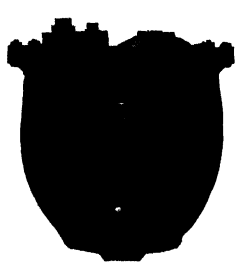
The thermostatic element in all Haines Traps is a Bourdon tube, charged with a volatile fluid and hermetically sealed. The expansion and contraction of the fluid, under varying temperatures, furnishes the operating power. The vertical seat of this trap prevents it from becoming inoperative from scale or other foreign matter.

HAINES HIGH PRESSURE TRAPS



For dripping high pressure mains, laundry equipment and all process fixtures with working pressures up to 125 pounds.

HAINES BOILER RETURN TRAPS



For vapor and atmospheric heating systems. Assures positive circulation by venting the air and returning the water of condensation to the boiler. Has no stuffing boxes or packed joints to leak air or water.

Each device is individually tested, factory adjusted and guaranteed.

Hoffman Specialty Company

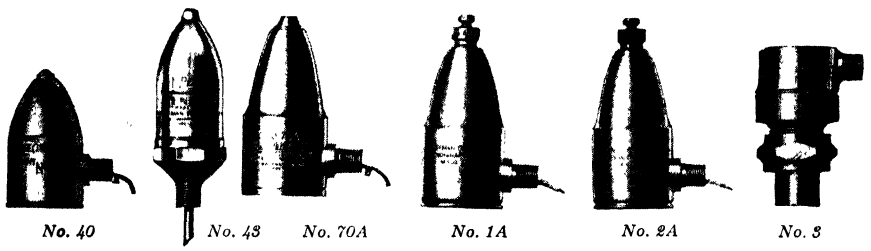
General Office and Factory

1001 York Street, **Indianapolis 7, Ind.**

Sales Representatives in Principal Cities

Manufacturers of Radiator Air Valves, Quick Vents and Air Eliminators for all types of Steam and Vacuum Heating Systems—Steam Traps of all kinds—Radiator Supply Valves—Vacuum and Condensation Pumps—and Hot Water Automatic Heat Control Systems.

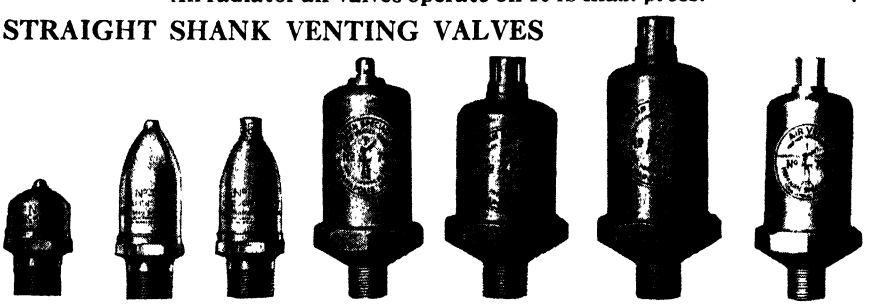
RADIATOR AIR VALVES FOR STEAM AND VACUUM SYSTEMS



No. 40 *No. 43* *No. 70A* *No. 1A* *No. 2A* *No. 3*

No. 40 Steam—Hoffman patented tongue syphon—⅛ in. connection—fixed port.
No. 41 and 43 Steam—Straight shank for convectors—telescopic syphon—⅛ and ¼ in. connections.
No. 70A Steam—Tongue Syphon—Non-adjustable, single port—⅛ in. connection.
No. 1A Steam—Tongue syphon—ADJUSTABLE air opening—⅛ in. connection.
No. 2A VACUUM—Tongue syphon—ADJUSTABLE air opening—⅛ in. connection.
No. 3 Steam—For Airline or PAUL systems—⅛ x ¼ in. conn.—union tailpiece.
All radiator air valves operate on 10 lb max. press.

STRAIGHT SHANK VENTING VALVES



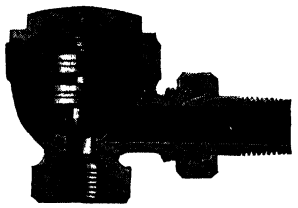
No. 4 *No. 4A* *No. 16A* *No. 74* *No. 75* *No. 76* *No. 79*

No. 4 Steam Mains—Will not close against water—25 lb press. ¾ in. connection.
No. 4A Steam Mains—Float closes against water—10 lb press. ¾ in. connection.
No. 16A VACUUM Mains—Float closes against water—10 lb press. ¾ in. connection.
No. 75 Steam Mains—Large systems—has float—10 lb press. ¾ in. connection.
No. 76 VACUUM Mains—Large systems—has float—10 lb press. ¾ in. connection.
No. 75A Steam Mains—Large systems at low pressure—has float—3 lb press. ¾ in. conn.
No. 76A VACUUM Mains—Large systems low pressure—has float—3 lb press. ¾ in. conn.
Nos. 74-75-75A-76-76A have cast iron bodies—others brass

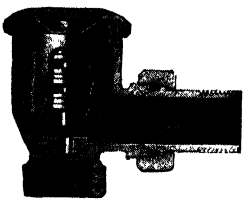
UNIT HEATER VENT VALVES

No. 74—Operates 0 to 35 lb. Vents all air at any pressure and whether rising or falling—can be used on steam mains—has cast iron body—¾ in. connection—finished in attractive Hoffman gray-green color.
No. 79—Hot Water Vent Valve—Positively removes air from piping of any hot water system. Max. pressure 75 lbs.—¾ in. connection at base and tapped at top for ¼ in. pipe connection.

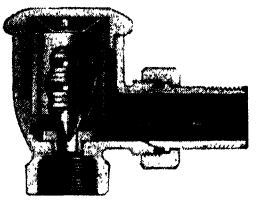
LOW, MEDIUM AND HIGH PRESSURE THERMOSTATIC TRAPS



Low Pressure



Medium Pressure



High Pressure

Low pressure traps have brass bodies, caps, and union nut and tail piece. 17C is made in Angle, Swivel and Vertical patterns. 8C is made in Angle and Straightway patterns. 9C is made in Angle pattern only. Thermostat and seat both renewable.

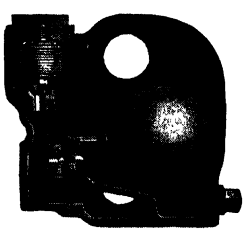
No. 17C Capacity 200 sq ft EDR 15 lb pressure ½ in. connection
No. 8C Capacity 400 sq ft EDR 25 lb pressure ¾ in. connection
No. 9C Capacity 700 sq ft EDR 25 lb pressure 1 in. connection

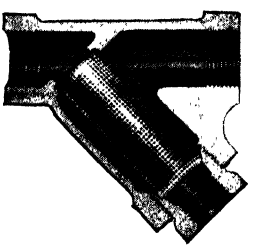
Medium Pressure Nos. 8 & 9 and High Pressure Nos. 8H & 9H have all bronze bodies and caps with union nut and tailpiece. Thermostats are 6 diaphragms of special non-corrosive metal. Thermostats and seats are renewable. ½ in. sizes are furnished in Angle, R.H., L.H., and Straightway patterns, others in Angle only. Medium Press. 50 lb limit. High Press. 125 lb.

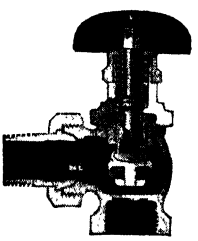
Capacities—Lb Condensate per Hour—Working Pressure—Lb per Sq. In. Gage

Traps		5	15	25	50	Traps		25	50	100	125
8	⅜"	100	180	235	400	8H	⅜"	235	400	550	590
8	½"	125	225	300	490	8H	½"	300	490	650	720
9	¾"	225	350	450	650	9H	¾"	450	650	875	950
9	1"	325	500	625	850	9H	1"	625	850	1125	1250

FLOAT TRAPS, DIRT STRAINERS AND SUPPLY VALVES





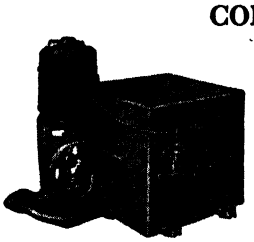


50 Series Float and Therm. Traps, are available in large capacities and four pressures, 15, 30, 60 and 125 lb. Used for venting and draining risers, steam mains, unit heaters, blast coils, etc. 50 Series Traps are made for easy servicing with all working parts mounted on cover. Remove four bolts to expose all parts. Pipe sizes are from ¾ in. to 2 in.

Radiator Supply Valves are made in sizes from ½ to 1½ in. in Angle and Straightway patterns. Brass bodies, union nut and tailpiece. No. 80 has reversible cone disc and bevelled seat. No. 85 is Modulating type. Both are packless.

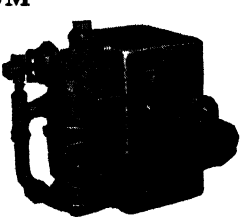
Hoffman Dirt Strainers are self-cleaning Y type. Brass strainer cylinders and cast iron body. Sizes ½ to 2 in. for 125 lb pressure. Should be used in line ahead of all float and thermostatic traps.

CONDENSATION AND VACUUM PUMPS



Condensation Pump

Hoffman-Economy pumps are available in varying capacities, D.C. and A.C. current, single, two, or three phase, and in pressures up to 200 lb. Also made in single and duplex units for different capacities and pressures.



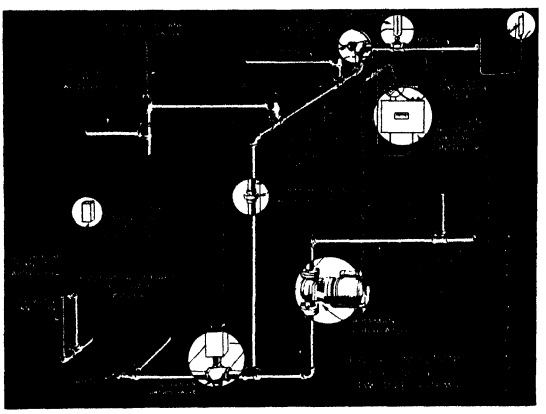
Vacuum Pump

HOFFMAN HOT WATER CONTROLLED HEAT

Especially Designed for Panel Heating

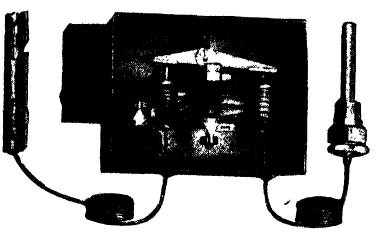
The Hoffman method vastly improves the ordinary forced hot water system by the application of *Continuous Circulation*. This method permits a smoothly modulated regulation of the heat supply. The Control Valve closes and the circulating stream by-passes the boiler as long as the heat requirements are satisfied.

When the circulating water begins to lose heat, the Control Valve is slowly opened by the Controller, permitting hot boiler water to enter the system. Thus, the delicate precision of the Hoffman Controller smoothly varies the temperature of the *continuously circulating* water so that the heat supply is always equalized with the heat loss and room temperature remains constant throughout all changes in the weather.



There is no type of building to which Hoffman Hot Water Controlled Heat cannot be applied. The system permits *zoning* of apartments, institutions, large residences and factories, thereby assuring a distribution of heat in direct relation to either personal temperature preference or to the functional activities of the building.

HEATING COMFORT IS ACHIEVED BY HOFFMAN SPECIALTIES



The Comfort Controller

The brain of the Hoffman system. It automatically maintains a constant comfort condition regardless of the outdoor temperature. Its accurate balancing mechanism electrically opens or closes the Hoffman Hot Water Control Valve as required.

Outdoor Temperature Anticipating Bulb

This Bulb transmits changes in the outdoor temperature to the balancing mechanism of the Comfort Controller.

Hot Water Temperature Bulb

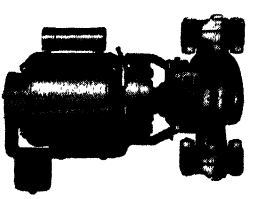
Accurately relays temperature changes of the supply main water to the balancing mechanism of the Hoffman Comfort Controller.

Hot Water Control Valve

Opens only sufficiently to supply the correct amount of water to maintain the proper water temperature being circulated through the system.

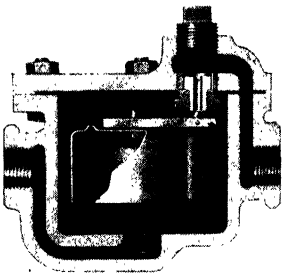
Balancing Orifice

A calibrated orifice used to balance the circuits through the boiler and through the Hoffman circulating pipe.



Hoffman Circulator

A centrifugal pump of prescribed capacity and low in power consumption. Usually installed in the return main and continuously circulates the water through the system. Continuous operation puts less strain and wear on the pump motor than intermittent operation as any engineer will attest.

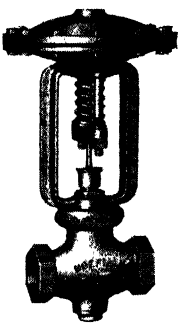


Series 600

HOFFMAN INVERTED BUCKET TRAPS

Working Pressures to 200 lbs

Simple mechanism assures high operating efficiency. Features include—straight-through pipe connection; simple seat adjustment; all working parts connected to bonnet and easily removed with it; stainless steel seat and pin.



Series 700

HOFFMAN PRESSURE REDUCING VALVES

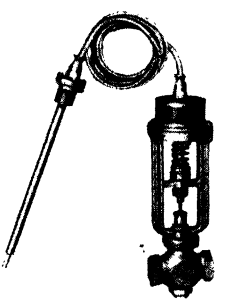
Series 710
Max. High Pressure.....250 psi.
Low Pressure Range....5 to 80 psi.

Series 700
Max. High Pressure.....200 psi.
Low Pressure Range....1 to 25 psi.

Choice of types specifically engineered for your needs—continuous service, or, for tight sealing against low pressure side when there is no demand—and with typical Hoffman features of design.

HOFFMAN TEMPERATURE REGULATORS

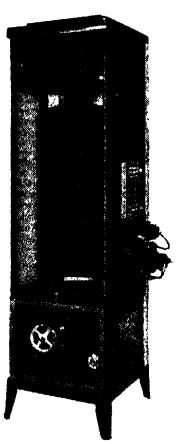
Series 1100– for steam pressure to 150 lb. per sq in. Standard temperature range—130F to 190F. Other ranges available from 80F to 250F. Self-motivated. Hydraulically formed bellows of selected material. Rugged all-bronze construction. For water heaters, convecters, fuel oil preheaters and other similar applications.



Series 1100

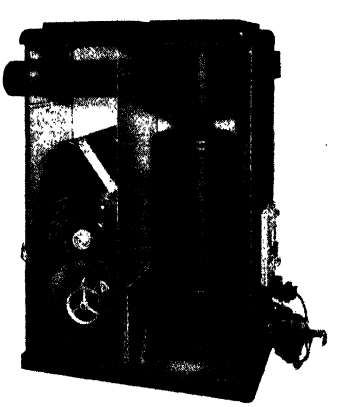
HOFFMAN CONTROLLED HEAT FURNACES

Warm Air—Vaporizing Oil Burner Type



(*Left*) HU-70 For Homes Without Basement

Capacity 70,000 Btu output at bonnet; mechanical draft two stage vaporizing burner; blower delivers 750 cfm; floor space 22½ x 22½ in.; height 81½ in.; shipping weight 408 lb.; assembled, with combination fan and limit control, all burner controls, thermostat, and draft regulator.



(*Right*) HB-75 Basement Unit

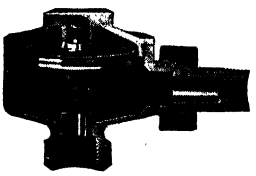
Capacity 75,000 Btu output at bonnet; mechanical draft two stage vaporizing burner; blower delivers 750 cfm; floor space 22 in. x 45 in.; 55 in. high; shipping weight 400 lb.; completely equipped.

ILLINOIS ENGINEERING COMPANY

General Offices
and Factory:
Chicago 8, Ill.

**Representatives
In Principal Cities**

Illinois Thermo Radiator Traps



Series G

Illinois Thermo Radiator Traps for vacuum, vapor and low pressure heating systems. Has cone type valve. Flushes thoroughly and seats perfectly at all times. Valve and seat are of hardened steel alloy. The duplex diaphragm is of special phosphor bronze. Scientific design and rugged construction assure flexibility and long life. These diaphragms have withstood over three million strokes on a breakdown test.

Ask for Bulletin.

Vapor Gauge

Vapair Vent Trap

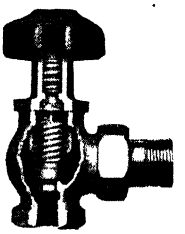
Boiler Return Trap

Illinois Selective Pressure Control Systems

Selective Controller

An entirely new and unique method of Steam Circulation Control . . . Heating Systems that set new standards in comfort, economy, simplicity and convenience of operation. Each system individually engineered to meet exact requirements. Recorded fuel savings, without sacrifice of comfort, warrant your investigation.

Illinois Radiator Supply Valve



Quick-opening, packless. Steam tight on 50 lb pressure. Large diameter of thread spool and machine cut threads make valve operation easy. Furnished in a complete line of sizes and patterns.

Illinois Vapor System

A two pipe low pressure steam circulating system which may be installed in any type of building, where the condensate can return to the boiler by gravity.

A sensitive damper regulator or other means of automatic control is used to control initial steam pressure above, at or below atmospheric pressure. Steam is regulated at the radiators by Illinois Packless Supply Valves. Condensate and air are discharged from the radiator through Illinois Thermostatic Radiator Traps. In the boiler room a Vapair Vent Trap and Boiler Return Trap are installed near the boiler. The vent trap eliminates air from the system and the Return Trap insures return of condensate to the boiler.

The system and the piping arrangement are simple. No metering orifices or vacuum pumps are needed. This system will be found suitable for many installations where low first cost and low operating cost are of prime importance. May be used with unit heaters or any type of radiation.

Illinois Float and Thermostatic Traps

Series G

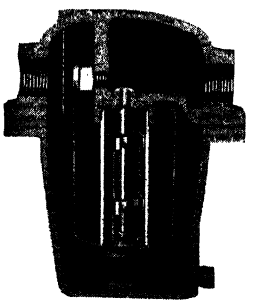
Unsurpassed for draining ventilating units, unit heaters, and for dripping mains and risers—wherever it is desirable quickly to vent air from the main as well as handle the water of condensation in quantity, whether hot or cold.

ILLINOIS ENGINEERING COMPANY

General Offices
and Factory:
Chicago 8, Ill.

Representatives
In Principal Cities

Illinois Steam Trap



Series 80

Valve and stem are separate from the bucket and operated only by the bucket at the extreme top and bottom of travel—result—*valve is always either full open or tight closed.* Provided with continuous thermostatic air vent. No wire drawing or cutting of valve and seat which are of hardened steel alloy.

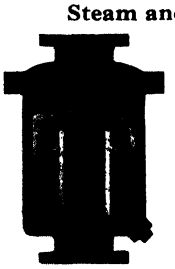
Illinois Thermostatic Traps for High Pressures

Series HG

Maximum working pressure 150 pounds. Used where neat appearance and compactness are desirable, as for trapping sterilizers or water stills in hospitals; steam jacketed kettles, coffee urns, warming tables and for process work. Also used extensively for air vents on blast type drying heaters. Multi-diaphragm of phosphor bronze. Heavy duty bronze body. Made in three sizes.

These traps are also furnished for medium pressures. *Write for literature.*

Steam and Oil Separators

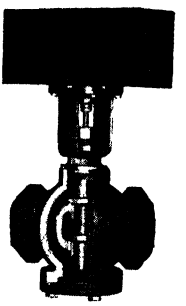


Vertical Steam Separators

Eclipse steam separators are made in both horizontal and vertical type, standard or extra heavy.

Eclipse oil separators are furnished in the horizontal type and have a removable baffle plate to facilitate cleaning of baffle and keeping the separator's efficiency at the highest point.

Illinois Motorized Valves (on and off)



Type ES

For automatic control of steam temperatures and pressures to prevent overheating and conserve steam; to control fluid levels; and to regulate flow in hot water heating systems. May be operated by any automatic contact device or by manual switches.

Furnished in three types.

Pressure Regulating Valve Semi-Steel Bodies, Bronze Trim

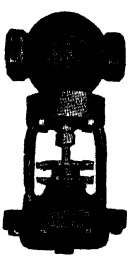


Fig. 121

Furnished in either single seat or double seat type as service requires, for the control of steam, air or gas. Control spring is completely enclosed, protecting it from dirt and rust. Valves are furnished with proper size diaphragm and proper length spring to give satisfactory service under all operating conditions. Furnished also in weight loaded type, Fig. 71.

Write for Bulletins.

Non-Return Valves

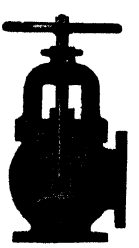


Fig. 260

Placed between boiler and header to prevent return of steam to boiler. Sensitive in operation. Extra heavy semi-steel bodies with bronze trim for 250 lbs steam working pressure. Bronze dash pot and water sealed pistons prevent valve sticking. Globe and angle patterns from 4 in. to 12 in.

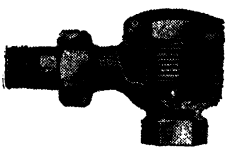
Sarco Company, Inc.

Empire State Bldg., **New York 1, N. Y.**

Branches in Principal Cities

SARCO CANADA LIMITED, 496 CHURCH ST., TORONTO 5, ONT.

PRODUCTS—A complete line of Specialties for Steam and forced hot water Heating Systems, and automatic control for same, combined with a competent engineering service to architects and heating engineers to assist them in providing modern heating.



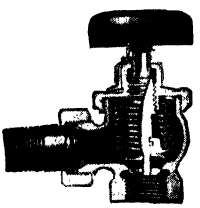
Radiator Trap, Type H

SARCO RADIATOR TRAPS

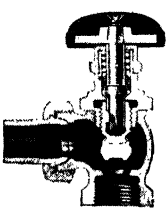
Type H is the standard radiator trap for vapor and vacuum systems. It is equipped with the well known Sarco heavy wall bellows, drawn from flat blanks and helically corrugated in our own plant. It operates noiselessly and positively at pressures from highest vacuum to 25 psi.

Body and cap are of cast brass, rough brass finish; self-aligning valve head and renewable seat of hard bronze; union connection on inlet.

Available in ½ in. and ¾ in. sizes, angle, straightway or corner offset patterns; also 1 in., angle style only. *Catalog No. HV-150.*



Type 45



Type SM

Radiator Valves

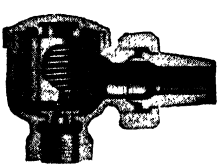
SARCO RADIATOR VALVES

Sarco offers two types of radiator valves. Where highest efficiency is desired, the bellows-packless valve, type 45, is recommended. The valve stem is sealed by a standard Sarco bellows. Leakage of air into the system under vacuum is impossible.

Modulating types with proportioning disc and indicating dial are available.

Type SM is of the "spring-packless" type, quick opening, non-rising stem. Also available for Hot Water Systems.

Bodies of all valves are cast brass, rough brass finish. Outlet fitted with union connection. Sizes ½ in. to 1½ in., with wheel handle or lock shield. *Catalog No. HV-150.*

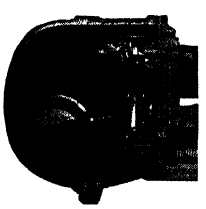


N-100 Medium Pressure Trap

SARCO N-100 TRAP

For high pressure radiators and heating coils in stationary and marine service, and for hospital and kitchen equipment. Has full length protecting shield and stainless steel valve head and seat. Sizes ⅜ in. to 1 in. pressures to 100 lb. *Catalog HV-190.*

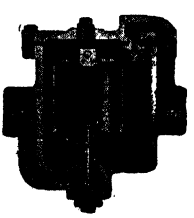
Also S-65 for pressures to 65 psi.



Float-Thermostatic Trap

SARCO FLOAT-THERMOSTATIC TRAPS

For dripping ends of mains and risers, and for stack or blast heaters, large unit heaters and hot water generators. Automatic thermostatic air vents built in. Available in six sizes with connections ¾ in. to 2 in. Pressures up to 200 psi. *Catalog HV-450.*



Inverted Bucket Trap

SARCO INVERTED BUCKET TRAPS

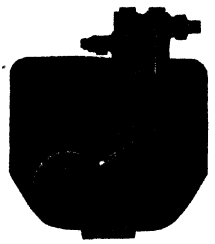
Are recommended for high pressure unit heaters and sometimes preferred for kitchen and laundry equipment. Strainers are built right into these sturdy traps. Seats and valves are stainless steel and renewable. Automatic air vents can be furnished for extra rapid removal of air. Available in sizes ½ in. to 2 in. for pressures up to 900 psi. *Catalog HV-350.*

SARCO ALTERNATING RECEIVER

A complete line of boiler return traps for vapor systems.

Returns water of condensation to boiler automatically, thereby assuring positive return of water under all pressure conditions.

Made in four sizes for up to 14,000 sq ft of radiation. *Catalog HV-165.*



Alternating Receiver

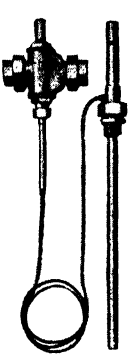
SARCO AIR ELIMINATORS

For venting air from vapor systems at one central point in the basement. Available in three sizes, for systems up to 15000 sq ft radiation. All are equipped with float valves to stop water escaping through the vent and with check valves to prevent ingress of air when system is under vacuum.

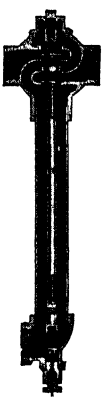
Also several types for hot water heating systems. *Catalog HV-170.*

SARCO SELF-CONTAINED TEMPERATURE REGULATORS

Sarco Temperature Regulators are simple, self-operated valves—the only self-contained units that use the irresistible force of liquid expansion. No stuffing boxes to leak, no auxiliary "power" required; all moving parts are *inside* the equipment. Here again—a type and size for every purpose—for steam, gas, oil, water or brine for temperatures ranging from 0 to 300° F. *Catalog HV-600.*



Type TR-21 Standard for hot water storage tanks, fan units, etc.



Water Blender Type MB

SARCO WATER BLENDERS AND TEMPERING VALVES

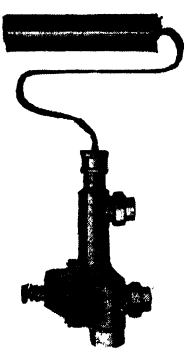
For mixing hot and cold water to deliver automatically water at any desired temperature. Two models are available, type MB for showers, wash basins, etc., and type DB, a tempering valve for use with submerged heating coils or tankless heaters. *Catalog HV-800.*

Water Blender Type DB

SARCOTHERM HOT WATER HEATING SYSTEM

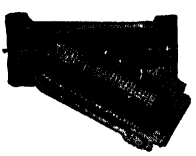
A simple, all-mechanical system for the control of radiator temperatures in direct relation to outside temperatures. Radiation is balanced by Sarcoflow fittings in the radiator outlets.

The Sarcotherm three-way valve recirculates a varying proportion of water around the boiler and back to the system as dictated by the thermostatic bulb outside the building. Write to Sarcotherm Controls, Inc., 280 Madison Ave., New York 16, N.Y. for *Catalog No. HV-1.*



Sarcotherm Weather Control Valve

SELF-CLEANING STRAINERS



For use in pipe lines carrying brine, steam, oil, gas, water, ammonia or air. Have large free screening area with minimum resistance to flow. Steam or air strainers can be cleaned by blowing through without disassembling. Made in cast iron, bronze or cast steel for pressures up to 500 psi, with brass, iron or monel screens. Available in sizes ¼ to 8 in. *Catalog No. HV-1200.*

WARREN WEBSTER & COMPANY

Pioneers of the Vacuum System of Steam Heating

Webster HEATING SYSTEMS

Main Office and Factory:
Camden, New Jersey

Webster Nesbitt UNIT HEATERS

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Licensees and Manufacturers for Canada and Newfoundland:
DARLING BROS., LTD., P. O. Box 187, Montreal, Canada

THE COMPANY

Warren Webster & Company have specialized for almost sixty years in the field of steam circulation and steam distribution, particularly vacuum, vapor and low pressure steam heating of buildings, and medium pressure steam in industrial and process heating applications.

The specialized experience of the Company is available through engineers at the Home Office and through the Representatives listed above. These engineers are thoroughly conversant with methods and equipment to control steam distribution and heat transfer, assuring maximum heating effectiveness with minimum fuel or steam consumption. Webster Representatives are prepared to supply on request full technical, availability and price information on all Webster Systems and Products.

WEBSTER HEATING SYSTEMS

There is a type of Webster Heating System to meet practically every need and purpose. These include Webster Steam Heating Systems for larger buildings of almost every type, and Webster Baseboard Heating, a hot water system particularly suited for small residences and other small buildings.

Webster Steam Heating Systems are all low pressure, two-pipe systems of steam circulation in which steam is delivered to radiators and other heating surfaces through supply piping and water of condensation and air are removed through separate return piping. Webster Radiator Valves and Thermostatic Traps are installed respectively on the supply and discharge connection of each radiator. Webster thermostatic or float and thermostatic traps are provided to assure removal of water of condensation and air from the piping.

Webster Steam Heating Systems are available with vacuum return, or with open return (vented to the atmosphere) with either Condensation Pump or Boiler Return Trap and Vent Trap to return water to the boiler, or with Vent Trap alone where condensate is wasted to the sewer, or in appropriate small installations.

Webster Vacuum System—A conventional vacuum heating system in which the return mains are joined together and connected to the suction end of one or more vacuum pumps which remove air and water of condensation and assists circulation by maintaining a lower pressure in the return than in the supply piping.

Webster Type "R" System—A two-pipe, low pressure or vapor heating system in which water of condensation is returned to the boiler by gravity, prompt return being assured regardless of variations in boiler pressure through the operation of a Webster Boiler Return Trap and Vent Trap in combination. Boiler Return Trap Equipment is available in sizes to care for systems ranging from the smallest to 16,000 sq ft equivalent direct radiation. Where desired, or where gravity return is not possible, a Condensation Pump may be substituted for the Boiler Return Trap Combination.

Webster Type "V" System—Employs only a Webster Vent Trap. For installations of 1000 sq ft equivalent direct radiation or less in which the following requirements are fully met. Oil burner, stoker or gas burner installations with vaporstat having cut-in pressure of about ¼ lb and cut-out pressure of about ¾ lb (not pressurestat), lockswitch or protector relay and one or more key room thermostats. Vent Trap at ample height above water level. Burner or stoker should not have too great capacity. Boiler Protector, or at least a low water cut-out.

Webster Moderator Systems—These are all Webster Steam Heating Systems with vacuum or open return *to which are added* (a) accurately sized metering orifices in radiators and other heating surfaces to balance distribution and permit "partial filling" of all radiators practically simultaneously and at various rates of steam flow, (b) Automatic control by Outdoor Thermostat for variations in outdoor temperature, (c) Manual Variator to provide for convenient adjustments for heating up, reduced night heating, shut off, etc.

"J" Series Moderator Controls—In this series the Outdoor Thermostat and Variator position a motor-operated Steam Control Valve through an Electronic Differential Pressure Control Cabinet to produce continuous steam delivery and heating effect at the radiators with automatic variation in heating for changes in outdoor temperature and automatic adjustment to compensate for variations in steam supply pressure.

"EH" Series Moderator Controls—In this series the Outdoor Thermostat and Variator may control a motor-operated steam valve or directly control oil or gas burner or stoker through a cycling Control Cabinet. Steam delivery is intermittent but in short cycles so that heating effect is substantially continuous, particularly with cast iron radiation. "EH" Series Controls are also applicable to forced circulation hot water systems including Webster Baseboard Heating.

Webster Baseboard Heating—A patented forced circulation hot water heating system in which the heating element fits behind a specially built metal baseboard. Air enters at the floor line, passes over the finned heating element, is warmed and comes out of slots at the top of the baseboard. The heating element is a copper tube with copper fins running in a continuous loop around the exposed walls of the house—a separate loop for each floor.

Webster Baseboard Heating uses less material and less labor than conventional radiator heating systems, while providing all the advantages claimed for forced hot-water, plus radiant effect from warmed baseboards and walls, plus natural convected air movement essential to comfort. Temperatures vary less then 2 deg from floor to ceiling.

STEAM HEATING AND PROCESS SPECIALTIES

Radiator Valves—Choice of spring retained packing, Type BW-P or Sylphon Bellows Packless Series 600-S. ½ in., ¾ in., 1 in., 1½ in. sizes. In angle, right and left hand; straightway, with single or double union. Spring retained packing. For low pressure vapor and vacuum steam heating service.

Double Service Valve—¾ in. and 1 in. sizes. Incorporates Webster Thermostatic Trap and Webster Radiator Supply Valve in a single compact unit. Drips down-feed riser and serves as supply valve to radiator or convector. Saves six fittings and installation work.

Thermostatic Traps—Series "7" (diaphragm type) and Series "5" (bellows type) for radiators and drips. ½ in., ¾ in. and 1 in. sizes. There are six body models for the ½ in. size alone. Maximum pressure, 25 lbs per sq in. For low pressure vapor and vacuum steam heating service. Series "78" for process. ⅜ in., ½ in., ¾ in. and 1 in. sizes. Class 2 for pressures of 60 to 150 lbs. Used to discharge air and water from heating coils of any apparatus using steam at process pressures.

Heavy Duty or Drip Traps—Series "26" Float-and-Thermostatic for heating and air conditioning. Most used sizes: 00026, 0026, 026. Pressures up to 15 lbs per sq in. Made for the pressure and capacity conditions encountered at all drip points. Series "79" Float-and-Thermostatic for process. For pressures up to 150 lbs per sq in. For use where large volumes of hot condensate must be handled more quickly than is possible by thermostatic traps alone

Dirt Strainers—½ in. to 6 in. sizes. Maximum working pressure 150 lbs per sq in. Placed ahead of traps in return lines of steam-using equipment and steam heating systems to catch dirt and other particles, preventing them from impairing the tightness of the traps.

Boiler Protectors—One size, with ¾ in. connections with or without electrical cut-out switch. Maximum pressure 15 lbs per sq in. Maximum cold water main pressure, 150 lbs per sq in., minimum not less than 25 lbs per sq in. Prevents breakage in low pressure heating boilers when the water level becomes inadequate.

Vacuum Pump Governors—In sizes ¾ in. to 3 in. Standard valve furnished for pressures up to 150 lbs per sq in. Special valve available for higher pressures. Govern flow of steam to steam-driven vacuum pumps.

Suction Strainers—Maximum working pressures 15 lbs per sq in. Installed ahead of vacuum pump to prevent dirt from damaging pump.

Vacuum Breakers—Sizes ¾ in., 1 in. and 1¼ in. adjustable on job. Size ⅛ in. for radiators is factory adjusted. For automatic breaking of vacuum at predetermined setting in heating systems, feed water heaters, hot water generators, industrial pressure chambers, etc.

Expansion Joints—Crosshead or internally guided. In single slip and double slip models in most widely used pipe sizes. For pressures up to 200 lbs per sq in. For steam, hot water, hot oil, hot gas, and condensate return lines.

RADIATION AND HEATING SURFACE

Webster System Radiation—Nonferrous convector radiation. Each Webster System Radiator includes a complete enclosure of furniture steel with baked prime coat. Contained within the enclosure is a prefabricated unit, combining heating surface, valve, trap and union connections, shipped ready to connect to supply and return piping.

Webster System Radiation was first offered in 1932. From its introduction until withdrawal from the market because of war conditions, more than 1,000 installations were made.

Now, available in an improved design, using the same basic material, copper tubing and aluminum fins. Increased rigidity of the tubing and the development of a new method of manufacturing has produced a fin surface of unusual rigidity, free of expansion and contraction noises.

Webster Type WI Extended Surface Radiation—Covered by patents and patents pending. Completely non-ferrous, being made up of 1⅛ in. outside diameter .035 in. thick specially annealed copper tubing with rib-reinforced, square pressed aluminum fins and brass female couplings with 1 in. i.p.s. tapping. Available in five lengths from 2 to 6 ft inclusive. Can be used to advantage in many buildings with steam or hot water heating, particularly where floor space or vertical wall space is limited.

WEBSTER-NESBITT UNIT HEATERS

Are manufactured by John J. Nesbitt, Inc., Philadelphia 36, Pa., and are distributed solely through Warren Webster & Company, Camden, New Jersey. Designed to circulate large volumes of air at comparatively low temperatures, assuring quick heating.

Ratings of Webster-Nesbitt Unit Heaters are based on tests made in accordance with standard test code of Industrial Unit Heater Association and A.S.H.V.E.

PROPELLER FAN UNIT HEATERS

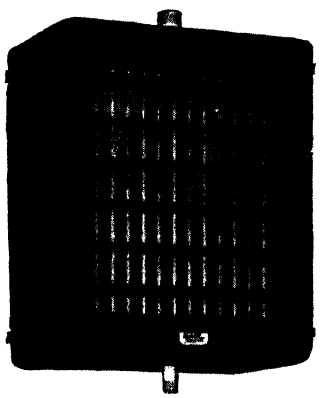


Fig. 11. Standard Propeller-Fan Type

Designed to incorporate four characteristics proved by wide experience to be essential to both proper application and satisfactory performance:

1.) *Selective range of sizes.* Manufactured in nine sizes. Heating capacities vary from 34,700 to 338,000 Btu per hour. Air deliveries from 470 to 4800 cfm.

2.) *Quiet Operation.* All fans have blades of exceptionally large areas and of a shape to impart a gradual acceleration to the air stream. Ample spacing is maintained between the fan and heating element. Motors are of sleeve bearing type and equipped with isolators.

3.) *Durable lightweight Heating Elements.* Extended fin-and-tube type, constructed of copper condensing tubes and plate-type aluminum fins.

4.) *Modern Casing Design.* Compact suspended type. Catalog W-N 126.

GIANT UNIT HEATERS

Sturdy blower-fan units for the economical heating of large areas.

Standard (Non-Thermadjust) Type. Used principally where heating is by recirculation only, and where constant heat output is desired during period of operation.

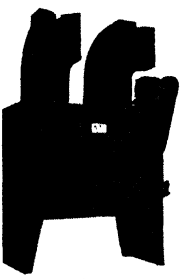


Fig. 12 Blower-Fan Type

Thermadjust Type. Employs dampers in front of casing and over face of heating element to provide mixing of unheated and heated air, producing heat output in accordance with requirements and continuous circulation of air volume.

Valve Controlled Type. Unit is of standard casing arrangement but equipped with Nesbitt Heating Surface with Steam-distributing Tubes which allows for automatic control of heat output.

Floor mounted, wall mounted, ceiling suspended, from 101,000 Btu, 3250 cfm, to 930,000 Btu, 15,200 cfm. Write for details. Catalog W-N 128.

LITTLE GIANT UNIT HEATERS

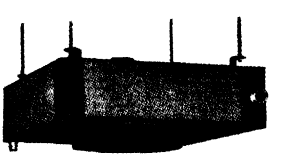


Fig. 13. "Little Giant" Down Blow Type

New, light compact draw-through high velocity down blow unit heaters. 122,000 Btu, 2370 cfm to 505,000 Btu, 10,080 cfm at basic rating of 2 lb steam and 60 deg entering air.

Down Blow Type. Generally used when the presence of cranes and other machinery requires that the unit and piping be located well above the floor level. Write for details. Catalog W-N 127.

Armstrong Machine Works

851 Maple Street, **Three Rivers, Mich.**

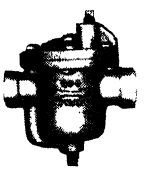
Steam Traps . . . Air Traps . . . Humidifiers
High Side Floats . . . Refrigerant Purgers

Representatives in Principal Centers

ARMSTRONG INVERTED BUCKET STEAM TRAPS

Armstrong offers a complete line of traps for draining low and medium pressure steam headers, pipe coil radiation, unit heaters, air conditioning equipment, process equipment, etc. Armstrong design and construction results in fast heating, uniformly high temperatures and long trap life with exceptionally low maintenance.

Automatic Air Discharge. Standard traps automatically discharge normal amounts of air along with condensate. Where large amounts of air must be vented quickly when steam is first turned on, Armstrong BLAST Traps with thermic bucket vents are recommended. Depending on size, air handling capacity ranges from 500 to 1500 cu ft free air per hour.



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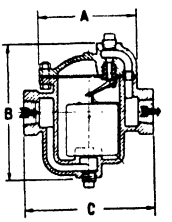

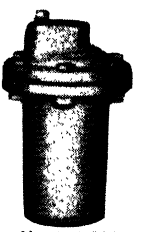

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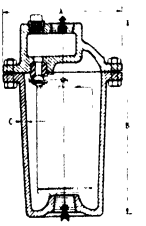


Side Inlet Traps		No. 800	No. 811	No. 812	No. 813
Pipe Connections		½" or ¾"	½" or ¾"	½" or ¾"	¾" or 1"
List Price (Regular)		$7.00	$10.00	$16.00	$22.00
List Price (Blast Trap)		$8.50	$11.50	$18.00	$24.00
Telegraph Code (Regular)		Aloe	Brown	Cherry	Dawn
Telegraph Code (Blast Trap)		Aloette	Brownette	Cherette	Dawnette
Dimension A		3¾"	3¾"	5⅝"	7"
" B		5⅜"	6⅞"	8 11/16"	11¼"
" C		5"	5"	6½"	7¾"
" D		....	....	....	....
" E		....	....	....	....
Number of Bolts		6	6	6	6
Diameter of Bolts		¼"	¼"	⅜"	½"
Weight		4½ lbs.	5½ lbs.	13½ lbs.	25 lbs.
Maximum Pressure, lbs.		125	250	250	250
Continuous discharge capacity in lb of water per hour at pressure indicated. For more complete information see the Capacity Chart in Armstrong Steam Trap Book.	5 Lb Pressure	450	830	1600	2900
	10	560	950	1900	3500
	15	640	1060	2100	3900
	20	690	880	1800	3500
	30	500	1000	2050	4000
	50	580	840	1900	4100
	70	660	950	2200	3800
	100	640	860	1800	3600
	125	680	950	2000	3900
	150	....	810	1500	3500
	200	....	860	1600	3200
	250	....	760	1300	3500

CAPACITIES, PRICES DIMENSIONS

Note that capacities of No. 811, 812 and 813 traps are the same as No. 211, 212 and 213 respectively. On most installations, the engineer therefore has a choice of side inlet—side outlet or bottom inlet—top outlet body styles.

Bottom Inlet Traps	No 211	No. 212	No. 213	No. 214	No. 215	No. 216
Pipe Connections	½"	½" or ¾"	½" or ¾"	1"	1" or 1¼"	1½" or 2"
List Price (Regular)	$ 9.25	$15.00	$20.75	$29.00	$38.00	$55.00
List Price (Blast Trap)	$10.75	$17.00	$22.75	$31.50	$40.50	$60.00
Telegraph Code (Regular)	Aspen	Birch	Walnut	Hemlock	Larch	Tamarack
Telegraph Code (Blast Trap)	Aspette	Birette	Walette	Hemlette	Larette	Tamrette
Height.....Dimension B	6⅜"	8"	10¼"	12½"	14"	16¾"
Diameter..... " A	4⅛"	5"	6⅜"	7½"	8½"	10 8/16"
Wall Thickness " C	5/16"	¼"	5/16"	⅜"	⅜"	7/16"
Diameter of Bolts	¼"	¼"	⅜"	⅜"	½"	½"
Number of Bolts	6	8	6	8	8	12
Weight	5½ lb	10½ lb	19 lb	32 lb	47 lb	80 lb
Maximum Pressure, lb	250	250	250	250	250	250

High Capacity, Compact Size. The high leverage of the patented free-floating lever makes it possible to open discharge orifices which are very large for over-all trap size.

Positive Action. The discharge valve is either wide open or closed tight. Fast opening and closing prevent wire-drawing.

Self-Cleaning. Swirling action of condensate during discharge carries dirt through trap. There are no dead spots for dirt to collect.

High Quality. 18-8 stainless interior parts. Valve and seat are chrome steel, hardened, ground and lapped. Low pressure trap parts same material and quality as those used for 1500 psi, 900° F.

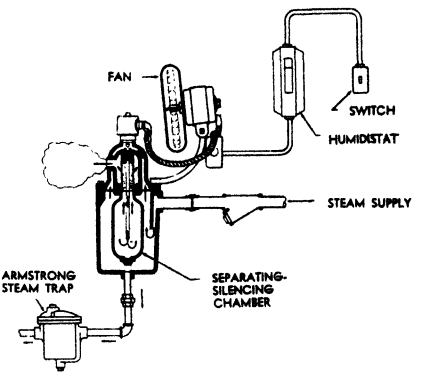
Armstrong Steam Trap Book. 36 pages of data on traps, selection, installation and maintenance. A usable handbook for any engineer dealing with traps. Free copy on request.

ARMSTRONG STEAM HUMIDIFIERS

For Stores, Offices, Hospitals, Factories, Laboratories

Operation. These units provide automatic, closely controlled humidification by introduction of steam directly into the atmosphere. Installation is comparable to that of unit heaters. Steam at 10 psi or less is required. A solenoid discharge valve on the humidifier is controlled by a sensitive humidistat. A fan mounted on the humidifier aids in steam dispersal, or a venturi nozzle can be supplied. Where an electric spark might represent an explosion hazard, compressed air operated models are available. In addition to the unit humidifier illustrated, there is a large model for installation in large air ducts and central heating systems. Capacities range from 31 to 630 lbs of steam per hour.

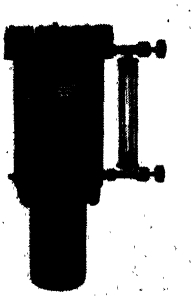
Advantages. Installation cost of Armstrong Humidifiers is as much as 80 per cent less than some types of equipment. The small C-2 unit lists at $120.00 complete with fan and motor, humidistat, strainer and steam trap. Operation, using steam at around $1.00 per ton, is economical. There is no extra load on the heating system. No dripping—any moisture in the steam is re-evaporated in the steam-jacketed separating chamber. Control is accurate within a few per cent R. H. There is almost no noise with open nozzle types.



Bulletin No. 177 gives complete data on required relative humidities, selection and installation of Armstrong Humidifiers. Available on request.

ARMSTRONG NON-CONDENSIBLE GAS PURGERS

Armstrong Purgers *automatically* remove air and other non-condensible gases from refrigerating systems, with minimium loss of refrigerant. Refrigerant gas is condensed in the cap of the purger, causing non-condensibles to separate out at the top from where they discharge through a needle valve. These purgers are suitable for systems from 12 to 1200 tons capacity —Ammonia, Freon, CO_2 and other refrigerants. Body is forged steel, interior parts stainless steel. List price is $200.00 BULLETIN NO. 173-A describes benefits of purging, gives complete data on installation and operation of Armstrong Purgers. Available on request.



All Armstrong products are sold on a basis of satisfaction guaranteed or your money back.

Jas. P. Marsh Corporation

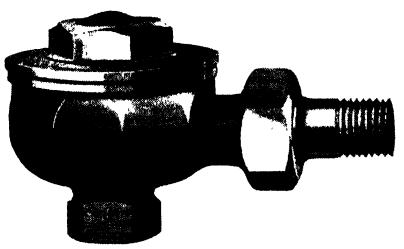
Dept. 5, **Skokie, Illinois**

Branches in Principal Cities

Marsh products include: Pressure, Vacuum and Compound Gauges; Dial Thermometers; Steam Traps; Vents; Packless Radiator Valves and other heating specialties.

Thermostatic Diaphragm Radiator Traps

These efficient traps are equipped with a phosphor bronze diaphragm, consisting of two wafers of tinned phosphor bronze, drawn and spun to perfection of temper.

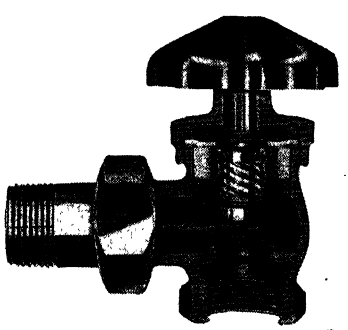


Thermostatic Diaphragm Radiator Trap

The wafers are spun together and soldered to form a seamless, sensitive, powerful expanding member—not easily fouled by dirt and foreign matter. Diaphragms are charged with a volatile fluid making them self-equalizing for use on pressures below atmosphere to 15 lbs gauge. Traps are factory adjusted.

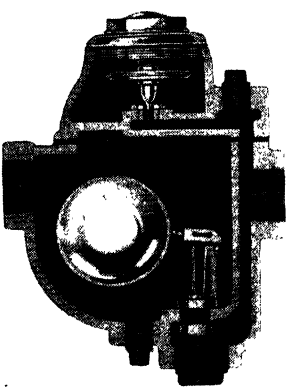
Packless Radiator Valves

Marsh all-metal packless valves are truly packless. These valves contain no packing to deteriorate, wear or crack, and are simple in design, with ample strength where strength is required. The principles upon which they are designed have been proved sound over many years of service. Valves operate easily—opening or closing tightly with less than one full turn. All valves are individually tested. Adaptable for use on hot water—forced or gravity systems—as well as all steam heating systems.



Packless Radiator Valve

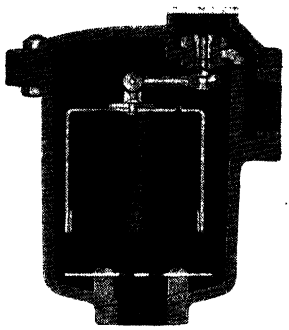
Marsh No. 12 Float and Thermostatic Traps



Float and Thermostatic Trap

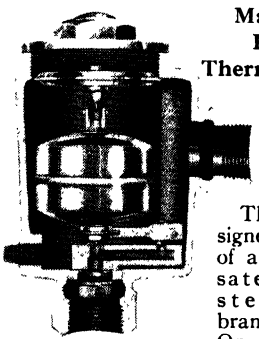
Marsh Heavy Duty Float and Thermostatic Traps are designed for removal of air and condensate from steam mains, branches, or risers, unit heaters, steam coils, etc. The size and weight of the trap permits installation in the piping without any other means of support. Condensation is discharged through a float operated valve located at the lowest point inside the trap body. Air vent is located in a by-pass in the cap or cover of the trap. Air passes through a passageway and out through the trap outlet. Construction permits removal of mechanism without disturbing the piping.

Marsh No. 500 Inverted Bucket Type Trap



This type is ideal for all types of hospital and kitchen equipment or similar service where a considerable volume of condensate is handled. The trap is self-venting, which, combined with the large water capacity assures unusually high efficiency in removing condensate, air and gases.

Marsh No. 17 Float and Thermostatic Trap

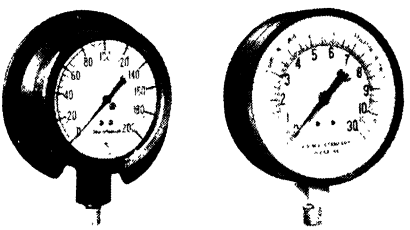


This trap is designed for removal of air and condensate from short steam mains, branches or risers. Operating characteristics adapt it for unit ventilators, unit heaters, and other equipment subjected to freezing temperatures when heating system is not in operation. Outlet discharge is water sealed at all times. Air vent is located in trap bonnet and air is normally discharged through a port directly to the outlet connection. A removable strainer protects mechanism. All working parts are made accessible by removing bonnet. The piping is all the support required for the No. 17 Trap.

Marsh Low Pressure Gauge

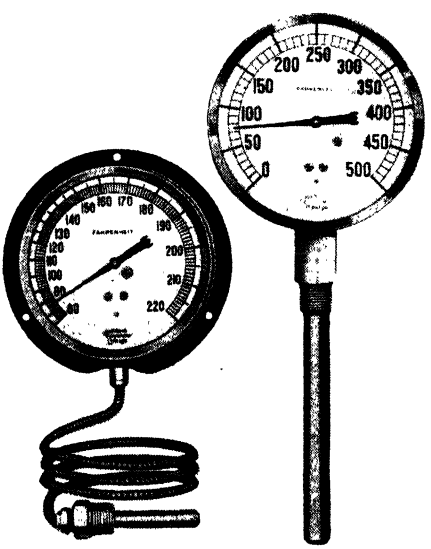
The Marsh *A.S.M.E.* standard, low pressure gauge will contribute to the economy and improve the operation of any type of steam boiler. It is finely built throughout and is available with the Marsh "Recalibrator" for quickly and easily resetting the hand to zero when the gauge is knocked out of adjustment.

Marsh Gauges include vacuum and compound types in a wide range of designs covering all services and pressures. Over 75 years of gauge manufacturing has reached its highest achievement in the Marsh "Mastergauge" for use where high pressures and temperatures are present and where maximum stamina and accuracy are essential.



Marsh Dial Thermometers

Have the same basic refinements found in Marsh Gauges. Typical Marsh Thermometers of bourdon tube type in self-contained and distant reading types are illustrated. They are available in either vapor tension or gas-filled types. Bimetallic types of dial thermometers are also available. Practically all temperature ranges up to 750° F. are covered. The "Recalibrator" is standard in all Marsh bourdon tube type thermometers. The Marsh line also includes recording thermometers.



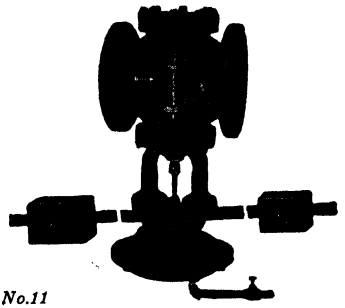
Ask for complete information covering any problem involving traps, vents, gauges, dial thermometers, packless valves, etc.

Mueller Steam Specialty Co., Inc.

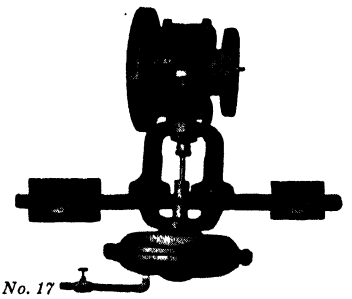
40-20 22nd Street, **Long Island City, N. Y.**

Steam, Water, Air, Oil and Gas Specialties for Heating and Power Plants

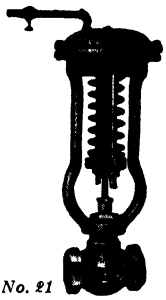
Pressure Reducing Valves—Straight Pattern and With Increased Outlet



No. 11



No. 17



No. 21

No. 11—For Vacuum, Vapor and Low Pressure Heating Systems. Initial Pressures, up to 200 lb; Reduced Pressures, 0 to 10 lb.

No. 17 and 21— For automatic control of reduced pressures on dead-end service, requiring a tight closing valve, such as tank heaters, kitchen utensils, sterilizing apparatus, laundry equipment, kettles, cookers, driers, etc. Initial Pressures up to 200 lb. Reduced Pressures 0 to 150 lb.

Constructed with full globe bodies. Center guide eliminates the wings on discs, and increases efficiency, assures minimum noise and prolongs the life of the seats and discs. Lever and weight operates on a steel roller bolt, assuring a most sensitive valve. Spring type furnished with special long springs for sensitive operation and wide ranges of reduced pressures.

No. 37

Water Pressure Reducing Valves

For controlling water pressures that require automatic and positive control of reduced pressures. Compact, and have full flow and renewable composition discs.

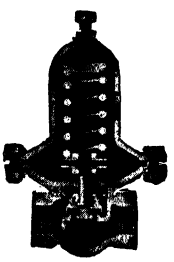
Standard and extra heavy weights suitable for all initial pressures and wide ranges of reduced pressures.

Diaphragm Operated Water Relief Valves

For relieving excessive pressure of hot or cold water, air, oil or gas.

Very sensitive, respond quickly.

Their construction is durable and compact, and accessible without disturbing pipe connections.



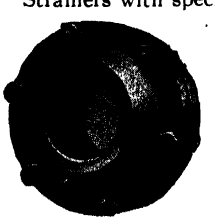
No. 63

Sediment Strainers for Steam, Water, Oil, Gas, Air, Etc.

For removing scale, cuttings, and other foreign matter from steam, water, air, oil and gas lines, or in connection with valves, pumps or other apparatus.

Furnished with iron bodies, plain or galvanized, with brass or copper mesh suitable for the service. Can be furnished all brass or nickel-plated iron or brass, or cast steel for extra high steam pressures, at additional cost.

Strainers with special mesh or of special metal furnished at a slight additional cost.



No. 125

Figures Nos. 145 and 165 Strainers have closed or open bottom baskets, so that the basket can be removed for cleaning, or all dirt and sediment can be blown out through bottom blow out connection.

No. 145

No. 165

CATALOG and BULLETINS covering our COMPLETE LINE gladly furnished on application.

Yarnall-Waring Company

Manufacturers of YARWAY Steam Specialties

133 Mermaid Ave., **Philadelphia 18, Pa.**

YARWAY IMPULSE STEAM TRAPS

Construction—The Yarway Impulse Steam Trap is unique in that there is only one moving part, the simple valve F. This trap is made of bar stock throughout, no castings used. For pressures up to 400 lb, body and bonnet of cold rolled steel, cadmium plated; cap of tobin bronze, valve and seat of heat treated stainless steel. For pressures 400 to 600 lb, trap is all stainless steel.

Operation—Movement of valve (F) is governed by changes in pressure in control chamber (K). At lower temperatures, condensate bypassing continuously through orifice in center of valve reduces chamber pressure below inlet pressure and valve opens, allowing free discharge of air and condensate through seat. As condensate approaches steam temperature, low chamber pressure causes vaporizing and the increased volume builds up pressure in control chamber, closing valve (F).

Other Advantages

Light Weight—Yarway traps need no support—½ in. trap weighs only 1⅜ lb. 2 in. trap weighs 8⅝ lb.

Small Size—Can be installed in cramped quarters—½ in. trap measures 2¼ in. long—2 in. trap, 4¾ in. long.

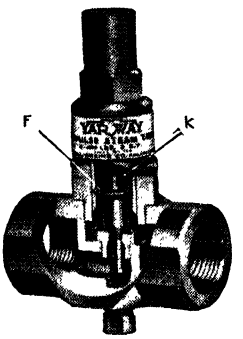
Will not air bind. *Require no priming.*

Insure quick heating.

Low Price—Often cheaper than repairing old traps.

Factory set to operate at all pressures up to 400 lb (or 600 lb) without change of valve seat.

Send for descriptive Bulletin T-1739.



List Prices, Weights and Dimensions

No. 60 Series—up to 400 lb and

No. 120 Series—up to 600 lb

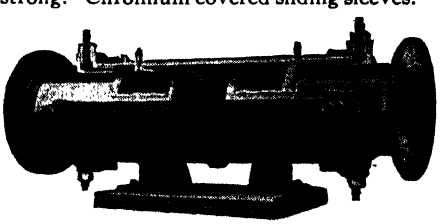
Size	Trap Complete	Weight Pounds	Length Inches
½" Nos. 60 or 120	$15.00	1¼	2⅝
¾" Nos. 61 or 121	22.00	2	3
1" Nos. 63 or 123	31.00	2½	3⅜
1¼" Nos. 64 or 124	48.00	4	3¾
1½" Nos. 66 or 126	68.00	5¾	4¼
2" Nos. 67 or 127	90.00	8½	4¾

Yarway Fine-Screen Strainers offer better protection against rust, scale and dirt for all steam equipment.

Made in ten standard sizes from ¼ in. to 3 in. Cadmium plated bodies. High grade Monel woven-wire screens. Many thousands in use. Write for Bulletin S-201.

YARWAY EXPANSION JOINTS

All-steel welded construction; light but strong. Chromium covered sliding sleeves.



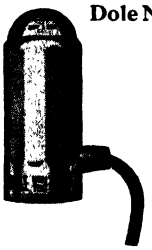
Cylinder guide and stuffing box integral, assuring perfect alignment. Internal limit stops. Gun-pakt and Gland-pakt types: Gun-pakt (illustrated) fitted with screw guns which permit addition of plastic packing while joint is under pressure. Sizes 2 in. to 24 in., single end or double end, flanged or welding ends; 150, 300 and 400 lb pressures. Also all-brass joints, ¾ in. to 2 in. For additional details send for Bulletin EJ-1911.

The Dole Valve Company

Main Offices and Factory: 1933 Carroll Avenue, **Chicago 12, Ill.**

THE ALL STAR LINE **Dole** AIR AND VACUUM VALVES

Selecting the right vent for a particular purpose is your assurance of the utmost efficiency and economy from one pipe steam heating systems. The Dole line covers every venting need and offers a complete choice for every purpose.



Dole No. 1A Vari-Vent Air Valve

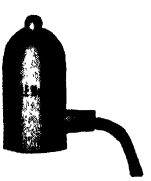
Modern gas, oil or stoker fired one pipe steam systems require QUICK venting. This radiator valve lets air escape twice as fast as ordinary valves and balances the flow of steam at the first "breath" of boiler pressure. Adjustable vari-vent feature gets air out of those "far away" radiators as quickly as those close to the boiler.

Dole No. 3 Air Valve

Vents radiators of hand fired gravity steam heating systems. Double shell construction provides separate passages for air and condensation—extra large float defeats spitting or water leakage. Complete venting assured at pressures up to 10 lbs.

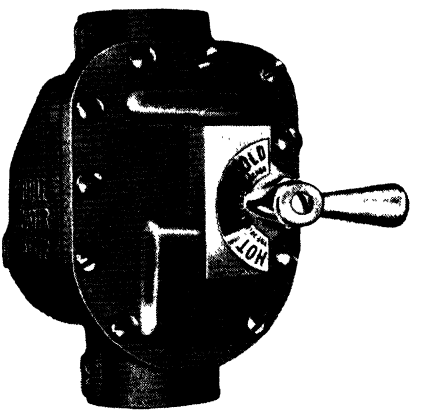
Dole No. 2B Vari-Vent Vacuum Valve

Adjustable radiator valve for "vacuumizing" and balancing gravity steam heating systems. Patented Dole bellows vacuum seal locks out air after it has been once expelled from the system. Easily adjusted vari-vent feature assists in equalizing steam flow to all radiators.



Dole No. 1933 Air Valve

Low cost valve for venting radiators of hand fired systems. Large float provides a seal against condensation to stop spitting.



Dole Water Mixer

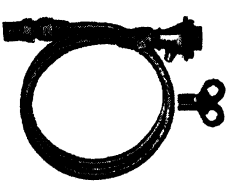
Specify Dole Water Mixers on all tankless heater installations. Dole Water Mixers will provide safer, tempered domestic hot water. Available in three sizes; ½ in., ¾ in. and 1 in. Adjustable temperature range controls domestic water to service from 125 to 175 deg F.

The use of a Dole Water Mixer increases the useable hot water of any tankless heater in that the draw through the heater is reduced, thus providing more time for heat absorption. The useable hot water is increased, too, because water at city temperatures is blended with the high temperature water discharged from a tankless heater.

Installation is accomplished easily and quickly at low cost.

Dole No. 14 Key Valve

Low cost venting device for concealed radiators and convectors of hot water heating systems. Protects panel fronts from rusty water stain.



Write The Dole Valve Company for complete catalog and handy selector chart which indicates the Dole Air or Vacuum Valve most suited for a particular need.

Jenkins Bros.

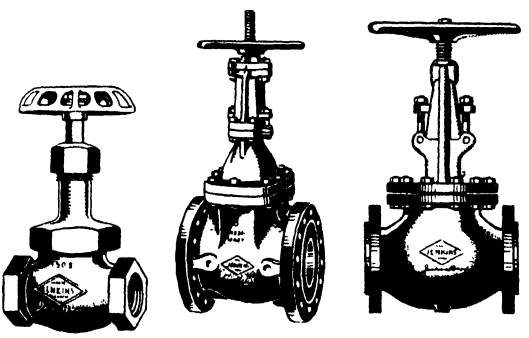
80 White Street, **New York 13, N. Y.**

BRIDGEPORT, CONN.; BOSTON, PHILADELPHIA, CHICAGO, SAN FRANCISCO, ATLANTA

LOOK FOR THIS DIAMOND MARK — REG. U.S. PAT. OFF. TRADE JENKINS MARK — Jenkins Bros

Leading Supply Houses Everywhere Stock Jenkins Valves

Jenkins VALVES for LIFETIME SERVICE



Bronze **Iron** **Steel**

FOR EVERY NEED

JENKINS CATALOG LISTS OVER 500 VALVES

Consult Jenkins Catalog for complete details on more than 500 different valves that cover practically all industrial plumbing and heating, and engineering requirements. Below is a brief list.

All-Iron Valves,—globe, angle, gate; **Angle Valves,**—bronze, steel, and iron body with bronze mounting or trimming.

Blow-Off or **Y Valves,**—bronze and iron.

Electrically Operated Valves, Gates, Globes, Angles, Fire Line Valves; Floor Stands; Foot Valves for gasoline service.

Gate Valves,—bronze, iron, steel; with solid wedge or double disc parallel seats; with removable bonnet and renewable bushing.

Globe Valves,—bronze, iron and steel; one piece and union bonnets; renewable and integral seats; rubber composition or metal discs and plugs.

Horizontal Check Valves,—bronze, iron and steel; **Hose Valves; Indicator Posts; Lock Shield Valves.**

Needle Valves; Non-Return Valves; Quick-Opening; Self-Closing Valves.

Radiator Valves; Rapid Action Valves; Regrinding Valves; bronze and iron body with bronze trimming; renewable plug seats and bevel seats of a special nickel alloy in globe, angle, check and swing check patterns.

Selclo Valves; Stop and Check Valves,—combination or automatic equalizing; Swing Check Valves,—bronze, iron and steel.

Stainless Steel Valves,—globe, angle, gate and check.

Underwriters' Pattern Valves, —check and gate; **Whistle Valves; Waterworks Valves.**

Carey PRODUCTS

The Philip Carey Mfg. Company

Lockland, Cincinnati 15, Ohio

Branches In All Principal Cities

CAREYDUCT is recommended wherever quietness, ease of installation, fire safety, fume resistance and good appearance are desirable or essential. Used in air conditioning systems widely before the war, Careyduct has proven itself on some of the largest governmental industrial and commercial installations in the country.

Write for engineering performance and installation data.

ACOUSTICAL. Careyduct is a natural sound absorber and non-conductor of sound. Quiets fan noise; won't pick up and "telegraph" other outside noises.

INSULATED. High-efficiency insulation assures delivery of hot or cold conditioned air to outlets with minimum change in temperature.

AIRTIGHT. Won't "breathe" or vibrate at high velocities. Slipjoint construction prevents leakage.

SAVES SPACE. Being 40% to 50% quieter than ordinary duct, Careyduct handles higher velocities, permitting the use of smaller sized ducts.

EASY TO INSTALL. Prefabricated Careyduct units are easy to install—particularly in tight places. Simple low cost fittings can be made in the shop or on the job.

FIREPROOF. Being 100% asbestos construction Careyduct won't smoulder or burn. Approved by *Underwriters' Laboratories, Inc.*

GOOD LOOKING. Surfaces are smooth and free from unsightly raised seams or joints. No stiffeners or braces. Blends well with modern interiors.

5 TYPES OF CAREYDUCT

Insulated and Acoustical Type. 100% asbestos construction—combines duct and insulation.

Key-lock Type. For high temperature applications up to 500 F. Impervious to water.

Single-wall Type. For heating and ventilating systems.

Reinforced Corner Type. Fabricated of Carey Firefoil or insulated sheathing. An ideal duct for large industrial installations.

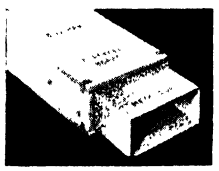
Asbestos-cement Type. Made of asbestos-cement wallboard in different thicknesses. Sizes: 23½ in. and up.

The Philip Carey Mfg. Company

Lockland, Cincinnati 15, Ohio

Branches In All Principal Cities

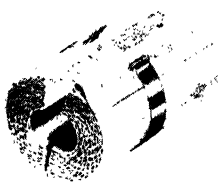
Carey PRODUCTS



CAREYCEL FOR AIR DUCTS

Uses: A fireproof, low cost, high efficiency asbestos board for insulating ducts and all types of air conditioning equipment.

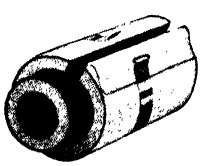
Description: Composed of 12 to 14 laminations of indented (not corrugated) asbestos felt per inch of thickness. Weight: approximately 1½ lb per board foot. Sheet Size: 36 in. x 36 in., or cut to order. Blocks: 6 in. x 36 in. Thickness: ½ in. up.



CAREYCEL FOR HEATING SYSTEMS

Uses: Pipe coverings and blocks for pipes, boilers, ovens and other apparatus where the temperature doesn't exceed 300 F.

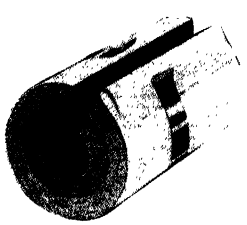
Description: Pipe covering sections 36 in. long by 1 in. thick, finished with cotton duck jacket and bands. Blocks: 6 in. x 36 in. Sheets: 36 in. x 36 in., or cut to order. Thickness: ½ in. up.



CAREY IMPERVO FOR COLD PIPES

Uses: A high efficiency insulation for cold or ice water pipes—keeps the water cold and prevents sweating.

Description: Laminated insulating felt with waterproof liner and jacket. 36 in. long in ½ in., ¾ in., double ½ in. and double ¾ in. thick sections, finished with cotton duck jackets and bands.



CAREY PROTECTO TO PREVENT FREEZING

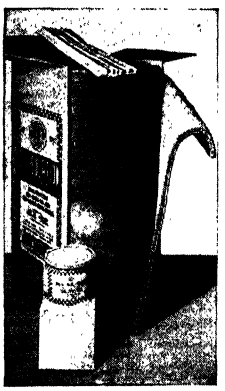
Uses: Designed especially to reduce the danger of freezing of exposed water pipes.

Description: Consists of an inner layer of hair felt, a waterproof felt liner and an outer layer of insulating felt. For severe conditions use two thicknesses. 36 in. long sections with cotton duck jacket and bands. One thickness only—approximately 1 in.

Grant Wilson, Inc.

141 West Jackson Blvd.
Chicago 4, Illinois

DUX-SULATION



Designed for efficient insulation of metal ducts in Heating, Ventilating and Air Conditioning equipment.

Dux-Sulation is composed of fine, flexible fibres fabricated into a strong felt with millions of dead air spaces, producing a thermal insulation efficiency of 70 per cent (K Factor .27 Btu). Saves 75 per cent of bare duct heat loss.

A heavy asbestos membrane is woven into the felt body below the surface, giving the protection of fire proof asbestos.

The outer surface is heavy woven fabric. A high sound deadening surface—absorbs 70 per cent of air borne noises—with low frictional resistance (F = 0.0001322).

Complete Package:—A flexible insulating blanket ½ in. and 1 in. thick. Comes complete with corner tape and adhesive for cementing on to sheet metal duct work. **Dux-Sulation** comes 36 in. wide in a roll containing 100 sq ft. Will not rot, chip or crack.

Surface Temperature of ½ in. Dux-Sulation applied to Metal Duct

Outside Duct Temperature	Room Temperature—Deg F			
	30	50	70	90
40° F	33	48	63	78
60° F	37	53	68	83
80° F	42	57	72	88
100° F	47	62	81	93
120° F	52	68	82	97
150° F	60	75	90	105

Dew Point Temperature—Deg F

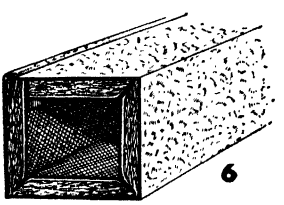
Relative Humidity	Room Temperature—Deg F (Dry Bulb)			
	30	50	70	90
20%	0	12	28	44
40%	10	27	45	64
60%	18	37	56	75
80%	25	44	64	84

Note: As determined through using the two Tables above, the Surface Temperature of the Dux-Sulation must be HIGHER than the DEW POINT to prevent condensation.

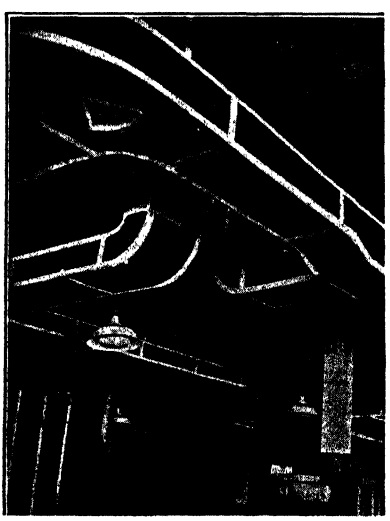
Asbestos Protected Dux-Sulation is applied to round pipes, rectangular ducts or irregular surfaces. It bends in any direction, even to very sharp and abrupt angles. The tape is applied to the corners and joints as illustrated.

Acoustical Values
70 Per Cent Reduction in Loudness

Frequency	Feet
1035	9.5
2048	9.7
4100	11.4
517	15.2
259	31.0
129	34.0



Dux-Sulation is also applied to the inside of ducts, as illustrated, for high sound absorption efficiency.



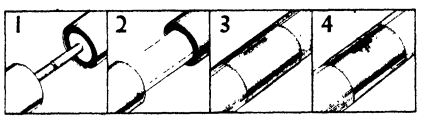
Durant Insulated Pipe Company

1015 Runnymede Street, P. O. Box 88

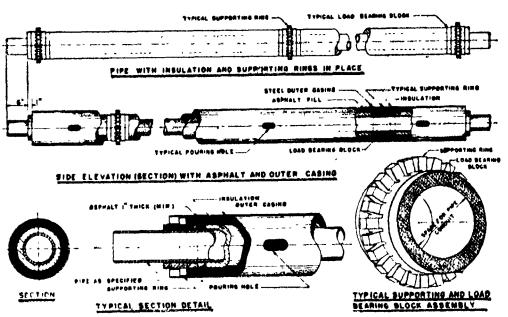
Palo Alto, California

TRADE-MARK
REG U S PATENT OFFICE

4 SIMPLE STEPS IN SEALING FIELD JOINTS



1. Field joint ready for inspection.
2. Joint covered with standard pipe insulation.
3. Special Durant joint casing in place ready for asphalt.
4. Asphalt poured in slot—to seal.



ADVANTAGES

- Completely waterproof.
- "Elimination" of electrolysis and corrosion.
- Requires no sub-drains.
- In multiple lines, individual Durant Pipes can be added, removed or replaced without disturbing others.
- Minimum trenching & field work.
- No rollers or pipe supports required.
- Tile or masonry protection not required.
- Lower field costs.
- Insulation protection is absolutely dependable.

CONSTRUCTION OF D.I.P.

The Durant Construction Principle involved consists of encasing the piping, or the insulation covering around the piping, with a heavy layer of High Melting-Point Non-Porous Asphalt. The asphalt is poured hot into a sheet metal form which is spaced concentrically around the pipe or insulation. For all underground conditions the thickness of the asphalt casing is one inch thick minimum for insulated piping. The insulation for all pipes carrying heat should be 85 per cent magnesia or Unibestos and for cold pipes either 85 per cent magnesia, Unibestos or moulded cork covering should be used. The thickness of the insulation will vary with the conditions of operation. See details in diagram illustration above.

Load bearing supports are provided within D.I.P. structure to prevent weight of pipe from resting on specified insulation. These load bearing supports are full circles slipped on between insulation sections at regular spacings during the fabrication of D.I.P. After covering and load bearing supports have been fitted to pipe, all joints are taped and sealed. A cylindrical jacket of heavy galvanized steel with a diameter large enough to provide a minimum 1 in. air space outside of the insulation, is placed concentrically around insulated pipe. This metal jacket has openings at regular intervals or a full length slot along the top. The insulated pipe is then ready to receive the asphalt protection which consists of a special grade of high-melting point asphalt heated to proper temperature and poured through openings in top of metal jacket.

INSTALLATION OF D.I.P.

Since the insulation and protection are factory-applied to D.I.P., field operations are limited to placing the pipe lengths into position, connecting them and then, after heat pressure tests, insulating and sealing the joints. In underground pipe systems, backfill can be made at once, and can be flooded with water to pack it. The system is completely waterproof as soon as the joints have been finished.

Foundations are practically never required for underground D.I.P. installations. The pipe needs merely to be placed on the bottom of the graded trench. Only comparatively narrow trenches are required and the individual lengths of D.I.P. can be readily lowered into the trench with rope slings. In the trench the pipe can be turned and slid into proper position and the exposed pipe ends provide plenty of clearance for workmen to connect and finish the joints.

H. W. Porter & Co.

INCORPORATED

Therm-O-Tile

REG. U.S. PAT. OFF.

817-G Frelinghuysen Ave., **Newark 5, New Jersey**

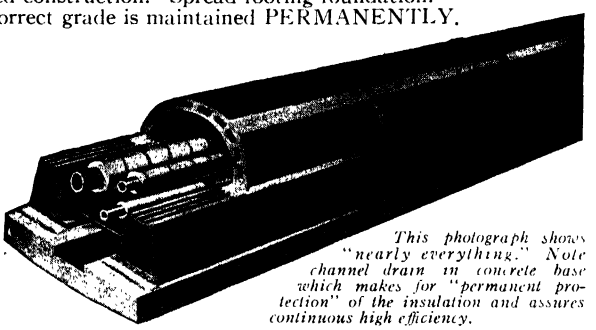
Permanent Protection and Insulation for Underground Pipe Lines

BALTIMORE, MD. CHARLOTTE, N. C. RICHMOND, VA.

Also sold and installed by Johns-Manville Construction Units in all principal cities.

This is what you get with Therm-O-Tile:-

1—Higher efficiency. Much better insulation. A truly DRY conduit.
2—Greater strength. Arched construction. Spread-footing foundation.
3—Long-lasting life. The correct grade is maintained PERMANENTLY.
4—No leakage. Positive sealing throughout.
5—Most convenient installation—on a concrete "sidewalk."
6—No condensation pockets at any time.
7—Greater economy.
8—Experienced engineering.
9—Competitive first cost, and definitely lower ultimate cost.



This photograph shows "nearly everything." Note channel drain in concrete base which makes for "permanent protection" of the insulation and assures continuous high efficiency.

THERM-O-TILE
STEAM CONDUIT SYSTEMS

"Long-Lasting"—Now that Therm-O-Tile has been on the market so many years, and its design is so well known by all leading heating and ventilating engineers, we again wish to emphasize the importance of "Permanent protection." It is not difficult to provide TEMPORARY protection and insulation for underground pipe lines. Threads and joints don't fail immediately, and foundations don't sag immediately, but unless the job is properly done in the first place it won't be long before water seeps in and ruins the insulation. So, watch out. With wet and spoiled insulation, efficiency drops drastically. Unless the conduit is built on a truly solid foundation there will be sagging and collection of water in pockets.

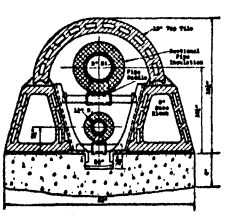
Ample Drainage, Always—In the Therm-O-Tile concrete base there is a drainage channel—clearly visible in photograph—which carries off all water that may enter the conduit from any source, thereby keeping the insulation PERMANENTLY dry. Drainage is entirely internal. The channel is accurately and PERMANENTLY sloped so that condensate or other pockets cannot form. Open to thorough inspection at any time at manholes. Amply large to keep the pipe space dry at all times.

"Spread Footing" Foundation—Positively preventing settling or sagging the Therm-O-Tile "Spread Footing" foundation base is a thick concrete slab poured directly in the trench bottom. Steel reinforced or placed on piles when installed over filled or boggy ground to insure PERMANENT protection.

Already Told—In previous issues of this GUIDE we gave details regarding the Tile Envelope which produces 27 different conduit cross sections. We told about the ideal accessibility of this conduit, its great strength, how it is water-proofed, and so on. For complete information ask for Bulletin 381.

Our Engineers Co-Operate—They have had exceptional experience in designing and installing steam conveying equipment for nearly every purpose.

Competitive in Cost—Despite the high efficiency, greater strength, dependability, and other outstanding features that are obtained in Therm-O-Tile, it is nevertheless competitive in total first cost. Final cost is much less, thanks to its permanence.



Single or Multiple Pipe Lines Using Sectional Pipe Insulation.

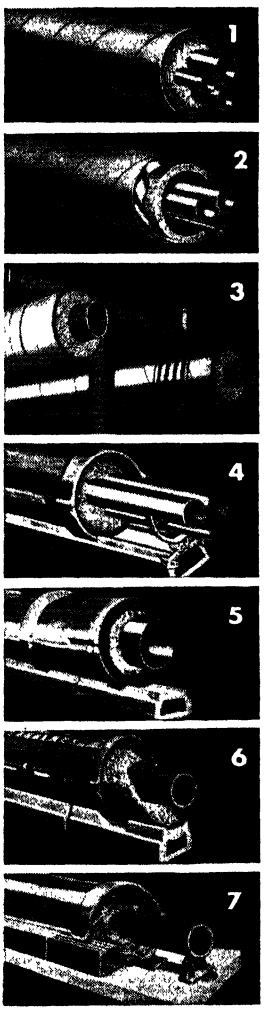
Showing a typical Therm-O-Tile piping arrangement when there are two pipe lines. Note the channel drain which "permanently protects" the insulation.

The Ric-wiL Company

INSULATED PIPE CONDUIT SYSTEMS

Union Commerce Bldg., Cleveland, Ohio • Agents in Principal Cities

There is a Ric-wiL insulated conduit system engineered to your specific needs—the transmission of steam, hot water, oil, hot or refrigerated process liquids—providing heat transfer with the lowest possible loss.



1. RIC-WIL INSULATED PIPE UNIT—SINGLE OR MULTIPLE PIPES

Prefabricated complete units with one or more pipes—in any specified combination—in helical corrugated conduit, coated and wrapped with asphalt saturated asbestos felt. 21-ft lengths for easy installation. Insulation is applied to any or all pipes in any thickness specified.

2. RIC-WIL INSULATED PIPE UNIT—FOR PROCESS LIQUIDS

An adaptation of the multiple system used where a steam or hot water line heats fluids in other lines. Pipes are insulated from the exterior but not from each other. Sizes and specifications as required—conduit same as for other insulated pipe units.

3. RIC-WIL FOILCLAD PIPE UNITS—FOR OVERHEAD LINES

Pipe and insulation are protected and waterproofed by a double coating of machine-applied, high temperature asphalt. Unit is then wrapped with asbestos felt and covered with a final spiral wrapping of copper or aluminum foil for maximum insulation and protection.

4. RIC-WIL STANDARD TILE CONDUIT—TYPE F

Vitrified glazed *A.S.T.M.* Standard Tile Housing—acid and waterproof—with foundation type base drain supporting weight of piping through correctly engineered pipe supports. Positive locked-in-place cement seals on sides and ends. For single or multiple pipes.

5. RIC-WIL SUPER TILE CONDUIT—TYPE F

Same advantages as Standard Tile but with walls approximately double thick for strength under heavy traffic or where overhead load is above normal. Will support concentrated static load of 6 tons per wheel under actual installation conditions. Base drain of extra-heavy tile.

6. RIC-WIL CAST IRON CONDUIT—TYPE F

Heavy reinforced cast iron conduit for use where underground pipe lines run close to or under railroad tracks. Durable, water-tight and vibration-proof. Positive locked-in-place cement seals on sides and ends with metal clamps for extra tightness.

7. RIC-WIL TILE CONDUIT—UNIVERSAL TYPE

Where installation conditions dictate the use of a concrete pad Ric-wiL Universal Tile is recommended. Side walls are double-cell vitrified trapezoidal block design. Arch may be Standard Tile, Super-Tile, or Cast Iron.

Ric-wiL accessories are available in all type systems; standard and special fittings, factory fabricated or field fabricated expansion devices, alignment guides, and anchors. Descriptive bulletins on request. ***Write:*** **The Ric-wiL Co., Dept. 278**

American 3 Way-Luxfer Prism Co.

431 S. Dearborn St., **Chicago-5, Ill.**

3-WAY Daylighting Products

26-20 Jackson Ave., **Long Island City,** N. Y.

AMERICAN GLASS BLOCK SKYLIGHTS

Light-Up—the AMERICAN *Way!*

American 3-Way Rooflights make use of Glass Blocks of special design and strength, manufactured by the proven process, incorporating designs on inner surfaces of plates, resulting in uniform even light distribution over wide areas, leaving top and bottom surfaces smooth for easy cleaning.

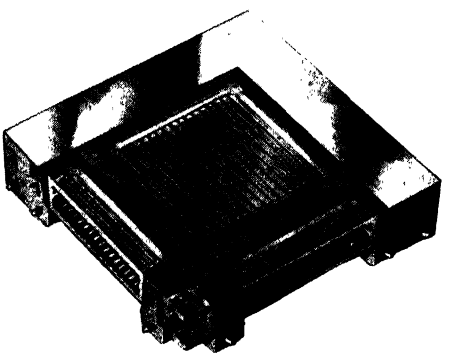
Glass Blocks are 9 in. x 9 in. x 2½ in. and spaced approximately 10⅝ in. on centers.

Low Heat Transfer

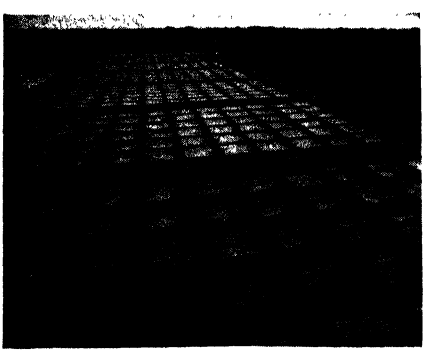
Tests conducted by methods suggested by the A.S.H.V.E. Code show that Glass Block Rooflights have about two and one-half times the insulating value of sheet metal skylights with no heat losses by "escape," since the construction is air-tight.

Solar Heat Transmission

Reduction in total solar heat gain as compared with ordinary windows is indicated by relative values given in Table 18 and Table 20 in Chapter 15.



Section of American Glass Block Skylight Showing Method of Block Application



American Glass Block Skylight

Triple Plates of Glass

Magnalite Diffusing Glass units may be attached to under side of glass block construction thus making for effective uniform light diffusion and even distribution; also very effective in condensation problems.

Insulated Construction

Construction of rigid reinforced concrete grids can be arranged with insulation materials sufficient to approximately equal the performance of the glass blocks.

Condensation

Due to the nature of the grid construction where insulation materials are employed with semi-vacuum glass blocks assemblies there is little or no tendency for condensation to form on the under side. Should relative high humidities or abnormal conditions exist, further insulation treatment can be provided.

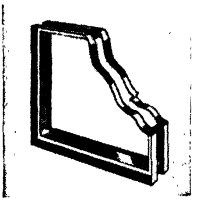
Glass Block Assemblies for all off-vertical arrangements are available. Details will be furnished on request.

3-Way Glass Block Skylights may also be furnished without special insulation treatment in reinforced concrete grid construction.

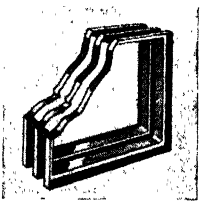
Write for Complete Information

Libbey·Owens·Ford Glass Company

Nicholas Building, **Toledo 3, Ohio**



THERMOPANE*
Insulating Glass



L-O-F Thermopane is a transparent factory-fabricated insulating glass unit composed of two or more panes of glass separated by ¼ in. or ½ in. of dehydrated captive air, hermetically sealed at the edges in the factory with a metal-to-glass bond.

Thermopane is made in more than 60 standard sizes, all of which can be used vertically or horizontally. The glass is specially cleaned before the patented Bondermetric seal is applied. The layer of air inside the Thermopane units is scientifically cleaned, dried and hermetically sealed. The patented, metal-to-glass seal bonds the two or more panes of glass into one unit to prevent dirt and moisture from entering the air space.

Thermopane Reduces the coefficient of heat transmission; increases the room-side surface temperature, thus promoting radiant comfort and lowering the dew point; furnishes a control of light quantity and quality through combinations of various types of glass, and deadens sound transmission to some degree.

Thermopane Uses are many, but may be briefly summarized as below:

Double-glass Thermopane: Glazing of wood or metal windows, doors and window walls for practically any purpose in structures requiring heating or air conditioning.

Triple-glass Thermopane: Large stationary units such as insulated glass walls in homes, apartments, public and commercial buildings and in show windows for refrigerated display where temperature differential must be considered.

Quadruple-glass Thermopane: Engineered to meet low temperature and high humidity conditions.

Thermopane Units provide a high resistance to heat flow, varying with the number of panes and the thickness of the air space used. In summer the low heat transmission coefficient reduces the load on air conditioning systems. In winter it saves heat. The greater efficiency of Thermopane makes it possible to incorporate larger windows in houses and keep the cost of fuel constant. For example, a house could have 107 sq ft of Thermopane instead of 35 sq ft of single glazing and not lose any more heat. Thermopane permits the influx of solar heat in exterior glazing of buildings without a prohibitive compensating loss from conduction.

*Reg. U. S. Pat. Off.

The over-all heat transmission coefficient U varies with the ranges of temperature at which the coefficient is determined. For most practical heat loss calculations coefficient U can be the value determined at zero deg outside temperature, 70 deg inside temperature, 15 mph outside air velocity, 0.25 mph average inside air velocity. The following table gives such values from actual tests with glass sizes 30 in. x 30 in.

Number of Panes	Glass Thickness	U Value		
		Air Space		
		None	¼″	½″
Single Glass	⅛″ ¼″	1.16 1.15		
Double Thermopane (one air space)	⅛″ or ¼″		.65	.58
Triple Thermopane (two air spaces)	¼″		.47	.40

The Room Side Surface Temperature of Thermopane is considerably higher than that of single glazing. Usually radiators or registers are near glass areas in buildings to offset conducted heat loss from a room and radiant loss from the bodies of persons near cold glass areas. The higher glass surface temperature of Thermopane greatly reduces the amount of heat which must be supplied, permitting more flexibility in room design.

Another Important Benefit from Thermopane is the prevention of frost or condensation from forming on the room-side surface of a single pane of glass in winter due to higher room humidity. The absence of condensation on the room-side surface of glass is of considerable importance where clear visibility is a factor as in residences, all types of commercial or industrial buildings and refrigerated display spaces.

More Complete Information on Thermopane is available by writing to Libbey-Owens-Ford, or its district office nearest to you, and requesting technical data sheets prepared by Don Graf, a general booklet about the product, and a brochure which discusses Solar Housing.

Pittsburgh Corning Corporation

Room 500-8, 632 Duquesne Way **Pittsburgh 22, Pa.**

PC FOAMGLAS INSULATION

When installed according to our specifications for recommended applications, PC Foamglas retains its original insulating efficiency *permanently.*

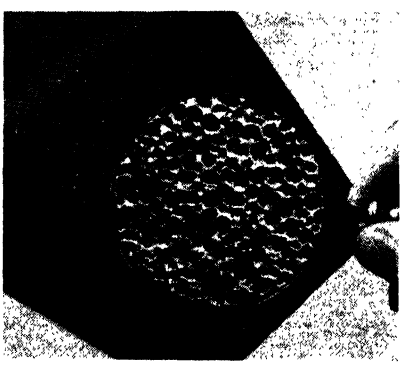
PC Foamglas is a cellular glass insulating material having unique characteristics. It is not a fiber, not a wool, not a board nor a batt. Consists of millions of glass enclosed air cells, in the form of big, rigid light-weight blocks.

Being glass, PC Foamglas is highly resistant to the fumes, acid atmospheres, vapors and other elements that so often cause deterioration of other insulating materials.

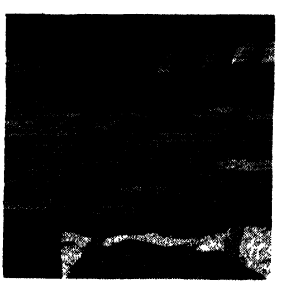
PC Foamglas has proved its ability to help maintain desired temperature levels and to minimize condensation--without maintenance, repairs or replacement--resulting in worthwhile economies. It is widely used in ductwork and core walls, on roofs and floors. As a pipe insulation, PC Foamglas can be used to insulate both hot and cold piping, indoors and outdoors. Note the illustrations of some typical applications.

When you are figuring on insulation, make sure that you have the latest information on PC Foamglas. Send for our booklets on wall, floor and roof insulation. They tell you what you want to know. Pittsburgh Corning Corporation also makes PC Glass Blocks.

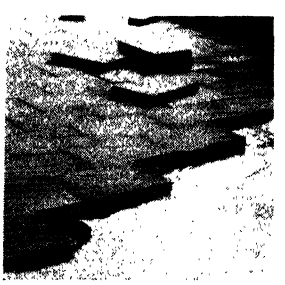
When you insulate with **PC Foamglas** you insulate for good



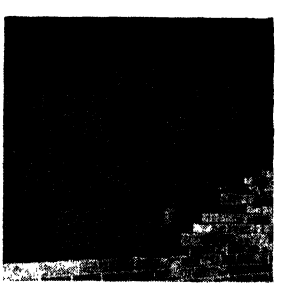
Here's the secret of permanent insulation. PC Foamglas is composed of tiny glass cells . . . millions of them. And these cells are filled with sealed-in air. PC Foamglas has the unique advantage of retaining *its original insulating value—permanently.*



This picture shows how PC Foamglas is applied to roofs. The Foamglas is laid on the roof deck, the specified number of plies of roofing felt are built up on the firm base which is provided by big solid blocks of PC Foamglas.



PC Foamglas, under the concrete cover-floor, prevents heat travel to and from this room. It helps to control temperature and minimizes condensation. Strong and rigid, PC Foamglas will support heavier than normal floor loads.



In core walls, PC Foamglas supports its own weight when laid between brick, tile, blocks and many other types of backing and facing. It helps control temperature and minimize condensation. It will not pack, rot or check.

Pittsburgh Corning Corporation

Room 702-8, 632 Duquesne Way, Pittsburgh 22, Pa.

PC GLASS BLOCKS

Distribution through Pittsburgh Plate Glass Company Warehouses in principal cities and by the W. P. Fuller Company on the Pacific Coast and by Hobbs Glass Ltd. in Canada. Also makers of PC Foamglas Insulation.

Glass Blocks allow the economical use of large glass areas, reduce heat loss in cold weather and materially aid air-conditioning. This is because each PC Glass Block contains a sealed-in dead-air space that is an effective retardant to heat transfer.

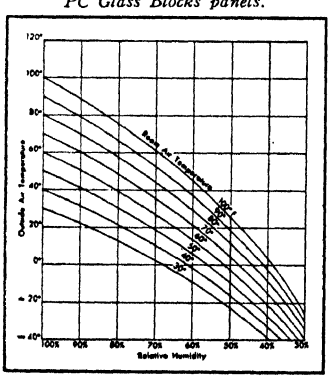
Thermal Insulation

Tests run by nationally recognized laboratories have established the value of glass blocks for insulation of light-transmitting areas. These tests have proved that with glass block panels, heat loss is slightly less than half that experienced with single-glazed windows. In computing heat losses through panels for most design purposes, it is recommended that a "*U*" value of 0.46 to 0.49 be used for all block sizes and face patterns. For complete data on heat transfer values see the section on heat transfer elsewhere in this Guide—page 136.

Surface Condensation

Due to high insulating value, condensation will not start forming on the room side of glass block panels until outside air has reached a temperature much lower than that necessary to produce condensation on single-glazed windows. The accompanying chart shows at what temperatures condensation will form..

Outdoor temperature required to produce Condensation on the room side surface of PC Glass Blocks panels.



For example, with inside air at 70°F and relative humidity at 40 per cent. condensation will not begin to form on the interior surfaces of a glass block panel until an outdoor temperature of −14 deg is reached. Under similar conditions with single-glazed sash, moisture will begin to form when the outdoor temperature reaches +33°F.

Solar Heat Gain

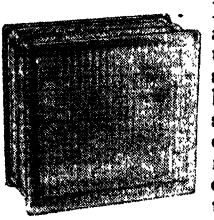
The use of glass blocks for light-transmitting areas results in a marked reduction in total solar heat gain as compared with ordinary windows. This factor is of considerable advantage in buildings that are properly air-conditioned, but does not eliminate the need for adequate ventilation or shading in non-air-conditioned rooms.

For data on solar heat gain through glass blocks see table 10 in the solar radiation section of this Guide—chapter 15. This table is for standard pattern glass blocks.

PC Glass Blocks Aid Air-Conditioning

Two of the chief aims of air-conditioning—temperature control and cleansing of air are aided by the use of PC Glass Blocks. Heat loss is less in winter—heat gain is less in summer. Ideal conditions are much more easily maintained without undue condensation. Solar heat transmission and radiation are reduced. Neither dirt nor drafts can filter in, for each panel is a tightly sealed unit.

Sizes and Shapes Available



PC Glass Blocks are available in ten attractive patterns, some of the patterns being designed for special control and direction of transmitted daylight. For complete information on the sizes and shapes of PC Glass Blocks, and for illustrations of the many patterns available, write the Pittsburgh Corning Corporation, Pittsburgh, Pa., or call the nearest Pittsburgh Plate Glass Company warehouse.

• • •

Additional technical data, including detailed figures on thermal insulation, solar heat gain, surface condensation, light transmission and construction data, will be furnished on request.

Owens-Illinois Glass Company

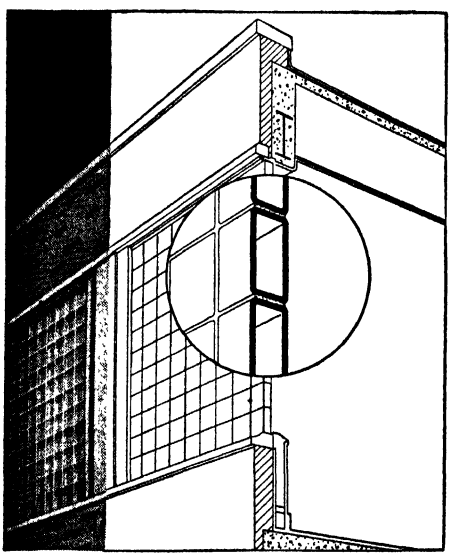
INSULUX PRODUCTS DIVISION, Toledo 1, Ohio

GLASS **INSULUX** BLOCK

Dealers in all principal cities

Insulux Glass Block Give Better Control of Interior Conditions

Insulux Glass Block are hollow, partially evacuated units, 3⅞ in. thick. Faces are smooth or ribbed. Solid panels of these block, laid in mortar, make a light-transmitting wall of high insulating value. Their proper use aids control of interior conditions to a point where initial and operating cost of heating or cooling equipment is reduced.



Conductivity

The *U* factor for ribbed glass block is 0.46; smooth face, 0.49. For design purposes, these factors may be used as constant for either 6 in., 8 in. or 12 in. block. See Chapter 6 of this volume for additional data.

This *U* factor is only 43 per cent of that of ordinary light-transmitting materials. The reason lies in the two heavy glass surfaces separated by partially-evacuated and hermetically sealed dead air space.

Surface Condensation

Because of the low overall air-to-air heat transfer, the room condensation point of a glass block panel is much lower than that of ordinary windows. This will permit higher humidities for both comfort air-conditioning and in industries where high humidity is part of the process. Glass block are not subject to deterioration caused by moisture.

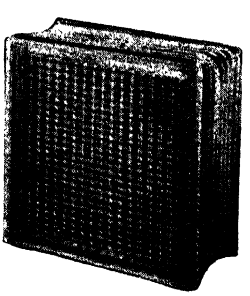
Infiltration

Insulux Glass Block are sealed in the building. They form a barrier against infiltration of dust, air and vapor. Winter drafts and summer vapor leakage are cut. Natural ventilation requirements can be met by installation of windows either inset in the panels or installed directly below the panels.

Solar Heat Gain

A comparative test showed 94 per cent more solar heat through steel sash than through glass block. However, as with sash, glass block transmit less solar heat when properly oriented and shaded. Data in Table 18, Chapter 15 of this GUIDE are for standard block. Other designs, such as the No-glare and Directional block afford further reduction. Data will be sent on request.

Design, Sizes, Erection



Insulux Glass Block is made in 10 face patterns for residential or industrial uses. Sizes are: 5¾ in. x 5¾ in., 7¾ in. x 7¾ in. and 11¾ in. x 11¾ in. All are 3⅞ in. thick. Blocks are erected by laying in mortar like any masonry material. *Complete technical data, description, etc., sent to you on request.*

American Flange & Manufacturing Co. Inc.

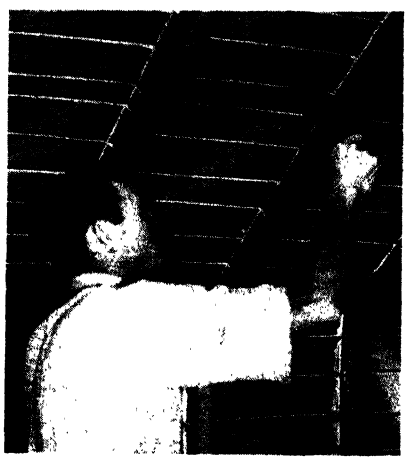
30 Rockefeller Plaza, New York 20, N. Y.
Circle 7-3741

Ferro-Therm

Reg. U. S. Pat. Off.

STEEL INSULATION

FULLY PROTECTED BY U. S. AND FOREIGN PATENTS ISSUED AND PENDING



Installing Ferro-Therm

Ferro-Therm Steel Insulation, made from rigid steel sheets with a special alloy coating, reflects 90 per cent to 95 per cent of all radiant heat. This high reflectivity, combined with extremely low heat storage capacity, provides maximum insulating efficiency in a minimum overall thickness.

Saves Pay Space and Weight

In building construction, the general practice is to install one sheet of Ferro-Therm between roof rafters or over ceiling joists and between studs of exterior walls. In cold storage construction, the number of sheets of Ferro-Therm depends on the temperature to be maintained and the U value required. The k value of Ferro-Therm, based on tests, is listed in the Data Book of the *American Society of Refrigerating Engineers* as 0.226 Btu per (hr) (sq ft) (°F temperature difference). Laboratory tests and thousands of applications have demonstrated that a wall of Ferro-Therm will provide insulating efficiency equivalent to a wall of mass insulation approximately twice as thick.

Assures Rapid Pull Down of Temperature

The low heat storage capacity of Ferro-Therm is extremely important in achieving rapid pull down of temperature, and in saving refrigeration costs for the initial and each subsequent cooling of space. Specifically, the heat storage capacity of a single sheet of No. 38 gauge is 0.029 Btu per (hr) (sq ft) (°F temperature difference). This is approximately 1/16 of the heat storage capacity of 1 sq ft of 1 in. thickness corkboard.

Permanent, Fire-proof Insulation

Ferro-Therm construction eliminates trapping of moisture condensate, with subsequent deterioration of the construction. As it is all-metal, Ferro-Therm cannot be penetrated by rodents, vermin or termites, and is absolutely non-combustible. The value of Ferro-Therm for fire protection is apparent.

125° Below Zero Maintained in Altitude Test Chambers

Ferro-Therm has proved its superiority in buildings, cold storage rooms, refrigerated cabinets, locker rooms, dry ice containers, refrigerated railway car construction, ovens, high-temperature storage tanks—in fact, practically every type of application where high insulating efficiency with economies in space and weight are a requisite. The most notable demonstration of Ferro-Therm performance has been its selection for the insulation of altitude chambers for the testing of Army and Navy aviation equipment and personnel. In these chambers, temperatures as low as −125° F were maintained, with a temperature drop of +70° F to −70° F in 10 to 12 min.

Our catalog, giving data and installation details on Ferro-Therm, will be sent upon request.

Armstrong Cork Company

Building Materials Division

Lancaster Pennsylvania

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TACOMA 2 WASH.....Asbestos Supply Co. of Tacoma

For detailed technical information, samples, and descriptive literature, ask any office or distributor. Specifications appear in Sweet's Catalogs for Architects, Engineers, and Power Plants.

PRODUCTS—Armstrong's Corkboard, Cork Covering, Mineral Wool Board—Foamglas*, Heat Insulations, Armstrong's Insulating Refractories, Cushiontone, Temlok**, Insulation Sundries.**

Corkboard

The thermal conductivity of Armstrong's Corkboard is 0.27 Btu per hour, per degree temperature difference, per inch thickness at 60°F mean temperature. It is furnished in rigid boards 12 in. x 36 in., 18 in. x 36 in., 24 in. x 36 in., and 36 in. x 36 in., in 1 in., 1½ in., 2 in., 3 in., 4 in., and 6 in. thicknesses. **Armstrong's Corkboard conforms in all details to Federal Specification HH-C-561b.**

Cork Covering

Armstrong's Cork Covering is made of pure cork in sizes to fit all standard pipe sizes. The inside surfaces of each piece are machined to assure an accurate fit, free from moisture-catching air pockets. Cork covering is rigid and will not sag. Thicknesses are: Light Duty (1.20 in. to 1.93 in.); Standard (1.70 in. to 3.00 in.); and Heavy Duty (2.63 in. to 4.00 in.).

Armstrong's Fitting Covers are rigid and are designed to fit accurately all types of standard ammonia and extra heavy fittings, screwed, flanged, and welded.

Mineral Wool Board

Armstrong's Mineral Wool Board equals or exceeds Federal Specification HH-M-371a for board or block form insulation; has low thermal conductivity; is moisture resistant, odorless; is easily handled and erected; possesses structural strength. Standard size 12 in. x 36 in.; thicknesses 1 in., 1½ in., 2 in., 3 in., 4 in.

Foamglas

Foamglas has a closed cellular structure which will not permit passage of air or moisture. It is efficient, moistureproof, fireproof, and offers effective, lasting insulation. This new type of insulation is made in standard 12 in. x 18 in. blocks; thicknesses 2 in., 3 in., 4 in., and 5 in. It may be used to insulate all types of low-temperature storage rooms.

Heat Insulation

The Armstrong Cork Co. distributes and offers contract service on a complete line of high temperature insulations. Included are: 85 per cent magnesia block and pipe covering; high temperature block and pipe covering; air cell block, sheet, and pipe covering; wool felt; hair felt; etc.

Engineering and Contract Service

All Armstrong offices and distributors maintain skilled erection crews. For aid in the solution of any technical problems involving insulation or acoustical treatment, and for literature and prices, get in touch with an Armstrong district office or distributor or the Armstrong Cork Co., Building Materials Division, Lancaster, Pennsylvania.

*T. M. Reg. U. S. Pat. Off., Pittsburgh Corning Corp.
**T. M. Reg. U. S. Pat. Off.

Baldwin-Hill Co.

549 Breunig Avenue, **Trenton 2, N. J.**

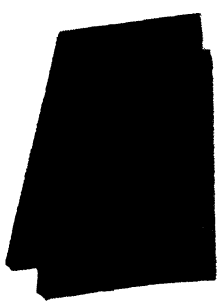
Plants in

TRENTON, N. J. KALAMAZOO, MICH. HOUSATONIC, MASS. HUNTINGTON, IND.

B-H No. 1 INSULATING CEMENT

A plastic insulation produced from high-temperature-resisting, nodulated B-H *black* Rockwool combined with high-grade, long-fibre asbestos and colloidal clay. Effective up to 1800 F; reclaimable up to 1200 F. Suitable for insulating large or small irregular surfaces, including those not suited to molded types of insulation. Contains a special *rust inhibitor* which prevents corrosion taking place between insulated surface and cement. Makes a secure bond on either hot or cold surfaces. Instantly adhesive, easy and economical to apply. When mixed with water to trowelable consistency, the nodules of B-H *black* Rockwool retain their physical properties; when dried out, the dead air cells in these nodules provide maximum insulating efficiency. Packed in strong 50-lb bags; can be stocked without breakage or loss.

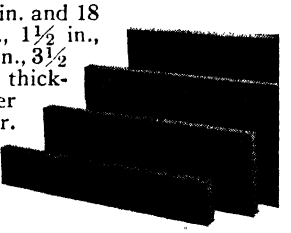
B-H KOLDBOARD



Effective from −150 to 300 F. Made from 100 per cent chemically stable B-H Rockwool fibres, felted and bonded together to form flat, semi-rigid blocks which do not disintegrate or break down structurally under severe service conditions. Koldboard will not support combustion nor smolder when flame is applied. Low moisture absorption: 0.68 per cent at relative humidity of 65 per cent at temperature of 75 F. Thermal conductivity: 0.29 Btu/sq ft/hr/F at a mean temperature of 70 F. Standard sizes: 18 in. and 36 in. long; 6 in., 12 in., 18 in., 24 in. wide; ½ in. to 4 in. thick; packed in high test fibre cartons.

B-H MONO-BLOCK

A one-block insulation effective over the full temperature range up to 1700 F. Fabricated of high-temperature-resisting B-H *black* Rockwool, felted by a special patented process. A strong, light-weight block, easily cut and fitted on irregular or flat surfaces. Low alkalinity factor insures stability under severe temperature conditions. Density—approx. 20 lb per cu ft. Standard sizes: 18 in. and 36 in. long; 6 in., 12 in. and 18 in. wide; 1 in., 1½ in., 2 in., 2½ in., 3 in., 3½ in. and 4 in. thicknesses. Other sizes to order. Packed in high-test cardboard cartons.

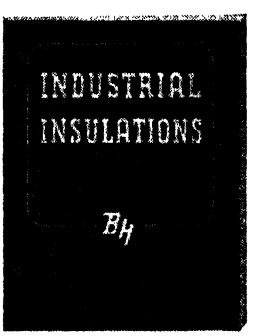


B-H DUCT SOUNDLINER

A rigid material felted of chemically stable Rockwool fibres. Provides an effective means of minimizing sound transmitted through the ducts, by installing it inside the ducts, also provides thermal insulation. Does not disintegrate nor support combustion. Easily cut and fitted around bends in the duct—attached with either bolts or specially prepared acoustical cement. Standard sizes: 24 in. x 36 in.; ½ in. or 1 in. thickness.

CATALOG ON REQUEST

We invite you to write for fully illustrated catalog giving more detailed specifications on these and other B-H Industrial Insulation Products of many types.



The Celotex Corporation

General Offices

120 South LaSalle Street, **Chicago 3**

CELOTEX

REG. U. S. PAT. OFF.

Celotex Cane Fibre Insulation products are made by felting the long, tough fibres of bagasse into strong, rigid boards. They are manufactured under the Ferox Process (patented) which effectively protects them from destruction by termites, fungus growth, and dry rot. They are integrally water-proofed which insures a non-hygroscopic insulation of low capillarity and enduring insulating efficiency.

Celotex Insulating Sheathing

An insulating, weather-resisting sheathing for use under any type of exterior. Surfaces and edges are moisture-proofed with a surface impregnation of asphalt.

Sizes: $^{25}/_{32}$ in. thick: 4 ft wide: 8 ft, 9 ft, 10 ft and 12 ft long.

Celotex Insulating Lath

Regular Insulating Lath—A cane fibre plaster base of high insulating efficiency. Surface provides a strong bond for plaster and the bevelled edges and shiplap joint provide additional reinforcement.

Size: 18 in. x 48 in.; thickness: $\frac{1}{2}$ in.

Celotex Roof Insulation

Regular Roof Insulation—A cane fibre product possessing superior insulating properties. It reduces roof heat transmission as shown by coefficients established in THE GUIDE; reduces roof movement due to contraction and expansion.

Size: 23 in. x 47 in.; thickness: $\frac{1}{2}$ in., 1 in., $1\frac{1}{2}$ in. and 2 in.

Cemesto

A completely fabricated fire and moisture resistant structural insulating wall unit. Consists of a Celotex cane fibre core surfaced on both sides with a $\frac{1}{8}$ in. layer of asbestos-cement board. The established low thermal conductivity of the Celotex core is maintained in the manufacture of Cemesto.

Sizes: 4 ft x 4 ft, 4 ft x 6 ft, 4 ft x 8 ft, 4 ft x 10 ft, 4 ft x 12 ft; thicknesses: $1\frac{1}{8}$ in., $1^{9}/_{16}$ in. and 2 in.

Celo-Siding

A weather-resistant, insulating, structural siding. Replaces wood or other sheathing materials and provides the exterior finish as well. Made of a Celotex cane fibre core that has been asphalt coated on all sides and edges. The weather side is additionally coated with a high grade asphalt into which mineral granules are firmly embedded.

Sizes: Thickness, $\frac{5}{8}$ in. and $\frac{7}{8}$ in.; $\frac{5}{8}$ in.—4 ft x 8 ft (square edges only); $\frac{7}{8}$ in.—2 ft x 8 ft tongue and groove (long edges only), and 4 ft x 8 ft, 4 ft x 10 ft (square edges only).

Celotex Rock Wool Products

Available in the following forms—Loose, Granulated, and Paper-backed Batts. Celotex Rock Wool is made from the clean fibres of molten rock. It is incombustible and integrally waterproofed.

Q-T Ductliner

An acoustical material designed especially for duct lining in air conditioning systems. Absorbs duct noises. Made of rock wool and a special binder. Designed to withstand air duct humidity conditions. Is fire resistant and will not smoulder or support combustion. Thermal conductivity of 0.30.

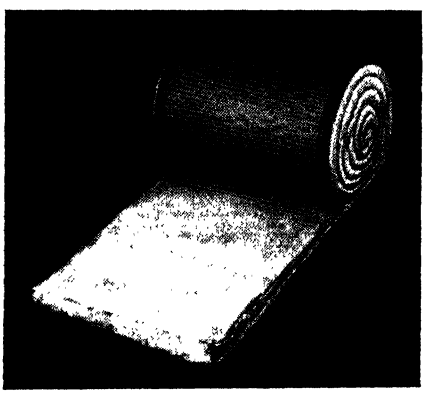
Douglas Co.

Waco, Texas

FLAME PROOF

FIRE-RESISTANT

HEAT Stopper Cotton Insulation



EFFICIENCY

The low thermal conductivity of Heat Stopper Insulation makes it ideally suited for all insulation requirements. **K factor: 0.24** Btu/hr/sq ft/ deg F/in. (See table.)

EASY TO INSTALL

Requires a minimum of labor and expense for installation. Unrolls like a rug. Complete flexibility insures uniform distribution in all odd shaped spaces. An easy one man job.

LIGHTWEIGHT

The fluffy lightness of Heat Stopper Insulation gives maximum protection with minimum load factor. **Density:** 7/8 lb/ cu ft.

NON-ABSORBENT

The natural wax-like coating on each of the cotton fibres, along with the aid of chemical treatment, makes Heat Stopper Insulation resistant to moisture.

FLAMEPROOF

Treated with a chemical formula for permanent fire-resistance. Effectively withstands 1800 deg blow torch test.

NON-IRRITATING TO THE SKIN

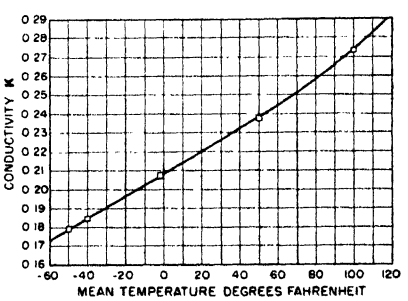
Heat Stopper Flameproof Cotton Insulation contains no splinter or needle like points to injure skin or breathing passages. Always clean and fresh, *has no odor.*

WILL NOT SETTLE OR PACK

Because of its natural resiliency, Heat Stopper Insulation will not pack down from vibration or age. If ever compressed for any reason, Heat Stopper quickly regains original thickness or better when exposed to air.

REPELS HOUSEHOLD PESTS

Heat Stopper Insulation will not harbor such household pests as insects, rats, mice, etc. Chemicals used in the tretament of Heat Stopper Insulation, although harmless to humans, is repulsive to household pests.



THERMAL CONDUCTIVITY OF 1" THICK HEAT-STOPPER INSULATION AT DENSITY OF 0.95 LBS. PER CUBIC FOOT

Heat Stopper Flameproof Cotton Insulation is available in a wide variety of widths and thicknesses to fit standard building requirements.

The Eagle-Picher Company

General Offices: American Building, **Cincinnati 1, Ohio**

Offices in Principal Cities

EAGLE-PICHER

A Remarkable Insulating Wool Made From Minerals

Years ago Eagle-Picher pioneered a method of fusing and fiberizing carefully selected minerals into a dark gray insulating wool. This mineral wool is chemically inert. Fibers are mechanically strong, extremely resilient and flexible. They withstand expansion and contraction without loss of efficiency even at elevated temperatures.

From this mineral wool, Eagle-Picher has fabricated a long list of insulating products to meet a wide range of temperatures and operating requirements.

H-2 Loose Wool

A clean fill insulation that is highly efficient for temperatures to 1200° F. Averages considerably lighter in weight than many rock and slag wools—goes farther. Fibers are soft and flexible. Eagle-Picher Insulation is as fireproof as the minerals from which it is made. Retains physical and chemical stability in presence of water. Packed in 40-lb bags.

7-B Granulated Wool

Another grade of fill insulation that has all the advantageous properties of Eagle H-2 Loose Wool. It consists of small pellets averaging ⅛ to ½ in. in size. For all fill jobs in irregular spaces. May be poured. Packed in 40-lb bags.

Low Temperature Felt

A highly efficient insulating material for subzero and low temperatures (to 400° F). Available in densities 6-lb to 8-lb per cu ft. Recommended for refrigerator rooms, trucks, refrigerators, stoves, etc. Sheds water. Extensively used in marine field.

Paper Backed Batts and Blankets

These light-weight, sturdily constructed batts and blankets are easy to apply. One side is protected with asphalt coated paper which serves as an approved vapor barrier. Strong tacking flanges. Quickly cut with knife or shears. Two thicknesses —Ful-Thik and Semi-Thik. For home use.

Super "66" Cement

A high-temperature insulating cement. Easy to apply and trowels to a smooth finish. Actively inhibits rust. Will stick on any clean, heated surface. Dry coverage 50-55 sq ft per 100 lb. 100 per cent reclaimable up to 1200° F. Packed in 50-lb bags.

Supertemp Blocks

An all-purpose high-temperature block insulation which will withstand elevated temperatures up to 1700° F without loss of efficiency or structural strength. Fibers are water-repellent. Light weight. Easily cut to fit irregularly shaped surfaces. Blocks withstand all normal vibration and abrasion encountered in use for which they are recommended. All standard sizes.

Insulseal

A protective coating for Industrial Insulation Blankets, Supertemp, "66" Cement and other kinds of heat insulation. Provides a permanent seal that safeguards insulation against air infiltration, moisture, water, fumes; also against vibration and abrasion. Does not support combustion.

For more complete specifications and technical data on these and other Eagle Insulating Products, see Sweet's Engineering or Power Plant catalogs.

Insul-Mastic Corporation of America

General Offices:

Oliver Bldg., Pittsburgh 22, Pa.

GILSONITE INSUL-MASTIC TYPE "D" INSULATION

One Single Application

INSULATES, DEADENS SOUND, RUSTPROOFS, WATERPROOFS
Steel, Copper, Tin, Galvanized Sheet Metal Ducts, Plates, Partitions, Buildings, etc.; Pipes, Pipe Lines; Oil Tanks, Water Tanks, etc.

One single application of Gilsonite Insul-Mastic Type "D" Insulation reduces the acoustic properties of metal plates, metal partitions, metal ducts, etc. It insulates against cold, reduces heat losses, is impervious to humidity conditions, and protects all surfaces over which it is applied against corrosion. It is chemically inert, and not subject to electrolysis.

Type "D" is waterproof throughout its entire mass, and is especially effective in preventing mildew and rot caused by condensation of moisture vapor on encased metal panels. The total moisture absorption when kept continually submerged in water, is only 3.2 per cent—too small to exert any practical effect.

A unique feature of Type "D" is that, without any form of mechanical attachment, it bonds perfectly with surfaces when applied at any angle from straight vertical to straight horizontal, including ceilings. Its bond is unaffected by extremes of heat or cold, and the material adheres tenaciously throughout its many year's life of full efficiency.

Type "D" is a highly viscous, semi-plastic material composed of from 65 per cent to 75 per cent granulated cork held in a matrix of genuine Gilsonite asphalt which surrounds each individual cork granule like a jacket. The total asphaltic base of Type "D" contains approximately 50 per cent washed select fine Gilsonite. Inert fillers of flake mica, asbestos fibre, etc., provide for prolonged efficient functioning.

Application of Type "D" is easily and rapidly made by spray under high air pressure, thereby assuring uniform thickness of covering over entire surfaces sprayed, regardless of "high" or "low" areas, angles, bolt or nail heads, or other surface irregularities. There are no joints or seams in a-sprayed-on application. (Type "D" can also be trowled.) The material dries in from 3 to 9 days depending upon weather, and reaches constant weight in about 18 days.

The density of Gilsonite Insul-Mastic Type "D" insulation is approximately 16 lb per cu ft when applied by spray and dried to constant weight. When applied by trowel, density varies according to the manner in which troweling is done; a fair average is 30 lb per cu ft when troweled by hand. The extremely low density (or high insulating value) of Type "D" obtained by spray application, is because that only by spraying can a large amount of desirable air cells be incorporated and retained in the mastic.

Quantities of Gilsonite Insul-Mastic Type Insulation required for different thicknesses, per 100 sq ft are approximately: ⅛ in.—12 gal; ¼ in.—20 gal; ⅜ in.—30 gal. When applied ¼ in. thick at the rate of 20 gal per 100 sq ft, the approximate weight of the applied material is 1½ lbs per sq ft. Shrinkage is negligible.

The thermal conductivity ("K" factor) of Gilsonite Insul-Mastic Type "D" Insulation, per sq ft per 1 in. thickness, is .36.

An application of Type "D" ¼ in. thick reduces heat flow through metal plates from 60 per cent to 65 per cent.

Gilsonite Insul-Mastic Type "D" retains its full functions of insulation and resistance to acids and akalies, throughout temperature ranges from 300 F to −30 F, but above 230 F, the coating becomes progressively more susceptible to injury by mechanical means. Down to −30 F, the material does not check, crack, scale, or lose its bond.

Type "D" has a black, tar colored finish and does not require any additional painting or other exterior surface treatment. If a bright surface is preferred, however, Insul-Mastic manufactures a gilsonite base aluminum paint which, by having the same base-binder as Type "D," is completely compatible with that material and which when sprayed over Type "D," will not discolor or run apart from it. The resulting combination has the added advantage of extremely high reflective properties. If a colored finish is desired for beautifying purposes, Vermont Slate granules may be sprayed over Type "D," while wet, in any color or blend of colors.

Type "D" is used as it comes from the drums. No pre-heating or other preparation of the material is necessary.

Catalog on request.

INSULITE

General Offices
500 Baker Arcade Bldg., **Minneapolis 2, Minnesota**

THIRTY-FOUR YEARS PROVEN DURABILITY

For 34 years engineers and architects have specified Insulite materials for structural uses, interior finish, low temperature duct lining, and for other thermal insulation and sound control work. Insulite materials have proved themselves practical through their performance on the job.

STRUCTURAL MATERIALS

Lok-Joint Lath—An insulating plaster base, fabricated from Graylite. Patented "Lok" firmly locks the sheets between supporting members. Thickness: ½ in. Size: 18 x 48 in.

Sealed Graylite Lok-Joint Lath—An insulating plaster base of Graylite, sealed on stud space side with an effective *moisture vapor barrier*. Has patented "Lok" on long edges. Same thickness and size as Graylite Lok-Joint Lath.

Bildrite Sheathing is an asphalt-containing wood fiber insulating board manufactured under an exclusive process which provides increased strength and moisture resistance. It is $^{25}/_{32}$ in. thick and has a gray-brown color. Thermal conductivity maximum: 0.36 Btu per inch thickness. Each sheet is marked to indicate proper nail spacing. Available in sizes 4 x 8 ft up to 4 x 12 ft with all edges square. Also available in 2 x 8 ft size with interlocking joint on long edges. Used as a structural sheathing board and as roof boarding.

Condensation Control—Where low outside temperatures and high inside humidities may occur, authorities recommend "sealing the warm side and venting the cold side" of the wall to prevent condensation. An adequate vapor barrier, Sealed Graylite Lok-Joint Lath, should be used on the warm (room) side of the wall thereby effectively reducing vapor transmission into the stud space. Bildrite Sheathing is designed to allow any surplus vapor in the stud space to "breathe" or be vented to the exterior air. If vapor is trapped within the stud space and cannot escape through the sheathing, destructive condensation may occur.

THE APPROVED INSULITE WALL OF PROTECTION

This construction consists of Bildrite Sheathing on the exterior of the frame work and Sealed Graylite Lok-Joint Lath on the interior. Transmission coefficient (U) is shown below.

	Interior Finish
Exterior Finish and Sheathing	No Insulation Between Studding
	Plaster (½ in.) on Sealed Graylite Lok-Joint Lath (½ in.)
Wood Siding, $^{25}/_{32}$ in. Bildrite Sheathing	0.15 Btu/sq ft./hr/°F

The above value is typical of results which can be obtained by utilizing Insulite materials in frame construction. For further (U) values refer to Chapter 6 pages 124 and 125.

Applying Bildrite Sheathing

Applying Lok-Joint Lath

INTERIOR FINISH MATERIALS

Graylite Building Board—An integrally treated asphalt containing wood fiber board of grayish brown color—burlap and linen textured surfaces. Thermal conductivity nominal 0.35 Btu per inch thickness. Furnished in thickness of ½ inch and sizes of 4 x 6 ft to 4 x 12 ft.

Smoothcote Interior Board—Factory Coated Insulating Board with smooth, finished surface one side, having 68 per cent light reflection. Furnished in ½ inch thickness only and in sizes of 4 x 6 ft to 4 x 12 ft.

Satincote Interior Board—Factory finished Insulating Board in colors light ivory and oyster white. Light reflection 80 per cent for the light ivory color. Requires no further decoration. Resistant to abrasion and washable. In ½ inch thickness and in sizes of 4 x 6 ft to 4 x 12 ft.

TileBoard—Available in Smoothcote and Satincote. TileBoard is furnished with the Lok-Grip Joint that permits concealed nailing and which together with the Lok-Pin (a flat diamond shaped metal dowel) definitely and mechanically safeguards against any falling units even though no face nailing is used.

Smoothcote and Satincote TileBoard available in ½ inch thickness and sizes of 12 x 12 inches to 16 x 32 inches.

Plank—Available in Smoothcote and Satincote. Plank has the Lok-Grip joint which permits concealed nailing and is beveled and beaded both long edges. Smoothcote and Satincote Plank furnished in ½ inch thickness, widths of 8 to 16 inches and lengths of 8 to 12 ft.

Acoustilite—A high efficiency acoustical material for sound control. Coefficient of sound absorption, at 512 cycles, is 0.79 when mounted on solid background and 0.80 when on furring strips. Noise reduction coefficient is 0.65 when mounted on solid background and 0.75 when on furring strips. Factory painted in buff, (light reflection 77 per cent) and in white (light reflection 80 per cent). Units have a butt joint and are beveled on four edges. Thickness, ¾ in.; sizes, 12x12 in. to 16x32 in.

Acoustilite or Fiberlite effectively quiet and control sound

Fiberlite—An efficient sound absorptive and decorative material. Coefficient of sound absorption, at 512 cycles, is 0.53 when mounted on a solid background and 0.72 when on furring strips. Noise reduction coefficient is 0.55 when mounted on solid background and 0.65 when on furring strips. Factory painted in buff (light reflection 77 per cent) and in white (light reflection 80 per cent). Units have a butt joint and are beveled on four edges. Thickness, ½ in.; sizes, 12x12 in. to 16x32 in.

HardBoard Products

HardBoard materials are tough, durable, grainless, pressed wood fiber boards with a hard, smooth surface. Available in a range of densities from 55 to 68 lb/cu ft. Thicknesses are from 1/10 to 5/16 in. and sizes of 4 x 2 ft to 4 x 12 ft.

Industrial Insulation

Industrial Insulation is a wood fiber board for use in all types of manufacturing industries producing items such as refrigerators, coolers, showcases, brooders, partitions and cabinets.

It can be cut-to-size and fabricated to customer's specifications. Three types of industrial board are available.

Lowdensite Industrial Board—A 10 to 14 lb density board with an average tensile strength of 100 lb/sq in. and an average conductivity of 0.30 Btu/hour /sq ft/F/inch thickness.

Ins-Lite Industrial Board—A 14 to 18 lb density board with an average tensile strength of 250 lb/sq in. and an average conductivity of 0.33 Btu/hour/sq ft/F /inch thickness.

Graylite Industrial Board—Differs from two above products in that it has an integral asphalt treatment which provides increased strength and moisture resistance as well as minimum thickness and linear expansion. A 16 to 20 lb density board with an average tensile strength of 350 lb/sq in. and an average conductivity of 0.35 Btu/hour/sq ft/F/inch thickness.

Insul-Wool Insulation Corp.

General Offices, **Wichita, Kansas**

Factories in Following Cities

ATLANTA, GA.
CLEVELAND, OHIO
COUNCIL BLUFFS, IA.
DALLAS, TEX
DES MOINES, IA.
DETROIT, MICH.
KANSAS CITY, MO.
ST. LOUIS, MO.
TRENTON, N. J.

WICHITA, KANS.

INSUL-WOOL THE QUALITY INSULATION

OKLAHOMA CITY, OKLA.

Insul-Wool is a non-mineral, fibrous insulation of the "fill" type—made of wood pulp, a natural insulation material. By the special "Insul-Wool" method, the wood pulp is converted into a loose fluffy substance which, when installed in a building, forms a soft heat-resisting blanket having millions of tiny air cells capable of resisting passage of either heat or cold.

UNIFORMITY OF PRODUCT

Only one grade of **Insul-Wool** is made and every "run" is tested at the factory to insure uniformity of product and unvarying high quality. It is free from grit, silicon particles, or "shot." **Insul-Wool** is distributed and installed only by specially trained men—direct factory representatives.

RESISTANT TO FIRE AND VERMIN

Insul-Wool's patented method of chemical treatment makes **Insul-Wool** thoroughly and permanently vermin and fire resistant.

ADVANTAGES OF INSUL-WOOL INSULATION

1. It is manufactured from wood pulp, a natural insulating material.
2. Chemical treatment makes **Insul-Wool** safe under all conditions and hazards.
3. Its light weight, 5/8 lb per square foot, 4 in. thick, adds very little load to the ceiling rafters.
4. **Insul-Wool** is a permanent type insulation which does not pack or settle and outlasts the building in which it is installed; this is backed by a Bonded Guarantee.
5. **Insul-Wool** does not attract moisture.
6. Cuts fuel costs up to 51 per cent and reduces Summer temperature up to 20° F in the home.
7. Meets U. S. Government requirements of Federal Construction with a thermal conductivity of 0.24 Btu per hour, per sq ft, per degree Fahrenheit, per inch thickness.

Analysis of Insul-Wool in Terms of Commercial Thickness

Material	Commercial Form	Comm'l. Thickness Inches	D. Wt. Per Cu. Ft.	C. Conductivity
INSUL-WOOL	Wood Fiber-Loose Type, permanently treated for vermin and fire.	1 4	2.5	0.24* 0.067**

*Kansas City Testing Laboratory, Inc., February 25, 1938.
**J. C. Peebles, Armour Institute of Technology, April 8, 1937.

Complete data on Insul-Wool Insulating Product will be sent upon request.

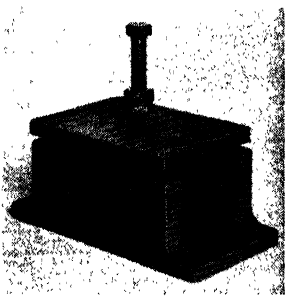
The Korfund Company, Inc.

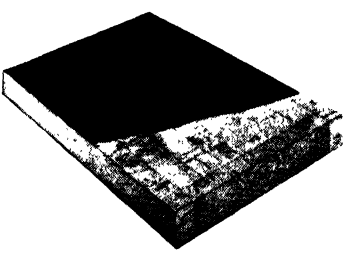
48-50 32nd Place

Long Island City 1, N. Y.

Representatives in KORFUND VIBRATION CONTROL **Principal Cities**

TYPE LK UNIVERSAL VIBRO-ISOLATORS are recommended for isolation of compressor and condensing units where almost perfect absorption of noise and vibration is required, as for instance on upper floors of office buildings, hospitals and hotels. These units absorb vibration in all directions and provide for both horizontal and vertical adjustment. Loading range 75-12,000 lb. Catalog LK-550.





KORFUND CORK PLATES provide a high degree of noise and vibration isolation when applied to compressors mounted on a slab of concrete. Since Cork Plates should be loaded to a minimum of 1,500 lb per sq ft, it is seldom necessary to cover the entire area of concrete. Instead, a number of Cork Plates of dimensions 8 in. x 8 in., or smaller, may be spaced under the concrete so that the load will be evenly distributed over the several plates. Bulletins Bc-13; Bc-22.

The TWIN RAIL FAN BASE is a development in fan and blower isolation which incorporates many new and exclusive features. Interchangeable prefabricated parts are used throughout. It is light in weight, yet has great rigidity to vertical and lateral stresses. The Twin Rail Base is easily assembled and installed, and is fully adjustable. Rubber-in-Shear, Cork, or Steel Spring Isolators are supplied, depending upon requirements. Catalog TR-800.

The Korfund Co., Inc., is exclusive national distributor of ARMSTRONG STANDARD DENSITY VIBRACORK in 2 in., 3 in., and 4 in. thicknesses, loading capacity 1500 to 4000 lb per sq ft.

Johns-Manville

Executive Offices: 22 East 40th Street, **New York 16, N. Y.**

Offices in All Large Cities

Johns-Manville Home Insulation

Johns-Manville Rock Wool Home Insulation is a light, fluffy mineral wool, highly efficient in heat-proofing practically any building, old or new. It is durable, rot-proof, fire-proof and odorless, and will not corrode or settle. Full stud thickness of this material will save up to 30 per cent on fuel in winter and help keep rooms up to 15 deg cooler in hottest weather. J-M Rock Wool Home Insulation is furnished in two forms: for new construction,

Applying J-M Super-Felt Type B batts in new home

in easily handled batts; for existing buildings, in nodulated form to be installed pneumatically.

For New Construction
J-M Super-Felt Type B Batts

Super-Felt Type B Home Insulation is furnished in pre-fabricated batts of uniform thickness and density, in both full stud thickness and semi-thick, in sizes 15 x 23 in. and 15 x 48 in., designed to fill completely the space between studs, joists and rafters on the usual 16 in. centers. The sturdy felted "wool" is strong enough to be handled rapidly without damage. The batts are backed with waterproof, vapor-resistant paper, extending on both the long sides in 1½ in. wide flanges, by which the batt is fastened in place and which also aid in sealing the joints. This backing protects against penetration of moisture from wet plaster and also resists infiltration of moisture vapor from the house into the wall.

As a further protection against moisture, the felted wool is also waterproofed.

Super-Felt may also be obtained in blanket form, in Thick, Medium and 1 in. thicknesses. The blankets have a waterproof vapor barrier paper on one side and a permeable kraft paper on the opposite side, cemented together along the long edges to form a strong nailing flange.

For Existing Homes and Buildings
Type A "Blown" Rock Wool

Type A Rock Wool is blown pneumatically into the spaces between studs in outer walls and between rafters or joists in roofs or attic floors. Insulation thickness in walls corresponds to stud depth, approximately 3⅝ in.; the density, approximately 5 to 8 lb per cu ft, assures maximum thermal efficiency. This type of insulation is installed only by Johns-Manville or by Approved J-M Home Insulation Contractors, who are equipped with the necessary apparatus and trained crews.

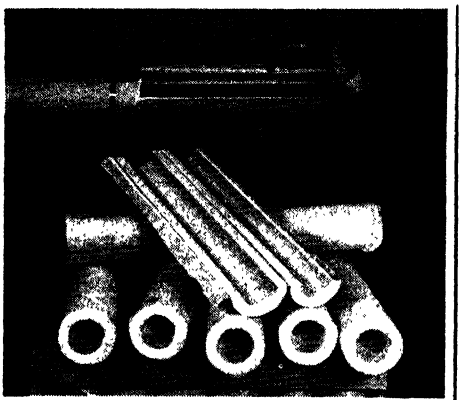
Write for Details

Complete information on all types of J-M Rock Wool Home Insulation will be furnished on request.

J-M Airacoustic Sheets for lining Air-Conditioning Ducts

J-M Airacoustic Sheets, for duct linings of air conditioning systems, are flameproof, highly sound-absorbent and moisture-resistant, with a surface which will not materially increase friction losses in the duct system. Write for Bulletin AC-23A.

Johns-Manville Pipe and Boiler Insulation



J-M 85% Magnesia Pipe Insulation

J-M Pre-Shrunk Asbestocel Pipe Insulation

Cellular type of insulation for pipes carrying low pressure steam or hot water.

Made up of alternate layers of plain and corrugated, specially-treated, moisture-resistant, asbestos paper. Three finishes: Glazed White for quick application, will not carry flame; asbestos paper; and regular canvas cover.

Furnished in 3-foot sections, in thicknesses of 2 to 8 plies, each ply approximately ¼ inch thick.*

J-M 85% Magnesia

Recommended as the most widely used insulation of the molded type for temperatures up to 600 F. Pipe insulation is furnished in sectional or segmental form for all commercial pipe sizes,* in thicknesses up to 3 in. Blocks are 3 in. by 18 in. and 6 in. by 36 in., flat or curved, from 1 in. to 4 in. thick. Minimum thickness for curved blocks, 1¼ in.

J-M Pre-Shrunk Wool Felt Pipe Insulation

Due to its dual-service liner—an asphalt-saturated felt—J-M Pre-Shrunk Wool Felt is equally effective and durable on either hot or cold water service piping. By the use of moisture-resistant felts, shrinkage troubles have been minimized.

Supplied in the regular canvas finish, it is furnished in 3-ft sections in thicknesses of ½ in., ¾ in., 1 in., Double ½ in., and Double ¾ in., for pipe sizes of ½ in. and larger.*

J-M Asbesto-Sponge Felted Pipe Insulation

Recommended on all high pressure steam piping at temperatures up to 700 F where insulation may be subjected to rough usage or where maximum efficiency and durability are desired. Furnished in 3-ft sections up to 3 in. thick, for all commercial pipe sizes.*

J-M Superex Combination

Superex Combination Insulation (an inner layer of high temperature Superex and an outer layer of 85% Magnesia) is recommended where temperatures exceed 600 F. Superex and Magnesia are both furnished in sectional and segmental pipe covering, and in block forms.

J-M Asbestocel Sheets and Blocks

Asbestocel Sheets and Blocks are used for insulating warm-air ducts, flues, heater casings and fan housings in ventilating systems. Temperature limit 300 F. Furnished 6 to 36 in. wide by 36 to 96 in. long, from ¼ in. to 4 in. thick.

J-M Rock Cork Sheets and Pipe Insulation

J-M Rock Cork is made of mineral wool and a moisture-proof binding ingredient molded into sheets for insulating refrigerated rooms, air conditioning and other low temperature equipment; and into sectional pipe insulation with an integral waterproof jacket, for all low temperature service. It is strong, durable, and will not support vermin. Because of its unusual moisture resistance, its high insulating efficiency is maintained in service.

Furnished in sheets 18 in. by 36 in., in 1, 1½, 2, 3 and 4 in. thicknesses; also 18 in. by 18 in. by 1 in. thick. In lagging form, for curved surfaces, supplied 18 in. long by 1½, 2, 3 and 4 in. thick, 2 to 6 in. wide, depending on diameter. In pipe covering form, in ice water, brine and heavy brine thicknesses, for all commercial pipe sizes.*

Details on Request

Write for complete information on any Johns-Manville insulating material.

*Also available in sections to fit straight runs of copper pipe or tubing with outside diameter ⅝ in. and larger.

Kimberly-Clark Corporation

Neenah, Wisconsin

KIMSUL INSULATION REG U. S. & CAN PAT OFF

KIMSUL* insulation . . .
a many-layer, wood fiber blanket with these 12 advantages:

A PRODUCT OF Kimberly Clark RESEARCH

1. Many-layer Construction. KIMSUL* insulation is scientifically designed on the many-layer principle. Dozens of layers create millions of tiny trapped-air cells, effectively shut heat in during winter, lock it out in summer.

2. Handy Compressed Package. KIMSUL comes compressed to 1/5th installed length. Reduces storage, shipping and handling charges.

3. Extra Width. The KIMSUL blanket is made extra wide to provide fully insulated fastening edges.

4. Flexibility. Fits in corners, tucks behind pipes, electrical wiring and other obstructions.

5. Excellent Caulking. Trimmed pieces make effective caulking around window and door frames.

6. PYROGARD† fire-resistant cover. Chemically treated to resist fire just as the inner layers of KIMSUL are treated.

7. Low "k" Factor. Thermal efficiency: 0.27 Btu/hr/sq ft/ deg F/in. (J. C. Peebles, Armour Institute).

8. Lasting Protection. KIMSUL is long-lived because of the materials from which it is made: wood fibers impregnated with asphalt.

9. Resists Fire, Moisture, Vermin and Fungi—Is Termite-Proof.

10. Non-Settling. Won't sag or settle. Rows of strong stitching, running the length of the blanket, hold KIMSUL at the proper density.

11. Light Weight . . . Easy To Install. 1,000 sq ft of Standard Thick KIMSUL weighs 115 lbs. Average density, including PYROGARD cover is 1.4 lbs per cu ft. A precut, prefabricated blanket, KIMSUL is easy for any one to install.

12. 3 Thicknessess . . . 4 Widths. KIMSUL blanket comes in Commercial Thick (about ½ in.), Standard Thick (about 1 in.) and Double Thick (about 2 in.) . . . giving choice of thicknesses to fit specific needs. Each thickness is available in four standard widths: 16 in., 20 in., 24 in., and 48 in.

*T.M. Reg. U.S. & Can. Pat. Off.
†Trademark

For easy measuring, trademarks are printed at approximately 2 ft intervals on expanded blanket.

KIMSUL can be cut to fit non-standard spaces. Just saw the KIMSUL roll as shown.

Clean, rapid and permanent installation in walls, ceilings or roofs. No sharp particles.

PERFORMANCE OF

KIMSUL INSULATED WALLS AND CEILINGS

Calculations apply to a one-story home in the Chicago area.
As shown in the table, almost any desired performance can be produced by insulating with KIMSUL. The economic thickness provides the best balance between insulation costs and resultant fuel savings.

		Surface Temperature (F)		Coal Consumption Reductions		
		Wall	Ceiling	Tons per Season	Tons Saved per Season	% Coal Saved
No Insulation....		60.0	52.0	12.1		
KIMSUL in Walls and Ceilings...	Commercial Thick.....	64.4	60.0	8.0	4.1	33.9
	Standard Thick.....	65.3	63.0	7.1	5.0	41.3
	Double Thick.....	66.5	65.4	6.4	5.7	47.1
	Commercial Thick in Walls Standard Thick in Ceilings.....	64.4	63.0	7.5	4.6	38.0
	Commercial Thick in Walls Double Thick in Ceilings.....	64.4	65.4	7.0	5.1	42.1
	Standard Thick in Walls Double Thick in Ceilings.....	65.3	65.4	6.7	5.4	44.6
KIMSUL in Ceilings Only	Commercial Thick.....	..	60.0	9.1	3.0	24.8
	Standard Thick.....	. .	63.0	8.5	3.6	29.7
	Double Thick.....	. .	65.4	8.1	4.0	33.1

SPECIFICATIONS AND INFORMATION

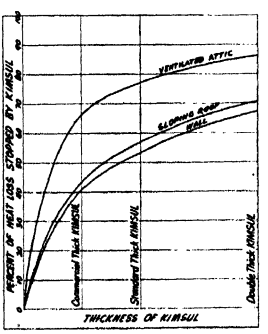
Specification	Nominal Thickness	Thermal Resistance "R"	Sq Ft/Roll Standard Widths		Approximate Net Weight per M Square Feet
			16, 20, 24 Inches	48 Inches	
Commercial Thick.....	0.5 In.	1.85	200	500	75 Lbs.
Standard Thick.....	1.0 In.	3.70	200	500	126 Lbs.
Double Thick.....	2.0 In.	7.40	100	250	236 Lbs.

FOR YOU—

This Application Data File.

A technical manual to help solve your insulation problems. A request on your letterhead will bring you a free copy.

Adapted for attic insulation in new or existing structures.



Graph shows percentage of heat loss stopped by the various thicknesses of KIMSUL.

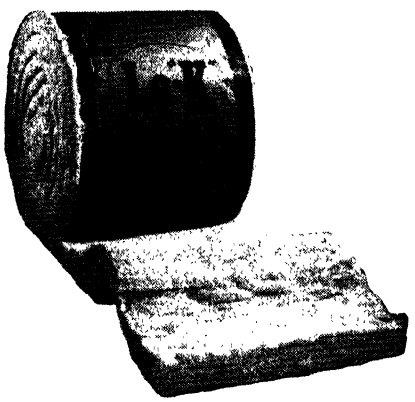
Flexible KIMSUL is easily applied to difficult positions.

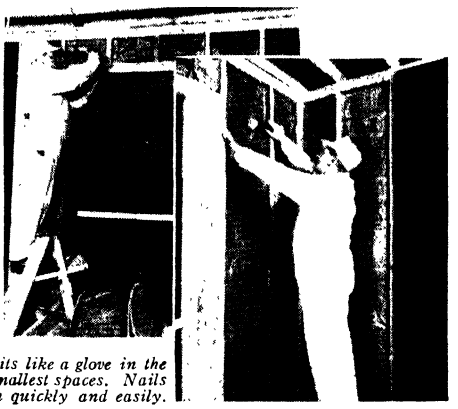
Lockport Cotton Batting Co.

Lockport, New York

FLAMEPROOFED **Lo-"K"** COTTON INSULATION

Fire proofed and manufactured under Department of Agriculture Specifications





Fits like a glove in the smallest spaces. Nails in quickly and easily.

Lo-"K" is made of processed American cotton of varying thicknesses, packaged in rolled form, *with* or *without* Kraft paper backing—an added moisture barrier.

Thermal Conductivity—The "k" value for cotton is 0.24 Btu/hr/sq ft/degree F/inch. (*See table.*)

Light Weight—Weight of 1 cu ft is ⅛ lb. (*See table.*)

Flame-Proofed—To comply with Department of Agriculture specifications to withstand a temperature of 1800° F. This flameproofing is accomplished by a process that Lockport has used exclusively for over 15 years.

Moisture-Resistant—Chemical treatment, combined with natural protective coating on cotton fibres, enables cotton to effectively resist moisture. Prevents rot and mildew.

Smooth Texture—Cotton contains none of the sharp particles that can harm workmen's hands during process of installation.

Flexible—Cotton batt may be expanded or contracted to fit any enclosure. It easily passes over and under pipes and wires.

Easy to Warehouse and Handle. Offers far more "compressibility." Requires one third the trucking and warehouse space of ordinary insulation.

Simple and Economical to Install. Saves from 25 to 40 per cent in time and labor costs.

Designed to Maintain Maximum Utility throughout the life of the structure. Resists all types of deterioration. Will not sag or settle.

Packaged in Rolled Form.

Thicknesses—inches: 1, 1½, 2, 3, 3⅝. Width—16, 20, 24 in. centers. Lengths: Standard from 12 ft up.

Available in Quantity—Lockport is establishing dealers in principal distributing centers. If your dealer doesn't happen to have Lo-"K" in stock, we invite your inquiry for prices and samples.

INSULATING VALUE OF VARIOUS INSULATORS[a]
The coefficients of conductivity (*k* value) are expressed in Btu per hour per square foot per degree Fahrenheit per 1 in. of thickness.

Type of Insulation	Wgt. per Cu Ft	*k*[b] Value
Cotton: Insulating Batt	.875	0.24
Rock Wool: Fibrous material made from rock	10.00	0.27
Mineral Wool: Fibrous material made from mineral slag	....	0.27
Glass Wool: Fibrous material made from glass slag	1.50	0.27
Rigid Insulation made from sugar cane fibre	13.50	0.33
Chemically treated wood fibre between layers of paper	3.62	0.25
Eel grass between layers of paper	3.40	0.25
Stitched and creped expanding fibrous blanket	1.50	0.27
Shavings: Various from planer	8.80	0.41
Corkboard: No binder added	7.00	0.27
Rigid insulation made from wood fibre	15.90	0.33
Rigid fibre board made from shredded wool and cement	24.20	0.46

[a] Compiled from Chapter 6.
[b] "*k*" indicates temperature conductivity.

Mundet Cork Corporation

7101 Tonnelle Ave. **INSULATION DIVISION** **North Bergen, N. J.**

Manufacturers of Corkboard, Cork Pipe Covering, Compressed Machinery Isolation Cork, Natural Cork Isolation Mats, and all kinds and varieties of Cork Specialties.

Authorized contractors for high temperature insulation.

Mundet Branches

ATLANTA, GA.	CINCINNATI 2, OHIO	JACKSONVILLE 6, FLA.	PHILADELPHIA 39, PA.
BOSTON (NO. CAMBRIDGE) 40, MASS.	DALLAS 1, TEX.	KANSAS CITY 7, MO.	ST. LOUIS 4, MO.
CHICAGO 16, ILL.	DETROIT 21, MICH.	LOS ANGELES (Maywood)	SAN FRANCISCO 7, CALIF.
	HOUSTON 1, TEX.	NEW ORLEANS 16, LA.	

Mundet Distributors are Located in the Following Cities—Names and Addresses on Request

ARIZONA	PHOENIX, TUCSON	MONTANA	ANACONDA	TEXAS	EL PASO
COLORADO	DENVER	OHIO	TOLEDO	UTAH	SALT LAKE CITY
CONNECTICUT	HARTFORD	OKLAHOMA	OKLAHOMA CITY	VIRGINIA	NORFOLK, RICHMOND
D. C.	WASHINGTON	OREGON	PORTLAND	WASHINGTON	SEATTLE, TACOMA
IOWA	AMANA	RHODE ISLAND	PROVIDENCE	W. VIRGINIA	CHARLESTON
MINNESOTA	MINNEAPOLIS	SOUTH DAKOTA	BROOKINGS	WISCONSIN	APPLETON
MARYLAND	BALTIMORE	TENNESSEE	JOHNSON CITY		
			KNOXVILLE, MEMPHIS, NASHVILLE		

NEW YORK, AVERILL PARK, BUFFALO, PLATTSBURG, ROCHESTER, UTICA, WESTBURY, L. I.

Natural Cork—Cork in its natural state consists of minute hermetically sealed cells containing "dead" air. Approximately 200,000,000 cells per cubic inch. Cell walls are resinous, resilient, and impervious to the passage of air. There is no "free" air to conduct heat or moisture through the mass and no capillary attraction.

Mundet "Jointite" Corkboard

—for all low temperature insulation and for acoustical correction. Natural cork is ground into ¼ in. to ⅝ in. granules and compressed under heat in moulds to produce Mundet flat or shaped corkboard. Air spaces between granules are eliminated by the pressure and the milled resin in the cell walls cements the mass into a homogeneous structure retaining the properties of natural cork.

Mundet Corkboard meets U. S. Government Master Specifications. Its heat transmission is guaranteed not to exceed .29 Btu when tested in accordance with Bureau of Standards regulations. In actual cold storage practice, this figure may be safely reduced to .27 Btu. Sold in standard 12 in. x 36 in. sheet. Standard thicknesses, ½ in., 1 in., 1½ in., 2 in., 3 in., 4 in., 6 in.

Section of Mundet Moulded Cork Pipe Covering with Fitting. The pipe covering is made in sections 36 in. long, to fit all sizes of pipe.

Mundet "Jointite" Cork Pipe Covering

Shown below, with fitting cover. Protects all types of low temperature lines. Made in 3 thicknesses, with complete line of standard covers, suitable for pipes carrying sub-zero to 50 F temperature.

Mundet Cork Vibration Isolation

Machinery vibration encountered in heating and ventilating work is effectively controlled by the use of Mundet Natural Cork Isolation Mats. These consist of blocks of pure cork, held together within a rigid steel frame or bound with asphalt paper applied with hot asphalt top and bottom. Mundet steel bound mats are usually used under exposed mounts; asphalt paper bound mats under concrete foundations of the envelope type.

Engineering and Specification Service

Our engineering department is at the service of Architects and Engineers, to assist and advise in the preparation of specifications pertaining to cork. This service is available without obligation to any one who has a low temperature insulation or a vibration isolation problem. Our latest catalogue will be sent on request. It is replete with information and data of value to every specification writer whose field touches our products.

Mundet Contract Service

Covers the complete installation of our products, in accordance with best established practice. Divided responsibility is avoided. Materials and workmanship are guaranteed.

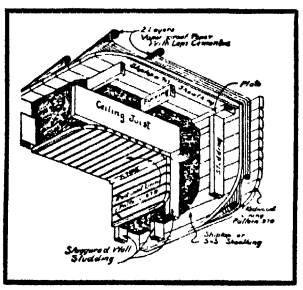
The Pacific Lumber Company

100 Bush Street, **San Francisco**

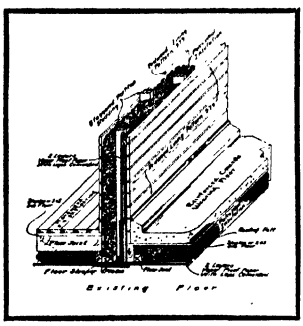
PALCO INSULATION WOOL

LOS ANGELES
CHICAGO
NEW YORK

FLAME PROOF SAFERIZED PROCESS



Typical Wall and Ceiling Wood Finish for Low Temperatures.



Accepted Partition Construction between Freezer and Cooler with Wood Finish Wall and Floor, and Concrete Chill Floor.

PALCO WOOL Provides Efficient Insulation

Constant low temperature control within extremely close ranges requires an insulation of high thermal efficiency. PALCO WOOL, with its low thermal conductivity of .255 Btu, has proved to be one of the most efficient types of insulation in use today throughout the United States and Canada. It has the quality of being entirely self-supporting within a wall. Because of its lasting resilience PALCO WOOL will not settle nor compact over an extended period. Permanence is further insured by its exceptional ability to withstand moisture and resist decay and deterioration. PALCO WOOL is inherently repellent to insects, vermin and pests. It is odorless itself, and will not absorb odors. Specially processed PALCO WOOL is additionally treated under an exclusive SAFERIZED process to make it flame-proof. Due to its permanent low cost, PALCO WOOL has proved exceedingly economical to use. Its high efficiency assures continued savings in operation and maintenance.

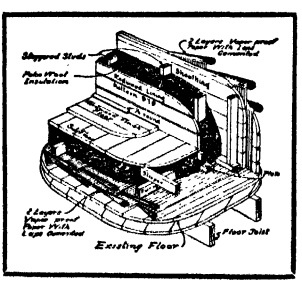
Check These 8 Proved Qualities of PALCO WOOL

1. High Thermal Efficiency
2. Economy
3. Durability
4. Non-Settlement
5. Odor-Proof
6. Vermin-Repellent
7. Moisture-Resistant
8. Fire-Resistant

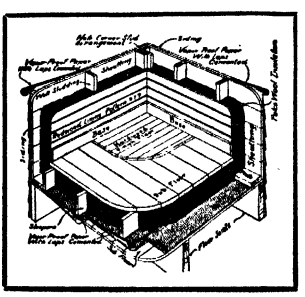
Recommended Thickness of PALCO WOOL

For temperature of:	Use
34° F	4″
25° F	6″
10° F	8″
0° F	10″
−10° F	12″
−20° F	14″
−30° F	16″
Walls between freezers (i.e. 0° F) and coolers (i.e. 36° F)	10″

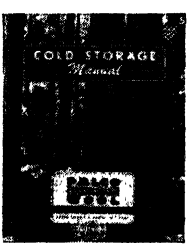
For Further Engineering Details, Send for Your Copy of the new PALCO WOOL COLD STORAGE MANUAL



Standard Wood Finish, Floor and Wall Construction for Freezers, etc.



Normal Frame Construction, Wood Walls, Flooring, and Exterior Siding for Cold Storage.



ALFOL INSULATION

Manufactured by

Reflectal Corporation

155 East 44th Street

New York 17, N. Y.

HEAT INSULATION for ALL PURPOSES

Easy to Apply

Handy Package—250 Sq Ft of Insulation

Alfol Building Blanket—for all Types of Building Structures.

Alfol Building Blankets consist of spaced layers of Alfol Aluminum Foil Insulation attached along the edges to a liner sheet of heavy vapor proof paper.

Packaged in handy rolls of 250 sq ft each for use on 16 in., 20 in. or 24 in. centers. Weighs less than 1/10 lb per sq ft.

- **High Insulation Efficiency.**
- **Positive Vapor Barrier.**
- **Low Heat Storage Capacity.**
- **Negligible in Weight.**
- **Moisture Proof.**
- **Durable.**
- **Odorless and Clean.**
- **Easily Applied.**
- **Low Cost.**

Specifications

Description	Widths	Net Area per Roll	Net Weight per Roll
Type I.—1 Layer ALFOL	16"-24"	250 sq. ft.	17 lbs.
Type II.—2 Layers ALFOL	16"-20"-24"	250 sq. ft.	19 lbs.

See technical data in Table 1, Section C, Page 116, this volume.

A L S O

• ALFOL PREFABRICATED INSULATION PANELS

For Tanks, Towers, And All Types of Heated Equipment.

• ALFOL ASBESTOS

Alfol Aluminum Foil Insulation Laminated To Asbestos For Ovens, Ranges, Boiler Jackets, Hot Water Heaters, And All High Temperature Insulation Purposes.

• ALFOL JACKETING

Heavy Reinforced Paper Combined With Alfol Aluminum Foil. Provides Insulation And Vapor Barrier In One Convenient Form. For Refrigerator Cars, Trucks, Buses, Trailers, Etc.

Write for complete information, catalogs and prices.

Silvercote Products, Inc.

161 East Erie Street, **Chicago, Ill.**

SILVERCOTE Reflective INSULATION

SILVERCOTE INSULATION

Silvercote—A reflective insulation designed to retard the transfer of heat by a combination of heat reflective surfaces and air spaces, is manufactured in three forms to meet various insulation requirements.

Silvercote Fabric—A fabric reinforced insulation and vapor barrier consisting of two sheets of Silvercote paper laminated with specially prepared asphaltum and reinforced with an interlining of ½ in. mesh jute fabric imbedded in the lamination. The two exposed silver-like surfaces retain their high reflectivity to radiant heat under the most severe conditions encountered in the building construction, air conditioning and refrigeration fields. Silvercote Fabric weighs approximately 100 lb per thousand sq ft and is available in 500 sq ft rolls in standard widths of 26 in., 36 in., 49 in., and 52 in. Special widths up to 120 in. can be manufactured for industrial users.

Silvercote Duplex—A product similar to Silvercote Fabric except that the reinforcing fabric is omitted. Silvercote Duplex has the same insulating and vapor barrier values as Silvercote Fabric. Silvercote Duplex is available in standard widths of 26 in., 36 in., 49 in., and 52 in. in 500 and 1000 sq ft rolls. Weight: approximately 65 lb per thousand sq ft.

Silvercote Simplex—An economical reflective insulation designed for use where a vapor barrier is not called for. Silvercote Simplex is a single sheet of kraft paper coated on both sides with the Silvercote surface. Silvercote Simplex is available in 2000, 1000 and 500 sq ft rolls of 36 in. and 54 in. width. Weight: approximately 30 lb per thousand sq ft.

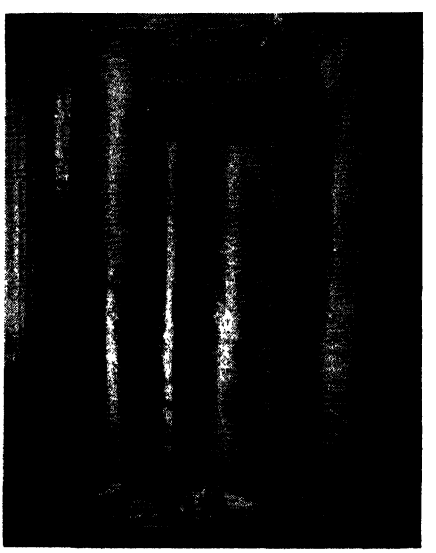
SILVERCOTE—HEAT AND WATER VAPOR BARRIER

Insulation Value—The thermal conductance of Silvercote Fabric dividing a 1½ in. vertical air space has been established by laboratory test as 0.23 Btu per hour per sq ft per deg F. The thermal conductance of Silvercote Fabric mounted in the center of a 1½ in. horizontal air space with heat flow in the upward direction is 0.26 Btu per hour per sq ft per degree F. With heat flow in the downward direction the thermal conductance is 0.16 Btu per hour per sq ft per degree F. The emissivity of Silvercote has been found by test to be 0.17. Copies of test reports on the conductance or emissivity of Silvercote are available upon request. Silvercote Duplex and Silvercote Simplex have the same insulation value as the Fabric.

Water Vapor Permeability—Silvercote Fabric and Silvercote Duplex each have a permeability to water vapor transmission of approximately 0.40 grains per hour per square foot per pound per square inch difference in vapor pressure. This is approximately ⅛ of the maximum allowable transmission for materials classed as vapor barriers.

ENGINEERING SERVICE

For complete specifications and engineering service address Silvercote Products, Inc., 161 East Erie Street, Chicago 11, Illinois.



Silvercote Fabric 36 in. wide applied over inside face of studs 16 in. on center. Excess 4 inch width in two stud spaces permits suitable vapor seal lap and forms sealed air space between Silvercote insulation and interior finish.

Wood Conversion Company

Dept. 220-8 First National Bank Building
St. Paul 1, Minnesota
NEW YORK CHICAGO

EFFICIENT INSULATION FOR EVERY NEED

For many years a leader in the insulation field, Wood Conversion Company manufactures a complete line of flexible, fiber and rigid insulation for all industrial and domestic purposes. This insulation is the product of scientific research, and is especially designed to embody the most desirable qualities for every use. Backed by the name of Weyerhaeuser, Wood Conversion Company insulation assures high efficiency and long, satisfactory service.

Balsam-Wool Sealed Blanket Insulation—A building insulation that is completely armored against the three major insulation enemies—wind, vibration and moisture. The Balsam-Wool mat is completely enclosed in tough waterproof liners which surround all four sides, with spacer flanges which assure positive application. Balsam-Wool will not settle or pack down within walls—is fire retardant and vermin-proofed.

K-25 Fiber—A clean, new wood fiber insulation with an amazingly low K factor. Shipped in compact bales, K-25 is easily processed on the job to create a lastingly effective insulation and is ideal for use in locker plants, cold storage plants, walk-in coolers, etc.

K-25 Fiber Pneumatic System—The modern, high-speed, automatic way to insulate domestic refrigerator cabinets and doors. Fluffed to proper low density in the manufacturer's plant, K-25 is blown into cabinets and doors under high pressure, forming a tightly felted insulating mat without joints, laminations or voids.

Tufflex—A soft, felted blanket material made from fleecy wood fiber, combines high insulating efficiency with toughness and exceptional resistance to heavy impact blows. Tufflex is light in weight and non-abrasive—will not tear or pull apart even when cut into narrow strips. Tufflex is available in rolls or sheets of various thicknesses and widths.

NU-WOOD STRUCTURAL INSULATION

Nu-Wood Interior Finish—A multiple-purpose wood fiber material available in tile, plank and board. Nu-Wood insulates, decorates and quiets noise. Nu-Wood's colors are soft and harmonious—will not fade. The Nu-Wood interior finish line includes Sta-lite, an insulating interior finish with more than 70 per cent light reflection.

Nu-Wood Insulating Lath—Used as a plaster base, assures strong, smooth, true walls and ceilings, free from cracks.

Nu-Wood Roof Insulation—Will fill all requirements of Federal specification LLL-N-321A. Furnished in any practical thickness.

M-47-7169

United States Gypsum Company

General Offices: 300 W. Adams Street, **Chicago, Ill.**

INSULATION PRODUCTS

Batt **Decorative** **Structural**

RED TOP* INSULATION WOOL

Red Top Batt

RED TOP MINERAL WOOL BATTS

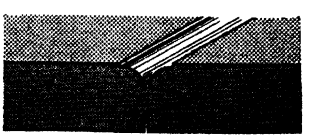
"k" Valve .27 Btu's

Made for standard (16 in. or 24 in. O.C.) framing in two thicknesses, Medium (Approx. 2 in.) and Thick (Approx. 3 in.). Lengths are either 24 in. or 48 in. Batts are provided with an efficient vapor barrier paper providing nailing flanges for easy application. Adequately packed to insure material will arrive at the job in good condition.

Decorative

Decorative

WEATHERWOOD* PLANK—Manufactured in widths of 8, 10, 12 and 16 inches and in lengths 6, 8, 10 and 12 feet—½ inch thick. The fitted edges (see cut) conceal nails and seal against dust and air infiltration. WEATHERWOOD Plank is made in Blendtex (gray and tan blends) and Hilite (ivory) colors. When combined in variations of shades and width, Weatherwood Plank produces maximum values in both insulation and decoration.



Tile and Plank Fitted Edge

*Reg. U. S. Pat. Off.

WEATHERWOOD TILE—Available in 12 x 12, 12 x 24, 16 x 16 and 16 x 32 inches in ½ and 1 inch thicknesses. Colors are Blendtex (gray and tan blends) and Hilite (ivory).

WEATHERWOOD PANELTILE—Hilite color available in 12 x 24 and 16 x 32 inches in ¾ inch thickness. Blentex colors available in 12 x 24 and 16 x 32 inches. Tile sizes 12 x 24 and 16 x 32 inches can be mill cross scored to represent ½ inch Tile Dimensions. All tile have fitted edges.

Structural

WEATHERWOOD SHEATHING—Asphalt coated. 2 feet x 8 feet x 25/32 inches thick, with tongue and grooved long edges for horizontal application. Also available in 4 x 8, 4 x 9, 4 x 10 and 4 x 12 feet in either ½ inch or 25/32 inches thickness with square edges for vertical application.

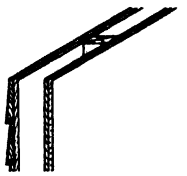
WEATHERWOOD BUILDING BOARD—4 feet wide, made in lengths 6, 7, 8, 9, 10 and 12 feet, ½, and 1 inch thick in either ivory or gray tan colors. Applied by nailing; effectively insulates, strengthens and decorates.

WEATHERWOOD INSULATING LATH—18 x 48 inches x ½ and ¾ inch thick with V joint on long edges. Gives an excellent plaster bond and also acts as a cushion for plaster with sound deadening qualities.

Heat Loss Factors

The heat loss factors shown on the opposite page indicate the comparative insulation value of various insulating treatments included in common construction systems.

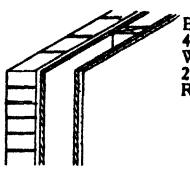
NOTE: These figures apply to 1 story buildings. To get figures for 2 story homes add 20 per cent to the values below for the wall constructions and divide by one-half for floor and ceiling constructions It is important to use correct factor due to variations in the ratio of wall and window areas.



WALLS

Basic Construction—Frame
Wood Siding
Wood Sheathing
2 x 4's
Rocklath & Plaster

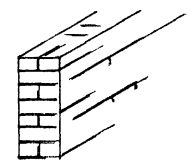
	No Wool Between Studs	Adding Red Top Wool 1"	2"	3"
Basic Construction	.248	.120	.083	.064
Substituting in Above Basic Const.				
a. 25/32" WW Sheathing	.186	.105	.076	.059
b. 1/2" WW Plaster Base	.183	.103	.076	.059
c. 3/4" WW Plaster Base	.157	.094	.069	.055
d. 1" WW Plaster Base	.143	.088	.067	.054
e. 25/32" WW Sheathing and 1/2" WW Plaster Base	.147	.090	.068	.054
f. 1/2" WW Bldg. Bd., Tile or Plank	.187	.104	.077	.059
g. 3/4" Bldg. Bd., or Tile	.160	.095	.070	.056
h. Gyplap Sheathing	.310	.135	.090	.068
i. 1/2" Sheetrock	.260	.123	.085	.064
j. Gyplap Sheathing and 1/2" Sheetrock	.330	.136	.091	.069



WALLS

Basic Construction—Brick Veneer
4" Brick
Wood Sheathing
2 x 4's
Rocklath & Plaster

	No Wool Between Studs	Adding Red Top Wool 1"	2"	3"
Basic Construction	.270	.125	.085	.065
Substituting in Above Basic Const.				
a. 25/32" WW Sheathing	.202	.111	.078	.061
b. 1/2" WW Plaster Base	.200	.107	.077	.060
c. 3/4" WW Plaster Base	.178	.102	.073	.058
d. 1" WW Plaster Base	.157	.094	.070	.055
e. 25/32" WW Sheathing and 1/2" WW Plaster Base	.162	.095	.070	.055
f. 1/2" WW Bldg. Bd., Tile or Plank	.215	.112	.079	.061
g. 3/4" WW Bldg. Bd. or Tile	.187	.104	.075	.059
h. Gyplap Sheathing	.350	.128	.087	.066
i. 1/2" Sheetrock	.288	.130	.088	.066
j. Gyplap Sheathing and 1/2" Sheetrock	.368	.142	.093	.069

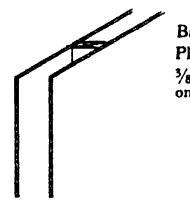


WALLS

Basic Construction
8" Brick Wall—4" Face Brick and 4" Common Brick—No interior finish

	No Wool Between Studs*	Adding Red Top Wool** 1"	2"	3"
Basic Construction	.500	..	..	..
Adding to Above Basic Const.				
a. 1/2" Plaster	.480	..	..	..
b. Rocklath and Plaster (Furred)	.300	.143	.093	.069
c. 1/2" WW Plaster Base and Pl. (Furred)	.220	.121	.084	.064
d. 3/4" WW Plaster Base and Pl. (Furred)	.190	.112	.079	.061
e. 1" WW Plaster Base and Pl. (Furred)	.160	.101	.073	.058
f. 1/2" WW Bldg. Bd., Tile or Plank	.230	.124	.085	.065
g. 3/4" WW Bldg. Bd., Tile or Plank	.200	.115	.081	.062
h. 1" WW Bd., Plank or Tile	.170	.104	.075	.059
i. 1/2" Sheetrock Furred	.320	.146	.095	.070

*Based on 3/8" Furring Strip **Based on Full Dimension



WALLS

Basic Construction—Plywood
Plywood on Wood Studs
3/8" Outside—1/4" Inside with one Air Space Over 3/4"

	No Wool Between Studs	Adding Red Top Wool 1"	2"	3"
Basic Construction	.431	.151	.095	.074
Substituting in Above Basic Const.				
a. 1/2" WW Bldg. Bd., Tile or Plank	.275	.126	.087	.065
b. 3/4" WW Bldg. Bd. or Tile	.230	.115	.081	.062
c. 1" WW Bldg. Bd. or Tile	.196	.106	.076	.060
d. 3/8" Sheetrock	.430	.151	.095	.074
e. 1/2" Sheetrock	.413	.148	.095	.074
f. Adding to basic construction 25/32" WW Sheathing	.218	.113	.080	.061

CEILINGS

Basic Construction
3/8" Rocklath and 1/2" Plaster

	No Wool Between Joists	Adding Red Top Wool 1"	2"	3"
Basic Construction	.610	.169	.116	.080
Substituting in Above Basic Const.				
a. 1/2" WW Plaster Base & Plaster	.329	.136	.091	.068
b. 3/8" WW Plaster Base & Plaster	.290	.128	.087	.066
c. 1" WW Plaster Base & Plaster	.213	.110	.079	.061
d. 1/2" WW Bldg. Bd., Tile or Plank. No Plaster	.356	.139	.092	.067
e. 3/4" WW Bldg. Bd. or Tile	.268	.124	.086	.065
f. 1/2" WW Bldg. Bd. or Tile	.220	.113	.080	.062
g. 3/8" Sheetrock	.670	.174	.118	.089
h. 1/2" Sheetrock	.635	.170	.115	.079

FLOORS

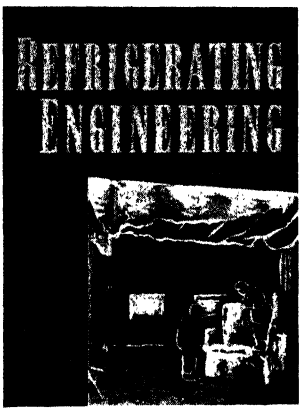
Basic Construction
Maple or Oak Flooring on Yellow Pine Sub-Flooring

	No Wool Between Joists	Adding Red Top Wool 1"	2"	3"
Basic Construction	.340	.138	.091	.068
Adding to Above Basic Const.				
a. 1/2" WW Bd. on bottom of joists	.180	.102	.075	.059
b. 3/4" WW Bd. on bottom of joists	.158	.094	.070	.055
c. 1" WW Bd. on bottom of joists	.141	.088	.066	.053

Above calculations based on data from A.S.H.V.E. GUIDE—1942.

American Society of Refrigerating Engineers

40 West 40th Street, **New York 18, N. Y.**



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LONG acknowledged the most authoritative periodical in the field, *Refrigerating Engineering* has added steadily to the practical value of its contents, and its number of readers has grown in proportion. A wide variety of material is presented, all from the viewpoint of its usefulness to the reader in his own business. This magazine is a must for men who keep in touch with all that is new and important in refrigeration and air conditioning. The annual subscription price is $3.

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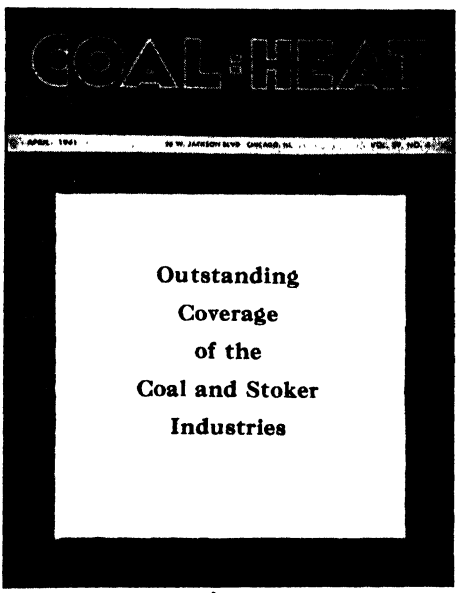
Coal-Heat

Published at

20 W. Jackson Blvd., **Chicago 4, Illinois**

Phone Wabash 9464



FOR information on the use and sale of stokers, coal and coal heating equipment, you can turn to COAL-HEAT with complete confidence.

Here is a magazine that appeals to every man concerned with the market, use and sale of solid fuel and modern heating equipment. Having long since recognized the importance of properly designed efficiently operated, properly maintained equipment to the successful use of coal, and therefore to the welfare of the coal industry, COAL-HEAT constantly emphasizes the significance of the "equipment factor" in heating merchandising.

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With over a million stokers in use today, the importance of COAL-HEAT's field is clearly evident. It has been and is COAL-HEAT's job to supply coal and stoker men with the information they need to insure satisfaction for stoker users. The same is true with hand-fired heating plants and all kinds of household and commercial coal heating equipment.

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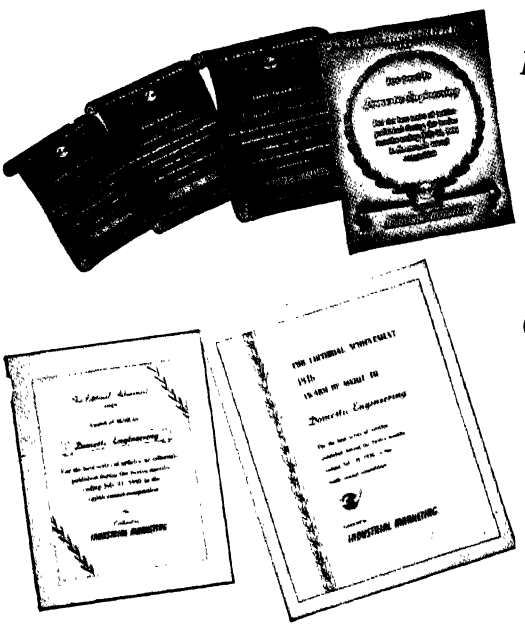
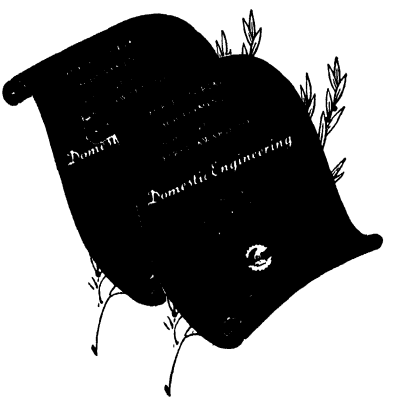
1900 Prairie Avenue, **Chicago 16, Illinois**



Again . . .
DOMESTIC ENGINEERING
Receives Awards for
Editorial Achievement

2 Awards in 1947!



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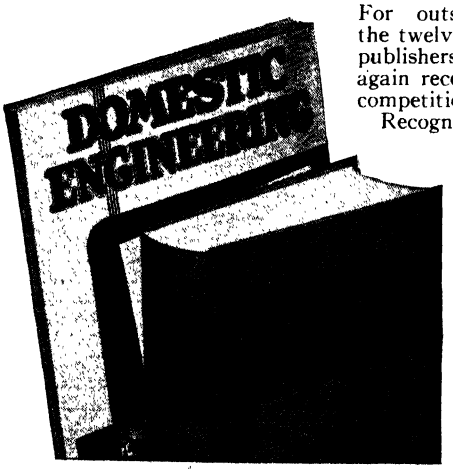

For outstanding editorial achievement during the twelve month period ending July 31, 1947, the publishers of DOMESTIC ENGINEERING have again received high honors in the annual editorial competition conducted by Industrial Marketing.

Recognition for two more of its many outstanding accomplishments thus has come again to an organization which has been amazingly consistent in the winning of these awards. 1939, 1942, 1943, 1944, 1945, 1946 and now 2 awards in 1947! 8 times these highly coveted honors have been accorded to DOMESTIC ENGINEERING in acknowledgment of its editorial excellence. Rarely has an honor so great been bestowed on one organization . . . seldom has such a degree of consistency been attained in the face of the keen competition offered by hundreds of the nation's leading business papers.

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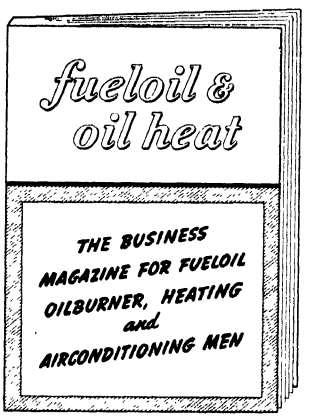

A. E. COBURN, *Editor*
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OILHEATING is a vertical, integrated industry, selling through the same retail outlets: oilburners, oilfired heating and air conditioning equipment, and fueloil.

Starting about 16 years ago, this integration of fuel and the equipment to burn it has grown until in 1947 two-thirds of all oilheating equipment (including boilers, furnaces and accessories) sales were made by companies that also supply the fuel, and about three-fifths of all heating oil was sold by companies also selling oilheating equipment.

FUELOIL & OIL HEAT, the only publication actively covering both the equipment and fueloil interests of dealers, was organized in 1922. It is recognized as the dominant editorial and advertising source for all heating contractors, fueloil dealers, furnacemen and others who actively sell oilheating; also for the many manufacturers who cultivate this vast market for their products and services through our low-cost advertising space.

Oilheating Manufacturers

Oilburner manufacturers in 1947 had factory shipments of 993,000 domestic burners and oil-boilers or oil-furnaces, more than 67 per cent above the industry's previous peak of 492,593 in 1946. This was accomplished in a year of constant material shortages.

Approximately 300 manufacturers of domestic oilburners and integral units are now in production, with a dozen of these supplying about half of the total output.

Dealers

Largest outlets for oilburners and related equipment in 1947 continued to be those firms who specialized in (had largest dollar volume in) oilburners or fueloil, the two groups accounting for 74 per cent of all oilburner retail business. The balance was divided among coal companies, who have added fueloil departments and sold 7 per cent of the oilburners, general heating dealers and contractors, who sold 5 per cent of the oilburners, with the remaining 14 per cent sold by a variety of dealer types.

Chief purchaser of domestic oilburners was the homeowner who had been shoveling coal. Of all 1947 oilburner installations, 57 per cent replaced handfired coal in old homes, 31 per cent went into new homes, 7 per cent replaced old oilburners 5 per cent replaced coal stokers and 1 per cent replaced gas heating burners.

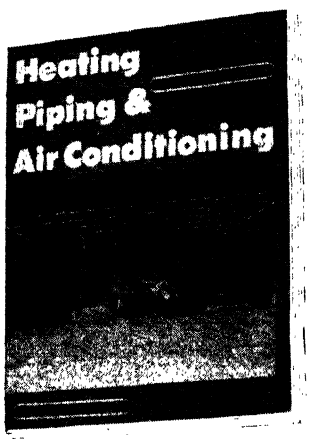
As the home building program got into full swing in 1947, dealers gave it much more attention than previously in the postwar period, since they had ample burners available above the numbers needed for the more profitable individual conversions from coal.

During the two and a half years since the war ended and restrictions on oilburning were lifted, the fueloil distributor has had a very strong gain in annual volume. At the close of 1947 the number of oilheated homes in the country was 57 per cent higher than the number when the war ended, and 27 per cent higher than at the end of 1946. In the oil industry, fueloil continues to expand in volume much faster than gasoline, and may soon become the principal petroleum product.

For a statistical picture of all phases of oilheating—wartime and postwar, send $1.00 for the January, 1948, Yearbook Issue and for a free copy of "Oilheating Tomorrow"—an 8-page statistical study.

KEENEY PUBLISHING COMPANY
6 North Michigan Avenue, **Chicago 2, Ill.**

Heating, Piping and Air Conditioning



This is the publication which carries the Journal of the A.S.H.V.E. in addition to its own regular editorial section. Its field is that of industry and large buildings. It is devoted to the design, installation, operation, and maintenance of heating, piping and air conditioning systems in such plants and buildings.

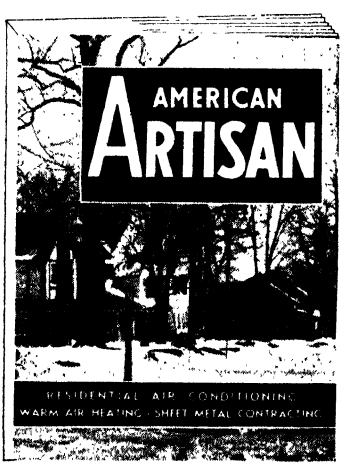
Each January issue includes a complete directory of commercial and industrial heating, piping, and air conditioning equipment, which lists all products, their trade names, and the manufacturers' addresses. It is the established buying and specifying guide of the industry.

H. P. & A. C. is read by consulting engineers and architects . . . contractors . . . and engineers in charge of heating, piping and air conditioning in industrial plants, and other large buildings, federal, state, and city governments, school boards, and public utilities. All A.S.H.V.E. members are subscribers.

Such coverage means, for the advertiser, consideration at all points in the selling of a heating, piping, or air conditioning product . . . consideration in its selection during the preparation of plans and specifications; in its actual purchase for installation; in its year-'round buying for operating and maintenance requirements. Without waste, the manufacturer of air conditioning products and equipment can reach through H. P. & A. C. those from whom he is seeking the necessary engineering acceptance. Write for our new booklet "A Quick Picture."

Member—A.B.P.—A.B.C. Subscription Prices—U.S. $3 per year.
Canada, Central and So. America—$4 per year. Elsewhere $6 per year.

American Artisan



AMERICAN ARTISAN covers the field of warm air heating, residential air conditioning, and sheet metal contracting. Its readers are warm air heating and sheet metal contractors, dealers, jobbers, manufacturers, and public utility companies.

A special section of each issue has been devoted to air conditioning since 1932, when it first became apparent that air conditioning for homes was to be along the lines of the central forced warm air heating system. As a result of the ready adaptability of this type of heating system to all air conditioning factors, hundreds of thousands of homes today have winter air conditioning—supplied through forced warm air heating with air cleaning and humidification. Cooling apparatus can be attached to these systems readily whenever year-'round air conditioning is desired.

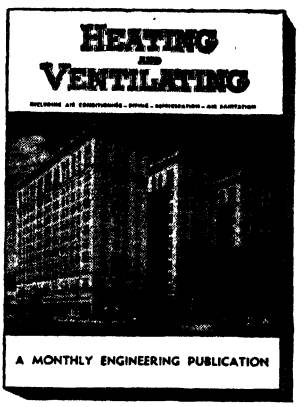
Each January issue includes a complete directory of warm air heating, air conditioning, and sheet metal products and equipment, which lists all products, their trade names, and the manufacturers' addresses.

The key man in the residential air conditioning picture is the warm air heating and sheet metal contractor—the one man experienced in "treating air" at a central place and getting it properly distributed. And the key publication—because it reaches these key men with an information service that has made it the recognized authority on residential air conditioning practice—is AMERICAN ARTISAN. For full information on this field, write for a copy of "A Quick Picture."

Member—A.B.P.—A.B.C. Subscription Prices—U.S. $3 per year.
Canada, Central and So. America—$4 per year. Elsewhere $6 per year.

HEATING — VENTILATING

AIR CONDITIONING - PIPING - HEATING - VENTILATION - REFRIGERATION



HEATING AND VENTILATING is a monthly publication read by engineers and contractors. These are the men who specify, install and maintain the mechanical equipment used in heating, ventilating, air conditioning and refrigeration systems of industrial, commercial and institutional buildings and residential projects. Its readers include also engineers and designers of the firms which manufacture this mechanical equipment.

The editorial content is edited to be of practical use to these engineers, and is prepared under the direction of field-experienced professional engineers.

Generally speaking, the emphasis is on practical rather than on theoretical considerations.

Each month an original Reference Data sheet is included for permanent use in a standard binder.

Special sections are published from time to time. These sections are devoted to subjects of timely interest, such as Heat Pump, Radiant Heating, Piping, Cooling Coils, Air Sanitation, Exhaust Hoods, Air Conditioning, etc. A comprehensive Buyers Directory is published each fall.

CIRCULATION

HEATING AND VENTILATING'S total distribution (A. B. C. Report, May, 1947)—classified as follows:

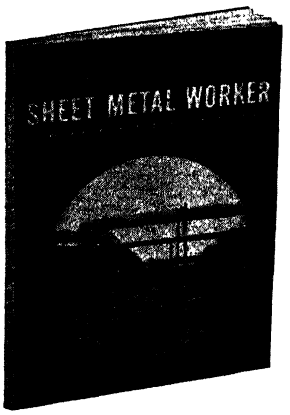
Consulting Engineers (388) and Architects (132) Engineers Employed by them (430)	950
Contractors (1,991) and Engineers Employed by Contractors (412)	2,403
Governments and School Boards and their Engineers	889
Public Utility Group	575
Industrial Firms, their Executives, Engineers and other Employees	2,005
Buildings, Real Estate Management Companies, their Engineers	677
Manufacturers of Air Conditioning, Heating, Piping and Ventilating Equipment, Their Officials and Employees (843) and Designing Engineers (227)	1,070
Manufacturers' Agents and Sales Engineering Firms (197) Sales Engineers and Salesmen (938)	1,135
Wholesalers (143) and Dealers (517)	660
Educational Institutions, Libraries, Technical Associations	458
Miscellaneous and Unclassified	324
	11,146
Field Staff, Correspondents, Exchanges, Advertisers, Advertising Agencies and Samples	589
TOTAL	11,735

Subscriptions to HEATING AND VENTILATING, 148 Lafayette St., New York 13, are $3.00 a year.

Sheet Metal Worker

Published by Edwin A. Scott Publishing Company

45 West 45th Street, **New York 19, N. Y.**



Subscription rates—$3.00 per year, U. S., Canada and Pan Amer. Foreign $4.00. Advertising rates on request.

THE January 1948 issue of SHEET METAL WORKER was its 74th Anniversary and Directory Number. It is the oldest publication in its field and is of vital importance to men interested in sheet metal work—air conditioning—warm-air heating and ventilation. Founded in 1874 and published to 1909 by David Williams Company; 1909 to 1920 by United Publishers Corp.; since 1920 by, the Edwin A. Scott Publishing Co.

Subscribers are mainly merchandising contractors purchasing practically all products and equipment which they fabricate, erect or install. Manufacturers, jobbers and distributors also subscribe.

The market has three main divisions:

(1) Equipment for resale in connection with erection or installation work.
(2) Materials for fabrication.
(3) Shop equipment and supplies.

Circulation: SHEET METAL WORKER is a member of the Audit Bureau of Circulations and the Associated Business Papers.

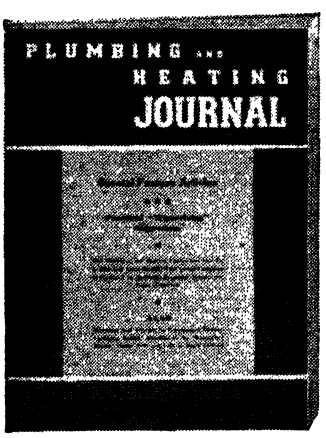
SHEET METAL WORKER also publishes books on heating, ventilating, sheet metal work, air conditioning, etc.

The Annual Issue published in January, contains a comprehensive and valuable Directory Section.

Plumbing and Heating Journal

Scott-Choate Publishing Co., Inc., *Publisher*

45 West 45th Street, **New York 19, N. Y.**



Subscription rates—$3.00 per year, U. S., Canada and Pan Amer. Foreign $4.00. Advertising rates on request.

PLUMBING and Heating Journal is edited to furnish a well-rounded, efficient service to the men engaged in the plumbing, heating, ventilating and air conditioning fields. It covers both the technical and business phases of their work.

It gives free technical service through a staff of practical engineers; expert merchandising assistance, and its technical and business articles are by men of recognized competence.

THE JOURNAL editorial department draws its news from scores of trained correspondents located at strategic points throughout the country.

This combination of the technical, business, news and other aspects of the industry enables THE JOURNAL to achieve a finely balanced magazine that gives the reader the type of information he wants and needs, in brief, compact form.

A department "With the Water Systems," informs the trade of the latest developments in the rural plumbing field and its increasing potentialities for the plumbing—heating contractor, especially with the recent extensions of rural electric lines throughout the country.

ENGINEERS OF HUMAN COMFORT

The Heating, Ventilating and Air Conditioning Engineer through his work and research brings to our homes, our offices and our factories, in both summer and winter, that climate best suited to our comfort and health, and he creates for our industries those atmospheric conditions which improve quality of product and speed production.

He is truly an *Engineer of Human Comfort* and a public benefactor.

It was in 1894 that a small group of nationally known engineers, educators, and manufacturers organized the A.S.H.V.E. for the express purpose of improving the art through the interchange of ideas and stimulation of scientific research and invention.

In 1894, it was agreed that the great art of heating and ventilating deserved and required recognition as an essential, distinctive and highly specialized division of modern engineering. These men realized the basic importance of heating and ventilating as the primary element in the well-being of civilized mankind, living and working mostly indoors.

These keen, alert, progressive men knew that the methods and equipment of their day could be improved even beyond their own vision if all the personalities striving for such improvement could be welded into one organized cooperative group, imbued with the same ideals and set toward the same goal. So they formed themselves into the nucleus of such an organization and called it THE AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS.

That the Charter Members had great faith in their enterprise is evident, although little did they dream that progress would be so rapid in their profession.

During the intervening years since that little group of 75 pioneers unfurled the banner of THE AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS—6065 of the real leaders of thought and action in heating, ventilating, and air conditioning have gathered about that standard and carried it proudly before them far along the way of real accomplishment. They may be identified among engineering groups by the distinctive emblem which was adopted by the Charter Members.

The record of the Society's accomplishments is a long and brilliant one, yet it must embrace but a small part of the real achievement which the Society has inspired both among its members and the many non-members whose work it has influenced. Rewarding the efforts of its founders, who gave unstintingly of their time and means, the Society has been tremendously effective in the advancement of the Art and Industry through its manifold activities.

FOUNDING OF THE A. S. H. V. E.

The organization of a Society of heating and ventilating engineers was first talked of by Hugh J. Barron and L. H. Hart in the early summer of 1894.

On August 2, 1894, a group of 15 men met at the office of *Heating and Ventilation*, 146 World Bldg., New York, and a committee of 5 was chosen to effect an organization.

The first meeting was called at 3:00 P.M., September 10, 1894, at the Broadway Central Hotel and temporary officers were elected: F. P. Smith, *Chairman*; and L. H. Hart, *Clerk*. The roll call showed that 75 persons had become Charter Members. It was voted that the name of the organization should be THE AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS and a Constitution and By-Laws were adopted. The following were elected to hold office until the 1st Annual Meeting, January 22-24, 1895: *President*, E. P. Bates, Syracuse, N. Y.; *First Vice-President*, W. M. Mackay, New York, N. Y.; *Second Vice-President*, W. F. Wolfe, Boston, Mass.; *Third Vice-President*, Chas. S. Onderdonk, Philadelphia, Pa.; *Treasurer*, Judson A. Goodrich, New York, N. Y.; *Secretary*, L. H. Hart, New York, N. Y.; *Board of Managers*, E. P. Smith, H. J. Barron, A. A. Cary, New York; James A. Harding, Vineyard Haven, Mass.; Henry Adams, Washington, D. C.; *Council on Membership*, Chas. W. Newton, Baltimore, Md.; R. C. Carpenter, Ithaca, N. Y.; Albert A. Cryer, New York; F. W. Foster, Boston; U. G. Scollay, Brooklyn, N. Y.

A. S. H. V. E. RESEARCH LABORATORY

Since 1919 THE AMERICAN SOCIETY OF HEATING AND VENTILATING ENGINEERS has maintained a permanent research staff and facilities devoted solely to the study of fundamental problems in the field of heating, ventilating and air conditioning. During the past quarter century much has been done to advance the art by establishing scientifically sound data which the engineer can apply in the design, operation, and maintenance of heating, ventilating, and air conditioning systems and equipment.

For twenty-five years the Society's Research Laboratory was located at the U. S. Bureau of Mines Building, Pittsburgh, Pa. The Laboratory was moved to Cleveland in 1944, and early in 1946 the Society purchased premises at 7218 Euclid Avenue. In addition to work at the Society's Laboratory, a substantial part of the research program has been carried on through the medium of cooperative agreements with leading educational institutions of the United States and Canada.

All research activities are planned and supervised by the Committee on Research of 15 elected members, assisted by various Technical Advisory Committees of the Society. The research activities are financed from Society funds, of which a portion comes from membership dues and from its publications, and these funds are amplified by contributions from friends in the industries engaged in the general field of heating, ventilating, and air conditioning.

THE GUIDE

A distinctly new service was inaugurated by the Society in 1922 when it established THE GUIDE. Now in 1948, as the 26th Edition of the HEATING VENTILATING AIR CONDITIONING GUIDE makes its appearance, it is notable that THE GUIDE has served effectively not only the membership but the entire profession and the allied industries, and has received world wide recognition as a reliable and authoritative compendium of useful heating, ventilating and air conditioning data.

Throughout the 26 years of its service THE GUIDE has become a reference book of unchallenged position in its special field of engineering. The intention of its founders, to provide an instrument of service containing reference material on the design and specification of heating, ventilating and air conditioning systems and containing essential and reliable information concerning modern equipment, has been carefully safeguarded by those responsible for the compilation of each edition.

During its quarter century of service THE GUIDE has progressed from a distribution of 5,000 copies to the present distribution of 18,000 and it has reached all parts of the world.

Throughout the years THE GUIDE has served a double purpose of providing the profession with a practical reference work and the advertiser with an effective medium for dissemination of catalog data.

1948
Roll of Membership

AMERICAN SOCIETY *of*
HEATING *and* VENTILATING ENGINEERS

Corrected to January 31, 1948

Published at the Headquarters of the Society
51 Madison Avenue, New York 10, N. Y.

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AMERICAN SOCIETY *of* HEATING *and* VENTILATING ENGINEERS

51 Madison Ave., New York 10, N. Y.

1947-48

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Glass: R. A. Miller, *Chairman;* A. B. Algren, Dr. F. L. Bishop, Jr., J. E. Frazier, J. S. Herbert, E. H. Hobbie, L. K. Jones, C. O. Mackey*, F. Preston, W. C. Randall, Vic Sanders, H. B. Vincent, G. B. Watkins.

Heating Load: T. F. Rockwell, *Chairman;* C. M. Ashley, R. A. Biggs, A. I. Brown, R. C. Cross*, R. S. Dill, W. S. Harris, J. M. Hartman, S. I. Rottmayer, M. W. Shears, G. H. Tuttle.

Industrial Ventilation: W. N. Witheridge, *Chairman;* A. D. Brandt, W. B. Harris, W. C. L. Hemeon, D. E. Humphrey, J. M. Kane, M. G. Kershaw, L. L. Lewis, L. G. Miller*, H. A. Mosher, Ralph Poole, B. F. Postman, B. R. Small, R. P. Warren, H. E. Ziel.

Insulation: E. R. Queer, *Chairman;* R. E. Backstrom, C. B. Bradley, H. E. Lewis, L. E. Pasek, H. E. Robinson, Vic Sanders, T. D. Stafford, R. K. Thulman*, T. T. Tucker, P. M. Woodworth.

Panel Heating and Cooling: G. D. Winans, *Chairman;* A. B. Algren, R. L. Byers, P. B. Gordon, L. N. Hunter*, John James*, J. S. Locke, H. F. Randolph. *Group A—Heat Distribution Within and Behind the Panel:* L. N. Hunter*, *Chairman;* P. B. Gordon, *Vice-Chairman;* A. B. Algren, R. A. Biggs, Wharton Clay, R. S. Dill, H. L. Flodin, Dr. F. E. Giesecke, W. S. Harris, C. F. Kayan, G. D. Lain, R. S. Leigh, C. W. Meininger, D. L. Mills, C. W. Nessell, P. S. Park, S. I. Rottmayer, S. M. Van Kirk, L. H. Yeager. *Group B—Heat Transfer Between the Panel and the Space:* John James*, *Chairman;* H. F. Randolph, *Vice-Chairman;* C. M. Ashley, J. T. Bergen, C. F. Boester, Linn Helander, A. L. Jaros, Jr., H. A. Lockhart, C. O. Mackey*, R. A. Miller, G. W. Penney, G. G. Sward, J. M. van Nieukerken. *Group D—Controls:* J. S. Locke, *Chairman;* A. B. Algren, H. W. Alyea, S. D. Browne, R. L. Campbell, C. M. Garner, P. B. Gordon, W. J. Hajek, A. J. Keating, Dr. Waldo Kliever, H. T. Kucera, P. F. Neess, R. S. Penn, J. K. M. Pryke, E. J. Ritchie, C. W. Signor, N. D. Skinner, A. S. Widdowfield.

Physiological Research: C.-E. A. Winslow, *Chairman;* Thomas Bedford, M.D., A. R. Behnke, M.D., A. C. Burton, M.D., E. F. DuBois, M.D., A. P. Gagge, F. W. Hutchinson*, R. W. Keeton, M.D., D. H. K. Lee, M.D., Andre Missenard, Charles Sheard.

Sensations of Comfort: C. P. Yaglou, *Chairman;* R. S. Arnold, A. R. Behnke, M.D., Thomas Chester, F. G. Ewens, M. K. Fahnestock*, J. D. Hardy, M.D., F. C. McIntosh, A. B. Newton, K. E. Robinson.

Sorbents: John Everetts, Jr., *Chairman;* F. C. Dehler, John A. Goff*, C. H. B. Hotchkiss, E. R. McLaughlin, J. C. Patterson, G. L. Simpson, F. J. Swaney.

Sound Control: T. A. Walters, *Chairman;* C. M. Ashley, P. H. Geiger, W. H. Hoppmann, II, G. C. Kerr, R. D. Madison*, J. S. Parkinson, A. G. Sutcliffe, T. H. Troller.

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*Member of Committee on Research.

Officers of Local Chapters, 1947-48

Atlanta

Headquarters, Atlanta, Ga.

Meets: First Friday in Month

President, H. KING MCCAIN
615 Trust Co. of Georgia Bldg.

Secretary, LEO SUDDERTH, JR.
306 Bona Allen Bldg., Atlanta 3

Central New York

Headquarters, Syracuse, N. Y.

President, H. G. STRONG
300 S. Geddes St., Syracuse 1

Secretary, G. F. KEANE
316 Haddonfield Dr., DeWitt, N. Y.

Central Ohio

Headquarters, Columbus, Ohio

Meets: Third Monday in Month

President, R. B. BRENEMAN
1282 Edgehill Rd., Columbus 8

Secretary, E. A. NORMAN, JR.
1150 Chesapeake Ave., Columbus

Cincinnati

Headquarters, Cincinnati, Ohio

Meets: First Tuesday in Month

President, H. K. JENNINGS
1639 Union Trust Bldg., Cincinnati 2

Secretary, K. B. LITTLE
832 Temple Bar Bldg., Cincinnati 2

Connecticut

Headquarters, New Haven, Conn.

President, S. R. OSBORNE
Waterbury 91

Secretary, WINFIELD ROEDER
405 Temple St., New Haven

Delta

Headquarters, New Orleans, La.

Meets: Second Tuesday in Month

President, J. S. BURKE
317 Baronne St., New Orleans 9

Secretary, R. B. GUEST
827 Dryades St., New Orleans 13

Golden Gate

Headquarters, San Francisco, Calif.

Meets: First Wednesday in Month

President, F. W. KOLB
598 Monadnock Bldg., San Francisco 5

Secretary, K. F. BALDWIN, JR.
419 Kentucky Ave., Berkeley 7

Illinois

Headquarters, Chicago, Ill.

Meets: Second Monday in Month

President, W. A. KUECHENBERG
1714 Sheffield Ave., Chicago 14

Secretary, G. W. BORNQUIST
629 W. Washington Blvd., Chicago 6

Officers and List of Chapters, 1947-48—(*Continued*)

Indiana

Headquarters, Indianapolis, Ind.
Meets: Fourth Friday in Month
President, I. W. COTTON
1035 N. Pennsylvania St., Indianapolis 4
Secretary, W. R. FENSTERMAKER
215 E. New York St., Indianapolis 4

Iowa

Headquarters, Des Moines, Ia.
Meets: Second Tuesday in Month
President, C. A. WHEELER
1217 Grand Ave., Des Moines
Secretary, D. E. WELLS
304 Home Federal Bldg., Des Moines 9

Kansas City

Headquarters, Kansas City, Mo.
Meets: First Monday in Month
President, P. C. LEFFEL
3323 Main St., Kansas City 2
Secretary, HENRY NOTTBERG, JR.
914 Campbell, Kansas City

Manitoba

Headquarters, Winnipeg, Man., Canada
Meets: Third Thursday in Month
President, D. S. SWAIN
1186 Downing St., Winnipeg
Secretary, A. W. MOSS
26 Ferndale Ave., Norwood, Manitoba

Massachusetts

Headquarters, Boston, Mass.
Meets: Third Tuesday in Month
President, ADOLPH EHRENZELLER
329 Washington St., Dorchester 21
Secretary, R. T. KERN
51 Claflin St., Leominster

Memphis

Headquarters, Memphis, Tenn.
Meets: First Monday in Month
President, N. C. LEDBETTER
22 S. Cooper St., Memphis 4
Secretary, A. T. BEVIL
1521 Waverly Ave., Memphis 6

Michigan

Headquarters, Detroit, Mich.
Meets: First Monday after 10th of Month
President, A. E. KNIBB
1003 Maryland Ave., Detroit 30
Secretary, L. A. BURCH
5853 Hamilton Ave., Detroit 2

Minnesota

Headquarters, Minneapolis, Minn.
Meets: First Monday in Month
President, L. C. GROSS
5324 Oaklawn Ave., Minneapolis 10
Secretary, L. J. KRAUSE
2753 4th Avenue S., Minneapolis 8

Montreal

Headquarters, Montreal, Que., Canada
Meets: Third Monday in Month
President, T. H. WORTHINGTON
405 Beaubien St. W., Montreal, Que.
Secretary, S. W. SALTER
910 New Birks Bldg., Montreal

Nebraska

Headquarters, Omaha, Neb.
Meets: Second Tuesday in Month
President, VERNE SIMMONDS
2416 Vane St., Omaha
Secretary, G. W. COLBURN
106 N. 15th St., Omaha 2

New York

Headquarters, New York, N. Y.
Meets: Third Monday in Month
President, M. C. GIANNINI
New York University, New York 53
Secretary, CARL H. FLINK
Room 3000, 51 Madison Ave., New York 10

North Carolina

Headquarters, Durham, N. C.
Meets: Quarterly
President, E. S. DEWITT
1211 Commercial Bank Bldg., Charlotte
Secretary, R. M. WARREN, JR.
1001 N. Church St., Charlotte 1

North Texas

Headquarters, Dallas, Tex.
Meets: Third Monday in Month
President, C. R. GARDNER
1000 St. Louis St., Dallas 1
Secretary, G. A. LINSKIE
3124 Milton St., Dallas 5

Northern Ohio

Headquarters, Cleveland, Ohio
Meets: Second Monday in Month
President, JOHN JAMES
3170 W. 106th St., Cleveland 11
Secretary, W. M. ROWE
1302 Swetland Bldg., Cleveland 15

Oklahoma

Headquarters, Oklahoma City, Okla.
Meets: Second Monday in Month
President, W. W. FRANKFURT
519 Apco Tower, Oklahoma City
Secretary, J. H. SPAAN, JR.
1303 N. Klein, Oklahoma City 6

Ontario

Headquarters, Toronto, Ont., Canada
Meets: First Monday in Month
President, D. A. STOTT
195 Spadina Ave., Toronto
Secretary, H. R. ROTH
57 Bloor St., W., Toronto, Ont.

Officers and List of Chapters, 1947-48—(*Concluded*)

Oregon

Headquarters, Portland, Ore.
Meets: Thursday after First Tuesday in Month
President, C. W. BRISSENDEN
Electric Bldg., Portland 5
Secretary, L. G. WILLIAMS
Box 304, Gladstone

Pacific Northwest

Headquarters, Seattle, Wash.
Meets: Second Tuesday in Month
President, E. H. LANGDON
72 Vine St., Seattle
Secretary, E. J. ROSEN
10238 18th Ave., S. W., Seattle 66

Philadelphia

Headquarters, Philadelphia, Pa.
Meets: Second Thursday in Month
President, E. H. DAFTER
12 S. 12th St., Philadelphia 7
Secretary, E. K. WAGNER
2240 N. Broad St., Philadelphia 32

Pittsburgh

Headquarters, Pittsburgh, Pa.
Meets: Second Monday in Month
President, D. W. LOUCKS
435 Sixth Ave., Pittsburgh 19
Secretary, E. H. RIESMEYER, JR.
231-33 Water St., Pittsburgh 22

Rocky Mountain

Headquarters, Denver, Colo.
Meets: First Wednesday in Month
President, J. F. MOHAN
2229 Blake St., Denver 2
Secretary, H. C. KUGELER
2365 Ash St., Denver 7

St. Louis

Headquarters, St. Louis, Mo.
Meets: First Tuesday in Month
President, J. H. CARTER
710 Key West Ave., Webster Groves 19
Secretary, J. S. ROSEBROUGH
1014 Arcade Bldg., St. Louis 1

South Texas

Headquarters, Houston, Tex.
Meets: Third Friday in Month
President, D. M. MILLS
Gray and Crawford, Houston 3
Secretary, L. L. LADEWIG
Box 1188, Houston 1

Southern California

Headquarters, Los Angeles, Calif.
Meets: Third Wednesday in Month
President, R. A. LOWE
6381 Hollywood Blvd., Los Angeles 28
Secretary, JOHN L. BLAKE
1700 S. Bedford St., Los Angeles 35

Southwest Texas

Headquarters, San Antonio, Tex.
President, F. C. BENHAM, JR.
702 S. Flores St., San Antonio
Secretary, L. S. PAWKETT
810 Insurance Bldg., San Antonio 5

Utah

Headquarters, Salt Lake City, Utah
Meets: First Wednesday in Month
President, E. V. GRITTON
2470 S. 15th, Salt Lake City 5
Secretary, C. E. FERGUSON
838 Garfield Ave., Salt Lake City

Virginia

Headquarters, Norfolk, Va.
President, R. C. THOMAS
819 Westover Ave., Norfolk 7
Secretary, J. F. REYNOLDS
Gatling and Marble Ave., Norfolk 2

Washington, D. C.

Headquarters, Washington, D. C.
Meets: Second Wednesday in Month
President, H. H. HILL
438 Woodward Bldg., Washington 5
Secretary, J. G. MUIRHEID
2013 New Hampshire Ave., N.W., Washington 9

Western Michigan

Headquarters, Grand Rapids, Mich.
Meets: Second Monday in Month
President, FRANK HARBIN, JR.
280 E. 6th St., Holland
Secretary, W. C. DEROO
500 E. 8th St., Holland

Western New York

Headquarters, Buffalo, N. Y.
Meets: Second Monday in Month
President, G. E. ADEMA
39 W. Balcom St., Buffalo 9
Secretary, J. H. BRYCE
88 E. Girard Blvd., Kenmore

Wisconsin

Headquarters, Milwaukee, Wis.
Meets: Third Monday in Month
President, J. R. VERNON
507 E. Michigan St., Milwaukee 2
Secretary, B. M. KLUGE
1817 S. 66th St., Milwaukee 14

Student Branch
Texas A. & M. College

Headquarters, College Station, Tex.
Meets: Third Thursday in Month
President, G. H. JACKSON
225 W. Nevada St., El Paso
Secretary, T. V. BURNS, JR.
P. O. Box 1651, College Station

Roll of Membership

AMERICAN SOCIETY *of* HEATING *and* VENTILATING ENGINEERS

1948

(Corrected to January 31, 1948)

HONORARY MEMBERS

CARRIER, WILLIS H. (1944) (M 1913), (Presidential Member), Syracuse, N. Y.
FIELDNER, A. C. (1944) Washington, D. C.

BALDWIN, WM. J. (1915) New York, N. Y. (Deceased May 7, 1924).
BILLINGS, DR. J. S. (1896) New York, N. Y. (Deceased March 10, 1913).
BOLTON, REGINALD PELHAM (1897), (Presidential Member), New York, N. Y. (Deceased February 18, 1942).
BRECKENRIDGE, L. P. (1920), North Ferrisburg, Vt. (Deceased August 22, 1940).
GORMLY, JOHN (Charter Member), Norristown, Pa. (Deceased January 31, 1929).
NEWTON, C. W. (Charter Member), Baltimore, Md. (Deceased August 6, 1920).
HOOD, O. P. (1929), Washington, D. C. (Deceased April 22, 1937).
JELLETT, STEWART A. (Charter Member), (Presidential Member), Philadelphia, Pa. (Deceased April 5, 1935).

LIST OF MEMBERS
Arranged Alphabetically

(*Asterisk indicates authorship of papers; • indicates address for mail)

(*M* **1923**; *A* **1918**; *J* **1916**) indicates, Election as Member 1923; Associate 1918; Junior 1916.
(**Pres. 1923**) indicates, Elected President in 1923 and is now a Presidential Member.

A

ABBOTT, Furman S. (*M* 1943) Chief Engr., W. H. Wheeler, Inc., 7 East 47th St., New York, N. Y., and • 80 Afterglow Ave., Montclair, N. J.

ABBOTT, Thomas J. (*M* 1938) Vice-Pres., • George C. Abbott, Ltd., 52 Shaftesbury Ave., and 294 Oriole Pkwy., Toronto, Ont., Canada.

ABENDROTH, Harold F. (*A* 1947) Sales Engr., • Temperature Control, 710 Commercial National Bank Bldg., Peoria 1, and 201 Ehrett St., Creve, Ill.

ABRAMS, Abraham (*M* 1927; *J* 1924) Cons. Engr., 112 Bon Air Ave., New Rochelle, N. Y.

ABRAMSON, Ralph J. (*A* 1938) Mech. Engr., 1834 Pratt Ave., Chicago 26, Ill.

ACHENBACH, Paul R.* (*M* 1942) Asst. Chief, Htg. & Air Cond. Section, • National Bureau of Standards, Connecticut Ave. and Van Ness St., Washington, D. C., and 1912 N. Randolph St., Arlington, Va.

ACHESON, L. K. (*M* 1944) Laboratory Coordinator, The Hoover Co., and • 816 Portage St., North Canton, Ohio.

ACHEY, Harry S. (*J* 1947) Assoc., C. E. Mills, 801 James Bldg., Chattanooga, Tenn., and • 1109 S. Crest Rd., Rossville, Ga.

ACHEY, H. Norwood (*A* 1947) Owner, Norwood Achey Co., and • John Ross Rd., Rossville, Ga.

ACKER, Charles B. (*M* 1946) Mech. Engr., • Yonge & Hart, Archts., 614 Blount Bldg., and 2025 North 11th Ave., Pensacola, Fla.

ACKERMANN, Reynold H. (*M* 1943) Engr., Charles S. Leopold, Cons. Engr., 213 Broad St., Philadelphia, and • 267 Cooper Ave., Lansdowne, Pa.

ADAIR, James S. (*A* 1941; *J* 1940) Owner, • James S. Adair, Sales Engrs., 306 Pere Marquette Bldg., New Orleans, and 715 Phosphor Ave., New Orleans 20, La.

ADAM, Ray W. (*A* 1938) Owner • W. A. Adam Co., 8810 Grinnell Ave., Detroit 13, and 951 E. Grand Blvd., Detroit, Mich.

ADAMS, Chester Z. (*M* 1939) Owner and Mgr., • Chet Adams Co., Box 1356, 209½ Bellemeade St., and 207 E. Avondale Dr., Greensboro, N. C.

ADAMS, Eugene E. (*A* 1938) Sales Engr., • Garden City Fan Co., Room 1508 A, 55 West 42nd St., New York 18, and 35-46–79th St., Jackson Heights, N. Y.

ADAMS, Eugene F. (*M* 1941) Mech. Engr., • Peter Kiewit Sons' Co., P. O. Box 739, and 276 Wai Nani Way, Honolulu, T. H.

ADAMS, Frank L. (*M* 1939) Htg. and Air Cond. Engr., • P. O. Box 840, Denver 1, and 1185 Grape St., Denver 7, Colo.

ADAMS, George F. (*M* 1944) Engr., • Midwest Plumbing & Heating Co., 2450 Blake St., Denver, and 3301 Jay St., Wheat Ridge, Colo.

ADAMS, Harold E. (*M* 1930) Chief Engr., • The Nash Engineering Co., South Norwalk, and Merrill Heights, Norwalk, Conn.

ADAMS, Neil D. (*M* 1929), (Council 1938-40) Supt., • Franklin Heating Station, 220 Second Ave., S. W., and R. F. D. No. 2, Elne-Dell, Rochester, Minn.

ADAMS, Octavius C. (*A* 1944) Sales Engr., Owner, • Adams Heating Equipment Co., 41 East 42nd St., Room 314, New York 17, and 32-20 93rd St., Jackson Heights, N. Y.

ADAMS, Robert B. (*A* 1946) Chief Power Plant Engr., Nordberg Manufacturing Co., 3073 S. Chase Ave., and • 2855 South 46th St., Milwaukee 7, Wis.

ADAMS, Robert Russell (*A* 1947) Supvr., Gilson Manufacturing Co., Ltd., Guelph and • 245 Kennedy Rd., Toronto 13, Ont., Canada.

ADAMS, Thomas K. (*M* 1946) Mgr., Htg. and Vent. Dept., • Reunert & Lenz, Ltd., P. O. Box 1092, and Halford Ave., Highlands N. Etn., Johannesburg, South Africa.

ADAMS, William J. (*A* 1945) Estimator, • 3911 W. North Ave., Chicago 47, and 1718 Nordica Ave., Chicago 35, Ill.

ADAMSON, L. C. (*A* 1945) Owner, • Air Conditioning & Heating Service Co., 3922 Troost, Kansas City 4, and 1920 East 71st Terrace, Kansas City, Mo.

ADDAMS, Homer (*Charter Member*; *Life Member*) (*Presidential Member*), (Pres., 1924; 1st Vice-Pres., 1923; Treas., 1915-22; Council, 1915-25) Chm., Board of Directors, Fitzgibbons Boiler Co., Inc., 101 Park Ave., New York 17, N. Y.

ADDAMS, Paul K. (*M* 1943) Pres., • Fitzgibbons Boiler Co., Inc., 101 Park Ave., New York 17, and 465 West 23rd St., New York 11, N. Y.

ADDIE, George R. (*M* 1945) Managing Dir., J. G. Wagstaff, Ltd., Alma Iron Works, Dukinfield, Cheshire, and • Mottram House, Mottram in Longdendale, Nr. Manchester, England.

ADDINGTON, Harold M. (*M* 1939) Leading Designer, Chemical Mfr., Nemours Bldg., Rm. 13524, and • 504 Delaware Ave., Wilmington, Del.

ADDINGTON, Herbert B. (*M* 1938) Cons. Engr., • Myers, Fuller and Addington, 21 East 40th St., New York 16, and 699 Ocean Ave., Brooklyn 26, N. Y.

ADEMA, George E. (*M* 1939) Prop., • N. M. Adema & Son, 39 W. Balcom St., Buffalo 9, and 299 Deerhurst Pkwy., Kenmore 17, N. Y.

ADLAM, T. Napier (*M* 1932) Vice-Pres. and Gen. Mgr., Sarco Manufacturing Corp., Empire State Bldg., Fifth Ave. and 34th St., New York, N. Y., and • 124 Forest Hill Rd., West Orange, N. J.

AEBERLY, John J. (*M* 1928), (Council, 1937-39) Chief of Bureau of Htg., Vtg. and Indus. Sanitation, City of Chicago, Room 702, City Hall, Chicago 2, and • 6225 N. Newcastle Ave., Chicago 31, Ill.

AHEARN, William J. (*M* 1929) 331 Newbury St., Boston, and • 131 Windermere Rd., Auburndale 66, Mass.

AHLFF, Albert A. (*M* 1923; *A* 1918) Sales, Rust-Oleum Corp., Evanston, Ill., and • 18 Heatherbrook Lane, Kirkwood 22, Mo.

AHLRICHS, Herman (*A* 1947) Owner, H. Ahlrichs Plumbing and Heating Co., and • 7 South 16th St., New Hyde Park, L. I., N. Y.

AIKEN, Hector H. (*A* 1947) Instructor, Mech. Engrg., • University of Arizona, and Rt. 6, Box 734, Tucson, Ariz.

AIKIN, A. A. (*M* 1945) Sales Engr., A A A Engineering Sales Co., and • Maplewood Manor, Lansing, Mich.

AIKIN, Frank W. (*A* 1945) Pres. and Treas., • Northern Controlled Heat Co., Inc., 557 Factory Square, and 126 Ward St., Watertown, N. Y.

AINSWORTH, Samuel E. (*A* 1939) Partner, • Roche Newton & Co., Box 1049, and 1524-25th St., Lubbock, Texas.

AITKEN, Milton Lawrence (*M* 1945) Gen. Mgr., Propellair, Inc., Div. of Robbins & Myers, Inc., and • 99 Broadmoor Blvd., Springfield, Ohio.

AITKEN, Thomas (*A* 1946) Owner, Aitken Co., 470 S. Nelson Rd., Columbus, and • 6422 Havens Corner Rd., Black Lick, Ohio.

AKERLOW, R. W. (*A* 1944) Sales Engr., • The Starns Roger Manufacturing Co., 1720 California St., and 935 S. Elizabeth St., Denver, Colo.

AKERMAN, Joseph R. (*M* 1946) Instructor in Mech. Engr., University of Wisconsin, M. E. Dept., and • 322 Karen Ct., Madison, Wis.

AKERS, George W. (*M* 1929) Pres., George W. Akers Co., 16525 Woodward Ave., Detroit 3, and • 1184 W. Tienken Rd., R. F. D. 2, Rochester, Mich.

ALBERT, William J. (*A* 1945) Air Cond. and Refrig. Designer, Stewart A. Jellett & Co., 1200 Locust St., Philadelphia, Pa., and • 665 Randolph St., Camden, N. J.

ALBRIGHT, C. Barton (*A* 1945) Owner, • C. Barton Albright, Engr., 114 Liberty St., New York, and 264 Rushmore Ave., Westbury Downs, L. I., N. Y.

ALBRIGHT, Joseph C. (*M* 1946) Cons. Engr., Davison Chemical Corp., Baltimore 3, Md., and • 107 Dartmouth Rd., Bala Cynwyd, Pa.

ALEXANDER, Granville P. (*M* 1944) Secy., • Htg., Piping & Air Cond. Contractors Philadelphia Assn., 328 Chestnut St., Room 208, Philadelphia 6, and Montgomery Ct., Apt. J-33, Narberth, Pa.

ALEXANDER, Hugh V. (*M* 1943) Branch Mgr., • Johnson Service Co., 922 Architects Bldg., Indianapolis 4, and 5700 Kingsley Dr., Indianapolis 5, Ind.

ALEXANDER, John L. (*A* 1944) Owner, • Charles H. Alexander & Son Co., 2746 Elmwood Dr. S.E., Grand Rapids 6, Mich.

ALEXANDER, John W. (*M* 1945) Design Engr., Office of the Supervising Architect, Public Buildings Administration, Washington 25, D. C., and • 403 Prince George St., Laurel, Md.

ALEXANDER, Keith O. (*M* 1943) Sales Engr., • Neil H. Peterson Co., 1129 Folsom St., San Francisco 3, and 454 Mastick Ave., San Bruno, Calif.

ALEXANDER, Samuel W. (*M* 1935) Pres., S. W. Alexander Co., Ltd., 182 Main St., and • 124 Kingsmount Park Rd., Toronto, Ont., Canada.

ALFAGEME, Braulio (*M* 1946) Almagro 1, Madrid, Spain.

ALFERY, Henry F. (*M* 1938) Pres., • Erie Manufacturing Co., 300 N. Eighth St., Milwaukee 3, and 1819 W. Center St., Milwaukee 6, Wis.

ALFSEN, Nikolai (*M* 1933) Civil Engr., Alfsen & Gunderson, Prinsensgt, 2B, and • Utsiktsveien 22, Stabekk, Oslo, Norway.

ALGER, Irving G., Jr. (*A* 1947) Mech. Engr., G. M. Simonson, 625 Market St., San Francisco 5, and • 2417 Taraval St., San Francisco 16, Calif.

ALGREN, A. B.* (*M* 1930) Assoc. Prof., Htg., Vent., and Air Cond., Engrg. Experiment Station, University of Minnesota, and • 5109-17th Ave. S., Minneapolis, Minn.

ALLAN, James E. (*M* 1946) Principal, • Hunt & Allan, 914 Main St., Cincinnati 2, and 2830 Harrison Ave., Cincinnati 11, Ohio.

ALLAN, William (*A* 1938) Pres., • Allan Engineering Co., 724 E. Mason St., Milwaukee 2, and 2735 N. Farwell Ave., Milwaukee 11, Wis.

ALLCORN, Luther H., Jr. (*A* 1946) Design Engr., The Bahnson Co., and • 2425 Elizabeth Ave., Winston-Salem 7, N. C.

ALLEN, Abraham B. (*A* 1945) Office Mgr., Oil Burning Engineers, Inc., 3146 W. Chicago Ave., Chicago 22, and • 2233 Birchwood Ave., Wilmette, Ill.

ALLEN, Arnold G. (*A* 1946) Sales Engr., • A. G. Allen Co., Liberty Bldg., Kentucky and Capitol Aves., Indianapolis, and Milroy, Ind.

ALLEN, A. Walter (*M* 1936) Sales Engr., Pease Foundry Co., Ltd., 227-235 Victoria St., Toronto, and • 151 Glen Ave., Ottawa, Ont., Canada.

ALLEN, Charles G. (*A* 1946) Engrg. and Dvlpt., Bryant Heater Co., 17825 St. Clair, Cleveland, and • 1212 Irene, Lynhurst, Ohio.

ALLEN, DeWitt M. (*M* 1936) • Allen & Ralston Co., Room 101, B. M. A. Bldg., 215 Pershing Rd., Kansas City 8, and 39 West 70th Terrace, Kansas City 5, Mo.

ALLEN, Edward C. (*S* 1948) Student, A. & M. College of Texas, • Box 2082 College Station, and 1906 Chestnut St., Houston, Texas.

ALLEN, Frank C. (*M* 1944) Mech. Engr., U. S. Bureau of Reclamation, U. S. Customhouse, Denver, and • 4467 King St., Denver 11, Colo.

ALLEN, George W. (*A* 1945) Steamfitter, Belsmith Air Conditioning & Refrigeration Co., 10 Stewart St., Las Vegas, and • Box 955, Henderson, Nev.

ALLEN, J. Lloyd (*M* 1944) Partner, • Allen & Kelley, Archts., 333 N. Pennsylvania, and 5699 N. Delaware, Indianapolis, Ind.

ALLEN, Michael H. P. (*M* 1946) Dir. and Gen. Mgr., • Bell's Asbestos & Engineering (Africa) Ltd., P. O. Box 4378, and 214 Killarney Ct., Johannesburg, South Africa.

ALLEN, Robert C., Jr. (*A* 1947) Branch Mgr., • General Controls Co., 4055 Broadway, Kansas City 2, and 8005 Spring Lane, Rt. 7, Kansas City, Mo.

ALLEN, Robert F. (*J* 1946) Engr., • Carrier Corp., 710 N. Harwood St., Dallas, Texas, and 83 Willow Ave., Larchmont, N. Y.

ALLEN, Raynold W. (*A* 1947) Mgr., Htg. Dept., • Atlas Supply Co., 236 S. Liberty St., and 422 Avalon Rd., Winston-Salem, N. C.

ALLEN, Roy H. (*A* 1946) Owner, • Allen Copper Coil Mfg. Co., Aqua Heating Co., 400 E. Pine St., Seattle 22, and 615 East 50th St., Seattle, Wash.

ALLEN, S. Rushmore (*M* 1947) Sales Engr., • American Blower Corp., 438 Woodward Bldg., Washington 5, D. C., and 3905 Fifth St. N., Arlington, Va.

ALLEN, William T. (*A* 1947) Supt. of Htg., Dept. of National Defence, Royal Canadian Engrs., Wolseley Barracks, and • 155 Chesley Ave., London, Ont., Canada.

ALLEN, William W. (*A* 1936) Pres., American Coolair Corp., Box 2300, Jacksonville, Fla.

ALLISON, H. H. (*A* 1946) Mech. Engr., • United Rexall Co., 355 S. Broadway, and 1106 Masselin Ave., Los Angeles, Calif.

ALLISON, John H. (*A* 1945) Sales Engr., E. J. Deckman Co., 1502 Oliver Bldg., Pittsburgh 22, and ● 601 Sherwood Rd., Pittsburgh 21, Pa.

ALLISON, Robert E. (*A* 1941) Owner ● American Sheet Metal Co., 601 First Ave., Dallas 10, and 7069 Fairdale, Dallas, Texas.

ALLISON, William F. (*A* 1947) Sr. Engr., E. A. Berman Co., 268 Northampton St., Boston, and ● 348 Webster St., Rockland, Mass.

ALLONIER, Howard R. (*A* 1936) Dist. Mgr., ● J. J. Nesbitt, Inc., 101 N. High St., Columbus 15, and Shawnee Hills, R. D. 1, Powell, Ohio.

ALLSHOUSE, Irvin P. (*A* 1946) 1922 Des Plaines Ave., Des Plaines, Ill.

ALLSOP, Rowland P. (*A* 1940; *J* 1934) Cons. Engr., ● 1221 Bay St., Toronto, Ont., and Stop 21 Kingston Rd., Scarboro Bluffs, Ont., Canada.

ALMERT, Harold (*A* 1944) Cons. Engr., 1605 York Ave., New York, and ● 519 East 86th St., Apt. 6-B, New York 28, N. Y.

ALSCHULER, John H. (*A* 1946) Designer, Parkins & Will, 309 W. Jackson Blvd., Chicago, and ● 1099 Merrill Ave., Hubbard Woods, Ill.

ALT, Harold L.* (*M* 1913) Basic Mech. Design Engr., Voorhees, Walker, Foley & Smith, 101 Park Ave., New York 16, and ● 115-27–225th St., St. Albans 11, N. Y.

ALTEMUELLER, George F. (*A* 1940) Utility Officer, Veterans Administration Hospital, Manhattan Beach, Brooklyn, and ● 2624 East 27th St., Brooklyn 29, N. Y.

ALVAREZ, Joaquin (*A* 1946; *J* 1942) Engr., Export Sales Div., ● Frick Company, Inc., and 118 W. Third St., Waynesboro, Pa

ALYEA, Harold W. (*M* 1944) Design and Dvlpt. Engr., ● Johnson Service Co., 507 E. Michigan St., Milwaukee, and 919 Arcadian Ave., Waukesha, Wis.

AMBROSE, Alfred H. (*J* 1943; *S* 1941) Treas., H. R. Ambrose & Sons, Inc., 46 Pleasent St., and ● 30 Central St., Woodstock, Vt.

AMBROSE, Eugene R. (*M* 1940) Air Cond. Engr., American Gas & Electric Service Corp., 30 Church St., New York 7, N. Y., and ● 412 Walnut St., Roselle Park, N. J.

AMEZAGA, Miguel F. (*M* 1946) Vice-Pres., ● Compania Electric de Cuba, Apartado 2284, and Calle 36 No. 59 Miramar, Havana, Cuba.

AMINOFF, Eugen (*A* 1947) Managing Dir., ● Varme & Sanitetsaktiebolaget Ido, Box 3110, Stockholm 3, and Wartavagen 4, Stockholm, Sweden.

AMMERMAN, A. S., Jr. (*M* 1944; *A* 1941; *J* 1937) Dist. Mgr., ● Aerofin Corp., 111 W. Washington St., Chicago 2, and 132 N. Wolf Rd., Des Plaines, Ill.

AMMERMAN, Charles R. (*Life Member*; *M* 1916) Pres., ● Ammerman, Davis & Stout, Inc., 912-23 K. of P. Bldg., and 4716 Rockwood Ave., Indianapolis, Ind.

AMMONS, Staron E. (*S* 1947) Student. ● Box 4388, College Station, and 212 13th Ave. N., Texas City, Texas.

AMPHLETT, A. L. M. (*A* 1947) Engr., ● Mingledorff's Inc., 735 Broad St., Box 638, and 1012 Carolina Ave., Augusta, Ga.

AMUNDSON, Carl H. (*M* 1944) Branch Mgr., ● Herman Nelson Corp., 759 N. Milwaukee, St., Milwaukee 11, and 609 North 115th St., Wauwatosa, Wis.

ANDEREGG, R. H. (*M* 1920) Vice-Pres. and Chief Engr., The Trane Co., and ● 450 Losey Ct., La Crosse, Wis.

ANDERSON, Carl G. (*M* 1942) Asst. Chief Engr., Union Special Machine Co., 400 N. Franklin St., Chicago, and ● 171 Perry St., Elgin, Ill.

ANDERSON, Carl O. (*M* 1944) Htg. and Vent. Engr., Board of Education, Room 536–228 N. LaSalle St., Chicago 1, and ● 900 N. Rush St., Chicago 11, Ill.

ANDERSON, Carroll S. (*M* 1920) Dist. Mgr. ● American Blower Corp., 1105 Architects Bldg., Los Angeles 13, and 4267 Holly Knoll Dr., Hollywood 27, Calif.

ANDERSON, David B. (*A* 1939; *J* 1936; *S* 1933) Wood Conversion Co., First National Bank Bldg., and ● 1999 Pinehurst Ave., St. Paul 5, Minn.

ANDERSON, Edward R. (*J* 1946) Appl. Engr., ● Westinghouse Electric Corp., Sturtevant Div., 1408 Walnut St., Des Moines 8, Ia., and 1932 N. Moreland Ave., Indianapolis 8, Ind.

ANDERSON, Edwin C. (*A* 1944) Owner, ● Edwin C. Anderson Co., 1863 Wazee St., Denver 2, and 1623 Adams St., Denver 6, Colo.

ANDERSON, Edwin J. (*A* 1939) Mfrs. Agent, ● Chicago Pump Co., 14 Smith St., Detroit 2, and 274 Lenox, Detroit 15, Mich.

ANDERSON, Edwin L. (*M* 1941) Chief Engr., Sun Chemical Corp., 100 Sixth Ave., New York 13, N. Y., and ● 63 Oakridge Rd., Verona, N. J.

ANDERSON, Einar (*A* 1940) Gen. Sales Mgr., Vulcan Iron & Engineering Ltd., Sutherland and Maple St., and ● 152 Bannerman Ave., Winnipeg, Man., Canada.

ANDERSON, Erik A. (*A* 1947) Asst. Dist Engr., Westinghouse Electric Corp., Sturtevant Div., 901 Walton Bldg., Atlanta, and ● 1121 Winburn Dr., East Point, Ga.

ANDERSON, George A. (*A* 1946) Chief Engr., William Adams Engineers, 3911 North Ave., Chicago 47, and ● 3030 Sheffield Ave., Chicago 14, Ill.

ANDERSON, George A. M. (*M* 1947; *A* 1939; *J* 1933) Pres., ● King Ventilating Co., and 717 S. Cedar, Owatonna, Minn.

ANDERSON, George E. (*S* 1946) Student, University of Minnesota, and ● 36 Melbourne Ave. S.E., Minneapolis 14, Minn.

ANDERSON, Granville W. (*A* 1943) Service Engr. ● Koppers Coal Division, 1217 Ford Bldg., Detroit 26, and 5096 Burns Ave., Detroit 13, Mich.

ANDERSON, Harvey E. (*A* 1944) Partner, ● Anderson & Litwack Co., Ventilating Contractors, 514-516 S. Laflin St., Chicago 7, and 460 Fair Ave., Elmhurst, Ill.

ANDERSON, James T. (*J* 1947) Instructor, ● Michigan State College, Engineering Division, and Bldg. 706, Cherry Lane, Apt. 108, East Lansing, Mich.

ANDERSON, N. B. (*A* 1945) Mgr., ● Lamar Supply Co., 3100 Lamar Ave., Houston, and 2910 Chartres, Houston 4, Texas.

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ANDERSON, Robert B. (*A* 1944) Owner, R. B. Anderson Heating Contr. & Engr., 1377 W. Alameda, Denver, Colo.

ANDERSON, Robert V. (*A* 1945) Div. Sales Mgr., Lennox Furnace Co., Inc., 400 N. Midler Ave., Syracuse, N. Y., and ● 306 N. Confederate Ave., Sandston, Va.

ANDERSON, Sydney, Jr. (*A* 1943) Dir., Natl. Acct. Sales, ● Chrysler Corp., Airtemp Div., Dayton, Ohio, and 8503 Irvington Ave., Bethesda, Md.

ANDERSON, William S., Jr. (*M* 1945) Partner, Axeman-Anderson Assocs., 233 West St., and ● 1332 Sheridan St., Williamsport, Pa.

ANDERSON, William T., Jr. (*M* 1946) Dir. of Research, ● Hanovia Chemical & Manufacturing Co., Chestnut St. and N. J. R. R. Ave., Newark 5, and 19 Bowdoin St., Maplewood, N. J.

ANDREAS, Charles A. (*A* 1946) Asst. Chief Mech. Engr., ● U. S. Army Air Force Proving Ground, Climatic Hangar, Eglin Field, and Valparaiso, Fla.

ANDREW, Gordon J. (*J* 1947) Htg. & Indus. Engr., W. T. Andrew Co., 15815 Hamilton Ave., Detroit 3, and ● 9959 Sussex Ave., Detroit 27, Mich.

ANDREWS, William G. (*A* 1941) Pres. & Gen. Mgr., ● Southern Refrigeration Corp., 1750 S. Jefferson St., P. O. Box 1095, and 2215 S. Jefferson St., Roanoke, Va.

ANDREWS, William R. (*M* 1942) Asst. Mgr., ● Ross Engineering of Canada, Ltd., 425 River St., Sect. "A" Verdun, Montreal 19, and 3770 Cote St. Catherine Rd., Montreal, Que., Canada.

ANDREWS, W. M. (*M* 1941) Partner, ● Lockwood & Andrews, Cons. Engrs., 904 Union National Bank Bldg., and 2333 Sunset, Houston, Texas.

ANGELL, Lawrence D. (*M* 1944) Minneapolis-Honeywell Regulator Co., New York, and ● 450 East 16th St., Brooklyn, N. Y.

ANGELO, Herbert G. (*A* 1944) Htg. and Vent., 4805 Washington, Denver 16, and ● 1225 East 14th Ave., Apt. 28, Denver, Colo.

ANGERMEYER, Albert H. (*A* 1936) Owner, ● Plumbing & Heating, 119 N. Commercial St., and 245 Webster St., Neenah, Wis.

ANGLIN, T. G. (*A* 1947) Cons. Engr., ● T. G. Anglin Engineering Co., Ltd., Room 703 Dominion Square Bldg., Montreal, and 540 Prince Albert, Montreal 6, Que., Canada.

ANGUS, Donald L. (*J* 1946) Engr., H. H. Angus, Cons. Engr., 1221 Bay St., and ● 102 St. Hubert Ave., Toronto, Ont., Canada.

ANGUS, Frank M. (*M* 1937) Owner, Texas Refrigeration & Engineering Co., 4030 Swiss Ave., Dallas 4, and ● 5134 Ridgedale, Dallas, Texas.

ANGUS, Harry H.* (*M* 1918), (Council, 1927-29), Consulting Engr., 1221 Bay St., and ● 34 Farnham Ave., Toronto, Ont., Canada.

ANIK, Bernard (*S* 1946) Student, Mech. Engrg. Dept., ● Purdue University, West Lafayette, Ind., and 3464 Knox Pl., New York, N. Y.

ANNABEL, Cecil H. (*A* 1946) Owner, ● Belsmith Co., P. O. Box 1568, and 10 Stewart St., Las Vegas, Nev.

ANOFF, S. M. (*J* 1940) Dept. Mgr., Albert Pick Co., Inc., 2159 Pershing Rd., and ● 5048 Marine Dr., Apt. A-5, Chicago 40, Ill.

ANSPACHER, T. H. (*M* 1939; *J* 1936) Dist. Mgr., ● Buffalo Forge Co., Tower Petroleum Bldg., Dallas 1, and 4512 Arcady St., Dallas, Texas.

ANTHES, Lawrence L. (*A* 1935) Pres., ● Anthes-Imperial Ltd., 30 Jefferson Ave., and 119 Dowling Ave., Toronto, Ont., Canada.

ANTHONY, William R. (*J* 1948) Partner, ● Anthony Co., 2220-19th St., and 2501-32nd St., Lubbock, Texas.

ANWAY, H. Wilbur (*M* 1943) Research Physicist, ● Wood Conversion Co., Arch St., and 1012 Prospect Ave., Cloquet, Minn.

APPELT, Joseph E. (*M* 1945) Mgr., The Trane Co., 1200 Godfrey S.W., Grand Rapids, and ● Green Ridge Dr., R. R. 1, Comstock Park, Mich.

APT, Sanford R. (*M* 1935) Mech. Engr., Parsons, Brinckerhoff, Hogan & Macdonald, 142 Maiden Lane, New York 7, and ● 36-39–205th St., Bayside, L. I., N. Y.

ARANDA, Arturo (*A* 1946) Engr., ● Dept. de Hidraulica-Morande, Institute of Inter-American Affairs, Casilla 9182, and Rosas 3114-F, Santiago, Chile.

ARAR, Raymond M. (*S* 1948) Student, University of Michigan, and ● 714 East University St., Ann Arbor, Mich.

ARCHAMBAULT, Joseph A. (*A* 1939) Mgr., Sales Office, ● C. A. Dunham Co., Ltd., Room 201-3, 6 Wellington N., and 55A Council St., Sherbrooke, Que., Canada.

ARCHER, David M. (*M* 1934) Sales Repr., ● Sarco Co., Inc., 143 Federal St., Boston 10, and 10 Harding Ave., Braintree, Mass.

ARCHER, William J. (*M* 1945) 175–19th Ave., San Francisco 21, Calif.

ARENBERG, Milton K. (*A* 1920) Pres., Robert Barclay, Inc., 122 N. Peoria St., Chicago, and ● 1415 Wildwood Lane, Highland Park, Ill.

ARGUE, Edgar J. (*A* 1935) Sales Engr., Anthes Foundry, Ltd., Saskatchewan Ave., and ● 773 McMillan Ave., Winnipeg, Man., Canada.

ARMBRUSTER, Frank T. W. (*M* 1936) Service Engr., American Radiator & Standard Sanitary Corp., 73 E. Naghten St., Columbus, and ● 105 First Ave., Waverly, Ohio.

ARMISTEAD, William C. (*M* 1937) Sales Engr., ● 153 Second Ave. N., Nashville 3, and Granny White Pike, Brentwood, Tenn.

ARMISTEAD, William C., Jr. (*S* 1947) Student, Vanderbilt University and ● 153 Second Ave. N., Nashville, Tenn.

ARMSPACH, Otto W. (*M* 1919) Dist. Chief Engr., Carrier Corp., 405 Lexington Ave., New York 17, and ● N. 2, Stratford Rd., Scarsdale, N. Y.

ARMSTRONG, Charles E. (*M* 1939) Regis. Mech. Engr., 624 N.E. Hazelfern Pl., Portland 13, Ore.

ARMSTRONG, Roy E. (*A* 1947) Bldg. Chief Engr., ● Humble Oil & Rerfrig. Co., Room 105 Humble Bldg., Houston, and 2912 Austin St., Houston 4, Texas.

ARNDT, Heinrich W. (*A* 1944) Owner, ● The Hobby Shop, Masonic Building Lobby No. 2, and 2007 Central Ave., Augusta, Ga.

ARNDT, Marquard H. (*M* 1947) Chief, Data & Control Branch, Atomic Energy Commission and ● 1434 Johnston Ave., Richland, Wash.

ARNOLD, C. J. (*A* 1946) Engr., Mental Deficiency Colony, and ● 3 Hensol Villas, Nr. Pontyclun, Glamorgan, South Wales, Great Britain.

ARNOLD, Jonah S. (*J* 1947) Designer ● Stuart-Aire Inc., 413 Greenwich St., New York, and 47 Harrison Ave., Brooklyn 11, N. Y.

ARNOLD, Richard S. (*M* 1944) Dist. Chief Engr., ● Carrier Corp., 300 Ivy St. N.E., Atlanta 3, and 2195 E. Lake Rd., Atlanta, Ga.

ARNOLD, Robert S. L. (*M* 1944; *A* 1920; *J* 1922) Owner, Robert Arnold Co., 602 Otis Bldg., Philadelphia 2, and ● Sherwood Lane, Wallingford, Pa.

ARNOLD, Thomas L. (*A* 1945) Mgr., ● Vulcan Radiator Co., 26 Francis Ave., Hartford 6, and 59 Beverly Rd., West Hartford 7, Conn.

ARONOFF, Melvin S. (*J* 1947) Design Engr., ● Herman Blum, Cons. Engr., 2812 Fairmount St., and 2926 Park Row, Dallas, Texas.

ARONSON, Henry H. (*A* 1939) Sales Engr., Dole Valve Co., Chicago, and ● Warrenville, Ill.

ARROWSMITH, John O. (*M* 1934) Supt. of Works, ● Canadian Kodak Co., Ltd., and 9 Humberview Rd., Toronto 9, Ont., Canada.

ARTHUR, John M., Jr. (*M* 1923) Div. Mgr., ● Kansas City Power & Light Co., 1330 Baltimore Ave., Kansas City 10, Mo., and 3311 State Ave., Kansas City, Kans.

ARTRAN, Carlyle (*A* 1945) Pres., ● Industrial Air Conditioning Corp., 3030 Fierro St., Los Angeles 41, and 2334 Birkdale St., Los Angeles 31, Calif.

ARVIDSON, Ernest R. (*M* 1943) Electrical Engrg. Draftsman, Carbide and Carbon Chemicals Corp., South Charleston, and ● 2820 Kanawha Terrace, St. Albans, W. Va.

ARZET, Fred A. (*A* 1944) Sales Engr., U. S. Radiator Corp., 309 East 19th St., Indianapolis, and ● 3704 N. Emerson Ave., Indianapolis 1, Ind.

ASBURY, Edgar M. (*A* 1946) Sales Engr., ● Armstrong Cork Co., 841 Electric Bldg., Houston, Texas.

ASH, Norman B. (*A* 1945) Pres., Braniff Engineering Co., 2908 Northwest 12th St., Oklahoma City, Okla.

ASH, Robert S. (*A* 1943; *J* 1940) Buyer, Montgomery Ward & Co., 29th Ave., & East 14th St., Oakland, and ● 8080 Earl St., Oakland 5, Calif.

ASHCRAFT, J. P. (*A* 1943) Owner, J. P. Ashcraft Co., and ● 2826 Fondren Dr., Dallas 5, Texas.

ASHLEY, Carlyle M.* (*M* 1931), (Council, 1943-46), Chief Dvlpt. Engr., ● Carrier Corp., 300 S. Geddes St., Syracuse 1, and 22 Lynacres Blvd., Fayetteville, N. Y.

ASHLEY, Edward E. (*M* 1912) Cons. Engr., Partner, Edward E. Ashley, Cons. Engr., ● 10 East 40th St., New York 16, N. Y., and 193 Middlesex Rd., Noroton Heights, Conn.

ASHLEY, Ronald D. (*M* 1944) Partner, ● United Equipment Co., 337 S. High St., Columbus 15, and 141 S. Southampton Ave., Columbus 4, Ohio.

ASHTON, Jed L. (*A* 1944) Owner, Ashton Heating & Air Conditioning, 163 Motor Ave., Salt Lake City 1, and ● 2686 Alden St., Salt Lake City 5, Utah.

ASKER, Gunnar C. F. (*A* 1948) Chief Engr., ● Dry Air Products Corp., 726 Jackson Pl. N.W., and 4530 Lowell St. N.W., Washington, D. C.

ATHERTON, Alfred E. (*A* 1937) Dir., ● A. E. Atherton & Sons, Pty., Ltd., 383 Latrobe St., Melbourne, and 129 Esplanade, Elwood, Vic., Australia.

ATHERTON, Russell C. (*M* 1945) Mech. Engr., M. J. Daly & Sons, Inc., 541 Bank St., Waterbury, and ● 74 Essex Ave., Waterbury 49, Conn.

ATKINS, George E. (*M* 1941) Cons. Engr., 1308 Hobart Bldg., San Francisco, and ● 64 Oak Ridge Rd., Berkeley, Calif.

ATKINS, Oren H. (*A* 1946) Designing Engr., United Electric Co., Louisville Ave., Monroe, and ● 302 Filhoil Ave., West Monroe, La.

ATKINS, Thomas J. (*M* 1945) Electrostatic Air Cleaning Engr., Westinghouse Electric Corp., Philadelphia, and ● 276 Henley Rd., Philadelphia 31, Pa.

ATKINSON, Robert P. (*S* 1948) Grad. Student, University of Minnesota, Minneapolis 14, and ● 4518 Upton Ave. N., Minneapolis 12, Minn.

ATKINSON, Russell R. (*A* 1946) Plbg. and Htg. Dept., Central Supply Co., 838 S.W. First St., Portland, and • 1631 S.W. Yamhill St., Portland 5, Ore.

ATKINSON, William J. (*A* 1946) Dept. Mgr., • Winnipeg Supply & Fuel Co., Ltd., 812 Boyd Bldg., and 758 Clifton St., Winnipeg, Man., Canada.

ATLAS, Sidney F. (*J* 1946) Owner, • Atlas Air Conditioning Co., 2915 Rusk Ave., Houston, Texas.

ATTEBERRY, Clark (*M* 1947) Owner & Mgr., Atteberry's Heating & Sheet Metal Works, P. O. Box 453, Mercedes, Texas.

ATWATER, Harry A. (*M* 1945) Chief Engr., Combustion Equipment Co., 1820 Cherry St., Kansas City 8, and • 641 West 67th St., Kansas City 5, Mo.

AUERBACH, Leonard F. (*A* 1947) Dir. of Sales, • Temperature Equipment Corp., 4505 Euclid Ave., Cleveland, and 1844 Forest Hills Blvd., East Cleveland 12, Ohio.

AUGUSTERFER, Raymond J. (*M* 1948) Treas., Ambrose-Augusterfer Corp., 247 E. Ashmead St., Philadelphia 44, Pa.

AUSLANDER, George (*M* 1946) Pres., • National Combustion Co., Inc., 101 Park Ave., New York 17, and Harbor Rd., Hewlett Harbor, L. I., N. Y.

AUSTIN, William H. (*A* 1943; *J* 1940; *S* 1937) Engr., Cox Engineering Co., 621-7 Putnam Ave., Cambridge 39, and • 1095 Hyde Park Ave., Hyde Park 36, Mass.

AVERA, A. F. (*M* 1944) Chief Engr., • Dallas Air Conditioning Co., 2809 Canton St., and 5810 Lewis, Dallas, Texas.

AVERA, William W. (*J* 1946) Engr., • The Bahnson Co., 1001 S. Marshall St., and Room 431, Y.M.C.A., Winston-Salem, N. C.

AVERY, Edward G. (*M* 1947) Sales Engr., • Sarco Co. Inc., 53 W. Jackson Blvd., Chicago 4, and 10535 S. Hale Ave., Chicago 43, Ill.

AVERY, Lester T. (*M* 1934), (Council, 1944-46), Pres., • Avery Engineering Co., 1906 Euclid Ave., Cleveland 15, and 21149 Colby Rd., Shaker Heights, Cleveland 22, Ohio.

AVILES, Alonso (*A* 1946) Owner, • P. O. Box 874, and 115 Wayside Dr., Nogales, Ariz.

AXEMAN, James E. (*M* 1932; *A* 1931; *J* 1925) • Axeman-Anderson Assocs., 233 West St., Williamsport 3, and 1328 Woodmont Ave., Williamsport, Pa.

AXTHELM, Fred G. (*A* 1945) Sales Engr., Front Rank Furnace Co., 2500 Ohio Ave., St. Louis 4, and • 648 N. Forest Ave., Webster Groves 19, Mo.

AYRES, James M.* (*S* 1946) Student, University of California, Berkeley, and • 2411 Bowditch Ave., Berkeley 4, Calif.

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B

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BABCOCK, Paul R. (*M* 1941) Cons. Engr., G. M. Simonson, 625 Market St., San Francisco, and • 328-24th St., Oakland 12, Calif.

BACHMANN, Arthur J. (*A* 1948; *J* 1940; *S* 1939) Service Mechanic, Minneapolis-Honeywell Regulator Co., 221 Fourth Ave., New York, and • 129 Brooklyn Ave., Westbury, L. I., N. Y.

BACHMANN, William L. (*M* 1947) Engr., • Tucker & Rice, Inc., 11 Garden St., Worcester, and Main St., East Brookfield, Mass.

BACKSTROM, Russell E.* (*A* 1931; *J* 1928) Mgr., Indus. Dept., • Wood Conversion Co., First National Bank Bldg., St. Paul 1, and 1655 Hillcrest Ave., St. Paul 5, Minn.

BACON, Earl (*A* 1946) Mgr., M. F. Fischer & Son, 203 Fredericksburg Rd., and • 1802 Clower St., San Antonio, Texas.

BACON, William H., Jr. (*A* 1942) Automotive Engr., Tide Water Associated Oil Co., East 22nd St., Bayonne, and • 217 Baker Ave., Westfield, N. J.

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BADHNI, J. (*M* 1946) Prop., Badhni, Engineering & Trading Co., 38 Avenue Ferdowsi, Teheran, Iran.

BAECHLIN, Alfred C., Jr. (*M* 1942) Gen. Sales Mgr., Northern Air Conditioning Corp., 21 Central Ave., Newark, N. J., and • 2033 North 40th St., Rt. 10, Box 716 M, Phoenix, Ariz.

BAGGALEY, Walter (*M* 1938) Advisory Equip. Engr., Research Div., • The Austin Co., 16112 Euclid Ave., Cleveland 12, and 3390 Glencairn Rd., Shaker Heights 22, Ohio.

BAGHI, A. R. Mir (*A* 1946) Service Engr., Anglo Iranian Oil Co., 115 Bawarda N., Abadan, Iran.

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BAILEY, Charles F. (*A* 1947; *J* 1939) Gen. Mgr., • Lorenzo Bailey & Co., and Windsor, Va.

BAILEY, Frank T. (*A* 1947) Vice-Pres. & Gen. Mgr., • Register & Grille Manufacturing Co., Inc., 70 Berry St., Brooklyn 11, N. Y., and 16 Cambridge Rd., Verona, N. J.

BAILEY, Frederick A., Jr. (*A* 1939) Prop., • Bailey's, 130 King St., Charleston 5, and 70 Warren St., Charleston, S. C.

BAILEY, Fred N. (*M* 1947) Industrial Engr., Harris Pump & Supply Co., and • 902 Agnew Rd., Pittsburgh 27, Pa.

BAILEY, George G. (*A* 1947) Htg. & Vent. Engr., Boynton Cole, 1873 Piedmont Rd., and • 3041 W. Roxboro Rd., Atlanta, Ga.

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BAILEY, Murray G. (*A* 1946) Sales, • C. A. Dunham Co., Ltd., 1139 Bay St., and 598 Sherbourne St., Toronto, Ont., Canada.

BAIN, Lawrence F. (*A* 1944) Constr. Supt., Narowetz Heating & Ventilating Co., 1722 W. Washington Blvd., and • 3324 N. Laramie Ave., Chicago, Ill.

BAIRD, Alexander D. G. (*A* 1944) Pres., • A. G. Baird, Ltd., 25 Ritchie Ave., Toronto, and Linden Rd., Scarborough Bluff, P. O. Scarborough, Ont., Canada.

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BAK, Stanley J. (*J* 1947) Sales Engr., The Crosbie Co., 2039 K St. N.W., Washington, and • 2410-20th St. N.W., Washington 9, D. C.

BAKER, Clyde H. (*M* 1945) Htg., Vent. and Plbg. Engr., Snyder & McLean, 2214 Penobscot Bldg., Detroit, and • 15444 Vaughan St., Detroit 23, Mich.

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BAKER, Edward L. (*A* 1945) Mgr., • Burbidge Coal Co., 311 S. Main St., Salt Lake City 1, and 1533 Glen Arbor, Salt Lake City 5, Utah.

BAKER, Harland E. (*A* 1946; *J* 1945) Partner, Baker & English, 1360 W. Ninth St., and • 3786 Freemont Rd., South Euclid 21, Ohio.

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BAKER, I. C. (*M* 1921) Vice-Pres., • Chrysler Corp., Airtemp Div., 1119 Leo St., Dayton 1, and 252 E. Monteray Ave., Dayton 9, Ohio.

BAKER, James (*M* 1944) Owner, • Ross & Greig Registered, 738 Notre Dame St. W., and 5715 Darlington Ave., Montreal, Que., Canada.

BAKER, John G. (*M* 1947) Chief Engr., Viking Manufacturing Corp., 1747 Chester Ave., and • 1279 West 102nd St., Cleveland, Ohio.

BAKER, John T. (*A* 1948) Htg.-Vtg. Engr., Magney, Tusler & Setter, 202 Foshay Tower, Minneapolis, and • 2612 Dupont Ave. S., Minneapolis 8, Minn.

BAKER, L. P. (*A* 1945) Engr., Kendall Baker & Co. Ltd., 365 Yonge St., Toronto, Ont., Canada.

BAKER, Merl (*S* 1946) Instructional Staff & Student, • Purdue University, Mech. Engrg. Bldg., West Lafayette, Ind., and Butler Rd., Hopkinsville, Ky.

BAKER, Roland H. (*M* 1928; *A* 1924) Pres., R. H. Baker Co., and • Elkins, N. H.

BAKER, Russell A. (*A* 1946) Branch Mgr., • Minneapolis-Honeywell Regulator Co., 121 W. Onondaga St., and 310 Carlton Rd., Syracuse, N. Y.

BAKER, T. A. (*M* 1942) Vice-Pres., • Baker Specialty & Supply Co., 701 Erie Ave., and 2205 E. Broadway, Logansport, Ind.

BAKER, Thomas (*M* 1938) Vice-Pres., Chief Engr., Herbert Keller Corp. 179 Ellison St., Paterson, N. J., and • 660 East 242nd St., New York, N. Y.

BAKER, William H., Jr. (*A* 1935) Asst. Mgr., Pittsburgh Sales Office, American Radiator & Standard Sanitary Corp., 102 Sixth St., Pittsburgh, Pa.

BAKKO, Reuben (*A* 1944) Air Conditioning Co. of So. Calif., 1003 Santa Fe Ave., Los Angeles 21, and • 212 W. Avenue 42, Los Angeles 31, Calif.

BAKSA, Stephen (*A* 1947) Plant Engr., • Johnson & Johnson, Walnut Ave., Cranford, and 28 Pulaski Ave., Carteret, N. J.

BALCH, Robert M., Jr. (*A* 1944) Sales Mgr., Apartment Controls Div., • Minneapolis-Honeywell Regulator Co., and 402 W. Minnehaha Pkwy., Minneapolis, Minn.

BALDWIN, C. W. (*M* 1947; *A* 1945) Vent. Engr., • U. S. Rubber Co., 1230 Avenue of the Americas, New York 20, and Clay, N. Y.

BALDWIN, Karl F., Jr. (*M* 1947; *A* 1941; *J* 1938) Mech. Engr., Clyde E. Bentley, 1441 Franklin St., Oakland, and • 419 Kentucky Ave., Berkeley 7, Calif.

BALDWIN, Ralph T. (*A* 1948) Treas., • E. C. Powers & Son, Inc., 135 Arch St., and 5936 Lansdowne Ave., Philadelphia, Pa.

BALL, F. T. (*A* 1940) • The Canadian Fairbanks-Morse Co., Ltd., 10255–104th St., and 11034–126th St., Edmonton, Alta., Canada.

BALL, William (*A* 1936) Pres., • Interstate Heating & Plumbing Co., 521 Southwest Blvd., Kansas City, Mo., and 1026 Shawnee Rd., Kansas City, Kans.

BALLAGH, A. Bruce (*A* 1946; *J* 1943) Sales Engr., • B. F. Sturtevant Co. of Canada, Ltd., 19 Melinda St., and 2405 Queen St. E., Toronto, Ont., Canada,.

BALLANTYNE, George L. (*A* 1936) Mgr., Htg. Dept., • Crane, Ltd., 1170 Beaver Hall Sq., Montreal, and 140 Ballantyne Ave. S., Montreal West, Que., Canada.

BALLMAN, William H. (*M* 1937) Prod. Mgr., • Holly Hill Fruit Products, Inc., Davenport, and 510 Revere St., Orlando, Fla.

BALSAM, Charles P. (*M* 1932) Gen. Mgr., • National Home Equipment Co., 50 Church St., New York 7, and 324 Fourth St., Brooklyn, N. Y.

BALSTER, Joseph A. (*A* 1947) Chief Engr., Cafritz Co., 1404 K Street N.W., and • 5520 Sherrier Pl. N.W., Washington, D. C.

BAMOND, Manuel J. (*M* 1942) Branch Office Mgr., • Temperature Control Equipment, 403 N. Desplaines St., Chicago 10, and 5859 Winthrop Ave., Chicago 40, Ill.

BANACH, Casimer J. (*A* 1946; *J* 1939) Engr., Chicago Fan & Fin Coil Co., 1937 W. Walnut St., Chicago 12, and • 819 N. Mozart Ave., Chicago 22, Ill.

BAND, Jack P. (*A* 1944) Mech. Engr., Giffels & Vallet, Inc., 1000 Marquette Bldg., Detroit 26, and • P. O. Box 2032, Detroit 31, Mich.

BANKS, John B. (*A* 1942) Branch Mgr., • Minneapolis-Honeywell Regulator Co., 122 N.E. Broadway, Portland 12, and 4615 Northeast 40th Ave., Portland 11, Ore.

BANKSTON, Clayton V. (*A* 1945) Dist. Sales Mgr., • Industries Sales Corp., 2927 Jackson Ave., and 29 San Jose Ave., New Orleans, La.

BANOWSKY, A. B. (*M* 1938) Mgr., Retail Div., Payne Furnace Co., P. O. Box 990, Beverly Hills, and • 2652 Glendon Ave., Los Angeles 34, Calif.

BAPPLER, Charles T. (*A* 1948) Regional Sales Mgr., McQuay, Inc., 122 East 42nd St., New York, and • 91-17 48th Ave., Elmhurst, N. Y.

BARBECK, Chester A. (*A* 1947) Sales Engr., • Matthews Engineering Co., 2122 Olive St., and 4616 Bowser Ave., Dallas, Texas.

BARBECK, William R. (*M* 1947) Partner, • Rodgers-Barbeck Co., 2021 Cedar Springs, and 3301 Greenbrier Dr., Dallas, Texas.

BARBER, Richard C. (*J* 1945) U. S. Naval Gun Factory, Washington, D. C., and • 4100 33rd St., Mt. Rainier, Md.

BARBIERI, Patrick J. (*A* 1943; *J* 1936; *S* 1933) Air Cond. Engr., • Armo Cooling & Ventilating Co., Inc., 30 West 15th St., New York, and 2237 Belmont Ave., Bronx, N. Y.

BARD, William S. (*M* 1946) General Mgr., F. D. Ramsey & Co., Inc., 504 Washington St., and • 1315 Michigan Ave., La Porte, Ind.

BARDO, Frederick J., Jr. (*A* 1947) Designer, Beman & Candee, Cons. Engr., Buffalo, and • 364 Walton Dr., Snyder 21, N. Y.

BAREITHER, Harlan D. (*S* 1947) Grad. Student, University of Illinois, and • 608 South Race, Urbana, Ill.

BARFUS, Louis (*M* 1946) Vice-Pres., • Sarcotherm Controls, Inc., 280 Madison Ave., New York 16, and 2775 East 16th St., Brooklyn, N. Y.

BARKER, M. Stanley (*A* 1943) Chief Engr., Carrier Engineering, Ltd., 30 Bloor St. W., and • 686 Eglington Ave. E., Toronto, Ont., Canada.

BARKLEY, Kenneth L. (*M* 1946) Designing Draftsman, • Ecusta Paper Corp., Box 200, Spindale, and 7 W. Jordan St., Brevard, N. C.

BARLOW, F. John (*A* 1945; *J* 1943) Chief Prod. Engr., Western Condensing Co., 935 E. John St., Appleton, Wis.

BARMANN, Paul V. (*M* 1946) Pres., • Lydick-Barmann Co., 505 Commerce St., and 1134 Clara St., Fort Worth, Texas.

BARNARD, M. Everett (*A* 1936) Dist. Mgr., Indus. Htg. Dept., • Carrier Corp., 12 South 12th St., Philadelphia 7, and 6730 Crittenden St., Philadelphia 19, Pa.

BARNARD, William B. (*S* 1948) Student, Purdue University, and • 712 Northwestern, West Lafayette, Ind.

BARNES, Arthur F. (*M* 1938) Owner & Mgr., Texas Engineering Co., 4607 Montrose, Houston 6, and • 3015 Jarrard St., Houston 5, Texas.

BARNES, Arthur R. (*M* 1937) Engr., • U. S. Supply Co., 1315 West 12th St., and 326 East 70th Terrace, Kansas City, Mo.

BARNES, Charles A. (*M* 1944) Engr., Metal Fabricators, 465 Bishop St. N.W., • P. O. Box 4304, Atlanta 2, and 947 Katherwood Dr. S.W. Atlanta, Ga.

BARNES, Hugh S. (*A* 1947; *J* 1940) Metal Fabricators, Inc., P. O. Box 3232, Charlotte 3, N. C.

BARNES, John C. (*A* 1944) Branch Mgr., • National Radiator Co., 401 N. Broad St., Philadelphia 8, and 143 Golf View Rd., Merion Golf Manor, Ardmore, Pa.

BARNES, John G., Jr. (*M* 1947) Engr., • Natkin & Co., 1924 Oak St., and 404 Huntington Rd., Kansas City 2, Mo.

BARNES, Lewis L. (*M* 1943; *A* 1942; *J* 1937) Chief Engr., Carrier Atlanta Corp., 306 Peachtree St., and • 3865 Wieuca Terrace, Atlanta, Ga.

BARNES, Raymond W. (*M* 1939) Cons. Engr., 631 Moore Bldg., San Antonio 5, and • 1208 N. Main Ave., San Antonio 2, Texas.

BARNES, Walter E. (*M* 1933) Pres., Barnes & Jones, Inc., 128 Brookside Ave., Jamaica Plain 30, Boston, and • 7 Woodlawn Ave., Wellesley Hills 82, Mass.

BARNES, Willis L. (*A* 1946) Sales Engr., • The H. L. Thompson Co., 414 Esperson Bldg., Houston 2, and 410 Marshall St., Houston, Texas.

BARNETT, Harry (*M* 1942) Dist. Mgr., • Zephyr Laundry Machinery Co., Box 1125, and Briarcliff Hotel, Atlanta, Ga.

BARNETT, Robert E. (*A* 1944) Structural Engr., Toltz King & Day, and • Grand Hotel, St. Paul, Minn.

BARNEY, William E. (*M* 1936) Mgr., Engr., • Hydraulic-Press Brick Co., South Park, and 7606 Hemlock Rd., Independence, Ohio.

BARNUM, Willis E., Jr. (*M* 1933; *J* 1930) Sales Engr., • Westerlin & Campbell Co., 5924 Second, Detroit 2, and 17106 Magnolia Pkwy., Detroit 19, Mich.

BARON, Arnold E. (*S* 1947) Student, Texas A. & M. College, College Station, and ●4500 Belclaire, Dallas, Texas.

BARR, George W. (*Life Member*), (*M* 1905), (Board of Governors, 1910), Dist. Mgr., ●Aerofin Corp., 2030 Land Title Bldg., Philadelphia 10, and Woods End, Villa Nova, Pa.

BARRETT, Campbell M. (*A* 1941) Mech. Inspector of Mines, Province of Ontario, Parliament Bldgs., Toronto, and ●93 Ramsey Rd., Leaside, Ont., Canada.

BARRY, James, Jr. (*M* 1946) Vice-Pres., Elliott & Barry Engineering Co., 4060 W. Pine Blvd., St. Louis 8, Mo.

BARRY, Wilfred W. (*A* 1945) Partner, ●Barry & Kemper, 12873 Fort Rd., and 10132–142nd St., Edmonton, Alta., Canada.

BARSHA, Nicholas B. (*A* 1947) Chief Engr., Airtherm Manufacturing Co., 700 S. Spring Ave., St. Louis 10, and ●207 Newell Dr., Ferguson, Mo.

BARTELS, Charles J. (*M* 1942) Owner, ●Automatic Stoker & Engineering Co., 207-8 Richardson Bldg., and 1416 Washington Ave., Parkersburg, W. Va.

BARTELS, Everett M. (*M* 1946; *A* 1941; *J* 1939) Supvsr. of Mech. Equip., ●Independent School District, 629 Third St., Des Moines 9, and 1104 E. Douglas, Des Moines 16, Iowa.

BARTH, Herbert E. (*M* 1920) Vice-Pres., ●American Blower Corp., P. O. Box 58, Roosevelt Park Annex, Detroit 32, and 15 East Kirby Ave., Detroit 2, Mich.

BARTH, John W. (*A* 1943; *J* 1939) 326 Olive Ave., Long Beach 12, Calif.

BARTHELMESS, Richard (*M* 1944) Mgr., ●Richard Barthelmess Sales Co., 1054 W. Adams St., Jacksonville 4, and 1711 Challen Ave., Jacksonville 5, Fla.

BARTLETT, Amos C.* (*M* 1940) Mgr., Htg. and Vent. Section, ●Westinghouse Electric Corp., Sturtevant Div., Hyde Park, and 22 Weston Ave., Braintree 84, Mass.

BARTLETT, C. Edwin (*M* 1922) Pres., ●Bartlett & Co., Inc., 201 South 42nd St., Philadelphia 4, and 3111 W. Coulter St., Philadelphia 26, Pa.

BARTLETT, George M. (*A* 1947) Mgr. of Heating Dept. & Sales Engr., W.E. Wesson, 100 Eagle St., Waterbury, and ●28 Wilmot Rd., Hamden, Conn.

BARTON, Fred C. (*M* 1943) Partner, ●Shuttleworth Conditioned Air, 117 E. Michigan St., and 1950 N. Olney St., Indianapolis, Ind.

BARTON, Jay (*M* 1937) Partner, Barton Engineering Co., 416 Stephenson Bldg., Detroit, Mich., and ●808 Holgate Ave., Defiance, Ohio.

BARTON, Kenneth L. (*M* 1945) Indus. Engr., ●The Foxboro Co., 420 Lexington Ave., Room 1643, New York 17, and 103 Ramsey Ave., Yonkers 2, N. Y.

BASSEVITCH, Abraham (*A* 1945) Design Engr., Meyer, Strong & Jones, 101 Park Ave., New York, and ●3002 West 28th St., Brooklyn 24, N. Y.

BASTEDO, Albert E. (*M* 1919) Vice-Pres. and Treas., ●Burnham Boiler Corp., 2 Main St., Irvington, and 55 Burnside Dr., Hastings-on Hudson 6, N. Y.

BATEMAN, William Hamilton (*A* 1944) Partner, ●Keystone Sales Co., 547 Lincoln Ave., P. O. Box 4201, Bellevue Station, and 1011 California Ave., Avalon, Pittsburgh 2, Pa.

BATES, John H. (*A* 1947; *J* 1941; *S* 1939) U. S. Army, and ●1313 W. Lehigh, Philadelphia, Pa.

BATTAN, S. W. (*M* 1940) Pres., ●Perma-Temp Products, Inc., 838 E. Federal St., Camden, N. J., and Hillcrest Hotel, Stenton Ave., Bethlehem Pike, Whitemarsh, Philadelphia, Pa.

BAUER, Albert E. (*M* 1935) Mgr., Special Prod. Div., Stainless & Steel Products Co., 1000 Berry Ave., St. Paul 4, and ●59 S. Victoria St., St. Paul 5, Minn.

BAUER, Jean (*J* 1946) ●Ventilator A. G., Staefa, and Basel, Switzerland.

BAUER, John (*M* 1946) Mgr. ●Bauer Heating & Plumbing Co., 627 Avenue A, and 924 Fourth Ave., Plattsmouth, Nebr.

BAUER, Ray F. (*M* 1945) Engr., ●434 N. Rock Island, and 225 N. Rutan, Wichita, Kans.

BAUM, Albert L. (*M* 1916) Partner, ●Jaros, Baum & Bolles, 415 Lexington Ave., New York 17, and 600 West 111th St., New York 25, N. Y.

BAUMAN, Carl S. (*M* 1948) Exec. Engr., Tex-Air Conditioning Co., ●1201 Jones St., and 910 Collier St., Fort Worth, Texas.

BAUMANN, Arnold W. (*M* 1948) Chief Engr., Arthur Harris & Co., 212 N. Aberdeen, and ●40 E. Oak, Chicago, Ill.

BAUMGARDNER, C. M. (*M* 1928) Exec., Vice-Pres., ●U. S. Radiator Corp., 300 Buhl Bldg., Detroit 31, Mich., and 416 Cumnor Rd., Kenilworth, Ill.

BAUTTS, Ray A. (*M* 1945) Asst. Mgr. Gas Dept., ●Arkansas Power & Light Co., 112 W. Washington Ave. (Box 812), and 1005 W. Oak St., Jonesboro, Ark.

BAWDEN, Leslie A. (*A* 1945) Midland Area Engr., Spirax Manufacturing Co., Ltd., Beechmont, Cheltenham, Gloucester, and ●38 Windsor Rd., Evesham, Worcestershire, England.

BAXTER, A. G. (*M* 1944) Htg. Engr., ●Enterprise Foundry Co., Ltd., Sackville, N. B., and 28 Clarence St., Amherst, Nova Scotia, Canada.

BAXTER, Henry A. (*A* 1944) Gen. Mgr., ●W. H. Cunningham & Hill, Ltd., 269-271 Richmond St. W., and 93 Castlewood Rd., Toronto, Ont., Canada.

BAXTER, William E. (*A* 1939) Pres., ●W. E. Baxter, Ltd., 2200 Hingston Ave., Montreal, and 89-51st Ave., Lachine, Que., Canada.

BAY, Charles H (*A* 1938) Sales Repr., ●The Detroit Edison Co., 2000 Second Ave., Detroit, and Woodward Ave., Bloomfield Hills, Mich.

BAYLESS, Robert L., Jr. (*A* 1946) Owner and Mgr., ●Valley Sheet Metal Co., 230 N. Ninth St., and 367 Orme Ave., Phoenix, Ariz.

BAZILLE, Clarence H. (*M* 1944) Cons. Engr., ●Clarence H. Bazille, Room 726, Pacific Bldg., 821 Market St., San Francisco 3, and Hotel Gotham, San Francisco 1, Calif.

BAZZONI, Joseph P. (*M* 1946; *A* 1942) Mech. Engr., Shaw, Metz & Dolio, 208 S. LaSalle, Chicago, and ●Rt. 2, Ottawa, Ill.

BEACH, Albert F., Jr. (*M* 1944) Appl. Engr., Carrier Corp., 405 Lexington Ave., New York, N. Y., and ●214 Columbia Ave., Cranford, N. J.

BEACH, Milton W. (*A* 1947) Sales Engr., M. W. Beach Sales & Engineering, 519 Main St., Cincinnati 2, and ●309 W. McMillan St., Cincinnati 19, Ohio.

BEACH, Ralph L. (*M* 1942) Dist. Engr., York Corp., 412 Houston St. N.E., P. O. Box 2210, Atlanta, and ●131 Clarion Ave., Decatur, Ga.

BEAGHEN, George W. (*A* 1944) Field Engr., ●American Blower Corp., 50 West 40th St., New York 18, and 146 Seventh Ave., Pelham, N. Y.

BEAIRD, Benjamin J. (*M* 1945) Chief Engr. and Estimator, Charles G. Heyne & Co., 2002 Rothwell, and ●1621 Kipling, Houston, Texas.

BEALS, Dowell E. (*M* 1941; *J* 1940) Owner, ●Beals Plumbing & Heating Co., 315 West 13th St., and 4001 Calmont St., Fort Worth, Texas.

BEAM, Lucien H. (*A* 1946) Supvsr. of Utility Operations, Fairchild Aircraft, Hagerstown, Md., and ●Route 4, Waynesboro, Pa.

BEAN, George S. (*A* 1935) Mgr., Stoker Div., ●North Western-Hanna Fuel Co., 2196 University Ave., St. Paul 4, and 4949-16th Ave., Minneapolis, Minn.

BEAN, Thomas H., Jr. (*M* 1944) Cons. Engr., 813 Hidalgo St., New Orleans 19, La.

BEARDEN, John D. (*A* 1946) Engr., ●Hall-Neal Furnace Co., 1324 N. Capitol Ave., and 145 E. Hoefgen St., Indianapolis, Ind.

BEARG, Milton J. (*M* 1944) Air Cond. Engr., Sanderson & Porter, 52 William St., New York 5, and ●192-39 Hollis Ave., Hollis 7, L. I., N. Y.

BEARMAN, Alexander A. (*M* 1937) Engr., ●20th Century-Fox Film Corp., 444 West 56th St., New York 19, and 3111 Broadway, New York 27, N. Y.

BEARSE, Allen H., Jr. (*A* 1945) Partner, ●Barrows Coal Co., 35 Main St., and 56 Western Ave., Brattleboro, Vt.

BEATTIE, James (*A* 1940) Owner, James Beattie, 7327 Tiremon, Detroit 4, and ●17215 Greenlawn Ave., Detroit 21, Mich.

BEATTY, John W. (*J* 1944; *S* 1941) Htg. Engr., ●Beatty Hardware Co., 118-120 Main St., and 612 State St., Beardstown, Ill.

BEATY, Stanford W. (*A* 1947) Air Cond. Engr., ●Arkansas Natural Gas Corp., P. O. Box 1734, Shreveport 4, and 3238 Southern Ave., Shreveport, La.

BEAUCHAMP, John H. (*A* 1945) Owner-Mgr., • Heating & Refrigeration Maintenance Co., 3913 S. Main St., and 1005 Isabella, Apt. 33, Houston 4, Texas.

BEAURRIENNE, Auguste* (*Life Member*; *M* 1912) Engr. Expert, 25 Rue des Marguettes, Paris XII, and • 18 Rue Petit Val, Sucy en Brie, Seine et Oise, France.

BEAVERS, G. R. (*M* 1929) c/o Margison and Babcock, Cons. Engrs., Indus. Designers, 119 Isabella St., Toronto, and • c/o 4, Earl St., Toronto 5, Ont., Canada.

BECHIR, Nicholas V. (*M* 1946) Asst., Refrig. Dept., • Volkart Brothers, 8 Clive St., and 21 Humayan Ct., Calcutta, India.

BECHTOL, J. J. (*A* 1942; *J* 1937) Engr., Estimator, L. E. Stevens Co., 626 Broadway, Cincinnati 2, and • 1282 Quebec Rd., Cincinnati 5, Ohio.

BECKER, C. S. (*M* 1939) Mech. Engr., • American Blower Corp., Room 1504, 228 N. LaSalle St., Chicago 1, and 514 S. Dunton Ave., Arlington Heights, Ill.

BECKER, George E. (*A* 1943) Secy.-Treas., Sales and Service, • Frigid Refrigerator Service, 3232 Olive, St. Louis 3, and 5329 Delor St., St. Louis, Mo.

BECKER, Philip F. (*M* 1947) Elec. Engr., Board of Transportation, 250 Hudson St., New York 13, and • 161 East 206th St., New York 58, N. Y.

BECKER, Sidney J. (*A* 1947; *J* 1944) Engr., • J. Becker, Inc., 6355 Park Ave., and 4804 Cote Des Neiges, Apt. 31, Montreal, Que., Canada.

BECKWITH, F. J. (*M* 1940) Htg. and Vent. Engr., Henley & Beckwith, 2628 Pearl St., and • R. F. D. 1, Box 250, Jacksonville, Fla.

BECRAFT, Edwin R. (*A* 1947) Export Director, The Trane Co., and • 1907 Adams St., La Crosse, Wis.

BEDARD, Earl L. (*A* 1946) Chief Engr., • Aldrich Mfg. Co., and Wyoming, Ill.

BEEBE, F. E. W. (*Life Member*; *A* 1915) Retired, 20 Denman Pl., Elizabeth 3, N. J.

BEECRAFT, Gerald A. (*A* 1946) Partner, • Atlas Air Conditioning Co., 22450 Fenkell Ave., Detroit 23, and 24320 Union Ave., Dearborn, Mich.

BEERS, Louis N. (*A* 1942) Sales Engr., Nicolai's Tucson Pipe Works, 416 W. Davis, and • 2745 N. Martin, Tucson, Ariz.

BEERS, Vance A. (*A* 1946) Htg. Dept., Marshall-Wells Co., 1420 N.W. Lovejoy, and • 3849 N. Kiska, Apt. 10 Portland, Ore.

BEERY, Clinton E.* (*M* 1936) Pres., Heat & Fuel Engineering Co., Inc., 1454 Hood Ave., Chicago, Ill.

BEERY, Vernon L. (*A* 1944) Sales Engr., Consolidated Industries, Inc., Lafayette, Ind.

BEGGS, Philip B. (*A* 1946) Partner, • Paul W. Beggs & Son, 665 Folsom St., San Francisco 7, and 1322-32nd Ave., San Francisco 22, Calif.

BEGGS, William E. (*M* 1927) Owner, W. E. Beggs Co., 234 Ninth Ave. N., and • 2580 W. Viewpoint Way, Seattle, Wash.

BEGOON, George F. (*A* 1945) Vice Pres., • The Thermix Corp., First National Bank Bldg., and 55 Orchard Drive, Greenwich, Conn.

BEIGHEL, H. A. (*A* 1927) Owner, • Allegheny Engineering Co., 503 Columbia Bldg., Pittsburgh, and 207 Puritan Rd., Rosslyn Farms, Carnegie, Pa.

BEINEKE, Robert C. (*A* 1947) Engr., • Fosdick & Hilmer, Consulting Engrs., 1703 Union Trust Bldg., Cincinnati 2, and 3745 Boudinot Ave., Cincinnati 11, Ohio.

BEIRN, John B. (*A* 1945) Sales Engr., American Radiator & Standard Sanitary Corp., 1617 Penna. Blvd., Pittsburgh, Pa., and • 9517 Ventnor Ave., Margate, N. J.

BEISEL, Karl E. (*J* 1944) Naval Archt., Norfolk Naval Shipyard, and • 20 Lawrence Circle, Apt. K-5, Portsmouth, Va.

BEITZELL, Albert E. (*A* 1933; *J* 1930) Vice-Pres., Combustioneer Corp., 409 Tenth St. S.W., Washington, D. C., and • 6701 N. Delfield St., Chevy Chase 15, Md.

BEKESHUS, J. Herbert (*M* 1945) Pres., • Pioneer Oil Heat, Inc., 229 River St., and 1503 Massachusetts Ave., Troy, N. Y.

BELANGER, William (*M* 1944) Owner, Southeastern Supply Co., 390 N. Front St., New Bedford, Mass.

BELDEN, Albert G., Jr. (*M* 1944) Pres., • Belden Co., 15 South 13th St., and 2700 Wilson Dr., Terre Haute, Ind.

BELFORD, Louis B. (*A* 1940) Eastern Supvsr., Air Cond. Control Div., • Minneapolis-Honeywell Regulator Co., 221 Fourth Ave., New York 3, and 295 Murray Ave., Larchmont, N. Y.

BELINE, Martin B. (*M* 1944) Gen. Sales Mgr., Wm. Bornstein & Son, Inc., Second & Kennedy Sts. N.W., Washington 11, D. C., and • 201 W. Bradley Lane, Chevy Chase, Md.

BELING, Earl H.* (*M* 1936; *A* 1930; *J* 1925) Owner, Chief Engr., • Beling Engineering Co., 1407 Seventh Ave., and 2428-13th St., Moline, Ill.

BELL, D. G. (*A* 1946) Chief Engr., • Robb and Rowley United Inc., 314 S. Harwood, Dallas 1, and 9714 Rockbrook, Dallas 9, Texas.

BELL, E. Floyd (*M* 1933) Pres., • Bell & Eiss, Inc., 2102 Foshay Tower, Minneapolis 2, and 5224 Oak Lawn Ave., Minneapolis, Minn.

BELL, John A. (*A* 1944) Field Engr., Furnasman Manufacturing Co., Ltd., Pembina Highway, and • 1117 "B" Grosvenor Ave., Winnipeg, Man., Canada.

BELL, Sydney R. (*M* 1939) Principal, • Sydney R. Bell & Assocs., Cons. Engrs., 374 Little Collins St., and 12 Queens Rd., Melbourne, Australia.

BELL, Thomas H. (*A* 1944) Engr. and Supt. of Constr., Columbus Heating & Ventilating Co., 182 N. Yale Ave., and • 296 S. Eureka Ave., Columbus, Ohio.

BELL, Wilbur C. (*J* 1946) Asst. Engr., B. F. Sturtevant Co., Div. of Westinghouse Electric, and • 1455 River St., Hyde Park, Boston 36, Mass.

BELLMAN, John V. (*A* 1946; *J* 1943) Chief Petty Officer, Directorate of Electrical Supply, Naval Service Headquarters, Ottawa, and • 170 Hope St., Toronto, Ont., Canada.

BELSKY, George A. (*M* 1945) Pres., George A. Bell, Inc., 215 East 37th St., New York, and • 78 Randolph Rd., White Plains, N. Y.

BELYEA, Roy E. (*A* 1944) Pres. and Mgr., • Belyea Brothers, Ltd., 1002 Bathurst St., and 207 Glenayr Rd., Toronto, Ont., Canada.

BEMAN, Myron C. (*M* 1926), (Council, 1934-39), Partner, • Beman & Candee, 271 Delaware Ave., Buffalo 2, and 262 E. Quaker St., Orchard Park, N. Y.

BEMARKT, George H. (*M* 1945) 516 North 19th St., Apt. 3, East St. Louis, Ill.

BEMIS, Paul D. (*M* 1942) Owner, • Consulting Engr., 36 Pearl St., Hartford 3, and 31 Riggs Ave., West Hartford, Conn.

BEMIS, Wilfred A. (*A* 1942) Owner, Bemis Supply Co., 1401 Macklind Ave., St. Louis, and • 129 Emerling Dr., Normandy 21, Mo.

BENGLE, Charles V. (*A* 1946) Dist. Repr., Air Cond. & Refrig. Div., • Worthington Pump & Machinery Corp., 801 Race St., Cincinnati 1, and 3629 Erie Ave., Cincinnati 8, Ohio.

BENHAM, Colin S. K. (*A* 1940; *J* 1937) Dir., • Benham & Sons, Ltd., 66 Wigmore St., London W. 1, and Hill House, Great Missenden, Bucks., England.

BENHAM, Ford C., Jr. (*A* 1942; *J* 1938) Air Cond. & Htg. Engr., M. F. Fischer & Son, 203 Fredericksburg Rd., and • 209 Harmon Dr., San Antonio, Texas.

BENN, Charles L. (*M* 1947) Supvsr. of Utilization Engrg., Equitable Gas Co., 610 Wood St., Pittsburgh, and • 59 Belvedere St., Pittsburgh 5, Pa.

BENNIS, Raymond R. (*M* 1947; *A* 1943) Chief Engr., • Contractors Refrigeration Corp., 89-35 Queens Blvd., Elmhurst, and 67-47-181st St., Flushing, N. Y.

BENOIST, LeRoy L. (*M* 1934) Owner & Mgr., • Benoist Brothers Supply Co., 117 S. Tenth St., and 1500 Main St., Mt. Vernon, Ill.

BENOIST, Raymond E. (*A* 1936) Mgr. and Engr., Benoist Brothers Supply Co., 117 S. Tenth St., and • 811 North 12th St., Mt. Vernon, Ill.

BENSEN, Clarence L. (*M* 1939; *J* 1935) Sales Mgr., Refrig. Dept., McQuay, Inc., 1600 Broadway St. N.E., and • 3042 Benjamin St. N. E., Minneapolis 13, Minn.

BENSINGER, Mark (*A* 1946; *J* 1936) Lt. (jg), and • 608 Bradley Lane, Fairview Heights, Portsmouth, Va.

BENSON, John C. (*A* 1945) Washington Branch Mgr., • Carrier Corp., 942 Investment Bldg., Washington 5, D. C., and 103 Southbrook Lane, Bethesda 14, Md.

BENSON, M. A. (*M* 1944) Branch Mgr., • Johnson Service Co., 2708 Live Oak, Dallas 1, and 815 Reverchon Dr., Dallas 11, Texas.

BENTLEY, Clyde E. (*M* 1937) Owner, • 405 Sansome, San Francisco 11, and 1875 San Antonio Ave., Berkeley, Calif.

BERGAN, John R. (*M* 1945; *A* 1941; *J* 1937) Eastern Sales Mgr., Moduflow Div., • Minneapolis-Honeywell Regulator Co., 221 Fourth Ave., New York 3, and 293 Murray Ave., Larchmont, N. Y.

BERGER, Clyde D. (*M* 1947) Mech. Engr., United Engineers & Constructors Inc., 1401 Arch St., and • 4518 Locust St., Philadelphia 5, Pa.

BERGER, J. L. (*M* 1939) Treas., • The J. L. McHale Co., 5915 Bonna Ave., Cleveland 3, and 2652 Edgerton Rd., Cleveland 18, Ohio.

BERGER, John V. (*M* 1947) Refrig. & Air Cond. Engr., McCombs Refrigeration Supply Co., 1524 15th St., Denver 17, and • 267 Acoma St., Denver 9, Colo.

BERGER, William W. (*A* 1946) Field Engr., John J. Nesbitt, Inc., P. O. Box 1503, and • 1352 Downs Ave., Charlotte, N. C.

BERGMAN, A. E. (*A* 1943) Pres., • A. E. Bergman, Inc., 1913 University Ave., St. Paul, and 2744 West River Rd., Minneapolis, Minn.

BERGMAN, Harold (*A* 1946) Sales Repr., • J. A. Zurn Manufacturing Co., 417 Citizens' Bldg., and 1521 Coventry Rd., Cleveland, Ohio.

BERKELEY, Clarence D. (*M* 1944) Chief Engr., Herman Nelson Co., 114 South 23rd St., and • 2304 North 20th St., Boise, Idaho.

BERLET, E. J., Jr. (*M* 1943) Branch Sales Mgr., York Corp., 5051 Santa Fe Ave., Los Angeles 11, and • 816 Clarence Ave., San Gabriel, Calif.

BERMAN, Louis K. (*M* 1908) Pres., • Raisler Corp., 129 Amsterdam Ave., New York 23, and 885 Park Ave., New York 21, N. Y.

BERMEL, Alfred H. (*M* 1943; *A* 1933; *J* 1928) Chief Mech. Estimating Engr., • August Arace & Sons, Inc., 642 Third Ave., Elizabeth, and 340 Cambridge Dr., Union, N. J.

BERNARD, Edgar L. (*J* 1941; *S* 1940) Cons. Engr., Clark-Babbitt Industries Inc., 75 Federal St., Boston 10, and • 40 Chester St., Boston 34, Mass.

BERNHARD, George (*M* 1944) Richfield Manufacturing Corp., 315 Fifth Ave., New York 16, and • 1175 E. Broadway, Hewlett, L. I., N. Y.

BERNHARDT, Raymond J. (*A* 1947) Mech. Engr., U. S. Engineering Corp., and • 634 W. Kings' Highway, San Antonio 1, Texas.

BERNSTROM, C. Bertil (*M* 1944) Chief Engr., Jaden Manufacturing Co., and • 223 W. Fifth St., Hastings, Nebr.

BERNZEN, John (*A* 1944) Vice-Pres., • The City Plumbing & Heating Co., 1123 Walnut, P. O. Box 71, and 833 Spruce, Boulder, Colo.

BERRY, Norton E. (*M* 1944) Dir. of Research, • Servel, Inc., Evansville 20, and Newburgh, Ind.

BERRY, Patrick M. (*A* 1944) Chief Engr., Standard Asbestos Manufacturing Co., 1844 East 40th St., Cleveland 3, Ohio.

BERRY, Robert U. (*M* 1939) Mgr., Indus. Marine & Contr. Div., Air Cond. Dept., • General Electric Co., 5 Lawrence St., Bloomfield, and 548 N. Maple Ave., East Orange, N. J.

BERRYMAN, Richard H. (*A* 1945; *J* 1940) Chief Engr., Thermocraft Co., 1801 E. McNichols Rd., and • 264 Worcester Pl., Detroit 3, Mich.

BERTOLETT, Chester (*M* 1940) Htg. and Vent. Engr., 515 Broadway, Dobbs Ferry, N. Y.

BERTRAM, John F. (*A* 1946) Dist. Mgr., • Minneapolis-Honeywell Regulator Co., Ltd., 156 Lombard St., and 354 Oakwood Ave., Winnipeg, Man., Canada.

BERTRAND, George F. (*M* 1946; *A* 1939) Owner, • George F. Bertrand Co., 12 South 12th St., Philadelphia 7, and 821 Blythe Ave., Drexel Hill, Pa.

BERZELIUS, Carl E. (*M* 1936) Central Indus. Sales Mgr., Certain-Teed Corp., 120 S. La Salle, Chicago, and • 1519 Vine Ave., Park Ridge, Ill.

BEST, E. Thompson (*M* 1944) Mgr., Air Cond. and Refrig., Frank A. McBride Co., 160 Ward St., Paterson, and • 189 Lakewood Ave., Ho-Ho-Kus, N. J.

BETTENCOURT, Henry J., Jr. (*S* 1948) Student, A. & M. College of Texas, College Station, and • 3815 Avenue S., Galveston, Texas.

BETZ, Harry D. (*M* 1928) Owner, Betz Engineering Co., 1330 Broadway, Kansas City 6, Mo., and • 5414 Aberdeen Rd., Kansas City 3, Kans.

BEVAN, John H. (*A* 1947) Chief Draftsman, • Trane Company of Canada, Ltd., 4 Mowat Ave., and 182 Dunn Ave., Toronto, Ont., Canada.

BEVIL, Alex T. (*A* 1944) Chief Engr., W. F. Slater Engineering Corp., 627 Monroe Ave., Memphis 3, and • 1521 Waverly Ave., Memphis 6, Tenn.

BEVINGTON, Curtis H. (*M* 1936) Owner, • C. H. Bevington Co., 330 S. Wells St., Chicago 6, and R. F. D. 2, Elmhurst, Ill.

BEVINGTON, Warren C. (*M* 1942) Pres., • Bevington, Taggart & Fowler, Inc., 730 Indiana Pythian Bldg., Indianapolis 4, and 3101 N. Meridian St., Indianapolis 8, Ind.

BIANCULLI, Vincent A. (*A* 1945) Engr., • James Biancolo & Son, 558 Broome St., New York 13, and 141-35-78th Rd., Flushing, N. Y.

BIBER, Herbert A. (*A* 1937) Asst. Supt., Koppers Bldg., Seventh Ave. and Grant St., Pittsburgh, and • 323 Barnes St., Wilkinsburg, Pittsburgh 21, Pa.

BIBLE, Hollis U. (*M* 1940) Cons. Engr., • 802 Milam Bldg., and 3121 Amherst, Houston, Texas.

BICHLER, Joseph S. (*S* 1948) Student, University of Michigan, Ann Arbor, and • 12145 Waltham Ave., Detroit 5, Mich.

BICHOWSKY, F. Russell, Dr. (*M* 1935) Lecturer, Div. of Mech. Engrg., • University of California, Berkeley 4, and 2020 Asilomar Dr., Oakland 11, Calif.

BICKEL, Henry A. (*J* 1947) Sales Engr., • Johnson Service Co., 1230 California St., Denver, Colo., and 4312 Chester Dr., Youngstown, Ohio.

BICKELL, George C. (*A* 1945) Sales Engr., • Tutein Equipment Co., 130 Bradford Ave., Pittsburgh 5, and R. D. 2, Wagner Rd., Allison Park, Pa.

BIERL, Joseph G. (*M* 1945) Vice-Pres., • Schollman Bros. Co., 4114 North 24th St., and 4927 North 34th Ave., Omaha, Nebr.

BIGELOW, Folger H. (*A* 1944) Branch Mgr., • Ilg Electric Ventilating Co., 313 Techwood Dr. N.W., and 720 E. Paces Ferry Rd. N.E., Atlanta, Ga.

BIGGERS, Richmond H. (*A* 1939) Mfrs. Agent, 2229 E. Jefferson Ave., Detroit 7, Mich.

BIGGS, Richard A. (*A* 1947) Dvlpt. Engr., Pittsburgh-Corning Corp., 632 Duquesne Way, Pittsburgh, and • P. O. Box 1423, Pittsburgh 30, Pa.

BIGHAM, Bruce H. (*A* 1947) Htg. Dept., Nelson Co., 2604 Fourth Ave., Detroit 1, and • 18960 Rutherford Ave., Detroit 19, Mich.

BILDERBACK, George R. (*A* 1945) Asst. Mgr., Advanced Refrigeration, Inc., 350 Peachtree N.E., and • 1975 Baker Rd. N.W., Atlanta, Ga.

BILGREI, Emanuel (*A* 1946) Gen. Mgr. and Chief Engr., • Marc Air Conditioning & Refrigeration Corp., 116 Penn St., and 146 Hewes St., Brooklyn 11, N. Y.

BILLINGSLEY, Oliver F., II (*A* 1944; *J* 1937) 2172 West 20th St., Long Beach, Calif.

BILLINGTON, Dan B. (*A* 1947) Sales Engr., • A. L. Vanderhoof Inc., 233 Hanna Bldg., Cleveland, and 1864 Forest Hills Blvd., East Cleveland, Ohio.

BINDER, Charles G. (*M* 1920) Mgr., Htg. Dept., Warren Webster & Co., 17th and Federal St., Camden, and • 115 Oak Terrace, Merchantville, N. J.

BINNS, Arthur J. H. (*M* 1946) Dir. and Owner, • F. J. Baynes, Ltd., 99-107 St. Paul's Rd., London N. 1, and 34 Oakley St., Chelsea, London S.W. 3, England.

BIRD, Charles (*A* 1934) Treas. and Gen. Mgr., The Cincinnati Supply Co., 450-456 E. Pearl St., Cincinnati, Ohio.

BIRD, G. L. H. (*A* 1946) Lecturer, Borough Polytechnic, London, S.E. 1, and • 17 Blomfield Rd., London, W. 9, England.

BIRDSALL, Harry W. (*A* 1947) Partner, The Arrow Co., S.W. Fourth Ave., and • Box 42, Ontario, Ore.

BIRKETT, Harold S. (*M* 1940) Coordinator, • The Brooklyn Union Gas Co., 176 Remsen St., Brooklyn 2, and 87 Deepwood Rd., Roslyn Heights, L. I., N. Y.

BIRNER, I. L. (*M* 1945) Mgr., Architects' Sales Service Dept., The Celotex Corp., 120 S. LaSalle St., Chicago 3, Ill.

BISBEE, Bertin A. (*A* 1945) Partner, Smith & Bisbee Hardware Co., 412-416 Main St., and • 212 W. First St. N., Marshall, Minn.

BISHOP, Albert H. (*M* 1944) Elec. Engr., Hume & Rumble, and • 3056 West 38th Ave., Vancouver, B. C., Canada.

BISHOP, Alvin C. (*A* 1946) Pres., • Commercial Sheet Metal & Engineering Co., and 2644 Bremerton Rd., Brentwood 17, Mo.

BISHOP, Charles R. (*Life Member*; *M* 1901), (Council, 1916) 22 Sagamore Rd., Bronxville, N. Y.

BISHOP, Frederick R. (*M* 1921) Mgr. of Sales, Blower Div., The Brundage Co., Kalamazoo, and • 8011 Dexter Blvd., Detroit 6, Mich.

BISHOP, Frederick W. (*A* 1945) Htg. & Piping Consultant, and • 89 St. Clare Ave., St. John's, Newfoundland.

BISHOP, J. A. (*M* 1939) Dist. Mgr., • American Blower Corp., 619 Texas Bank Bldg., Dallas 2, and 1115 N. Windomere St., Dallas 8, Texas.

BISHOP, M. W. (*M* 1942; *A* 1939; *J* 1935) (Council, 1947) Dept. Mgr., • American Blower Corp., 228 N. LaSalle St., Room 1504, Chicago 1, and 218 N. Merril Ave., Park Ridge, Ill.

BISPALA, John T. (*A* 1940) Partner, Bispala Bros., 2328 First Ave., Hibbing, Minn.

BJERKEN, Maurice H. (*M* 1938) Northwestern Mgr., • Hoffman Specialty Co., 438 Builder's Exchange, Minneapolis 2, and 4952-17th Ave. S., Minneapolis, Minn.

BLACK, Edgar N., 3rd (*M* 1922) Philadelphia Mgr., • Fitzgibbons Boiler Co., Inc., 1717 Sansom St., Philadelphia, and 111 Woodside Rd., Haverford, Pa.

BLACK, James M. (*A* 1945; *J* 1940; *S* 1939) Engr., Avery Engineering Co., 1906 Euclid Ave., Cleveland 15, and • 3140 East 135th St., Cleveland 20, Ohio.

BLACKHALL, Wilmot R. (*M* 1922) Partner, • Blackhall Heating & Plumbing Supplies, 1104 Bay St., and 332 Waverly Rd., Toronto, Ont., Canada.

BLACKMAN, Alfred O. (*Life Member*; *M* 1911) Greenwich Lodge, 47 Lafayette Pl., Greenwich, Conn.

BLACKMAN, Robert C. (*A* 1945; *J* 1944) Power Engr., Allison Div., General Motors Corp., and • 1267 N. Lynhurst Dr., Indianapolis 8, Ind.

BLACKMORE, F. H. (*M* 1923) Vice-Pres. in Charge Mfg., • U. S. Radiator Corp., 1500 United Artists Bldg., Detroit 31, and 515 Tooting Lane, Birmingham, Mich.

BLACKMORE, Joseph J. (*A* 1939; *J* 1937) Mfrs. Agt., • 4030 Chouteau Ave., St. Louis, Mo., and 312 S. Fillmore St., Edwardsville, Ill.

BLACKSHAW, J. L.* (*M* 1937; *J* 1929) Mgr., Atlanta Branch, Air and Refrigeration Corp., P. O. Box 1671, Atlanta 1, and • 1444 Funston St. S.E., Atlanta, Ga.

BLACKSTONE, A. L., Jr. (*J* 1947) Instructor, University of South Carolina, School of Engrg., and • 2227 Wheat St., Columbia, S. C.

BLACKWELL, Alfred H. (*A* 1946) Mgr., Harmor Products Co., Inc., 923 Harrison St., San Francisco 7, and • 453 Hawthorne Ave., Palo Alto, Calif.

BLACKWELL, J. S. (*A* 1944) Prop., • Air Engineering, 870 Massachusetts Ave., Indianapolis 4, and 5034 Broadway, Indianapolis 5, Ind.

BLADEN, Arthur M. (*M* 1945) Owner, • Neiler, Rich & Bladen, 431 S. Dearborn St., Chicago 5, and 334 N. Kenilworth Ave., Oak Park, Ill.

BLAIR, Donald W. (*M* 1947; *A* 1940) Designer, Stone & Webster Engineering Corp., 49 Federal St., Boston 7, and • 59 Frost St., Cambridge, Mass.

BLAIR, Ernest L. (*M* 1941) Chief Bldg. Service Engr., Stone & Webster Engineering Corp., 49 Federal St., Boston 7, and • 108 Willow Ave., Wollaston 70, Mass.

BLAIR, Harold C. (*A* 1947) Owner, • Harold C. Blair Manufacturers' Service, 5735 Cass Ave., Detroit 2, and 4015 Three Mile Dr., Detroit 24, Mich.

BLAIR, Howard A. (*A* 1945) Mgr., Service and Const. Dept., • Westinghouse Electric Corp. Sturtevant Div., Hyde Park 36, and 172 Lindbergh Ave., Needham Heights 94, Mass.

BLAKE, Albert H. (*M* 1943) Managing Dir., • B. F. Sturtevant Co. of Canada, Ltd., 137 Wellington St. W., and 5 Glenroy Ave., Toronto, Ont., Canada.

BLAKE, John L. (*A* 1943) Chief Engr., Air Cond. Dept., M. G. M. Studios, 10202 Washington Blvd., Culver City, and • 1700 S. Bedford St., Los Angeles 35, Calif.

BLAKELEY, Hugh J. (*M* 1935) Partner, • Hubbard, Lawless and Blakeley, Cons. Engrs., 110 Whitney Ave., New Haven 10, and 24 Bradley Ave., East Haven, Conn.

BLAKER, Alfred H. (*A* 1939) Secy.-Treas., • National Korectaire Co., 1619 Cortland St., Chicago, and 6018 N. Francisco Ave., Chicago 45, Ill.

BLANCHARD, Norris M. (*M* 1942) Owner, • The Norris Blanchard Co., 1305 W. O. W. Bldg., Omaha 2, and 5609 Western Ave., Omaha 3, Nebr.

BLANDING, Robert L. (*M* 1938) Retired, • 1385 Smith St., North Providence 11, R. I.

BLANKENSHIP, Dick (*A* 1946) Asst. Engr., • W. Bruce Morrison, Cons. Engrs., Cascade Bldg., Portland 4, and 9017 N. Milne St., Portland 3, Ore.

BLANKIN, Merrill F. (*M* 1927; *A* 1926; *J* 1919), (*Presidential Member*), (Pres., 1943; 1st Vice-Pres., 1942; Treas., 1939-41), (Council, 1939-44), Pres., • Blankin Equipment Corp., N.E. Cor. 35th St. and Indiana Ave., Philadelphia 32, and 528 E. Gates St., Philadelphia, Pa.

BLAS, Romualdo J. (*M* 1936) Engr., • Venezuela Basic Economy Corp., Apartado 1944 and La Campina, Caracas, Venezuela, S. A.

BLASE, Theodor F. (*J* 1946) Draftsman, • Air Conditioning & Engineering Co., 91 Smith St., Durban, and 88 Nirvana Rd., Brighton Beach, Natal, South Africa.

BLATHERWICK, Howard E. (*A* 1947) Sales, • Warden King Ltd., 2104 Bennett Ave., and 3236 Mercier Ave., Montreal, Que., Canada.

BLAZEK, Louis J., Jr. (*J* 1948) Mech. Engr., Ellerbe & Co., East 505, 1st National Bank Bldg., and • 512 St. Peter, St. Paul, Minn.

BLAZER, Benjamin V. (*A* 1940) Owner, • M. Blazer & Son, 173 Market St., Passaic, and 48 13th Ave., Paterson, N. J.

BLEIER, Frank P. (*M* 1945; *A* 1944) Cons. Designer, 547 W Addison St., Chicago 13, Ill.

BLOCH, Leonard L. (*A* 1944) 4440 Ambrose Ave., Los Angeles 27, Calif.

BLOJ, Carlos (*J* 1948) Engrg. Management, Sociedad Industrial Electer, Av. J. P. Alessandri 361, and • Av. R. Lyon 3060, Santiago, Chile, S. A.

BLOOM, Louis (*M* 1935) Pres., • Freeport Plumbing & Heating Engrs., 50 N. Main St., and 108 Lexington Ave., Freeport, L. I., N. Y.

BLOOM, Ralph L. (*M* 1945) Mech. Engr., • 623 Sexton Bldg., Minneapolis 15, and 3754 Joppa Ave., Minneapolis 16, Minn.

BLOOMSTER, Edgar L. (*M* 1943) Cons. Engr., E. L. Bloomster, 116 New Montgomery St., San Francisco 5, and • 200 El Benito Way, Millbrae Highlands, San Mateo Co., Calif.

BLUM, Herman, Jr. (*M* 1947; *A* 1944; *J* 1936) Owner, Herman Blum, Engr.-Cons., • 2812 Fairmount St., Dallas 4, and 4438 Emerson, Dallas 5, Texas.

BLUM, Richard J., Jr. (*A* 1940) Vice-Pres., • The Kirk & Blum Mfg. Co., 2850 Spring Grove Ave., Cincinnati 25, and 6126 Hempwood Ave., Cincinnati 24, Ohio.

BLUM, Robert D. (*M* 1946) Sr. Appl. Engr., York Corp., and • 652 E. Philadelphia St., York, Pa.

BOALES, William G. (*M* 1936; *A* 1923) Owner, • Wm. G. Boales & Assocs., 6429 Hamilton Ave., Detroit 2, and 43 Edgemere Rd., Grosse Pointe Farms 30, Mich.

BOBST, Earl F. (*A* 1948) Sales, American Radiator & Standard Sanitary Corp., 73 E. Naghten St., Columbus 15, and • 666 S. Cassingham Rd., Columbus 9, Ohio.

BOCK, I. I. (*A* 1944) Owner, • Carrier-Bock Co., 708 N. Harwood, Dallas 1, and 4654 N. Versailles, Dallas, Texas.

BODEN, Walter F. (*A* 1937) Branch Mgr., • Modine Manufacturing Co., 424 E. Wells St., Milwaukee 2, and 4472 S. Lake Dr., Cudahy, Wis.

BODINGER, J. H. (*M* 1931) Pres., J. H. Bodinger Co., Inc., 446 West 38th St., New York 18, N. Y.

BODINUS, William S. (*M* 1946) Branch Mgr., Carrier Corp., 20 N. Wacker Dr., Chicago, and • 5510 Cornelia Ave., Chicago 41, Ill.

BODKIN, Taylor B. (*J* 1947) Comm'l Sales Mgr., • Bodkin & Morris Refrigeration & Electric Co., Box 445, and 806 Montgomery Ave., Sheffield, Ala.

BOEDDENER, George (*A* 1946) Managing Dir., • National Warm Air Heating & Air Conditioning Assn., Society for Savings Bldg., Cleveland 14, and 19832 Roslyn Dr., Rocky River, Ohio.

BOEHLER, Carl L. (*A* 1944) Sales Mgr., • J. A. Walsh & Co., Inc., P. O. Box 1773, Houston 1, and Rt. 12, Box 700, Houston, Texas.

BOEHM, John C., Jr. (*A* 1945) Secy., The John C. Boehm Co., 9002 Madison Ave., Cleveland 2, Ohio.

BOEHM, Robert C. (*J* 1946) Branch Mgr., General Controls Co., 517 South 20th St., and • 1854 Windsor Blvd., Birmingham, Ala.

BOELTER, L. M. K.* (*M* 1944) Dean, • College of Engineering, University of California, and 254 Bronwood Ave., Los Angeles 24, Calif.

BOEMI, Henry (*A* 1947) Engr., Albert Fentzlaff, Inc., 11 West 42nd St., New York 18, and • 943 81st St., Brooklyn, N. Y.

BOESTER, Carl F.* (*M* 1939; *A* 1936) (Council 1947) Dir. of Housing Research, • Purdue Research Foundation, Purdue University, Lafayette, and Union Club, West Lafayette, Ind.

BOGATY, Hermann S. (*M* 1921) Designing Engr., Proctor & Schwartz, Seventh St. and Tabor Rd., Philadelphia 20, and • 735 E. Phil-Ellena St., Philadelphia, Pa.

BOGEN, Arthur D. (*M* 1945) Mgr., • The Home Furnace Co., 330-34 E. Livingston Ave., Columbus 15, and 2207 Yorkshire Rd., Columbus 8, Ohio.

BOGGS, Dennis (*M* 1943) Asst. Chief Engr., Avery Engineering Co., 1906 Euclid Ave., Cleveland 15, and • 5315 Thomas St., Maple Heights, Ohio.

BOGGS, Harold V. (*A* 1946) Owner, • H. V. Boggs Co., 226 State Tower Bldg., Syracuse, and 1431 Broad St., Syracuse 3, N. Y.

BOHREN, Arthur H. (*A* 1947) Partner & Mgr., • Bohren Plumbing Service & Supply Co., 4255 S.E. Belmont St., and 7117 S.W. Fifth St., Portland 15, Ore.

BOKMAN, Thomas P. (*J* 1948) Design Engr., Westinghouse Construction Dept., Maloney Bldg., 337 Blvd. of Allies, Pittsburgh, and • 3140 Beechwood Blvd., Pittsburgh 17, Pa.

BOLAND, L. C., Jr. (*M* 1941) Cons. Engr., 774 Spring St. N.W., and • 1140 Rosedale Dr. N.E., Atlanta, Ga.

BOLES, Harry S. (*A* 1944) Asst. Gen. Power Engr., • Pullman Standard Car & Mfg. Co., 11001 Cottage Grove Ave., and 13702 Indiana Ave., Chicago, Ill.

BOLIN, Harold W. (*S* 1948) Student, David Ranken, Jr., School of Mechanical Trades, St. Louis, Mo., and R. R. No. 1, Oaktown, Ind.

BOLLE, Ferdinand G., Jr. (*A* 1947) Gen. Foreman, J. Brodie & Son, Inc., 1329 E. Fort Street, Detroit, and • 18221 Steel Ave., Detroit 21, Mich.

BOLTON, Otis J. (*S* 1946) Student, Texas A. & M. College, College Station, and • New Baden, Texas.

BOND, Harry H. (*M* 1938) Cons. Engr., • 11 West 42nd St., Room 1282, New York 18, and 137-81 Belknap St., Springfield Gardens 13, L. I., N. Y.

BOND, Horace A. (*M* 1930) Prof. Engr., 152 Washington Ave., and • 12 Ramsey Pl., Albany, N. Y.

BONDE, Ira E. (*J* 1945) Chief Draftsman, Engineer Iron Works, San Jose, and • 183 Willow Rd., Palo Alto, Calif.

BONDY, Winfield S. (*M* 1946) Cons. Engr., • 213 East 38th St., New York 16, and 1993 E. Second St., Brooklyn 23, N. Y.

BONEBRAKE, John H. (*A* 1946) Asst. to J. Donald Kroeker, Cons. Mech. Engr., and • 9116 N. Woolsey Ct., Portland, Ore.

BONNER, John (*M* 1943) Htg. Engr., • The John Bonner Co., 121 Hanover St., Boston 13, and 27 Park Circle, Arlington 74, Mass.

BOOKER, Jack W. (*M* 1943) Engr., • Westinghouse Electric International Co., 40 Wall St., New York, N. Y., and 407 Elm St., Cranford, N. J.

BOONE, Fred S. (*A* 1943) Secy.-Treas., Hall-Neal Furnace Co., 1324 N. Capitol Ave., Indianapolis 7, and • 17 West 35th St., Indianapolis 8, Ind.

BOOT, Arthur (*M* 1943) Owner, • Arthur Boot Co., 1444 Lake Dr. S.E., and 928 Orchard Ave. S.E., Grand Rapids 6, Mich.

BOOTH, Charles A. (*Life Member*; *M* 1917) Vice-Pres., • Buffalo Forge Co., 490 Broadway, and 142 Summit Ave., Buffalo, N. Y.

BOOTH, Clifford A. (*A* 1942) • Fiberglas Canada, Ltd., 1253 McGill College Ave., Montreal, Que., Canada.

BOOTH, Roger W. (*A* 1945) Chief Engr., The Lennox Furnace Co., and • 1516 Kalsem Blvd., Marshalltown, Iowa.

BORAK, Eugene (*M* 1937) 2237 Pennsylvania, Detroit 14, Mich.

BORG, Elmer H. (*M* 1938) Partner, • Brooks & Borg, 820 Hubbell Bldg., Des Moines 9, and 3101 Easton Blvd., Des Moines 17, Ia.

BORKAT, Philip (*A* 1943; *J* 1936) Chief Engr., Viking Air Conditioning Corp., 5600 Walworth Ave., Cleveland 2, and • 869 East 128th St., Cleveland 8, Ohio.

BORNEMANN, Walter A. (*M* 1924; *J* 1923) Sales Engr., • Carrier Corp., 12 South 12th St., Philadelphia 7, and 123 W. Wharton Ave., Glenside, Pa.

BORNQUIST, George W. (*A* 1943) Pres., • Bornquist, Inc., 629 W. Washington Blvd., Chicago 6, and 517 N. Euclid Ave., Oak Park, Ill.

BORNSTEIN, Alfred B. (*A* 1942) Secy., • Wm. Bornstein & Son, 141 Kennedy St. N.W., Washington, D. C., and 9501 Brunett Ave., Silver Spring, Md.

BORNSTEIN, William (*M* 1943; *A* 1937) Partner, • William Bornstein & Son, 141 Kennedy St. N.W., and 5206-14th St. N.W., Washington, D. C.

BORRY, John V. (*S* 1946) Student, University of Minnesota, and • 2881 S. Irving, Minneapolis, Minn.

BORTMAN, Isaac M. (*A* 1946) Owner, Perfect Air Conditioning Co., 422 Luray Pl. N.W., Washington 10, D. C.

BORTON, A. Robert (*A* 1943; *J* 1939) Appl. Engr., Robinson & Stanger, 1005 Empire Bldg., Pittsburgh 22, and • 356 Huntington Ave., Emsworth, Pittsburgh 2, Pa.

BORZELLO, Nick (*A* 1947) Engr., Drying Systems, Inc., 1800 W. Foster Ave., Chicago, and • 736 S. Highland Ave., Oak Park, Ill.

BOSTON, E. B. (*A* 1948) Pres., • Air Products Equipment Co., 1856 N. Cleveland Ave., Chicago, and 163 N. Euclid Ave., Oak Park, Ill.

BOSTROM, H. R. (*A* 1945) Owner, • Bostrom Sheet Metal Works, 1509 Marshall Ave., St. Paul, 4, and 3529-46th Ave. S., Minneapolis 6, Minn.

BOTELHO, Nanto J. (*A* 1937) Director and Chief Engr., • Geibrasil-Cia de Engenharia Av. Pres. Wilson 198-12 Andar, P. O. Box 1269, and Av. Copacabana 209, Apt. 803, Rio de Janeiro, Brazil, S. A.

BOTTORF, James D. (*S* 1948) Student, Purdue University, Lafayette, Ind., and • 1601 Frederica St., Owensboro, Ky.

BOTTUM, Edward W. (*A* 1942; *J* 1938) Chief Engr., Skuttle Manufacturing Co., 517 E. Larned, Detroit, and • 19303 Rutherford, Detroit 19, Mich.

BOUCHER, Kent D. (*M* 1944) Mgr., Carrier Div., • United Clay Products Co., 931 Investment Bldg., Washington 5, D. C., and 1002 S. Mansion Dr., Silver Spring, Md.

BOUEY, Angus J. (*A* 1937; *J* 1930) Sales Engr., • The B. F. Sturtevant Co., 681 Market St., San Francisco 5, and 4810 Fulton St., San Francisco, Calif.

BOUILLON, Lincoln (*M* 1933) Professional Engr., • 426-1411 Fourth Avenue Bldg., and 3220 Sierra Dr., Seattle, Wash.

BOVARD, Carl A. (*A* 1945) Owner, Carl A. Bovard, 42 Hillcrest Ave., Lake Placid, N. Y.

BOVAY, Harry E., Jr. (*M* 1946) Cons. Engr., • Esperson Bldg., Houston 2, and 3132 Southmore, Houston 4, Texas.

BOWEN, Leroy F. (*A* 1942) Br. Mgr., • Pete Armstrong Co., 421 S. Durfee, El Monte, and 15913 Roselle, Lawndale, Calif.

BOWEN, Judson P. (*A* 1945) Dist. Mgr., • Penn Electric Switch Co., 36 Fifth St. N.W., and 725 Woodward Way N.W., Atlanta, Ga.

BOWERS, A. F. (*A* 1919) Pres., • Industrial Heating & Engineering Co., 828 N. Broadway, Milwaukee 2, and 2853 N. Hackett Ave., Milwaukee, Wis.

BOWERS, Charles L. (*M* 1944) Pres., • Bowers Sheet Metal Co., Inc., 1155 Victory Dr. S.W., Atlanta, and 3050 Sylvan Rd., P. O. Box 290, Hapeville, Ga.

BOWERS, Orrin E. (*A* 1947) Engr. & Sales Mgr., Boyle Fuel Co., 1014 North Division, and • Rt. 7, Country Homes, Spokane, Wash.

BOWIE, Robert (*M* 1945) Chief Engr., • H. G. Skelton & Co., Box 1140, and 5 Av. LeSueur, Sea Point, Capetown, South Africa.

BOWLER, R. W. (*J* 1946; *S* 1943) Bowler & Co., and • 2733 France Ave., Minneapolis, Minn.

BOWLES, John R. (*A* 1948) Sales Engr., Cia. Industria E Comercio Glossop, Caixa Postal 1546, Sao Paulo, Brazil, S. A.

BOWMAN, Murray K. (*A* 1947) Service Mgr., • Perfex Controls Ltd., 73 Simcoe St., Toronto 1, and 102 Cowan Ave., Toronto, Ont., Canada.

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BUTLER, Peter D. (*M* 1922) Sales, U. S. Radiator Corp., and • 127 Edgewater Rd., Cliffside Park, N. J.

BUTLER, Richard C. (*J* 1947) Engr., Pfeifer & Shultz, and • 4800 Lyndale, S., Minneapolis 9, Minn.

BUTLER, Robert P. (*A* 1944) Partner, • Kerr Machinery Co., 608 Kerr Bldg., Detroit 26, and 2061 Avon Lane, Birmingham, Mich.

BUTT, Roderick E. W. (*A* 1936; *J* 1930) Deputy Principal Tech. Officer, Petroleum Warfare Dept., London, and • 23 Warwick Sq., London, S.W. 1, England.

BUZZARD, Francis H. (*M* 1939) Chief Engr., • Charles S. Leopold, 213 S. Broad St., Philadelphia 7, Pa., and 624 Wood Lane, Haddonfield, N. J.

BYERLEY, Francis A., 3rd (*A* 1944) Chief Engr., Sun Chemical Corp., 2314 West Kinzie St., Chicago 12, and • 426 Surf St., Chicago, Ill.

BYERS, Robert L. (*M* 1942) Partner, • John Paul Jones, Cary & Millar, 1740 East 12th St., Cleveland 14, and 2261 Woodward Ave., Lakewood 7, Ohio.

BYRD, T. I. (*A* 1936) Sales Mgr., The Lau Blower Co., 2001-2029 Home Ave., Dayton 7, and • 2311 S. Sutphin St., Middletown, Ohio.

BYRNE, Joseph J. (*A* 1939) Htg. Engr., • Kleen-air Furnace Co., 5329 N.E. Sandy Blvd., and 6416 N.E. Rodney Ave., Portland, Ore.

BYRUM, Eli G., Jr. (*J* 1946) Engr., The Bahnson Co., 1001 S. Marshall St., and • 416 S. Sunset Dr., Winston-Salem, N. C.

BYSOM, Leslie L. (*M* 1938) Mech. Engr., Public Works Design Sec., Puget Sound Navy Yard, and • 1214 Eighth St., Bremerton, Wash.

C

CADENAS, Manuel A., Jr. (*J* 1945) Plant Engr., • U. S. Rubber Co., Ltd., Apartado 2582, Havana, and Calle 22, No. 61, Reparto Miramar, Marianao, Havana, Cuba.

CADY, Edward F. (*A* 1943; *J* 1937) Mech. Engr., The Austin Co., 16112 Euclid Ave., Cleveland, Ohio, and • 2242 E. Portland St., Phoenix, Ariz.

CAIL, Milton Leo (*J* 1945) Chief Engr., E. A. Berman Co., 268 Northampton St., Boston, and • 111 Atlantic Ave., Revere 51, Mass.

CAIN, James A. (*A* 1947) Div. Mgr., • A. M. Byers Co., 307 Mortgage Guarantee Bldg., and 3487 Ivey Rd. N.W., Atlanta, Ga.

CAIRNCROSS, George F. (*A* 1948) Pres., • Cowlitz Heating Co., 735 Commerce Ave., Longview, and 205 N. Pacific, Kelso, Wash.

CALCATERRA, Louis A. (*A* 1944) Sales Engr., and • 3538 Reed's Lake Blvd., Grand Rapids, Mich.

CALDWELL, Arthur C. (*M* 1930) Engr., L. S. Tarleton, 1500 Walnut St., Philadelphia 2, and • 550 South 48th St., Philadelphia 43, Pa.

CALDWELL, Robert J. S. (*M* 1941) Resident Engr., Thermaire (Pty.), Ltd., P. O. Box 1107, Port Elizabeth, South Africa.

CALDWELL, William C. (*M* 1948) Sales Mgr., Sheldons, Ltd., 97 Grand Ave. S., and • 16 McKenzie St., Galt Ont., Canada.

CALDWELL, W. J. (*A* 1945) Gen. Mgr., • William J. Caldwell Co., 1129 Vermont Ave. N.W., Washington 5, D. C., and 4508 Cheltenham Dr., Bethesda 14, Md.

CALEB, David (*M* 1923) Engr., • Kansas City Power & Light Co., 1330 Baltimore Ave., Kansas City 6, and 141 Spruce St., Kansas City 1, Mo.

CALHOON, Floyd N. (*M* 1942) Assoc. Prof. of Mech. Engrg., • University of Michigan, 237 W. Engineering Bldg., and 605 Oswego St., Ann Arbor, Mich.

CALL, Joseph (*M* 1938; *J* 1936) Vice-Pres., Elliott-Lewis Co., 2518 N. Broad St., Philadelphia 32, and • 50 Fairfield Rd., Havertown, Pa.

CALLAHAN, Peter J. (*M* 1934) Inspecting Engr., Central Hanover Bank & Trust Co., 60 Broadway, New York, N. Y., and • 3 Cubberly Pl., Jersey City, N. J.

CALLAHAN, Thomas H. (*M* 1943) Asst. Treas., • Callahan Equipment Co., Inc., 11 William St., and 101 Hillair Circle, White Plains, N. Y.

CALLAN, John J., Jr. (*A* 1943) Sales Mgr., Htg. Equipment Dept., • Claflin-Sumner Coal Co., 10 Franklin St., Worcester 8, and 15 Montague St., Worcester 3, Mass.

CALLAN, William D. (*A* 1944) Mgr., Careyduct Dept., The Philip Carey Manufacturing Co., Lockland, and • 2211 Lawn Ave., Norwood, Ohio.

CALLAWAY, James H. (*A* 1944) Htg. and Vent. Engr., Southern Blow Pipe & Roofing Co., 109 N. Highland Park Ave., Chattanooga, Tenn., and • Alpine Dr., Beverly Hills, Rossville, Ga.

CALLINS, Jack G. (*S* 1947) Student, Texas A. & M. College, Box 1590, College Station, and • 619 E. Cincinnati Ave., San Antonio, Texas.

CALLIS, Daniel K. (*A* 1946) Pipe Shop Foreman, Inland Steel Co., 3210 Watling St., East Chicago, and • 5339 Kent Ave., Hammond, Ind.

CALNAN, Daniel J. (*A* 1942) • Calnan Stoker Sales & Service, 453 McLean Ave., Yonkers 5, and 6 Homewood Ave., Yonkers 2, N. Y.

CALNAN, Edward J. (*M* 1941) Control Supt., • Ontario Paper Co., Ltd., Thorold, and 208 Russell Ave., St. Catherines, Ont., Canada.

CALONGNE, Henry J., Jr. (*A* 1944) Mech. Engr., • Emile M. Babst Co., 1050 Camp St., New Orleans 13, and 5810 Marshal Foch St., New Orleans 19, La.

CAMBRIDGE, W. A. (*A* 1944) Pres., • Reid & Cambridge, Ltd., 1223 Green Ave., Westmount, and 3577 Decarie Blvd., Montreal, Que., Canada.

CAMERON, Joseph A., Jr. (*A* 1944) Vice-Pres., N. Y. Office, • The Marley Co., Inc., 2 Rector St., New York 6, N. Y., and 34 Meadowbrook Rd., Short Hills, N. J.

CAMPAU, W. R. (*M* 1940) Gen. Mgr., Kendall Heating Co., 1636 N.W. Lovejoy St., Portland 9, Ore.

CAMPBELL, Bowen (*M* 1946) Pres., Campbell Heating Co., 3127 Dean Ave., and • 2404 East 29th St., Des Moines, Ia.

CAMPBELL, Everett K. (*Life Member*; *M* 1920), (Council, 1931-33; 1939-43; Treas., 1942-43), Pres., • E. K. Campbell Heating Co., 1809 Manchester Ave., Kansas City 3, and 5730 Paseo, Kansas City 4, Mo.

CAMPBELL, G. Courtney (*M* 1945) Sr. Partner, • Campbell-Elsey Co., 325-6 Ness Bldg., Salt Lake City 1, and 1444 Emerson Ave., Salt Lake City 5, Utah.

CAMPBELL, George Summers (*A* 1941; *J* 1937) Cons. Engr., • 411 Ochs Bldg., and 306 Sunnyside Dr., Chattanooga, Tenn.

CAMPBELL, George W. (*M* 1947; *A* 1946; *J* 1939) Engr., Urdahl & Everetts, Cons. Engrs., 734 Jackson Pl. N.W., Washington 6, and • 5306 Marlyn Dr., Washington 16, D. C.

CAMPBELL, Kirk (*M* 1944) Vice-Pres., • E. K. Campbell Heating Co., 1809 Manchester, Kansas City 3, and 6100 Harrison, Kansas City 4, Mo.

CAMPBELL, Ralph L. (*A* 1946) Htg. Engr., • Coast to Coast Stores, Central Organization, Inc., 29 S.E. Main St., Minneapolis, and 6617 Lake Shore Dr., Minneapolis 9, Minn.

CAMPBELL, Robert E. (*M* 1945) Atlantic Div. Mgr., Tyler Fixture Corp., Niles, Mich., and • 277 Larch Ave., Dumont, N. J.

CAMPBELL, Roger P. (*M* 1948; *J* 1939) Secy., • E. K. Campbell Heating Co., 1809 Manchester Ave., Kansas City 3, and 3605 Summit St., Kansas City 2, Mo.

CAMPBELL, Simon (*A* 1947) Designing Engr., Musgrave & Co., Ltd., St. Ann's Ironworks, and • "Kharakvasla", 78 Mt. Merrion Ave., Belfast, North Ireland.

CAMPIA, Oscar J. (*M* 1946) Cons. Engr. and Partner, • Hayden Harding & Buchanan, 662 Park Square Bldg., Boston 16, and 39 Warren Ave., Hyde Park 36, Mass.

CAMPION, Charles R. (*M* 1944) Partner, • Wrightson & Campion, 55 West 42nd St., New York 18, and 332 Bard Ave., Staten Island 10, N. Y.

CANDEE, Bertram C. (*M* 1933) Partner, Beman & Candee, 271 Delaware Ave., Buffalo 2, and • 19 Tremont Ave., Kenmore 17, N. Y.

CANNON, Vernon K. (*A* 1944) Gen. Mgr., • Winslow Furniture Co., 215 Kinsley Ave., and 417 W. Fourth St., Winslow, Ariz.

CANTERBURY, Howard M. (*A* 1945) Mfrs. Repr., Utility Fan Corp., 234 Cayton, Houston 12, Texas.

CANTWELL, Algernon B. (*A* 1945) Engr., Kansas City Coal Service Inst., 540 Dwight Bldg., Kansas City 6, and • 3614 Central Ave., Kansas City 2, Mo.

CAPLAN, Knowlton J. (*J* 1946) Vent. Engr., • Bureau of Industrial Health, Michigan Department of Health, Lansing 4, and 504 W. Lapeer, Lansing 15, Mich.

CAPPS, Edgar L. (*A* 1946) Pres., • E. L. Capps Assocs., Inc., P. O. Box 1915, Norfolk 1, and 619 Pennsylvania Ave., Norfolk 8, Va.

CAPRON, R. G. (*A* 1946) Technical Advisor, Indus. Burner Div., Svenska Oil-O-Matic A. B., Wahrendorffsgatan 8, and • Angskarsgatan 6, Stockholm, Sweden.

CARBONE, James H. (*M* 1937) Htg., Vent. Inspector, City of New York, Municipal Bldg., New York, and • 121-13-198th St., St. Albans, N. Y.

CARDENAL A., Luis G. (*J* 1947) Partner, • Cardenal-Lacayo Fiallos Cia. Ltda., Managua D. N., and Calle Colon, Managua D. N., Nicaragua, C. A.

CARDER, William W. (*A* 1944) Branch Mgr., • Johnson Service Co., 313 Bona Allen Bldg., Atlanta 3, and 677 Peeples St. S.W., Atlanta, Ga.

CARLE, William E. (*Life Member*; *M* 1926) Pres.-Treas., • Carle-Boehling Co., Ltd., 1641 W. Broad St., Richmond 20, and 4015 W. Franklin St., Richmond 21, Va.

CARLETON, Herbert G. (*A* 1944) Assoc. Mech. Engr., Maritime Commission, Dept. of Commerce Bldg., Washington, D. C., and • Box 143, College Park, Md.

CARLEY, Thomas S. (*A* 1945) Sales Mgr., Wholesale and Stoker Divs., • Minneapolis-Honeywell Regulator Co., 2747 Fourth Ave. S., Minneapolis, and 236 W. Franklin St., Minneapolis 4, Minn.

CARLOCK, Marion F. (*M* 1936) Mfrs. Agent, 1125 Locust St., St. Louis 1, and • 2003 Spanish Dr., St. Louis 17, Mo.

CARLSEN, Howard J. (*S* 1947) Student, Michigan College of Mining & Technology, 1405 College Ave., Houghton, and • 112 Sixth St., Gladstone, Mich.

CARLSON, Clarence J. (*A* 1944) Owner-Mgr., C. J. Carlson Co., 2701 Roosevelt Ave., Indianapolis, Ind.

CARLSON, C. O. (*A* 1937) Owner, • C. O. Carlson Heating Co., 1627 Washington Ave. N., and 3526 Humboldt Ave. N., Minneapolis, Minn.

CARLSON, E. Eugene (*A* 1946) Engr., B. F. Sturtevant Co., 89 Broad St., Boston, and • 9 Sutcliffe Ave., Canton, Mass.

CARLSON, Everett E. (*M* 1932; *A* 1929) • The Powers Regulator Co., 2118 Pine St., St. Louis 3, and 6675 Washington Ave., St. Louis 5, Mo.

CARLSON, Richard M. (*J* 1947) Engr., Pfeifer and Shultz, 702 Wesley Temple Bldg., Minneapolis 4, and • 3148 32nd Avenue S., Minneapolis 6, Minn.

CARNAHAN, John H. (*M* 1948; *A* 1940; *J* 1937) Mech. Engr., • Carnahan & Thompson, Engrs., 320 O.N.G. Bldg., Oklahoma City 2, and 3116 Northwest 26th St., Oklahoma City 7, Okla.

CARNS, Vernon J. (*A* 1945) Boyd Engineering Co., 718 N. Stanton, and • 3420 Louisville St., El Paso, Texas.

CAROFANO, Dominick A. (*M* 1947) Htg. Engr., Mfg. Coated Abrasives, and • 1821 Highland Ave., Troy, N. Y.

CARPENTER, R. H. (*M* 1921), (Council, 1930-35), Mgr., New York Office, • Nash Engineering Co., Graybar Bldg., 420 Lexington Ave., New York 17, and 20 Jefferson Ave., White Plains, N.Y.

CARRIER, Earl G. (*M* 1936; *J* 1929), (Council, 1946-47), Pres., Carrier-Mandell, Inc., 177 State St., Boston, and • 326 Highland Ave., Winchester, Mass.

CARRIER, Willis H. (*Honorary Member*; *Life Member*; *M* 1913), (*Presidential Member*), (Pres., 1931; 1st Vice-Pres., 1930; 2nd Vice-Pres., 1929), (Council, 1923-32), Chairman of the Board, • Carrier Corp., 300 S. Geddes St., Syracuse 1, and 2570 Valley Dr., Nedrow, N. Y.

CARROLL, Daniel E. (*A* 1941) Owner, Carroll Sheet Metal Works, Inc., 46-10-70th St., Woodside, and • 216-09-40th Ave., Bayside, N. Y.

CARROLL, Edgar E. (*A* 1939) Owner, Partner, • Kleenair Furnace Co., 5329 N.E. Sandy Blvd., and 2434 Northeast 43rd Ave., Portland 13, Ore.

CARROLL, John R., Jr. (*J* 1947; *S* 1946) Instructor, • University of Illinois, 103 M. E. Lab., Urbana, and 708 S. First, Champaign, Ill.

CARROLL, William M. (*A* 1943; *J* 1938) Gen. Mgr., Macklanburg Supply Co., 129-133 Northwest 23rd, Oklahoma City, Okla.

CARSEY, E. A. (*M* 1944) Asst. Chief Engr., • The Kirk & Blum Mfg. Co., 2838 Spring Grove Ave., Cincinnati 25, and 359 Howell Ave., Cincinnati 20, Ohio.

CARSON, C. C. (*M* 1943) Equip. Dvlpt. and Design, Sec. 638, U. S. Navy Dept., Washington, and • 6753 Potomac Dr. N.W., Washington 16, D. C.

CARSON, James H. (*A* 1946) Owner, • Carson Pacific Boiler Service, 536 East 172nd St., Bronx 57, and 315 East 167th St., Bronx 56, N. Y.

CARTER, Addison B. (*A* 1946) Pres-Treas., • Farwell Co., Inc., Buckner Blvd., Dallas 10, and 2942 Linfield Dr., Dallas, Texas.

CARTER, A. W. (*M* 1940; *J* 1936) • Michael Stuart Co., Ltd., 116 Bloor St. West, Toronto, and Box 72, Stouffville, Ont., Canada.

CARTER, Chester A. (*M* 1944) Chief of Mech. Section, Military Branch of Engrg. Div., District Engineer Office, and • 2014 Emmet St., Omaha, Nebr.

CARTER, D. (*M* 1934) Cons. Engr., P. O. Box 614, Hongkong, China.

CARTER, Donald G. (*S* 1946) Student, Washington University, St. Louis, and • 139 Reavis Pl., Webster Groves 19, Mo.

CARTER, Henry G. (*A* 1944) Mfrs. Agt., 5505 Branch Ave., Tampa 4, Fla.

CARTER, John H.* (*M* 1936) Partner, • Bodine & Carter, 122 W. Lockwood Ave., and 139 Reavis Pl., Webster Groves 19, Mo.

CARTIER, Marcel E. (*M* 1944) Research Engr., American Radiator & Standard Sanitary Corp., Cie Nationale des Radiateurs, 149 Boulevard Haussmann, Paris, France.

CARTWRIGHT, Stewart E. (*S* 1946) Student, Texas A. & M. College, Box 1464, College Station, and • Oleander Homes, Apt. 2-B, Galveston, Texas.

CARY, Edward B. (*M* 1935) Partner, • John Paul Jones, Cary & Millar, 1740 East 12th St., Cleveland 14, and 3074 Livinstone Rd., Shaker Heights, Ohio.

CASE, Delbert V. (*M* 1937) Mgr., • Natural Cooler Storage, U. S. D. A., P. O. Box 476, and 1106 Kansas Ave., Atchison, Kans.

CASE, Delbert V., Jr. (*A* 1947) Mech. Engr., • J. Gordon Turnbull, Inc., 4300 New Haven Rd., and 819 E. Wayne, Ft. Wayne, Ind.

CASE, Donald P. (*A* 1944) Engr., • Mac Callum Steel Corp., 216 E. Almond St., Compton, and 3814 Agnes, Lynwood, Calif.

CASE, Walter G. (*A* 1930) Mgr., Ideal Boilers & Radiators, Ltd., Ideal House, Great Marlborough St., London, W. 1, and • 66 The Ridgeway, Kenton, Harrow, Middlesex, England.

CASEY, Byron L. (*M* 1921) Dist. Mgr., • Ilg Electric Ventilating Co., 222 N. LaSalle St., Chicago 1, and 404 Vine Ave., Park Ridge, Ill.

CASEY, John J. (*A* 1947) Mgr., Plbg. & Htg. Dept., • Dealers Service & Supply Co., 8440 St. Charles Rock Rd., St. Louis 14, and 3532 St. Lukes Lane, Overland 14, Mo.

CASHIN, William K. (*M* 1946) Vice-Pres., • W. D. Cashin Co., 69 "A" St., Boston 27, and West Falmouth, Mass.

CASKEY, Luther H., Jr. (*A* 1948; *J* 1941; *S* 1938) Gen. Mgr., L. H. Caskey, • 225 N. Queen St., and 401 West Martin St., Martinsburg, W. Va.

CASKEY, Thomas C. (*M* 1943) Owner, Caskey Engineering Co., 1736 First Ave. S., Seattle 4, and • 11642-26th Ave. S., Seattle 88, Wash.

CASPERD, Henry W. H. (*A* 1947) Mech. Engr., • Foundation Co. of Ontario, Ltd., 1220 Bay St., and 483 Briar Hill Ave., Toronto, Ont., Canada.

CASSELL, William L. (*M* 1936) Principal, • William L. Cassell, 912 Baltimore Ave., Kansas City, and R. F. D. No. 6, Independence, Mo.

CASTROW, Otto E. (*A* 1947) Estimator, Asbestos Supply Co., Portland, and • 8305 S.W. Birchwood Rd., Portland 1, Ore.

CATLETT, W. A. (*A* 1943) Owner, • Catlett Engr., 9020 Garland Rd., and 9602 El Patio Dr., Dallas 18, Texas.

CATON, Ross R., Jr. (*J* 1945) Pres., Caton Supply Co., 828 W. Vernor Highway, Detroit 1, and • 15395 Linwood, Detroit 21, Mich.

CAUGHMAN, Richard B. (*J* 1947) Airtemp Engr., Export Div., • Chrysler Corp., Box 1688, Detroit 31, and 1446 Montclair Ave., Detroit 14, Mich.

CAUHORN, A. V. (*A* 1943) Owner, • A. V. Cauhorn Co., 10001 Broadstreet, and 12660 Montevista, Detroit 4, Mich.

CAVANAGH, P. A. (*M* 1944) Mgr., • The Herman Nelson Corp., 1015 Chestnut St., Philadelphia 7, and 15 Runnemede Ave., Lansdowne, Pa.

CAZIN, Gerald (*A* 1945) Piping & Air Cond. Contr., Cazin & Houtz, 928 Main St., and • 1013 Lombard St., Evanston, Wyo.

CHADWICK, George R. (*M* 1945) American Heating & Piping Co., 130 E. Elm St., Lima, Ohio.

CHADWICK, John B. (*M* 1944) Tech. Engrg. Repr., Textile Air Systems, Ltd., Bury Road Works, Radcliffe, and • 11 Orville Dr., Levenshulme, Manchester 19, Lancashire, England.

CHALMERS, C. H. (*Life Member*; *M* 1938) Gen. Mgr., • Chalmers Oil Burner Co., 318 First Ave. N., Minneapolis 1, and 523 Seventh St. S.E., Minneapolis 14, Minn.

CHAMBERS, Fred W. (*M* 1936) Pres., • F. W. Chambers & Co., Ltd., 1650 Yonge St., and 55 Glengowan Rd., Toronto 12, Ont., Canada.

CHAMBERS, S. A. (*M* 1944) Vice-Pres. and Secy., • Almirall & Co., Inc., 53 Park Pl., New York 7, N. Y., and 81 Ross Ave., Hackensack, N. J.

CHAMPAGNE, Alex (*A* 1946) Owner, O. Champagne & Fils, 1478 City Hall Ave., Montreal, and • 3170 Tremblay, Montreal 26, Que., Canada.

CHAMPLIN, Robert C. (*M* 1945; *A* 1938) Dist. Mgr., Richmond Radiator Co., 2461 Guardian Bldg., Detroit 26, and • 13640 Mendota Ave., Detroit 4, Mich.

CHANDLER, Roy (*A* 1944) Exporter of Air Conditioning Equipment, R. Chandler Co., P. O. Box 591, Grand Central Annex, New York, N. Y.

CHAPIN, C. Graham (*M* 1933) Treas., • Hopson & Chapin Manufacturing Co., 231 State St., and 66 Faire Harbour Pl., New London, Conn.

CHAPIN, Harvey G. (*M* 1935) • Westerlin & Campbell Co., 185 N. Wabash Ave., Chicago 1, and 8352 Maryland Ave., Chicago, Ill.

CHAPMAN, D. Bascom (*M* 1941) Dist. Office, • Clarage Fan Co., 323 Curtis Bldg., 2842 W. Grand Blvd., Detroit 2, and 16713 Blackstone, Detroit 19, Mich.

CHAPMAN, William A., Jr. (*M* 1936) Realtor, and • Auhay Dr. & Arroyo Rd., Santa Barbara, Calif.

CHAPMAN, William P. (*J* 1947) Engr., Prod. Engrg. Dept., National Tube Co., Frick Bldg., Pittsburgh 19, and • P. O. Box 73, Pittsburgh 30, Pa.

CHAPPELL, Henry D. (*M* 1942) Mech. and Elec. Engr., • Burroughs Adding Machine Co., 6071 Second Ave., Detroit 32, and 15493 Whitcomb Ave., Detroit 27, Mich.

CHAR, Raghav D. (*M* 1945) Owner, • Industrial & Agricultural Engineering Co., 43 Forbes St., Bombay 1, and "Villa Vyla" 17th Rd., Khar, Bombay 21, India.

CHARLES, Paul L. (*M* 1938) Mgr. and Sole Owner, • Walsh & Charles, Ltd., 206 Tribune Bldg., and 145 Ash St., Winnipeg, Canada.

CHASE, Arthur M., Jr. (*M* 1938) Owner, • Production Equipment Co., P. O. Box 895 (2804 Leeland Ave.), Houston 1, and 3333 Ozark St., Houston 4, Texas.

CHASE, Chauncey L. (*M* 1931) Cons. Engr., • 15 William St., New York 5, and 222 Chapel Rd., Manhasset, L. I., N. Y.

CHASE, Jim C. (*J* 1945) Dist. Mgr., • Aerofin Corp., 603 Great National Life Bldg., Dallas 1, and 7047 Coronada, Dallas 14, Texas.

CHASE, R. E., Jr. (*A* 1946; *J* 1941) T.W.A., Inc., 353 West 57th St., New York, N. Y.

CHASE, Roger E., Sr. (*M* 1946; *A* 1939) Pres., • R. E. Chase & Co., Inc., Tacoma Bldg., Tacoma 2, and 117 N. Tacoma Ave., Tacoma 3, Wash.

CHATFIELD, Arthur J. (*M* 1943) Engr., Messrs. John Lewis Properties, Ltd., Architects & Engineers Office, 70 Wigmore St., London, W. 1., and • 29 Woodside Rd., Malden, Surrey, England.

CHAUVIN, Jean-Paul (*A* 1948) Mgr., • Sorel Mill & Builders Supply Ltd., 20 Prince St., Sorel, P. Q., and 1504 Darling St., Montreal, P. Q., Canada.

CHEASLEY, Thos. C. (*M* 1943) Fuel Engr., • Sinclair Coal Co. & Affiliates, 114 West 11th St., Kansas City 6, and 437 East 72nd St., Kansas City 5, Mo.

CHEATWOOD, William H. (*A* 1948) Mgr. Refrig. Dept., Interstate Elec. Co. of Shreveport, Inc., and • R. F. D. 1, Box 194A, Houghton, La.

CHEESEMAN, Evans W. (*A* 1946; *J* 1937; *S* 1934) Asst. Engr., Perfection Stove Co., 7609 Platt Ave., Cleveland 4, and • 1555 Rosewood, Lakewood 7, Ohio.

CHENEVERT, J. Georges (*M* 1938) Cons. Engr., • Surveyer, Nenniger & Chenevert, 1010 St. Catherine St. W., Dominion Sq. Bldg., Room 1203 Montreal, and 536 Outremont Ave., Outremont, Que., Canada.

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CHERRY, Lester A.* (*M* 1921) Cons. Engr., Cherry, Cushing & Preble, 361 Delaware Ave., Buffalo 2, and 151 Euclid Ave., Kenmore 17, N. Y.

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CHESTER, F. L.* (*A* 1940) Mgr., • W. G. Chester & Son, 222 Bannatyne Ave., and 26.C. Panama Ct., Winnipeg, Man., Canada.

CHESTER, Thomas* (*Life Member*; *M* 1917) Cons. Engr., 370 Townsend St., Birmingham, Mich.

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CHIDESTER, Charles W. (*A* 1946) 1251 West 41st Pl., Los Angeles 37, Calif.

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CHINN, George I. (*M* 1947) Chief Engr., • Gerotor May Corp., P. O. Box 86, Baltimore 3, and 3407 Woodbrook Ave., Baltimore 17, Md.

CHIPMAN, Edward E. (*J* 1948; *S* 1943) Mgr., Plbg. & Htg. Dept., Crane Co., 40-24th St., Pittsburgh, and • 1536 Bellaire Pl., Pittsburgh 26, Pa.

CHOATE, James E. (*M* 1945) Mgr., Choate Supply Co., Box 192, Rogers, Ark.

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CHRISTENSON, Harry (*A* 1931) Partner, • Hunter-Prell Co., 15-19 E. Jackson St., and 121 Sunset Blvd., Battle Creek, Mich.

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CHUR, Robert R. (*A* 1946) Mgr., • W. A. Case & Son Manufacturing Co., 115 N. Geddes St., Syracuse, and 2 N. Pebble Hill Dr., Dewitt, N. Y.

CHURCH, H. J. (*M* 1922) Mgr., • Darling Bros., Ltd., 137 Wellington St. W., Room 902, Toronto 2, and 358 Main St. N., Weston, Ont., Canada.

CHURCH, Lloyd M. (*M* 1943) Dist. Mgr., • Carrier Corp., 12 South 12th St., Philadelphia 7, and 21 E. Levering Mill Rd., Bala-Cynwyd, Pa.

CHURCH, Richard A. (*J* 1945) Engr., Carrier Corp., 12 South 12th St., Philadelphia 7, and • 4404 Cottman Ave., Philadelphia 35, Pa.

CHYTRAUS, Oscar E. (*A* 1945) Owner, Oscar E. Chytraus Co., 328 W. Second S., and • 1173 South 11th E., Salt Lake City, Utah.

CILACIYAN, Ara (*S* 1947) Grad. Student, University of Minnesota, and • 512 Ontario St. S.E., Minneapolis 14, Minn.

CLAPPERTON, Robert (*M* 1946; *J* 1942) Mech. Asst. to Chief Archt., Canadian National Railways, 355 McGill St., Room 703, Montreal, and • 25 Roosevelt Ave., Town of Mt. Royal, Que., Canada.

CLAPPERTON, T. Clyde (*M* 1944) Vice-Pres., • Michael Stuart Co., Ltd., 116 Bloor St. W., and 68 The Kingsway, Toronto, Ont., Canada.

CLAR, Robert, Jr. (*M* 1947) Htg. & Piping Engr., Murray W. Sales & Co., 801 W. Baltimore, Detroit, and • 16636 Washburn, Detroit 21, Mich.

CLARE, Fulton W. (*M* 1927) Mech. Engr., U. S. Division Engineer, 50 Whitehall St., and • 935 Plymouth Rd. N.E., Atlanta, Ga.

CLARK, Albert C. (*A* 1939) 7129 N. Campbell, Portland 3, Ore.

CLARK, Allan M. (*M* 1945; *J* 1942) Joint Mgr., • Canadian Blower & Forge Co., Ltd., Room 301, 1221 Bay St., Toronto 5, and 11 Langton Ave., Toronto 12, Ont., Canada.

CLARK, Andrew M. (*A* 1946) Mgr., Htg. Div., James Morrison Brass Manufacturing Co., Ltd., 276-8 King St. W., and • 160 Douglas Ave., Toronto, Ont., Canada.

CLARK, Arthur E. (*A* 1945) Engr., • Grinnell Company of Canada, Ltd., 2440 Dundas St. W., and 49 Mountview Ave., Toronto 9, Ont.. Canada.

CLARK, Dwight L. (*A* 1945) Sheet Metal Worker, and Air Cond. Teacher, Puget Sound Naval Shipyard, and • 10 Schley Blvd., Bremerton, Wash.

CLARK, E. Harold (*M* 1936) Mfr's. Agent, • 600 Michigan Theatre Bldg., Detroit 26, and 2539 Lakewood, Detroit 15, Mich.

CLARK, H. G., Jr. (*A* 1946) Partner, • Catlett Engineers, 9020 Garland Rd., and 9606 El Patio Dr., Dallas 18, Texas.

CLARK, James R. (*A* 1948; *J* 1942) • Page & Co., 1001 N. Church St., and 1501 Pecan Ave., Charlotte 4, N. C.

CLARK, Joe R. (*S* 1947) Student, Texas A. & M. College, and • Box 5663, College Station, Texas.

CLARK, John W. (*S* 1948) Student, University of Michigan, and 405 Forest, Ann Arbor, Mich.

CLARK, L. O. Ray (*M* 1944) Dist. Engr., Westinghouse Electric Corp., Sturtevant Div., 36 Pearl St., Hartford 3, and • 230 Farmington Ave., Hartford, Conn.

CLARK, Lynn W. (*M* 1944; *A* 1938) Sales Engr., • Hall-Neal Furnace Co., 1324 N. Capitol Ave., and 737 West 32nd St., Indianapolis, Ind.

CLARK, Robert John (*A* 1944) Partner, • Clark Equipment Co., P. O. Box 989, and 1457 E. Cleveland St., Clearwater, Fla.

CLARK, Robert L. (*A* 1939) Pres., The Clark Asbestos Co., 1893 East 55th St., Cleveland 3, and • 927 Caledonia Ave., East Cleveland 12, Ohio.

CLARK, Royal J. (*A* 1948) Estimator, • The B. A. Walterman Co., 210 W. McMicken Ave., Cincinnati 14, Ohio, and 239 Upland Ave., South Hills, Covington, Ky.

CLARKE, John H. (*M* 1942; *A* 1941) Design Engr., Standard Oil Co., Whiting, Ind., and • 18458 Roy St., Lansing, Ill.

CLARKE, Joseph L. (*M* 1946) Owner, • Clarke Bros., 42 Jackson Pl., and 1433 N. Pennsylvania St., Indianapolis, Ind.

CLARKE, William L. (*A* 1948) Repr., • T. L. Osberger Co., 1001 Michigan Trust Bldg., and 309 Paris Ave. S.E., Grand Rapids, Mich.

CLARKSON, Robert C., Jr. (*M* 1943) Cons. Engr., 1006 Edmonds Ave., Drexel Hill, Pa.

CLAY, Wharton (*M* 1939; *A* 1938) Secy., • National Mineral Wool Assn., 1270 Sixth Ave., Room 2906, New York 20, and 127 S. Broadway, Nyack, N. Y.

CLAY, Wilton L. (*J* 1948) Sales Engr., • Gulf Engineering Co., 916 South Peters, and 1319 Amelia St., New Orleans, La.

CLEGG, Carl (*M* 1922) Dist. Mgr., • American Blower Corp., 550 Dwight Bldg., and 3513 Gillham, Kansas City 6, Mo.

CLEGG, Eugene (*A* 1947) Estimator, H. G. McGill & Sons, and • 1401 McDougal Ave., Phenix City, Ala.

CLEMENS, J. Edward (*M* 1944) Engr. in charge of Design, Plant Engrg. Dept., Allison Div. of General Motors Corp., Plant No. 5, P. O. Box 894, Indianapolis 6, and • 2625 N. Meridian St., Indianapolis 5, Ind.

CLEMENS, Joseph D. (*J* 1942; *S* 1940) 717 Colfax Ave., Vancouver, B. C., Canada.

CLEMENT, Eugene R., Sr. (*A* 1942) Pres., • E. R. Clement, Inc., Box 2461, Noble Station, Bridgeport, Conn.

CLEMINS, Richard J. (*J* 1945) Air Cond. Engr., Coolidge Locher Co., 224 S. Staples St., Corpus Christi, Texas.

CLIFFORD, Leslie F. (*A* 1946) Office Engr., Association of American Railroads, 59 E. Van Buren, Chicago 5, and • 1306 W. North Ave., Chicago 22, Ill.

CLIFTON, John A. (*A* 1938) Mgr., • Renown Plumbing Supplies, Ltd., 236 Parliament St., and 369 Belsize Dr., Toronto, Ont., Canada.

CLINE, Carl C. (*A* 1947) Owner, • Southern Refrigeration Co., 2609 Elm St., and 3855 Mt. Royal, Dallas, Texas.

CLO, Harry E. (*A* 1943; *J* 1939) Engr., • American Air Filter Co., 228 N. LaSalle St., Chicago 1, and 2747 West 108th St., Chicago 43, Ill.

CLOSE, James W. (*A* 1944) Pres., Sheet Metal Workers Union 620 S. Ashland Blvd., Chicago, and • 6114 N. Washtenaw Ave., Chicago 45, Ill.

CLOSE, Paul D.* (*M* 1928) Tech. Advisor, • Simpson Industries, 1065 Stuart Bldg., Seattle 1, and 5656 Keswick Dr., Seattle, Wash.

CLOW, Sherwood A. (*A* 1947; *J* 1942) 109 N. Chatsworth Ave., Larchmont, N. Y.

CLUCAS, Edward T. (*M* 1944) Appl. Engr., Minneapolis-Honeywell Regulator Co., 4030 Chouteau Ave., St. Louis 10, and • 1629 McLaren Ave., St. Louis, Mo.

COAD, J. Dennis (*A* 1943) Service Engr., • D. C. Air Conditioning Service Co., 1125 Locust St., St. Louis 1, and 6439 Lloyd Ave., St. Louis 10, Mo.

COBURN, Joseph B. V. (*M* 1944) Combustion and Service Engr., International Chimney Corp., Curtis Bldg., Buffalo, and ● 1459 Wehrle Dr., Williamsville 21, N. Y.

COCHRAN, L. D. (*A* 1945) Pres., ● The L. D. Cochran Co., Box 142, Washingtonville, and 3447 Logan Rd., Youngstown, Ohio.

COCHRAN, L. H. (*M* 1934) Dist. Mgr., ● American Blower Corp., 625 Market St., San Francisco 5, and 130 Camino Del Mar, San Francisco, Calif.

COCHRANE, Richard L. (*J* 1946) Engrg. Draftsman (Heating), ● The James Robertson Co., Ltd., 215 Spadina Ave., and 120 MacPherson Ave., Toronto, Ont., Canada.

COCHRANE, William (*A* 1944) Air Cond. Engr., Federal Shipbuilding & Drydock Co., Lincoln Highway, Kearney, and ● 91 Beech St., Arlington, N. J.

COCKINS, William W. (*A* 1941; *J* 1937) Partner, Scott Co., 243 Minna St., San Francisco 3, and ● 744 Grizzly Peak Blvd., Berkeley 8, Calif.

COCKLEY, Jonathan E. (*M* 1943) Air Cond. Engr., ● Indiana Gas & Water Co., Inc., 1630 N. Meridian St., and 3463 N. Sherman Dr., Indianapolis, Ind.

COCKMAN, T. E. (*A* 1945) Resident Mgr., ● B. F. Sturtevant Co. of Canada, Ltd., 620 Cathcart St., 553 New Birks Bldg., and 4823 Patricia Ave., Montreal, Que., Canada.

CODDINGTON, Bert A. (*J* 1948) Draftsman, ● The Coddington Co., 355 Stockton St., San Francisco, and 73 Winship, San Anselmo, Calif.

CODDINGTON, Dwight A. (*A* 1948) Specification Writer, ● The Coddington Co., 355 Stockton St., San Francisco, and 73 Winship Ave., San Anselmo, Calif.

CODERE, Jean-Moise (*A* 1944) Dir., Codere, Ltd., 18 Wellington N., Sherbrooke, Que., Canada.

CODY, Henry C. (*M* 1936) Sales Engr., Herman Goldner Co., Inc., 425 W. Lehigh Ave., Philadelphia 33, and ● 7336 North 21st St., Philadelphia 38, Pa.

COFFEY, George B. (*A* 1945) Chicago Div. Mgr., ● A. M. Byers Co., 135 S. LaSalle St., Chicago 3, and 2311 West 111th St., Chicago 43, Ill.

COGHLAN, Sherman F. (*A* 1937) Pres., J. M. Montgomery & Co., Inc., 306 W. Third St., Los Angeles, and ● 414 Ninth St., Santa Monica, Calif.

COHAGEN, Chandler C. (*M* 1919) Archt., ● 212 Hedden Bldg., and 235 Avenue G, Billings, Mont.

COHEN, Philip (*M* 1932) Mgr., ● Westinghouse Electric Corp., Sturtevant Div., 933 Leader Bldg., Cleveland 14, and 12805 Shaker Blvd., Apt. 511, Cleveland 20, Ohio.

COHEN, Seymour A. (*J* 1944; *S* 1942) Engr., Samuel Cohen, Inc., 44-52 Waverly St., New Haven 11, and ● 54 Waverly St., New Haven, Conn.

COHEN, William P. (*S* 1947) Student, ● Carnegie Inst. of Technology, 5931 Walnut St., Pittsburgh 6, Pa., and 261 S. Maple Dr., Beverly Hills, Calif.

COHN, Henry (*J* 1942) Pres., Cohn-Daniel Corp., 3027 Taylor St., and ● 4502 Kelton Dr., Dallas, Texas.

COLAS, Nicholas A. (*J* 1948; *S* 1946) Student Engr., Farrel-Birmingham Co., and ● P. O. Box 132, Ansonia, Conn.

COLBURN, Gerald W. (*A* 1946) Dist. Mgr., ● Minneapolis-Honeywell Regulator Co., 106 North 15th St., Omaha 2, and 2865 Ida, Omaha, Nebr.

COLBY, John H. (*A* 1944; *J* 1939) ● 20 Winchester St., Boston and 25 Jefferson Rd., Wellesley Hills, Mass.

COLBY, John R. (*A* 1944) Owner, ● Colby Equipment Co., 314 E. New York St., Indianapolis 4, and 5514 Rosslyn Ave., Indianapolis, Ind.

COLBY, John W. (*J* 1946) Secy.-Treas., The Colton Corp., 72-74 Main St., and ● P. O. Box 268, Whitewater, Wis.

COLCLOUGH, Otho T. (*A* 1933) ● American Embassy, and 399 Hamilton Ave., Ottawa, Ont., Canada.

COLE, C. Boynton (*M* 1940; *J* 1937) Owner, ● Boynton Cole, Contracting Engr., Htg. & Vtg., 1875 Piedmont Rd. N.E., and 1843 Flagler Ave. N.E., Atlanta, Ga.

COLE, Grant E. (*A* 1925) Exec. Vice-Pres. and Gen. Mgr., ● Trane Co. of Canada, Ltd., 4 Mowat Ave., Toronto, Ont., Canada.

COLE, Harold S. (*M* 1944) Engr., Stone & Webster Engineering Corp., 49 Federal St., Boston 7, and ● 1960 Commonwealth Ave., Boston 35, Mass.

COLE, Victor (*J* 1945) Engr., Carrier Corp., 405 Lexington Ave., New York 17, and ● 1555 Grand Concourse, New York 52, N. Y.

COLEMAN, James L., Jr. (*A* 1946) Vice-Pres. and Secy., ● Sauer, Inc., 2701 East St., and 2707 Norwood Ave., Pittsburgh 14, Pa.

COLEMAN, John B. (*M* 1920) Chief Engr., ● Grinnell Corp., 260 W. Exchange St., P. O. Box 1435, Providence 1, and 124 Camp St., Providence 8, R. I.

COLFORD, John (*A* 1937) Pres., ● John Colford, Ltd., 2007 Guy St., Montreal 25, and 51 Upper Bellevue Ave., Westmount, Que., Canada.

COLLE, S. S. (*A* 1938) Owner & Engr., Air Conditioning Engineering Co., 79 Vitre St. W., Montreal 1, and 4968 Fulton Ave., Montreal, Que., Canada.

COLLETTE, John R. (*A* 1947) Mgr., Field Sales, ● Fitzgibbons Boiler Co., Inc., 101 Park Ave., New York 17, and Over Look Rd. N., White Plains, N. Y.

COLLIER, J. Robert (*A* 1945) Mfrs. Repr., Taco Heaters, Inc., and ● 4808 Pleasant Ave., Minneapolis 9, Minn.

COLLIER, William I. (*M* 1921) ● W. I. Collier & Co., 3414 Duvall Ave., Baltimore 16, and Ellicott St., Ellicott City, Md.

COLLINS, Desmond M. (*M* 1948) Bldg. Serv. Engr., Stone & Webster Engineering Corp., 49 Federal St., Boston, and ● 125 Blue Hills Pkwy., Milton, Mass.

COLLINS, Edward E. (*M* 1946) Engr., ● Bramwell Construction Co., 560 Mission St., San Francisco 5, and 6417 Colton Blvd., Oakland 11, Calif.

COLLINS, George J. (*A* 1945) Pres., ● Texas Mechanical Co., P. O. Box 2463, and 529 Fraser St., Houston, Texas.

COLLINS, Jerome (*S* 1948) Student, Purdue University, Lafayette, and ● 109 W. Fourth, Huntingburg, Ind.

COLLINS, John F. S., Jr. (*M* 1933), (Treas., 1946-47; Council, 1940-47), Secy.-Treas., National District Heating Assn., 827 N. Euclid Ave., Pittsburgh 6, Pa.

COLLINS, John W. (*M* 1946) 51 Woodmount Ave., Toronto, Ont., Canada.

COLLINS, Joseph A. (*M* 1943) Mgr., ● Frontier Oil Refining Corp., Oil Burner Div., 367 Northampton St., and 289 Commonwealth Ave., Buffalo, N. Y.

COLLINS, Leo F.* (*M* 1941) Chem. Engr., The Detroit Edison Co., Detroit 26, Mich.

COLLINS, William A., Jr. (*J* 1948; *S* 1947) Industrial Engr., Lone Star Gas Co., Box 342, Denison, and ● 1124 N. Hurt St., Sherman, Texas.

COLEMAN, Robert C. (*A* 1940) Vice-Pres., McQuay, Inc., 1600 Broadway N.E., Minneapolis 13, and ● 102 Exeter Pl., St. Paul 4, Minn.

COLMENARES, Gaspar Vizoso (*A* 1938) Vice-Pres. and Gen. Mgr., ● Refrigeracion y Aires Acondicionado, S. A., Lamparilla No. 9, Habana, and Calle 9, entre 6 y Ave. R. Mendoza, Alturas de Miramar, Habana, Cuba.

COLOMBO, Joseph D. (*J* 1946) Engrg. Draftsman, Consolidated Conditioning Corp., 26 West 47th St., New York, and ● 4534 Carpenter Ave., Bronx 66, N. Y.

COLP, John L. (*J* 1948) Gen. Mgr., ● Home Equipment & Supply Co., 306 S. Division St., and R. R. 2, Carterville, Ill.

COLTON, Frederick R. (*M* 1945) Branch Mgr., ● Norris Warming Co., 94 Exchange Bldgs., New St., Birmingham, and 36 Palace Rd., Flat 12, London S.W. 2, England.

COLVIN, Oliver Dyer (*M* 1943) Pres., Cargocaire Engineering Corp., 15 Park Row, New York, N. Y.

COMBS, Charles F. (*A* 1946) Sales Engr. & Vice-Pres., Russell J. Smith, Inc., 1601 S. Grand Blvd., St. Louis 4, and ● 3531 Cambridge, St. Louis 17, Mo.

COMPTON, Basil C. (*A* 1946) Sales Engr., D. C. Air Conditioning Co., 1125 Locust St., St. Louis, and ● 5948 Victoria, St. Louis 10, Mo.

COMSTOCK, Glen M. (*A* 1926) Professional Engr., ● Comstock, Campbell & Edwards, 1610 Investment Bldg., Pittsburgh 22, and 1319 Murdoch Rd., Pittsburgh 17, Pa.

CONATY, Bernard M. (*M* 1935) Mfrs. Repr., • 505 Crosby Bldg., Buffalo 2, and P. O. Box 342, Jennings Rd., Eden, N. Y.

CONGER, Henry L. (*M* 1943) Chief Utilities Branch, U. S. Engr. Dept., Box 2240, Honolulu, and • 1550 H- Young St., Honolulu 19, T. H.

CONNELL, E. C. (*M* 1944) Htg. Engr., Sullivan Valve & Engineering Co., 2932 E. Trent, Box 2208, Spokane, and • 415 N. Raymond St., Rt. 1, Opportunity, Wash.

CONNELL, Lloyd L. (*M* 1946) Tech. Dir., • Stoker Manufacturer's Assn., 307 N. Michigan Ave., Chicago 1, and 3026 Hickory Rd., Homewood, Ill.

CONNELL, Maurice H. (*M* 1945) Sr. Partner, • Maurice H. Connell & Assoc., Langford Bldg., 2nd Floor, Miami 32, and 1101 N. Greenway Dr., Coral Gables, Fla.

CONNELL, Richard F. (*M* 1916) Mgr., Sales Engrg., • U. S. Radiator Corp., 300 Buhl Bldg., Detroit 31, and 2970 Burlingame, Detroit, Mich.

CONNER, R. M. (*M* 1931) Dir. Labs., • American Gas Association Laboratories, 1032 East 62nd St., Cleveland 14, and 2551 Charney Rd., Cleveland, Ohio.

CONNOR, William A. (*A* 1946) Service Engr., Page-Hersey Tubes, Ltd., 100 Church St., Toronto, and • 301 Kingswood Rd., Toronto 13, Ont., Canada.

CONNORS, Edward C. (*A* 1940) Engr. Custodian, Chicago Board of Education, 5500 Madison St., and • 6556 Ponchartrain Blvd., Chicago 30, Ill.

CONNORS, Francis E. (*S* 1948) Student, David Ranken Jr. School of Mechanical Trades, St. Louis, Mo., and • R. R. No. 3, Vandalia, Ill.

CONOVER, Donald Davis (*A* 1944) Mgr., A. W. Culin Co., 29 S. Third St., Harrisburg, and • 430 Manoa Rd., Havertown, Pa.

CONOVER, E. W. (*M* 1944) Research Engr., Detroit Steel Products Co., 2250 E. Grand Blvd., Detroit 11, Mich.

CONRAD, Alton F., Jr. (*A* 1947) Sales Engr., • AveryEngineering Co., 1906 Euclid Ave., Cleveland 15, and 3257 East 103rd St., Cleveland 4, Ohio.

CONRAD, Roy (*M* 1935) 975 Wilshire Blvd., Los Angeles 14, Calif.

CONROY, W. T. (*A* 1944) Htg. and Plbg. Contr., • 1525 Locust St., and 1810 East 78th St., Kansas City, Mo.

CONSTANT, Earl S. (*A* 1942; *J* 1935) Sales Engr., Arthur Forsyth Co., 3150 Elliot Ave., Seattle 1, and • 3015-30th Ave. W., Seattle 99, Wash.

CONVERSE, Thornton J. (*M* 1941) Engr., • Douglas Orr, Archt., 96 Grove St., New Haven, and Stony Creek, Conn.

CONWAY, Frank J. (*A* 1947) Vice-Pres., • W. J. Gemeny Co., 2528 W. Madison, Chicago, and 643 Ontario St., Oak Park, Ill.

CONWAY, Richard W. (*M* 1946) Sales Engr., The H. B. Smith Co., Inc., 331 Madison Ave., New York 17, and • 172 Voorhis Ave., Rockville Centre, L. I., N. Y.

COOGAN, John T. (*M* 1946) Chief Engr., Mellish & Murray Co., 1715 Carroll Ave., Chicago 12, and • 3024 N. Sacramento Ave., Chicago 18, Ill.

COOK, Benjamin F. (*M* 1945) Cons. Engr., • 812 Midland Bldg., 1221 Baltimore Ave., Kansas City 6, and 1720 Overton Ave., Independence, Mo.

COOK, H. Dale (*A* 1938) Sales Engr., Perfex Corp., 500 W. Oklahoma, Milwaukee, and • 5061 N. Idlewild, Milwaukee 11, Wis.

COOK, Harold V. (*J* 1946) Jr. Partner, • Louis Cook Plumbing & Heating Co., 2126 Arapahoe St., Denver 2, and 1801 Grant St., Apt. 106, Denver 4, Colo.

COOK, Ralph P. (*M* 1930) Supt., Engrg. and Maintenance Dept., in charge of Engrg. Div., • Eastman Kodak Co., Kodak Park Works, Rochester 4, and 663 Seneca Pkwy., Rochester, N. Y.

COOK, Robert L. (*J* 1948; *S* 1947) Jr. Engr., Air Cond. Dept., United Gas Corp., and • 946 Althea Dr., Houston, Texas.

COOK, W. L. (*A* 1945) Pres., • P. S. Cook Plbg. Co., 1722 Thomes St., and 314 East 21st St., Cheyenne, Wyo.

COOKE, Walter (*M* 1947) Mfrs. Agent, • 816 Howard Ave., New Orleans 13, and R.F.D. 2, Box 66-A, Hammond, La.

COOKE, William L. (*A* 1944) Managing Dir., • W. L. Cooke, Ltd., Cor. Kent and York St., Newmarket, Auckland S.E. 1,, and 747 Remuera Rd., Auckland S.E. 2, New Zealand.

COOLEY, Edgerton C. (*M* 1938) Owner-Pres. • E. C. Cooley Co., 625 Market St., San Francisco 5, and P. O. Box 870 B, Route 2, Los Altos, Calif.

COOMBE, James (*A* 1932) Pres., • William Powell Co., 2525 Spring Grove Ave., and 2363 Grandin Rd., Cincinnati, Ohio.

COON, Clifford A. (*A* 1947) Mgr. Htg. and Sheet Metal Dept., Klarr & Wilson, Third and Adams, and • 509 North 28th, Corvallis, Ore.

COON, Thurlow E. (*Life Member*; *M* 1916) Pres., • The Coon-DeVisser Co., Inc., 2051 W. Lafayette, Detroit 16, and 826 Edison Ave., Detroit 2, Mich.

COOPER, Albert W. (*M* 1944) Branch Mgr., • Johnson Service Co., 1230 California St., Denver 4, and 1213 Olive St., Denver 7, Colo.

COOPER, Benjamin G. (*A* 1947) Mech. Design Engr., W. E. Dunn Manufacturing Co., and • 248 West 18th St., Holland, Mich.

COOPER, C. H. (*A* 1944) Partner, • Cooper Bros. Heat Service Co., 1345 East 22nd Ave., Eugene, Ore.

COOPER, Dale S. (*M* 1938; *A* 1937) Cons. Engr., Dale S. Cooper & Assocs., 524 West Bldg., Houston 2, and • 216 E. Cowan Dr., Houston, Texas.

COOPER, Donald E. (*A* 1948; *J* 1939) Partner, • D. E. Cooper & Son, 540 Hood St., and 740 Lomond Dr., Salem, Ore.

COOPER, George P. (*A* 1944) Director of Engrg., • Empire-Hanna Coal Co., Ltd., 805 C. P. R. Bldg., Toronto, and 27 Dartmouth Cres., Mimico, Ont., Canada.

COOPER, John A. (*A* 1947) 522 E. Clover Dr., Rt. 5, Box 376 G, Memphis, Tenn.

COOPER, John W. (*M* 1932; *A* 1925; *J* 1921) Repr., • Buffalo Forge Co., 2118 Pine St., St. Louis 3, and 612 Hawbrook Dr., Kirkwood 22, Mo.

COOPER, Kenneth G. (*A* 1947) Designer, • Richard A. Belsham, 3500 Main Highway, Miami, and 123 Ave., Zamora, Coral Gables, Fla.

COOPER, W. B. (*M* 1946) Chief Engr., • Advanced Refrigeration Co., 1042 Gilbert Ave., and 225 Woolper Ave., Cincinnati, Ohio.

COOPER, William H. (*J* 1947) Engr., • The Bahnson Co., and 822 Lockland Ave., Winston-Salem, N. C.

COOPERMAN, Edward (*A* 1947; *J* 1943; *S* 1940) Ensign, B. O. Q., Bks. E-3, N. C. T. C., Davisville, R. I., and • 3444 Ward St., Pittsburgh 13, Pa.

CORBIT, Charles A. (*A* 1943) Pres., • Corbit's Inc., 225 S. Front St., and 901 Centre Ave., Reading, Pa.

CORBMAN, A. L., D.D.S. (*A* 1947) Dir., Research & Coordination, • Corbman Bros., 315 N. Seventh St., Philadelphia 6, and 7200 Gillespie St., Philadelphia 32, Pa.

CORDES, Elmer W. (*A* 1947) Sales Engr., • Union Electric Co. of Mo., 315 North 12th St., St. Louis 1, Mo.

COREY, George R., Sr. (*M* 1945) Superior Coal Co., 78 Narragansett Ave., Providence 7, R. I.

CORLEW, James B. (*A* 1945) Owner, • Corlew Engineering Co., 111 E. Sixth St., Chattanooga 3, and 206 Hillcrest Dr., Chattanooga, Tenn.

CORNELIUS, George E. (*A* 1943) Elec. Engr., Philadelphia Suburban Transportation Co., 69th St. Terminal Bldg., Upper Darby, and • 6 Chestnut Lane, Moylan, Pa.

CORNWALL, Charles C. (*M* 1946) Engr., The Bahnson Co., 1001 S. Marshall St., and • 214 West St., Winston-Salem, N. C.

CORR, Frank J. (*A* 1947) Supvsr. Engr., • Air-Flo Heating Co., 2412 Aurora, and 349 West 47th, Seattle, Wash.

CORREA, Benjamin A. (*A* 1946) Elec. Engr., • I. G. E., Wimco., Ltd., Box 74, Willemstad, Curacao, Netherlands, West Indies, and P. O. Box 38, Newtown, Conn.

CORRIGAN, James A. (*M* 1944; *A* 1940; *J* 1935; *S* 1930) Treas., • Corrigan Co., 2525 St. Louis Ave., St. Louis 6, and 7128 Washington Ave., St. Louis 5, Mo.

CORRIGAN, Thomas J. (*A* 1945) Vice-Pres., • Corrigan Co., 2525 St. Louis Ave., St. Louis, and 7215 Maryland Ave., University 5, Mo.

CORYELL, Glynn L. (*M* 1943) Chief Field Engr., U. S. Machine Corp., and • Country Club Park, Lebanon, Ind.

COST, George W. (*A* 1946; *J* 1939; *S* 1938) Assoc., T. F. Rockwell, Cons. Engr., 900 Century Bldg., Pittsburgh, and • 404 Pennsylvania Ave., Irwin, Pa.

COSTA, Ciro A. (*M* 1945) Cons. Engr., Santa Paula, Marcos Paz, F. C. S., Argentina, S. A.

COSTELLO, Philip F. (*A* 1947) Sr. Partner, • Costello Brothers Engineering Co., 175 W. Lincoln Ave., and 46 S. Terrace Ave., Mt. Vernon, N. Y.

COTTER, Robert P. (*A* 1946) Pres., • Ebert Air Conditioning Co., 1026 W. Ashby, and 1339 W. Rosewood Ave., San Antonio 1, Texas.

COTTON, Irwin W. (*M* 1943) Pres., • The I. W. Cotton Co., Inc., 1035 N. Pennsylvania St., and 1035 N. Pennsylvania St., Apt. A., Indianapolis 4, Ind.

COUCH, George R. (*A* 1944) Pres.-Treas., • George R. Couch Co., Inc., 157 Charter Oak Ave., Hartford 5, and 15 Bushnell St., Hartford 6, Conn.

COUCH, Henry J. (*A* 1947) Sales Engr., • Air Filter & Equipment Co., 228 N. LaSalle St., Room 1310, Chicago 1, and 10049 S. Talman Ave., Chicago 43, Ill.

COULTER, Thomas H. (*A* 1943) Vice-Pres., • 135 S. LaSalle St., Chicago 3, and 201 Kedzie St., Evanston, Ill.

COUSART, Kirkpatrick (*A* 1947) Owner • Lydon-Cousart Co., 305 Builders Bldg., and 307 Ridgewood Ave., Charlotte, N. C.

COVER, E. B. (*M* 1937) 8022 Flora, Kansas City 5, Mo.

COVER, Richard Root (*A* 1936) Mech. Engr., National Institute of Health, Bethesda, Md., and • 1914 N. Upton St., Arlington, Va.

COWAN, Armand (*A* 1945) Pres., • Stuart Cooling Corp. of Florida, 1335 Northwest 21st St., Miami 42, Fla.

COWARD, Charles W. (*M* 1935) Partner, • Coward-Eastman Co., 43 South 23rd St., Philadelphia 3, Pa., and Cherry Lane, Riverton, N. J.

COX, Edward H. (*M* 1943) Owner, Edward H. Cox, • Heating & Ventilating Equipment, 304 Crosby Bldg., Buffalo 2, and 106 S. Lake St., Hamburg, N. Y.

COX, LeRoy E. (*A* 1944) Engr., Almirall & Co., Inc., 53 Park Pl., New York, N. Y., and • 20 Laurel Pl., Glen Ridge, N. J.

COX, Robert G. (*J* 1948) Mech. Engr., 207 Yarmouth St., Dallas 8, Texas.

COX, Robert M. (*J* 1947) Installation Engr., • Florida Hill York Corp., 1225 S.W. Eighth St., and 5972 Southwest 42nd St., Miami, Fla.

COX, Samuel F. (*M* 1939) Research Dir., Glass Div., • Pittsburgh Plate Glass Co., Creighton, and 1722 Orchard Ave., Arnold, Pa.

COX, Vernon G. (*A* 1939) Dist. Sales Mgr., • Century Electric Co., 514 Texas Bank Bldg., 810 Main St., Dallas 2, and 207 Yarmouth St., Dallas 8, Texas.

COX, William A., Jr. (*M* 1946) Pres., • Cox-Frank Corp., 403-7 Adams Bldg., Norfolk 1, and Box 188, R. F. D. 1, Virginia Beach, Va.

COX, William W. (*Life Member*; *M* 1923) Mgr., • Heating Service Co., 326 Columbia St., Seattle 4, Wash., and 137 S. Flores, Los Angeles 36, Calif.

COYNE, John H. (*A* 1943) Air Cond. Engr., T. J. Conner Inc., 3092 Spring Grove Ave., Cincinnati, and • 6303 Hammel Ave., Cincinnati 12, Ohio.

CRABBIN, William W. (*A* 1944) Master Sheet Metal Worker, U. S. Coast Guard Yard, Curtis Bay, Baltimore 26, and • 312 Washburn Ave., Baltimore 25, Md.

CRAIG, Joseph A. (*J* 1940) Partner, • Roy E. Gorgen Co., 811 Wesley Temple Bldg., and 2634 W. River Dr., Minneapolis, Minn.

CRAIG, William G. (*M* 1945) Administrative Asst., • Grove Regulator Co., 6529 Hollis, Oakland, and 1311 Hopkins St., Berkeley, Calif.

CRANAGE, Thomas (*M* 1943) Dist. Sales Mgr., • Clarage Fan Co., 333 N. Michigan Ave., Chicago 1, and 399 Sunset Lane, Glencoe, Ill.

CRANE, Robert M. (*J* 1948; *S* 1947) Oil Well Supply Co., Seminole, Okla.

CRARY, James O. (*M* 1944) Pres., Industries Sales Corp., 2927 Jackson Ave., New Orleans 13, La.

CRAWFORD, Arthur C. (*A* 1938) Air Cond. Engr., Potomac Electric Power Co., Washington, and • 429 Butternut St. N.W., Washington 12, D. C.

CRAWFORD, David H. (*J* 1948; *S* 1947) Student Engr., The York Corp., and • The Y.M.C.A., York, Pa.

CRAWFORD, Fred A. (*A* 1945) Owner, Home Comfort Heating Co., 5131 Rohms Ave., Detroit 13, Mich.

CRAWFORD, James N. (*M* 1946) Sales Mgr., Gas Htg., Bryant Heater Co., 17825 St. Clair Ave., Cleveland 10, and • 21262 Byron Rd., Shaker Heights 22, Ohio.

CRAWFORD, John H., Jr. (*A* 1936; *J* 1930) Engr., Westinghouse Electric Corp., Air Cond. Div., 9 Rockefeller Plaza, New York, N. Y., and • 289 Reynolds Terrace, Orange, N. J.

CRAWLEY, James B. (*S* 1946) Student, Texas A. & M. College, Box 1962, College Station, and • Rt. 2, Longview, Texas.

CREEARS, Tom H. (*M* 1945) Owner, • T. H. Creears Co., 1824 S. Hope St., Los Angeles 15, and 3458 Knollcrest Ave., Los Angeles 43, Calif.

CRESSY, L. Villere (*M* 1940) Mech. Engr., • James M. Todd & Assocs., Cons. Engrs., 217 N. Peters St., and 3217 De Soto St., New Orleans, La.

CREW, F. D. (*A* 1944; *J* 1941) Pres., • The F. D. Crew Corp., 1539 Race St., Philadelphia 2, and Paoli, Pa.

CREW, Morris W. (*M* 1944) Mgr., Industrial Control Div., Perfex Corp., and • Shorecrest Hotel, Milwaukee, Wis.

CRIQUI, Albert A.* (*M* 1919) Chief Engr., Buffalo Forge Co., 490 Broadway, Buffalo, and • 39 St. Johns Ave., Kenmore 17, N. Y.

CRIQUI, Albert E.* (*M* 1944) Mech. Engr., • Buffalo Forge Co., 490 Broadway, Buffalo, and 89 Dorset Dr., Kenmore 17, N. Y.

CRISMAN, Leon J. (*M* 1945) Owner-Engr., • Crisman Heating & Air Conditioning Co., 502 N. Larch St., Lansing, and Apt. No. 252-C, Hillcrest Village, East Lansing, Mich.

CROCKER, Charles G. (*M* 1948) Air Cond. Engr., United Gas Corp., • Box 2628, Houston 1, and 3301 University Blvd., Houston 5, Texas.

CROCKFORD, Richard H. (*M* 1947) Mech. Engr., • Reliance Engineering Co., Box 1292, Charlotte 1, and 1405 Pecan Ave., Charlotte 4, N. C.

CROCKWELL, Walter H. (*A* 1946) Sales Engr., • Service Heat & Power Co., 815 Lydia St., Oakland, and 577-14th Ave., No. 6, San Francisco, Calif.

CROFT, Huber O. (*M* 1941) Dept. Head, Mech. Engrg., • University of Iowa, 122 Engineering Bldg., and 250 North St., Iowa City, Ia.

CROLEY, Jack G. (*A* 1947; *J* 1940) Engr., Carrier Atlanta Corp., 306 Peachtree St., Atlanta, and • 216 N. Washington St., College Park, Ga.

CROMIE, Robert W. (*M* 1947) Engr., Hajoca Corp., Baltimore & Union Ave., P. O. Box 111, and • 144 W. Albemarle Ave., Lansdowne, Pa.

CRONE, Charles E. (*M* 1922) Pres., Charles E. Crone Co., 1656 N. Ogden Ave., Chicago 14, Ill.

CRONE, Thomas E. (*Life Member*; *M* 1920) Retired, and • 164th and Chapin Pkwy., Jamaica 3, L. I., N. Y.

CRONEY, P. Alfred (*M* 1938) 302 Prospect St., Westfield, N. J.

CRONSTROM, Kenneth A. (*A* 1944) Prop., • Cronstroms Heating & Sheet Metal, 4225 Hiawatha Ave., Minneapolis 6, and 4210 Standish Ave., Minneapolis, Minn.

CROPPER, Robert O. (*M* 1938) 835 W. High St., Lexington, Ky.

CROSBY, Edward L. (*M* 1936) Pres., • Henry Adams, Inc., Federal Land Bank Bldg., 2315 St. Paul St., Baltimore 18, and 700 Brookwood Rd., Baltimore 29, Md.

CROSBY, Henry S. (*M* 1946) Dir. of Plant Engrg., • General Mills, Inc., 400 Second Ave. S., Minneapolis 1, and Long Lake, Minn.

CROSE, Oliver P. (*M* 1947) Comml. Mgr., • Murphy & Miller, Inc., 1326 S. Michigan Ave., Chicago, and 921 Oakwood Ave., Wilmette, Ill.

CROSLAND, Robert B., Jr. (*A* 1948; *J* 1946) Sales Engr., • The Bahnson Co., and Vice-Pres., Stimson Engineering Corp., Box 367, Salem Station, and 409 Arbor Rd., Winston-Salem, N. C.

CROSS, F. G. (*M* 1936) Vice-Pres., • The Fulton Sylphon Co., and 31 Nokomis Circle, Knoxville, Tenn.

CROSS, Lloyd E. (*A* 1945) Gen. Supt., • American Foundry & Furnace Co., 709 North 11th St., Milwaukee 3, and 2407 North 44th St., Milwaukee 10, Wis.

CROSS, Robert C.* (*M* 1937) Head of Mech. Div., • Sears, Roebuck & Co., Dept. 817, 925 S. Homan Ave., Chicago, and 4106 Linden Ave., Western Springs, Ill.

CROSS, Robert E. (*M* 1938; *A* 1931) Dist. Mgr., Minneapolis-Honeywell Regulator Co., P. O. Box 559, Springfield, and • Granville Center, Mass.

CROSS, William D. (*A* 1943) Pres., • Cross Engineering Co., 11 E. Broad St., and Old Raritan Rd., Westfield, N. J.

CROUSE, Marion E. (*J* 1948; *S* 1947) Asst. Foreman, Columbia Cooling & Heating Co., 500 Hampton St., and • 2602 Glenwood Rd., Columbia, S. C.

CROUT, M. M. (*M* 1939; *A* 1938) Mgr., Southern Dist., • York Corp., 412 Houston St. N.E., Atlanta 1, and 2946 Dale Dr. N.E., Atlanta, Ga.

CROWE, Robert H., (*A* 1948) Sales Repr., N. O. Nelson Co., 1701 Franklin Ave., Houston, and • 2102–10th St., Galena Park, Texas.

CRUMLEY, Mearl T. (*M* 1941) Mgr., Mech. Engrg. Section, U. S. Naval Air Station, Jacksonville, and • 1132 Ingleside Ave., Jacksonville 5, Fla.

CRUMP, Alvin L. (*M* 1937) Partner • A. L. Crump and Co., 407 S. Dearborn St., Chicago 5, and 2701 Payne St., Evanston, Ill.

CRUMP, Samuel (*A* 1943) Pres., • Samuel Crump Co., Ltd., 317 Eglinton Ave. W., Toronto 12, and 34 Braemar Ave., Toronto, Ont., Canada.

CUCCI, Victor J. (*M* 1930) Cons. and Marine Engr., • Room 282, 50 Church St., New York, and 451-55th St., Brooklyn, N. Y.

CULBERT, William P. (*M* 1943; *A* 1929) Partner, • Culbert-Whitby Co., 2019 Rittenhouse Sq., Philadelphia 3, and 929 Alexander Ave., Drexel Hill, Pa.

CULLEN, Charles W. (*A* 1947) Mgr., • Peoples National Gas Co., 545 Wm. Penn Pl., Pittsburgh 19, and Riverside Rd., R. D. No. 1, Verona, Pa.

CULVER, Frank C. (*A* 1945) Mfrs. Repr., Day and Night Manufacturing Co., and • 4730 15th Ave. N. E., Seattle 5, Wash.

CUMMING, Robert W. (*M* 1928) Engr. and Sales Exec., Sarco Co., Inc., 350 Fifth Ave., Empire State Bldg., New York 1, and • 81 Alkamont Ave., Scarsdale, N. Y.

CUMMINGS, Carl H. (*A* 1927; *J* 1926) The Bryant Heater Co., 1020 London Rd., Cleveland, Ohio.

CUMMINGS, George C. (*M* 1944) New York Repr., Dravo Corp., 512 Fifth Ave., and • 4 West 43rd St., New York 18, N. Y.

CUMMINGS, Robert J. (*A* 1944; *J* 1940) Engr. and Estimator, • Franck & Fric Co., 7109 Kinsman Rd., Cleveland 4, and 18110 Maple Heights Blvd., Bedford, Ohio.

CUMMINGS, Thomas P. (*A* 1942) Cummings Engineering Co., 3005 West 48th St., and • 5145 Seventh Ave., Los Angeles 43, Calif.

CUMMINS, George H. (*M* 1919) Dist. Mgr., • Aerofin Corp., 1200 United Artists Bldg., Detroit 26, and 16210 Ashton Rd., Detroit, Mich.

CUMMISKEY, Jerome F. (*A* 1940) Midwestern Sales Mgr., Air Cond. Controls Div., Minneapolis-Honeywell Regulator Co., 351 E. Ohio, Chicago 11, and • 7706 Eastlake Terrace, Chicago 26, Ill.

CUMNOCK, H. (*A* 1938) Pres., Little Rock Refrigeration Co., Inc., 417 W. Capitol Ave., Little Rock, Ark.

CUNNINGHAM, John S. (*A* 1941; *J* 1937; *S* 1935) Pres., • Thermo-Products, Inc., and North Judson, Ind.

CUNNINGHAM, Thomas M. (*M* 1931; *A* 1930) Dir. of Indus. Relations, Carrier Corp., 300 S. Geddes St., Syracuse 1, N. Y.

CUPITT, Robert (*A* 1943) Messrs. Fletcher Bros. (Pressings) Ltd., Eagle Works, 329 Holyhead Rd., Handsworth, Birmingham 21, and • 1 Beeches Dr., Erdington, Birmingham 24, England.

CURL, Robert S. (*A* 1941) Owner, • Robert S. Curl and Assocs., 80 S. Third St., and 1482 Whittier Ave., Columbus, Ohio.

CURLEY, Ellis I. (*A* 1941) American Blower Corp., 783 Broad St. Station, Philadelphia 3, Pa.

CURRIE, Raymond C. (*A* 1946) Mgr. and Engr., • Pacific Heating & Sheet Metal Co., 3420-18th St., and 837 Kirkham St., San Francisco, Calif.

CURRY, Roger F. (*J* 1940; *S* 1938) Htg. Engr., Cleverdon, Varney & Pike, 120 Tremont St., Boston, and • 80 Ripley St., Newton Centre, Mass.

CURRY, William Hubert (*M* 1946) Sales Engr., • John A. Dodd Co., 299 Techwood Dr., N.W., Atlanta, and Rt. 1, Smyrna, Ga.

CURTICE, Jean M. (*A* 1936) Owner & Mgr., • Curtice-Spencer Co., 900 Lincoln Ave., and 906 Lincoln Ave., La Junta, Colo.

CURTIS, A. Ray (*A* 1945) Owner and Mgr., • A. Ray Curtis Co., 2205 Highland Dr., and 2642 Beverly St., Salt Lake City, Utah.

CURTIS, Grant B., Jr. (*J* 1947) Htg. Engr., • Crane Co., Washington St. Viaduct, and 1043 Juniper, Atlanta, Ga.

CURTIS, Herbert F. (*A* 1934) Vice-Pres., Auer Register Co., 3608 Payne Ave., Cleveland, Ohio.

CUSHING, C. F. (*M* 1938) Vice-Pres., • Payne Furnace Co., 336 N. Foothill Rd., Beverly Hills, Calif., and 13415 S. Woodland Ave., Cleveland, Ohio.

CUSHING, R. C. (*A* 1940) Sales Mgr., Air Cond. Controls Div., Pacific Region, • Minneapolis-Honeywell Regulator Co., 1136 Howard St., San Francisco 3, and 209 Kenyon Ave., Berkeley 8, Calif.

CUSTER, John B. (*S* 1948) Student, University of Minnesota, Minneapolis, and • 50 S. Cretin, Apt. 304, St. Paul, Minn.

CUTLER, Joseph A. (*M* 1916) (Council, 1920-26) Pres. and Gen. Mgr., • Johnson Service Co., 507 E. Michigan St., Milwaukee 2, and 4811 N. Lake Dr., Milwaukee 11, Wis.

CUTTING, Richard Hawley (*M* 1942) Partner, Archts. Engrs., • 4900 Euclid Ave., Cleveland 3, and 3795 Glenwood Rd., Cleveland Heights 21, Ohio.

D

DABBS, John T. (*A* 1940) Commercial Zone Sales Supvsr., York Corp., 119 South 11th St., St. Louis 2, Mo.

DADDARIO, F. T. (*A* 1946; *J* 1939) Owner, • Carolina Air Conditioning Co., 309 McMannen St., Durham, N. C.

DAFTER, Edwin H. (*M* 1938) Sales Engr., • Carrier Corp., 12 South 12th St., Philadelphia 7, and 117 Crosshill Rd., Overbrook Hills, Philadelphia 31, Pa.

DAHL, Lawrence J. (*S* 1943) Rt. 7, Minneapolis 11, Minn.

DAHLGREN, Gustave E. (*A* 1940) Mgr., Insulation Dept., • Thorkelsson, Ltd., 1331 Spruce St., and 533 Basswood Pl., Winnipeg, Man., Canada.

DAHLSTROM, Godfrey A. (*M* 1943; *A* 1927) Mech. Engr., Minnesota Mining & Manufacturing Co., 900 Fauquier Ave., St. Paul 6, and • 3721 47th Ave. S., Minneapolis 6, Minn.

DAHLSTROM, John A. (*M* 1944) Head of Furnace Dvlpt. Div., • Perfection Stove Co., 7609 Platt Ave., Cleveland, and 420 Canterbury Rd., Bay Village, Ohio.

DAHMS, Alfred A. (*A* 1944) Dist. Mgr., • Allis-Chalmers Manufacturing Co., 1009 Waldheim Bldg., and 7431 Mercier, Kansas City 6, Mo.

DAILEY, J. F. (*M* 1944) Pres., • Typhoon Air Conditioning Co., Inc., (Ice Air Cond. Co., Inc.,) 794 Union St., Brooklyn 15, and 13 Manchester Rd., Eastchester, N. Y.

DAITSH, Abe (*A* 1944; *J* 1938) Air Cond. and Refrig. Engr., 8A Avenue Normandie, Sea Point, Capetown, Union of South Africa.

DALTON, Robert T. (*A* 1943) Owner, Dalton Sales & Service, 3602 East 138th St., Cleveland 20, Ohio.

DALY, John D. (*A* 1947) Sales Engr., • A. F. Hinrichsen, Inc., 50 Church St., New York 7, N. Y., and Longview Ave., Lincoln Park, N. J.

D'AMBLY, A. Ernest (*M* 1924; *J* 1921) Owner, • A. Ernest D'Ambly, 117 South 17th St., Room 900, Philadelphia 3, and 1835 DeLancey St., Philadelphia, Pa.

DANE, Irving S. (*M* 1947) Widger Miller Corp., 47 Ellery St., South Boston 27, Mass.

DANIEL, Charles E. (*M* 1947) Cons. Engr., 325 N. Charles St., Baltimore, and • 1020 N. Calvert, Cambridge, Md.

DANIEL, David C. (*A* 1947) Jr. Asst. Indus. Engr., Arkansas Louisiana Gas Co., Slattery Bldg., Shreveport, and ●719 Benton Rd., Bossier City, La.

DANIEL, James M. (*J* 1948; *S* 1946) Engr., Natkin & Co., 1015 Sampson, Houston 3, and ●1125 Usener, Houston 9, Texas.

DANIEL, W. Edwin (*A* 1941; *J* 1939) Tech. Dir., ●The Fuel Efficiency Co., and Ashby (Blackfriars) Ltd., 20 Upper Ground, London, S. E. 1, and 46 Melrose Rd., London, S.W. 18, England.

DANIELS, Donald David (*J* 1947) Mgr., ●Trane Company of Canada, Ltd., 408 Westman Chambers, and 414–18th Ave., Regina, Sask., Canada.

DANIELSON, L. C. (*A* 1946) Chief Engr., ●Atkinson-Jones Cos., APO 331 Okinawa, c/o Postmaster, San Francisco, Calif., and Russell, Kans.

DANIELSON, Wilmot A.* (*M* 1935), (Council, 1944–47) Pres., Danielson Associates, Inc., 813 Vance Ave., Memphis, and ●Tru-Dan Acres, Raleigh, Tenn.

DANNEHY, James J. (*A* 1946) Engr., Refrigeration Maintenance Corp., 321 E. Grand Ave., Chicago, and ●1630 W. Balmoral Ave., Chicago 40, Ill.

DANOWITZ, Chester J. (*A* 1947; *J* 1942) Air Cond. Engr., Ebasco Services Inc., 2 Rector St., New York, N. Y., and ●60 E. Washington Ave., Atlantic Highlands, N. J.

DAPPER, M. J. (*A* 1944) Owner, Dapper Furnace Co., 1123 S. Tacoma Ave., Tacoma, Wash.

DARBY, F. Norman (*M* 1944) Engr. in charge Htg. and Vent. Sect., Sun Shipbuilding & Dry dock Co., Chester, and ●5236 Cedar Ave., Philadelphia 43, Pa.

DARBY, J. Wilson (*A* 1947) Owner, ●J. W. Darby Co., P. O. Box 6043, Houston 6, and 5413 Belmont, Houston 5, Texas.

DARBY, Thomas E. (*M* 1944) Utilization Engr., ●The Ohio Fuel Gas Co., 99 N. Front St., Columbus 15, and 29 Tibet Rd., Columbus 2, Ohio.

DARLING, A. B. (*A* 1929) Comptroller, ●Darling Brothers, Ltd., P. O. Box No. 187, and 4009 Grey Ave., Montreal, Que., Canada.

DARLING, John W. (*A* 1947) Sales Engr., ●Ontario Plumbing and Heating Supplies, Ltd., 858 DuPont St., and 795 Eglinton Ave. E., Toronto, Ont., Canada.

DARLING, Robert B. (*A* 1944) Owner, ●Robert B. Darling Co., 280 Madison Ave., New York 16, and 65 Highland Ave., Port Washington, N. Y.

DARRAH, Richard D. (*M* 1944) Sales Engr., Dravo Corp., 300 Penn Ave., Pittsburgh 22, and ●515 Roslyn Pl., Pittsburgh 6, Pa.

DARTS, John A. (*M* 1919) Exec. Vice-Pres., Fitzgibbons Boiler Co., Inc., 101 Park Ave., New York 17, and ●610 West 110th St., New York 25, N. Y.

DASING, Emil (*M* 1937) Design Engr., Sears, Roebuck & Co., 925 S. Homan Ave., Chicago, and ●2618 W. Eastwood Ave., Chicago 25, Ill.

DASTUR, Maneck N. (*A* 1948; *J* 1945) Jr. Engr., ●Carrier Corp., International Div., c/o Miss F. Keene, 122 East 42nd St., New York 17, N. Y.

DAUBER, Oscar W. (*M* 1937) Cons. Engr., ●Naess and Murphy, 1661 Railway Exchange Bldg., Chicago 4, and 532 Greenwood Ave., Kenilworth, Ill.

DAUCH, Emil O. (*M* 1921) Pres., ●McCormick Plumbing Supply Co., 1675 Bagley Ave., and 729 Bedford Rd., Grosse Point Park, Detroit, Mich.

DAUGHERTY, Robert J. (*A* 1947) Sales Engr., Flick Distributing Co., 49 Central Ave., Cincinnati, and ●628 Main St., Hamilton, Ohio.

DAUSSAT, Waldo J. (*A* 1945) Mech. Engr. U. S. Navy Public Works Dept., Bldg. 16, U. S. Naval Repair Base, New Orleans 14, and ●6318 Clara St., New Orleans 15, La.

d'AUTREMONT, Hubert F. (*A* 1947) Cons. Engr., 711 West 62nd St., Los Angeles, Calif.

DAVENPORT, Lind B. (*M* 1944) Chief Engr., ●Air Conditioning Company of Southern California, 1005 Santa Fe Ave., Los Angeles 21, and 139 Melrose Ave., Monrovia, Calif.

DAVEY, Geoffrey I. (*M* 1937) Chartered Cons. Engr., ●Gutteridge, Haskins & Davey, City Mutual Bldg., 60 Hunter St., Sydney, and Netherby, Bangalla St., Warrawee, New South Wales, Australia.

DAVIDSON, James W. (*A* 1944) Pres. and Owner, Davidson Heating, Reg'd., Val Morin, Terrebonne County, Que., Canada.

DAVIDSON, John C. (*M* 1940; *J* 1936) Field Engr., Chrysler Airtemp Sales Corp., 4708 Isabel Ave., Minneapolis, Minn.

DAVIDSON, L. Clifford (*M* 1927) Partner, ●Davidson & Hunger, 220 South 16th St., Philadelphia 2, and 322 Winding Way, Merion, Pa.

DAVIDSON, P. L. (*M* 1924; *J* 1921) Cons. Engr., 1420 Walnut St., Philadelphia 2, and ●New Hope, Pa.

DAVIDSON, William J. (*M* 1945) Appl. Engr., N. O. Nelson Co., 118 E. River St., and ●602 Gaylord, Pueblo, Colo.

DAVIES, Albert T. (*A* 1946) Chief Mech. & Elec. Engr., C. Howard Crane, 7 Buckingham Gate, London S. W. 1., and ●33 Townsend Dr., St. Albans, Herts, England.

DAVIES, Charles (*M* 1945) Pres., ●Davies Air Filter Co., 250 East 43rd St., New York, and 265 Coligni Ave., New Rochelle, N. Y.

DAVIES, George W. (*Life Member*; *M* 1918) Mgr., ●F. W. Davies & Co., 19 Maclaggan St., Dunedin, C.1, and P. O. Box 390, Dunedin, N.2, Colinswood, Macandrew Bay, New Zealand.

DAVIS, Bert C. (*Life Member*; *M* 1904), (Council, 1917) Big Flats, N. Y.

DAVIS, Charles (*M* 1938) Engr., James H. Merritt and Co., 215 East 27th St., New York 16, and ●3920 Bronx Blvd., New York 66, N. Y.

DAVIS, Clemant A. L. (*A* 1942) Vice-Pres., John H. Kitchen & Co., 1016 Baltimore, Kansas City 6 and ●3200 East 32nd St., Kansas City 3, Mo.

DAVIS, Clyde W. (*M* 1947) Pres., ●C. W. Davis and Son Inc., 201 19th St., and 918 Ninth St., Huntington, W. Va.

DAVIS, C. R. (*M* 1927) Branch Mgr., ●Johnson Service Co., 2328 Locust St., St. Louis 3, and 7527 Forsythe Blvd., Clayton 5, Mo.

DAVIS, Donald W., Jr. (*A* 1946; *J* 1939) Branch Mgr., ●Sturtevant Div., Westinghouse Electric Corp., 854 Empire Bldg., Milwaukee 3, and 3748 North 56th St., Milwaukee 10, Wis.

DAVIS, Edward James (*A* 1943; *J* 1938) Sales Engr., Gurney Foundry Co., Ltd., 4 Junction Rd., and ●224 St. Clements Ave., Toronto, Ont., Canada.

DAVIS, George C. (*M* 1939; *J* 1936) Vice-Pres., ●Northern Public Service Corp., Ltd., 1120 Dorchester Ave., and 366 Ash St., Winnipeg, Man., Canada.

DAVIS, George L., Jr. (*A* 1938) Estimator, R. L. Spitzley Heating Co., 1200 W. Fort St., Detroit 26, and ●3636 Bedford St., Detroit 24, Mich.

DAVIS, John C. (*M* 1945) Pres. & Mgr., ●J. C. Davis, Ltd., 408 New Hargrave Bldg., Winnipeg, and 152 La Verandrye St., St. Boniface, Man., Canada.

DAVIS, John T. (*M* 1945) Sales Engr., The Trane Co., and ●1836 Sul Ross, Houston 6, Texas.

DAVIS, Joseph (*M* 1927; *A* 1926) Htg. Engr. and Contr., ●120 W. Tupper St., Buffalo 1, and 166 Huntington Ave., Buffalo 14, N. Y.

DAVIS, Keith T. (*M* 1937) Chief Engr., ●Bryant Heater Co., 17825 St. Clair Ave., Cleveland 10, and 2984 Claremont Rd., Shaker Heights 22, Ohio.

DAVIS, Leonard V. (*A* 1945) Research and Design Engr., Russell Stovers Candies of Denver, 2015 Arapahoe St., and ●17 E. Maple St., Denver, Colo.

DAVIS, Lester T. (*M* 1946) Project Mgr., ●Standard Engineering Co., Inc., 2129 Eye St. N.W., Washington 7, D. C., and 9305 Glenville Rd., Silver Spring, Md.

DAVIS, Telford R. (*M* 1942) Vice-Pres., ●Ammerman, Davis & Stout, Inc., Engrs., 912-23 K. P. Bldg., Indianapolis 4, and 1311 N. Drexel Ave., Indianapolis 1, Ind.

DAVIS, Wayne M. (*A* 1944) Field Engr., Box 990, Muncie, Ind.

DAVIS, Wilson L. (*A* 1946) Mgr., South Bend Office, American Blower Corp., 407 S. Notre Dame Ave., South Bend 22, and ●1429 E. Ewing Ave., South Bend, Ind.

DAWSON, Eugene F. (*M* 1934) Chairman, ●School of Mech. Engrg., University of Oklahoma, and 719 Chautauqua St., Norman, Okla.

DAWSON, Fred C. (*M* 1944) Cox Engineering Co., 621 Putnam Ave., Cambridge, Mass.

DAWSON, Ralph E. (*A* 1946) Chief Engr., Green Colonial Furnace Co., 322 S.W. Third, and ●1004 58th, Des Moines, Ia.

DAY, Harold C. (*A* 1934) Field Mgr., ● American Radiator & Standard Sanitary Corp., P. O. Box 1226, Pittsburgh 30, and 133 Crescent Dr., Pittsburgh 16, Pa.

DAY, Irving M. (*A* 1936) Sales Engr., ● Binks Manufacturing Co., 718 Mills Bldg., Washington 6, D. C., and 405 Cumberland Ave., Chevy Chase 15, Md.

DAY, L. Carroll (*A* 1947) Pres. & Gen. Mgr., ● Day-York Distributors, 2182 N. Lewis Ave., Portland, and 5440 S.E. Lincoln St., Portland 15, Ore.

DAY, Sidney S. (*A* 1945) Owner, Sidney S. Day, ● 3333 N. Vancouver Ave., Portland 12, and 447 N.E. Hazelfern Pl., Portland 15, Ore.

DAY, V. S.* (*M* 1924) Prod. and Price Controller, Carrier Corp., S. Geddes St., Syracuse, N. Y.

DEAN, Carl H. (*M* 1936) Sales Dir., Heating Research Corp., P. O. Drawer 391, Anderson, Ind.

DEAN, Charles L. (*Life Member*; *M* 1932) Assoc. Prof. of Mech. Engrg., University of Wisconsin, 305 University Extension Bldg., Madison 5, and ● 102 Grand Ave., Madison, Wis.

DEAN, Edwin C. (*M* 1945) Partner, Russellville Plumbing & Heating Co., 113 E. Main St., and ● 901 N. Denver, Russellville, Ark.

DEAN, Francis F. (*M* 1947) Engr., J. E. Sirrine Co., Box 960, Greenville, and ● 507 E. Orr St., Anderson, S. C.

DEAN, Frank J., Jr. (*A* 1942; *J* 1935; *S* 1934) Pres., Temperature Engineering Corp., 14th and McGee Sts., Kansas City 6, Mo.

DEAN, Vernon C. (*M* 1945) Cons. Engr., ● 603 Murray Bldg., Grand Rapids 2, and 1812 Martin S.E., Grand Rapids, Mich.

DEBES, Charles N. (*M* 1946) Owner, ● Charles N. Debes & Assocs., Rockford Trust Bldg., and 1841 E. State St., Rockford, Ill.

DeBRA, Fred B. (*A* 1945) Pres., ● Fred B. DeBra Co., 3837 Spring Grove Ave., Cincinnati 23, and 1559 Brandon Ave., Cincinnati 30, Ohio.

de BRUYN, Leo F. (*A* 1946) Sales Engr., ● Minneapolis-Honeywell Regulator Co., Langstrasse 83, and Hotel Neptune, Zurich, Switzerland.

DEE, Vaughn C. (*A* 1947) Estimator, Gorman-Lavelle Co., 2341 East 22nd St., Cleveland, and ● 22063 Wentworth, Berea, Ohio.

DEES, Leonard L. (*M* 1945) Owner, Kansas Sheet Metal Co., 206 W. Sixth, Topeka, Kans.

DEEVES, Edward W. (*A* 1944; *J* 1940) Partner, ● Fred Deeves & Sons, 1422A 17th Ave. W., and 2403 33rd St. W., Calgary, Alta., Canada.

DeFLON, James G. (*A* 1946; *J* 1942) Cooling Tower Engr., The Fluor Corp., 2500 S. Atlantic Blvd., and ● 2563 Fidelia St., Los Angeles 22, Calif.

DEGILIO, Louis (*J* 1943) ● Arctic Refrigeration Service, 119 Pine St. S., and 164 Birch St. S., Timmins, Ont., Canada.

DEGLER, Howard E. (*M* 1948) Tech. Dir., ● The Marley Co., 3001 Fairfax Rd., Kansas City 15, Kans., and 2420 Harris Blvd., Austin, Texas.

DEHLER, Frank C. (*M* 1944) Chemical Engr., ● The Davison Chemical Corp., 20 Hopkins Pl., Baltimore 3, and 3439 Guilford Terrace, Baltimore 18, Md.

DeJARLAIS, Gordon M. (*A* 1946; *J* 1945) Engr., Fedders Quigan Corp., 57 Tonawanda St., Buffalo, and ● 297 Sanders Rd., Buffalo 17, N. Y.

DELALANDE, Andre (*M* 1945) Engr., Nash-Kelvinator Corp., Export Div., 14250 Plymouth Rd., Detroit 32, Mich., and ● 51 rue la Fontaine, Paris (XVI^e), France.

DeLAND, Charles W. (*M* 1924; *J* 1923) Vice-Pres., ● C. W. Johnson, Inc., 715 W. Randolph St., Chicago 6, and 2021 Estes Ave., Chicago, Ill.

DELANY, William F. (*A* 1947) Chief Draftsman, Trane Company of Canada, Ltd., King and Dufferin Sts., and ● 104 Bude St., Toronto, Ont., Canada.

DelCAMPO, Edward (*A* 1946) Sales Engr., ACELCO, Santo Domingo 1751, Buenos Aires, and ● Laprida 902, Vicente Lopez, F.C.C.A., Argentina, S. A.

DELL, John A. (*A* 1947) Pres., ● The Dell Corp., Morton Grove, and 1510 Walnut Ave., Wilmette, Ill.

DeLUCIA, F. Arthur (*A* 1945) Engr.-Estimator, ● A. J. Mongillo Co., 928 Grand Ave., and 325 Willow St., New Haven 11, Conn.

DEMAREST, Richard T. (*A* 1947; *J* 1938) Personnel Mgr., ● Fitzgibbons Boiler Co., Inc., 23 Mercer St., and Hotel Pontiac, Oswego, N. Y.

DEMETER, Julius (*A* 1939) ● Amer-Ind., Inc., Engrs., 420 Madison Ave., New York 17, and 303 East 71st St., New York, N. Y.

DEMING, Roy E. (*M* 1941; *A* 1939) Designing Engr., Furnaces, Kalamazoo Stove & Furnace Co., Rochester Ave., Kalamazoo, Mich.

DEMPSEY, Edward P. (*M* 1945) Htg. and Vent. Engr., The Glenn Martin-Nebraska Co., Box 1269, Omaha 1, and ● 2431 Camden Ave., Omaha 11, Nebr.

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DeNEILLE, J. Lawrence (*M* 1943) Pres., ● Eichler Co., 2125 Locust St., St. Louis, and 7227 Maryland Ave., University City, Mo.

DENNY, Harold R. (*A* 1934) Eastern Mdse. Mgr., ● American Blower Corp., 50 West 40th St., New York, N. Y., and 429 Edgewood Ave., Westfield, N. J.

DENSON, Walter, Jr. (*A* 1944) Secy.-Treas., ● Walter Denson & Son, 902 N. Myrtle Ave., and 2730 Cherokee Ave., Jacksonville, Fla.

DEPPMANN, Arthur C. (*A* 1947) Pres., Deppmann and Furney Plumbing and Heating Co., 650 W. Baltimore Ave., and ● 4780 W. Outer Dr., Detroit, Mich.

DEPPMANN, Ray L. (*A* 1937) Owner, ● R. L. Deppmann Co., 5853 Hamilton Ave., and 13201 Cloverlawn Ave., Detroit, Mich.

DERBY, Malcolm R. (*M* 1946) Engr., Kroeschell Engineering Co., 215 W. Ontario St., Chicago 10, and ● 420 S. Batavia Ave., Batavia, Ill.

DeROO, William C. (*A* 1945) Engr., ● Hart & Cooley Manufacturing Co., 500 E. Eighth St., and 567 Central Ave., Holland, Mich.

DeSALES, Monteiro, Jr. (*M* 1939) Engr., Isnard & Cia, Rue Lavradio, 67, and ● P. O. Box 3963, Rio de Janeiro, Brazil, S. A.

DESMOND, Owen (*A* 1947) Sales Mgr., ● Modine Manufacturing Co., and 1824 College Ave., Racine, Wis.

DeSOMMA, A. Edward (*A* 1943; *J* 1937) Sr. Engr., Naval Archt., Bureau of Ships, U. S. N., Washington, D. C., and ● 48-29 (a) South 28th St., Arlington, Va.

DESPLANCHES, Andre (*M* 1946) Gen. Mgr., Procedes Ozonair, 63 Rue de Lancry, Paris 10, and ● 52 Ave. Motte-Picquet, Paris 15, France.

DesREIS, John F. (*M* 1946) 50 Fernwood Rd., Summit, N. J.

DETWEILER, John R. (*J* 1945) Engr., ● Detweiler Brothers, Inc., and 627 W. Main, Twin Falls, Idaho.

DEUBEL, Justin A. (*M* 1945) Engr., Perfex Corp., 500 W. Oklahoma Ave., Milwaukee 7, and ● R. 1, Box 135 C, Hales Corners, Wis.

DEUTH, Gerald Q. (*A* 1944) Pvt., U. S. Army, and ● 39 West 11th Ave., Columbus, Ohio.

DEVER, Henry F. (*M* 1936; *A* 1935) Pres., ● The Brown Instrument Co., Wayne and Roberts Aves., Philadelphia 44, and 544 Howe Rd., Merion Station, Pa.

DEVERALL, Charles R. (*A* 1945; *J* 1944) National Homes Corp., Lafayette, and ● 1812 Garden St., West Lafayette, Ind.

DeVINES, Hollis L. (*A* 1946) Mech. Engr., ● Reg. F. Taylor, 811 Bankers Mortgage Bldg., and 4608 Keystone, Houston, Texas.

DEVLIN, James J. (*A* 1947) Partner, ● W. C. Devlin & Son, 30 W. Tenth St., and 47 West 40th St., Bayonne, N. J.

DEVORE, Angus B. (*A* 1937) Pres., Carl Lipp, Inc., 1234 Wisconsin Ave. N.W., Washington 7, and ● 3525 Davenport St. N.W., Washington 8, D. C.

DeWILDE, M. P. (*A* 1946) Chief Engr., Air Cond. Dept., N. V. Industrieele Mij. Gebr. vanSwaay, Stadhouderslaan 16, The Hague, and ● Koepelweg 3, Noordwijk aan Zee, Holland.

deWITT, Earl S. (*A* 1936) Branch Mgr., ● American Blower Corp., 1211 Commercial Bank Bldg., and 232 Cottage Pl., Charlotte, N. C.

DEYO, Clyde D., Jr. (*A* 1947) Asst. Chief Utilities Engr., Electro-Motive Div., General Motors Corp., La Grange, and ● 608 N. Grove Ave., Oak Park, Ill.

DIAMOND, David D. (*A* 1942; *J* 1937) 1516 Sargent St., St. Paul, Minn.

DIAS, William B. (*A* 1948) Owens-Corning Fiberglas Corp., 718 Fifth Ave., New York, N. Y., and ● Linwood Ave., Riverside, Conn.

DIBBLE, S. E.* (*Life Member*; *M* 1917), (*Presidential Member*), (Pres., 1925; 1st Vice-Pres., 1924; 2nd Vice-Pres., 1923), (Council, 1921-26), Prof., Supt., Patton Masonic School for Boys, Patton School, Elizabethtown, Pa.

DICKASON, Gray D. (*M* 1938) Pres.-Treas., ● Genesee Heating Service, Inc., 950 Sibley Tower Bldg., Rochester 4, and 1 Meadow Lane, Rochester 10, N. Y.

DICKENS, Lester A. (*A* 1941) Owner, ● Dickens & Co., 17706 Miles Ave., Warrensville Heights, and 3710 Grosvenor Rd., Cleveland Heights, Ohio.

DICKENSON, Malcolm E. (*M* 1936) Pres. and Gen. Mgr., ● Livingston Stoker Co., Ltd., 33 Sanford Ave. S., and 964 Cumberland Ave., Hamilton, Ont., Canada.

DICKEY, Albert T. (*A* 1946) Air Cond. Engr., ● Cox & Blackburn, 2301 Commerce St., Houston 2, and 3103 Harrisburg Blvd., Houston, Texas.

DICKEY, Arthur J. (*M* 1921) Pres. and Gen. Mgr., C. A. Dunham Co., Ltd., 1523 Davenport Rd., Toronto 4, and ● 9 Mossom Pl., Toronto 3, Ont., Canada.

DICKINSON, Neville S. (*A* 1943) Pres., ● Motor Sales & Engineering Co., Inc., 1060 Broad St., Newark 2, and 507 Richmond Ave., Maplewood, N. J.

DICKINSON, Robert P., Jr. (*A* 1946; *J* 1938) Resident Sales Engr., ● Minneapolis-Honeywell Regulator Co., 1919 Benedict Circle, St. Albans, W. Va.

DICKSON, Donald R. (*J* 1946; *S* 1941) Field Engr., ● American Blower Corp., 625 Architects & Builders Bldg., Indianapolis 4, and 3423 N. Drexel Ave., Indianapolis 1, Ind.

DICKSON, George P. (*M* 1936) Mgr., B. F Sturtevant Co., Div. of Westinghouse Electric, Haddon and Crestmont Ave., Camden, and ● 430 Cooper St., Woodbury, N. J.

DICKSON, Robert B. (*M* 1919) Pres., ● Kewanee Boiler Corp., and 145 E. Division St., Kewanee, Ill.

DICKSON, Robert W., Jr. (*M* 1947; *A* 1943; *J* 1938) Field Engr., ● American Blower Corp., 1302 Swetland Bldg., Cleveland 15, and 932 Montford Rd., Cleveland Heights 21, Ohio.

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DILL, Richard S.* (*M* 1939) Chief, Heat and Air Cond. Sect., ● National Bureau of Standards, Washington 25, D. C., and 1603 S. Springwood Dr., Silver Spring, Md.

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DILLENDER, Eugene A. (*M* 1939) Mech. Engr., Wyatt C. Hedrick, Archt. & Engr., 5201 Fannin St., Houston 4, and ● 4825 Chenevert, Apt. 5, Houston, Texas.

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DISNEY, Melvin A. (*M* 1942; *A* 1934) Gen. Mgr., Watertemp Inc., 3818 Hampton Blvd., St. Louis 9, and ● R. R. 1, Box 556, Glencoe, Mo.

DISTEL, Robert E. (*M* 1941; *J* 1938) Pres. & Gen. Mgr., ● Distel Heating Co., P. O. Box 298, Lansing 2, and 547 Bailey St., East Lansing, Mich.

DIVER, M. L. (*M* 1925) Cons. Engr., P. O. Box 1016, San Antonio 6, Texas.

DIXON, Arthur G. (*M* 1928) Secy., ● Modine Manufacturing Co., and 442 Wolff St., Racine, Wis.

DIXON, Meredith F. (*A* 1946) Fuel Oil and Burner Dept., ● Imperial Oil, Ltd., 56 Church St., Toronto 1, and 64 St. Clair Ave. W., Apt. 507, Toronto, Ont., Canada.

DIXON, William (*A* 1946) Htg. Engr., ● Nelson Co., 2604 Fourth Ave., Detroit 1, Mich.

DODD, John A. (*M* 1944) Owner, ● John A. Dodd Co., 299 Techwood Dr. N.W., and 3370 Nancy's Creek Rd., Atlanta, Ga.

DODDS, Forest F. (*M* 1920) Mgr., Kansas City Sales Office, American Radiator & Standard Sanitary Corp., 503-6 National Fidelity Life Bldg., 1002 Walnut St., Kansas City 6, and ● Park Lane Hotel, 4600 Mill Creek Dr., Kansas City, Mo.

DODGE, Harry A. (*M* 1936) Cons. Engr., ● 419 Fourth Ave., New York 16, and 514 West End Ave., New York 24, N. Y.

DODGE, Raymond V., Jr. (*M* 1946) Engr., ● Richardson-Wayland Electrical Corp., 122 W. Church Ave., Roanoke, and ● 714 Windsor Ave., Ral. Ct., Roanoke 15, Va.

DOEPPENSCHMIDT, Lawrence C. (*A* 1946) Owner Better Heating & Air Conditioning Co., 5211 Lawndale Ave., Houston 3, Texas.

DOERING, Frank L. (*M* 1919) American Radiator & Standard Sanitary Corp., 238 Boston Ave., Lynchburg, Va.

DOERRFUSS, Harry W. (*M* 1944) Sales Engr., ● Warren Webster Co., 26 South 20th St., Philadelphia 3, Pa., and 35 Harvard Rd., Audubon, N. J.

DOHERTY, John J. (*A* 1942) ● Fells Plumbing, Heating & Builders' Supplies, Inc., 654 Main St., and 10 Maple Rd., Winchester, Mass.

DOHERTY, Raymond S. (*A* 1946) N. Y. Sales Mgr., ● Taco Heaters, Inc., 342 Madison Ave., New York, and 82-06-34th Ave., Jackson Heights, N. Y.

DOHERTY, Roger J. (*A* 1945) Vice-Pres., Shaw Perkins Manufacturing Co., 1645 Oliver Bldg., Pittsburgh, and ● 363 Lehigh Ave., EE Pittsburgh 6, Pa.

DOING, L. J. (*M* 1944) Engr., Selle Equipment & Contracting Co., 803 E. Markham, and ● 910 Barber, Little Rock, Ark.

DOLAN, H. P. (*M* 1944) Dir. of Engrg. and Operation of Bldgs., Board of Education, 1354 Broadway, Detroit 26, and ● 14419 Strathmoor Ave., Detroit 27, Mich.

DOLAN, Raymond G. (*M* 1926; *J* 1922) Secy.-Treas., ● Tom Dolan Heating Co., Inc., 614-16 W. Grand Ave., Oklahoma City 2, and 708 Northwest 40th, Oklahoma City, Okla.

DOLAN, William H. (*A* 1941) Pres., ● The Jennison Co., 17 Putnam St., and 65 Highland Ave., Fitchburg, Mass.

DOLGE, Emil A. (*A* 1945) Mgr., Htg. Dept., A. V. McDonald Manufacturing Co., Des Moines, and ● P. O. Box 976, Des Moines 4, Ia.

DOLL, Errol V. (*J* 1948) Engrg. Draftsman, The Austin Co., 618 Grand Ave., and ● 668 Calmar Ave., Oakland, Calif.

DOLLINGER, Lewis L., Jr. (*A* 1946) Vice-Pres., Dollinger Corp., 11 Centre Park, Rochester 3, N. Y.

DOME, Alan G. (*M* 1945; *A* 1938; *J* 1936) Mgr., Htg. Dept., Comfort Products, Inc., 5521 Wayne Ave., Philadelphia 44, and ● 314 E. Allens Lane, Philadelphia, Pa.

DOMINY, Charles B. (*J* 1942) Mech. Engr., Puget Sound Naval Shipyard, and ● 53-B Baer Blvd., Bremerton, Wash.

DONCEEL, Guillaume T. (*M* 1944) Indus. Engr., ● Oklahoma Natural Gas Co., P. O. Box 1620, Oklahoma City 1, and 1727 Northwest 13th St., Oklahoma City 6, Okla.

DONELSON, William N. (*M* 1943; *J* 1937) Partner, ● Rock & Donelson, 830 Vincent, Cleveland 14, and 4461 Glenview, Warrensville Heights, Cleveland, Ohio.

DONIE, Rowland A. (*A* 1946) Sales Engr., ● Minneapolis-Honeywell Regulator Co., 1007 N. Meridian, Indianapolis 4, and 89 W. Westfield Blvd., Indianapolis, Ind.

DONNELLY, James A.* (*Life Member*; *M* 1904), (Treas., 1912-14), (Board of Governors, 1913), (Council, 1914), Largent, W. Va.

DONNELLY, Joseph F., Sr. (*M* 1943) Combustion Engr., Dist. Sales Mgr., Cleveland Steel Products Corp., 7304 Madison Ave., Cleveland, Ohio, and ● 409 Highland Ave., Upper Montclair, N. J.

DONNELLY, Russell (*M* 1923) Sales Engr., Nash Engineering Co., 420 Lexington Ave., New York 17, N. Y.

DONOHOE, Charles F. (*M* 1941) Tech. Engr., Central Htg. Dept., • The Detroit Edison Co., 2000 Second Ave., Detroit 26, and 10065 Lincoln Dr., Huntington Woods, Mich.

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DONOVAN, Richard F. (*A* 1946) Engr., • General Appliance Engineering Co., and 122 LeTourneau Ct., Toccoa, Ga.

DONOVAN, William J. (*A* 1930) 2239 North 27th St., Philadelphia, Pa.

DOODY, Frank A. (*J* 1946) Appl. Engr., Fulton Sylphon Co., Wrigley Bldg., Chicago, and • 415-B S. Taylor Ave., Oak Park, Ill.

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DORFAN, Morton I. (*M* 1929) Mgr., Dust and Fume Engrg. Div., American Foundry Equipment Co., S. Byrkit Ave., Mishawaka, Ind., and • 1217 Malvern Ave., Pittsburgh 17, Pa.

DORFFI, Arthur A. (*J* 1948; *S* 1947) Jr. Engr., Sohio Petroleum Co., 407 N. Eighth St., P. O. Drawer D-15, St. Louis, Mo.

DORNHEIM, G. A. (*M* 1912; *J* 1906) Vice-Pres., Buensod-Stacey, Inc., 60 East 42nd St., New York 17, and • 15 Hamilton Ave., Bronxville 8, N. Y.

DOSTER, Alexis (*A* 1934) Mfrs. Agt., Box "Y", Litchfield, Conn.

DOUDICAN, Charles T. (*M* 1946) Htg. Engr., M. J. Gibbons Supply Co., 601 E. Monument Ave., Dayton 2, and • 416 Wiltshire Blvd., Dayton 9, Ohio.

DOUGHERTY, Charles P. (*A* 1946) Owner, • Dougherty Heating Co., 826 S.E. Seventh, Portland 14, and 3034 Northeast 22nd, Portland 12, Ore.

DOUGHTY, Charles J. (*M* 1925) Mech. Supvsr. of Constr. and Design, The Austin Co., 19 Rector St., New York 6, and • Apt. 7C, 155 East 49th St., New York 17, N. Y.

DOUGLASS, Thomas C. (*M* 1943) Owner, • 1701 Carmelita Ave., and 1400 Alvarado Ave., Burlingame, Calif.

DOUGLASS, Thomas C., Jr. (*A* 1947) Sales Engr., Western Fiberglas Supply, Ltd., 739 Bryant St., San Francisco 7, and • 359 San Benito Way, San Francisco 16, Calif.

DOVENER, Robert F. (*A* 1941) **Engr.,** • Atchison & Keller, Inc., 1246 Taylor St. N. W., Washington 11, D. C., and 4365 N. Pershing Dr., Arlington, Va.

DOVER, Donald E. (*J* 1945) Refrig. Engr., • Carrier Corp., 419 Boylston St., and 201 Bay State Rd., Boston, Mass.

DOW, Clifford H. (*A* 1947) Engr., • Minneapolis-Honeywell Regulator Co., 799 Beacon St., Boston, and 122 Vernon St., Wakefield, Mass.

DOWDELL, J. R. (*A* 1941) Owner, • J. R. Dowdell & Co., 4024 Swiss Ave., Dallas 4, and 4400 Windsor Pkwy., Dallas 5, Texas.

DOWDY, Rufus B. (*M* 1939) Sales Engr., • Haydn Myer Co., Inc., P. O. Box 746, and 203 Capitol Pkwy., Montgomery, Ala.

DOWLER, Edward A. (*M* 1937) Chief Engr., • B. F. Sturtevant Co. of Canada, Ltd., and 14 Crescent Rd., Galt, Ont., Canada.

DOWNE, Edward R. (*M* 1927) Engr., C. A. Olsen Manufacturing Co., and • 261 E. Broad St., Elyria, Ohio.

DOWNES, Alfred H. (*A* 1937) Draftsman, • Gay Engineering Co., 2730 East 11th St., Los Angeles 23, and 1342½ Bond St., Los Angeles 15, Calif.

DOWNES, Nate W. (*M* 1917), (Council, 1928-30) Asst. Supt. in charge of Bldgs. and Grounds, • School Dist. of Kansas City, Mo., 1840 E. Eighth St., Kansas City 1, and 2119 East 68th St., Kansas City 5, Mo.

DOWNS, Sewell H. (*M* 1931), (*Presidential Member*), (Pres., 1944; 1st Vice-Pres., 1943; 2nd Vice-Pres., 1942; Council, 1936-45) Vice-Pres., Clarage Fan Co., Kalamazoo, and • 1562 Spruce Dr., Kalamazoo 40, Mich.

DRAVAGE, Thom D. (*A* 1945) Htg., Vtg. and Air Cond. Engr., Arthur E. Rowe & Assocs., 1743 East 25th St., Cleveland, and • Chillicothe Rd., R. 2, Willoughby, Ohio.

DRESSELL, Russell E. (*M* 1942; *A* 1938) Mech. Engr., Riggs, Distler & Co., Inc., 216 N. Calvert St., Baltimore 2, and • 3916 Ednor Rd., Baltimore 18, Md.

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DRIEMEYER, R. C. (*A* 1942; *J* 1937) Chief Engr., York Pacific Co., 1229 Fye St., and • 1808 Capitol Ave., Sacramento 14, Calif.

DRIGGS, Alfred A., Jr. (*A* 1947) Mgr., • Westinghouse Electric Corp., Sturtevant Div., 31 Clinton St., Newark, N. J., and R. D. 2, Montgomery, N. Y.

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DRISCOLL, William H.* (*Life Member*; *M* 1904), (*Presidential Member*), (Pres., 1926; 1st Vice-Pres., 1925; 2nd Vice-Pres., 1924; Treas., 1923; Council, 1918-27) Vice-Pres., • Carrier Corp., 300 S. Geddes St., Syracuse, N. Y., and 50 Glenwood Ave., Jersey City, N. J.

DROBA, Charles B. (*M* 1944) Mech. Engr., M. C. Larson, Cons. Engr., 1726 M St. N.W., and • 3412 Oliver St. N.W., Washington, D. C.

DROPKIN, David* (*M* 1942) Assoc. Prof., Mech. Engrg., • College of Engrg., Cornell University, and Slaterville Rd., Ithaca, N. Y.

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DuBOIS, Louis J. (*M* 1931) Westerlin & Campbell Co., 1113 Cornelia Ave., Chicago 13, and • 1012 South Western Ave., Park Ridge, Ill.

DUBRY, Ernest E. (*M* 1924) Supt., Central Htg., Detroit Edison Co., 2000 Second Ave., Detroit 26, and • 9116 Dexter Blvd., Detroit 6, Mich.

DuCHATEAU, Manuel F. (*A* 1942; *J* 1938) Mgr., • Crane Co., 205 S. Lyndon St., and 2307 Fairfield, Greensboro, N. C.

DUDLEY, William H., Jr. (*M* 1945; *A* 1940) Dist. Mgr., The Trane Co., 340 Audubon Blvd., New Orleans 15, La.

DUFAULT, Felix H. (*A* 1936) Mgr., Furnace Div., • General Steel Wares, Ltd., 2355 Delisle St., P. O. Box 248, Montreal 2, and 5115 Bordeaux St., Apt. 6, Montreal 34, Que., Canada.

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DUITCH, Paul R. (*A* 1947) Mech. Engr., • Iowa Sheet Metal Contractors, Inc., 315 Second Ave., and 930 39th St., Des Moines, Iowa.

DUKE, Raymond Q. (*A* 1947) Air Cond. Engr. Bldg. Operation, • The Detroit Edison Co., 2000 Second Ave., Room 314 G. O., Detroit 26, and 621 S. Mildred St., Dearborn, Mich.

DUKEHART, Morton McI. (*M* 1942) Owner, • Morton McI. Dukehart & Co., 801 Maryland Trust Bldg., Baltimore 2, and 419 Woodlawn Rd., Baltimore 10, Md.

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FAUST, Frank H. (*M* 1936; *J* 1930) Mgr., Commercial Engng. Div., Air Cond. Dept., • General Electric Co., 5 Lawrence St., Bloomfield, and 36 Afterglow Ave., Montclair, N. J.

FAUST, Harold G., Jr. (*A* 1947) Sales Engr., • Crane Co., 1328 West 12th St., Kansas City, Mo., and 6010 Fontana, Mission, Kans.

FAVA, Albert A. (*M* 1945) Plant Engr., Atlantic Gelatin Co., Inc., Hill St., Woburn, and • 6 Pine St., Stoneham 80, Mass.

FAVRET, Louis E. (*M* 1945) Pres. and Treas., • Williamson-Favret Furnace Co., 55 E. Goodale St., Columbus 8, and 314 Oakland Park Ave., Columbus 2, Ohio.

FAXON, Harold C. (*M* 1937) 1621–19th St. N.W., Washington, D. C.

FAY, Allyn C. (*A* 1947) Buyer, Steam & Hot Water Htg., Montgomery-Ward & Co., Administration Bldg. 6B, Chicago, and • 127-74 Loveland St., R. F. D. 1, Blue Island, Ill.

FEDER, Nathan (*M* 1947; *J* 1938) Chief Engr., E. Kalisch, Inc., 554 West 48th St., New York, and • 1319 Morrison Ave., New York 59, N. Y.

FEELY, Frank J. (*M* 1935; *A* 1929) Mgr. of Sales, The Taylor Supply Co., 700 Monroe Ave., Detroit, and • 380 Neff Rd., Grosse Pointe 30, Mich.

FEHLIG, John B. (*Life Member*; *M* 1918) Retired, • Warm Air Htg., 528 Delaware St., and 2927 Brooklyn Ave., Kansas City, Mo.

FEHLIG, John B., Jr. (*A* 1941) Asst. Mgr., Excelsior Heating Supply Div., 528 Delaware, Kansas City 6, and • 6412 Paseo, Kansas City 5, Mo.

FEILZER, Joseph H. (*A* 1948; *J* 1944; *S* 1943) 2909-39th Ave. S., Minneapolis 6, Minn.

FEINBERG, Emanuel (*M* 1945; *A* 1944; *J* 1937) Pres., American Thermal Industries, Inc., 440 Illinois, Detroit 1, and • 18667 Ohio, Detroit 21, Mich.

FEIRN, William H. (*M* 1938) Engr., • C. A. Hooper Co., 453 W. Gilman, and Shorewood Hills, Madison, Wis.

FEITEL, J. York (*A* 1943) Pres., • Jordy Engineering Co., 813 Howard Ave., New Orleans 13, and No. 2A, Neron Pl., New Orleans, La.

FELDERMANN, William (*A* 1937) Pres., • Walton Laboratories, Inc., 1186 Grove St., Irvington 11, and 303 Montrose Ave., South Orange, N. J.

FELDMAN, A. M.* (*Life Member*; *M* 1903) Cons. Engr., Retired, and • 320 Central Park West, New York 25, N. Y.

FELDMAN, Morton M. (*J* 1946) Partner, • Phil Feldman & Sons, 938-40 S. Townsend St., Syracuse 3, and 137 Cumberland Ave., Syracuse 9, N. Y.

FELDMAN, Nathan R. (*J* 1946) Air Cond. Engr., • Vent-O Air Conditioning Corp., 526 Fourth Ave., and 205 East 17th St., Brooklyn, N. Y.

FELDSTEIN, Harold (*M* 1947; *A* 1946; *J* 1938) Mgr., Valley Temperature Control Co., 6235 San Fernando Rd., Glendale 1, and • 1726 Maltman Ave., Los Angeles 26, Calif.

FELLOWS, J. R. (*M* 1946) Dept. of Mech. Engrg., • 105 Mech. Engrg. Lab., University of Illinois, and 703 W. California, Urbana, Ill.

FELS, Arthur B. (*Life Member*; *M* 1919) Pres., • The Fels Co., 42 Union St., Portland, and Yarmouth, Me.

FELTWELL, Robert H. (*Life Member*; *M* 1905) Htg. Engr., National Bureau of Standards, Room 9, West Bldg., Washington 25, and • 1347 Michigan Ave. N.E., Washington 17, D. C.

FELZER, William (*A* 1946) Mech. Engr., Shop Supt's. Office, San Francisco Naval Shipyard, and • 801–25th Ave., Apt. 6, San Francisco, Calif.

FENKER, Clement M. (*M* 1946) Engr., A. M. Kenney, Inc., 1211 Enquirer Bldg., Cincinnati 2, and • R. R. 11, Mt. Healthy, Cincinnati 31, Ohio.

FENN, Charles V. (*M* 1945) Branch Mgr., • Carrier Corp., 300 Ivy St. N.E., Atlanta 3, and 124 Vidal Blvd., Decatur, Ga.

FENNER, Everett M. (*M* 1946) Owner and Chief Engr., Scientific Engineering Co., 22 Hobson Ave., Centredale 11, R. I.

FENNER, Walter M. (*A* 1945) Engr.-Secy.-Treas., Central Mill & Plumbing Supply Corp., 46 E. Swan St., and • 1012 Studer Ave., Columbus, Ohio.

FENSTERMAKER, S. E. (*M* 1909) Partner, • S. E. Fenstermaker & Co., 937 Architects & Builders Bldg., Indianapolis 4, and R. R. No. 1, Carmel, Ind.

FENSTERMAKER, Sidney, Jr. (*M* 1945; *J* 1943) S. E. Fenstermaker & Co., 937 Architects & Builders Bldg., Indianapolis 4, and Box 433, R. R. 16, Indianapolis, Ind.

FENSTERMAKER, Ward R. (*A* 1948; *J* 1944) Sales Engr., • John J. Nesbitt, Inc., 215 E. New York St., and 4525 Marcy Lane, Apt. 246, Indianapolis, Ind.

FERDERBER, Murray B., M.D.* (*M* 1938) Physician, 5722 Fifth Ave., Pittsburgh, Pa.

FEREDAY, Maurice (*A* 1946) Owner, • Fereday Plumbing & Heating, 156 S. Third Ave., and 1352 E. Bonneville, Pocatello, Idaho.

FERGESTAD, Marvin L. (*M* 1938; *J* 1935) Pres., • Insulation Engineers, Inc., 2120 Lyndale Ave. S., Minneapolis 5, and 2736 Joppa, Minneapolis 16, Minn.

FERGUSON, Clemon E. (*M* 1944) Owner-Mgr., Clem E. Ferguson Co., 838 Garfield Ave., Salt Lake City, Utah.

FERGUSON, Ralph R. (*M* 1934; *A* 1927; *J* 1925) Mgr., Air Cond. Dept., American Blower Corp., 50 West 40th St., New York, N. Y., and • 77 Edgewood Ave., West Orange, N. J.

FERGUSON, Wallace N. (*A* 1946) Htg. Engr., • Canadian Industries, Ltd., 1155 Beaver Hall Sq., Room 130, Montreal, and 3472 Shuter St. Apt. 2, Montreal 18, Que., Canada.

FERRARA, Anthony L. (*A* 1944) Partner, • Standard Heating Co., 410 W. Lake St., Minneapolis 8, and 443 Buchanan St. N.E., Minneapolis, Minn.

FERRARINI, Joseph (*A* 1947) Engr., Conversions & Surveys, Inc., 90 Broad St., New York 4, N. Y., and • 1721 Queens Lane No. 105, Arlington, Va.

FERRETTI, Julius J. (*A* 1944) New York Mgr., • U. S. Air Conditioning Corp., 420 Lexington Ave., New York 17, and 1814 West 12th St., Brooklyn, N. Y.

FERRIS, Allan F. (*M* 1945) Partner, • Ferris & Hamig, Cons. Engrs., 1706 Olive St., St. Louis 3, and 5078A Wells Ave., St. Louis 13, Mo.

FERRIS, Arthur L. (*A* 1941) Repr., Hart & Cooley Manufacturing Co., 103 Douglas Ave., Toronto, Ont., Canada.

FERRIS, Donald McKenzie (*M* 1944) Mech. Engr., • The Budd Co., 12141 E. Charlevoix, Detroit 14, and 736 Chicago Blvd., Detroit 2, Mich.

FETSCHER, John J. (*M* 1944) Engr., • U. S. Rubber Co., 1230 Ave. of the Americas, New York 20, and 221 Beach 123rd St., Rockaway Park, N. Y.

FICARRA, Francis X. (*A* 1946) Parsons, Brinckerhoff, Hogan & MacDonald, 120 Wall St., New York, and • 665 Ocean Pkwy., Brooklyn 30, N. Y.

FIDELIUS, Walter R. (*M* 1936) Asst. Chief Engr., Optimus Equipment Co., Matawan, and • 335 Broad St., Red Bank, N. J.

FIEDLER, Harry W. (*M* 1923) Owner, • Air Conditioning Utilities, 8 West 40th St., New York, and 16 Dobbs Terrace, Scarsdale, N. Y.

FIELD, Erlund (*A* 1947) Vice-Pres., • Whitty Company, Inc., 86 Western Ave., Boston, and 86 Concord Rd., Weston, Mass.

FIELD, Eugene, Jr. (*S* 1946) Student, Texas A. & M. College, College Station, and • 200 S. Congress, Bryan, Texas.

FIELDNER, A. C.* (*Honorary Member*) Chief, Fuels and Explosives Branch, • Bureau of Mines, U. S. Department of the Interior, Washington 25, and Cosmos Club, Washington, D. C.

FIFE, Charles M. (*A* 1947) Mgr., Electric Home Bureau, • West Penn Power Co., P. O. Box 1736, Pittsburgh 30, and 7919 Union St., Swissvale 18, Pa.

FIFE, G. Donald (*M* 1937; *A* 1931; *J* 1929) Engr., Aerofin Corp., 11 West 42nd St., New York 17, N. Y., and • 20 Ridge Rd., Cos Cob, Conn.

FINCH, Lloyd (*A* 1946) Archt., • 21 C. P. R. Office Bldg., and 1448 Wellington Crescent, Winnipeg, Man., Canada.

FINE, Arthur T. (*A* 1946) Owner and Mgr., • Hartford Oil Heating Co., 161 S. Whitney St., and 94 Warrenton Ave., Hartford 5, Conn.

FINE, Maurice E. (*M* 1948) Chief Mech. Engr., Harold H. Hermann & Assoc. Inc., 701 Enquirer Bldg., Cincinnati 2, and • 2805 Digby Ave., Cincinnati 20, Ohio.

FINK, Robert C. (*M* 1946) Mgr., Industrialaire Co., 1600 Hutchison Ave., and • 2000 Club Rd., Charlotte, N. C.

FINLAY, Alvin E. (*M* 1942) Htg. Engr., Portland Gas & Coke Co., 132 N.W. Flanders St., Portland 9, and • 4919 Northeast 13th Ave., Portland 11, Ore.

FINN, Charles W. (*M* 1944) Pres. and Gen. Mgr., • The Pyramid Co., 320 Eighth Ave. N., Seattle 9, and 529 North 137 St., Seattle, Wash.

FINNELL, Edgar C. (*A* 1948). • Minneapolis-Honeywell Regulator Co., 420 N. Fifth St., and 4520 30th Ave. S., Minneapolis, Minn.

FINNEY, Brandon (*M* 1937) Htg. Engr., Brandon Finney & Assocs., and • 1620 N. Fuller Ave., Hollywood 46, Calif.

FISCHER, Carl S. (*M* 1944) Secy.-Treas., • Fischer Heating & Plumbing Co., 367 Adams Ave., and 1800 Autumn, Memphis, Tenn.

FISCHER, Frank P. (*A* 1940) Owner, • Frank P. Fischer Engineering Co., 342 S. Diamond St., New Orleans, and 1820 Audubon St., New Orleans 18, La.

FISCHER, Fred C. (*A* 1947) Vice-Pres., • Sink & Edwards, 621 E. Ohio St., and 514 N. Dequincy St., Indianapolis, Ind.

FISCHER, William F. (*M* 1947) Asst. Supt., • Edison Marquette Co., 72 W. Adams St., Room 1122, Chicago 3, and 388 Chestnut St., Winnetka, Ill.

FISHER, Albert E. (*A* 1945) Partner, • Kerr Machinery Co., 608 Kerr Bldg., Detroit 26, and 572 Lakeland Ave., Grosse Pointe, Mich.

FISHER, Bert P. (*A* 1943) Owner, • Southern Furnace & Supply Co., P. O. Box 92, Houston 1, and 6528 Rutgers St., Houston 5, Texas.

FISHER, Ernest F. (*M* 1947) Pres., • Faraday Engineering Co., Glenville, Pa.

FISHER, Stanley L. V. (*A* 1946) Trane Company of Canada, Ltd., 4 Mowat Ave., Toronto, and • 43 Nealon Ave., Toronto 6, Ont., Canada.

FITCH, Wilbur R. (*A* 1945) 39 Lewis Rd., Belmont, Mass.

FITTS, Joseph C. (*M* 1930) Secy., • Heating, Piping and Air Conditioning Contractors National Assn., Room 1401, 1250 Avenue of the Americas, New York 20, N. Y., and 215 Kenilworth Rd., Ridgewood, N. J.

FITZ, Jean Chandler (*M* 1938) Precipitator Specialist, Raytheon Manufacturing Co., 60 East 42nd St., New York, and • 405 Webster Ave., New Rochelle, N. Y.

FITZGERALD, Frank R. (*A* 1946) Sales Engr., Minneapolis-Honeywell Regulator Co., 2840 E. Olympic Blvd., Los Angeles, and • 733 W. Enloe St., El Monte, Calif.

FITZGERALD, Matthew J. (*M* 1934) Pres., Standard Asbestos Manufacturing Co., 820 W. Lake St., Chicago, and • 1117 N. Linden Ave., Oak Park, Ill.

FITZGERALD, William E. (*A* 1943; *J* 1936; *S* 1935) Pres., • Fitzgerald Plumbing & Heating Co., Inc., 939 Louisiana Ave., Shreveport, and 1905 Gilbert St., Shreveport 9, La.

FITZSIMONS, J. P. (*M* 1941; *A* 1940; *J* 1934; *S* 1932) Mgr., • Trane Company of Canada, Ltd., 905 Railway Exchange Bldg., 637 Craig St. W., Montreal, and 6091 Terredonne Ave., N. G. D., Montreal, Que., Canada.

FITZSIMONS, Robert H. (*A* 1946) Dist. Mgr., • Trane Company of Canada, Ltd., 63 John St. S., and 63 London St. S., Hamilton, Ont., Canada.

FLAGG, Louis F. (*A* 1947) Sales Engr., Minneapolis-Honeywell Regulator Co., 1919 K St. N.W., Washington, D. C., and • 318 Holly Ave., Takoma Park 12, Md.

FLAGG, William J. (*A* 1947) Chief Engr., • Ohlssons Cape Breweries Ltd., P. O. Box 12, Claremont Cape Point, South Africa.

FLANAGAN, James B. (*A* 1939) Mgr., • Warden King, Ltd., 2104 Bennett St., and 4243 Westhill Ave., N. D. G., Montreal, Que., Canada.

FLANIGAN, William P. (*M* 1948; *J* 1944) Vice-Pres., Lloyd E. Mitchell, Inc., 4650 Reisterstown Rd., and • 5508 Greenleaf Rd., Baltimore, Md.

FLARSHEIM, Clarence A. (*M* 1947; *A* 1940; *J* 1933) Owner, • Clarence A. Flarsheim, 338 Board of Trade Bldg., 10th and Wyandotte, Kansas City 6, and 4415 Roanoke Pkwy., Kansas City 2, Mo.

FLECK, William R. (*A* 1947) Mgr. & Partner, • M & T Furnace Co., 10500 Lorain Ave., and 3054 West 103rd St., Cleveland 11, Ohio.

FLEISHER, Walter L.* (*Life Member*; *M* 1914), (*Presidential Member*), (Pres., 1941; 1st Vice-Pres., 1940; 2nd Vice-Pres., 1939), (Council, 1936-42) Pres., • Air & Refrigeration Corp., 475 Fifth Ave., New York 17, and Saw Mill Farm, New City, N. Y.

FLEISHER, Walter L., Jr. (*A* 1947; *J* 1945) Mance Corp., 400 W. Broadway, New York 12, N. Y.

FLEMING, Clarence L. (*A* 1947) Owner & Operator, • Fleming Refrigeration Co., 805-A M & M Bldg., and 6830 Japonica, Houston, Texas.

FLEMING, James G. (*A* 1946) Sales Engr., Douglas Engineering Co., Ltd., 139 Arlington Ave., Toronto, Ont., Canada.

FLEMING, Paul B. (*M* 1941) Cons. Engr., • Room 406, 1900 Euclid Ave., Cleveland 15, and 20859 Erie Rd., Rocky River, Ohio.

FLETCHER, Saxton W. (*M* 1945) Pres., • J. O. Ross Engineering Corp., 350 Madison Ave., New York 18, and 880 North St., White Plains, N. Y.

FLETTRICH, Harold L. (*A* 1945) Owner, 2314 Iberville St., and • 5828 Catina St., New Orleans, La.

FLINK, Carl H. (*M* 1923) Tech. Secy., • American Society of Heating and Ventilating Engineers, 51 Madison Ave., New York 10, and 166 Summit Ave., Mt. Vernon, N. Y.

FLINN, George S. (*M* 1947; *A* 1946) Air Cond. Engr., J. J. Nolan & Co., 78 Washington, and • 490 Greer, Memphis, Tenn.

FLINN, J. D. (*M* 1943) Partner, • Flinn & Thorpe, Engrs., 119 Madison Ave., and 1516 Vollintine Ave., Memphis, Tenn.

FLINT, Coll T. (*M* 1919) Sales Mgr., The H. B. Smith Co., Inc., 104 Hanover St., Boston, and • 8 Searle Ave., Brookline, Mass.

FLOCKE, Kenneth N. (*A* 1946; *J* 1940) Chief Indus. Hygiene Engr., Oregon State Industrial Accident Commission, c/o Oregon State Board of Health, 1022 Southwest 11th Ave., Portland 5, and • Apt. 24, 1515 N. Ainsworth St., Portland 11, Ore.

FLOETER, Elliott G., Jr. (*A* 1946) Sales Engr., • Way Engineering Co., P. O. Box 8066, Houston 4, and 2706 Albans Rd., Houston, Texas.

FLORETH, John J. (*M* 1939) Gen. Sales Mgr., Westerlin & Campbell Co., 185 N. Wabash Ave., Chicago 1, and • 924 S. Crescent Ave., Park Ridge, Ill.

FLY, E. Paul (*A* 1947; *J* 1942) Vice-Pres., Geo. M. Fly & Sons, 1706 Church St., Nashville 3, and • Kimbark Dr., 3, Nashville 5, Tenn.

FOGG, Joseph H. (*A* 1942; *J* 1940) Naval Archt., U. S. Maritime Commission, Dept. of Commerce Bldg., Washington, D. C., and • 217 E. Bellefonte Ave., Alexandria, Va.

FOLEY, John J. (*A* 1938) Pres., • Universal Refrigeration, Ltd., 593 Adelaide St. W., and 176 Cortleigh Blvd., Toronto, Ont., Canada.

FOLSOM, Rolfe A. (*M* 1938) Owner, The Interlocking Block Co., P. O. Box 387, San Jose 3, and • 316 Crest Dr., San Jose 12, Calif.

FOOTE, Avery G. (*M* 1943) Regional Commercial Sales Mgr., • Frigidaire Division, General Motors Corp., 1355 Market St., San Francisco 3, and 365 Vermont Ave., Berkeley 7, Calif.

FOOTE, Earle E. (*M* 1936) Gen. Supt., Consumers Central Heating Co., 108 East 11th St., and Rt. 12, Box 501A, Tacoma, Wash.

FORAN, Laverne E. (*J* 1948) Mech. Engr., • Chicago Steel Furnace Co., 9326 S. Anthony, Chicago 17, and 1200 E. Madison Park, Chicago 15, Ill.

FORDERBRUGEN, Kevin J. (*A* 1941; *J* 1938), Chief Engr., • Minnesota Valley Natural Gas Co., and 1202 S. Minnesota St., St. Peter, Minn.

FOREST, Leo (*A* 1947) Owner, Godin Sheet Metal Works Reg'd., 547 de Lasalle, Montreal, and • Co. Rouville St., Hilaire, Que., Canada.

FORFAR, D. M. (*M* 1917) Mech. Engr., • Grinnell Co., Inc., 240 Seventh Ave. S., and 4817 Emerson Ave. S., Minneapolis, Minn.

FORRESTER, Charles O. (*A* 1945) Mech. Engr., Federal Public Housing Authority, 801 Georgia Savings Bank Bldg., and • 278-12th St. N.E., Atlanta, Ga.

FORRESTER, Norman J. (*A* 1936) Mgr., Contract Div., The Garth Co., 750 Belair Ave., and • 23 Nelson Ave., Montreal West, Que., Canada.

FORSBERG, William (*M* 1919) Secy., The Hopson & Chapin Manufacturing Co., 231 State St., New London, Conn.

FORSLUND, Oliver A. (*M* 1936) Owner, Forslund Pump & Machinery Co., 1717-19 Main St., Kansas City 8, and • 108th St. and State Line, Kansas City 5, Mo.

FORSYTH, Stuart L. (*M* 1944) Mgr., Elec. Htg. for Homes, Westinghouse Electric Corp., 5915 Green St., Emeryville 8, Calif.

FOSS, Benjamin S., Jr. (*A* 1944) Texas Repr., • The Lewin-Mathes Co., 711 Construction Bldg., Dallas 1, and "Halfway Hill," Rt. 7, Dallas, Texas.

FOSS, Edwin R. (*A* 1936) Dist. Mgr., • The Powers Regulator Co., 142 Spring St. N.W., Atlanta 3, and 257 Bolling Rd. N.E., Atlanta, Ga.

FOSTER, Charles (*Life Member*; *M* 1923) Cons. Engr., • 316 Medical Arts Bldg., Duluth 2, and 2831 E. First St., Duluth, Minn.

FOULDS, P. A. L. (*Life Member*; *M* 1916) Cons. Engr., 72 Whitin Ave., Rever 51, Mass.

FOULGER, Sid W. (*A* 1946) Partner, • Thermal Engineering Co., P. O. Box 446, Salt Lake City, and Kaysville, Utah.

FOWLES, Harry H. (*A* 1940; *J* 1934) Engr. and Estimator, L. P. Bail, 45 Riverside St., Lewiston, and • 154 Field Ave., Auburn, Me.

FOX, Ernest (*M* 1935) Htg. Engr., • C. A. Dunham Co., Ltd., 1139 Bay St., Toronto, and 531 Rushton Rd., Toronto, Ont., Canada.

FOX, Ernest C. (*M* 1944) Vice-Pres., • Hager-Fox Heating & Refrigeration Co., 1125 S. Pennsylvania Ave., and 928 W. Michigan Ave., Lansing, Mich.

FOX, Francis J. (*A* 1945) Owner, • Gas Heat Engineering Co., 345 E. Lake St., Minneapolis 8, and 3501-11th Ave. S., Minneapolis 7, Minn.

FOX, John H. (*M* 1935) Sales Mgr., • Minneapolis-Honeywell Regulator Co., Ltd., Vanderhoff Ave., Toronto 12, and 37 Macdonell Ave., Toronto 3, Ont., Canada.

FOX, Winford L. (*A* 1944) Engr., U. S. Machine Corp., Lebanon, and • 1912 N. Meridian St., Indianapolis 2, Ind.

FOXHALL, William B. (*A* 1946) Assoc. Editor, Heating & Ventilating, 148 Lafayette St., New York, and • 35-15-84th St., Jackson Heights, N. Y.

FRAMBACH, Frederick S. (*M* 1946) Engr., The Bahnson Co., Winston-Salem, N. C., and • 703 Embree Crescent, Westfield, N. J.

FRANCK, Peter (*A* 1947; *J* 1938) Armo Cooling & Ventilating Co., 30 West 15th St., New York 11, and • 59 Bradley Rd., Scarsdale, N. Y.

FRANK, George D. (*M* 1945) Mgr., Indus. Div., York-Shipley, Inc., and • R. D. 5, York, Pa.

FRANK, John M. (*M* 1918; *A* 1912) Pres., • Ilg Electric Ventilating Co., 2850 N. Crawford Ave., Chicago, and 1152 Chatfield Rd., Hubbard Woods, Ill.

FRANK, Milton S. (*J* 1948) Chem. Engr., • Neil H. Peterson Co., 1129 Folsom St., and 860 Bush St., Apt. 2, San Francisco, Calif.

FRANKEL, Gilbert S. (*M* 1926) Mgr., Federal and Marine Dept., Buffalo Forge Co., 310 Woodward Bldg., Washington 5, D. C., and • 5800 Kirkside Dr., Chevy Chase 15, Md.

FRANKENFELD, Henry V. (*A* 1947) • National Plumbing & Heating, 4004 N. Fourth St., Albuquerque, New Mexico, and 1521 N. Western, Oklahoma City, Okla

FRANKFURT, W. W. (*M* 1943) Cons. Engr., • Coston & Frankfurt, Archts. & Engrs., 519 Apco Tower, and 1524 Northwest 38th St., Oklahoma City, Okla.

FRANKHOUSER, Elmer V. (*M* 1946) Supt. of Power, Radio Corporation of America, R. C. A. Victor Div., Camden, N. J., and • 174 Glencoe Rd., Upper Darby, Pa.

FRANKLE, Harry R. (*M* 1941) Partner, • Midwest Air Control, 510 Third St., and 547-44th St., Des Moines, Ia.

FRANKLE, Milton S. (*A* 1946) Vice-Pres. and Sales Mgr., • Air Control, Inc., 720 Brandeis Theatre Bldg., Omaha, Nebr., and 263 West End Ave., Apt. 20, New York, N. Y.

FRANKLIN, John K. (*A* 1948) Htg. Engr., McCrea Equipment Co., • 516 Second St. N.W., and 514 Second St. N.W., Washington 1, D. C.

FRANKLIN, Ralph S. (*M* 1919) Mech. Engr., Lockwood Greene Engineers, Inc., 40 Central St., Boston, and • 320 Grove St., Melrose, Mass.

FRANKLIN, Samuel H., Jr. (*A* 1938) Pres., • Virginia Air Conditioning Co., Inc., 1419 Park Ave., and 204 Colonial Ct., Lynchburg, Va.

FRASER, George M. (*A* 1946) Archt. Service Representative, United States Gypsum Co., Chicago, and • 314 Lee St., Evanston, Ill.

FRASER, James J. (*A* 1936) Managing Dir., Honeywell-Brown, Ltd., 1 Wadsworth Rd., Perivale, Greenford, and 29 Wellesley Rd., Strawberry Hill, Middlesex, England.

FRAZEE, Francis B. (*A* 1946) Appl. and Sales Engr., Westerlin & Campbell Co., 1113 W. Cornelia St., Chicago 13, and • 5168 N. Lovejoy Ave., Chicago 30, Ill.

FRAZIER, J. Earl (*A* 1936) Pres. and Secy., • Frazier-Simplex, Inc., 436 E. Beau St., and 7 Wilmont Ave., Washington, Pa.

FREAN, Frederick C. (*A* 1948) Tech. Dir., • The Air Treatment Engineering Co. Ltd., 100 Gelderd Rd., Leeds 12, and 15 The Lane, Alwoodley, Leeds, England.

FREDERICK, Holmes W. (*M* 1937) Asst. Dir., Dept. of Buildings and Grounds, • 301 University Hall, Columbia University, New York 27, N. Y., and R. D. 1, Box 3, Riverside Ave., Riverside, Conn.

FREDERICK, Vernon L. (*A* 1946) Owner, Mech. Contr., 2217 M St. N.W., and • 3805 S St. N.W., Washington, D. C.

FREEMAN, Alfred W. (*J* 1940; *S* 1939) Engr., • The Freeman Co., 121 Greenpoint Ave., Brooklyn 22, and 130-06-219th St., Springfield Gardens 13, N. Y.

FREEMAN, Cassius W. (*M* 1945) Chief Designer and Assoc., • Paul D. Bemis, 36 Pearl St., Hartford 3, and 290 Forest St., East Hartford, Conn.

FREEMAN, J. Albert (*A* 1940; *J* 1938) Partner Engr., • Western Engineering Co., 2105 S.E. Ninth Ave., Portland 14, and 4436 S.W. Dosch Rd., Portland 1, Ore.

FREEMAN, Lewis E. (*A* 1946) Mgr., Plbg. and Htg. Dept., • Sullivan Hardware Co., 331 W. Washington St., and 10 Tindal Ave., Greenville, S. C.

FREIJE, W. F. (*M* 1943) Mgr., Refrig. Div., • Hayes Brothers, Inc., 236 W. Vermont St., Indianapolis 4, and 5411 W. Morris St., Indianapolis 8, Ind.

FREITAG, Frederic G. (*M* 1932) Lake Hill, Ulster Co., N. Y.

FREITES, Andres A. (*J* 1945) Constr. and Maint. Supvsr., • Esso Standard Oil (Caribbean), S. A., P. O. Box 1198, and Ave. Independencia 34, Ciudad Trujillo, Dominican Republic.

FRENCH, Donald (*M* 1926) Vice-Pres., in Charge of Engrg. Div., • Carrier Corp., 300 S. Geddes St., Syracuse 1, and Cazenovia, N. Y.

FRENSDORF, Stuart F. (*A* 1947) Sales Engr., Slawson Equipment Co., Inc., 1792 East 40th St., Cleveland 3, and • 12700 Shaker Blvd., Cleveland 20, Ohio.

FRENTZEL, Herman C. (*M* 1936) Cons. Engr., Frentzel Engineering Co., 724 E. Mason St., Milwaukee 2, and • 4303 N. Wildwood Ave., Milwaukee 11, Wis.

FREY, George W. (*A* 1946) Vice-Pres., • Central Supply Co., 2929 Fourth Ave. S., Minneapolis 8, and 4736-12th Ave. S., Minneapolis 7, Minn.

FREYDER, G. Gill (*A* 1945) Air Cond. Engr., • Commonwealth Edison Co., 72 W. Adams St., Chicago 90, and 131 Clinton St., Park Ridge, Ill.

FRICKE, Robert A. (*S* 1947) Student, Michigan College of Mining & Technology, and • Box 643, Houghton, Mich.

FRIEDLER, Joseph J., Jr. (*M* 1940) Dist. Mgr., • Ilg Electric Ventilating Co., 304 Natchez Bldg., New Orleans 12, and 500 Audubon Blvd., New Orleans 15, La.

FRIEDLIEB, Morton J. (*J* 1942) Plant Engr., Super Electric Products Corp., 1057 Summit Ave., Jersey City, N. J., and • 2417 Dickens Ave., Far Rockaway, L. I., N. Y.

FRIEDLINE, James M. (*A* 1942; *J* 1937) Capt., 0317228, Hdq. 79th Engr., Const. Bn., A. P. O. 74, San Francisco, Calif., and • Plymouth, Ia.

FRIEDMAN, Arthur (*A* 1936) Pres., • Air Controls, Inc., 2310 Superior Ave., Cleveland 14, and 15700 S. Morland Blvd., Shaker Heights, Ohio.

FRIEDMAN, David H., Jr. (*M* 1936) Major, 531 Whitney Ave., New Haven, Conn.

FRIEDMAN, F. J.* (*M* 1921) Cons. Engr., • McDougall & Friedman, 1235 McGill College Ave., Montreal 2, Que., Canada.

FRIEDMAN, Milton (*A* 1939; *J* 1935; *S* 1933) 333 West End Ave., Apt. 14C, New York, N. Y.

FRIEND, Walter F. (*M* 1941) Mech. Engr., • Ebasco Services, Inc., 2 Rector St., New York 6, and 470 West 24th St., New York 11, N. Y.

FRISSE, John L. (*A* 1945) Owner, The Thermal Products Co., 4500 Euclid Ave., Cleveland 3, and • 17412 Shelburne Rd., Cleveland Heights 18, Ohio.

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FROELICH, H. Allen (*A* 1939) Owner, • H. Allen Froelich, Air Conditioning & Appliances, 110 W. Seventh St., and 728 W. Chestnut St., Junction City, Kans.

FROESE, E. A. (*M* 1944) Branch Mgr., York Corp., 804 Security Bldg., Denver 2, and • 1922 Locust St., Denver 7, Colo.

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FUITE, Richard J. (*A* 1945) Dist. Repr., • Hoffman Specialty Co., 780 Natoma St., San Francisco 3, and 2300 N. Point St., San Francisco 23, Calif.

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FULLMAN, James B. (*A* 1946; *J* 1941) Arch. Repr., A. M. Byers Co., 30 Rockefeller Plaza, New York 20, N. Y., and • Scofieldtown Rd. & Woodley Lane, R. D. 2, Stamford, Conn.

FULMOR, Ira P. (*M* 1942) Owner, • Air Conditioning Co., of Southern California, 1003-1005 Santa Fe Ave., Los Angeles 21, and 325 Arnaz Dr., Los Angeles 36, Calif.

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GABLE, H. R.* (*A* 1943) Design Engr., • Union Steel Products Co., 500 N. Berrien, and 917 N. Clinton, Albion, Mich.

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GAMBLE, Cary B. (*M* 1940; *A* 1935) Partner, Cary B. Gamble & Assocs., 314½ St. Charles Ave., New Orleans 12, and • 3432 Upperline St., New Orleans 15, La.

GAMMILL, O. Eldrige, Jr. (*M* 1940; *A* 1937; *J* 1930) Dir. of Sales (Heavy Machinery), Carrier Corp., 300 S. Geddes St., Syracuse 1, and • 403 Oak St., Syracuse, N. Y.

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GANT, H. P.* (*M* 1915), (*Presidential Member*), (Pres., 1923; 1st Vice-Pres., 1922; 2nd Vice-Pres., 1921), (Council, 1918; 1921-24) R. D. 1, Glenmore, Pa.

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GEIGER, Irvin H. (*M* 1919) Reg. Prof. Engr., • 410 Telegraph Bldg., and 240 Maclay St., Harrisburg, Pa.

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GEISER, Richard A. (*A* 1947) Engr., • Lincoln Bouillon & Associates, 426–1411 Fourth Ave. Bldg., and 4830 East 43rd, Seattle, Wash.

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GERDSEN, Arno H. (*A* 1945) Pres., • The A. H. Gerdsen Co., 224 E. Second St., Cincinnati 2, and R. R. 14, Beechgrove Dr., Cincinnati 11, Ohio.

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GERRISH, Grenville B. (*M* 1944; *A* 1936; *J* 1930) Pres., • Wolverine Equipment Co., 31 Main St., Cambridge 42, and 26 Standish Rd., Melrose 76, Mass.

GERRISH, Harry E. (*Life Member*; *M* 1910), (Council, 1919) Pres., • Morgan-Gerrish Co., 1111 Nicollet Ave., Room 370, Minneapolis 2, and 4534 S. Fremont Ave., Minneapolis 9, Minn.

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GERSTENBERGER, Edgar J. (*A* 1938) Secy.-Treas., Glendale Supply Co., 1819 W. Glendale Ave., Milwaukee 9, and • 3824 North 17th St., Milwaukee 6, Wis.

GESSELL, E. T. (*M* 1941) • W. E. Lewis & Co., 610 Thomas Bldg., Dallas 1, and 2705 E. Amherst, Dallas 5, Texas.

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GHOSE, Khagendra N. (*A* 1938) Cons. Engr., 17 State St., New York, N. Y., and • 39 Ramkanta Bose St., Bagh Bazar, Calcutta, India.

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GIBBONS, Michael J., Jr. (*A* 1944) Htg. Engr., M. J. Gibbons Supply Co., 601 E. Monument Ave., Dayton 2, and • 206 Canterbury Dr., Dayton 9, Ohio.

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GILBERT, I. Wolfe (*A* 1945) Co-Owner, Gilbert & Knight Co., 1300 Broad St., and • 223 Pleasant St., Utica, N. Y.

GILBERT, Leslie S. (*M* 1937) Owner, • Gilbert Engineering Co., 1305 Liberty Bank Bldg., Dallas 1, Texas.

GILBERT, Thomas (*A* 1940) Sales Engr., Empire Brass Manufacturing Co., Ltd., 20 Jackson St. W., Hamilton, and • 12 South Drive, St. Catharines, Ont., Canada.

GILBOY, John P., Jr. (*M* 1941) Cons. Engr., • John P. Gilboy Co., 300 Bowman Bldg., and 1606 Sanderson Ave., Scranton, Pa.

GILBOY, William O. (*M* 1945) Appl. Engrg. Supvsr., Carrier Corp., 300 S. Geddes St., and • 954 Lancaster Ave., Syracuse, N. Y.

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GILLE, Hadar B. (*M* 1930) Cons. Engr., Hugo Theorells Ingeniorsbyra AB, Lagerlofsgatan 8, Stockholm, and • Svanhildsvagen 19, Nockeby, Sweden.

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GLANZER, Clarence J. (*M* 1944) Vice-Pres., • Merit Machine Co., Merit Appliances Div., Box 84, Northfield, and Vesta Ave., Northfield Center, Ohio.

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GOODWIN, Walter C. (*M* 1945) Mgr. of the Precipitron Dept., Westinghouse Electric, Hyde Park, Boston 36, and • 503 Rock Rd., Needham, Mass.

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GORDON, Hugh H. W. (*A* 1946) Gen. Mgr., ● Air Conditioning & Engineering Co., Ltd., 33 Wepener St., Booysans, and "Enthaba," P. O. Sandown, Johannesburg, South Africa.

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GOTTSCHALL, Walter C. (*A* 1945) Pres. and Estimator, Industrial Insulation, Inc., Terminal Office Bldg., Pittsburgh 19, and ● 530 Hillcrest Pl., Pittsburgh 16, Pa.

GOTTWALD, C. (*Life Member*; *A* 1916) Pres., ● The Ric-wil Co., 1562 Union Commerce Bldg., Cleveland, and 2225 Stillman Rd., Cleveland Heights, Ohio.

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GOULD, James L. (*A* 1948; *J* 1942) Pilot, Air Corps, Columbus, Miss., and ● 1701 Poyntz Ave., Manhattan, Kans.

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GRAHAM, F. D. (*M* 1940) ● York Corp., 509 Delta Bldg., New Orleans 12, and 420 Betz Pl., New Orleans 20, La.

GRAHAM, Robert L. (*A* 1947) Br. Mgr., ● American Blower Corp., 301 National Theatre Bldg., Richmond 19, and 702 Spottswood Rd., Spottswood Park, Richmond 21, Va.

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GRANT, Walter A.* (*M* 1943; *A* 1933; *J* 1929) Dir. of Research, Carrier Corp., Syracuse, and ● 219 Huntleigh Ave., Fayetteville, N. Y.

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GREENLAND, Sidney F. (*M* 1934) Tech. Htg. and Vent. Consultant, J. Brockhouse & Co., Ltd., West Bromwich, Staffs., and • 75 Grestone Ave., Handsworth Wood, Birmingham 20, England.

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GRIEFNOW, Otto W. (*A* 1947) Chief Engr., • The Waterman Waterbury Co., 1121 Jackson St. N.E., Minneapolis 13, and 2610 Thomas Ave. N., Minneapolis, Minn.

GRIESS, Philip G. (*M* 1937) Mech. Engr., Walter Kidde, Constructors, Inc., 140 Cedar St., New York, N. Y., and • 189 Walnut Ave., Bogota, N. J.

GRIEST, Kermit C. (*A* 1940; *J* 1936) C W/O, Commander Service Force, • Pacific Fleet, F.P.O., San Francisco, Calif., and 38 Greenlee Rd., Pittsburgh 10, Pa.

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GRIFFIN, Charles J. (*M* 1940) Lt. (jg), and • 8231 S. Loomis Blvd., Chicago, Ill.

GRIFFIN, DeWitt C. (*M* 1943) Owner, • DeWitt C. Griffin & Assocs., 717 Lloyd Bldg., Seattle 1, and 6521–32nd N.W., Seattle 7, Wash.

GRIFFITH, Claude A. (*A* 1938) Htg. and Vtg. Engr., Griffith Air Conditioning Service, and • 16 Altamont Terrace, Cumberland, Md.

GRIFFITH, H. T. (*M* 1938) Partner, • c/o Lincoln Bouillon & Assocs., 426–1411 Fourth Ave. Bldg., and 1909 Third Ave. W., Seattle, Wash.

GRIFFITH, Joseph B. (*A* 1942; *J* 1938) Works Mgr., Bryant Heater Co., and • 902 Rusk, Tyler, Texas.

GRIGG, James L. (*A* 1945) Pres., Acme Sheet Metal Corp., 2316 Gosnold Ave., Norfolk, Va.

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GRIMMER, Richard A. (*A* 1946) Mech. Engr., R. K. Werner, Cons. Engr., 316 W. T. Waggoner Bldg., Fort Worth, and • 3233 Waits Ave., Fort Worth 4, Texas.

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GRISWOLD, Arthur S. (*M* 1945) Staff Engr., Central Htg. Dept., • The Detroit Edison Co., 2000 Second Ave., Detroit, and 5015 Pon Valley, Bloomfield Hills, Mich.

GRISWOLD, Edgar A. (*A* 1945) Cons. and Design Engr., and • 6641 Pollard St., Los Angeles 42, Calif.

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GROSS, Lyman C. (*M* 1931) • Lyman C. Gross-Cons. Engr., 432 Sexton Bldg., Minneapolis 15, and 5324 Oaklawn Ave., Minneapolis 10, Minn.

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GROSS, Victor L. (*A* 1944) • 281 Storer Ave., New Rochelle, N. Y.

GROSSENBACHER, Henry E. (*A* 1938) Pres., • Grossenbacher Furnace Co., Inc., 9416 W. Milton Ave., and 9741 Lackland Rd., Overland 14, Mo.

GROSSMAN, F. Arthur (*A* 1942; *J* 1938; *S* 1937) Air Cond. Engr., Servel, Inc., 122 S. Michigan Ave., Chicago 3, and • 512 Miller Dr., Elgin, Ill.

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GROSVOLD, F. E. (*M* 1944) Owner, • F. E. Grosvold Heating & Plumbing, 417 Wisconsin St., and 711 E. Grand Ave., Eau Claire, Wis.

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GRUENDEL, William C. (*A* 1947) Htg. Sales Engr., McKee Plumbing Supply Co., 2701 St. Clair Ave., Cleveland 14, and • 83 East 233rd, Euclid 17, Ohio.

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GRUTZMACHER, Robert L. (*M* 1945) Vice-Pres., • Natural Gas Equipment, Inc., 540 Petroleum Bldg., Los Angeles 15, and 2121 N. Foothill Blvd., Altadena, Calif.

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GUENTHER, Clarence G. (*A* 1947) Mgr.-Owner, • Air Flow Engrg. Co., 519 N. Santa Fe, and 606 W. Evans, Pueblo, Colo.

GUEST, James F. (*J* 1948) Sales Engr., Earnshaw Sheet Metal Supply, and • 96 Glenwood Heights, Mansfield, Ohio.

GUEST, P. L., Jr. (*A* 1939) Owner, • P. L. Guest Sales Co., 311 Piedmont Bldg., and 716 Dover Rd., Greensboro, N. C.

GUEST, Ross Burton (*M* 1945; *A* 1940) Owner and Mgr., • The Guest Sheet Metal Works, 827-37 Dryades St., New Orleans 13, and 1028 City Park Ave., New Orleans, La.

GUIBERT, Raul (*A* 1947) Contracting Engr., • Lavalle 1473, and Montes de Oca 41, Buenos Aires, Argentina, S. A.

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GUNDERSEN, Reidar (*M* 1946) Engr., • Calefaccion "Watersteam", Sarmiento 470, and Sucre 3759, Buenos Aires, Argentina, S. A.

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GUNZEL, Rudolph M. (*M* 1942) Sales Repr., • R. M. Gunzel & Co., 320 Crocker St., Los Angeles 13, and 375 LaMirada Ave., San Marino 9, Calif.

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HAIRSTON, Joseph T. (*A* 1947) Sales Mgr., H. J. Swanson Co., 435 Locust Ave., Long Beach 2, and • 820 East 61st St., Long Beach 5, Calif.

HAITMANEK, Louis M. (*A* 1938) Htg., Vtg., & Air Cond. Engr., and • 217 Rose St., Newark 3, N. J.

HAJEK, William J. (*M* 1945) P. O. Box 405, Knoxville, Tenn.

HAKES, Leon M. (*M* 1932; *J* 1929) Resident Repr., • Warren Webster & Co., 210 Reynolds Arcade Bldg., Rochester 4, and 144 Inglewood Dr., Rochester 11, N. Y.

HALE, Fred J. (*M* 1936) Mgr., • Empire Sheet Metal Works, Ltd., 1606 W. First Ave., and 995 Mathers Ave. W., Vancouver, B. C., Canada.
HALEY, Harry S.* (*M* 1914) Owner, Cons. Engr., • 58 Sutter St., San Francisco 4, and 735–21st Ave., San Francisco, Calif.
HALEY, Robert T. (*A* 1943) Mgr., House Heating Dept., • Minneapolis Gas Light Co., 739 Marquette Ave., and 5340 Beard Ave. S., Minneapolis, Minn.
HALL, Elmo (*M* 1944) 1130 E. Yale St., Englewood, Colo.
HALL, George (*A* 1937) Pres., • Hyland Hall & Co., 218 N. Bassett St., Madison 3, and 4201 Wanetan Trail, Madison 5, Wis.
HALL, John A. (*M* 1943) Sales Engr., • A. L. Vanderhoof, Inc., 233 Hanna Bldg., Cleveland 15, and 11030 Granger Rd., Garfield Heights, Ohio.
HALL, John R. (*M*1937; *J* 1932) Vice Pres. & Gen. Mgr., Industrial Ovens, Inc., 13825 Triskett Rd., Cleveland 11, and • 17700 Fries Ave., Lakewood 7, Ohio.
HALL, Mora S. (*M* 1934) Owner, Colony Construction Co., P. O. Box 201, Dickinson, Texas.
HALL, Norman H. (*A* 1945) Supt. of Service, • East Ohio Gas Co., 1405 E. Sixth St., Cleveland 14, and 147 Beachview Rd., Willoughby, Ohio.
HALL, Robert E. (*S* 1947) Student, University of Oklahoma, Norman, Okla., and • 7346 Colgate Ave., University City, Mo.
HALL, Robert S. (*J* 1947) Sales Engr., • Companhia Industria & Comercio Glossop, Rua Florencio de Abreu 438, and Rua Monte Alegre 211, Sao Paulo, Brazil.
HALL, Roger E. (*A* 1947) Engr., Alhambra Sheet Metal, 2007 Mission Rd., Alhambra, and • 444 S. Madison, Pasadena, Calif.
HALLE, Simon (*M* 1946) Owner-Mgr., • Halle's, 119-121 N. Nevada Ave., Colorado Springs, Colo.
HALLENBECK, C. W. (*M* 1944) Dist. Engr., • T. C. Heyward, 1408 Independence Bldg., Charlotte, and 2157 Norton Rd., Charlotte 4, N.C.
HALSTEAD, William R. (*J* 1948; *S* 1947) Htg. Repr., • Conditioned Air Engineers, Inc., 169 Marietta St. N.W., and 377 Tenth St. N.E., Atlanta, Ga.
HALT, Howard R. (*M* 1943) Mgr., Htg. Div., Thos. J. Sheehan Co., 2233 Olive St., St. Louis 3, and • 8729 Annetta Ave., St. Louis 15, Mo.
HAMACHER, Karl F. (*M* 1938) Partner, • Hamacher & Williams, 2540 W. Wells St., Milwaukee 3, and 4387 S. Austin St., Milwaukee 7, Wis.
HAMAKER, Hendrik J. (*M* 1946) Managing Dir., • N. V. Technische Maatschappij, Heringa en Wuthrich, Zijlweg 133, Haarlem, and Veursche weg 138, Voorschoten, Holland.
HAMBLEY, Charles J. (*S* 1947) Student, Purdue University, Lafayette, and • 331 Northwestern Ave., West Lafayette, Ind.
HAMBLIN, Clyde M. (*M* 1943) Principal Engr. (Air Cond.), Bureau of Ships, Navy Dept., Washington, and • 1429 Iris St. N.W., Washington 12, D. C.
HAMER, Fred S. (*M* 1945) Design Engr., Surface Combustion Corp., 400 Dublin Ave., Columbus, and • 2448 Northwest Blvd., Columbus 8, Ohio.
HAMIG, Louis L. (*M* 1941; *A* 1940; *J* 1935) Partner, • Ferris & Hamig, Cons. Engrs., 1706 Olive St., St. Louis 3, and 7530 Buckingham Dr., Clayton 5, Mo.
HAMILTON, M. S. (*M* 1942) Southeastern Sales Mgr., Air Cond. Controls Div., Minneapolis-Honeywell Regulator Co., 5 N. Rhodes Center, and • 3372 Walters Ct. N.E., Atlanta, Ga.
HAMLET, F. A. (*M* 1944; *A* 1936) Branch Office Mgr., • C. A. Dunham Co., Ltd., Dominion Sq. Bldg., Room 832, 1010 St. Catherine St. W., Montreal 2, and Grove Hotel, Beaconsfield, Pointe Claire, Que., Canada.
HAMLIN, James B. (*A* 1937) Capt., U. S. Engineers Office, and • 3695 Highland Park Pl., Memphis, Tenn.
HAMLIN, Millard R. (*M* 1946) Mfrs. Repr., • 20 S. Third St., Room 224, Columbus 15, and 429 Piedmont Rd., Columbus 2, Ohio.
HAMM, John G. (*J* 1947) Sales Engr. • The Trane Co., 850 Cromwell Ave., St. Paul 4, and 3300 Fremont Ave. S., Minneapolis 8, Minn.
HAMMEKEN, L. Palacios (*S* 1947) Student, National University of Mexico, and • Sta. Maria La Ribera 63, Mexico, D. F., Mexico.
HAMMETT, Lewis D. (*S* 1947) Student, • Texas A. & M. College, Box 1115, College Station, and • 714 Florey St., Kilgore, Texas.
HANBURGER, Fred W. (*M* 1938) Cons. Engr., 252 West 76th St., New York 27, N. Y.
HANCOCK, Floyd A. (*A* 1947) Engr., • The Auer Register Co., 3608 Payne Ave., and 628 E. 96th St., Cleveland, Ohio.
HAND, William L. (*M* 1944) Pres., • W. H. Engineering Co., 4102 S. LaSalle St., Chicago 9, and 8832 Dante Ave., Chicago 19, Ill.
HANDMAN, Norman J. (*J* 1946) Appl. Engr., R. B. Rogers Co., Inc., 1120 Leggett Ave., and • 2000 Washington Ave., New York, N. Y.
HANEY, Arnold A. (*A* 1947) Mgr., Refrig. & Air Cond. Div., • N. O. Nelson Co., 1701 Franklin, Houston, and 803 Westway, Galena Park, Texas.
HANFMANN, Alexander M. (*M* 1947) Factory Planning Engr., Western Electric Co., Electronics Shops, 118 E. Susquehanna St., and • 2014 Washington St., Allentown, Pa.
HANKINS, Richard P. (*A* 1947) Cons. Engr., • 303 Crenshaw Bldg., Third & Main Sts., Richmond 19, and 1202 Park Ave., Richmond 20, Va.
HANKS, Charles M. (*A* 1947) Control Application Engr., • Parker Building Specialties, Inc., 1066 Howard St., San Francisco, and P. O. Box 316, Sausalito, Calif.
HANLEIN, Joseph H. (*M* 1937) Vice-Pres., • Wilberding Co., Inc., 1822 Eye St. N.W., Washington 6, and 5420 Connecticut Ave. N.W., Washington, D. C.
HANLEY, Edward V. (*A* 1933) Pres., • S. V. Hanley Co., 1653 N. Farwell Ave., Milwaukee 2, and 844 E. Birch Ave., Whitefish Bay 11, Wis.
HANLEY, T. F., Jr. (*M* 1933) Pres., Hanley & Co., 1503 S. Michigan Ave., and • 1640 East 50th St., Chicago, Ill.
HANNAN, Lloyd F. (*A* 1945) Owner, • Ace Sheet Metal Works, 444 Clementina St., San Francisco 3, and 1343–32nd Ave., San Francisco 22, Calif.
HANNIGAN, William (*M* 1940) Bldg., Supt., • Acacia Mutual Life Insurance Co., 51 Louisiana Ave. N.W., Washington, D. C., and Rt. 2, Silver Spring, Md.
HANSEN, Clarence E. (*M* 1946) Secy., • The Smith & Oby Co., 6107 Carnegie Ave., Cleveland 3, and 3336 Ormond Rd., Cleveland Heights 18, Ohio.
HANSEN, John S. (*A* 1945) Testing Engr., • Sears Roebuck & Co., Dept. 817, 925 S. Homan Ave., Chicago 7, and 115 South Blvd., Oak Park, Ill.
HANSEN, Willis A. (*M* 1943) Designer, Clyde E. Bentley, Constr. Engr., 405 Sansome St., San Francisco, and • 1440 California St., Berkeley 3, Calif.
HANSON, Frank E. (*M* 1946) Gas Engr., • American Radiator & Standard Sanitary Corp., 675 Bronx River Rd., Yonkers 4, and 427 E. Third St., Mount Vernon, N. Y.
HANSON, Kenneth H. (*A* 1946) Sales Engr., Minneapolis-Honeywell Regulator Co., 122 N.E. Broadway, and • 6317 Southeast 40th, Portland, Ore.
HANSON, Lars C. (*M* 1945) Dir. of Reciprocating Refrigeration Dvlp., Carrier Corp., 300 S. Geddes St., Syracuse 1, and • 282 Robineau Rd., Syracuse 4, N. Y.
HANSON, Leon C. (*A* 1939) Secy.-Mgr., Bjorkman Bros. Co., 712 Tenth St. S., Minneapolis, Minn.
HANSON, Leslie P. (*M* 1937; *A* 1936; *J* 1935; *S* 1933) Sales Mgr., Air Cond. Equip. Div., U. S. Air Conditioning Corp., 2101 Kennedy N.E., and • 5027 Nokomis Ave. S., Minneapolis, Minn.
HANSON, Roy W. (*A* 1946) Dist. Mgr., Bastian-Morley Co., Inc., LaPorte, Ind., and • 6443 Vickery Blvd., Dallas, Texas.
HANTHORN, Walter (*M* 1947; *A* 1942; *J* 1939) Engr., Kleenair Furnace Co., 5329 N.E. Sandy Blvd., and • 2946 Northeast 54th Ave., Portland 13, Ore.
HAPPERFIELD, G. J. (*M* 1943) Managing Dir., • Chandos Engineering Co., Ltd., 17 High St., Egham, Surrey, and 468 Staines Rd., Twickenham, Middlesex, England.
HARBERGER, G. L. (*A* 1939) Mgr., Boiler and Htg. Dept., Eastern Foundry Co., Boyertown, and • 641 King St., Pottstown, Pa.
HARBIN, Frank, Jr. (*M* 1941) Supt., • Home Furnace Co., 280 E. Sixth St., and 181 West 21st St., Holland, Mich.

HARBORDT, Otto E. (*A* 1936) Treas., ● U. S. Supply Co., 1315 West 12th St., and 4600 Mill Creek Pkwy., Kansas City, Mo.
HARDEN, J. Clinton (*M* 1938) 106 Michigan Ave., Dowagiac, Mich.
HARDER, Ervin P. (*A* 1944) Prod. Appl. Engr., Herman Nelson Corp., 4060 W. Pine, St. Louis, and ● 1235 A. Claytonia Terrace, Richmond Heights 17, Mo.
HARDIN, James T. (*M* 1943) Mgr., Heating Dept., Roland M. Cotton Co., Inc., 1720 E. Tenth St., and ● 3720 N. Pennsylvania St., Apt. 15, Indianapolis, Ind.
HARDING, Edward R. (*M* 1936) State Mgr., ● Kewanee Boiler Corp., P. O. Box 536, 431 Jefferson Std. Bldg., Greensboro, and Four Acres, Route 1, Guilford College, N. C.
HARDING, Louis A.* (*Life Member*; *M* 1911), (*Presidential Member*), (Pres., 1930; 1st Vice-Pres., 1929; 2nd Vice-Pres., 1928), (Council, 1922-31) Cons. Engr., 85 Cleveland Ave., Buffalo 9, N. Y.
HARDING, Walter (*M* 1941) Dir., Norris Warming Co., Ltd., Burley House, Theobalds Rd., London, and ● Danesfield House, 33 Bute Gardens, Wallington, Surrey, England.
HARE, Arthur L. (*A* 1946) Branch Mgr., ● Kewanee Boiler Corp., 127 Federal St., Boston 10, and 34 Highland Ave., Newtonville 60, Mass.
HARE, W. Almon (*M* 1941) Pres., Hare Engineering Co., 825 Hammond Bldg., Detroit 26, Mich., and ● 833 Kildare Rd., Windsor, Ont., Canada.
HARGIS, Alexander H. (*J* 1947) Engrg. Draftsman, ● T. F. Hargis, Jr., 432 Miller Bldg., Yakima, and Route 1, Zillah, Wash.
HARMAN, Ralph H. (*A* 1945) Owner, ● Ralph H. Harman, Archt., 133 W. High St., and 330 Broadmoor Blvd. N., Springfield, Ohio.
HARMONAY, W. L. (*M* 1944; *A* 1935) Pres., ● Michael Harmonay Corp., 567 Yonkers Ave., Yonkers 4, and 1360 Midland Ave., Bronxville, N. Y.
HARPER, Donald R. (*A* 1947) Sales Engr., ● The D. R. Harper Co., 1409 Schofield Bldg., Cleveland 15, and 25205 Chatworth Dr., Euclid, Ohio.
HARPER, Everett C. (*M* 1946) Appl. Engr., York Corp., 412 Houston St. N.E., and ● 2029 Tuxedo Ave. N.E., Atlanta, Ga.
HARRIGAN, Edward M. (*Life Member* 1947; *M* 1915) Pres. and Gen. Mgr., ● Harrigan & Reid Co., 1305 Bagley Ave., and 7450 LaSalle Blvd., Detroit, Mich.
HARRIGAN, Edward R. (*M* 1939) Lt., U. S. Navy, Navy Yard, New York, N. Y., and ● 19 Erwin Pl., Caldwell, N. J.
HARRIGAN, John E. (*A* 1945) Mech. Inspector, The Austin Co., 19 Rector St., New York 6, and ● 1 Chestnut St., Schenectady 7, N. Y.
HARRIGAN, Paul D. (*M* 1947) Cons. Engr., ● Harrigan-Hill, 37 Whitney Ave., New Haven, and 66 Charles St., Milford, Conn.
HARRINGTON, David W.* (*A* 1943) ● Texas Distributors, Inc., 3914 Live Oak Street, Dallas 4, and 1549 El Campo, Dallas, Texas.
HARRINGTON, Elliott D.* (*M* 1932; *A* 1930) Mgr., Induction Motor Div., ● General Electric Co., 1 River Rd., Schenectady 5, and The Hawthorne, R. D. 2, Altamont, N. Y.
HARRINGTON, Jeremiah P. (*A* 1944) Mech. Engr., Ralph E. Phillips, Cons. Engr., Architects Bldg., Los Angeles, and ● 1614 Greenwood Ave., San Gabriel, Calif.
HARRINGTON, Larry J. (*M* 1941) Owner, Larry Harrington Co., 1971 N.W. Lovejoy St., Portland 9, Ore.
HARRIS, Albert M. (*M* 1947) Pres. & Gen. Mgr., ● Harris & Beeman, Inc., 1933 E. Lancaster St., and 1400 N. Riverside Dr., Fort Worth, Texas.
HARRIS, Harold R. (*M* 1946) Owner, Sales Engr., H. R. Harris Co., 708 Sixth Ave. S., Minneapolis 15, and 1683 Summit Ave., St. Paul 5, Minn.
HARRIS, Herbert J. (*A* 1945) Pres., ● Marion Oil & Service Corp., and ● 7 Croydon Rd., Yonkers 2, N. Y.
HARRIS, H. Melvin (*M* 1946) Engr. and Factory Repr., ● Warren Webster & Co., & Kewanee Boiler Corp., 2301 N. Charles St., and 1509 Sheffield Rd., Baltimore 18, Md.
HARRIS, Robert C. (*A* 1946) Sales Engr., ● Minneapolis-Honeywell Regulator Co., 420 N. Fifth Ave., Minneapolis, Minn.
HARRIS, Wallace L. (*J* 1947) Sales Engr., Harris Brothers Plbg. Co., 217 W. Lake St., Minneapolis 8, and ● 6215 West 36th St., St. Louis Park, Minn.
HARRIS, Warren S.* (*M* 1942) Special Research Assoc. Prof., ● University of Illinois, 801 W. Green St., and 802 N. Broadway, Urbana, Ill.
HARRISON, Howard W. (*A* 1946) Htg. Sales Engr., ● Georgia Power Co., P. O. Box 1719, Atlanta 1, and 143 Mobile Ave. N.E., Atlanta 5, Ga.
HARRISON, Maurice E. (*A* 1946) Sales Mgr. and Engr., Htg. and Vtg. Dept., Northern California Hardware Co., 209 Mississippi St., San Francisco, and ● 1216 Fruitvale Ave., Oakland, Calif.
HARRISON, Paul N. (*A* 1945) Owner, ● Paul N. Harrison Co., 50 Hawthorne, San Francisco, and 2301 Ivy Dr., Oakland, Calif.
HARRISON, William Z. (*A* 1944) Owner, ● Harrison & Co., 210 S.W. Temple St., Salt Lake City 1, and 1127 E.S. Temple St., Salt Lake City 2, Utah.
HARROWER, William C. (*A* 1947) Htg. Engr., Timken Silent Automatic, 209 E. Washington Ave., and ● 1028 Greenwood Ave., Jackson, Mich.
HARRYMAN, Merl M. (*A* 1947) Office Engr., Becklean Co., 1316 Oak St., Kansas City 6, and ● 321 Cypress, Kansas City 1, Mo.
HART, Harry M.* (*Life Member*; *M* 1912), (*Presidential Member*), (Pres., 1916; 1st Vice-Pres., 1915), (Council, 1914-17), Pres., ● L. H. Prentice Co., 1048 Van Buren St., Chicago 7, and 3730 Lakeshore Dr., Chicago, Ill.
HART, James E. (*M* 1947) Partner, ● Watson & Hart, 1001 E. Bessemer Ave., Greensboro, and Cone Lake, Guilford Co., N. C.
HART, John H. (*M* 1942) Mech. Engr. (Sr.), Federal Housing Administration, Vermont and K St., Washington, D. C., and ● 1506 Mt. Eagle Pl., Alexandria, Va.
HART, Stanley (*M* 1938) Pres., ● Tuttle & Bailey, Inc., and 60 Chatham Rd., New Britain, Conn.
HART, Theodore S. (*M* 1938) Pres., Brenton & Hart Co., 138 Brighton Ave., Allston, Mass.
HARTIN, William Rhett, Jr. (*A* 1944; *J* 1935) Vice-Pres. and Secy., W. R. Hartin & Sons, Inc., 2123 Green St., Columbia 41, and ● 2744 Trenholm Rd., Columbia 32, S. C.
HARTMAN, John M. (*M* 1927) Engr., ● Kewanee Boiler Corp., and 618 Elliott St., Kewanee, Ill.
HARTMAN, P. C., Jr. (*A* 1946) Pres., ● P. C. Hartman Co., 833 West 21st St., and 200 North Shore Rd., Norfolk, Va.
HARTMANN, Charles W., Jr. (*A* 1944) Sales Engr., A. F. Hinrichsen, Inc., 50 Church St., New York, and ● 551-72nd St., Brooklyn 9, N. Y.
HARTMANN, Henry (*M* 1947) Engr., Comml. Gas Utilization, ● Brooklyn Union Gas Co., 176 Remsen St., Brooklyn, and 36 Rockville Dr., Baldwin, L. I., N. Y.
HARTNETT, Daniel E. (*A* 1947) Htg. Engr., ● Wigman Co., 313-319 Perry St., and 4623 Military Rd., Sioux City, Iowa.
HARTON, A. J. (*A* 1935) Co-Owner, ● The Service Co., 416 Edmond St., and 730 E. Hyde Park Ave., St. Joseph, Mo.
HARTSFIELD, Charles G. (*M* 1944) Vice-Pres. and Gen. Mgr., ● Atlantic Engineering Co., Box 2262, and 2702 W. Market St., Greensboro, N. C.
HARTSOOK, Granville S., Jr. (*A* 1939) Pres., ● Hartsook Supply Co., Inc., 21 S. Royal Ave., and Browntown Rd., Front Royal, Va.
HARTWEIN, C. E. (*M* 1933) Supt. Htg. and Service Div., Laclede Gas Light Co., 231 W. Lockwood Ave., Webster Groves 19, and ● 135 Peeke Ave., Kirkwood 22, Mo.
HARTWELL, Joseph C. (*Life Member*; *M* 1922) Pres., ● Hartwell Co., Inc., 87 Weybosset St., and 16 Freeman Pkwy., Providence, R. I.
HARTWIG, Walter J. (*A* 1945) Planning Specialist, War Dept. Corps of Engrs., Los Angeles Dist., 751 Figeroa St., Los Angeles, and ● 3643 Clarington Ave., Los Angeles 34, Calif.
HARVEY, A. D. (*A* 1928); *J* 1925) Vice-Pres., ● The Dorr Co., Inc., 570 Lexington Ave., New York 22, and 1175 Park Ave., New York 28, N. Y.
HARVEY, Ernest W. (*A* 1943) Appl. Engr., ● Westinghouse Electric Corp., 1014 Fairfax Bldg., and 210 East 72nd St., Kansas City, Mo.
HARVEY, John W. (*M* 1942) Managing Dir., Sterigas Construction Co., Ltd., 2 Gorst Rd., London, N.W. 10, and ● 64 Crowshott Ave., Stanmore, Middlesex, England.

HARVEY, Lyle C. (*M* 1928) Pres., • The Bryant Heater Co., 17825 St. Clair, Cleveland 10, and 2666 Leighton Rd., Cleveland, Ohio.

HASHAGEN, John B. (*M* 1930) Production Mgr., Fearn Laboratories, 9401 W. Belmont Ave., Franklin Park, and • 4236 N. Mozart St., Chicago, Ill.

HASTINGS, Addison (*M* 1942) Asst. Secy., Sales Engr., Burnham Boiler Corp., and • Lewis Rd., Irvington, N. Y.

HATCH, George (*A* 1941) Pres., • Air Conditioning Engineering Co., Ltd., 1104 Bay St., Toronto, Ont., Canada, and 3527 Carnation Ave., Los Angeles 26, Calif.

HATCH, O. J. (*A* 1941) Mgr., Clare Bros. Western, Ltd., 179 Notre Dame Ave. E., and • 640 Jubilee Ave., Winnipeg, Man., Canada.

HATTERSLEY, Eugene H. (*M* 1943) Member of Firm, • A. Hattersley & Sons, 212 E. Main St., and Apt. 30 Windsor Apts., 521 W. Berry St., Fort Wayne 2, Ind.

HATTIS, Bernard S. (*J* 1948) Partner, Robert E. Hattis, Cons. Engr., • 223 W. Jackson Blvd., Chicago 4, and 7020 S. Jeffery Blvd., Chicago 49, Ill.

HATTIS, Robert E. (*M* 1926) Cons. Engr., • 223 W. Jackson Blvd., Chicago 4, and 1454 Fargo Ave., Chicago 26, Ill.

HATZENBUEHLER, Edwin J. (*M* 1947) Mgr., Indus. & Comml. Gas Dept., • Lone Star Gas Co., 1915 Wood St., and 7434 Coronado, Dallas, Texas.

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HAUER, B. T. (*A* 1946) Owner, • Hauer Power Equipment Co., 831 Temple Bar Bldg., Cincinnati 2, and 3619 Brentwood Ave., Cincinnati 8, Ohio.

HAUER, Fred W. (*A* 1938) Owner, • Fred Hauer & Co., 315 Elmhurst Ave., Peoria 4, Ill.

HAUF, Joseph C., Jr. (*M* 1944) Mgr., Gen. Div., York-Shipley, Inc., York, Pa., and • 4204 Tuscany Ct., Baltimore 10, Md.

HAUS, Irvin J. (*A* 1937; *J* 1935) Plant Engr., • Nash Kelvinator Corp., Seaman Body Plant, 3880 N. Richards St., Milwaukee 1, and 2211 North 51st St., Milwaukee 8, Wis.

HAUSLER, Walter (*M* 1947) Owner & Mgr., Institute of Heat Economy Ceresstrasse 27, and • Zollikerstrasse 238, Zurich, Switzerland.

HAUSMAN, L. M. (*M* 1945) Pres., L. M. Hausman & Co., 912 Taft Ave., Manila, P. I.

HAUSSER, Fred L. (*A* 1945) Partner, Ward & Hausser, 17 Seyms St., Hartford 5, and • 178 Four Mile Rd., West Hartford 7, Conn.

HAWES, Harold D. (*J* 1942; *S* 1940) Lt. U. S. Army, and • 454 Tollsome Hill Rd., Bridgeport, Conn.

HAWISHER, Harold H. (*A* 1938) Mech. Engr., • Automatic Heating & Engineering Co., 416-418 N. Main St., and 411 S. Jameson Ave., Lima, Ohio.

HAWK, Charles A., Jr. (*A* 1944) Consultant, 1104 Farragut St., Pittsburgh 6, Pa.

HAYES, Charles R., Jr. (*J* 1947) Draftsman, A. C. Engineering & Drafting, 519 Apco Tower, and • 1608 Northwest 28th St., Oklahoma City, Okla.

HAYES, Grant J. (*A* 1946) Engr., • Hayes Brothers, Inc., 236 W. Vermont St., Indianapolis 4, and 2849 N. Capitol Ave., Indianapolis 8, Ind.

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HAYES, Joseph G. (*Life Member*; *M* 1908) Pres. and Engr., Hayes Brothers, Inc., 236 W. Vermont St., Indianapolis 4, Ind.

HAYES, William C. (*J* 1946) Secy.-Treas., • Hayes Distributing Co., P. O. Box 202, Portsmouth, and 305 Norman Rd., Green Acres, Portsmouth, Va.

HAYES, William G. (*A* 1946) Pres., • The Hayes Distributing Co., P. O. Box 202, Portsmouth, and 305 Norman Rd., Green Acres, Portsmouth, Va.

HAYMAN, A. Eugene, Jr. (*A* 1941; *J* 1935; *S* 1930) Sun Oil Co., Marcus Hook, Pa., and • 2715 Washington St., Wilmington 239, Del.

HAYNES, C. V. (*Life Member*; *M* 1917), (*Presidential Member*), (Pres., 1934; 1st Vice-Pres., 1933; 2nd Vice-Pres., 1932), (Council, 1926-29; 1932-35) Specialist, The American Co., and • P. O. Box E., Woodford Sta., Portland 5, Me.

HAYS, Herbert G. (*M* 1945) Chief Engr., • Armstrong Furnace Co., 851 W. Third Ave., Columbus 8, and 868 Kenwick Rd., Columbus, Ohio.

HEAD, Frederick T. (*A* 1946) Sales Repr., Surface Combustion Corp., Janitrol Div., 225 Broadway, New York, and • 305 Sixth Ave., Pelham 65, N. Y.

HEAGERTY, William H. (*A* 1940) Sales Engr., • Chandler Bldg., and 5100 N. Capitol St., Washington, D. C.

HEALY, Dennis L., Jr. (*A* 1946) Secy., • Healy-Ruff Co., 2255 University Ave., and 2124 Grand Ave., St. Paul 4, Minn.

HEAPHY, J. Arthur (*A* 1945) Pres. and Owner, • D. J. Heaphy & Son, 133 N. Geddes St., Syracuse 4, and 101 Wellesley Rd., Syracuse, N. Y.

HEARD, John A. E. (*A* 1946) Sales Engr., • Carrier Engineering Co., Ltd., 24 Buckingham Gate, London S.W. 1, and Cleddav, The Chase Rayleigh, Essex, England.

HEARNE, Rufus D. (*A* 1946) Northern Dist. Sales Mgr., • L. J. Mueller Furnace Co., 2005 W. Oklahoma, and 2495 N. Oakland Ave., Milwaukee, Wis.

HEATH, George A. (*A* 1944) • P. O. Box 207, 40 W. Main St., and 24 W. Marble St., Mechanicsburg, Pa.

HEATH, William R. (*M* 1931) Asst. Chief Engr., • Buffalo Forge Co., 490 Broadway, and 119 Wingate Ave., Buffalo, N. Y.

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HEAVEN, Lewis P. (*M* 1943) Owner, • Heaven Engineering Co., 1527 Wyandotte, Kansas City 8, and 642 East 46th St., Kansas City 4, Mo.

HEBLEY, Henry F. (*M* 1934) Dir. of Research, • Pittsburgh Consolidation Coal Co., 2045 Koppers Bldg., Pittsburgh, and 216 Jefferson Dr., Mt. Lebanon, Pittsburgh 16, Pa.

HECKEL, Edmund P. (*M* 1918) E. P. Heckel & Assoc., Cons. Engrs., 100 W. Monroe St., Chicago 3, and • 314 Cuttriss Pl., Park Ridge, Ill.

HECKEL, Edmund P., Jr. (*A* 1948; *J* 1941) Sales Engr., Emmert & Trumbo Mfrs. Repr., 20 N. Wacker Dr., Chicago 6, and • 123 Belle Plaine Ave., Park Ridge, Ill.

HECKERT, W. P. (*A* 1947) Owner, • Heckert Sheet Metal Works, 311 East 31st, and 717 West 36th St., Kansas City, Mo.

HECKLER, Frank W. (*A* 1946) Member of Firm, • Heckler Bros., 965 Liberty Ave., Pittsburgh 22, and 43 Rhodes Ave., Pittsburgh 20, Pa.

HEDEEN, L. E. (*M* 1942; *A* 1941; *J* 1938) Cons. Engr., Todd, Hedeen & Assocs., 180 W. First St., and 601 Moir, Waterloo, Iowa.

HEDGES, H. Berkley (*M* 1919) Mgr., Blast Coil Surface Sales, • John J. Nesbitt, Inc., State Rd. and Rhawn St., Holmesburg, Philadelphia 36, and 114 Waverly Rd., Wyncote, Pa.

HEDLEY, Park S. (*M* 1923) Partner, • Park S. Hedley Co., 452 Franklin St., Buffalo 2, and 31 Westgate Rd., Kenmore, N. Y.

HEDLUND, Richard A. (*A* 1946) Asst. Staff Engr., Johns Manville Co., Manville, and • 928 Grant Ave., Plainfield, N. J.

HEEBNER, Walter M. (*M* 1922) Sales Engr., Warren Webster & Co., 1060 Broad St., Newark, and • 282 Highwood St., Teaneck, N. J.

HEGELE, Richard H. (*A* 1945) Owner and Mgr., H. W. Hegele Co., 231 N. Main St., and • 338 E. Court, Urbana, Ohio.

HEIBEL, Walter E. (*M* 1917) Dist. Mgr., • Aerofin Corp., 11 West 42nd St., New York 18, N. Y., and 12 Richmond Dr., Old Greenwich, Conn.

HEIDENREICH, George (*M* 1947) Sales Engr., • G. Heidenreich Co., Inc., 320 Chamber of Commerce Bldg., Indianapolis 4, and 5768 N. Delaware St., Indianapolis, Ind.

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HELLER, Joseph A. (*A* 1938) 150 West 79th St., New York 24, N. Y.

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HELSTROM, Herman G. (*M* 1936) Northwest Sales Mgr., William Brothers Boiler & Manufacturing Co., 1057 Tenth Ave. S.E., and • 4608 Arden Ave. S., Minneapolis 10, Minn.

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HENDRIKSEN, Leonard (*A* 1938) Owner, Hendriksen Sheet Metal & Heating Service, 1919 N. Vernon Ave., Flint 6, Mich.

HENDRIX, William T. (*A* 1948) Member of firm, Mech. Equip. Designer, • Wolf & Hahn, 459 Hamilton St., and 131 N. Franklin St., Allentown, Pa.

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HENRY, Ernest C. (*M* 1938) Engr., McCoy Heating Co., 303 S. Water St., and • 1115 Park Ave., Bay City, Mich.

HENRY, Ray W. (*A* 1945) W. B. Young Supply Co., 208 Delaware St., Kansas City 6, Mo. and • 2652 Minnesota Ave., Kansas City 2, Kans.

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HENTON, L. W. J. (*M* 1947) Gaumont British Picture Corp., Ltd., Holborn Empire Offices, Holborn, London W. I., and • 3 Chesterfield Rd., West Ewell, Surrey, England.

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HERMAN, Kenneth R. (*J* 1947) Purchasing Agent, • Armor Insulating Co., 800 Forrest St. N.W., Atlanta, and 441 Mimosa Dr., Decatur, Ga.

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HERMAN, Neil B. (*A* 1943; *J* 1937; *S* 1936) Engr., • Allied Store Equipment Co., 116 N. Seventh St., Minneapolis 3, and 4217 Garfield Ave. S., Minneapolis 9, Minn.

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HEWETT, Robert E. (*J* 1946) Draftsman, R. P. Allsop, Cons. Engr., 1221 Bay St., and • 7 Mountjoy Ave., Toronto, Ont., Canada.

HEYMSFIELD, Herbert R. (*M* 1941) Automatic Htg. Instructor, Brooklyn Technical High School, Brooklyn, and • 80-74 Kent St., Jamaica Estates, L. I., N. Y.

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HICKEY, Daniel W. (*A* 1931) Pres., D. W. Hickey & Co., Inc., 1841 University Ave., St. Paul 4, Minn.

HICKMAN, Charles W. (*J* 1946) Engr., Therma Zone Co., 178 Grand Ave., Oakland 12, and • 11 Palm Ave., San Rafael, Calif.

HICKMAN, Herbert V. (*M* 1945; *A* 1938) Htg. Engr. and Gen. Mgr., • Neil H. Peterson Co., 1129 Folsom St., San Francisco 1, and 11 Palm Ave., San Rafael, Calif.

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HICKS, Beatrice A. (*A* 1947) Vice-Pres., • Newark Boiler Regulator Co., 15 Ward St., and 99 Morse Ave., Bloomfield, N. J.

HIERONYMUS, R. E. (*M* 1947) Partner, • Aldis & Co., 53 W. Jackson Blvd., Chicago 4, and 3845 Woodland Ave., Western Springs, Ill.

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HIGH, John M. (*M* 1940; *A* 1938) Mgr., Insulation Div., The Ruberoid Co., 500 Fifth Ave., New York, N. Y.

HIGHTOWER, George B. (*M* 1946) Partner & Pres., Conditioned Air Engineers, Inc., 169 Marietta St. N.W., and • 3630 Peachtree Rd., Atlanta, Ga.

HILDER, Frederick L. (*M* 1937) Chief Engr., Electric Furnace-Man, Inc., Fourth and Furnace Sts., Emmaus, and • 2604 Walnut St., Allentown, Pa.

HILL, Edward, Jr. (*M* 1947; *A* 1942; *J* 1939) Cons. Mech. Engr., Franklin, Kump and Falk, 9 Main St., San Francisco, and • 3355 Octavia St., San Francisco 23, Calif.

HILL, E. Vernon, M. D.* (*Life Member*; *M* 1914; *A* 1912), (*Presidential Member*), (Pres., 1920; 1st Vice-Pres., 1919; 2nd Vice-Pres., 1918), (Council, 1915-21) Pres., E. Vernon Hill and • 6826 W. Highland Ave., Chicago 31, Ill.

HILL, Fred M. (*M* 1944) Estimator, Htg., Vtg. and Air Cond., and • 225 East Ave. 39, Los Angeles 31, Calif.

HILL, Harold H. (*M* 1935) S. E. Div. Mgr., • American Blower Corp., 438 Woodward Bldg., Washington 5, and 3002 Rodman St. N.W., Washington 8, D. C.

HILL, H. Gordon (*M* 1943; *J* 1938) Chief Engr., • Chatco Steel Products, Ltd., and 2 Mary St., Chatham, Ont., Canada.

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HILL, N. Edward (*M* 1944) Chief Designer, L. J. Mueller Furnace Co., 2005 W. Oklahoma Ave., Milwaukee 7, and • 122 N. Hartwell Ave., Waukesha, Wis.

HILL, Vaughn H. (*M* 1943; *J* 1938) Motor Wheel Corp., Lansing, and • 2111 Colvin Ct., Lansing 10, Mich.

HILLARD, Henry F. (*M* 1945) Chief Engr., Distribution Div., • Mountain Fuel Supply Co., 36 S. State St., and 125 South 13th East St., Salt Lake City, Utah.

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HINNANT, C. H., Jr. (*M* 1943; *J* 1938) Chief Engr., • Universal Leaf Tobacco Co., Richmond Trust Bldg., Richmond 14, and 1023 West 45th St., Richmond 24, Va.

HINNANT, Robert H. (*J* 1945) Assoc., • C. H. Hinnant, Archt. & Mech. Engr., 403 Lynch Bldg., and 341 Woodland Ave., Lynchburg, Va.

HINRICHSEN, Arthur F. (*M* 1928) Pres., • A. F. Hinrichsen, Inc., 50 Church St., Room 1970, New York 7, N. Y., and 281 Morris Ave., Mountain Lakes, N. J.

HIRATSUKA, Shigeki (*A* 1946) Syska & Hennessy, 144 East 39th St., and • 50 West 69th St., New York 23, N. Y.

HOAGLAND, Everett J. (*A* 1947) Sales Engr., • Johnson Service Co., 20 Winchester St., Boston, and 64 Fenno St., Wollaston, Mass.

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HOECKER, George F., Jr. (*A* 1941) Mgr., Sears, Roebuck & Co., 275 Hobart St., Perth Amboy, and • 475 W. Inman Ave., Rahway, N. J.

HOERTEL, Harold E. (*A* 1946) Mech. Engr., The Frank A. McBride Co., 70 East 45th St., New York, N. Y., and • 27 Laurel Ave., Dumont, N. J.

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HOLBROOK, Frank M. (*M* 1944) • Alpha Steam Specialty Co., 15 Park Row, New York 7, N. Y., and 625 Union County Pkwy., Union, N. J.

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HOLDEN, Robert G. (*A* 1942) Construction Engr., • National Tube Co., and 4387 E. Lake Rd., Lorain, Ohio.

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HOLE, Kenneth W. (*A* 1943) Exec. Sales Engr., Miles Aircraft, Ltd., The Aerodrome, Reading, Berkshire, England.

HOLE, William G. (*M* 1942) Mgr., Air Filter Div., • Darling Bros., Ltd., 140 Prince St., Montreal, and 1765 Graham Blvd., Mt. Royal, Que., Canada.

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HOLLAND, William T. (*M* 1943; *A* 1941) Engr., • c/o Thos. E. Hoye Heating Co., 1906 W. St. Paul Ave., Milwaukee 3, and 2338 North 71st St., Wauwatosa 13, Wis.

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HOULIS, Louis D. (*M* 1935) Master Baker Ovens, 558 Pedretti Ave., Cincinnati 5, Ohio.

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JACKSON, Joseph S. (*M* 1947; *A* 1946) Indus. Engr., ● United Engineers & Constructors, Inc., 1401 Arch St., Philadelphia, and 355 Winola Ave., Kingston, Pa.

JACKSON, Marshall S. (*M* 1919) Mfrs. Repr., ● Powers Regulator Co., 250 Delaware Ave., Buffalo 2, and 108 Larchmont Rd., Buffalo 14, N. Y.

JACKSON, Melvin W. (*A* 1945) Pres., ● Dallas Engineering Co., 2000 S. Akard, Dallas 1, and 4637 Southern, Dallas 9, Texas.

JACKSON, Robert B. (*M* 1944) Co-Partner, ● Lieb-Jackson Co., 337 S. High St., Columbus 15, and 2342 Tremont Rd., Columbus 8, Ohio.

JACKSON, Robert E. (*S* 1948) Student, A. & M. College of Texas, College Station, and ● 213 Bolivar St., Denton, Texas.

JACKSON, Robert O. (*A* 1946) Sales Engr., ● Jackson Engineering Co., 936 Architects and Builders Bldg., Indianapolis 4, and 1837 N. Talbot, Indianapolis, Ind.

JACKSON, Walter F. (*A* 1943; *J* 1939) Chief Engr., ● American Stove Co., 1200 Long Ave., Lorain, and 116 Bell Ave., Elyria, Ohio.

JACOBI, Bruce A. (*A* 1945; *J* 1939) Chief Engr., Lerner Stores, Corp., 354 Fourth Ave., New York, and ●44 Gramercy Park, New York 10, N. Y.

JACOBS, Robert H. (*A* 1947) Sales Engr., ● Minneapolis-Honeywell Regulator Co., 2405 N. Maryland Ave., and 4448 N. Ardmore Ave., Milwaukee 11, Wis.

JACOBSON, A. D. (*A* 1946) Owner, ● A. D. Jacobson Plumbing & Heating Co., 2030 Central St., Kansas City 8, and 1008 West 70th Terrace, Kansas City, Mo.

JACOBSON, Elliot L. (*J* 1947) Vice-Pres., ● A. D. Jacobson Plumbing and Heating Co., Inc., 2030 Central, Kansas City 8, and 4801 Roanoke Pkwy., Kansas City, Mo.

JACOBUS, David S. (*Life Member*; *M* 1916) Retired, and ●93 Harrison Ave., Montclair, N. J.

JAFFKE, Walter W. (*A* 1945) Asst. Buyer, ● Nelson Co., 2604 Fourth Ave., Detroit 1, and 13342 Coyle Ave., Detroit 27, Mich.

JAHN, Rudolph, Jr. (*S* 1947) Student, ● Texas A. & M. College, Box 4398, College Station, and 314 Irvine St., Yoakum, Texas.

JAHN, William Edward (*J* 1946) Instructor, ● University of Minnesota, 165 Mech. Engrg. Bldg., Minneapolis 14, and 33 Inner Dr., St. Paul 5, Minn.

JAKOBY, Albert C. (*A* 1938) 1913 E. Clearfield St., Philadelphia, Pa.

JALLES, Armando R. (*J* 1948) Design and Sales Engr., Carrier Lix Klett, S. A., ● Florida 229, 10°, and Cabildo 808, Buenos Aires, Argentine Republic, S. A.

JALONACK, Irwin G. (*M* 1940; *A* 1933; *S* 1930) Chief Mech. Engr., Levitt & Sons, Northern Blvd., Manhasset, and ●12 E. Court, Roslyn Heights, L. I., N. Y.

JAMES, Hamilton R. (*M* 1931) Service Equip. Engr., Day & Zimmermann, Inc., Packard Bldg., Philadelphia, and ● 55 W. Drexel Ave., Lansdowne, Pa.

JAMES, Jack K. (*J* 1948; *S* 1946) Sales Engr., Boyd Engineering Co., 112 W. Granite Ave., and ●1301 N. Fifth St., Albuquerque, N. M.

JAMES, John W.* (*M* 1937; *J* 1933) ● Iron Fireman Manufacturing Co., 3170 West 106th St., Cleveland 11, and 15918 Clifton Blvd., Lakewood 7, Ohio.

JAMES, R. E. (*M* 1945) Mgr., Htg. Dept., Harry Cooper Supply Co., 223 Water St., and ●811 E. Elm St., Springfield, Mo.

JAMES, Rex P. (*A* 1948) Sales Engr., ● York Corp., 307 Frost Natl. Bank Bldg., San Antonio 5, and 1612 El Monte, San Antonio 1, Texas.

JAMES, Richard G. (*S* 1948) Student, Purdue University, ● FPHA 545-1 Airport Rd., West Lafayette, and 411 East 37th St., Indianapolis, Ind.

JAMES, William B. (*M* 1947) Br. Mgr., Htg. & Air Treatment Div., The Brightside Foundry & Engineering Co., Ltd., 17 Summer Row, Birmingham 3, and ● 47 Edward Rd., Quinton, Birmingham 32, England.

JAMIESON, John R., Jr. (*S* 1948) Student, University of Minnesota, and ●827 S.E. Sixth St., Minneapolis, Minn.

JAMISON, Ernest K. (*A* 1944) Contract Engr., The Huffman-Wolfe Co., 308 Standard Bldg., and ●3369 Walters Ct. N.E., Atlanta, Ga.

JANDER, Yorke (*A* 1947) Pres., ● Admiral Air Conditioning Corp., 222 N. Fifth Ave., Mt. Vernon, and 1 Devon Way, Hastings-on-Hudson, N. Y.

JANES, Thomas J. (*M* 1945) Engr., ● University of California, Berkeley 4, and 1733 Madera St., Berkeley 7, Calif.

JANET, Harry L. (*M* 1920) Engr., Buensod-Stacey, 60 East 42nd St., New York, and ● 688 Decatur St., Brooklyn, N. Y.

JANITZ, Robert H. (*M* 1944) Co-Partner, Fred G. & Robert H. Janitz, 619 Virginia Ave., Indianapolis 3, and ● 23 N. Colorado Ave., Indianapolis 1, Ind.

JANOS, William A. (*M* 1940) Sr. Mech. Engr., Manufacturer of Communications Equip., ● Western Electric Co., Inc., 195 Broadway, New York 7, and 21-11-23rd Terrace, Astoria 5, N. Y.

JANSSEN, Fred (*M* 1945) Appliance Controls Engr., ● Public Service Company of Colorado, 1123 W. Third Ave., Denver 9, and 2946 S. Sherman St., Englewood, Colo.

JANSSEN, Henry J. (*M* 1944) Treas., ● Child & Scott Co., Inc., 153 East 38th St., New York, N. Y., and 410 Palisade Ave., Union City, N. J.

JARCHO, Martin D. (*A* 1939; *J* 1936) Vice-Pres., ● Jarcho Bros., Inc., 304 East 45th St., New York, and 110-55-72nd Rd., Forest Hills, N. Y.

JARDINE, Douglas C. (*M* 1929; *A* 1926) Owner, ● Douglas Jardine, P. O. Box 126, and 1216 N. Cascade Ave., Colorado Springs, Colo.

JARRETT, Roland F. (*M* 1945) Dir., Flexaire Heaters, Ltd., 108 Victoria St., London S. W. 1, and ● "Glovers," Woodlands, Sevenoaks, Kent, England.

JARVIS, George E. (*M* 1943) Vice-Pres. and Secy., ● A. E. Holmes & Brothers Co., 911-15 Banks Ave., and 2628 Hughitt Ave., Superior, Wis.

JASPER, Harold C. (*A* 1944) Pres., Andy J. Egan Co., Inc., 332 Bond Ave. N.W., Grand Rapids 2, and ●1529 Fourth St. N.W., Grand Rapids 4, Mich.

JEFFERSON, Cecil H. (*A* 1946) Engr., ● Vermiculite Institute, 2540 Eastwood Ave., Evanston, and 601 Meadow Dr., Glenview, Ill.

JEHLE, Ferdinand (*M* 1938; *A* 1937) Dir. of Engrg., ● Hoffman Specialty Co., 1001 York St., Indianapolis 7, and 3055 N. Meridian St., Apt. 9, Indianapolis 8, Ind.

JENA, Frederick T. (*A* 1946) Partner, ● Advance Heating Co., 910 Herrick Ave., and 832 Blaine Blvd., Racine, Wis.

JENKINS, Chester P. (*M* 1945) Chief Adm. Engr., ● LaDel Conveyor & Manufacturing Co., and 120 North Ave. N.W., New Philadelphia, Ohio.

JENKINS, Francis H. (*A* 1946) Mech. Engr., ● Western Condensing Co., 935 E. John St., and 1028 E. Pacific St., Appleton, Wis.

JENKINS, Harry C. (*A* 1946) Sales Mgr., Moduflow Div., Minneapolis-Honeywell Regulator Co., 2747 Fourth Ave. S., Minneapolis, Minn.

JENKINS, J. Caden (*A* 1946) Gen. Sales Mgr., Holly Manufacturing Co., 875 S. Arroyo Pkwy., Pasadena 5, and ● 259 E. Grandview Ave., Sierra Madre, Calif.

JENKINS, Raymond L. (*M* 1946) Cons. Mech. Engr., 4316 Blossom, Houston 7, Texas.

JENKINS, Sydney D. (*M* 1940) Partner, H. F. Clarke & Co., 1114 Fifth St. W., and ● 2212-33rd Ave. W., Calgary, Alta., Canada.

JENKINSON, V. J. (*A* 1940) Sales Mgr., Htg. Controls Div., Minneapolis-Honeywell Regulator Co., Ltd., Vanderhoof Ave., Leaside, Toronto 12, and ● 3 Highgate Rd., Toronto 9, Ont., Canada.

JENNER, John W. (*A* 1948) Pres. and Mgr., ● Shelley Electric Co., 123 S. Main, and 1522 Cooledge, Wichita, Kans.

JENNEY, Hugh B. (*A* 1933) Gen. Sales Mgr., ● Standard Sanitary & Dominion Radiator, Ltd., Royce and Lansdowne Ave., and 96 Dawlish Ave., Toronto, Ont., Canada.

JENNINGS, Burgess H.* (*M* 1942) Prof. of Mech. Engrg. and Dept. Chairman, Northwestern University, Northwestern Technological Institute, Evanston, Ill.

JENNINGS, Hal K. (*M* 1943) Vice-Pres., ● Kuempel Co., Union Trust Bldg., Cincinnati 2, and R. R. 2, Loveland, Ohio.

JENNINGS, Harvey S. (*M* 1947) Elec. Engr., Bechtel International Inc., Dhahran, Saudi-Arabia, and ● Box 1771, Spokane, Wash.

JENNINGS, Irving C. (*M* 1924) Pres., ● The Nash Engineering Co., and 138 Flax Hill Rd., South Norwalk, Conn.

JENNINGS, James H. (*M* 1944) Plant Engr., ● 430 N. Ninth St., Noblesville, and 4817 Indiana Ave., Fort Wayne, Ind.

JENNINGS, Robert B. (*A* 1946) Dist. Mgr., ● The Trane Co., 2901 N. High St., Columbus 2, and 166 Kenworth Ave., Columbus 8, Ohio.

JENNINGS, Stanley A. (*M* 1935) Engr., Trane Co. of Canada, Ltd., 4 Mowat Ave., and ● 36 Glen Oak Dr., Toronto, Ont., Canada.

JENNINGS, W. G. (*A* 1930) Vice-Pres., ● Minneapolis-Honeywell Regulator Co., 799 Beacon St., and 1970 Commonwealth Ave., Boston, Mass.

JENNY, Thomas J. (*A* 1948) Air Cond. Sales Engr., Gulf Engineering Co. Inc., 916 S. Peters St., New Orleans 13, and ● 4423 Loyola Ave., New Orleans 15, La.

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JENSEN, Albert O. (*A* 1944) Owner, ● Albert O. Jensen Wholesale Furnace & Supply Co., 515 North 18th St., Omaha 2, and 7409 North 57th St., Omaha, Nebr.

JENSEN, J. Ebbe (*M* 1947) Pres., Western Blower Co., 1800 Airport Way, Seattle 4, and ● Corbin Rd., Vashon Island, Wash.

JESPERSEN, S. Friis (*M* 1947) Cons. Engr., ● Vesterbrogade 10, Copenhagen V, and Bloksbjerget 24, Klapenborg, Denmark.

JESPERSEN, Soren J. (*M* 1944) Sr. Partner, Power Engineering Company, 1086 East 21st S., Salt Lake City, and ● 604 S. Ninth E., Salt Lake City 2, Utah.

JESSUP, Benjamin A. (*A* 1946) Vice-Pres., ● Richards & Jessup Co., Inc., 615 Main St., Stamford, and 48 Field St., Glenbrook, Conn.

JESSUP, F. Judson, Jr. (*A* 1944) 55 Woodland Park Dr., Tenafly, N. J.

JOCKEL, Hugh C. (*A* 1947) Sales Engr., ● Grinnell Co. of Canada, Ltd., 700 Beaumont Ave., Montreal, and 331 Beaconsfield Blvd., Beaconsfield, Que., Canada.

JOHANNESEN, Ralph C. (*M* 1943) Mech. Engr., O. W. Ott Cons. Mech. Engr., 514 Spring Arcade Bldg., Los Angeles 13, and ● 3468 Sierra Vista Ave., Glendale 8, Calif.

JOHNS, Charles F. (*M* 1939) Sackville, New Brunswick, Canada.

JOHNS, Harold B.* (*M* 1928; *J* 1927) Bell & Gossett Co., Morton Grove, and ● 543 N. Elmwood Ave., Oak Park, Ill.

JOHNSON, Allen J.* (*M* 1935) Cons. Engr., 344 Congress Ave., Lansdowne, Pa.

JOHNSON, Blaine A. (*M* 1946) Barney Olson, Inc., Peoples Gas Bldg., 122 S. Michigan Ave., Chicago 3, and ● 5724 N. Natoma Ave., Chicago, Ill.

JOHNSON, Carl E. (*A* 1939) Htg. and Vtg. Engr., ● C. E. Johnson & Assoc. 404 Bona Allen Bldg., and 1154 Ridgewood Dr. N.E., Atlanta, Ga.

JOHNSON, Carl W. (*Life Member*; *M* 1912) Pres., ● C. W. Johnson, Inc., 715 W. Randolph St., Chicago 6, and 1809 Morse Ave., Chicago 26, Ill.

JOHNSON, Carl William (*M* 1945) Mech. Engr., Mountain States Telephone & Telegraph Co., 931-14th St., Denver 2, and ● 2250 S. Clayton St., Denver 10, Colo.

JOHNSON, C. Kenneth (*A* 1945) Research Engr., Anemostat Corporation of America, 1051 New Britain Ave., and ● 187 Mayflower St., Elmwood, Conn.

JOHNSON, C. W. (*M* 1933; *J* 1931) Vice-Pres. and Gen. Mgr., ● Canadian Sirocco Co., Ltd., P. O. Box 360, and 11 Villaire Ave., Riverside, Windsor, Ont., Canada.

JOHNSON, Edward B. (*M* 1919) Designer, Parsons, Brinckerhoff, Hogan & Macdonald, 120 Wall St., New York, and ● 154 Wardwell Ave., Staten Island 2, N. Y.

JOHNSON, Enar A. (*M* 1947) Engr., G. M. Orr Engineering Co., 1004 Marquette, Minneapolis, and ● 2047 Grand Ave., St. Paul 5, Minn.

JOHNSON, Fred R. (*A* 1946) Vice-Pres., Johnson Heating Supply Co., 725 Northeast 25th Ave., Portland 12, and ● 2657 N. Kilpatrick St., Portland 3, Ore.

JOHNSON, Fred W. (*M* 1939) Pres., ● Johnson Larsen Co., 6530 Beaubien St., Detroit 2, and Adams and Beaver Rds., R. F. D. 2, Birmingham, Mich.

JOHNSON, Harry H. (*A* 1944) Owner and Mgr., ● City Plumbing & Heating Co., 760 N. Third St., Box 634, and 412 South 12th St., Laramie, Wyo.

JOHNSON, Helge S. (*A* 1933; *J* 1927) Partner, ● Koithan & Johnson, Reprs., Buffalo Forge Co., 39 Cortlandt St., New York 7, and 6 Forest Lane, Scarsdale, N. Y.

JOHNSON, Hiram K. (*A* 1945) Vice-Pres., ● F. S. Lamson Co., Inc., 1013 Marquette Ave., Minneapolis 2, and 4904 Tenth Ave. S., Minneapolis 7, Minn.

JOHNSON, Hugh F., Jr. (*J* 1945) Field Engr., ● Carrier Corp., 20 N. Wacker Dr., Chicago 6, Ill., and 30 Johnson Ave., Indianapolis, Ind.

JOHNSON, James J. (*M* 1944) ● Marshal & Johnson, 1275 Sherman St., Denver 3, and 66 Ash St., Denver 7, Colo.

JOHNSON, John B., Jr. (*A* 1947) Sales Engr., Westinghouse Electric Corp., Mansfield, and ● 248 Stanford Ave., Elyria, Ohio.

JOHNSON, Leslie Otto (*M* 1938; *J* 1930) Sales Engr., ● 215 Hines Bldg., Box 434, and 339 Sixth Ave., Huntington, W. Va.

JOHNSON, Oliver W. (*M* 1938) Chem. Engr., Standard Oil Company of California, 225 Bush St., San Francisco, and ● 1831 Waverly St., Palo Alto, Calif.

JOHNSON, Paul H. (*J* 1946) Bryant Heater Co., 17825 St. Clair Ave., Cleveland 10, and ● 2854 Sedgewick Rd., Cleveland 20, Ohio.

JOHNSON, Philip B. (*A* 1945) Design Engr., Curtiss Wright Corp., 5900 E. Fifth Ave., Columbus, and ● 59 S. Ogden Ave., Columbus 4, Ohio.

JOHNSON, Ralph B. (*M* 1940) Owner, ● Ralph B. Johnson & Co., 1605 Westheimer St., P. O. Box 1961, Houston 1, and 2111 W. Main St., Houston 6, Texas.

JOHNSON, Raymond C., Dr. (*M* 1944) Vice-Pres., Research, ● Anthracite Institute, 237 Old River Rd., and Hotel Sterling, Wilkes-Barre, Pa.

JOHNSON, Raymond L. (*M* 1946; *A* 1943; *J* 1942) Research Engr., Young Radiator Co., 709 S. Marquette St., and ● 2003 Marquette St., Racine, Wis.

JOHNSON, Richard W. (*A* 1947) Sales Repr., Republic Heaters Co., 2153 W. Fullerton Ave., Chicago 47, and ● 3551 N. Vincent Ave., Minneapolis 12, Minn.

JOHNSON, Roy W. (*A* 1945) Partner, ● Johnson-Lenz, 293 Jefferson Ave., Memphis 3, and 346 N. Willett, Memphis 7, Tenn.

JOHNSON, Russell A. (*J* 1945) Cons. Engr., Russell A. Johnson, Engr. Cons., 333 N. Michigan Ave., Chicago, and ● 371 Miller Dr., Elgin, Ill.

JOHNSON, Sigurd O. (*A* 1948; *J* 1946) Sales Engr., • Buffalo Forge Co., 39 Cortlandt St., New York, N. Y., and P. O. Box 167, Colonia, N. J.

JOHNSON, Sterling Chester (*A* 1947) Partner, • Burnett-Johnson Appliance Co., 37 Clarksville, and 1940 E. Washington, Paris, Texas.

JOHNSON, Tracy R. (*M* 1938) Branch Mgr., • The Trane Co., 1026 Fleming Bldg., Des Moines 9, and 6510 Forest Ave., Des Moines 11, Ia.

JOHNSON, Walter L. (*A* 1947) Sales Engr., Norman S. Wright & Co., 233 Ninth Ave. N., and • 1153 West 58th St., Seattle 7, Wash.

JOHNSON, Walter R. (*A* 1947) Chief Engr. & Supt. of Construction, Nickey Brothers, Inc., 2700 Summer Ave., and • 2643 Hanover Ave., Memphis, Tenn.

JOHNSON, Wilfrid E.* (*M* 1946) Mgr. of Engrg., • General Electric Co., 5 Lawrence St., Bloomfield, and 48 Baker Rd., Livingston, N. J.

JOHNSON, William A. (*A* 1945) Pres., Johnson-Goodyer, Inc., • 45 Bristol St., P. O. Box 576, New Haven, and 361 Fountain St., New Haven 15, Conn.

JOHNSTON, Arthur K. (*A* 1942) Owner, • 431 S. E. Sixth Ave., Portland 14, and Rt. 3, Box 913, Portland, Ore.

JOHNSTON, James Ambler (*M* 1912) Partner, Carneal & Johnston, Atlantic Life Bldg., Richmond 19, Va.

JOHNSTON, Jerrold J. (*J* 1948; *S* 1946) Mech. Engr., Tech. Sect., E. I. DuPont de Nemours & Co., Sabine River Works, and • 206 Hobson Ct., Orange, Texas.

JOHNSTON, J. O. (*A* 1945) Engr., • City Fuel Oil & Coal Co., 15th Ave. and Second St. S., and Box 474, St. Petersburg, Fla.

JOHNSTON, Lowell T. (*A* 1945) Master Mech., Johnstone Brothers Fuel Co., P. O. Box 207, 22nd St. Sta., St. Petersburg, and • 2332 Lakeview Ave. S., St. Petersburg 7, Fla.

JOHNSTON, Robert E. (*M* 1929; *A* 1926) Pres., • R. E. Johnston Co., Ltd., 1070 Homer St., and 4583 Connaught Dr., Vancouver, B. C., Canada.

JOHNSTON, Robert M. (*A* 1942; *J* 1937) Lt., U. S. N. R., Dept. Marine Engrg., U. S. Naval Academy, Annapolis, and • Cumberstone, Anne Arundel County, Md.

JOHNSTON, T. Walter (*A* 1947) Territory Sales Mgr., Lennox Furnace Co., Marshalltown, Ia., and • Box 173, Auburn, Calif.

JONES, Alfred (*Life Member*; *M* 1928) Retired, and • 912 Darby Rd., Havertown, Pa.

JONES, Allan T. (*M* 1937; *J* 1935) Chief Engr., • S. A. Armstrong, Ltd., 115 Dupont St., Toronto 5, and 264 Westwood Ave., Toronto, Ont., Canada.

JONES, Arthur L. (*M* 1947) Dist. Mgr., • American Blower Corp., Room 612, Syracuse Kemper Bldg., and 124 Fernwood Ave., Syracuse, N. Y.

JONES, Charles D. (*A* 1946) Owner & Mgr., • Charles D. Jones & Co., 3023 Main St., Kansas City 8, and 1824 West 72nd Terrace, Kansas City 5, Mo.

JONES, David C. (*A* 1946) Mgr. and Owner, • Service Heat & Power Co., 636-21st St., Oakland, and 51 Barbara Rd., Orinda, Calif.

JONES, Donald R. A. (*A* 1942) Indus. Gas Engr., Southern California Gas Co., 515 E. Compton Blvd., and • 404 S. Chester Ave., Compton, Calif.

JONES, Edgar C. (*J* 1947) Engr., Page Air Conditioning Co., Inc., 220 S. College St., and • 2212 Chambwood Dr., Charlotte, N. C.

JONES, Edwin (*M* 1933; *J* 1924) Engr. and Estimator, • Watt Plumbing, Heating & Supply Co., 608 S. Cincinnati, and 1436 East 17th Pl., Tulsa, Okla.

JONES, Edwin A. (*M* 1919) Staff Engr., Chrysler Corp., Airtemp Div., and • 1848 Tennyson Ave., Dayton 6, Ohio.

JONES, F. Chandler, Jr. (*M* 1947) Equip. Engr., Htg. & Air Cond. Dept., • Westinghouse Electric Corp., Sturtevant Div., Hyde Park, and 133 Gibbs St., Newton Centre 59, Mass.

JONES, Frank (*S* 1947) Student, and • Warren Rd., Ashland, Mass.

JONES, Harold L. (*M* 1920) • 33 Clay St., Newark 4, and 11 Cambridge Rd., Glen Ridge, N. J.

JONES, Harold S. (*J* 1942; *S* 1940) Jr. Engr., Stewart Distributing Co., 1019 E. Broadway, Louisville 4, and • Box 361, Rt. 6, Arlington Rd., Avondale, Louisville 7, Ky.

JONES, Hubert L. (*M* 1943) Pres., • Air Conditioning Engineering Corp., Box 1925, Ft. Worth, and 1101 Sixth Ave., Fort Worth 4, Texas.

JONES, James T. (*A* 1939) Engr., Merchandise and Serv. Dept., • The Empire District Electric Co., and 525 N. Sergeant, Joplin, Mo.

JONES, Joe T. (*A* 1945) Appl. Engr., • Fulton Sylphon Co., 417 Barr Bldg., Washington 6, and 1428 Saratoga Ave. N.E., Washington 18, D. C.

JONES, John D. (*A* 1945) Owner, • Bryant Gas Heating Co., 626 Broadway, Cincinnati 2, Ohio, and 26 Sunset Ave., Fort Thomas, Ky.

JONES, John Paul (*M* 1937) Sr. Partner, • John Paul Jones, Cary & Millar, 1740 East 12th St., Cleveland 14, and 3041 Fairfax Rd., Cleveland Heights, Ohio.

JONES, Lawrence K. (*M* 1939) Mgr., Special Test Sect., • Pittsburgh Testing Laboratory, 1330 Locust St., and 320 S. Aiken Ave., Pittsburgh, Pa.

JONES, Leslie R. (*A* 1947) Sales Engr., Pacific Pumping Co., 526 N.W. Broadway, and • 2154 N.W. Upshur, Portland, Ore.

JONES, Oran D. (*S* 1946) 513 Logansport, Nacogdoches, Texas.

JONES, Sidney Joseph (*M* 1946) Southern Area Mgr., • Thermotank, Ltd., Colneside Works, Trout Rd., West Drayton, and 52 Devonshire Rd., Harrow, Middlesex, England.

JONES, Thomas S. (*A* 1941) Mgr., Crane Co., 1328 West 12th St., Kansas City 7, Mo.

JONES, T. Paul (*A* 1944) Owner and Gen. Mgr., • Air Equipment Co., 2730 Zuni St., and 801 Teller St., Lakewood, Denver, Colo.

JONES, Warren L. (*A* 1946) Owner, Anchor Supply Co., 1507 N. First St., and • 229 Graceland Pl., Albuquerque, N. M.

JONES, William C. (*M* 1941) Mgr., • Johnson Service Co., 1931 K St. N.W., Washington 6, D. C., and Triadelphia Rd., R. F. D. 2, Ellicott City, Md.

JORDAN, Frank W. (*M* 1946) Pacific Coast Dist. Mgr., • Westinghouse Electric Corp., Sturtevant Div., 681 Market St., San Francisco 5, Calif.

JORDAN, Paul R. (*M* 1943) Pres., • Paul R. Jordan & Co., 311 E. South St., Indianapolis 4, and 2230 East 75th St., Indianapolis, Ind.

JORDAN, Richard C.* (*M* 1940; *J* 1935; *S* 1933) Prof. and Asst. Head, Dept. of Mech. Engrg., • University of Minnesota, and 1101 E. River Rd., Minneapolis 14, Minn.

JORDY, Jules J. (*A* 1947; *J* 1940) Lt., U.S.N.R., Engr. and Contr., • Jordy Brothers, Inc., 518 Julia St., New Orleans, La.

JORGENSEN, Earl W. (*S* 1948) Student, University of Michigan, Ann Arbor, • 953 E. Michigan, Ypsilanti, Mich.

JOSLIN, George C. (*A* 1943) Territorial Repr., • Carver Pump Co., 1916 N. Meridian St., Indianapolis 2, and 525 N. Colorado Ave., Indianapolis 1, Ind.

JOUANNO, Edouard P. (*M* 1946) Engr., Autocalor, 24 Rue Erlanger, Paris, (XVI), and • 11 bis Rue des Dardanelles, Paris, (XVII), France.

JOY, Frank A. (*M* 1947) Assoc. Prof. of Engrg. Research, Engineering Experiment Station, State College, Pa.

JOYCE, Harry B. (*M* 1944) Registered Engr., • 616 Commerce Bldg., and 613 Virginia Ave., Erie, Pa.

JOYCE, James J. (*A* 1941) Supt. Constr. and Service, • The Powers Regulator Co., 142 Spring St. N.W., and 525 Mellview Ave., Atlanta, Ga.

JUDSON, Albert L. (*A* 1947) Chief Engr., Iron Fireman Manufacturing Co., Heating Control Div., 2838 S.E. Ninth Ave., and • 7339 S.E. 35th Ave., Portland 2, Ore.

JUER, Frederick (*A* 1946) Sales Engr., • Minneapolis-Honeywell Regulator Co., 325 E. Central Pkwy., and 408 Considine Ave., Cincinnati, Ohio.

JUERGENS, Walter A. (*A* 1940) Owner, • Walter A. Juergens, 710 Times Star Tower, Cincinnati 2, and 1447 Aster Pl., Cincinnati, Ohio.

JUHL, Edward F. (*A* 1945) Chief Engr., Thorpe Bros., Inc., 1100 Andrus Bldg., Minneapolis 2, and • 4432 Stevens Ave., Minneapolis 9, Minn.

JUNG, Francis P. (*A* 1946) Dist. Engr., Indus. Hygiene Service, • Tennessee Department of Public Health, 879 Madison Ave., and 1430 C Pendleton, Memphis, Tenn.

JUNG, Howard G. (*A* 1948) Engr. & Sales, The Zack Co., 2311 Van Buren, and ● 8045 S. Green St., Chicago, Ill.

JUNG, John S. (*M* 1930; *A* 1923) Owner, ● John S. Jung Heating Co., 2409 W. Greenfield Ave., and 1516 S. Layton Blvd., Milwaukee 4, Wis.

JUNGELS, Alton J. (*M* 1945) Engr., Dealer Sales, John A. Connelly Co., 4308 N. Broad St., Philadelphia, and ● 1711 Erlen Rd., Philadelphia 26, Pa.

JUNGELS, John W. (*A* 1947) Mgr., Differential Htg. and Serv., C. A. Dunham Co., 450 E. Ohio St., Chicago 11, and ● 728 Front St., Aurora, Ill.

JUNGER, Henry G. (*A* 1946) Sales Engr., Anemostat Corporation of America, 10 East 39th St., New York, and ● 214-16–111th Rd., Queens Village, N. Y.

JUNKER, W. H. (*M* 1936) Cons. Engr., W. W. Carlton & Assoc., 15 E. Eighth St., Cincinnati 14, and ● 6068 Dryden Ave., Cincinnati 13, Ohio.

JUSTICE, Jack T. (*A* 1945) Prop., Conditionaire, 215 E. Kingshighway, and ● 727 W. Vine, Paragould, Ark.

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KLEINHOMER, William G. (*A* 1943) Mech. Engr., Wohlpart and Hart, 155 East 42nd St., New York, and • 2142 Troy Ave., Brooklyn 3, N. Y.

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KLINE, F. L. (*A* 1946) Gas Engr., • Iowa Power & Light Co., 312 Sixth Ave., and 4022 Sixth Ave., Des Moines, Ia.

KLINE, W. O. (*M* 1946) Air Cond. Div., Frick Co., and • 12 N. East Ave., Waynesboro, Pa.

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KLUGER, Edwin C. (*A* 1947) Sales Engr., Jas. P. Marsh Corp., 2073 Southport Ave., Chicago, Ill., and • 4803 Montauk Ave., Parma 9, Ohio.

KNAB, Edward A. (*M* 1943) Sole Owner, • E. A. Knab, Htg. and Plbg. Contr., 3723 N. Oakland Ave., and 1115 W. Greentree Rd., Milwaukee 11, Wis.

KNECHT, A. Wilson (*M* 1948) Asst. Chief Engr., Walter Kidde Constructors, Inc., 140 Cedar St., New York 6, and • 20 Grosbeak Rd., Yonkers 2, N. Y.

KNEE$Σ, Victor C. (*A* 1945) Sales Engr., • Southland Supply Co., 2400 South Harwood, and 3124 Princeton, Dallas, Texas.

KNIBB, Alfred E. (*M* 1930) Htg. Engr., • L. L. McConachie Co., 1003 Maryland Ave., Detroit 30, and 9333 E. Jefferson Ave., Detroit 14, Mich.

KNIGHT, Richard C. (*A* 1946) Mgr., Htg. and Vtg. Dept., • Macatee, Inc., P. O. Box 838, and 3504 Greenbrier, Dallas, Texas.

KNIGHTON, John K. (*M* 1944) Mgr. of Sales, • Servel, Inc., and Schenk Rd., R. R. 7, Evansville, Ind.

KNIPE, William E. (*A* 1946) Owner, William E. Knipe Sales & Service, 9202 Delphine, St. Louis 14, Mo.

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KNOWLES, E. L. (*A* 1937) Owner, • Marshall Heating Co., 1324 Marshall St. N.E., Minneapolis 13, and 400 Thomas Ave. S., Minneapolis 5, Minn.

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KNOX, J. Roy (*A* 1945) Branch Mgr., • U. S. Radiator Corp., 1713 E. Carson St., Pittsburgh 3, and 18 Home Kort, West View, Pittsburgh 2, Pa.

KNOX, Walter (*M* 1943) Appl. Engr., Rheem Manufacturing Co., 20 N. Wacker Dr., Chicago 6, Ill.

KOCH, Albert H. (*M* 1938) Branch Mgr., • Minneapolis-Honeywell Regulator Co., 5060 Wayne Ave., Philadelphia 44, and 410 Charles Lane, Wynnewood, Pa.

KOCH, Joseph J. (*A* 1947) Partner, • J. F. Shelton Co., 200 Poplar, and 420 N. McNeil, Memphis, Tenn.

KOCH, Richard G. (*A* 1935) Engr., Sales Dept., • Milwaukee Gas Light Co., 626 E. Wisconsin Ave., Milwaukee 2, and 5707 W. Brooklyn Pl., Milwaukee 10, Wis.

KOCHEL, R. K. (*A* 1945) Project Engr. Refrig., • Jack & Heintz Precision Inc., Cleveland, and • R. D. 1, Mogadore, Ohio.

KOEHLER, C. Stewart (*A* 1936) Air Cond. Controls Div., Minneapolis-Honeywell Regulator Co., 221 Fourth Ave., New York 3, and • 3135 Hull Ave., New York 67, N. Y.

KOENIG, Andrew C. (*A* 1948; *J* 1940) Sales Engr., J. A. Koenig, 701 E. Missouri St., Evansville, and • 635 E. Louisiana St., Evansville 11, Ind.

KOENIG, Max E. R. (*M* 1947) Chief Engr., Htg. Dept., Louis de Roll Iron Works Ltd., Klus, and • Balsthal/SO, Switzerland.

KOHN, Walter P. (*A* 1946) Indus. Appl. Engr., York Corp., 2700 Washington Ave., and • 3647 East Blvd., Cleveland, Ohio.

KOLASA, Marion J. (*A* 1947; *J* 1942) Partner, • Kolasa Products, 19639 Van Dyke Ave., Detroit, and 19650 Norwood Ave., Detroit 12, Mich.

KOLB, Fred W. (*M* 1938) Owner, • 598 Monadnock Bldg., San Francisco 5, and 82 Macondray St., San Francisco 11, Calif.

KOLB, Robert P. (*M* 1939) Prof. of Heat-Power Engrg., Supt. of Heat & Power, ● Worcester Polytechnic Institute, Worcester 2, and 46 Beechmont St., Worcester 5, Mass.

KOLBER, Irving A. (*J* 1948; *S* 1947) Engr., Murphy & Miller, Inc., 1326 S. Michigan Ave., Chicago, and ● 1257 Lunt Ave., Chicago 26, Ill.

KOLLAS, Will J. (*M* 1939) Engr., The Lynch Co., 6000 N.E. Union Ave., and ● 6104 N. Missouri Ave., Portland 11, Ore.

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KOPECKY, Joseph J. (*A* 1946) Designer-Draftsman, Voorhees, Walker, Foley & Smith, 20 Broad St., New York, and ● 209 East 76th St., New York 21, N. Y.

KOPER, C. H. (*A* 1946) Sales Engr., ● B. F. Sturtevant Co., Div. of Westinghouse Electric, 933 Leader Bldg., Cleveland 14, and 2138 Glenbury St., Cleveland 7, Ohio.

KORN, Charles B. (*M* 1922) Engr. and Member of Firm, Reber-Korn Co., 817 Cumberland St., and ● 1022 S. Eighth St., Allentown, Pa.

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KOSTER, Howard H. (*A* 1942; *J* 1939) Appl. Engr., Westinghouse Electric International Co., 40 Wall St., New York 5, N. Y., and ● 44 Aubrey Rd., Upper Montclair, N. J.

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KOTZEBUE, Robert W. (*M* 1944) Partner, Bell-Kotzebue Co., 1505 E. Houston St., San Antonio 2, and ● 438 Paseo Encinal, San Antonio 1, Texas.

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KRAPOHL, William H. (*M* 1941) Owner, ● A. & K. Engineering Co., Inc., 1838 Centre St., and 79 Prospect St., West Roxbury, Boston 32, Mass.

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KRUSE, W. C., Jr. (*M* 1938) Owner, ● Kruse Engineering Co., 24 Commerce St., Newark 2, and 292 Scotland Rd., South Orange, N. J.

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KUEMPEL, Leon L. (*M* 1936; *J* 1929) Pres., Keco Industries, Inc., Union Trust Bldg., Cincinnati 2, and ● 3702 Homewood Rd., Cincinnati 27, Ohio.

KUGEL, Edmund F. (*A* 1947) Supt. of Installation, Montag Stove & Furnace Works, 2011 N. Columbia Blvd., and ● 5524 N.E. Rodney Ave., Portland 11, Ore.

KUGEL, H. Kenneth (*M* 1938) Chief Engr., Smoke Regulation & Boiler Inspection, 102 District Bldg., Washington 4, and ● 3825 Morrison St. N.W., Washington 15, D. C.

KUGELER, H. Coors (*M* 1944) Appl. Engr., The Stearns Roger Manufacturing Co., 1720 California St., Denver 2, and ● 2365 Ash St., Denver 7, Colo.

KUGLIN, Charles R. (*M* 1945) Chief Engr., R. V. Mehaffey Associated Engineers, 30 N. LaSalle St., Chicago, and ● 10207 S. Wood St., Chicago 43, Ill.

KUHLMAN, Charles E. (*J* 1947) Asst. Supt., Kuhlman Homes Co., 1711 Natl. Bank Bldg., Detroit, and ● 11828 Rossiter, Detroit 24, Mich.

KUHLMANN, Rudolf (*M* 1928) Mgr., ● Ameresco, Inc., 50 Church St., New York, and Glenwood Gardens, Yonkers, N. Y.

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KURTH, Franz B., Jr. (*J* 1945) Liaison Engr., Anemostat Corporation of America, 10 East 39th St., New York, N. Y., and ● 2411 Loretta Dr., Tucson, Ariz.

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L

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LAIR, P. H. (*M* 1940) Engr. Coordinator, Ebasco Services Inc., 2 Rector St., New York, N. Y., and • 24 Glenwood Dr., Short Hills, N. J.

LAJOIE, J. Rene (*A* 1946) Chief Instructor, Htg. and Plbg. Comm., Montreal Bldg. Trades Apprenticeship, 2275 Laurier E., Montreal, and • 3735 Basset, Montreal 18, Que., Canada.

LAMB, Jordan H. (*A* 1947) Engr., Twin Coach Co., Kent, and • c/o General Delivery, Rt. 1, Hudson, Ohio.

LAMBERSON, L. D., Jr. (*A* 1946) Chief Engr., • Williamson Favret Furnace Co., 55 E. Goodale St., Columbus 8, and 871 Euclaire Ave., Bexley, Columbus 9, Ohio.

LAMBERT, Edward G. (*A* 1945) Mgr., • Building Maintenance Service, Inc., 810 S. St. Paul, and 217 S. Ravinia, Dallas, Texas.

LAMBERT, Edward H. (*A* 1944) Pres., E. H. Lambert & Co., Room 28, 130 Main St., Stamford, and • Hendrie Ave., Riverside, Conn.

LAMBERT, Ernest (*A* 1946) Mgr., Htg. Dept., Crane Ltd., 93 Lombard St., Winnipeg, Man., Canada.

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LAMBERT, Thomas A. (*M* 1946) Assoc. Mech. Engr., Norfolk Naval Shipyard, Public Works Dept., Portsmouth, and • 1123 Manchester Ave., Norfolk 8, Va.

LAMMONS, John B. (*A* 1944) Mfrs. Repr., • J. B. Lammons, P. O. Box 502, and 930 N. Evergreen St., Memphis, Tenn.

LAMONT, James F. (*A* 1946) Gen. Sales Mgr., The M. S. Little Manufacturing Co., 151 New Park Ave., Hartford, Conn.

LAMONTAGNE, A. F. (*A* 1936) Sales Mgr., • Gurney Foundry Co., Ltd., 100 Principal St., St. Laurent, and 5040 Victoria Ave., Montreal, Que., Canada.

LAMOUREUX, Philip J. (*A* 1947) Engr., • E. R. Clement, Inc., 1346 Kossuth St., Bridgeport, and Pine Creek Rd., Fairfield, Conn.

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LANDERS, David N. (*A* 1944) Owner, • Landers Plumbing & Heating Co., 241 Marietta St. N.W., Atlanta 3, and 56-26th N.W., Atlanta, Ga.

LANDERS, John J. (*M* 1932) • Landers Engrg. Co., 170 Franklin St., Buffalo, and 120 Burroughs Dr., Snyder, N. Y.

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LANG, George T. (*M* 1946) Mech. Engr. in charge of Air Cond., A. S. S. A. Ltda. S. A. I., Avenida Alcorta 2601, and • Bulnes 1940, Buenos Aires, Argentina, S. A.

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LANGDON, Tom C. (*J* 1943) Owner, • T. C. Langdon Co., 2603 N.E. Union Ave., and 1910 N.E. Weidler St., Portland 12, Ore.

LANGE, Fred F. (*M* 1947; *A* 1934) Pres., • The Mechanical Service Co., 809 Pence Bldg., Minneapolis 3, and 510 Fourth Ave. S.W., Faribault, Minn.

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LANOU, J. Ernest (*M* 1931) Mgr., • F. S. Lanou & Son, 90 St. Paul St., and 48 Brookes Ave., Burlington, Vt.

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LARSON, Carl W. (*M* 1936) Htg. Engr. and Providence, R. I. Repr., Barnes & Jones, Inc., 128 Brookside Ave., Jamaica Plain 30, and • 184 Sycamore St., Roslindale 31, Mass.

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LARSON, Clifford P. (*A* 1939; *J* 1936) Asst. to Vice-Pres., • Minnesota & Ontario Paper Co., 500 Baker Arcade, and 17 East 54th St., Minneapolis, Minn.

LARSON, G. L.* (*M* 1923), (*Presidential Member*), (Pres., 1936; 1st Vice-Pres., 1935; 2nd Vice-Pres., 1934; Council, 1929-37) Prof. of Mech. Engrg., • University of Wisconsin, Mech. Engrg. Bldg., Madison, and 1213 Sweetbriar Rd., Shorewood Hills, Madison, Wis.

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LAUTZ, Fritz A. (*M* 1936) Maint. Engr., American Bemberg Corp., Elizabethton, and • R. F. D. 1, Johnson City, Tenn.

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LAWRENCE, Floyd D. (*A* 1938) Field Repr., • Clarage Fan Co., 500 Fifth Ave., Room 1024, New York 18, N. Y., and 60 Gardiner St., Noroton Heights, Conn.

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LAYTON, Robert E., Jr. (*J* 1947) Sales Engr., L. O. Layton Supply Co., 1416 W. Erwin, and • Box 461, Tyler, Texas.

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LEE, Boyd J. (*A* 1945) Owner, • B. J. Lee Co., 236 Adams Ave., Memphis 3, and 1674 Faxon Ave., Memphis, Tenn.

LEE, Burton H. (*M* 1945; *A* 1940) Chief Engr., Mance Corp., 400 W. Broadway, New York 12, and • 50 Mohican Park Ave., Dobbs Ferry, N. Y.

LEE, Carl M. (*A* 1944) Foreman, Air Cond. Dept., Allison Div., General Motors Corp., Plant 5, Tibbs and Raymond St., Indianapolis, and • 4535 Brookville Rd., Indianapolis 1, Ind.

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LEE, William R. (*A* 1947) Bldg. Supt., • Southwestern Art Association, 303 Beacon Bldg., and 1019 S. Main St., Tulsa 3, Okla.

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LEFEBVRE, Eugene J. (*M* 1937) Engr., Warden King, Ltd., 2104 Bennett Ave., Montreal, and ●12 Melbourne Ave., Westmount, Que., Canada.

LEFFEL, Paul C. (*A* 1941) Htg. Equip. Distributor, ● The Leffel Co., 3323 Main St., Kansas City 2, and 316 East 75th St., Kansas City, Mo.

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Le GRAND, I. F. (*M* 1947) Managing Partner, ●Air Engineers, 125 S. Eighth St., and Route 1, Allentown, Pa.

LEHMAN, Max G. (*A* 1937) Owner, ●M. G. Lehman, 720 O St., and 3225 W. Pershing Rd., Lincoln, Nebr.

LEIBY, Robert S. (*A* 1944) Owner and Mgr., ●Robert S. Leiby Sheet Metal Co., 212 N. Grant Ave., Columbus, and 6870 Havens Corners Rd., New Albany, Ohio.

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LEVINE, Lawrence J. (*A* 1946; *J* 1940) D.I.C. Staff Member, Massachusetts Institute of Technology, Dept. of Aeronautical Engineering, Cambridge 39, and ●9 Westchester Rd., Newton 58, Mass.

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LEVINSON, David S.* (*J* 1948; *S* 1946) Engineer, ●Surface Combustion Corp., Air Cond. Div., Toledo 1, Ohio, and 53 W. Ferguson Ave., Wood River, Ill.

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LEWIN, Bram J. (*A* 1947) Engr., ●Lewin Mathes Co., 1111 Chouteau Ave., St. Louis 2, and Conway & Ballas Rds., St. Louis County, Mo.

LEWIN, Jacob (*A* 1946) Owner, ●J. Lewin & Co., 1075 Laurier St. W., Outremont, and 4925 Victoria Ave., Montreal, Que., Canada.

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LEWIS, Daniel H. (*A* 1944) Owner, ●Lewis Engineering Service, 19003 John R, and 1059 W. Lantz, Detroit 3, Mich.

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LEWIS, Herald F. (*M* 1940; *A* 1937) Major, Stuttgart Mil. Post, APO 154, New York, N. Y.

LEWIS, Harry E. (*A* 1942; *J* 1939) Mgr., Insulation Engrg. Dept., • The Eagle-Picher Sales Co. Insulation Div., 900 American Bldg., Cincinnati, Ohio, and 137 Walnut St., Southgate, Ky.

LEWIS, J. C. (*A* 1944) Owner, • J. C. Lewis Co., 3815 Garrott St., Houston 6, and 4914 Linden, Bellaire, Texas.

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LEWIS, L. L.* (*M* 1918) Vice-Pres., • Carrier Corp., S. Geddes St., Syracuse 1, and 207 Sedgwick Dr., Syracuse 3, N. Y.

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LINDSAY, Griffith W. (*M* 1937) Supvsr., Estimating and Time Study, Chrysler Corp., Airtemp Div., 1119 Leo St., Dayton, and • 301 N. Garland Ave., Dayton 3, Ohio.

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MARSHALL, W. D. (*M* 1935) Mgr., Noland Co., Inc., 1823 N. Arlington Ridge Rd., and ● 3232 Woodrow St. N., Arlington, Va.

MARSTON, Anson D. (*A* 1937) Colonel, ● Corps of Engrs., U. S. Army, Instructor, Command & General Staff College, and 614 McClellan Ave., Fort Leavenworth, Kans.

MART, Leon T. (*M* 1941) Pres., ● The Marley Co., Inc., 3001 Fairfax Rd., Kansas City, Kans., and 6840 Tomahawk Rd., Kansas City, Mo.

MARTEL, C. L. (*A* 1946) Secy.-Treas. ● Martel Engineering, Inc., 13739 Gratiot Ave., Detroit, and 24501 Colin Kelly, Centerline, Mich.

MARTENIS, William W. (*M* 1946) Chief Project Coordinator, Engrg. Dept., Minneapolis-Honeywell Regulator Co., 2753 Fourth Ave. S., and ● 300 Busch Terrace, Minneapolis, Minn.

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MARTIG, Robert W. (*M* 1947) Vice-Pres., ● Farnes & Martig, Inc., 417 N.E. Couch St., Portland 14, and Rt. 2, Box 321, Portland 10, Ore.

MARTIN, Albert B. (*M* 1917) Distr. Mgr., ● Kewanee Boiler Corp., 549 Washington Blvd., Chicago 6, and 860 Spruce, Winnetka, Ill.

MARTIN, G. D. (*M* 1941) Branch Mgr., ● Grinnell Company of Pacific, 601 Brannan St., San Francisco 17, and 398 Menlo Oaks Dr., Menlo Park, Calif.

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MARTIN, Henry L. (*M* 1945) Div. Head, Steam Sales and Service, Boston Edison Co., 39 Boylston St., Boston, and ● 75 Hunnewell Ave., Newton 58, Mass.

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MARTIN, Kenneth E. (*M* 1947) Branch Mgr., ● American Blower Corp., 203 Patterson Bldg., Omaha 2, and 4112 Nicholas, Omaha 3, Nebr.

MARTIN, Raymond (*A* 1937) Sales Engr., ● Vapor Car Heating Company of Canada, Ltd., 65 Dalhousie St., Montreal, and 27 Morris Ave., Ste. Therese, Que., Canada.

MARTIN, R. J. Wesley (*J* 1946) Draftsman, Imperial Iron Corp., Ltd., 30 Jefferson Ave., and ● 68 Northcote Ave., Toronto, Ont., Canada.

MARTIN, Samuel S. (*J* 1948; *S* 1946) General Mgr., ● Martin Engineering Co., Box 825, San Juan, Texas.

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MARTIN, Thomas I., Jr. (*J* 1947) Asst. to Prod. Mgr., Insulation Dept., ● Reynolds Metals Co., Third & Grace Sts., Richmond, and 901 S. East St., Culpeper, Va.

MARTIN, Wilbert A. (*A* 1944) Mgr., Air Cond. Dept., American Heating Co., 55 K St. S.E., Washington, D. C., and ● 8805 Reading Rd., Silver Spring, Md.

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MARTIN, William T. (*M* 1943) Chief Engr., Beech-Nut Packing Co., and ● 87 Cliff St., Canajoharie, N. Y.

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MARTYN, Henry J. (*A* 1937) Pres., ● Martyn Bros., Inc., 1000 St. Louis St., Dallas 2, and 5306 Ridgedale St., Dallas, Texas.

MARTYN, Henry J., Jr. (*J* 1948; *S* 1946) Constr. Foreman, Martyn Brothers, Inc., 1000 St. Louis St., and ● 3307 Cherrywood, Dallas, Texas.

MARVIN, Philip R. (*A* 1945) Dir. of Research and Dvlpt., ● Milwaukee Gas Specialty Co., 722 N. Jackson, Box 461, Milwaukee 1, and 6828 W. Wisconsin, Milwaukee 13, Wis.

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MARZORATI, Giuseppe (*M* 1938) Tecnica Industriale dott. ing., ● 28 Via Mauro Macchi, and 9 Via Baldissera, Milano, Italy.

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MASON, Ray B. (*M* 1941) Mgr., Kansas City Branch, ● Kewanee Boiler Corp., 2014 Wyandotte St., and 121 East 70th Terrace, Kansas City, Mo.

MASON, Raymond P. (*M* 1945) Asst. Supt. Engr., U. S. Army Transport Service, Planning Sect., Bldg. 310, Ft. Mason, and ● 27 Westminister Ave., Berkeley 8, Calif.

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MASON, Robert Edwards (*J* 1947) Engr., Air Cond. Div., Sidles Co., 502 South 19th St., and ● 4340 Binney St., Omaha, Nebr.

MASSAGLIA, Paoli E. C. (*J* 1947; *S* 1945) Jr. Engr., Black & Veatch, and ● 3814 Parallel Ave., Kansas City, Kans.

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MATHER, Harry H. (*A* 1929) Mfrs. Agent, 1212 Commercial Trust Bldg., Philadelphia 2, and ● 377 Windemere Ave., Drexel Hill, Lansdowne P. O., Pa.

MATHERS, William (*A* 1947) Partner, ● Mathers-Curl & Associates, 80 S. Third St., and 630 E. Town St., Columbus 15, Ohio.

MATHESON, Elmer E. (*A* 1946) Owner, Appliance Shop, and ● 1001 W. Yakima St., Pasco, Wash.

MATHEWSON, M. E. (*M* 1937) Secy., ● A. M. Kinney, Inc., 1211 Enquirer Bldg., Cincinnati 2, and 1110 Priscilla Lane, Cincinnati 8, Ohio.

MATHEY, Nicholas J. (*M* 1945) 325 Fourth Ave. S., Clinton, Ia., and ● Apt. 13, Lane I, Sunflower, Kans.

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MATHIS, John (*A* 1938) Vice-Pres., ● Standard Furnace & Supply Co., 413-17 S. Tenth St., and 3115 Edw. Creighton Ave., Omaha, Nebr.

MATHIS, Julien W. (*A* 1921) ● New York Blower Co., 3145-55 Shields Ave., and 7929 Bishop St., Chicago, Ill.

MATHIS, Luther Norman (*A* 1948) L. N. Mathis Heating & Air Conditioning Co., 115 W. Thorain, San Antonio, Texas.

MATHISON, R. S. (*A* 1938) Weathermakers (Canada), Ltd., 735 Dovercourt Rd., Toronto 4, and ● 44 Strathgowan Ave., Toronto 12, Ont., Canada.

MATOUSEK, A. G. (*M* 1937) Mgr., Gamble Store, Schuyler, Nebr.

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MATTHEWS, John E. (*M* 1934) 2155 Sinden Ave., Knoxville, Tenn.

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MATTHEWS, R. R. (*M* 1944) Owner, ● Matthews Engineering Co., 2122 Olive, Dallas 1, and 3556 Rankin, Dallas 5, Texas.

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MATTSON, Roger K. (*J* 1945) Engr., McQuay, Inc., 1600 N.E. Broadway, Minneapolis, and ● 3611 Bryant S., Minneapolis 8, Minn.

MATZ, George N. (*M* 1938) Mech. Engr., A. Ernest D'Ambly, 2101 Architects Bldg., Philadelphia, and ● 649 Ferne Ave., Drexel Hill, Pa.

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MAWBY, Pensyl (*M* 1934) Dist. Mgr., Lehigh Navigation Coal Co., 123 S. Broad St., Philadelphia, and ● 15 E. Ridley Ave., Ridley Park, Pa.

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MAXWELL, William D. (*J* 1948) Designer-Mech., J. Donald Kroeker, Cons. Engr., 402 Failing Bldg., Portland 4, and ● 8947 Southeast 39th St., Portland 2, Ore.

MAY, Arthur O. (*A* 1938) Secy., ● Stannard Power Equipment Co., 53 W. Jackson Blvd., Room 925, Chicago 4, and 5736 N. Bernard St., Chicago 45, Ill.

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MAY, Edward M. (*M* 1931) Branch Mgr., Steel Products Engineering Co., 1601 S. Michigan Ave., Chicago, and ● 848 N. Ridgeland Ave., Oak Park, Ill.

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MAY, James W. (*M* 1938; *J* 1935) Dir. of Research, ● American Air Filter Co., 215 Central Ave., and 3908 Elfin Ave., Louisville, Ky.

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MAYCOCK, Ambrose A. (*M* 1947; *A* 1945) Mgr., ● A. A. Maycock Co., 234 Seventh Ave., Salt Lake City 8, Utah.

MAYCOCK, George E. (*A* 1945) Htg. and Vent. Engr., A. A. Maycock Co., 234 Seventh Ave., and ● 233 "E" St., Salt Lake City, Utah.

MAYER, William J. (*A* 1943) Field Service Engr., ● A. M. Byers Co., 10 E. Lexington St., Baltimore 2, and 1100 Edgemont Rd., Towson 4, Md.

MAYLARD, John B. (*A* 1943) Arch.-Engr., 1139 Morgan Ave., LaGrange Park, and ● 211 Custer St., Evanston, Ill.

MAYNARD, J. Earle (*M* 1931) Engr., U. S. Radiator Corp., 1500 United Artists Bldg., Detroit 31, and ● 2441 Kendall, Detroit 6, Mich.

MAYNE, Ivan E. (*A* 1945) Owner, • Consolidated Heating & Ventilating Co., 1709 W. Eighth St., Room 906, Los Angeles 14, and 1748 Rancho Real Rd., Temple City, Calif.

MAYNE, Walter L. (*M* 1938) Prod. Sales Engr., • Tanner Manufacturing Co., P. O. Box 860, 4201 Bell St., Lawrence Park, and 401 Beverly Dr., Erie, Pa.

MAYO, William P., Jr. (*A* 1947) Sales Engr., Thomas H. Sullivan & Co., 2626 S. Main St., and • 2218 Smith St., Houston, Texas.

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McBRIDE, J. Nevins (*A* 1941) Vice-Pres., • Frank A. McBride Co., 160 Ward St., Paterson 1, and 288 Derrom Ave., Paterson 4, N. J.

McBRIDE, Joseph A. (*J* 1943) Asst. Secy., • Frank A. McBride Co., 160 Ward St., Paterson 1, and 585 East 27th St., Paterson 4, N. J.

McCABE, John H. (*M* 1944) Dist. Mgr., • American Blower Corp., 1730 Glenarm St., Denver 2, and 567 S. York St., Denver 9, Colo.

McCAIN, H. King (*M* 1939; *A* 1938; *J* 1937) Cons. Engr., • Newcomb & Boyd, 615 Trust Company of Georgia Bldg., and 3619 Ivy Rd. N.E., Atlanta, Ga.

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McCALLUM, Chester E. (*M* 1946) Chief Engr., and Mgr., Htg. & Air Cond. Dept., Landingham Plumbing & Heating Co., 231 N. Trade St., Winston-Salem, N. C.

McCALMON, Robert T. (*A* 1946) Sales Engr., • A. M. Byers Co., 2544 West 28th Ave., Denver 11, and 1385 Holly, Denver 7, Colo.

McCANDLESS, Howard F. (*M* 1946; *A* 1945) Cons. Engr., First National Bank Bldg., P. O. Box 1669, Monterey, and • Rt. 1, Box 432, Aptos, Calif.

McCANN, Frank D. (*A* 1939) Dist. Repr., The Hertner Electric Co., 369 Lexington Ave., New York 17, and • 113 Chippewa Rd., Tuckahoe 7, N. Y.

McCANN, John L. (*A* 1945) Mgr., Plbg. and Htg. Dept., Harris Pump & Supply Co., Brady and Sidney Sts., Pittsburgh 3, and • 726 Lafferty Dr., Pittsburgh 10, Pa.

McCANN, Stanford C. (*A* 1944) Owner, • S. C. McCann Co., 1004 Baltimore, Kansas City 6, and 1002 W. Gregory Blvd., Kansas City 5, Mo.

McCARL, Harry E. (*M* 1944) Htg. and Vent. Engr., United States Rubber Co., 6600 E. Jefferson Ave., Detroit, and • 5774 Haverhill, Detroit 24, Mich.

McCARTHY, F. Wayne (*A* 1945) Branch Mgr., • Minneapolis-Honeywell Regulator Co., 1911 Ingersoll, and 1235–37th, Des Moines, Ia.

McCAUL, Lynn K. (*M* 1942) Sales Engr., The Coon-DeVisser Co., 2051 W. Lafayette, Detroit 16, and • 620 W. Woodland, Ferndale 20, Mich.

McCAULEY, Dale G. (*A* 1946) Pres., Lansing Heating-Ventilating Co., 1213 Center St., Lansing 6, Mich.

McCAULEY, James H. (*M* 1921) Pres., • J. H. McCauley & Son, 5620 West 65th St., Chicago, and 1123 Pleasant St., Oak Park, Ill.

McCLANAHAN, L. C. (*M* 1939) Dist. Mgr., • Aerofin Corp., 1121 Fidelity Bldg., Cleveland, and 29 Water St., Chagrin Falls, Ohio.

McCLEAN, Fred C. (*A* 1947) Pres., • Fred C. McClean Heating Supplies, Inc., 47 Park St., and 24 Clement St., Springfield, Mass.

McCLELLAN, James E. (*M* 1922) Vice-Pres., Mehring & Hanson Co., 162 N. Clinton St., Chicago, and 738 Marion St., Highland Park, Ill.

McCLINTOCK, Walter G. (*A* 1945) Dist. Mgr., • Reznor Manufacturing Co., P. O. Box 8, and 303 N. Main St., Milan, Tenn.

McCLINTOCK, William (*M* 1935) Mech. Engr., Kellex Corp., Woolworth Bldg., New York, and • 4116 Carpenter Ave., New York 66, N. Y.

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McCLUNG, K. R. (*A* 1946) Dept. Supvsr., • G. A. MacArthur Co., 2387 Hampden Ave., St. Paul 4, and R. 3, Como Station, St. Paul 8, Minn.

McCLUNG, Tom H. (*A* 1942; *J* 1939) Sales Engr., • Brod & McClung, 19 N.W. First Ave., Portland 9, and 2341 Northeast 61st Ave., Portland 13, Ore.

McCLURE, Charles J. R. (*A* 1947) Sales Engr., • The Trane Co., 2335 S. Grand Ave., St. Louis 4, and 839 Belt Ave., St. Louis 12, Mo.

McCONACHIE, L. L. (*M* 1943; *A* 1928) Owner, L. L. McConachie Co., 1003 Maryland, and • 1415 Harvard Rd., Grosse Pointe, Mich.

McCONNER, Charles R. (*A* 1925; *J* 1922) Gen. Sales Mgr., • Clarage Fan Co., Kalamazoo 16F, and 526 John St., Kalamazoo 44, Mich.

McCORMACK, Denis (*M* 1933) Cons. & Constr. Engr., Onions & Bouchard, Hamilton, and • Somerset Bridge, Bermuda.

McCORMICK, George W., Jr. (*A* 1941) Asst. Secy., • The National Association of Fan Manufacturers, 5-208 General Motors Bldg., Detroit 2, and 15836 Puritan Ave., Apt. D, Detroit, Mich.

McCOY, C. E. (*M* 1936) Partner, • Turner-McCoy, Fifth and Locust Sts., North Little Rock, and 3923 Oakwood Rd., Little Rock, Ark.

McCOY, Floyd F. (*A* 1946) Pres., • Floyd F. McCoy Heating Co., 303 S. Water St., and 401 Fitzhugh St., Bay City, Mich.

McCOY, Philip W. (*M* 1946) Asst. Chief Htg. Engr., • Bryant-McCoy Co., Box 65, Jamestown, and 96 West Fairmont, Lakewood, N. Y.

McCOY, Thomas F. (*Life Member; M* 1924) Mgr., • The Powers Regulator Co., 125 St. Botolph St., Boston 15, and 90 Church St., Weymouth Heights, Mass.

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McCREA, Lester W. (*M* 1940) Prop., • McCrea Sales Co., 15 East 21st St., Baltimore 18, and 1521 Pentridge Rd., Apt. 227, Baltimore 12, Md.

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McCULLOUGH, Goodall W. (*A* 1948) Sales Engr., Electronic Supply & Engineering Co., • 1014 McGowen St., and 6030 Floyd Dr., Houston, Texas.

McCULLOUGH, Henry G. (*M* 1936) Vice-Pres., S. S. Fretz, Jr., Inc., 1902 Chestnut St., Philadelphia 3, and • 7042 Lincoln Dr., Philadelphia 19, Pa.

McCULLOUGH, John L. (*M* 1939) Sales Engr., • English & Lauer, Inc., 1978 S. Los Angeles St., and 409½ S. Catalina St., Los Angeles 5, Calif.

McCUMBER, Burton R. (*M* 1945) Frozen Food Products, Inc., 600 W. Genesee St., Syracuse 4, and • 19 Leitch Ave., Skaneateles, N. Y.

McCUNE, Laban J. (*M* 1943) Engr. and Bldg. Mgr., • Clinic Foundation, 118 E. Sixth St., Tulsa 3, and 401 Springer Bldg., Tulsa, Okla.

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McDANIELS, James A. (*A* 1944) Air Cond., Allison Div., General Motors Corp., Speedway City, Indianapolis, and • 4950 Ford St., Speedway City, Indianapolis 8, Ind.

McDERMOTT, John P. (*A* 1942; *J* 1939) Mech. Engr., • The Trane Co., 308 Dekum Bldg., Portland 4, and 5425 S.E. Harold Ct., Portland, Ore.

McDONALD, Frank L. (*M* 1944) Branch Mgr., • Barber-Colman Co., 816 W. Fifth St., Los Angeles and 1655 Rose Ave., San Marino, Calif.

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McDONALD, John J. (*M* 1943) Pres., The McDonald Co., 43-47 Lansdowne St., Boston, and ● 401 Beacon St., Chestnut Hill 67, Mass.

McDONALD, Thomas (*A* 1931) Vice-Pres., Minneapolis-Honeywell Regulator Co., 2747 Fourth Ave. S., Minneapolis 8, Minn.

McDONNELL, Everett N. (*M* 1923), (Council, 1940-47) Pres., ● McDonnell & Miller, Inc., 400 N. Michigan Ave., and 219 Lake Shore Dr., Chicago 11, Ill.

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McFARLAN, A. I. (*M* 1942) Pres., ● A. I. McFarlan Co., Inc., 21 West St., New York 6, N. Y., and 691 Dorian Rd., Westfield, N. J.

McGARY, Robert O. (*M* 1946) Vice-Pres., Buensod-Stacey, Inc., P. O. Box 1755, and ● 2015 Dilworth Rd. E., Charlotte 3, N. C.

McGAVOCK, Edward A. (*J* 1947) Owner, Central Sales & Engineering Co., 1069 W. Jefferson St., and ● 303 N. Avon St., Rockford, Ill.

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McGEORGE, Richard H. (*M* 1937) Mgr., Htg. and Air Cond. Dept., McCord Radiator & Manufacturing Co., 2587 E. Grand Blvd., and ● 14565 Glastonbury Rd., Detroit, Mich.

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McGOVERN, Arthur F. (*A* 1945) Dist. Supvsr. and Engr., ● Modine Manufacturing Co., 83 S. High St., Columbus 15, and 362 S. Harding Rd., Columbus 9, Ohio.

McGOVERN, Tom R. (*A* 1947) Pres. & Gen. Mgr., ● The Baxter-Nafz Co., 6 W. North St., and 2208 Fountain Blvd., Springfield, Ohio.

McGOWN, Frederick H., Jr. (*A* 1947; *J* 1941; *S* 1939) Sales Engr., Northrup Supply Corp., 17 Prospect St., Oneonta, and ● 4 Pine Blvd., Cooperstown, N. Y.

McGRAIL, Thomas E. (*M* 1926) Local Repr., ● Canadian Sirocco Co., Ltd., 63 Sparks St., and 39 Thomas St., Carlington, Ottawa, Ont., Canada.

McGRATH, William L. (*M* 1945) Project Engr., Carrier Corp., Syracuse, and ● 113 Carlton Rd., Syracuse 4, N. Y.

McGREW, Joseph A. (*A* 1944) Owner, ● J. A. McGrew Supply Co., 2163 Market St., Denver 2, and 2380 Leyden St., Denver 7, Colo.

McGRUER, A. E. (*M* 1945) Elec. Engr., ● Canadian Pacific Railway Co., Room 244, Union Station, and 1954 Bloor St. W., Toronto, Ont., Canada.

McGUINNESS, C. H. (*A* 1943) Owner, ● Iowa Kol-Master Stokers, 205 Plymouth Bldg., Des Moines 9, and 663-49th St., Des Moines, Ia.

McGUIRE, James W. (*M* 1945) Owner, ● 370 Lexington Ave., New York, and 86-22 Dongan Ave., Elmhurst, N. Y.

McHUGH, James J. (*A* 1946) Sales Engr., ● Johns-Manville International Corp., 22 East 40th St., New York 16, and 18 Hampton Rd., Scarsdale, N. Y.

McILVAINE, John H. (*M* 1929) ● John H. McIlvaine, 1321 Arch St., Philadelphia 7, and 601 Pembroke Rd., Bryn Mawr, Pa.

McINDOE, James F. (*M* 1939) Mgr., Combustion Div., Enterprise Engine & Foundry Co., 600 Florida St., San Francisco 10, and ● 44 Santa Rosa Ave., Sausalito, Calif.

McINTIRE, James F.* (*Life Member; M* 1915; *A* 1914), (*Presidential Member*), (Pres., 1939; 1st Vice-Pres., 1938; 2nd Vice-Pres., 1937), (Council, 1926-28; 1932-40) Retired, Until May 1, 1948—The Billows Apts., Apt. 8, 16813 Gulf Blvd., St. Petersburg 6, Fla., and after May 1, 3261 Sherbourne Rd., Detroit 21, Mich.

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MOLLENBERG, Harold J. (*M* 1936) Pres., Mollenberg-Betz Machine Co., 22 Henry St., Buffalo, and • 111 Saratoga Rd., Snyder 21, N. Y.

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MONIER, Kurt A. J. (*A* 1946) Partner, • A. J. Monier & Co., 1446 N. Flores St., and 131 Ligustrum, San Antonio, Texas.

MONIES, Ellis A. (*M* 1944) Dist. Mgr., F. E. Myers & Brothers Co., Ashland, Ohio, and • 760 Ogden St., Denver, Colo.

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MONTESANO, Frank P. (*M* 1944) Mgr., The Frank A. McBride Co., 158-60 Ward St., and • 84 Lakeview Ave., Paterson, N. J.

MONTGOMERY, Cornelius T., Sr. (*M* 1947) Partner and Engr., Bowman and Montgomery Co., and R. D. 2, Bethlehem, Pa.

MONTGOMERY, Earl L. (*A* 1947) Sales Engr., • Sheldon's Ltd., 738 Notre Dame St. W., and 164 Decelles St., Ville St. Laurent, Montreal, Que., Canada.

MONTGOMERY, Edward G. (*A* 1938) Special Repr., Steel Company of Canada, Ltd., 525 Dominion St., Montreal, and • 20 Finchley Rd., Hampstead, Que., Canada.

MONTGOMERY, Foster W. (*A* 1948) Sales Engr., J. A. Walsh & Co., 3215 McKinney Ave., and • 1925 South Blvd., Houston 6, Texas.

MONTGOMERY, John Russell (*A* 1937) Mgr., Standards and Research, • Truscon Steel Co., Albert St., Youngstown 1, and 296 Granada Ave., Youngstown 4, Ohio.

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MOONEY, Mark E. (*A* 1945) Dir. of Sales, Applied Refrig., Carrier Corp., Syracuse, and • 125 Butternut Dr., DeWitt, N. Y.

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MOORE, Henry W. (*M* 1935) Mgr., Air Cond. Dept., Henry Niemes, Inc., 3242 Spring Grove Ave., Cincinnati 25, and • 3164 Queen City Ave., Cincinnati 11, Ohio.

MOORE, Herbert S. (*A* 1923) Dist. Repr., Iron Fireman Manufacturing Company of Canada, Ltd., 602 King St. W., Toronto 2, and • 107 Clendenan Ave., Toronto 9, Ont., Canada.

MOORE, H. Lee (*M* 1919), (Council, 1927-28) Repr., • Buffalo Forge Co., Buffalo Pumps, Inc., 345 Fourth Ave., Pittsburgh 22, and 7065 Flaccus Rd., Ben Avon, Pittsburgh 2, Pa.

MOORE, Joseph J. (*M* 1946) Field Engr., A. M. Byers Co., 1250 Sixth Ave., New York 20, N. Y., and • 90 York Sq., New Haven 11, Conn.

MOORE, MacDonell (*A* 1940) Pres. and Gen. Mgr., • The Moore Fuel Corp., 11 West St., Danbury, and R. D. 2, Bethel, Conn.

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MOREHOUSE, H. P. (*M* 1933) Gen. Htg. and Air Cond. Repr., Public Service Electric & Gas Co., 80 Park Pl., Newark, and • 30 Timber Acres Rd., Summit, N. J.

MOREHOUSE, J. Stanley (*M* 1938) Dean of Engrg., Prof. of Mech. Engr., • Villanova College, Villanova, and 102 Llandoff Rd., Upper Darby, Pa.

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MORGAN, Robert W. (*M* 1938) Chief Engr., Fedders-Quigan Corp., 57 Tonawanda St., Buffalo 7, and • 32 Windover, Hamburg, N. Y.

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MOSS, Alfred W. (*A* 1945; *J* 1943) Dept. Mgr., ● Walter Woods, Ltd., 782 Main St., and 268 Vale Ave., Winnipeg, Man., Canada.

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MULRONEY, George J. (*A* 1946) Branch Sales Office Mgr., ● C. A. Dunham Co., Ltd., 189 St. John St., and 137 Boulevard Laurier, Quebec, Que., Canada.

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MUNKELT, Frederick H. (*M* 1938) Vice-Pres., ● W. B. Connor Engineering Corp., 114 East 32nd St., New York 16, and 317 East 17th St., Brooklyn 26, N. Y.

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NEARINGBURG, Arthur (*A* 1938) Sales Engr., ● Sheldons, Ltd., 1221 Bay St., and 130 Floyd Ave., Toronto, Ont., Canada.

NEE, Raymond M. (*M* 1936) Sr. Power Engr., American Cyanamid Co., 30 Rockefeller Plaza, New York 20, and ● 949 Palmer Rd., Bronxville 8, N. Y.

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NEIMAN, Charles H., Jr. (*M* 1945) Chief Engr., York-Shipley, Inc., Jessop Pl. and P. R. R., and ● 330 W. Jackson St., York, Pa.

NELLIGANN, Gilbert (*A* 1948) Sales Engr., ● Fitzgibbons Boiler Co., 101 Park Ave., New York 17, and 126 East 30th St., New York 16, N. Y.

NELSON, Arthur N. (*M* 1947) Mech. Engr., Sessions Engineering Co., 1 N. La Salle St., Chicago 2, and ● 3832 N. Monticello Ave., Chicago, Ill.

NELSON, Arthur W.* (*M* 1944) Lt. Col., Engrg. Section, Hq. Far Eastern Air Forces, A. P. O. 925, San Francisco, Calif.

NELSON, Charles E. (*M* 1947) Sales Repr., ● Johnson Service Co., 28 East 29th St., New York, N. Y., and 34 Lum Ave., Chatham, N. J.

NELSON, Delmar W.* (*M* 1928) Prof., Mech. Engrg., ● University of Wisconsin, Mech. Engrg. Bldg., 1513 University Ave., Madison 6, and 3906 Council Crest, Madison, Wis.

NELSON, Franklin L. (*S* 1948) Student, David Ranken Jr. School of Mechanical Trades, St. Louis, Mo., and ● 1229 S. Paxton, Sioux City, Iowa.

NELSON, George O. (*M* 1923) Engr., Carstens Bros., Ackley, Iowa.

NELSON, Harold M. (*M* 1937) Pres., ● H. M. Nelson & Co., Inc., 1223 Connecticut Ave., Washington 6, D. C., and Falls Church, Va.

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NELSON, Roy O. (*M* 1938) Asst. Sales Mgr., Marsh Heating Equipment Co., 2120 Southport Ave., Chicago 14, and ● 5636 N. Bernard St., Chicago 45, Ill.

NELSON, Vernon E. (*A* 1945) Pres., ● General Corp., 3353 University Ave. S.E., and 5226–34th Ave. S., Minneapolis, Minn.

NELSON, Walter L. (*M* 1945; *A* 1944) Chief Mech. Engr., District Government, Washington 4, and ● 2225 Quincy St. N.E., Washington 18, D. C.

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NESBITT, Albert J.* (*M* 1921) Pres., ● John J. Nesbitt, Inc., State Rd. and Rhawn St., Holmesburg, Philadelphia 36, and Rockfield Farm, Tennis Ave. and Welsh Rd., Ambler, Pa.

NESMITH, Oliver E. (*A* 1936) Dir. of Engrg. and Research, Eureka Vacuum Cleaner Co., Bell & Hanna, and ● 107 Warner, Bloomington, Ill.

NESS, W. H. C. (*M* 1931) Pres., ● Master Fan Corp., 1323 Channing St., Los Angeles 21, and 215 N. Kingsley Dr., Los Angeles, Calif.

NESSELL, C. W. (*M* 1937) Acct. Exec., ● Minneapolis-Honeywell Regulator Co., 351 E. Ohio St., Chicago 11, and ● 303 Manawa Trail, Mt. Prospect, Ill.

NEST, Richard E. (*M* 1936) Chief Engr., General Oil Burner Co., 2300 Sinclair Lane, Baltimore 13, and ● 6000 Pinehurst Rd., Baltimore 12, Md.

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NEUBAUER, Edwin W. (*M* 1939) Engr., ● Campbell Norquist & Co., 1127 S.W. Morrison St., Portland 5, and 4804 N.E. Davis, Portland 15, Ore.

NEUMAN, Steven I. (*A* 1947) Sr. Tech. Engr., ● W. H. Brady and Co. Ltd., Churchgate St., Bombay, British India.

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NEWBANKS, Niles N. (*A* 1948) Skelgas Div., Skelly Oil Co., 4045 Troost, Kansas City, Mo., and ● 8202 Rose Ave., Overland Park, Kans.

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NIGHTINGALE, George F. (*A* 1946) Sales Engr., C. H. Bevington Co., 330 S. Wells St., Chicago, and ● 2136 Linneman St., Glenview, Ill.

NINMAN, Alex T. (*A* 1947) Sales, R. E. Chase & Co., 407 New Fliedner Bldg., Portland 5, and ● 4713 N. Willamette Blvd., Portland 3, Ore.

NITZBERG, Samuel H. (*A* 1947) Pres., ● Atlantic Pipe Bending & Fabricating Corp., 552 River Rd., Edgewater, and 168 E. Springvalley Ave., Maywood, N. J.

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NORMAN, George C. (*M* 1944) Engr., ● Koithan & Johnson, 27 Washington St., Newark 2, and 12 Exeter Rd., Short Hills, N. J.

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NORRIS, William P. (*M* 1944; *J* 1938) Engr., Baker Ice Machine Co., 813 Hempstead St., St. Louis 6, and 410 N. Newstead Ave., St. Louis 8, Mo.

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NORTH, Clarence P. (*M* 1942) Chief Engr., • Campbell Heating Co., P. O. Box 833, Des Moines 4, and 3614 E. Seventh St., Des Moines 16, Ia.

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NORTON, Ernest H. (*A* 1946) Owner, • 616 Lloyd Bldg., Seattle 1, and 5019 Phinney Ave., Seattle 3, Wash.

NORTON, John Arthur (*M* 1940) Mgr., Htg. Sales Div., Crane, Ltd., 306 Front St. W., Toronto, and • 136 Hanna Rd., Leaside, Ont., Canada.

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NOTTBERG, Gustav (*A* 1933) Vice-Pres., • U. S. Engineering Co., 914 Campbell, and 650 West 67th St., Kansas City, Mo.

NOTTBERG, Henry, Jr. (*A* 1946; *J* 1937) Secy., • U. S. Engineering Co., 914 Campbell, and 150 West 54th St., Kansas City, Mo.

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NOWITZKY, Herman S. (*A* 1931) Supt. Constr. Maint. and Repairs, Wilmer & Vincent Circuit, Fabian Theatres, 1501 Broadway, New York 18, N. Y., and • 821 Llewellyn Ave., Norfolk 7, Va.

NOYES, Richard R. (*A* 1946; *J* 1938) Field Engr., • Canadian Sirocco Co., Ltd., 630 Dorchester St. W., and 4940 Coronet, Apt. 2, Montreal, Que., Canada.

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NUNLIST, Frank J., Jr. (*M* 1943) Chief Engr., L. J. Mueller Furnace Co., 2005 W. Oklahoma Ave., Milwaukee 7, and • 8717 W. Cleveland Ave., Milwaukee, Wis.

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NUSBAUM, S. Richard (*A* 1944; *J* 1940) Mgr., • Pennsylvania Engineering Co., 1119-21 N. Howard St., Philadelphia, and Wynnewood Park Apts., Wynnewood, Pa.

NUSSBAUM, Otto J. (*A* 1944) Chief Research Engr., Kramer Trenton Co., Olden and Breunig Aves., Trenton 5, and • 56 McKinley Ave., Trenton 9, N. J.

NUTTING, Arthur* (*M* 1940) Chief Engr., • American Air Filter Co., 215 Central Ave., and 4040 Ormond Rd., Louisville, Ky.

NUTTING, Robert E. (*A* 1948) Supt., • Jaden Manufacturing Co. & Dutton-Lainson Co., Mfg. Div., 1601 W. Second St., and 418 E. Seventh St., Hastings, Nebr.

NYE, L. Bert, Jr. (*M* 1947; *A* 1943; *J* 1936) Staff Engr., Washington Gas Light Co., 1100 H St. N.W., Washington, D. C., and • McLean, Va.

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OAKLEY, LeRoy W. (*M* 1937) Owner, • L. W. Oakley Sales Co., 408 W. Clinch Ave., and 2003 Laurel Ave., Knoxville, Tenn.

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OBERG, H. C. (*A* 1933) Mgr., Engrg. Dept., Crane Co., Fifth and Broadway, and • 1362 W. Minnehaha St., St. Paul, Minn.

OBERLIN, James A. (*J* 1946) Distel Heating Co., Lansing, and • 221 N. Bostwick Ave., Charlotte, Mich.

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O'CONNELL, Thomas D'Arcy (*A* 1942) Pres., • Thomas O'Connell, Ltd., 1169 Ottawa St., Montreal 3, and 9 McCullough Ave., Outremont 8, Que., Canada.

O'CONNELL, Walter H. (*J* 1948) Jr. Engr., Lehigh Engineering Co., 1150 Mauch Chunk Rd., and • 81 West Goepp St., Bethlehem, Pa.

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O'DANIEL, Presley (*A* 1945) Branch Mgr., York Corp., 1807 Fidelity Bldg., Kansas City 6, and • 7139 Summit, Kansas City 5, Mo.

O'DONNELL, Lawrence D. (*A* 1944) Mgr., • McCarthy's Sheet Metal Works, Box 105, and 816 Buntin St., Vincennes, Ind.

O'DOWER, Hugh J. (*A* 1938) Owner, • O'Dower Engineering Co., 756 Board of Trade Bldg., Kansas City 6, and 6844 Locust, Kansas City 5, Mo.

OELGOETZ, J. F. (*M* 1938) Owner, J. F. Oelgoetz Co., 3365 N. High St., and • 279 E. North Broadway, Columbus, Ohio.

OFFEN, Ben (*M* 1928) Owner, • B. Offen & Co., 343 S. Dearborn St., and Sheridan Rd., Chicago, Ill.

OFFNER, Alfred J.* (*M* 1922), (*Presidential Member*), (Pres., 1946; 1st Vice-Pres., 1945; 2nd Vice-Pres., 1944; Treas., 1935-38), (Council, 1935-47) Cons. Engr., • 139 East 53rd St., New York 22, and 160-15-11th Ave., Beechurst, L. I., N. Y.

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OLDS, Dean (*M* 1944) Chief Engr., • The Coleman Co., Inc., 250 N. St. Francis, and 222 N. Bleckley, Wichita, Kans.

OLDS, Stephen T. (*A* 1945) Sales Mgr. and Engr., • Wm. C. Maunz Co., Inc., 383 E. Delavan Ave., Buffalo 14, and 400 Elmwood Ave., Buffalo, N. Y.

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OOSTEN, Louis S. (*A* 1944; *J* 1938) Asst. Chief Engr., • Bell & Gossett Co., 8200 N. Austin Ave., Morton Grove, and 725 Case St., Evanston, Ill.

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PIERPOINT, Harry Y. (*A* 1943) Owner, • J. A. Pierpoint, 3554 Appleton St. N.W., Washington 8, D. C.

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PINDELL, William R. (*A* 1947) Mgr., • Northwest Foundry & Furnace Co., 2345 S.E. Gladstone St., Portland 2, and 3739 N.W. Thurman St., Portland, Ore.

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ROEBUCK, William, Jr. (*M* 1917) Owner, • 220 Delaware Ave., Buffalo 2, and 1240 Delaware Ave., Buffalo, N. Y.

ROEDER, Winfield (*M* 1941) Branch Mgr., • American Blower Corp., 405 Temple St., and 484 Whitney Ave., New Haven, Conn.

ROFFEE, Lawrence W. (*A* 1947) Htg. & Vtg., Engr., • U. S. Bureau of Reclamation, Denver Federal Center Bldg., 1-B, and 435 Ogden St., Denver, Colo.

ROGERS, Charles S. (*A* 1940) Sales Engrg., • L. P. Steuart & Brothers, Inc., 138-12th St., N.E., and 1831 P St. S.E., Washington, D. C.

ROGERS, Walter M. (*A* 1947) Sales Engr., Thermal Products Co., 4501 Prospect Ave., Cleveland 3, and • Worton Blvd., Cleveland 21, Ohio.

ROHRABACHER, Warren E. (*J* 1946) Instructor, Mech. Engrg., Texas A. & M. College, College Station, Texas.

ROLAND, John (*M* 1944) Htg. Engr., • Conco Engineering Works, and 1104 Washington St., Mendota, Ill.

ROLL, Paul E. (*A* 1946) Branch Mgr., • Carrier Corp., 911 Electric Bldg., Houston 2, and 7505 Erath St., Houston 12, Texas.

ROMA, G. N. (*M* 1947) Estimator & Engr., Carlson Manufacturing Co., 50 E. Springfield Rd., Barberton, and • 964 Brittain Rd., Akron, Ohio.

ROMER, William H. (*A* 1945) Htg. Engr., • J. F. Higgins Heating Co., 509 Westminster St., Providence, and 124 Waverly St., Providence 7, R. I.

ROMPEL, Walter A. (*A* 1944) Refrigeration Engrg., P. O. Box 544, New Braunfels, Texas.

RONALD, Edward R. (*M* 1946) Partner, Warren & Ronald, 1705 Heyburn Bldg., Louisville 2, and • 554 Sunnyside Dr., Louisville 6, Ky.

ROOSE, Robert W.* (*J* 1946) Research Asst. in Mech. Engrg., 102 Mech. Engrg. Lab., University of Illinois, Urbana, and • 54 E. Grogory Dr., Champaign, Ill.

ROOT, Edwin B. (*M* 1936) Chief Engr. and Asst. Gen. Mgr., Jackson & Church Co., Furnace Div., and • 132 Wylie Ct., Saginaw, Mich.

ROSE, Harold J. (*M* 1938) Vice-Pres. and Dir. of Research, • Bituminous Coal Research, Inc., 912 Oliver Bldg., Pittsburgh 22, and 219 Lytton Ave., Pittsburgh 13, Pa.

ROSE, Howard J. (*M* 1934) Sales Co., Inc., 26 West 47th St., New York, and • 100 Norman Rd., New Rochelle, N. Y.

ROSE, James S. (*A* 1945) Branch Mgr., • Ilg Electric Ventilating Co., 55 New Montgomery St., San Francisco 5, and 41 Ethel Ave., Mill Valley, Calif.

ROSE, Jerome C. (*M* 1937) Air Cond. Engr., Buensod-Stacey, Inc., 60 East 42nd St., and • 80-31 213th St., Queens Village 8, N. Y.

ROSEBROUGH, J. Stoddard (*M* 1943; *A* 1937) 1014 Arcade Bldg., St. Louis 1, and 218 Parkhurst Terrace, Webster Groves 19, Mo.

ROSEBROUGH, Robert M. (*M* 1920) Central Dist. Mgr., • L. J. Mueller Furnace Co., 1012 Arcade Bldg., St. Louis 1, and 34 Hardith Hill Ct., Rockhill, St. Louis 19, Mo.

ROSEBY, Thomas A. (*M* 1939) Asst. Gen. Mgr., • Carrier Air Conditioning, Ltd., 36 Bourke St., and 4 Fernhurst Ave., Cremorne, Sydney, N. S. W., Australia.

ROSELL, Axel F. (*M* 1935) Cons. Mech. Engr., • Axlander & Rosell Konstruktionsbyra AB, Grevgatan 49, Stockholm, and Fafnervagen 12, Djursholm, Sweden.

ROSEN Edmond J. (*A* 1939) Tech. Engr., Merill N. Musgrave & Co., 2019 Third Ave., Seattle 1, and • 10238-18th Ave. S.W., Seattle 66, Wash.

ROSENBERG, Philip (*A* 1928) Vice-Pres. and Treas., Universal Steel Equipment Corp., 135 West 23rd St., and • Hotel Hamilton, 141 West 73rd St., New York, N. Y.

ROSENBLATT, Arthur M. (*M* 1938) Pres., • Rosenblatt & Kerstein, Inc., 923 Virginia St. E., P. O. Box 33, and 1250 Edgewood Dr., Charleston, W. Va.

ROSENSTEIN, David L. (*S* 1948) Student, University of Minnesota, and 316 17th Ave. S.E., Minneapolis, Minn.

ROSER, Edward, III (*A* 1944; *J* 1943) Air Cond. and Refrig. Engr., U. S. Engineers, Ft. Leavenworth, and • 318 North 20th St., Leavenworth, Kans.

ROSS, Burton W. (*A* 1947) Sales Engr., • South African General Electric Co., 30 Chiappini St., and De Waal Rd., Fish Hoek, Cape Town, South Africa.

ROSS, David S. (*J* 1943; *S* 1941) Vice-Pres., Sam Ross & Sons, 846 Broadway, Lorain, Ohio.

ROSS, Earl F. (*M* 1944) Chief Mech. Engr., W. C. Kruger & Co., Archts.-Engrs., Sena Plaza, P. O. Box 308, and • 315 Tesuque Dr., Santa Fe, N. M.

ROSS, J. D. (*A* 1937) Mgr., Htg. and Refrig. Div., • Railway & Engineering Specialties, Ltd., 5754 Western Ave., Montreal 28, and 88 Percival Ave., Montreal, W., Que., Canada.

ROSS, John H. (*M* 1946) Cons. Engr., • 102 Charles St. W., Toronto 5, and 438A Jane St., Toronto 9, Ont., Canada.

ROSS, John O.* (*M* 1920) Pres., • Ross Industries Corp., 350 Madison Ave., New York 17, and 3 East 69th St., New York 21, N. Y.

ROSS, Kenneth A. (*A* 1944) Chief Engr., Kitsilano High & Jr. High Schools, Vancouver School Board, 590 Hamilton St., and • 3204 West 13th, Vancouver, B. C., Canada.

ROSS, Morwick (*A* 1946; *J* 1945) 3234 Wellington Rd., Parkfairfax, Alexandria, Va.

ROSS, Roderick (*M* 1937) Sr. Partner, • Roderick Ross & Traill, Cons. Engrs., 4 St. James' Bldg., 123 William St., Melbourne C1, and 5 Burns St., Elwood, Melbourne, S 3, Australia.

ROSS, Sidney S. (*A* 1945) Owner, Air Cond.-Sheet Metal, 193 Bridge St., Brooklyn 1, and • 39-41-50th St., Woodside, N. Y.

ROSSITER, Irvin J. (*A* 1939) Field Engr., • American Blower Corp., 231 W. Wisconsin, Milwaukee 3, and 4517 N. Marlborough, Milwaukee 11, Wis.

ROTH, Charles F. (*A* 1930) Pres., • International Exposition Co., Grand Central Palace, 480 Lexington Ave., New York 17, and 141 East 36th St., New York, N. Y.

ROTH, Harold R. (*M* 1935), (Council, 1945-47) Dist. Mgr., • Canadian Sirocco Co., Ltd., 57 Bloor St. W., and 5 Castleview, Toronto, Ont., Canada.

ROTH, Herman P. (*M* 1945) Research Assoc. in Medicine, University of Southern California, School of Medicine, Los Angeles 7, and • 2000 Agnes Rd., Manhattan Beach, Calif.

ROTH, John L. (*M* 1946) In Charge—Comml. Activities, • General Electric Co., 1602 S. Hanna St., and 827 Kinnaird, Ft. Wayne, Ind.

ROTHENBACH, Walter J. (*A* 1946) Sales Engr., • John J. Nesbitt, Inc., 11 Park Pl., New York 7, N. Y., and 306 N. Bellevue Ave., Langhorne, Pa.

ROTHMANN, S. Charles* (*M* 1936) Indus. Hygiene Engrg. Consultant, Div. of Labor Standards, Room 6312, Labor Dept. Bldg., 14th & Constitution Ave., Washington 25, and • Apt. 208-25, Kennedy St. N.W., Washington, D. C.

ROTHROCK, Ralph K. (*A* 1944) Owner, 5316 Dryades St., New Orleans 15, La.

ROTTMAN, George B. (*M* 1944) Engr., • W. H. Sullivan Co., Inc., 313½ S. Greene St., and 401 S. Chapman St., Greensboro, N. C.

ROTTMANN, Paul O. (*M* 1948) Paul O. Rottmann, Cons. Engr., • 204 Hunter Bldg., and 456 Albany Ave., Shreveport, La.

ROTTMAYER, S. I. (*A* 1933; *J* 1928) Mech. Engr., • Samuel R. Lewis & Assocs., 100 W. Monroe St., Chicago 3, and 309 S. Oak Park Ave., Oak Park, Ill.

ROTZ, J. M. (*M* 1944) Owner, • J. M. Rotz Engineering Co., 804 Merchant's Bank, Indianapolis 4, and R. R. 16, Box 449, Indianapolis 44, Ind.

ROUSE, R. K. (*M* 1948) Owner, • R. K. Rouse, Sales Engr., Suite 1, 228 N. Main St., and 306 E. Faris Rd., Greenville, S. C.

ROUSH, Benjamin B. (*A* 1946) Mech. Engr., National Distillers Products Corp., and • Rt. 9, Frankfort, Ky.

ROWE, William A.* (*Life Member*; *M* 1921), (Council 1929-31) 718 Longfellow Ave., Detroit 2, Mich.

ROWE, William M. (*M* 1946; *A* 1944; *J* 1936) Field Engr., • American Blower Corp., 1302 Swetland Bldg., Cleveland 15, and 151 Bradley Ave., Chagrin Falls, Ohio.

ROWLEY, Frank B.* (*M* 1918), (*Presidential Member*), (Pres., 1932; 1st Vice-Pres., 1931; 2nd Vice-Pres., 1930; Council, 1927-33) Prof., University of Minnesota, Minneapolis, and • Excelsior, Minn.

ROY, Ernest W. (*M* 1945) Prcs., • Roy Equipment Co., Inc., 311 W. Church Ave., and 4638 Chambliss Ave., Knoxville, Tenn.

ROY, Raul (*A* 1945) Sales Engr., • Sarco Canada, Ltd., 496 Church St., and 105 Merrell E., Toronto, Ont., Canada.

ROYCE, Robert F. (*J* 1946; *S* 1945) Berrien Co., Lakeside, Mich.

RUBEL, Harry L. (*A* 1943) Pres., • Rubel & Jensen Co., 646 Central Ave., and 33 S. Munn Ave., East Orange, N. J.

RUBIN, Louis (*A* 1944) Co-Owner, • Hudson Heating Co., 11350 Schaefer Highway, Detroit 27, and 2917 Leslie, Detroit 6, Mich.

RUBIN, Saul (*J* 1947) Scientific Engr., Joy Manufacturing Co., La-Del Div., and • 214 Cedar Lane, N.W., New Philadelphia, Ohio.

RUCHTE, Carl O. (*A* 1943) Architectural Examiner, Federal Housing Administration, 12th Floor, W. O. W. Bldg., Omaha 2, and • 5035 Bedford Ave., Omaha 4, Nebr.

RUDBERG, John A. (*J* 1948) Ellerbe and Co., Archts. & Engrs., 1st National Bank Bldg., and • 2611 Upton N., Minneapolis, Minn.

RUDD, Dann J. (*M* 1937) Asst. Mech. Engr., New York City Board of Education, 49 Flatbush Ave., Ext., Brooklyn, and • 580 Deer Park Ave., Babylon, L. I., N. Y.

RUDIO, H. M. (*M* 1921) Engr., Buensod-Stacey, Inc., 60 East 42nd St., New York, N. Y. and • 317 Grier Ave., Elizabeth, N. J.

RUDLOFF, Charles S. (*J* 1948; *S* 1947) Sales Engr., • A. M. Lockett & Co., Ltd., National Standards Bldg., Houston, and 2910 Bagby St., Houston 6, Texas.

RUDOLPH, R. R. (*M* 1943) Principal, • General Exporting & Importing Co., 723 Central Bldg., Seattle 4, and 2300 North 38th St., Seattle, Wash.

RUEMMELE, Albert M. (*A* 1943; *J* 1938) Major, S-4 Section, Hq. School Troops, Fort Knox, Ky.

RUFF, Adolph G. (*M* 1935) Supt. of Power, U. S. Playing Card Co., Park Ave., Norwood, and • 3824 Woodford Rd., Cincinnati, Ohio.

RUFF, Alonzo W. (*M* 1944) Mech. Engr., • V. C. Patterson & Assocs., 415 W. Market St., and 538 W. Springettesbury Ave., York, Pa.

RUFF, DeWitt C. (*M* 1922) Treas., • Healy-Ruff Co., 2255 University Ave., St. Paul 4, and 2211 St. Clair Ave., St. Paul 5, Minn.

RUGART, Karl (*A* 1924) Mfrs., Repr., • 26 South 20th St., Philadelphia 3, and 612 Bryn Mawr Ave., Penn Valley, Narberth P. O., Pa.

RUGG, Henry H. (*A* 1947) Sales Repr., • The Wm. Powell Co., 703 Ashland Ave., St. Paul 5, and R. R. No. 9, Mahtomedi, Minn.

RUGGLES, Robert F. (*M* 1936) Partner, Ruggles & Loughran, 50 Church St., New York 7, and • 15 Gregg Pl., Randall Manor Staten Island 1, N. Y.

RUMBOLD, Allan H. (*M* 1941) Pres., • Rumbold & Co., Inc., 379-381 Nelson St. S.W., Atlanta, and R. F. D. 1, Norcross, Ga.

RUMMEL, Adolph J.* (*M* 1937) Partner, • Langhammer-Rummel Co., 436 Main Ave., and 235 North Dr., San Antonio, Texas.

RUMSEY, John L. (*M* 1941) Chief Engr., • Macnsons, 151 Tehama St., San Francisco 6, and Box 1025, Belvedere, Marin Co., Calif.

RUNGE, Edwin A. (*A* 1944) Chief Engr., Lee Engineering Co., Union National Bank Bldg., Youngstown, and • 429 Maplewood Ave., Struthers, Ohio.

RUNGE, Nathan P. (*M* 1945) Sales Engr., • Garden City Fan Co., 332 S. Michigan Ave., Chicago 4, and 346 Greenleaf Ave., Wilmette, Ill.

RUNNINGS, Henry M. (*M* 1943) Regis. Mech. Engr., 16261 Griggs Ave., Detroit 21, Mich.

RUPERT, J. Daniel (*A* 1947) Engr., • Miller Davis Plbg. & Htg. Co., 2211 Miller Rd., Kalamazoo, Mich.

RUPP, Chester J. (*S* 1947) Student, Michigan State College, East Lansing, and • 720 W. Ottawa St., Lansing, Mich.

RUSH, Merle K. (*M* 1946) Sales Engr., Hucker Sales Co., 1700 Walnut St., Philadelphia 3, and • 520 Twin Oaks Dr., Wynnewood, Pa.

RUSSELL, Boyd A. (*A* 1941) 318 Long Branch Pkwy., Takoma Park, Md.

RUSSELL, Edgar N. (*M* 1947) Dir. & Tech. Engr., • Rosser & Russell, Ltd., 30 Conduit St., London W. 1, and "Merok," Camp Rd., Gerrards Cross, Buckinghamshire, England.

RUSSELL, Harold E. (*M* 1947) Supvsr., • Comml. & Indus. Htg. & Air Cond. Div., Cincinnati Gas & Electric Co., 4th & Main Sts., Box 960, and 3315 Hewitt Crescent, Cincinnati, Ohio.

RUSSELL, James R. (*A* 1945) Constr. Engr., Standard Chemical Co., 195 Fleet St. E., and • 45 DeVere Gardens, Toronto, Ont., Canada.

RUSSELL, Joseph Nelson (*Life Member*; *M* 1899) Rosser & Russell, Ltd., 30 Conduit St., London W. 1, and • St. Elmo Marsham Way, Gerrards Cross, Bucks, England.

RUSSELL, W. A. (*M* 1943) Chief Engr. and Sales Mgr., Skinner Heating & Ventilating Co., Inc., 1948 N. Ninth St., St. Louis 6, and • 7918 Kingsbury Blvd., Clayton 5, Mo.

RUSSELL, William B. (*M* 1944) Vice-Pres., • Kewanee Boiler Corp., and 409 E. Prospect, Kewanee, Ill.

RUTH, Robert J. (*J* 1946) Sales Engr., American Blower Corp., 402 Essex Bldg., 84 S. Tenth St., Minneapolis, and • 4431 Zenith Ave. N., Robbinsdale, Minn.

RUUD, Robert E. (*A* 1947) Mech. Engr., • F. J. & W. J. Spriggs, 160 W. Fourth St., St. Paul 2, and 1360 Stanford, St. Paul 5, Minn.

RYAN, Frank J. (*A* 1946) Mgr. and Supvsr., • William D. Ryan, Plumbing & Heating, P. O. Box 5148E, 126 Duckworth St., and 1 Carpasian Rd., St. John's, Newfoundland.

RYAN, Harold J. (*M* 1940) Pres., • Harold J. Ryan, Inc., 101 Park Ave., New York 17, and Poquott Village, East Setauket, L. I., N. Y.

RYAN, Joseph B. (*M* 1938) Engr., • 526 Railway Exchange Bldg., and 3860 Charlotte Ave., Kansas City, Mo.

RYAN, Key W. (*J* 1947; *S* 1946) Supvsr. Sales & Serv., South Wind Home Heater, Stewart-Warner Corp., South Wind Div., 1514 Drover St., Indianapolis 7, and • 4015 N. Kenwood Ave., Indianapolis 8, Ind.

RYAN, William F. (*M* 1940; *A* 1939; *J* 1933) Chief Engr., The Salina Supply Co., 302-304 N. Santa Fe, and • 310 W. Republic, Salina, Kans.

RYBOLT, Arthur L. (*A* 1938) Gen. Mgr., • The Rybolt Heater Co., Miller St., and 1108 Center St., Ashland, Ohio.

RYDBERG, John A. (*M* 1946) Dr. Tech., • Kungl. Tekniska Hogskolan, and c/o John Ericssonsgatan 15, Stockholm, Sweden.

RYDEN, Eric H. (*M* 1946) Dvlpt. Engr., The C. A. Olsen Manufacturing Co., and • 117 Glenwood St., Elyria, Ohio.

RYDEN, R. S. (*A* 1946) Owner, • R. S. Ryden & Co., 403 Insurance Bldg., and R. 2, Box 208R, San Antonio, Texas.

RYERSON, Herbert E. (*M* 1937) Dist. Mgr., Cardox Corp., 520 Park Bldg., Pittsburgh 22, Pa.

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SAAR, Laird F. (*A* 1945) Owner, Saar Heating & Engineering Co., 206½ W. Yakima Ave., Yakima, Wash.

SABIN, Edward R. (*M* 1919) Pres., • E. R. Sabin & Co., 4710 Market St., Philadelphia, Pa., and 205 Page Ave., Allenhurst, N. J.

SABLE, Edward J. (*M* 1939) Vice-Pres. and Treas., • The T. O. Murphy Co., 25-27 E. College St., and 246 W. Lorain St., Oberlin, Ohio.

SACHS, Sam (*A* 1948; *J* 1940) Mech. Engr., Constr. & Equip. Dept., Montgomery Ward & Co., 619 W. Chicago Ave., Chicago, and • 1642 W. Pratt Blvd., Chicago 26, Ill.

SACK, Herman S. (*A* 1944) Archt. and Engr., Waldorf System, Inc., 169 High St., Boston, and • 29 Kodaya Rd., Waban 68, Mass.

SADLER, C. Boone (*M* 1928) Civil Engr., Public Works Office, 11th Naval Dist., San Diego, and • 3211 S. Giebe Rd., Arlington, Va.

SAENGER, Lester W. (*A* 1947; *J* 1941) Maint. Engr., National Bearing Div., American Brake Shoe Co., 4930 Manchester Ave., St. Louis 10, and • 21 Hillard Rd., Glendale 22, Mo.

SAGAR, Paul B. (*A* 1945) Dvlpt. Engr., Norman Products Co., 1150 Chesapeake Ave., Columbus, and • 3957 Riveredge Rd., Cleveland 11, Ohio.

SAGINOR, S. V. (*M* 1939) Gen. Mgr., Davey Compressor Co., 266 N. Water St., and ● 900 Bryce Rd., Kent, Ohio.

SAHAB, Mohamed S. (*S* 1946) Grad. Student, Cornell University, Ithaca, and ● 105 Park St., Groton, N. Y.

SAIN, Kenneth L. (*J* 1947) Field Engr., U. S. Air Conditioning Corp., 342 Oklahoma Natural Bldg., Oklahoma City, and ● 2203 Dorchester Dr., Oklahoma City 6, Okla.

SALAUN, Harold L. (*A* 1946) Comml. Supvsr., ● New Orleans Public Service, Inc., 317 Baronne St., and 5843 Vicksburg St., New Orleans, La.

SALE, Francis B. (*A* 1939) Sales Engr., Preferred Utilities Manufacturing Corp., 1860 Broadway, New York 23, and ● 1 Ascan Ave., Forest Hills, N. Y.

SALE, G. N. (*A* 1946) Mgr., Process Service, ● Dominion Oxygen Co., Ltd., 159 Bay St., and 406 Armadale St., Toronto, Ont., Canada.

SALEH, Mohamed (*A* 1947) Gen. Mgr., ● Universal Engineering & Trading Co., Inc., P. O. Box 26, Faggala, Cairo, and Sohag, Egypt.

SALEVA, Gustavo (*A* 1945) Pres., ● Electrica-Commercial, Inc., Apartado 3751, San Juan, and Calle Taft 55, Santurce, Puerto Rico.

SALINGER, Robert J. (*M* 1945) Mech. Engr., Reg. F. Taylor, Cons. Engr., 910 Bankers Mortgage Bldg., Houston 2, and ● 4510 Dewberry Lane, Houston 4, Texas.

SALTER, Stanton W. (*M* 1942) Vice-Pres., Engineering Equipment Co., Ltd., 620 Cathcart St., Montreal, and ● 153 Hillcrest Ave., Montreal, W., Que., Canada.

SALTER, Thomas J., Jr. (*A* 1947) Asst. Engr., Sierra Pacific Power Co., 21 E. First St., and ● 244 Hill St., Reno, Nev.

SALZER, Alfred R., Jr. (*A* 1947; *J* 1940) Cons. Mech. Engr., ● 1026 Bienville St., New Orleans 16, and 3363 DeSaix Blvd., New Orleans, La.

SAMPSON, Will D. (*M* 1945) Dist. Mgr., ● B. F. Sturtevant Co., Div. of Westinghouse Electric, 1608 Canton Ave., and 4327 Taos Rd., Dallas, Texas.

SAMUELS, Sidney (*M* 1941; *A* 1928; *J* 1925) Pres., ● Sidney Samuels, Inc., 165 Amsterdam Ave., New York 23, and 245 West 107th St., New York 25, N. Y.

SANBERN, E. N.* (*M* 1923) Asst. Secy. and Mgr., Jobbed Products Div., Hoffman Specialty Co., Inc., 1001 York St., Indianapolis 7, and ● 4025 Park Ave., Indianapolis 5, Ind.

SANDBERG, Julian A. (*A* 1946) Estimator, Trane Co., 850 Cromwell Ave., St. Paul 4, and ● 757 Delaware Ave., St. Paul 7, Minn.

SANDER, Andy J. (*M* 1941) Chief Engr., c/o A. Epstein, 2001 W. Pershing Rd., and ● 2457 East 74th St., Chicago 49, Ill.

SANDERS, Charles M., Jr. (*A* 1946; *J* 1938) Specialty Sales, ● Minneapolis-Honeywell Regulator Co., 2753 Fourth Ave. S., Minneapolis 8, and Bayers Grove, Excelsior, Minn.

SANDERS, George O. (*A* 1945) Branch Mgr., ● Penn Electric Switch Co., 7310 Grand River Ave., Detroit 4, and 19484 Prest Ave., Detroit 19, Mich.

SANDERS, Vic (*A* 1945) Equip. Engr., Pittsburgh Corning Corp., 632 Duquesne Way, Pittsburgh 22, and ● 230 Glenrock Dr., Bridgeville, Pa.

SANDERS, William L. (*A* 1945) Partner, ● Midwest Plumbing & Heating Co., 6243 Prospect, Kansas City, and 103rd Blueridge, R. R. 1, Hickman Mills, Mo.

SANDERS, William R. (*M* 1946) Vice-Pres. & Secy., Mag-Bestos Co., Box 365, and ● R. F. D. 3, Johnson City, Tenn.

SANDFORT, John F. (*M* 1942; *J* 1938) Asst. Prof., Mech. Engrg. Dept., ● Iowa State College, and 411 Eighth St., Ames, Ia.

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SANFORD, A. L. (*M* 1915) Mech. Engr., C. H. Johnston, Archts. & Engrs., 715 Empire Bank Bldg., St. Paul 1, and ● 1037 Davern St., St. Paul 5, Minn.

SANFORD, Edward H. (*J* 1948; *S* 1947) Design Engr., The Texas Co., P. O. Box 712, and ● 3434 Eighth St., Port Arthur, Texas.

SANFORD, Ellwood C. (*M* 1947) Engr., Fred W. Kolb, 681 Market St., San Francisco, and ● Box 222A, Route 2, Martinez, Calif.

SANFORD, Harold L. (*A* 1945) Owner, Pres., ● Sans Corp., 132 Blackstone Ave., and 69 Townline Rd., R. D. 4, Jamestown, N. Y.

SANFORD, Sterling S.* (*M* 1930) Htg., Vtg. and Air Cond. Engr., ● The Detroit Edison Co., 2000 Second Ave., Detroit 26, and 279 Hillcrest Rd., Grosse Pointe Farms 30, Mich.

SANGER, Ernest (*A* 1944) Mfrs. Agent, Watts Regulator Co., and ● 1045 Wayburn Ave., Detroit 30, Mich.

SANTAGOSTINO, Mario (*M* 1947) Tech. Mgr., ● c/o Ditta Giacomo Jucker, Via Mauro Macchi, 28, and Via Privata Arpesani 4, Milano, Italy.

SAPP, Charles L. (*M* 1945; *A* 1936) Secy.-Mgr., Farquhar Furnace Co., 150 Owens Ave., and ● 620 N. Walnut St., Wilmington, Ohio.

SARKAR, S. R. (*M* 1946) Chief Engr., Trane Air Conditioning Dept., ● Keymer Bagshawe & Co., Ltd., 22 Strand Rd., P. B. 399 Calcutta and Jamirtta P. O., Dist: Dacca, Bengal, India.

SATTERLEE, Harry A. (*M* 1947; *A* 1944; *J* 1940) Partner, ● The Schulte Plumbing & Heating Co., 215-21 W. Tenth St., and 1006 N. Sergeant, Joplin, Mo.

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SAUNDERS, Claude V. (*M* 1946) Mech. Engr., L. C. Kingscott & Assoc., Inc., P. O. Box 671, Kalamazoo 99, and ● 906 Hazard Ave., Kalamazoo 19, Mich.

SAUNDERS, Douglas G. (*A* 1943) Estimator and Supvsr., ● John Plaxton Co., Ltd., 244 Main St., and 696 Warsaw Ave., Winnipeg, Man., Canada.

SAUNDERS, L. P. (*M* 1933), (Treas. 1944-45; Council, 1941-47) Chief Engr., Research Engrg., ● Harrison Radiator Div., General Motors Corp., and Tuscarora Club, Lockport, N. Y.

SAUNDERS, M. G., Jr. (*A* 1946) Prod. Mgr., ● The Bahnson Co., 1001 S. Marshall St., Winston-Salem, and 2414 Buena Vista Rd., Winston-Salem 5, N. C.

SAUNDERS, M. Kerby (*A* 1945) Pres., ● Kerby Saunders, Inc., 630 West 52nd St., New York 19, and 1136 Fifth Ave., New York, N. Y.

SAUNDERS, Sidney George (*M* 1944) Dir.-Chief Engr., Earleymil, Ltd., 212A, Shaftsbury Ave., London, W.C. 2, and ● 113 Winkworth Rd., Banstead, Surrey, England.

SAURWEIN, G. K. (*M* 1938) Mech. Engr., ● New England Gas & Electric System, 729 Massachusetts Ave., Cambridge, and 639 Boston Post Rd., Weston, Mass.

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SCHAAD, Fred N. (*M* 1944) Dist. Repr., • Warren Webster & Co., Westport Bank Bldg., Westport and Broadway, Kansas City 2, and 408 West 61st St., Kansas City 4, Mo.

SCHAAR, Martin (*A* 1947) Owner, • Wisconsin Furnace Co., 1310 W. Walnut St., Milwaukee 5, and 3272 North 45th St., Milwaukee, Wis.

SCHAARSCHMIDT, Karl F. (*A* 1945) Partner, The Burns Heating Co., 1042 Holden Ave., Detroit 2, and • 5121 W. Chicago Blvd., Detroit 4, Mich.

SCHAD, Clifford A. (*A* 1938; *J* 1937) Engrg. Dept., United States Air Conditioning Corp., Como Ave. S.E., at 33rd, Minneapolis 14, and • 4425-43rd Ave. S., Minneapolis, Minn.

SCHAEFER, Armand (*A* 1945) Dist. Mgr., Iron Fireman Manufacturing Co., 429 S. Ashland Ave., and • 1429 Farragut, Chicago, Ill.

SCHAFER, Harry C. (*M* 1937) Sales Mgr., Iroquois Gas Corp., 45 Church St., Buffalo, and • 197 Union St., Hamburg, N. Y.

SCHAMPEL, Howard B. (*A* 1943) Design Engr., Minnesota Mining & Manufacturing Co., 900 Fauquier Ave., and • 2122 Knapp St., St. Paul 8, Minn.

SCHARMER, George A. (*A* 1945) Pres., New Milford Construction & Repair Co., Inc., 206 River Rd., and • 182 Cleveland St., New Milford, N. J.

SCHARRES, John W. (*A* 1946) Designing Engr., E. R. Gritschke, Cons. Engr., 125 W. Madison St., Chicago 2, and • 5448 Princeton Ave., Chicago 9, Ill.

SCHAUER, Robert A. (*A* 1944; *J* 1942) Chief Htg. & Air Cond. Engr., • J. C. Penney Corp., Constr. Dept., 330 West 34th St., New York 1, N. Y., and 2534 Eighth Walk, Jackson Heights, N. Y.

SCHECHTER, Jack E. (*A* 1941; *J* 1937) Chief Engr., James H. Martin, Inc., 503 West 43rd St., New York 18, and • 28 Brower Ave., Woodmere, L. I., N. Y.

SCHEIDECKER, Daniel B. (*A* 1919) Pres., • Hunter-Clark Ventilating System Co., 2800 Cottage Grove Ave., Chicago 16, and 4626 N. Kilbourn Ave., Chicago 30, Ill.

SCHENCK, William P. (*M* 1947) Engr., • Petrol Corp., 2012 Chestnut St., Philadelphia 3, Pa.

SCHERGER, Fred J. (*A* 1942) Sales Engr., • Mundet Cork Corp., 14401 Prairie, Detroit 21, and 3754 Kipling, Berkley, Mich.

SCHERNBECK, Fred H. (*A* 1930) • William Brothers Boiler & Manufacturing Co., 1057 Tenth Ave. S.E., and 5045 Portland Ave., Minneapolis, Minn.

SCHERRER, James R., Jr. (*A* 1946) Chief Engr., • Security Manufacturing Co., 1630 Oakland Ave., Kansas City 3, and 3808 East 62nd St., Kansas City 4, Mo.

SCHICK, Karl W. (*A* 1946) Southwest Regional Mgr., • Minneapolis-Honeywell Regulator Co., 2507 Commerce St., Dallas 1, and 6216 Winton, Dallas, Texas.

SCHILKEN, Donald R. (*A* 1947) Sales Mgr., Alexander-Stafford Corp., 1 Iona Ave. N.W., and • 914 Franklin St. S.E., Grand Rapids, Mich.

SCHIMPKE, Burton J. (*S* 1947) Engr., • Centri-Spray Corp., 14290 Meyers Rd., Detroit 27, and 28050 Goldengate Dr., Birmingham, Mich.

SCHIWETZ, D. P. (*M* 1945) Branch Mgr., • York Corp., Box 1007, Charlotte 1, and 825 Romany Rd., Charlotte 3, N. C.

SCHLENK, Hugo, Jr. (*M* 1945) Engrg. Dept., • The Northwest Paper Co., and 214 Chestnut St., Cloquet, Minn.

SCHLENTNER, Karl O. (*M* 1948) Asst. Mgr. of Research, • The National Radiator Co., 221 Central Ave., and 1155 Edson Ave., Johnstown, Pa.

SCHLICHTING, Walter G. (*M* 1932) Mgr., Air Cond. Dept., Clarage Fan Co., 619 Porter St., Kalamazoo 16, and • 224 S. Fletcher Ave., Kalamazoo 51, Mich.

SCHMIDT, Alexander F. (*M* 1943) Gen. Supvr., Air Cond. Dept., Ansco-Div. of General Aniline & Film Corp., Charles St., and • 174 Crary Ave., Binghampton, N. Y.

SCHMIDT, Carl W. (*M* 1944) Regis. Engr., Washington Lane, R. D. 1, Ambler, Pa.

SCHMIDT, Harry (*M* 1937) Cons. Engr., Air Cond., Htg., Vtg., & Refrig., 130 Westville Ave., Caldwell, N. J.

SCHMIDT, Jack F. (*J* 1946) Instructor, Engrg. Training Dept., • Carrier Corp., 300 Geddes St., Syracuse 1, and 225 Robineaw Rd., Syracuse 4, N. Y.

SCHMITT, William C. (*J* 1945; *S* 1944) Mech. Engr., Wm. J. Schmitt, Inc., 118 Brown St., Rochester 6, and • 590 Beach Ave., Rochester 12, N. Y.

SCHNEEBERG, Floyd Henry (*J* 1943) Instructor, William Hood Dunwoody Industrial Inst., 818 Wyazata Blvd., Minneapolis, and • 1444 Edgerton, St. Paul 1, Minn.

SCHNEIDER, Charles H. (*A* 1946; *J* 1938) Branch Mgr., • Ilg Electric Ventilating Co., 706 Professional Bldg., Pittsburgh 22, and 1413 Park Blvd., Dormont, Pittsburgh 16, Pa.

SCHNELL, Robert H. (*A* 1938) Mech. Draftsman, B. E. Landes, Cons. Engr., 722 Old Colony Bldg., Des Moines, and • 1617-33rd St., Des Moines 11, Ia.

SCHNURR, William J. (*A* 1947) Pres., • Schnurr & Kraemer Ltd., 125 Weber St. W., and 125 Brubacher St., Kitchener, Ont., Canada.

SCHOEDEL, Joseph J. (*A* 1947) Engr., Htg. & Vtg., John Harrison Co., Butler Plank Rd., Pittsburgh, and • 730 Horning Ave., Pittsburgh 27, Pa.

SCHOEN, Daniel D. (*J* 1942) Mech. Engr., R. B. Rogers Co., 1120 Leggett Ave., New York, and • 272 S. Broadway, Yonkers 5, N. Y.

SCHOENHERR, Edgar J. (*A* 1946) Mech. Engr., Dept. of Public Works, Archt'l. Branch, Dominion Government, and • 244 Charlotte St., Ottawa, Ont., Canada.

SCHOENIJAHN, Robert P. (*M* 1919) Owner, • 303-305 Industrial Trust Bldg., Wilmington 7, and 719 Nottingham Rd., Wilmington 56, Del.

SCHOEPFLIN, P. H. (*M* 1920) Pres., • Niagara Blower Co., 405 Lexington Ave., New York, and 9 Broadmoor Rd., Scarsdale, N. Y.

SCHOERNER, R. T. (*M* 1943) Chief Engr., • Taco Heaters, Inc., 137 South St., Providence, and 48 Fairway Dr., Oaklawn, R. I.

SCHOONOVER, William A. (*J* 1947) Sales Engr., • The Trane Company, 626 Broadway, Room 307, Cincinnati, and 2637 Park Ave. No. 3, Norwood, Ohio.

SCHOTT, Frederick C. (*A* 1945) Co-Owner, • Atlas-Butler Furnaces, Inc., 243 N. Fifth St., Columbus 15, and 160 W. Royal Forest Blvd., Columbus 2, Ohio.

SCHREIBER, Herbert W. (*A* 1937) Branch Mgr., • Johnson Service Co., 507 E. Michigan St., Milwaukee 2, and 6187 Washington Circle, Milwaukee 13, Wis.

SCHREIBER, W. F. (*M* 1945) Owner, • Schreiber Institute of Refrigeration, 902 Westport Rd., Kansas City 2, Mo., and 6200 Terry Dale Rd., Merriam, Kans.

SCHROCK, Robert E. (*S* 1948) Student, University of Michigan, and • 555 Packard, Ann Arbor, Mich.

SCHROEDER, Delman E. (*A* 1943) Student, 1531 Douglas St., Ames, Ia.

SCHROEDER, William R. (*A* 1939) Pvt., 345th Infantry, Camp McKain, Miss., and • 201 Kedzie W., Evanston, Ill.

SCHROTH, August H. (*Life Member*; *M* 1911) Metropolitan New York Repr., Columbia Radiator Co., and • 167 N. Grove St., East Orange, N. J.

SCHUBERT, Arno G. (*M* 1939) Asst. Prof., Mech. Engrg., Rensselaer Polytechnic Institute, Troy, and • 1301 Broadway, Watervliet, N. Y.

SCHUCHART, Oscar W. (*J* 1948; *S* 1946) Jr. Engr. & Designer, George R. Rhine, Cons. Mech. Engr., 1208 Alamo Natl. Bldg., San Antonio 5, and • 1403 W. Hollywood, San Antonio 1, Texas.

SCHUETT, Donald F. (*A* 1946) Mgr., Air Cond. Dept., Calcasieu Lumber Co., P. O. Box 996, and • 2515 Winsted Lane, Austin, Texas.

SCHUETZ, Clyde C. (*A* 1936) Research Engr., United States Gypsum Co., 1253 Diversey Pkwy., Chicago, and • 206 S. Edward St., Mt. Prospect, Ill.

SCHULEIN, Lars E. (*A* 1942) Sales Repr., • 431 S. Dearborn St., Chicago 5, and 617 South 23rd Ave., Bellwood, Ill.

SCHULER, William B. (*A* 1947) • Products, Inc., 304 Home Federal Bldg., Sixth & Grand Ave. Des Moines 9, and 1620 Vine St., West Des Moines, Iowa.

SCHULER, William R. (*M* 1947) Engr., Robson & Woese, Cons. Engrs., Syracuse, and • 119 Hopper Rd., Syracuse 7, N. Y.

SCHULMEISTER, Walter A. (*M* 1944) • S. E. Dockstader, Inc., of Washington, D. C., 10 Power Bldg., North Tonawanda, and R. F. D. 1, Niagara Falls, N. Y.

SCHULTE, Russell A. (*S* 1948) Student, David Ranken Jr. School of Mechanical Trades, and • 4703 St. Louis Ave., St. Louis, Mo.

SCHULTZ, Albert W. (*M* 1936) Owner, Albert W. Schultz Co., R. J. Mangan Co., 925 Seventh Ave., S., Minneapolis 4, and • 5204 France Ave. S., Minneapolis 10, Minn.

SCHULTZ, Clyde W. (*A* 1946) Engr., Green Engineering Co., 208-210 Bever Bldg., and • P. O. Box 883, Cedar Rapids, Iowa.

SCHULTZ, Stewart F. (*A* 1943) Builders Htg. & Supply Co., 703 Pontiac State Bank Bldg., Pontiac, and • 4755 Walnut Lake Rd., Birmingham, Mich.

SCHULTZE, Donald P. (*A* 1948) Sales Engr., Hart & Cooley Mfg. Co., 500 E. Eighth, and • 78 East 12th, Holland, Mich.

SCHULZ, Burnett J. (*J* 1948; *S* 1946) Schulz Oil Co., 2900 E. Seventh St., Bay City, Texas.

SCHULZ, W. F. (*M* 1944) Cons. Engr., • 870 Shrine Bldg., and 1839 Overton Park Ave., Memphis, Tenn.

SCHULZE, Ben H. (*M* 1921) Eastern and Gov't. Sales Mgr., • Kewanee Boiler Corp., 40 West 40th St., New York 18, N. Y., and Four Brooks Farm, Pipersville, Pa.

SCHUMACHER, C. W. (*M* 1943) Partner, General Heating & Cooling Co., 1920-22 Grand Ave., Kansas City, Mo.

SCHUMACHER, John F. (*A* 1944) Draftsman, • Columbus Heating & Ventilating Co., R. 3, Sta. G, and 3290 Groveport Pike, Columbus 7, Ohio.

SCHUNDLER, Hans Otto, Jr. (*A* 1946) Insulation Sales Mgr., • F. E. Schundler & Co., Inc., (E Div.) 45-15 Vernon Blvd., Long Island City, N. Y., and 10 Lorraine Rd., Madison, N. J.

SCHURMAN, John A. (*M* 1936; *J* 1935) Appl. Engr., York Corp., 2700 Washington Ave., Cleveland 13, and • 16307 Lakewood Heights Blvd., Lakewood 7, Ohio.

SCHURMAN, John H. (*A* 1947) Partner, • Huntington Heating & Supply Co., 916 Sixth Ave., and 1120 11th St., Huntington, W. Va.

SCHUSTER, Paul H. (*A* 1942) Htg. Engr., • East Texas Plumbing Supply Co., P. O. Box 1432, and 509 Idylwood Dr., Longview, Texas.

SCHWARTZ, Fred D. (*A* 1945) Professional Engrg. Consultant, • 1324½ Wilshire Blvd., Los Angeles 14, and 1053 Crenshaw, Los Angeles, Calif.

SCHWARTZ, Maurice (*A* 1938) Pres., • Schwartz Appliances, Inc., 119 Doughty Blvd., Inwood, L. I., and 804 Bolton Rd., Far Rockaway, N. Y.

SCHWERMAN, Carl H. (*M* 1947) Engr., R. B. Hayward Co., 1714 Sheffield Ave., Chicago 14, and • 115 S. William St., Mount Prospect, Ill.

SCHWIND, L. Morgan (*A* 1947) Mgr., Control Div., Hester-Bradley Co., 2835 Washington, St. Louis 3, and • R. 5, Box 584, Kirkwood 22, Mo.

SCHWIRTZ, Ben A. (*A* 1948) Sales Repr., • The Trane Co., 1026 Fleming Bldg., Des Moines, and Box 574, Fort Des Moines, Iowa.

SCHWITZER, Louis, Jr. (*M* 1945) Exec. Vice-Pres., • Schwitzer-Cummins Co., 1125 Massachusetts Ave., Indianapolis 7, and 6449 N. Chester, Indianapolis 44, Ind.

SCOFIELD, Paul C. (*A* 1937; *J* 1933) Project Engr., Air Research Manufacturing Co., 9851 Sepulveda, Los Angeles, and • 425 E. Randolph, Glendale 7, Calif.

SCOTT, Angus C. (*A* 1946) Sales, • Hall-Neal Furnace Co., Indianapolis, and Milford, Ind.

SCOTT, Clarence E. (*M* 1943) Mgr., Indus. Htg. Refrig. Div., Fedders Manufacturing Co., Inc., 57 Tonawanda St., and • 800 W. Ferry St., Buffalo, N. Y.

SCOTT, Donald C. (*A* 1943) Asst. Mgr., Ware Coupling & Nipple Co., and • 90 Church St., Ware, Mass.

SCOTT, Edwin Earl (*A* 1943) Partner, • Johnson & Scott, 918 Dermon Bldg., Memphis 3, and 11 S. Auburndale, Memphis, Tenn.

SCOTT, F. William (*J* 1947; *S* 1943) Mech. Engr., Weapons Div., Naval Ordnance Laboratory, Navy Yard, Washington 25, and • 2013–31st St. S.E., Washington 20, D. C.

SCOTT, George M. (*Life Member*; *M* 1915) Pres., Child & Scott Co., Inc., 153 East 38th St., New York, and • 38 Stratford Rd., Scarsdale, N. Y.

SCOTT, James (*M* 1943) Mgr., York Corp., 659 E. Sixth St., Cincinnati, Ohio, and • R. D. 5, York, Pa.

SCOTT, John C. (*A* 1946) Sales Engr., • The Powers Regulator Co., 3819 N. Ashland Ave., and 2320 East 70th St., Chicago, Ill.

SCOTT, Philip R. (*A* 1948) Cons. Engr., Assoc., • Gutteridge, Haskins & Davey, 472 Bourke St., and 140 Abbott St., Sandringham, Melbourne, Australia.

SCOTT, Roy M. (*A* 1941) Mfrs. Repr., • 323 Tenth St., San Francisco 3, and 35 Fairfield Way, San Francisco, Calif.

SCOTT, William P., Jr. (*M* 1941; *J* 1939) Sr. Partner, Scott Co., 243 Minna St., San Francisco 3, and • 2700 Broadway, San Francisco 23, Calif.

SCOTT, Wirt S. (*M* 1943) Engr., • Philadelphia Electric Co., 1000 Chestnut St., and 4619 Chester Ave., Philadelphia 43, Pa.

SCROGGS, Frank M. (*A* 1947) Sales Mgr., City Fuel Oil & Coal Co., P. O. Box 550, St. Petersburg, and • 720 16th Ave. S., St. Petersburg 5, Fla.

SCURLOCK, Ulvan M. (*A* 1946) Owner, • Bill Scurlock Air Conditioning & Heating Service Co., 4048 Main St., and 4207 Baltimore, Kansas City, Mo.

SEABRIGHT, Frederick C. (*A* 1944) Engr., Columbus Heating & Ventilating Co., Columbus, and • 455 W. Sixth Ave., Columbus 1, Ohio.

SEALY, Sydney I. (*A* 1946) Mgr., • Matthew Hall & Co., Ltd., 95/97 Princess St., Manchester 2, and 18 Regents Close, Bramhall, Cheshire, England.

SEAT, J. Harvey (*A* 1946) Owner., • J. Harvey Seat & Assocs., 161 Simpson St. N.W., and 2450 Peachtree Rd. N.E., Atlanta, Ga.

SECKINGER, Benjamin J., Jr. (*M* 1941) Vice-Pres., • Seckinger Sons Co., Inc., 180 Forsyth St. S.W., and 1110 Lanier Blvd. N.E., Atlanta, Ga.

SEDGWICK, David E. (*A* 1947) Secy., • The Waterman-Waterbury Co., 1121 Jackson St. N.E., Minneapolis 13, and 4055 Pleasant Ave. S., Minneapolis 8, Minn.

SEDGWICK, S. W. (*M* 1944) Resident-Mgr., • Trane Company of Canada, Ltd., 130 Seventh Ave. E., and 3029 Roxboro Glen Rd., Calgary, Alta., Canada.

SEELBACH, Herman, Jr. (*M* 1944; *A* 1937) Dist. Mgr., • Minneapolis-Honeywell Regulator Co., 45 Allen St., Buffalo 2, and 189 Union St., Hamburg, N. Y.

SEELBACH, William R. (*A* 1946) Pres., • Bryant-Seelbach Co., 1934 Elmwood Ave., Buffalo 7, and Windover, Hamburg, N. Y.

SEELERT, E. H. (*A* 1935) Secy.-Treas., McQuay, Inc., 1600 Broadway N.E., and • 2540 W. Lake of Isles Blvd., Minneapolis, Minn.

SEELEY, Lauren E. (*M* 1930), (Council, 1944-46) Dean of the College of Technology, • University of New Hampshire, and School St., Durham, N. H.

SEELINGER, Harold N. (*A* 1947) Engr., • Meyer Strong & Jones, Inc., 101 Park Ave., New York, and 268 Eldert St., Brooklyn 7, N. Y.

SEEPE, Paul E. (*A* 1944) Sales Engr., • Minneapolis-Honeywell Regulator Co., 4-5 Rhodes Center, Atlanta, and 123 Clarion Ave., Decatur, Ga.

SEGLE, Thomas L. (*A* 1942) Htg. Engr., Wells & Wade Hardware, Inc., S. Wenatchee Ave., Wenatchee, Wash.

SEIBERT, Earl W. (*A* 1946) Pres., • Advanced Refrigeration Co., 1042 Gilbert Ave., Cincinnati, and R. 3, Hamilton, Ohio.

SEIGEL, Lawrence G.* (*A* 1945; *J* 1943) Prof., Case Institute of Technology, 10900 Euclid Ave., Cleveland 6, and • 943 Vineshire Rd., Cleveland 21, Ohio.

SEITER, J. Earl (*M* 1928) Mgr., Dist. Steam Dept., • Consolidated Gas Electric Light & Power Company of Baltimore, Room 503, Lexington Bldg., Baltimore 3, and 5710 Loch Raven Blvd., Baltimore 12, Md.

SEITZ, Ralph C. (*M* 1945) Space Htg. Dept., • Central New York Power Corp., 300 Erie Blvd. W., Syracuse 2, and DeWittshire Rd., DeWitt, N. Y.

SELBY, S. Allen, Jr. (*A* 1947) Project Engr., Dvlpt. Dept., Chase Brass & Copper Co., and • 150 Hillside Ave., Waterbury, Conn.

SELDEN, Karl W., Jr. (*A* 1942) Branch Mgr., Minneapolis-Honeywell Regulator Co., 2400 Wilkinson Blvd., and • 232 S. Terrence St., Charlotte, N. C.

SELF, V. Floyd (*M* 1941) Sales Promotion, • Anemostat Corporation of America, 10 East 39th St., New York 16, and 615 Harrison Ave., Harrison, N. Y.

SELIG, E. T., Jr. (*M* 1936) Dir. of Engrg., c/o Richmond Radiator Co., New Castle, Del.

SELLMAN, Nils T. (*M* 1922) Vice-Pres., • Westchester Lighting Co., 9 S. First Ave., Mt. Vernon, and 56 Walworth Ave., Scarsdale, N. Y.

SELTZER, Paul A. (*A* 1943; *J* 1938) 314 McClatchy Bldg., Upper Darby, and • 79 W. Drexel Ave., Lansdowne, Pa.

SELVING, Holger T. (*M* 1945) Mech. Engr., Fisher Body Div., Works Engrg. Dept., 11-135 General Motors Bldg., Detroit, and • 8570 Pinehurst Ave., Detroit 4, Mich.

SEMEL, Edward (*A* 1943; *J* 1941) Engr., Huffman-Wolfe Co. of Philadelphia, 4660 North 18th St., Philadelphia, and • 6029 Ellsworth St., Philadelphia 43, Pa.

SENK, Edmund P. (*A* 1947; *J* 1946) Mech. Engr., Robert E. Hattis, Cons. Engrs., 28 E. Jackson Blvd., Chicago, and • 5655 Windsor Ave., Chicago 30, Ill.

SETZER, Charles M., Jr. (*A* 1948) Sales Mgr., • Charles M. Setzer & Co., P. O. Box 1867, and 2808 Willow Dr., Charlotte, N. C.

SEVERNS, William H.* (*M* 1933) Prof., Mech. Engrg., University of Illinois, and • 609 Indiana Ave., Urbana, Ill.

SEYFANG, William G. (*M* 1939) Managing Engr., • Board of Education, City Hall, and 116 Dorchester Rd., Buffalo, N. Y.

SEYMOUR, Cyril D. (*A* 1945) Pres., Seymour Plumbing & Heating Contractors, Ltd., 97 Ridley Blvd., Toronto 12, Ont., Canada.

SEYMOUR, James E. (*A* 1937) Pres. & Treas., Seymour Corp., 346 Russell St., and • 208 Lakewood Blvd., Madison 4, Wis.

SGAMBATI, Anthony P. (*A* 1947; *J* 1944; *S* 1939) Engr., Power, Industrial & Process Piping, c/o Daugherty Co., Inc., 502 Union National Bank Bldg., Youngstown, and • 39 Third St., Campbell, Ohio.

SHAER, I. Ernest (*A* 1934) Treas. and Sales Mgr., • Shaer & Turner Engineering Co., 87 Gardner St., West Roxbury 32, and 154 Seaver St., Roxbury, Mass.

SHAFER, Howard S. (*M* 1946) Branch Mgr., • American Blower Corp., 400 Key Bldg., Oklahoma City 2, and Rt. 2, Box 117, Oklahoma City, Okla.

SHAFER, Marvin L. (*M* 1947) Mech. Engr., and • 5501 Hanover, Dallas 9, Texas.

SHAFER, W. P., Jr. (*A* 1944; *J* 1941; *S* 1939) Engr., • Shafer Plumbing & Electric Co., 414 N. St. Mary's St., and 107 Westover Rd., San Antonio, Texas.

SHAFFER, Chester E. (*M* 1937) Research Engr., • Koppers Co., Kearny, and 645 Belgrove Dr., Arlington, N. J.

SHANAHAN, John J. (*M* 1946) Owner, • 2715 Monticello Ave., and 122 East 27th St., Norfolk 8, Va.

SHANKLIN, Arthur P. (*M* 1929) Vice-Pres., • Carrier Corp., 300 S. Geddes St., Syracuse 1, and 203 Sedgwick Dr., Syracuse, N. Y.

SHANKLIN, John A. (*M* 1928) Vice-Pres. and Treas., West Virginia Heating & Plumbing Co., 233 Hale St., Charleston, W. Va.

SHANNON, Baker L. (*J* 1946) Engr., Reg. F. Taylor, Cons. Engr., 1003 Milam Bldg., Houston, and • 6315 Alleghany, Apt. 2, Houston 5, Texas.

SHAPIRO, Charles A. (*A* 1943; *J* 1938) Lt., • S. L. C. U. 44, U. S. N. L. F. E. D., Albany 6, Calif.

SHAPIRO, Morris (*M* 1941) Cons. Engr., • 908 20th St., Washington, and 6323 Luzon Ave. N.W., Washington 11, D. C.

SHARP, Henry C. (*M* 1935) Owner, • H. C. Sharp Co., 4060 W. Pine Blvd., St. Louis 8, Mo., and 1326 Waldron Ave., University City 14, Mo.

SHARP, H. Ross (*A* 1946) Vice-Pres., • Sharp Heating Supply, Inc., 7804 Wade Park Ave., Cleveland, and 1850 Garfield Rd., East Cleveland 12, Ohio.

SHARP, John E. (*A* 1947) Owner, • Sharp's Stoker & Heating Co., 215 N. Fifth St., Springfield, Ill.

SHARP, John R. (*A* 1937) Lt. Col., • Exec. Officer, U. S. Engineer Office, Huntington 18, and McCoy Rd., Huntington, W. Va.

SHARPE, Vernon W. (*M* 1945) Chief Engr., Pryne & Co., Towne Ave., Pomona, and • 2670 Oak Knoll Ave., San Marino 9, Calif.

SHATALOFF, Nicholas S. (*M* 1947) Engr., Buensod-Stacey, Inc., 60 East 42nd St., New York, and • 614 West 152nd St., New York 31, N. Y.

SHAVER, C. W., Jr. (*A* 1946) Archt. and Owner, 22 S. Main, Sheridan, Wyo.

SHAW, Burton E.* (*A* 1936; *J* 1934) Vice-Pres. in charge Engrg. and Prod., Photoswitch, Inc., 77 Broadway, Cambridge, and • Ipswich Rd., East Boxford, Mass.

SHAW, George W. D. (*M* 1944) U. S. Army Engrs., 700 Union Guardian Bldg., Detroit 26, and • 14541 Longacre Rd., Detroit 27, Mich.

SHAW, J. A. (*M* 1938) Gen. Elec. Engr., • Canadian Pacific Railway Co., Windsor St. Station Room 900, and Hudson Heights, Montreal, Que., Canada.

SHAW, N. J. H. (*M* 1927; *J* 1925) Sales Engr., Barnes & Jones, Inc., 128 Brookside Ave., Jamaica Plain, and • 100 Athelstane Rd., Newton Centre 59, Mass.

SHAWHAN, Samuel F. (*M* 1945) Engr., • Carrier Corp., 300 S. Geddes St., Syracuse 1, and 101 Woodbine Ave., Syracuse, N. Y.

SHEA, Francis X. (*A* 1944) East Divisional Mgr., • Farr Co., 601 West 26th St., New York 1, and 63-209 Alderton St., Rego Park, N. Y.

SHEA, Michael B. (*Life Member*; *M* 1930) 106 N. Aberdeen Ave., Wayne, Pa.

SHEAHAN, John A. (*M* 1945) Chief Htg. Engr., • Atlanta Gas Light Co., 243 Peachtree St. N.E., and 573 Seminole Ave. N.E., Atlanta, Ga.

SHEARER, William A., Jr. (*J* 1941; *S* 1939) Mech. Engr., E. I. duPont de Nemours & Co., Inc., 13015 Du Pont Bldg., and • 1001 Park Pl., Wilmington, Del.

SHEARS, Matthew W. (*M* 1922) Htg. Engr., • C. A. Dunham Co., Ltd., 1523 Davenport Rd., Toronto 4, and 39 Sylvan Ave., Toronto, Ont., Canada.

SHEDD, Robert W. (*A* 1948) R. L. Deppmann Co., 1514 Wealthy St. S.E., Grand Rapids 6, Mich., and 719 Ashland Ave., Rockford, Ill.

SHEDROFF, David I. (*J* 1947) Student, • 64 Kirkland St., Cambridge 38, Mass., and 793 East 125th, Cleveland 8, Ohio.

SHEERE, Albert D. (*A* 1945) Div. Mgr., • A. M. Byers Co., 1502 Esperson Bldg., Houston 2, and 2621 Sunset Blvd., Houston 5, Texas.

SHEFFIELD, Raymond A. (*M* 1942) Owner, Air Conditioning Engineering Co., 44 First St., Cambridge 41, and • 53 Brandon Rd., Milton 87, Mass.

SHEFFLER, M. (*M* 1921) Partner, • Sheffler-Gross Co., 1000 Drexel Bldg., Philadelphia 6, and 419 Chapel Rd., Melrose Park, Montgomery Co., Pa.

SHEFFLER, Marcus A. (*S* 1947) Student, Drexel Institute of Technology, and • 6722 North 16th St., Philadelphia 26, Pa.

SHELBY, Alexander W. (*M* 1942) Secy., • Shelby-Skipwith, Inc., 972 Union Ave., and 1748 Vinton Ave., Memphis, Tenn.

SHELBY, Lloyd W. (*J* 1948) Asst. Supt. of Bldgs., • Vanderbilt University, Nashville 4, and 1400–25th Ave. S., Nashville 5, Tenn.

SHELDON, Nelson E. (*M* 1927) Branch Mgr., • Carrier Corp., 820 Reynolds Arcade Bldg., Rochester 4, and 41 Lanark Crescent, Rochester 9, N. Y.

SHELDON, Herbert P. (*M* 1947) Vice-Pres., Harry F. Haldeman, Inc., 1106 S. Hope St., Los Angeles 15, and • 2055 Midwick Dr., Altadena, Calif.

SHELDON, Robert W. (*A* 1942) Htg. Engr., The Lake Shore Gas Co., Ashtabula, and ● 745 Eastlawn St., Geneva, Ohio.

SHELDON, William D., Jr. (*A* 1936; *J* 1934) Chief Engr., Sheldon's, Ltd., and ● Cedar St., Galt, Ont., Canada.

SHELEY, Earl D. (*M* 1937) Pres., ● Glanz & Killian Co., 1761 W. Forest Ave., Detroit 8, and Box 243, Birmingham, Mich.

SHELFER, Edwin L. (*A* 1946) Owner, Mgr., ● Shelfer Air Conditioning Co., 1425 Franklin Ave., and 2414 Colonial Ave., Waco, Texas.

SHELL, Jack D. (*M* 1940) Dept. Head in charge of Htg., Vent. and Air Cond., Jefferson Amusement Co., and ● 1296 Washington Blvd., Beaumont, Texas.

SHELLDROP, Tonn F. (*M* 1942) Asst. Engr., The Port of New York Autfiority, 111 Eighth Ave., New York, and ● 10 Washington St., Hempstead, L. I., N. Y.

SHELLEY, Karl B. (*M* 1947; *A* 1944) Project Engr., Wertz Engineering Co., 441 N. Second St., Reading, and ● 510 State St., Shillington, Pa.

SHEPARD, Carl R. (*M* 1941) Sr. Mech. Engr., U. S. Public Buildings Administration, Room 856, U. S. Appraisers Bldg., 630 Sansome St., San Francisco 11, and ● Apt. 101, 2339 Hilgard Ave., Berkeley 9, Calif.

SHEPARD, Edward C. (*M* 1943) Mech. Engr., Federal Shipbuilding & Drydock Co., Lincoln Highway, Kearny, and ● 14 Bodwell Terrace, Millburn, N. J.

SHEPARD, John deBerard (*M* 1937; *J* 1929) Assoc., P. L. Davidson, Cons. Engr., Box 2235, Greenville, S. C.

SHEPARD, L. Warren (*A* 1947) Sales Engr., Minneapolis-Honeywell Regulator Co., 35 Webster St., Hartford, and ● 78 State St., Guilford, Conn.

SHEPPARD, Frank A. (*M* 1918) ● Johnson Service Co., 1031 Wyandotte St., Kansas City 6, and 27 East 70th St., Kansas City 5, Mo.

SHEPPARD, Franklin A. (*A* 1946) Vice-Pres., ● Mechanical Appliance & Transmission Co., 1410 Stanley St., Room 806, and Hudson Heights, Montreal, Que., Canada.

SHEPPARD, Wallace K. (*M* 1942) Supvsr. of Htg. Sales, ● The Peoples Natural Gas Co., 545 William Penn Way, and 6420 Darlington Rd., Pittsburgh, Pa.

SHEPPERD, P. D. (*A* 1940; *J* 1938) Sales Engr., ● Johnson Service Co., 230 E. Alexandrine, Detroit 1, and 829 Cherokee Ave., Royal Oak, Mich.

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SHEPSTONE, Oscar (*M* 1943) Special Engr., Piping Dept., ● Dravo Corp., 300 Penn Ave., Pittsburgh 22, and 1443 Termon Ave., Pittsburgh 12, Pa.

SHER, Alvin I. (*J* 1946; *S* 1943) ● Sher's, 27 E. Superior St., Duluth 2, and 3025 E. Superior St., Duluth, Minn.

SHERBROOKE, Walter A. (*M* 1938) Pres., ● Piping Specialties, Inc., 114 Liberty St., New York 6, and 49 Margaret St., Great Kills, Staten Island 8, N. Y.

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SHERIDAN, Thomas J. (*A* 1947) Sales Engr., Burns Bros., 11 West 42nd St., New York 18, and ● 3151 Perry Ave., New York 67, N. Y.

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SHERMAN, V. L. (*M* 1935) Engrg. Editor, Consolidated Book Publishers, 153 N. Michigan Ave., Chicago 1, and ● 643 Hillside Ave., Glen Ellyn, Ill.

SHERMAN, Warren P. (*M* 1937) ● Simmons Industries, Inc., 412 Margaret St., Jacksonville 4, and Mandarin, Fla.

SHERRER, J. W., Jr. (*A* 1945) Mgr., Packaged Air Cond. Dept., Danforth Co., 5820 Center Ave., Pittsburgh, and ● 4064 Miller St., Pittsburgh 21, Pa.

SHIELDS, Carl D. (*A* 1947) Engr., Design Div., ● E. I. duPont deNemours & Co., Inc., Engineering Dept., Wilmington 98, and Shipley Rd., R. D. 3, Wilmington, Del.

SHIELDS, Roy W. (*M* 1945) Engr., Samuel R. Lewis, 100 W. Monroe St., Chicago 3, and ● 9115 S. Ada St., Chicago, Ill.

SHIFFLETTE, Donald F. (*A* 1948) Gen. Mgr., ● Stoker Sales & Service Company of Columbus, Inc., 230 N. Front St., and 1665 Hess Blvd., Columbus, Ohio.

SHILLER, Benjamin P. (*A* 1947) Chief Estimator, Young Brothers Co., 6500 E. Mack, Detroit 7, and ● 6141 Neff, Detroit 24, Mich.

SHILSTON, R. Aynsley (*M* 1943) Asst. Engr., Public Works (Mech. Dept.) ● Birmingham Corp., 38 Cambridge St., Birmingham 1, and 39 School Rd., Birmingham 13, England.

SHIMAZAKI, Thomas T. (*A* 1947) Mech. Engr., Ellerbe & Co., E-505, First National Bank Bldg., St. Paul, and ● 365 W. Central Ave., St. Paul 3, Minn.

SHIPP, William H. (*A* 1945) Sales Engr., Minneapolis-Honeywell Regulator Co., 108 Cummington St., Boston, and ● 124 Lewis Rd., Belmont 78, Mass.

SHIRE, A. C. (*M* 1942) Chief, Div. of Inventions and Engrg., ● Office of Technical Services, Dept. of Commerce, Washington, and 3215 Macomb St., Washington 8, D. C.

SHOALS, Charles A. (*M* 1948) Mech. Engr., ● Reg. F. Taylor, Cons. Engr., Bankers Mortgage Bldg., Houston, and 905 W. Alabama, Houston 6, Texas.

SHOEMAKER, R. W. (*M* 1947) 3533 Oak Knoll Blvd., Oakland 5, Calif.

SHORBA, Michael (*A* 1947) Engr., Bryant Gas Heating Co., 824 Marquette, Minneapolis, and ● 1457 Eleanor St., St. Paul, Minn.

SHORT, Wm. W. (*A* 1942) Pres., ● Wm. W. Short Co., Inc., 274 Madison Ave., New York 16, and 541 West 113th St., New York, N. Y.

SHREEVE, L. Dale (*A* 1944) Pres., M. & M. Supply Co., 902 S. Walnut, and ● 914 W. North St., Muncie, Ind.

SHROCK, John H. (*M* 1924) Vice-Pres., New York Blower Co., 171 Factory St., and ● 2026 Indiana Ave., LaPorte, Ind.

SHULL, Dean E. (*J* 1948) Htg. Engr., Hajoca Corporation, 515 East 11th St., Chattanooga, and ● 1233 Highland Dr., Chattanooga 5, Tenn.

SHULL, Leon F. (*A* 1945) 1065 York St., Denver 6, Colo.

SHULTZ, Earle (*A* 1919) Vice-Pres., Illinois Maintenance Co., 72 W. Adams St., Chicago 3, Ill.

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SHUMATE, James C. (*A* 1945) Vice-Pres., ● Noland Co., Inc., 512 Spring St., Atlanta 3, and 411 Pine Tree Dr. N.E., Atlanta, Ga.

SHUSTER, Wilbur W. (*M* 1946) Cons. Engr., ● Wm. E. Bodenstein & W. W. Shuster, 405 Second National Bank Bldg., and 3446 Wabash Ave., Cincinnati, Ohio.

SHUTTLEWORTH, Riley (*M* 1943) Prop., ● Shuttleworth Conditioned Air Co., 117 E. Michigan St., Indianapolis 4, and 2859 N. Meridian St., Indianapolis 8, Ind.

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SIDBURY, Roy W. (*A* 1944) Sales Engr., ● Chase Brass & Copper Co., Inc., 236 Grand St., Waterbury 91, and 79 Chapman Ave., Waterbury, Conn.

SIEGEL, Daniel E. (*J* 1940; *S* 1938) Partner, Guaranteed Heating & Engineering Co., 1923 Olive, St. Louis 3, and ● 7716 Wise Ave., Richmond Heights 17, Mo.

SIEGERT, Edward P. (*A* 1947) Mgr., ● Central Supply Co., 838 S.W. First Ave., and 5116 Southeast 37th Ave., Portland, Ore.

SIERK, Harry G. (*A* 1947) Engrg. Draftsman, Magney, Tusler & Setter, 202 Foshay Tower, Minneapolis, and ● 2625 S. Emerson Ave., Minneapolis 8, Minn.

SIGEL, Robert J. (*M* 1948) Sales Engr., York Corp., 1616 Walnut St., Philadelphia, and ● 104 Wynnedale Rd., Narberth, Pa.

SIGGINS, George S. (*A* 1943) Owner, • Industrial Fuel Burning Equipment, 737 Springfield Ave., Irvington, and 78 S. Harrison St., East Orange, N. J.

SIGMUND, R. W. (*M* 1932) Branch Mgr., • Westinghouse Electric Corp., Sturtevant Div., 419 Provident Bank Bldg., 630 Vine St., Cincinnati 2, and 130 Wm. H. Taft Rd., Cincinnati 19, Ohio.

SIGNOR, Carl W. (*M* 1946) Engr., • The Detroit Edison Co., 2000 Second Ave., Detroit 26, and 2140 W. Huron River Dr., Ypsilanti, Mich.

SILBERSTEIN, Bernard G. (*M* 1937) Dist. Mgr., • Ilg Electric Ventilating Co., 622 Broadway, and 814 E. Mitchell Ave., Cincinnati, Ohio.

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SILVERA, Americo (*A* 1943; *J* 1939) Appl. Engr., Carrier Corp., International Div., 122 East 42nd St., New York 17, and • 30-41–91st St., Jackson Heights, N. Y.

SIMKIN, Milton (*A* 1942; *J* 1936; *S* 1933) Engr., Charles Simkin & Sons, 130 Paterson St., Perth Amboy, and • 118 Grove Ave., Woodbridge, N. J.

SIMMONDS, Verne (*M* 1943) Sales Engr., 233 Grain Exchange Bldg., Omaha 2, and • 2416 Vane St., Omaha, Nebr.

SIMMONS, George P. (*A* 1946) Partner, Noah M. Simmons Co. 22 N. Ritter Ave., and • 4780 Wentworth Blvd., Indianapolis 1, Ind.

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SIMMONS, Noah L. (*A* 1946) Partner, • Noah M. Simmons Co., 22 N. Ritter Ave., and 4702 Wentworth Blvd., Indianapolis 1, Ind.

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SIMONS, B. C. (*M* 1938) Branch Mgr., • Minneapolis-Honeywell Regulator Co., 4030 Chouteau Ave., St. Louis 10, and 454 W. Swon Ave., Webster Groves, Mo.

SIMONS, Edward (*M* 1938) Cons. Engr., • 525 Market St., San Francisco 5, and 40 Villa Terrace, San Francisco 14, Calif.

SIMONSON, G. M. (*M* 1937) Cons. Engr., • 625 Market St., Room 309, San Francisco 5, and 20 Lorita Ave., Piedmont 11, Calif.

SIMPKINS, Arthur C. (*A* 1947) Mgr., Mech. Dept., Canadian Comstock Co., Ltd., 206 Laird Dr. N., and • 503 Broadway Ave., Leaside, Ont., Canada.

SIMPSON, C. Edward (*M* 1947) Mgr., Montreal Branch, • Carrier Engineering Ltd., 1396 St. Catherine St. W., Montreal, and 1123 Osborne Ave., Montreal 19, Que., Canada.

SIMPSON, Edward H. (*A* 1947) Engr., • Simpson & Rubin, Inc., 723 10th Ave., New York 19, and 117-01B Park Lane South, Kew Gardens 15, N. Y.

SIMPSON, G. L. (*M* 1941) Vice-Pres., Gen. Mgr., • Pittsburgh Lectrodryer Corp., P. O. Box 1766, Pittsburgh 30, and 317 Pine Rd., Edgeworth, Sewickley P. O., Pa.

SIMPSON, Harry (*A* 1945) Htg. Contr., 120 O'Connor Dr., Toronto, Ont., Canada.

SIMPSON, Harry A. (*A* 1947) Owner, • Simpson Engrg. Serv., 795 Walnut St., and 1054 Monroe Ave., Memphis, Tenn.

SIMPSON, John A. (*A* 1946) Archt., • 408 McKevitt Bldg., and 421 W. Sewells Point Rd., Norfolk, Va.

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SIMPSON, Walter A. (*A* 1946) Mgr.-Secy.-Treas., • R. E. Chase & Co., New Fliedner Bldg., Portland 5, and 2135 N.W. Marshall, Portland 10, Ore.

SIMPSON, Walter B. (*A* 1945) Div. Mgr., • A. M. Byers Co., 1270 Arcade Blvd., St. Louis 1, and 7747 Kingsbury, Clayton 5, Mo.

SIMPSON, William D. (*A* 1946) Engr., Buffalo Forge Co., 301 Standard Life Bldg., Pittsburgh 22, and • 646 Shady Dr. E., Pittsburgh 16, Pa.

SIMPSON, William K. (*M* 1919) M. S. Little Manufacturing Co., Hartford, and • 21 Sands St., Waterbury, Conn.

SINES, Chester F. (*M* 1945) Mech. Engr., Design Branch, Coordinator, Puget Sound Naval Shipyard, Des. Branch, P. S. H. S., and • 615 Times Ave., Bremerton, Wash.

SINGER, Gerald G. (*A* 1947) Pres., • Atlas Industries, Ltd., 159 Marie Ann E. and 4866 Isabella Ave., Montreal, Que., Canada.

SINGER, J. H. (*J* 1947) Sales Engr., Florida Hill York Corp., 1225 S.W. Eighth St., Miami, and • P. O. Box 231, Miami Beach, Fla.

SINGLETON, Arthur B. (*M* 1943) Engr., Kerr Machinery Co., Detroit, and • 711 Collingwood Ave., Detroit 2, Mich.

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SINGLETON, William H. (*M* 1945) Vice-Pres., and Treas., Mehring & Hanson Co., 1240 Jefferson Davis Highway, Arlington, and • 628 Oakland Terrace, Alexandria, Va.

SINGMASTER, J. Walter (*M* 1943) Pres. Lehigh Valley Supply Co., Third and Oak Sts., Allentown, and • 101 E. Main St., Macungie, Pa.

SINISH, William R. (*M* 1943) Htg. and Vent. Engr., A. M. Strauss, Archt., Cal. Wayne Bldg., Fort Wayne, and • 14008 Charlotte Ave., Fort Wayne 3, Ind.

SISK, R. J. Van (*M* 1943) Vice-Pres. and Gen. Mgr., Piedmont Engineering Corp., and • 2539 Forest Dr., Charlotte, N. C.

SITTON, Elbert R. (*A* 1945) Sales Engr., B & B Engineering & Supply Co., 2900 Washington, P. O. Box 1144, Houston, and • 1211 Elm Pl., Houston 8, Texas.

SKAGERBERG, Rutcher (*M* 1939) Chief Engrg. Sect., • Public Housing Admin., Longfellow Bldg., Washington, D. C., and 420 Tyler Pl., Alexandria, Va.

SKAGGS, George E. (*M* 1945) Staff Engr., • Donald R. Warren Co., 500 S. Figueroa St., Los Angeles, and 693 Spruce St., Oakland, Calif.

SKIDMORE, John G. (*M* 1944) Constr. Engr., • Port of New York Authority, 111 Eighth Ave., and 208 Woodbine Rd., Roslyn Heights, L. I., N. Y.

SKINNER, Alton, Jr. (*A* 1944; *J* 1940) Supt., • J. R. Bagwell Co., P. O. Box 2007, and 1202 Vickers Ave., Durham, N. C.

SKINNER, Frank (*A* 1944) Estimator, Texas Mechanical Co., Houston 1, and • 3379 Tampa St., Houston 4, Texas.

SKINNER, Neil D. (*M* 1947) Pres., • Hoffman Specialty Co., 1001 York St., Indianapolis 7, and 5730 Carrollton Ave., Indianapolis, Ind.

SLATER, W. F. (*M* 1944) Pres., • W. F. Slater Engineering Corp., 627 Monroe Ave., Memphis 3, and 115 Morningside Park, Memphis, Tenn.

SLATER, William H. (*J* 1945) Engr., Carrier Corp., 12 South 12th St., Philadelphia, Pa., and • 425 Lakeview Ave., Haddonfield, N. J.

SLATTERY, Patrick H. (*A* 1946) Service Mgr., • Kentucky Utilities Co., 406 Broadway, and 1664 Broadway, Paducah, Ky.

SLAWSON, Lloyd E. (*A* 1938) Pres., • Slawson Equipment Co., Inc., 1792 East 40th St., Cleveland 21, and 1179 Sylvania Rd., Cleveland Heights 21, Ohio.

SLEISTER, Park E. (*A* 1943) Field Supt., • Leo A. Daly Co., Archt. & Engrs., 629 Insurance Bldg., Omaha, and • 6565 Maple St., Omaha 4, Nebr.

SLEMMONS, John D. (*M* 1937) Mgr., • American Blower Corp., 2–15th Ave., Columbus 1, and R. F. D. 2, Wilson Bridge Rd., Worthington, Ohio.

SLOANE, David J. (*J* 1943; *S* 1939) U. S. Army, and • 56th General Hospital, Ft. Jackson, S. C.

SLUDER, C. T. (*M* 1944) Mech. Engr., • Federal Housing Administration, 1001 Vermont Ave., N.W., Washington, and 1320–21st St. N.W., 45, Washington 6, D. C.

SMAK, Julius R. (*A* 1934) Engr., Fletcher-Thompson, Inc., 211 State St., Bridgeport, and • 160 Morehouse Highway, R. D. 6, Fairfield, Conn.

SMALL, Alex G. (*M* 1945) Assoc. Htg. and Vent. Engr., Los Angeles City Board of Education, 1425 S. San Pedro St., Los Angeles 15, and • 1575 Casa Grande St., Pasadena 7, Calif.

SMALL, Bartlett R. (*M* 1938; *A* 1937; *J* 1932) Staff Engr., ● Aluminum Company of America, 801 Gulf Bldg., Pittsburgh 19, and 18 S. Linwood Ave., Pittsburgh 5, Pa.

SMALL, Ray A. (*M* 1941) Mech. Engr., Const. Div., Veterans Administration Station, Marietta, Ga.

SMART, J. H. (*A* 1944) Vice-Pres. in charge of Sales, ● Tuttle & Bailey, Inc., and 419 Lincoln St., New Britain, Conn.

SMERLING, Daniel (*A* 1944) Dist. Sales Engr., ● Flynn & Emrich Co., 52 Whitney Ave., P. O. Box 1169, and 538 Norton Pkwy., New Haven, Conn.

SMILES, Roy H. (*M* 1941) Dist. Dealer Mgr., ● Carrier Corp., 12 South 12th St., Philadelphia 7, and 514 Overlook Rd., Philadelphia 28, Pa.

SMITH, Alan McK. (*J* 1947) Engr., Otis Massey Co, 201 Hutchens, Box 293, and ● 102 Dresden, Houston, Texas.

SMITH, Albert M. (*A* 1947) Asst. Chief Engr., Williard Sales & Service Inc., 2901 N. Broad St., Philadelphia, and ● 2031 Nedro Ave., Philadelphia 38, Pa.

SMITH, Alexander S. (*A* 1944) Sales Repr., ● Jenkins Bros., 570 Gas & Electric Bldg., Denver 2, and 2332 Ash St., Denver, Colo.

SMITH, Alfred J. (*M* 1945) Cons. Engr., 70 Wigmore St., London W. 1, and ● 56 The Avenue, Muswell Hill, London N. 10, England.

SMITH, Arthur J. (*A* 1947) Engr., ● J. C. Marlow & Co., Inc., 1139 Peachtree St., and 1830 Peachtree Rd. N.W., Atlanta, Ga.

SMITH, Bernard (*A* 1945) Cons. Engr., ● 17 St. Georges Rd., and Springthorpe, Douro Rd., Cheltenham, Glos., England.

SMITH, Charles H. (*M* 1944) Secy. and Dir., ● L. J. Wing Manufacturing Co., 154 West 14th St., New York 14, N. Y., and 501 Highland Ave., Newark 4, N. J.

SMITH, Clifford F., Jr. (*J* 1943; *S* 1941) Mech. Engr., Clifford F. Smith Plumbing & Heating Co., 312 S. Minn Ave., and ● 1609½ S. Center Ave., Sioux Falls, S. D.

SMITH, C. Warner (*A* 1948) Middle Atlantic Dist. Mgr., ● Ilg Electric Ventilating Co., 1432 Commercial Trust Bldg., Philadelphia 2, and 112 Righters Mill Rd., Narberth, Pa.

SMITH, David J. (*A* 1948; *J* 1941) Sales Mgr., ● Walter H. Eagan Co., 2336 Fairmount Ave., Philadelphia 30, and 524 Mercer Rd., Merion Park, Merion P. O., Pa.

SMITH, D. Kennard (*A* 1947) Owner, ● 840 N. Holly St., Philadelphia 4, and 218 E. Marthart Ave., Havertown, Pa.

SMITH, Donald S. (*J* 1947) Engr., ● Natkin and Co., 1015 Sampson St., Houston 3, and 4127 Dartmouth, Houston 5, Texas.

SMITH, Donald V. H. (*M* 1947) Donald Smith & Partners, Cons. Engrs., 15 Balham Park Rd., London S.W. 12, and ● 62 West Common, Harpenden, Herts., England.

SMITH, Edward D. (*A* 1944) Vice-Pres. & Mgr., Machinery Div., The Lang Co., Inc., 267 W. First South, Salt Lake City 9, and ● 1732 Laird Ave., Salt Lake City 5, Utah.

SMITH, Edward O. (*M* 1947) Asst. Mgr., ● Inspection Dept., Eastern Gas & Fuel Assocs., Coal Div., 2420 Koppers Bldg., Pittsburgh 19, and 3438 Delaware Ave., Pittsburgh 14, Pa.

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SMITH, Emmett A. (*A* 1947) Mfrs. Agent, ● Southern Heater Co., Inc., 844 Barronne St., and 50 Fountainbleau Dr., New Orleans, La.

SMITH, Eric H. (*A* 1947) Tech. Asst. to Sales Dir., The Standard & Pochin Bros. Ltd., Evington Valley Rd., and ● 48 Holmfield Ave., Leicester, England.

SMITH, Ernest T. (*M* 1943) Engr., ● The Detroit Edison Co., 2000 Second Ave., Detroit 26, and 4400 Three Mile Dr., Detroit 24, Mich.

SMITH, Gard W. (*M* 1927) Sales Engr., Premier Furnace Co., 1131 Guilford St., Huntington, Ind.

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SMITH, George E. (*M* 1944; *A* 1942) Engrg. Draughtsman, Grade 1, Dept. of Works & Housing for Commonwealth of Australia, and ● "Highroyd," 1 Musgrave St., Mosman, Sidney, N. S. W., Australia.

SMITH, Guy F. (*A* 1945) Sales Engr., The H. B. Smith Co., Inc., 605 Fox Bldg., Philadelphia 3, and ● 46 W. Essex Ave., Lansdowne, Pa.

SMITH, Harley H. (*A* 1946) Branch Mgr., ● United States Radiator Corp., Pacific Steel Boiler Div., 1505 N. Capitol, Washington, D. C., and 1523 Ethel Ave., Lincoln Park 25, Mich.

SMITH, Harold C. (*M* 1941) Owner, ● Smith Steam Specialty Co., 1116-18 Temple Bldg., Kansas City 6, and 5840 Olive St., Kansas City 4, Mo.

SMITH, H. Gilman (*M* 1944) Sales Engr., ● Aladdin Heating Corp., 2222 San Pablo Ave., Oakland 12, and 751 Warfield Ave., Oakland 10, Calif.

SMITH, Howard W., Jr. (*A* 1944) Engr., Southern California Telephone Co., 740 S. Olive St., Los Angeles 55, and ● 1954 Milan Ave., South Pasadena, Calif.

SMITH, Jay V. (*A* 1947) Engr., Western Furnaces, Inc., 950 Commerce, Tacoma, and ● 502 S. Eye, Apt. No. 3, Tacoma 3, Wash.

SMITH, Lawrence J. (*M* 1943) Dir. of Research, Bell & Gossett Co., 8200 N. Austin Ave., Morton Grove, and ● 455 Lenox St., Oak Park, Ill.

SMITH, Lloyd W. (*S* 1946) Student, Texas A. & M. College, P. O. Box 2534, College Station, Texas.

SMITH, Milton S. (*M* 1919) Vice-Pres. and Treas., Buensod-Stacey, Inc., 60 East 42nd St., New York 17, N. Y., and ● 13 N. Terrace, Maplewood, N. J.

SMITH, Norman A. (*A* 1944) Mgr., ● Norman A. Smith Co., 96 Vine Ave., Toronto 9, and 269 Willard Ave., Toronto, Ont., Canada.

SMITH, Oliver F., Jr. (*J* 1944) Mech. Engr., Wertz Engineering Co., 441 N. Second St., Reading, and ● 1521 Delaware Ave., Wyomissing, Pa.

SMITH, Oscar L. (*A* 1947) Sales Engr., McDowell Heating & Cooling Corp., 3603-05 Kienlen Ave., St. Louis 20, and ● 5736 Neosho St., St. Louis 9, Mo.

SMITH, Owen J. (*A* 1946) Assoc., Verne Simmonds Co., and ● 3204 Fontenelle Blvd., Omaha, Nebr.

SMITH, Robt. W. (*A* 1947) Pres., ● Robt. W. Smith & Co., Ltd., 85 Vitre St. W., and 3535 Benny Ave., N. D. G., Montreal, Que., Canada.

SMITH, Roger C. (*A* 1940) Asst. Branch Engr., York Corp., 119 South 11th St., St. Louis 2, and ● 217 N. Meramec Ave., Clayton 5, Mo.

SMITH, Roger K. (*M* 1942) School of Engrg., The University of Buffalo, Buffalo, N. Y.

SMITH, Russell B. (*A* 1945) ● Hunter-Prell Co., 15 E. Jackson St., and 96 Greenwood, Battle Creek, Mich.

SMITH, Russell H. (*M* 1945) Prop., ● Russell H. Smith Equipment Co., 5 E. Long St., Columbus 15, and 560 Arden Rd., Columbus 2, Ohio.

SMITH, Russell J. (*M* 1944) Pres., Russell J. Smith, Inc., ● 1601 S. Grand Blvd., St. Louis 4, and 7707 Lile Ave., St. Louis 17, Mo.

SMITH, Sidney T. (*J* 1941) Partner, ● Sid Smith & Co., 411 W. Fifth St., and 2123 W. Third St., Waterloo, Ia.

SMITH, Stanley K. (*M* 1945) Pres., ● The H. B. Smith Co., Inc., 57 Main St., Westfield, and 33 Colony Rd., Springfield 6, Mass.

SMITH, Stelle, Jr. (*A* 1948) Pres., ● Stellco, Inc., 411 Washington S., and 3015 E. Calhoun Blvd., Minneapolis, Minn.

SMITH, Stuart (*A* 1936) Dist. Mgr., Reynolds Metal Co., 19 East 47th St., New York, and ● 593 Manor Lane, Pelham 65, N. Y.

SMITH, Ulysses G. (*A* 1947) Owner ● U. G. Smith Electric & Manufacturing Co., 6518 N. Denver, and 6556 N. Greenwich Ave., Portland 3, Ore.

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SMITH, Walter H. (*M* 1939) Chief Engr., The T. Eaton Co., Ltd., 190 Yonge St., Toronto, and • Box 31, Islington, Ont., Canada.
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SMITH, W. O. (*A* 1937) Owner, Midland Heating Specialties Co., 19254 John R, Detroit 3, Mich.
SMITHERS, Theodore (*J* 1948; *S* 1947) Engr., Curt Collins Co., 521 W. Exchange, Akron, and • 2029 11th St., Cuyahoga Falls, Ohio.
SMOOT, Charles B. (*M* 1942) Engr., • Maurice H. Connell & Assocs., Langford Bldg., Miami, and 1217 Ave., Venetia, Coral Gables 34, Fla.
SMOOT, T. H. (*M* 1935) Vice-Pres., Anchor Post Products, Inc., 151 N. Haven St., Baltimore 24, and • 1302 Southview Rd., Baltimore 18, Md.
SMYERS, Edward C. (*A* 1933) Sales Engr., Barber-Colman Controls, 1013 Penn Ave., Wilkinsburg, and • 148 Jamaica Ave., West View, Pittsburgh, Pa.
SMYTH, George E. (*A* 1944) Field Engr., Consolidated Conditioning Corp., 26 West 47th St., New York, N. Y., and • 329 Central Ave., Hawthorne, N. J.
SNAVELY, A. Bowman (*M* 1937) Chief Engr., Hershey Chocolate Corp., Hershey, Pa.
SNAVELY, Earl R. (*M* 1937) Sales Mgr., Instrument Div., Thomas A. Edison, Inc., West Orange and • Parkway Dr., Rt. 3B37, Clark, Rahway, N. J.
SNIDER, Clay T. (*M* 1947) Sales Engr., Minneapolis-Honeywell Regulator Co., 1136 Howard St., San Francisco, and • 240 S. Seventh St., Richmond, Calif.
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SNOW, David (*M* 1946) Mfrs. Agent, • Peerless of America, Inc., 233 Broadway, New York 7, N. Y., and 111 Glen Ave., Maplewood, N. J.
SNOW, Edward E. (*M* 1945) Chief Designer and Engr., Mellor Bromley & Co., Ltd., St. Saviours Rd., and • 32 Spencefield Lane, Evington, Leicester, England.
SNOW, Ralph C. (*J* 1947) Sales Engr., English & Lauer, Inc., 1978 S. Los Angeles St., Los Angeles 11, and • 9509 Goebel Ct., Los Angeles 45, Calif.
SNYDER, Edwin F., Jr. (*A* 1946; *J* 1940) Htg. Engr., Minneapolis-Honeywell Regulator Co., 2753 Fourth Ave. S., and • 4324 Zenith Ave. N., Minneapolis 12, Minn.
SNYDER, Edwin J. (*J* 1944; *S* 1943) Jr. Engr., • Wylie Plumbing & Heating Co., 2047 Pennsylvania Ave., Baltimore 17, and 3903 Dolfield Ave., Baltimore 15, Md.
SNYDER, Jay W. (*M* 1917) Member of Firm, • Snyder & McLean, 2214 Penobscot Bldg., Detroit, and 15810 Asbury Park, Detroit 27, Mich.
SNYDER, L. R. (*A* 1944) L. R. Snyder Co., and • 7034 Lakewood Blvd., Dallas 14, Texas.
SNYMAN, G. C. (*A* 1941) Mgr., Overseas Div., • Celotex Corp., 120 S. LaSalle St., Chicago 3, and Evanshire Hotel, Evanston, Ill.
SOBEL, Frank (*S* 1939) Pvt., U. S. Army, and • 115 Post Ave., New York, N. Y.
SOCKWELL, Charles, Jr. (*A* 1942) Partner, Sockwell Co., 156 Rogers St. N.E., and • 2562 Boulevard Dr. N.E., Atlanta, Ga.
SOCKWELL, Charles, Sr. (*M* 1942) Partner, Sockwell Co., 156 Rogers St. N.E., Atlanta, and • 5447 Roswell Rd., Dunwoody, Ga.
SOCKWELL, Tyrus R. (*A* 1942) Partner, • Sockwell Co., 156 Rogers St. N.E., and 372 Morgan Pl. S.E., Atlanta, Ga.
SODEMANN, William C. B. (*Life Member*; *M* 1919) Pres., • Sodemann Heat & Power Co., 2306 Delmar Blvd., St. Louis, and 7542 Teasdale Ave., University City, Mo.
SODERBORG, G. Lloyd Sr. (*A* 1946) Mgr., • Engineering Sales Co., 35 Post Office Pl., and 250 Truman Ave., Salt Lake City, Utah.
SOLSTAD, Lester L. (*A* 1945; *J* 1936) Mgr., Austin Sheet Metal Works, 5109 W. Chicago Ave., Chicago 51, and • 1649 N. Oak Park Ave., Chicago 35, Ill.
SOMERS, William S. (*M* 1938) Engr., Armco Industrial & Commercial, Caixa Postal 19, Rio de Janeiro, Brazil.
SOMMERFIELD, Sumner S. (*M* 1948; *A* 1941; *J* 1936) Mech. Engr., Kroeschell Eng. Co., 215 W. Ontario St., Chicago, and • 1913 Indiana St., Wheaton, Ill.
SOMMERS, William J. (*M* 1937) Dist. Repr., • Ilg Electric Ventilating Co., 505 Delaware Ave., Buffalo 2, and 235 Hartford Ave., Kenmore 17, N. Y.
SONTAG, Harcourt C. (*M* 1947) Head, Htg., Vent. & De-Icing Sect., Bureau of Aeronautics, Navy Dept., Washington, D. C., and • 4717 37th St. N., Arlington, Va.
SOPER, Horace A. (*M* 1916) Pres., • American Foundry & Furnace Co., Washington at McClun, and 1122 E. Monroe St., Bloomington, Ill.
SORENSEN, Edward (*A* 1947) Mech. Engr., Keller & Gannon, 369 Pine St., San Francisco, and • 1548 Jasmine St., San Mateo, Calif.
SORMANE, Walter (*A* 1944) Gen. Sales Mgr., Conco Engineering Works, and • 912–13th Ave., Mendota, Ill.
SORONEN, Robert C. (*A* 1947) Htg. & Vtg. Engr., D. J. Murray Manufacturing Co., 1002-24 Third St., and • 206 Grant St., Wausau, Wis.
SOULE, John P. (*J* 1942) Mech. Engr., • Modine Manufacturing Co., 101 Park Ave., New York, N. Y., and Gordon Rd., Essex Fells, N. J.
SOULE, Lawrence C.* (*Life Member*; *M* 1908) Secy. and Cons. Engr., Aerofin Corp., Syracuse, N. Y., and • Gordon and Stewart Rds., Essex Fells, N. J.
SPAAN, John H., Jr. (*M* 1945) Mgr., J. M. O'Connor Co., 1633 N.W. Fifth St., Oklahoma City 4, and • 1303 N. Klein, Oklahoma City 6, Okla.
SPALL, Edward G. (*A* 1939) Vice-Pres., • Perfex Controls, Ltd., 73 Simcoe St., Toronto 1, and 291 Windermere Ave., Toronto 3, Ont., Canada.
SPANTON, Milton D. (*A* 1947) Mgr., Plbg. & Htg. Dept., • Coast-to-Coast Stores, 29 S.E. Main St., and 335 West 49th St., Minneapolis, Minn.
SPARKS, James D. (*M* 1944; *A* 1937) Northwest Repr., Ilg Electric Ventilating Co., 7331 W. Green Lake Way, Seattle 3, Wash.
SPEARS, Joe M., Jr. (*S* 1946) Student, • Texas A. & M. College, Box 72, College Station, and 407 S. College Ave., Bryan, Texas.
SPECKMAN, Charles H. (*Life Member*; *M* 1918) Cons. Htg. and Vent. Engr., • 382 Philadelphia Bourse Bldg., Philadelphia 6, and 1217 S. Fourth St., Philadelphia, Pa.
SPEER, Julian (*A* 1944) Mgr., • Julian Speer Co., 101 N. High St., and 101 N. Ridge Rd., Columbus, Ohio.
SPELLER, Frank N.* (*Life Member*; *M* 1908) Metallurgical Consultant, 6411 Darlington Rd., Pittsburgh 17, Pa.
SPENCE, Morton R. (*A* 1942; *J* 1934) Vice-Pres., • Rundle & Spence Manufacturing Co., 445 N. Fourth St., and 709 E. Lexington Blvd., Milwaukee, Wis.
SPENCE, Robert A. (*A* 1946; *J* 1937) Mech. Engr., • Harvard University, Lehman Hall, Cambridge 38, and 33 Barnard Rd., Belmont 78, Mass.
SPENCER, Charles H. (*M* 1944) Factory Agent, Sales and Service Engr., 1421 S. Main St., Salt Lake City 4, Utah.
SPENCER, Roland M. (*M* 1945; *A* 1940; *J* 1938) Dist. Sales Mgr., • The Powers Regulator Co., 3819 N. Ashland Ave., Chicago 13, and 7315 Lunt Ave., Chicago 31, Ill.
SPENCER, Scott A. (*M* 1947) Engr., • Edward E. Ashley, 10 East 40th St., New York, and Hickory Kingdom Rd., Bedford Village, N. Y.
SPENCER, Warner E. (*A* 1938) Repr., • National Radiator Co., 241 S. Elmwood Ave., Buffalo 2, and 212 Bidwell Pkwy., Buffalo, N. Y.
SPERRY, Harvey A. (*A* 1947) Steam & Hot Water Inspector, City of Minneapolis, 213 City Hall, Minneapolis 15, and • 2755 Pierce St. N.E., Minneapolis 13, Minn.
SPIEGEL, Daniel (*J* 1948) Engr., Consolidated Conditioning Corp., 26 West 47th St., New York, and • 100 Neptune Ave., Woodmere, N. Y.
SPIELMANN, Gordon P. (*A* 1931; *J* 1923) Owner, • Harrison-Spielmann Co., 480 Milwaukee Ave., Chicago 10, and 730 N. Prospect Ave., Park Ridge, Ill.

SPIETH, Benjamin (*M* 1941) Chief Engr., ● Modine Manufacturing Co., and 400 Harvey Dr., Racine, Wis.

SPITZ, Nathaniel (*J* 1945) Head of Sales and Installation, ● City Coal Co., 410 Bank St., and 300 Ocean Ave., New London, Conn.

SPITZLEY, Joseph H. (*A* 1948; *J* 1943) Vice-Pres., ● R. L. Spitzley Heating Co., 1200 Fort St. W., Detroit 26, and 11 Farrand Park, Highland Park, Mich.

SPITZLEY, Ray L. (*A* 1944) Inspector of Refineries, Class B, General Petroleum Corp., Torrance, and ● 11542 Rochester, West Los Angeles 25, Calif.

SPITZLEY, R. L. (*M* 1920) Pres. and Gen. Mgr., ● R. L. Spitzley Heating Co., 1200 W. Fort St., Detroit 26, and 26 Renaud Rd., Grosse Pointe Shores 30, Mich.

SPOERR, Frank F. (*A* 1942; *J* 1937) Sales Engrg., Carrier Corp., Marine Dept., 405 Lexington Ave., New York, and ● 21 Willow Ave., Hempstead, L. I., N. Y.

SPOFFORTH, Walter (*M* 1930) Mech. Engr., U. S. Navy, Drake Puget Sound, Seattle, and ● 15248 Maplewild Ave., Seattle 66, Wash.

SPRAGUE, George W. (*A* 1947) Mgr., Moduflow Dept., Minneapolis-Honeywell Regulator Co. 799 Beacon St., Boston, and ● 16 Curtis St., Marblehead, Mass.

SPRAGUE, Kenneth T. (*A* 1948) Dist. Repr., Bell & Gossett Co., and ● 1431 Teall Ave., Syracuse 6, N. Y.

SPRIGGS, Carl U. (*A* 1945) Asst. Sales Mgr., Carrier Corp., Syracuse, and ● 101 Hampshire Rd., Syracuse 3, N. Y.

SPRINGER, J. J. (*A* 1945) Owner, ● Oneida Supply Co., 157-159 Cedar St., and 506 Broad St., Oneida, N. Y.

SPROTT, John I. (*A* 1941) Sales Engr., ● Ray Oil Burner Co., 401 Bernal Ave., and 70 Crestlake Dr., San Francisco, Calif.

SPROULL, Howard E. (*M* 1920) Div. Sales Mgr., ● American Blower Corp., 1005-6 American Bldg., Cincinnati 2, and 3588 Raymar Dr., Cincinnati 8, Ohio.

SPURGEON, Joseph H. (*M* 1924) Mfrs. Agent, ● Spurgeon Co., 5050 Joy Rd., Detroit 4, and 17215 Pennington Dr., Detroit 21, Mich.

SPURLOCK, Benjamin H., Jr. (*M* 1944) Prof., Dept. of Mech. Engrg., University of Colorado, Boulder, Colo.

SPURNEY, F. E. (*A* 1938) Branch Mgr., Butler Manufacturing Co., 1127 Barr Bldg., Washington 6, D. C., and ● 28 W. Baltimore St., Kensington, Md.

SQUIER, Ralph T. (*M* 1947) Asst. Dir. of Research, Minneapolis-Honeywell Regulator Co., 2753 Fourth Ave. S., Minneapolis, and ● 3351 Colfax Ave. S., Minneapolis 8, Minn.

STACEY, Alfred E., Jr.* (*M* 1914), (2nd Vice-Pres., 1947; Council 1941-44; 1947) Process Consultant, Carrier Corp., 300 S. Geddes St., Syracuse, and ● 41 Academy St., Skaneateles, N. Y.

STACK, A. E. (*A* 1935) Lab. Supt., Washington Gas Light Co., 11th and H Sts. N.W., Washington 5, D. C., and ● 7911 Chicago Ave., Silver Spring, Md.

STACY, Stanley C. (*M* 1931) Mech. Engr., ● Board of Education, 13 S. Fitzhugh St., Rochester 4, and 111 Valley Rd., Rochester 10, N. Y.

STAFFORD, J. Fuller (*A* 1938) Owner, 519 N. Snelling Ave., St. Paul 4, and ● 4545-18th Ave. S., Minneapolis 7, Minn.

STAFFORD, Thomas D. (*M* 1947; *A* 1937) Vice-Pres. and Mgr., ● Alexander-Stafford Corp., 1 Ionia Ave. N.W., and 954 Ogden Ave. S.E., Grand Rapids, Mich.

STAHL, W. A. (*M* 1938) Supt., ● Merchandise Mart, 222 Bank Dr., Chicago 54, and 2504 Harrison St., Evanston, Ill.

STAINS, W. A. (*M* 1945) Cons. Mech. & Elec. Engr., 521 E. Valencia Ave., Burbank, Calif.

STALEY, Martin E. (*M* 1946) Cons. Mech. Engr., ● 31 Chandler Bldg., San Antonio 5, and 128 Perry Ct., San Antonio 2, Texas.

STAMBERGER, Robert F. (*A* 1944) Estimator and Supt., The Stamberger Co., 3115 Mayfield Rd., and ● 2289 Lamberton Rd., Cleveland Heights, Ohio.

STAMMER, E. L. (*Life Member*; *M* 1919) Retired, 7046 Winona, St. Louis 11, Mo.

STAMPS, Harold F. (*A* 1946) Field Engr., Henry Valve Co., 3260 W. Grand Ave., Chicago 51, and ● 2118 S. Tenth Ave., Maywood, Ill.

STANDRING, Ronald A. (*A* 1942; *J* 1938) Mgr., Domestic Burner Div., Vipond-Tolhurst, Ltd., 845 Querbes Ave., Outremont, and ● 2358 Leclaire St., Montreal, Que., Canada.

STANEK, Edward W. (*A* 1947) E. J. Stanek, Htg. Contr., 13804 Kinsman Rd., and 13802 Kinsman Rd., Cleveland 20, Ohio.

STANGER, R. B. (*M* 1920) Prop., ● Robinson & Stanger, Empire Bldg., Pittsburgh 22, and Middle Rd., Glenshaw, Pa.

STANGER, William F. (*M* 1945) Sales Engr., Robinson & Stanger, 1005 Empire Bldg., Pittsburgh 22, and ● 337 S. Millvale Ave., Pittsburgh 24, Pa.

STANLEY, Robert L. (*M* 1938) Field and Research Engr., Naco Manufacturing Co., 7631 Roseberry Ave., Huntington Park, and ● 9223 Seventh Ave., Inglewood, Calif.

STANSBURY, Edward J., Jr. (*A* 1947) Sales & Estimating Engr., ● Mundet Cork Corp., P. O. Box 1443, and 1234 Tulane, Houston, Texas.

STARK, J. Emil (*A* 1947) Estimator, Wray M. Scott Co., Inc., and ● 1518 S. Tenth St., Omaha, Nebr.

STARK, Roscoe C. (*S* 1948) Student, University of Michigan, Ann Arbor, and ● 1770 Quincy Ct., Willow Run, Mich.

STARRETT, Forrest W. (*A* 1946) Sales Engr., Knight-Randall Co., 8316 Woodward, Detroit 2, and ● 13145 Maiden Ave., Detroit 13, Mich.

STEADMAN, Clifford C., Jr. (*A* 1947) ● The Bahnson Co., 1001 S. Marshall St., and 146 Taylor St., Winston-Salem, N. C.

STEARNS, Ellis J., Jr. (*M* 1944) Engr., National Bureau of Standards, Washington, D. C., and ● 933 Parker St., Falls Church, Va.

STECKHAN, Louis (*M* 1941) Sales Engr., ● Crane Co., 30 South 16th St., St. Louis 3, and 3240 Liberty St., St. Louis 11, Mo.

STEELE, Harris S. (*J* 1948; *S* 1947) Engr., Jarcho Bros., Inc., 304 East 45th St., New York, and ● 227 Hopkins St., Brooklyn 6, N. Y.

STEELE, J. B. (*M* 1932) Chief Operating Engr., Winnipeg School District No. 1, Ellen and William Ave., and ● 184 Waterloo St., R. H., Winnipeg, Man., Canada.

STEEVES, Donald R. (*A* 1944) Owner, Steevesway Heat, 301 MacPherson Ave., and ● Apt. 405, 3110 Yonge St., Toronto, Ont., Canada.

STEFFNER, Edward F. (*A* 1937; *J* 1934) Partner, Residential Heating Service, 1429 East 133rd St., East Cleveland 12, Ohio.

STEGGALL, Howard B. (*M* 1942; *A* 1934) Vice-Pres., United States Radiator Corp., 300 Buhl Bldg., Detroit, and ● Wilson Rd., Bloomfield Hills, Mich.

STEILEN, Louis J. (*M* 1946) Chief Engr., Lehigh Engineering Co., 1150 Mauch Chunk Rd., Bethlehem, and ● 205 Pennypack Circle, Hatboro, Pa.

STEIN, Jerome (*J* 1942; *S* 1940) Secy., Torrington Supply Co., Inc., 125 Maple St., and ● 756 Waterville St., Waterbury, Conn.

STEIN, Samuel C. (*J* 1948; *S* 1947) Drying Systems, Inc., 1800 Foster Ave., Chicago, Ill., and ● 20 Ashton Rd., Yonkers 5, N. Y.

STEIN, William (*M* 1946) Chief Engr., Indus. Stoker Div., Combustion Engineering Co., 200 Madison Ave., New York 16, and ● 2207 East 29th St., Brooklyn 29, N. Y.

STEINKE, Bernard J. (*A* 1948; *J* 1940; *S* 1937) Supvsr. Engr., ● U. S. Rubber Co., Maple St., Naugatuck, and 261 Peach Orchard Rd., Waterbury 82, Conn.

STEINMETZ, C. W. A. (*M* 1934) Mgr., Marine and Export Dept., ● American Blower Corp., 50 West 40th St., New York 18, N. Y., and 50 Oakwood Ave., Bogota, N. J.

STELL, William H., Jr. (*M* 1944) Owner, ● Arnold R. Kamman Co., 493 Franklin St., Buffalo 2, and 648 Clay Ave., Rochester 13, N. Y.

STEMPEL, Edward H. (*M* 1942) Consultant, and 268 E. Market St., York, Pa.

STENCEL, R. A. (*M* 1938) Chief Engr., Canadian Ice Machine Co., Ltd., 65 Villiers St., and ● 224 Inglewood Dr., Toronto, Ont., Canada.

STENGEL, Frank J. (*A* 1935) 39 Walnut Ave., Millburn, N. J.

STENN, Sherwin (*S* 1947) 209 Mech. Engrg. Lab., University of Illinois, Urbana, Ill.

STEPAN, Theodore E. (*M* 1946) Mech. Engr., • Mississippi River Commission, Box 80, and 2922 Cherry St., Vicksburg, Miss.

STEPHEN, Charles O. (*A* 1945) Owner, • Stephen & Lambert, 128 E. Fifth, and 1925 Greenwood, Pueblo, Colo.

STEPHENSON, James H. (*A* 1946) Sales Engr., • Johnson Service Co., 1309 Anita St., Houston 4, Texas.

STEPHENSON, J. R. (*A* 1940) • J. R. Stephenson & Co., 278 Main St., and 647 Strathcona St., Winnipeg, Man., Canada.

STEPHENSON, Kiser A. (*M* 1941) Pres., • Stephenson Co., 125 Merritts Ave. N.E., and 923 St. Charles Ave. N.E., Atlanta, Ga.

STERMER, Clarence J. (*M* 1936) Engr., Crane Co., 836 S. Michigan Ave., and • 7839 Clyde Ave., Chicago 49, Ill.

STERN, Edward J. (*A* 1941) Dist. Mgr., • Armstrong Cork Co., 701 Burt Bldg., Dallas 1, and 223 E. Davis St., Dallas 8, Texas.

STERN, Lester M. (*J* 1945; *S* 1944) Engr., Cleveland Pneumatic, 3718 East 77th, and • 1062 Carlyon Rd., East Cleveland 12, Ohio.

STERN, Richard M. (*A* 1946) Mech. Engr., Victor N. Jones & Assocs., 706 Republic Bldg., Seattle 1, and • 6227 Vassar Ave., Seattle 5, Wash.

STERNBERG, Edwin (*A* 1932; *J* 1931) Design Engr., Fred Moesel Assoc., 101 Park Ave., and • 16 East 98th St., New York, N. Y.

STERNE, C. M. (*M* 1943; *A* 1934) Chief Engr., Metropolitan Refining Co., 50-23 23rd St., Long Island City 1, N. Y.

STERNER, Douglas S. (*M* 1941; *A* 1940; *J* 1936) Sales Engrg., York Corp., 907 Florida Bank Bldg., and • 8 E. Vanderbilt Ave., Orlando, Fla.

STERRY, H. Lee (*A* 1945) Dir. of Business Research, • Carrier Corp., and 308 Gordon Ave., Syracuse, N. Y.

STEVENS, Earl Knights (*A* 1940) International Exposition Co., 480 Lexington Ave., New York 17, N. Y.

STEVENS, Francis D. (*M* 1947) Chief Engr., • Refrig. Div., Noma Electric Corporation of Md., Barber, and 113 Market St., Perth Amboy, N. J.

STEVENS, Harold C. (*A* 1947) • Hunter Clark Ventilating System Co., 2800 Cottage Grove Ave., Chicago 16, and 4837 Kimbark Ave., Chicago 15, Ill.

STEVENS, Harry L. (*M* 1934; *A* 1927; *J* 1924) Pres., • M. M. Stevens Co., 108-110 W. Sherman St., and 320 West 20th Ave., Hutchinson, Kans.

STEVENS, Howard R. (*M* 1941) Owner, Stevens Heating & Supply Co., 225 E. Fourth St., Reno, Nev.

STEVENS, Howard Riley (*J* 1946) Air Cond. Foreman, Allison Division, General Motors Corp., Indianapolis, and • 638 N. Livingston Ave., Indianapolis 8, Ind.

STEVENS, Joseph W. (*M* 1944) Dir. of Sales, Cyclotherm Corp., 90 Broad St., New York 4, and • 303 Maple Rd., Syracuse 9, N. Y.

STEVENS, Judson E. (*A* 1941) Vice-Pres., • Superior Sheet Metal Works, Inc., 318 and 328 Spokane St., and 39 520 Vassar St., P. O. Box 2542, Reno, Nev.

STEVENS, Kenneth M. (*A* 1943; *J* 1936) Branch Mgr., • The Powers Regulator Co., 1510 Main St., and 5728 Cherry, Kansas City 6, Mo.

STEVENS, Stanley A. (*A* 1945) Engr., • Matthew Hall & Co., Ltd., 28 Dorset Sq., and 30A Falloden Way, Golders Green, London N.W. 11, England.

STEVENS, T. Robert (*A* 1947) Htg. Engr., • Sarcotherm Controls, Inc., 2922 Empire State Bldg., New York, and 3611–31st Ave., Long Island City 3, N. Y.

STEVENS, Wayne H. (*A* 1939) Engr., • Shellenberger, Gregg & Co., 2211 N. Prospect Ave., Milwaukee 2, and 2521 E. Stratford Ct., Milwaukee 11, Wis.

STEVENS, William B. (*A* 1944) Owner, • Stevens Furnace Co., 79 S. LaSalle St., and 65 S. View St., Aurora, Ill.

STEVENS, William R. (*A* 1934) Partner, • L. E. Stevens Co., 626 Broadway, Cincinnati 2, Ohio, and 30 Chalfonte Ct., Ft. Thomas, Ky.

STEVENSON, Daniel B., Jr. (*M* 1946) Engr., The Austin Co., 510 N. Dearborn, Chicago, Ill., and • Lumberton, Miss.

STEVENSON, Mel J. (*M* 1935) Cons. Engr., Indus. Multi-Vent Div., The Pyle-National Co., 1334 N.Kostner Ave., Chicago 51, and • 2970 N. Sheridan Rd., The Wellington Arms, Apt. 805, Chicago 14, Ill.

STEVENSON, W. W. (*M* 1928) Steam Htg. Engr., • Allegheny County Steam Heating Co., 435 Sixth Ave., Pittsburgh 19, and 1125 Lancaster Ave., Pittsburgh 18, Pa.

STEWART, Charles W. (*M* 1919; *A* 1918) Vice-Pres., Sales, • Clark Manufacturing Co., 1830 East 38th St., Cleveland 14, and 2487 Noble Rd., Cleveland Heights, Ohio.

STEWART, Clement W. (*M* 1944) Marine Specialist, Ilg Electric Ventilating Co., 15 Park Row,—1108, New York 7, N. Y., and • 828 Fifth Ave., River Edge, N. J.

STEWART, Duncan J.* (*M* 1936; *A* 1930) Vice-Pres. and Gen. Mgr., • Barber-Colman Co., Drawer 99, and R. R. 4, Rockford, Ill.

STEWART, Irll A. (*A* 1945) Mech. Engr., Chief, Refrig. and Vent. Unit, • Headquarters Army Engineer, Sixth Army, Bldg. No. 35, Room 222, Presidio of San Francisco, and 350 South 43rd St., Apt. 2-F, Richmond, Calif.

STEWART, James P. (*A* 1940; *J* 1937) Engr., Carrier Corp., 300 S. Geddes St., Syracuse, and • 224 Greenwood Pl., Syracuse 10, N. Y.

STEWART, John L. (*A* 1944) Gen. Mgr. and Vice-Pres., • Calif.-Fresno Supply Co., P. O. Box 1186, and 1334 Floradora, Fresno, Calif.

STEWART, John N. (*A* 1939) Plan Examiner, District of Columbia, 102 District Bldg., and • 6124–32nd Pl. N.W., Washington 15, D. C.

STEWART, Ralph M. (*A* 1945) Mgr., Vice-Pres., • Bryant Gas Heating Co., 824 Marquette Ave., and 26 West 22nd St., Apt. 309, Minneapolis, Minn.

STEWART, Wesley O. (*M* 1944; *A* 1938) Branch Mgr., • Johnson Service Co., 412 East 11th St., Los Angeles 15, and 4100½ Los Feliz Blvd., Los Angeles, Calif.

STICKLE, Fred A. (*A* 1945) Pres. and Gen. Mgr., Stickle Steam Specialties Co., 2215 Valley Ave., Indianapolis 1, and • 2339 Broadway St., Indianapolis 5, Ind.

STICKRATH, Kenneth J. (*A* 1945) Owner, 316 Shaw Ave., and 2821 Capital St., McKeesport, Pa.

STILES, Gordon S. (*A* 1941; *J* 1936) Engr., • Geo. B. Mallory Co., 1436 Blackstone, and 4611 Home, Fresno, Calif.

STILLER, F. W. (*A* 1945) 4501 S. Aldrich, Minneapolis 9, Minn.

STILPHEN, Norman E. (*M* 1945) Owner, • Stilphen Engineering Co., 26 Roberts St., and 253 Main St., Sanford, Me.

STIMSON, DeParx (*M* 1945) Pres., Stimson Engineering Corp., Dir. of Tech. Sales, The Bahnson Co., and • 121 Idlewilde Dr., Winston-Salem, N. C.

STINARD, Rutherford L. (*M* 1946) Cons. Engr., 6209 Boulevard E., West New York, N. J.

STIPP, Roy A. (*M* 1946) Mfrs. Repr., • Buffalo Forge Co., P. O. Box 1796, 21 Blue Bldg., and 1 Longview Terrace, Greenville, S. C.

STITES, Richard, Jr. (*A* 1943; *J* 1937) Sales Engr., • Coon Devisser Co., 2051 W. Lafayette, Detroit 16, and 17537 Hartwell, Detroit 21, Mich.

ST. LAURENT, Guy (*A* 1942) Htg. Contr., • Hector Groulx, Engrg., 7375 Chambord St., and 8381 Drolet St., Montreal, Que., Canada.

STOBBE, Gustav C. (*A* 1944) Gen. Supt., Becker-Seidel-Clark Co., 4500 Euclid Ave., Cleveland 3, and • 1805 Tampa Ave., Cleveland 9, Ohio.

STOCK, Charles S. (*M* 1936) Gen. Sales Mgr., The Herman Nelson Corp., 1824 Third Ave., Moline, Ill., and • R. R. 1, Bettendorf, Ia.

STOCKWELL, William R. (*Life Member*; *M* 1903; *J* 1901) Gen. Mgr., Mfg. Div., Weil-McLain Co., Michigan City, Ind.

STOFFER, Glen H. (*M* 1945) Branch Dealer Mgr., • Carrier Corp., 950 Dierks Bldg., Kansas City 6, and 20 West 36th St., Kansas City 2, Mo.

STOKES, Alvin D. (*M* 1936) Gen. Supt., Riggs Distler & Co., Inc., 216 N. Calvert St., Baltimore, and • 424 Winston Ave., Baltimore 12, Md.

STOKES, Thomas A. (*M* 1946) Air Cond. Engr., • Cary B. Gamble & Assocs., 314½ St. Charles St., and 7521 Plum St., New Orleans, La.

STOKLEY, John M. (*A* 1946) Pres., ● Stokley's Services, Inc., 4000 Colley Ave., and 7438 Hampton Blvd., Norfolk, Va.
STOLBERG, Charles P. (*M* 1947) Chief Mech. Engr., ● The H. K. Ferguson Co., Ferguson Bldg., Cleveland 14, and 3613 Lynnfield Rd., Shaker Heights 22, Ohio.
STOLKER, Edward A. (*A* 1945) Owner, ● Stolker Engineering Co., 4201 Brown St., Philadelphia 4, and 2601 Parkway 30, Philadelphia, Pa.
STONE, A. A. (*A* 1943) Branch Mgr., Mundet Cork Corp., 505 Southland Life Annex, Dallas 1, and ● 601 Second Ave., Dallas 10, Texas.
STONER, Dean W. (*A* 1948) Sales Repr., ● Kewanee Boiler Corp., 2014-20 Wyandotte St., and 412 West 47th St., Kansas City, Mo.
STONER, William C. (*A* 1944) Moore-Stoner Co., 500 Stewart Ave. S.W., Atlanta, Ga.
STOREY, J. H. (*M* 1944) Pres., ● John Tweddle, Ltd., 80 Jean Talon St. W., and 452 Carlyle Ave., Town of Mt. Royal, Montreal, Que., Canada.
STORMS, Robert M. (*M* 1936) Partner, Storms & Lowe, 6381 Hollywood Blvd., Los Angeles 28, and ● 354 W. Wilson Ave., Glendale 3, Calif.
STOTESBURY, Bernard (*M* 1942) Partner, Ottawa Plumbing & Heating Contractors, 111 Third Ave., Ottawa, Ont., Canada.
STOTT, Douglas A. (*A* 1940) Mgr., ● The Powers Regulator Company of Canada, Ltd., 195 Spadina Ave., Toronto, and 30 MacNaughton Rd., Leaside, Ont., Canada.
STOTT, F. W. (*M* 1938) Branch Sales Mgr., C. A. Dunham Co., Ltd., 1139 Bay St., Toronto, and ● Thomas St., Oakville, Ont., Canada.
STOTZ, Robert Bertan (*A* 1946) Field Engr., Chrysler Airtemp Sales Corp., 404 Citizens & Southern Bank Bldg., Atlanta 3, and ● 308 Merritt St., Apt. A, Marietta, Ga.
STOUT, Arthur G. (*M* 1943) Owner, Cons. Engr., ● Arthur G. Stout & Assocs., 400 W. Madison St., Chicago 6, and 105 East Ave., Park Ridge, Ill.
STOVER, Rolland S. (*A* 1944) Owner, ● R. S. Stover Co., Kresge Bldg., and 207 N. Eighth St., Marshalltown, Ia.
STOVER, Warren H. (*A* 1946) Dist. Mgr., Air Cond. Dept., ● General Electric Co., P. O. Box 909, Portland 7, and 6116 Northeast 21st Ave., Portland, Ore.
STRACHAN, George W. (*M* 1945) Project Engr., Dravo Corp., 300 Penn Ave., Pittsburgh, and ● 1848 Hillsdale Ave., Pittsburgh 16, Pa.
STRACKE, Samuel L. (*J* 1947; *S* 1946) Engr., ● Valley Weathermakers, Inc., 607 W. Harrison St., Harlingen, and 3019 Windsor Ave., Waco, Texas.
STRAHAN, James L. (*M* 1946) Tech. Dir., ● Asphalt Roofing Industry Bureau, 2 West 45th St., New York, and Larchmont Acres, Apt. 221-C, Larchmont, N. Y.
STRAIN, Andrew James (*A* 1942) Gen. Mgr., ● Ruud Manufacturing Co., 474 Bathurst St., Toronto 2B, and 376 St. Clements Ave., Toronto 12, Ont., Canada.
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TURNER, George W. (*M* 1944) Mgr., • George B. Mallory Co., 1436 Blackstone Ave., and 203 Shields, Fresno, Calif.

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TURNER, John P., Jr. (*M* 1942) Field Sales Mgr., Air Cond. Dept., • General Electric Co., 5 Lawrence St., Bloomfield, and 727 Mosswood Ave., Orange, N. J.

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WELLS, Edward E. (*M* 1941) Gen. Engrg. Dept., Aluminum Company of Canada, Ltd., 1700 Sun Life Bldg., Montreal, and • 6 St. John Rd., Pointe Claire, Montreal 33, Que., Canada.

WELLS, William F.* (*M* 1939) Dir. of Lab. for Study of Air-Borne Infection, • University of Pennsylvania, Medical School, Philadelphia, and 112 Pine Ridge Rd., Media, Pa.

WELSHMAN, Hugh, Jr. (*M* 1946) Mgr., Indus. Piping Div., • Grinnell Co., Inc., 260 W. Exchange St., Providence, and 12 Woodford Rd., Barrington, R. I.

WELTER, Gustave (*M* 1946) Vice-Pres. and Chief Engr., • The Bigelow Co., P. O. Box 706, New Haven 3, Conn.

WEMPE, Robert H. (*A* 1948) Engr., McCarty Bros. Equipment Corp., • 7801 Lake St., River Forest, and 914 Sherman Ave., Evanston, Ill.

WENDEL, Frederick E. (*A* 1947) Owner, • Fred Wendel, Piping Contr., First National Bank Bldg., 617 Oradell Ave., and 442 Third St., Oradell, N. J.

WENDT, Edgar F. (*M* 1918) Pres., • Buffalo Forge Co., 490 Broadway, and 120 Lincoln Pkwy., Buffalo, N. Y.

WENDT, Edwin H. (*A* 1942; *J* 1936) Engr. and Treas., O. A. Wendt Co., 1655 W. Fullerton Ave., Chicago 14, and • 6205 Forest Glen, Chicago 30, Ill.

WENDT, William R., Jr. (*J* 1945) Sales Mgr., Westerlin & Campbell Co., 185 N. Wabash Ave., Chicago, Ill., and • 2443 North 66th St., Wauwatosa 13, Wis.

WENINGER, Merle (*A* 1945) Dist. Mgr., Powers Regulator Co., 1813 South Ave., and • 113 Eloise Terrace, Syracuse 7, N. Y.

WERKER, Herwart (*M* 1939) Engr., American Radiator & Standard Sanitary Corp., Inst. of Thermal Research, 675 Bronx River Rd., and • 38 Loring Ave., Yonkers 4, N. Y.

WERLEY, William C. (*A* 1945) Western Repr., Peerless Foundry Co., Indianapolis, Ind., and • 4023 Quincy St., St. Louis 16, Mo.

WERLLA, Billy C. (*S* 1946) Student, • Texas A. & M. College, Box 5543, College Station, and 905 Sears, Denison, Texas.

WERNER, Charles V. (*M* 1945) Sales Engr., H. H. Wright Co., 1322 Walnut St., and • 4219 Kenwood, Kansas City, Mo.

WERNER, John G. (*M* 1937) Mgr., • Bryant Air Conditioning Corp., 740 11th St. N.W., Washington 1, and 3130 Wisconsin Ave. N.W., Washington 16, D. C.

WERNER, P. H. (*A* 1941; *J* 1939) Sales Repr., • Barber-Colman Co., 90 New St., Newark 2, N. J., and 7926 Nichener St., Philadelphia 19, Pa.

WERNER, Richard K. (*M* 1936) Cons. Engr., • 316 W. T. Waggoner Bldg., Fort Worth 2, and 5436 Collinwood, Fort Worth 7, Texas.

WERWATH, Karl O. (*A* 1948) Vice-Pres., Milwaukee School of Engineering, • 1020 N. Broadway, and 2209 E. Newton Ave., Milwaukee, Wis.

WESBY, Vernon Lathrop (*A* 1944) Chief Engr.-Utilities, General Motors Corp., Electro-Motive Div., La Grange, and • 6827 S. Throop St., Chicago 36, Ill.

WESLEY, Edward D. (*A* 1945) Pres., E. D. Wesley Co., • 715 W. Lincoln Ave., and 2953 South 43rd St., Milwaukee 12, Wis.

WESLEY, Ray O. (*A* 1937) Partner, • Navarre Plumbing & Heating Co., 2308 Fourth Ave., Seattle, and R. F. D. 1, Woodinville, Wash.

WESLEY, William (*A* 1945) Owner, • Wesley Refrigeration Service, Box 423, and 315 Oakwood St., Rome, N. Y.

WESNER, Eugene L. (*J* 1947) Draftsman, • U. S. Rubber Co., 549 E. Georgia St., and 2458 N. Pennsylvania St., Indianapolis, Ind.

WESSLER, George H., Jr. (*A* 1947) Sales Engr., General Electric Co., 1801 N. Lamar, Dallas, and P. O. Box 372, Arlington, Texas.

WEST, Charles H., Jr. (*A* 1941) Vice-Pres., Massey, Wood & West, Inc., P. O. Box 5008, Richmond 20, Va.

WEST, J. Hoyt (*A* 1944) Owner and Mgr., • West Brothers Sheet Metal, 370 Jones Ave. N.W., and 106 W. Lake Ave. N.W., Atlanta, Ga.

WEST, Lionel C. (*A* 1947) Engr., • Iron Fireman Mfg. Co. of Canada, Ltd., 80 Ward St., and 190 Pacific Ave., Toronto, Canada.

WEST, William P. (*J* 1947) Sales Engr., • Johnson Service Co., 311 Bona Allen Bldg., and 1559 Westwood Lake S.W., Atlanta, Ga.

WESTBROOK, Charles H. (*A* 1945) Partner, • American Plumbing & Heating Co., 1806 Classen, and 1442 Northwest 25, Oklahoma City, Okla.

WESTENDARP, Francisco G. (*M* 1939) Engr., Apartado 1843, Mexico, D. F.

WESTON, Charles E. (*A* 1946) Partner, American Home Heating Co., 1433-35 Fillmore Ave., Buffalo 11, and • 484 Stockbridge Ave., Buffalo 15, N. Y.

WESTOVER, Wendell (*M* 1936) Pres., • Westover-Wolfe, Inc., 21 Plaza, Albany 7, and Loudon Heights, N. Y.

WESTPHAL, Edward R. (*M* 1945) Mgr. of Plants, • Weil-McLain Co., Blaine St., and Long Beach, Michigan City, Ind.

WESTPHAL, Norman E. (*A* 1946; *J* 1940; *S* 1937) Asst. Plant Mgr., • Weil-McLain Co., and Long Beach, Stop 21, Michigan City, Ind.

WETZELL, Horace E. (*M* 1934) Pres., • The Smith & Oby Co., 6107 Carnegie Ave., Cleveland 3, and 21144 Aberdeen Rd., Rocky River 16, Ohio.

WEYENBERG, Henry (*M* 1946) Chief Engr., • Holland Furnace Co., and 587 Lawndale Ct., Holland, Mich.

WHEALTON, Daniel J. (*A* 1944) Design Draftsman, Meyer, Strong & Jones, Inc., 101 Park Ave., New York 17, and • 593 Sixth St., Brooklyn 15, N. Y.

WHEELER, B. J. (*A* 1946) Owner, Wheeler Engineering Co., 2755 N.E. Broadway, Portland, Ore.

WHEELER, Charles A. (*M* 1941) Branch Mgr., • Johnson Service Co., 1217 Grand Ave., and 345 49th St., Des Moines, Ia.

WHEELER, Charles W. (*M* 1942) Engr., • The Ric-wiL Co., 1562 Union Commerce Bldg., Cleveland, and 11859 Edgewater Dr., Lakewood, Ohio.

WHEELER, Harold E. (*M* 1944) Pres., • Air Comfort Corp., 816 N. Kostner Ave., Chicago 51, and 32 Ravine Terrace, Highland Park, Ill.

WHEELER, James A. (*M* 1946) Branch Mgr., American Blower Corp., 631 M & M Bldg., Houston 2, and • 8514 Baker Dr., Houston, Texas.

WHEELER, Joe, Jr. (*M* 1938) Sales Repr., • Johnson Service Co., 28 East 29th St., New York, and P. O. Box 150, Port Washington, L. I., N. Y.

WHEELER, William H. (*A* 1948) Pres., • Airkem, Inc., 7 East 47th St., and 330 East 50th St., New York, N. Y.

WHELAN, Leo (*M* 1945) Dir. of Education, New York Technical Institute, 108 Fifth Ave., New York, and • 1017 Lincoln Pl., Brooklyn, N. Y.

WHELAN, William J. (*M* 1937) Purch. and Estimating, • Harrigan & Reid Co., 1365 Bagley Ave., Detroit 26, and 3790 Seminole Ave., Detroit 14, Mich.

WHELLER, Harry S. (*M* 1916) Pres. and Gen. Mgr., L. J. Wing Manufacturing Co., 154 West 14th St., New York 11, N. Y., and • 725 Union Ave., Elizabeth 3, N. J.

WHITACRE, Verne L. (*M* 1946) N. Y. Dist. Mgr. of Insulation, Johns-Manville Sales Corp., 22 East 40th St., New York 16, N. Y., and • 275 Engle St., Englewood, N. J.

WHITAKER, Kenneth L. (*A* 1947) Managing Dir., The Bristol Fan Co., Bath Rd., Totterdown, and • 29 Cooper Rd., Westbury-on-Trym, Bristol, England.

WHITE, Arthur A. (*A* 1945) Managing Dir., • Gilbert & Barker Manufacturing Co., Ltd., 64 Jefferson Ave., and 133 Hillhurst Blvd., Toronto, Ont., Canada.

WHITE, Eugene B. (*M* 1934) Archt. and Engr., • Y. M. C. A. Architectural & Engineering Bureau, 19 S. LaSalle St., Chicago 3, and 126 S. East Ave., Oak Park, Ill.

WHITE, Francis R. L. (*M* 1947) Chief Tech. Officer, The Brightside Foundry and Engineering Co. Ltd., Htg. & Air Treatment Div., 17 Summer Row, Birmingham 3, and • 28 Abbotts Rd., Kings Heath, Birmingham 14, England.

WHITE, James A. (*M* 1946) Engr. and Secy.-Treas., Sterling Engineered Welderies Ltd., 26 Athletic Ave., and • 108 Blantyre Ave., Toronto, Ont., Canada.

WHITE, Jesse E. (*M* 1946) Mech. Engr., Norfolk Naval Shipyard, Public Works Design Sect., Portsmouth, and • 7607 Gloucester Ave., Norfolk 5, Va.

WHITE, John C. (*Life Member; M* 1932) Cons. Engr., Steam & Mech., • 550 State St., Madison 3, and 1221 W. Dayton St., Madison 5, Wis.

WHITE, John Hazen (*A* 1944; *J* 1943) Pres. and Treas., • Taco Heaters, Inc., 342 Madison Ave., New York 17, N. Y., and Meadowbank Rd., Old Greenwich, Conn.

WHITE, Maxwell H. (*A* 1945) Archt., • 804 Finance Bldg., Cleveland 15, and 10120 Wilbur Ave., Cleveland 6, Ohio.

WHITE, Philip H. (*M* 1948) Engr., Bldg. Service Div., Stone & Webster Engineering Corp., 49 Federal St., Boston, and • 36 Richards Rd., Watertown 72, Mass.

WHITE, Ralph A. (*A* 1947) Owner, • White Engineering Co., Box 226, Graham, and R. F. D. No. 1, Haw River, N. C.

WHITE, Thomas J. (*A* 1941; *J* 1938) Engr., • American Blower Corp., 625 Market St., San Francisco 5, and 2340 Pelham Pl., Oakland 11, Calif.

WHITE, W. Emery (*M* 1941) Engr., H. H. Wright Co., 1322 Walnut St., Kansas City 6, and • 7411 Ward Pkwy., Kansas City 5, Mo.

WHITE, William Robert (*M* 1938; *A* 1936) Mfrs. Agent, The William R. White Co., 4916 Grand Ave., and • 4916 Grand Ave., Omaha 11, Nebr.

WHITE, William Russell (*A* 1946) Indus. Engr., • Washington Gas Light Co., 1100 H St. N.W., Washington 1, D. C., and 609 Park Ave., Falls Church Va.

WHITEHEAD, Emil R. (*A* 1946) Sales, Slater Engineering Corp., 627 Monroe Ave., and • 1138 Panama, Memphis, Tenn.

WHITELAW, H. Leigh (*M* 1916) Managing Dir., • Association of Gas Appliance & Equipment Mfrs., 60 East 42nd St., New York 17, N. Y., and Cummings Point, Stamford, Conn.

WHITMER, Robert P. (*M* 1935) Secy., • American Foundry & Furnace Co., and 1404 E. Washington St., Bloomington, Ill.

WHITNAH, Scott (*M* 1945) Mech. Engr., • Scott Whitnah, Lang & Assocs., Inc., 603 Second Ave. S., Minneapolis, and R. F. D. 3, Wayzata, Minn.

WHITNEY, C. W. (*M* 1935) Vice-Pres., Petrol Corp., 1132 N. Charles St., Baltimore 1, and • Box 216, Route 14, Baltimore 20, Md.

WHITT, Sidney A. (*M* 1946; *A* 1938; *J* 1937) Chief Engr., Cordley & Hayes, 443 Fourth Ave., New York 16, and • 630 Palisade Ave., Yonkers, N. Y.

WHITTAKER, Geoffrey S. (*M* 1947) Mech. Engr., Albert Kahn Associated Archts. & Engrs., 345 New Center Bldg., Detroit 2, and • 18285 Snowden, Detroit, Mich.

WHITTAKER, Wayne K. (*A* 1935) Engr., Irving Trust Co. Bldg., 1 Wall St., New York, and • 119-23-226th St., St. Albans, L. I., N. Y.

WHITTEMORE, William M., Jr. (*A* 1948; *J* 1945) Indus. Sales Engr., Crane Co., 532 Eighth Ave. S., and • 1501 Ashwood Ave., Nashville, Tenn.

WHITTEN, H. E. (*Life Member; M* 1924) Pres. and Treas., H. E. Whitten Co., 9 Federal Court, Boston, and • 56 Highland Rd., Somerville, Mass.

WHITTIER, F. Weston (*J* 1947) Prod. Engr., Western Electric Co., 418 N. Franklin St., Allentown, and • 4 W. Church St., Bethlehem, Pa.

WHITTINGTON, William P. (*M* 1944) Pres., • Whittington Pump & Engineering Co., 245 S. Meridian St., Indianapolis 4, and 7620 Central Ave., Indianapolis 44, Ind.

WHITTLESEY, Con. (*M* 1941) Engr., Combustioneer Corp., 409 Tenth St. S.W., Washington, D. C., and • 1500 S. Barton St., Arlington, Va.

WHYBREW, George H. (*M* 1944) Chief Mech. Engr., • Giffels & Vallet, Inc., 1000 Marquette Bldg., Detroit 26, and 4140 Fulton Pl., Royal Oak, Mich.

WHYTE, Frederic J. (*M* 1944) Tech. Advisor, • Norris Warming Co., Ltd., 5-11 Theobalds Rd., London W. C. 1, and 45 Sidcup Rd., Lee, London S. E. 12, England.

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WIDDOWFIELD, A. S. (*A* 1941; *J* 1937) Sales Engr., The Mercoid Corp., 4201 Belmont Ave., Chicago 41, Ill.

WIDMER, Walter J. (*A* 1939) Secy.-Treas., • Widmer Plumbing & Heating Co., 34 N.E. Seventh Ave., Portland 14, and 1565 N. Shaver St., Portland 12, Ore.

WIEDEMAN, Walter (*A* 1945) Owner, • Reeves Wiedeman Co., 2611 Warwick, Kansas City 8, and 5343 Rockhill Rd., Kansas City 4, Mo.

WIEDENMANN, W. A. (*A* 1942) Owner, • W. C. Wiedenmann & Son, 1820-24 Harrison St., and 5718 Rockhill Rd., Kansas City, Mo.

WIEGAND, Horace M. (*A* 1947) Sales Engr., Wright Engineering Corp., 414 Stanley Ave., and • 1137 Jefferson Ave., Evansville, Ind.

WIEGMANN, Karl H. (*A* 1946) Plant Engr., Durite Plastics, Inc., 5000 Summerdale Ave., Philadelphia 24, and • 3305 Decatur St., Philadelphia 36, Pa.

WIEGNER, Henry B. (*Life Member*; *M* 1919) Office Mgr., Johnson Service Co., 20 Winchester St., Boston 16, and • 143 Standish Rd., Watertown 72, Mass.

WIELAND, John J. (*M* 1944) Mech. Engr., R. F. D. 1, Alto, Mich.

WIGGLESWORTH, George L., Jr. (*S* 1948) Student, University of Michigan, and • 1209 South State St., Ann Arbor, Mich.

WIGGS, G. Lorne* (*M* 1936; *A* 1932; *J* 1924), (Council, 1938-40) Sr. Partner, • Wiggs, Walford, Frost & Lindsay, Suite 405, Crescent Bldg., 1411 Crescent St., Montreal 25, and 429 Lansdowne Ave., Westmount 6, Que., Canada.

WIGLE, Kenneth G. (*A* 1945) Pres., • Bruce Wigle Plumbing & Heating Co., 9117 Hamilton, Detroit 2, and 16565 Baylis, Detroit 21, Mich.

WIIK, Alfred (*A* 1946) Mgr. and Partner, Twin City Plumbing & Heating Co., 2912 Bloomington Ave., and • 4732–16th Ave. S., Minneapolis 7, Minn.

WIIK, Edward M. (*A* 1945) Htg. Engr., Twin City Plumbing & Heating Co., 2912 Bloomington Ave. S., Minneapolis, and • 3429 Portland Ave. S., Minneapolis 7, Minn.

WILCOX, Leland J. (*A* 1948) Dvlpt. Engr., Surface Combustion Corp., 400 Dublin Ave., and • 860 Northwest Blvd., Columbus, Ohio.

WILD, Harry (*A* 1947) Design Engr., Ministry of Supply, and • 41 Heaton Moor Rd., Heaton Moor, Stockport, Cheshire, England.

WILDE, Dale R. (*M* 1944) Engr., Williams, Gritton and Wilde, 204 Dooly Bldg., Salt Lake City 1, and • 153 S. Seventh, E., Salt Lake City 2, Utah.

WILDER, Edward L. (*Life Member*; *M* 1915) Retired, 369 Bonnie Brae Ave., Rochester 7, N. Y.

WILDER, Frank B. (*J* 1946) Engr., Charles S. Leopold, Cons. Engr., 213-5 S. Broad St., Philadelphia, and • 118 Fayette St., Conshohocken, Pa.

WILDER, Wentworth (*A* 1947) Indus. Sales Engr., • York Corp., 911 Walnut St., Kansas City 6, and 2840 Forest Ave., Kansas City, Mo.

WILDERMUTH, Russell O. (*A* 1946) 2435 Frisby Ave., Bronx 61, N. Y.

WILDMAN, Eugene L. (*A* 1942; *J* 1939) Mech. Engr., W. M. Anderson Co., 600 Schuylkill Ave., and • 4909 Catharine St., Philadelphia, Pa.

WILE, Daniel D. (*M* 1944) c/o Refrigeration Engineering, Inc., 7250 East Slauson Ave., Los Angeles, Calif.

WILHELM, Joseph E. (*M* 1943; *J* 1936; *S* 1934) Vice-Pres. and Chief Engr., Avery Engineering Co., 1906 Euclid Ave., Cleveland 15, and • 294 East 195th St., Euclid 19, Ohio.

WILKE, Ira W. (*M* 1946) Htg. Engr., Texas Public Service Co., 422 Congress Ave., and • 2201 Quarry Rd., Austin, Texas.

WILKES, Gordon B.* (*M* 1937) Prof. of Heat Engrg., • Massachusetts Institute of Technology, Cambridge 39, and 51 Everett St., Newton Centre, Mass.

WILKINS, E. Spencer (*M* 1945) Chief Engr., Air Handling Dept., Wertz Engineering Co., Inc., 441 N. Second St., Reading, and • R. D. 2, Mohnton, Pa.

WILKINSON, Arthur (*A* 1936) Mgr., The Wilkinson Engineering Agencies, 985 Sherbrooke St., West Montreal 2, Que., Canada.

WILKINSON, F. J. (*M* 1933) Mgr., Central Engrg. Service Dept., Montgomery Ward & Co., Chicago Ave. and Larabee St., Chicago, and • 18257 Martin Ave., Homewood, Ill.

WILL, Clarence A. (*A* 1944) Owner, • 5402 Broadway, P. O. Box 6009, Indianapolis 20, and R. R. 4, Box 161, Noblesville, Ind.

WILL, Donald S. (*A* 1947) Br. Mgr., Payne Furnace Co., 4019 Atlantic Ave., and • 1831 Marshall Pl., Long Beach 7, Calif.

WILL, Harold C. (*M* 1946) Mgr., Air Conditioning Div., J. A. Walsh and Co., P. O. Box 1773, Houston 1 and • 5017 Winnetka, Houston 4, Texas.

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WILLEY, Earl C.* (*M* 1934) Prof., Gen. Engrg., • Oregon State College, and 121 North 29th St., Corvallis, Ore.

WILLIAM, Frederic C. (*M* 1943) Field Engr., • American Blower Corp., 1003 Statler Bldg., Boston 16, and 91 Parker Rd., Wellesley 81, Mass.

WILLIAMS, Allen W. (*Life Member*; *A* 1915) Secy.-Treas., • National Warm Air Register Manufacturers Inst., 5 E. Long St., Room 808, Columbus 15, and 51 Meadow Park, Bexley 9, Ohio.

WILLIAMS, Charles R. (*M* 1945) Vice-Pres., Dickie Construction Co., Ltd., 17 Yorkville Ave., and • 91 Dewbourne Ave., Toronto, Ont., Canada.

WILLIAMS, Chester D. (*M* 1938) Mgr., • General Air Conditioning & Heating Co., 2001 Peralta St., Oakland 7, and 5747 Country Club Dr., Oakland 11, Calif.

WILLIAMS, Donald D. (*M* 1942; *A* 1940; *J* 1938) Product Supvsr., A. O. Smith Corp., Box 584, and • 2656 N. Lefeber, Milwaukee, Wis.

WILLIAMS, Donald L. (*M* 1941) Engr., • General Air-Conditioning & Heating Co., 2001 Peralta St., and 67 Glen Ave., Oakland 11, Calif.

WILLIAMS, E. Bryan (*A* 1943) Asst. Chairman Mech. Engrg., • Armour Research Foundation, 35 West 33rd St., Chicago 16, and 413 Dempster, Evanston, Ill.

WILLIAMS, Edgar H. (*J* 1945) Air Cond. Engr., • Hungerford Coal Company, Inc., 1604 E. Broad St., and 4802 Old Brook Rd., Apt. 21, Richmond, Va.

WILLIAMS, Elwin C. (*A* 1939) Hoffman Specialty Co., Inc., 4028 Egbert Ave., Cincinnati 20, Ohio.

WILLIAMS, F. K. (*A* 1947) Designer, Public Works Dept., State of Victoria, Australia, Treasury Gardens, Melbourne, and • 203 Raleigh St., Thornbury N. 17, Victoria, Australia.

WILLIAMS, Frank H. (*A* 1940; *J* 1934) Process Engr., General Motors, 5-227 G. M. Bldg., Detroit 2, and • 17701 Manderson Rd., Detroit 3, Mich.

WILLIAMS, Garland E. (*J* 1943) Engrg. Draftsman, Norfolk Naval Shipyard, Portsmouth, and • 4305 Newport Ave., Apt. 4, Norfolk, Va.

WILLIAMS, Glenn (*A* 1947) Refrig. Supt., Hayes Bros., Inc., 236 W. Vermont, Indianapolis, and • 1001 S. Auburn, Indianapolis 21, Ind.

WILLIAMS, G. M. (*M* 1943) Cons. Engr., • Architects & Builders Bldg., Indianapolis, and 316 Berkeley Rd., Indianapolis 8, Ind.

WILLIAMS, Harvey O. (*A* 1945) Field Service Engr., • A. M. Byers Co., 1502 Esperson Bldg., Houston 2, and 1901 Swift St., Houston 5, Texas.

WILLIAMS, H. Edmund (*A* 1947; *J* 1939) Chief Engr., Majestic Refrigerator Corp., 625 Broadway, New York, and • 256 Sterling Pl., Brooklyn, N. Y.

WILLIAMS, Henry B. (*M* 1945) Asst. Chief Engr., McQuay, Inc., 1600 Broadway, N.E., Minneapolis, and • 2804–37th Ave. S., Minneapolis 6, Minn.

WILLIAMS, James K. (*A* 1944) Constr. Supt., • Robert S. Leiby Co., 212 N. Grant Ave., and 1213 Wilson Ave., Columbus, Ohio.

WILLIAMS, J. Walter (*Life Member*; *M* 1915) Pres., • Forest City Plumbing Co., 332 E. State St., and 923 E. State St., Ithaca, N. Y.

WILLIAMS, Kenneth O. (*A* 1944) Dist. Repr., H. A. Thrush & Co., Peru, Ind., and • 3200 Oliver Ave., East St. Louis, Ill.

WILLIAMS, Lyle G. (*M* 1939) Engr., • Williams Plumbing Co., Inc., Portland Ave. at Berkeley, Gladstone, and 330 E. Arlington St., Gladstone 1, Ore.

WILLIAMS, O. L. (*A* 1944) Owner, • Bryant-Williams Co., 936 Ridge Ave., Pittsburgh 12, and 104 Mayfair Dr., Pittsburgh 16, Pa.

WILLIAMS, William A. (*M* 1943) Engr., Htg. and Vent., General Electric Co., River Works, 920 Western Ave., Lynn, and • 10 Sevinor Rd., Marblehead, Mass.

WILLIAMS, William E. (*A* 1947) Mgr., Dist. Office, • The Powers Regulator Company of Canada, Ltd., 985 Sherbrooke St. W., and 5265 Cote St., Catherine Rd., Montreal, Que., Canada.

WILLIAMSON, Chester C. (*M* 1942) Dist. Sales Mgr., Chicago Metal Hose Corp., 92 Washington St., Brookline 46, and • 3 Surrey Lane, Natick, Mass.

WILLIAMSON, James O., Jr. (*M* 1946) Mech. Engr., Air University, Air Installations, A-4, Maxwell Field, and • 308 Southview Ave., Montgomery 6, Ala.

WILLNER, Ira (*M* 1937) Pres., • Willner Heating Co., Inc., 415 Lexington Ave., New York 17, and 125 East 93rd St., New York 28, N. Y.

WILLOUGHBY, J. D. (*A* 1945) Owner, F. W. Willoughby Co., 2045 Curtis St., Denver 2, Colo.

WILLSON, Frank J. (*M* 1941) Vice-Pres., • Dollinger Corp., 11 Centre Park, Rochester 3, and 2219 Westfall Rd., Rochester 10, N. Y.

WILMOT, Charles S. (*M* 1919) Engr., Day and Zimmermann, Inc., 715 Packard Bldg., Philadelphia, and • 436 Haverford Ave., Narberth, Pa.

WILSON, Alexander M. (*A* 1947; *J* 1942; *S* 1939) 18 Carisbrooke St., Andover, Mass.

WILSON, Arthur A. (*M* 1944) Mgr., Growers Refrigerating Co., P. O. Box 184, and • Route 2, Box 434C, Medford, Ore.

WILSON, Broadus (*M* 1945) Pres., • General Air Conditioning Co., 510 Glenwood Ave., and 2108 White Oak Rd., Raleigh, N. C.

WILSON, Charles H. (*A* 1947) Power and Htg. Engr., Ford Motor & Climate Control, Ford Motor, Northville & Climate Control, Joy Rd., Detroit, and • 9912 Hubbard, Rosedale Gardens, Plymouth, Mich.

WILSON, Donald P. (*M* 1943) Factory Mgr., McQuay, Inc., 1600 Broadway, N.E., Minneapolis 13, and • 3380 Brunswick, Minneapolis 16, Minn.

WILSON, Frederick W. (*A* 1948) Engr., • R. E. Kramig Co., Inc., 222-24 East 14th St., Cincinnati 10, and 8375 Newberry St., Cincinnati 15, Ohio.

WILSON, George H. (*A* 1945) Owner, • Wilson Refrigeration Engineering, 211 Bird St., and 422 N. Seventh St., Hannibal, Mo.

WILSON, Harry F. (*M* 1945) Cons. Engr., • 4908 Delmar Blvd., St. Louis 8, and 3221 Capehart Dr., Normandy 20, Mo.

WILSON, Herbert H. (*A* 1946) Sales Mgr., • Ilg Electric Ventilating Co., 517 Farnsworth Bldg., and 1872 Netherwood Ave., Memphis 6, Tenn.

WILSON, Howard F. (*J* 1947) Htg. Engr., • Michigan Consolidated Gas Co., 47 N. Division Ave., Grand Rapids 2, and 1061 Prospect S.E., Grand Rapids, Mich.

WILSON, James (*M* 1942) Service Engr., Darling Bros., Ltd., 140 Prince St., and • 4259 Hingston Ave., N. D. G., Montreal, Que., Canada.

WILSON, James A. (*A* 1947) Div. Mgr., • United Gas Corp., Box 2628, Houston 1, and 1519 Branard, Houston 6, Texas.

WILSON, James E. (*A* 1947) Engr. & Estimator, Dallas Air Conditioning Co., 2809 Canton and • 3014 Ivandell, Dallas, Texas.

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WILSON, John D. (*A* 1946) Mgr., Air Cond. & Refrig. Dept., Hager Fox, 1124 S. Pennsylvania, and • 204 Alden St., Spring Lake, Mich.

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WILSON, Kentner L. (*A* 1944) Branch Mgr., • Minneapolis-Honeywell Regulator Co., 415 Brainard St., Detroit 1, and 2608 Woodstock Dr., Detroit 3, Mich.

WILSON, Maurice J. (*M* 1945) Sales Engr., Carrier Corp., 300 Ivy St. N.E., Atlanta 3, Ga.

WILSON, Raymond W. (*M* 1934) Member of Firm, Wilson-Brinker Co., 308 Pythian Bldg., Kalamazoo 9, and • 2414 S. Westnedge Ave., Kalamazoo 34, Mich.

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WILSON, Thomas B. (*A* 1947) Cons. Engr., Thos. B. Wilson, "Century House," Sledgate Lane, Wickersley, Rotherham, Yorkshire, England.

WILSON, Victor H. (*A* 1938) Contr. and Mfrs. Agent, • 210 Union Bus Terminal Bldg., Nashville 3, and "The Thistle-Patch," Donelson, Tenn.

WILSON, Westray E. (*A* 1939) Lt. Col., U. S. Army, • Wilson Plumbing Co., 227 Haywood Rd., and 110 Salola St., Asheville, N. C.

WILSON, W. H. (*A* 1932) Chief Power Plant Engr., Pullman-Standard Car Manufacturing Co., Pullman Car Works, 111th St. and Cottage Grove Ave., and • 22 West 110th Pl., Chicago 28, Ill.

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WINANS, G. D. (*M* 1929), (Council, 1944-46) Asst. Supt. of Central Htg., • The Detroit Edison Co., 2000 Second Ave., Detroit 26, and 16183 Wisconsin Ave., Detroit 21, Mich.

WINCHESTER, Paul D. (*A* 1948) Engr., • Hart & Cooley Mfg. Co., 500 East 12th, and 221 West 12th, Holland, Mich.

WINDSOR, William G. (*M* 1944) Electrical Engr., S. A. Railways, Airways & Harbours, c/o C. E. E., S. A. R. Hdqrs. J. H. B. S. A., and • 11 Third Ave., Hill Extension, Johannesburg, Transvaal, South Africa.

WINKLER, Ralph A. (*A* 1940; *J* 1937) Vice-Pres., A. E. Winkler & Sons, Inc., 2337 North 31st St., Milwaukee 10, and • P. O. Box 179, Elm Grove, Wis.

WINNER, Robert J. (*J* 1948) Test Engr., General Electric Co., and • 1214½ Delaware, Ft. Wayne, Ind.

WINSLOW, C.-E. A., Dr.* (*Life Member*; *M* 1932), (*Presidential Member*), (Pres., 1945; 1st Vice-Pres., 1944; 2nd Vice-Pres., 1943) (Council 1940-46) Yale University School of Medicine, Historical Library, 333 Cedar St., and • 313 St. Ronan St., New Haven 11, Conn.

WINTERBOTTOM, J. W. (*M* 1944) Pres., • Winterbottom Supply Co., and 432 Denver St., Waterloo, Ia.

WINTERBOTTOM, Ralph F. (*M* 1923) Owner, • Heating & Cooling Supply Co., 178 W. First St., and 720 Moir St., Waterloo, Ia.

WINTERER, Frank C. (*M* 1920) Branch Sales Mgr., • American Radiator & Standard Sanitary Corp., 300 Broadway, St. Paul 1, and 836 Juno Ave., St. Paul 2, Minn.

WINTERS, H. Gordon (*A* 1946) Htg. Engr., Trane Company of Canada, Ltd., 637 Craig St., W., Montreal, and • 16 Lamarque St., Ste. Therese de Blainville, Que., Canada.

WIRTH, Edward D. (*A* 1947) Buyer, Plbg. & Htg., Montgomery Ward & Co., 619 W. Chicago Ave., and • 4439 N. California Ave., Chicago 25, Ill.

WISE, Mason W. (*M* 1941) Owner, M. W. Wise Co., and • 1656 Melrose Dr. S.W., Atlanta, Ga.

WISE, Ray A. (*A* 1944) Member of Firm, • The Sweeny & Wise Co., 10210 Woodland, Cleveland 4, and 2124 Lamberton Rd., Cleveland Heights 18, Ohio.

WISER, C. E. (*A* 1941) Mgr., Northwest Region, Minneapolis-Honeywell Regulator Co., 420 N. Fifth St., Minneapolis, and • 2620 Park Ave. S., Minneapolis 7, Minn.

WITHERIDGE, David E. (*A* 1945; *J* 1936) Cons. Engr., W. A. Witheridge Co., 2340 Mershon St., Saginaw, Mich.

WITHERIDGE, John M. (*J* 1947) Engr.-Partner, • W. A. Witheridge Co., 2340 Mershon St., and 1224 Janes St., Saginaw, Mich.

WITHERIDGE, William N. (*M* 1944) Vent. Consultant, General Motors Corp., Research Lab. Div., P. O. Box 188, North End Station, Detroit 2, and • 3741 W. Outer Dr., Detroit 21, Mich.

WITMER, Howard S. (*A* 1937) United States Rubber Co., 6600 E. Jefferson Ave., Detroit 5, and • 27 Sylvan Ave., Pleasant Ridge, Mich.

WITSCHY, Roy J. (*A* 1946) Owner, • Witschy Oil Co., West 19th and Railroad Ave., and 2103 Avenue F, Scottsbluff, Nebr.

WITTBOLD, Richard H. (*A* 1945) Dist. Repr., Barber-Colman Co., and Farr Co., and • 3818 Brandt St., Houston, Texas.

WITTE, George C., Jr. (*S* 1948) Student, Purdue University, Lafayette, Ind., and • 2618 Willing, Fort Worth 4, Texas.

WITTENMEIER, Frederick G. (*M* 1945) Vice-Pres. in charge of Engrg., • Wittenmeier Machinery Co., 850 N. Spaulding Ave., Chicago 51, and 4444 N. Wolcott Ave., Chicago, Ill.

WITTIG, Frederick E. (*A* 1946; *J* 1943) Asst. Prof. of Mech. Engrg., • Michigan College of Mining & Technology, Houghton, and 6 Cherokee Ave., P. O. Box 505, Painesdale, Mich.

WODAL, Joseph J. (*A* 1947) Mech. Engr., • The Austin Co., 777 E. Washington Blvd., Los Angeles 21, and 12626 Cometa Ave., San Fernando, Calif.

WOEHLKE, Herman J. (*M* 1944) Estimator and Asst. Mgr., • Bell Plumbing & Heating Co., 1228 E. Evans Ave., and 2255 S. Marion, Denver 10, Colo.

WOESE, Carl F. (*M* 1934) Cons. Engr., • Robson & Woese, Inc., 1001 Burnet Ave., Syracuse 3, and 256 Robineau Rd., Syracuse 4, N. Y.

WOFFENDEN, Harold (*M* 1945) Principal, Woffenden & Co., Engrs., Cabot House, Clifton Down Rd., Bristol 8, England.

WOLF, Raymond B. (*J* 1948; *S* 1946) • Welders Equip. Co., Harlington, and 3192 Cable St., Beaumont, Texas.

WOLF, Robert L. (*A* 1945) Combustion Engr., • City of Indianapolis, Room 401-E City Hall, and 632 East 66th St., Indianapolis, Ind.

WOLFE, Allen H. (*M* 1944) Vice-Pres., The Huffman-Wolfe Co., 669 N. High St., Columbus 16, and • 2186 Yorkshire Rd., Columbus, Ohio.

WOLFE, Benjamin M. (*A* 1946) Design Engr., Co-Partner, • Coast Heating and Sheet Metal Co., 602 S. Tremont, and R. F. D. Box 448, Oceanside, Calif.

WOLFE, Charles H. (*M* 1944) Mech. Engr., 1324 E. Cooke Rd., Columbus, Ohio.

WOLFE, Clarence E., Sr. (*M* 1947; *A* 1944) Vice-Pres., • Reynolds Corp., 4224 S. Lowe Ave., Chicago 9, and 1907 Clarence Ave., Berwyn, Ill.

WOLFE, John S. (*M* 1941) Chief Engr., Ruemelin Manufacturing Co., 3860 N. Palmer St., Milwaukee, and • 5650 N. River Forest Dr., Milwaukee 9, Wis.

WOLFE, Jules S. (*A* 1946) Mgr., Purchasing, Engrg. Dept., • Famous Players Canadian Corp., Ltd., 1200 Royal Bank Bldg., and 332 Spadina Rd., Toronto, Ont., Canada.

WOLFF, Richard A. (*M* 1945) Secy., • Wolff & Munier, Inc., 222 East 41st St., New York 17, and 250 West 94th St., New York 25, N. Y.

WOLIN, M. W. (*A* 1947; *J* 1938; *S* 1937) 12 Whittier Ave., New Brunswick, N. J.

WOLLENBERGER, Louis (*M* 1938) Sales Supvsr., • Coast Counties Gas & Electric Co., 22 Pacific Ave., and Pasatiempo Country Club, Santa Cruz, Calif.

WOLLERMAN, Arthur E. (*M* 1944) Sales Mgr., • B. F. Sturtevant Co., Div. of Westinghouse Electric, 85 E. Gay St., Columbus 13, and 387 Demorest Ave., Columbus 4, Ohio.

WOLLRIK, Helge V. (*A* 1946) Mgr., Htg., Sanitary, and Vent. Dept., • A. B. Gustavsbergs Fabriker, Gustavsberg, and Klippvaegen 5, Ektorp, Sweden.

WOLPERT, Nathan N. (*A* 1945) Assoc. Editor, Heating & Ventilating, 148 Lafayette St., New York 13, and • 4 Prospect Ave., Glen Cove, L. I., N. Y.

WOLTERS, Harold W. (*M* 1944) Sales Engr., Wilson Brinker Co., 308 Pythian Bldg., Kalamazoo, and • 820 Staples Ave. N.W., Kalamazoo 54, Mich.

WONG, Kai Fong (*J* 1946) Mech. Engr., P-4, Navy Yard, Pearl Harbor, and • P. O. Box 103, Wahiawa, Oahu, T. H.

WONG, Wilfred S. B. (*M* 1938) Managing Dir., • American Engineering Corp., 985 Nanking Rd., West and 669 Changteh Rd., Shanghai 9, China.

WOOD, Alfred W. (*A* 1941; *J* 1938) Mgr., • Climate Control Co., 99 Carling St., and 47 Riverview Ave., London, Ont., Canada.

WOOD, Charles F. (*M* 1937) Air Cond. Mgr., Prod. Development and Appl. Dept., Frigidaire Div., General Motors Sales Corp., 300 Taylor St., Dayton 1, and • R. R. 1, Spring Valley, Ohio.

WOOD, David J. (*A* 1946) Mgr., Cincinnati Branch, York Corp., 659 E. Sixth St., Cincinnati, and • 1631 Alcor Terrace, Cincinnati 30, Ohio.

WOOD, F. J. (*A* 1947) Vice-Pres., • Wood Motor Co., and 1107 Park Pl., Eau Claire, Wis.

WOOD, Fred C. (*M* 1946) Mgr., Air Cond. Sales, • York Corp., and 1507 Clover Lane, York, Pa.

WOOD, Gerald K. (*A* 1946) Sales Engr., • Ilg Electric Ventilating Co., 209 S. High St., and 262 East 13th Ave., Columbus, Ohio.

WOODBRIDGE, William L. (*A* 1944) Pres., Radiant Panel Heating, Inc., 610 Farr St., Milford, Mich.

WOODGER, Herbert W. (*M* 1939) Pres. & Treas., • Berkshire Sheet Metal Works, Inc., 65 McKay St., Pittsfield, and Lenox Rd., Stockbridge, Mass.

WOODHOUSE, Graham D. (*A* 1938) Vice-Pres., • Dowagiac Steel Furnace Co., 110 Beeson St., and 204 Indiana Ave., Dowagiac, Mich.

WOODMAN, Lawrence E. (*M* 1934) Owner, • Woodman Engineering Co., 203 E. Capitol, and 925 Adams, Jefferson City, Mo.

WOODRUFF, Charles S. (*A* 1946) Specification Engr., Cons. Engrg. & Air Cond., 910 Bankers Mortgage Bldg., Houston, and • 7014 Golf St., Houston 12, Texas.

WOODS, Baldwin M., Dr. (*M* 1937), (*Presidential Member*), (Pres., 1947; 1st Vice-Pres., 1946; Council, 1942-47) Dir. of University Extension, University of California, and • 249 The Uplands, Berkeley 5, Calif.

WOODSON, Edward G. (*M* 1944) Dist. Mgr., • The Trane Co., 705 Columbian Tower, Memphis 3, and 80 Lombardy Rd., Memphis, Tenn.

WOODSON, James W. (*M* 1946) Owner and Chief Engr., Woodson Heating Co., and • 5267 Beaconsfield, Detroit 24, Mich.

WOOLCOCK, Edwin (*M* 1947; *A* 1938) Owner, • Woolcock Plumbing & Heating Co., 2217-15th St., and 440 Memorial Pkwy., Niagara Falls, N. Y.

WOOLLARD, Mason S. (*M* 1934) Assoc., Harry H. Angus & Assocs., Cons. Engrs., 1221 Bay St., Toronto 1, and • 107 Langley Ave., Toronto 6, Ont., Canada.

WOOLMAN, Harry D. (*A* 1946) Sales Engr., Minneapolis-Honeywell Regulator Co., 420 N. Fourth St., Minneapolis, and • R. 3, Box 342, Excelsior, Minn.

WOOLSTON, Robert H. (*A* 1944; *J* 1941) Partner, • Woolston Woods Co., 2132 Cherry St., Philadelphia, and 12 English Village, Wynnewood, Pa.

WOOTEN, M. Frank, Jr. (*M* 1941; *A* 1940); Cons. Engr., • Wooten & Wooten, Cons. Engrs. & Archts., Latta Arcade, Charlotte 2, and 400 Cherokee Rd., Charlotte, N. C.

WORKMAN, Albert E. (*A* 1941) Htg. and Air Cond. Sales Dir. • United Gas Corp., P. O. Box 2628, Houston 1, and Rt. 12, Beinhorn Rd., Box 601, Houston, Texas.

WORMLEY, Robert F. (*A* 1938) Mgr., Engineered Prods. Div., • Grinnell Company of Canada, Ltd., 2440 Dundas St. W., Toronto, and 1 L'Estrange Pl., Toronto 9, Ont., Canada.

WORSHAM, Herman (*M* 1925; *J* 1918) Mgr., War Products Training Service, • Frigidaire Div., General Motors Corp., 300 Taylor St., Dayton 1, and 524 Daytona Pkwy., Dayton 6, Ohio.

WORTH, William E. (*A* 1947) Sales & Serv. Engr., • Illinois Testing Laboratories, Inc., 660 Third Street, San Francisco 7, and 1101 Francisco St., San Francisco, Calif.

WORTHINGTON, Thomas H. (*M* 1937) Asst. Mgr., Eastern Sales, Standard Sanitary & Dominion Radiator, Ltd., 405 Beaubien St. W., Montreal, Que., Canada.

WORTON, William (*M* 1937) Mgr., • C. A. Dunham Co., Ltd., 504 Scott Block, and 292 Lansdowne Ave., Winnipeg, Man., Canada.

WRAY, Hubert L. (*J* 1947) Office Engr., Dan J. McQuaid Engineering Service, 1026 17th St., and • Apt. 28, 1730 Logan St., Denver, Colo.

WRENE, Torsten (*J* 1946) Engr., Ingenjorsfirman, TEWE, Torsten Wrene, Tomtebogatan 34, Stockholm, Sweden.

WRIGHT, Calvert C.* (*M* 1944) Chief Div. of Fuel Technology, • The Pennsylvania State College, and 314 Arbor Way, State College, Pa.

WRIGHT, Clarence E. (*A* 1940; *J* 1935; *S* 1933) Mgr., Htg. Dept., • Fairmont Wall Plaster Co., P. O. Box 272, and "Jayenne," Fairmont, W. Va.

WRIGHT, C. P. (*A* 1944) Mgr., • C. P. Wright & Co., 4300 Carnegie Ave., Cleveland 3, and 2987 Torrington Rd., Shaker Heights 22, Ohio.

WRIGHT, Harris H. (*M* 1917) Owner, H. H. Wright Co., 1322 Walnut St., Kansas City 6, and • 808 Greenway Terrace, Kansas City 5, Mo.

WRIGHT, Jack (*A* 1944) Owner, • Canadian Plumbing & Heating Specialties, Ltd., 701 Craig, W., Montreal, and 24 Thurlow, Hampstead, Que., Canada.

WRIGHT, John B. (*M* 1940) c/o The Nash Engineering Co., South Norwalk, Conn.

WRIGHT, John F. (*A* 1945) Prcs., • Air Comfort Assocs., Inc., 412-414 Stanley Ave., Evansville, Ind.

WRIGHT, K. A. (*M* 1921) Branch Mgr., • Johnson Service Co., 1905 Dunlap St., Cincinnati 14, and 1729 E. McMillan St., Cincinnati, Ohio.

WRIGHT, Lawrence T., Jr.* (*A* 1948; *J* 1943) Asst. Dir., Engrg. Research Dept., Standard Oil Co. (Indiana), 910 S. Michigan Ave., Chicago 80, and • 14828 Washington Ave., Harvey, Ill.

WRIGHT, Norman S., Jr. (*A* 1942; *J* 1941) Mfrs. Repr., • 250 Perry St., San Francisco, and 1015 Mariposa Ave., Berkeley 11, Calif.

WRIGHT, Paul H. (*A* 1946) Sales Engr., • Minneapolis-Honeywell Regulator Co., 400 Broadway, Denver 9, and 1160 Sherman, Apt. 407, Denver, Colo.

WRIGHTSON, Wilbor T. (*M* 1937) Eastern Mgr., • Garden City Fan Co., 55 West 42nd St., New York 18, and 22 Sagamore Rd., Bronxville 8, N. Y.

WUNDERLICH, Milton S.* (*M* 1925), (Council 1946-47) Dir. of Research, Minnesota & Ontario Paper Co., 500 Baker Arcade, Minneapolis, and • 545 Mt. Curve Blvd., St. Paul 5, Minn.

WURTS, Henry H. (*M* 1947) Designer, Meadon Blower and Pipe Works, Inc., 23 Meserole Ave., Brooklyn, and • 230 Fenimore St., Brooklyn 25, N. Y.

WYATT, DeWitt H. (*M* 1936) Cons. Engr., Robinson Heaters, Inc., 1397 North Grant Ave., Columbus 1, and • 123 Acton Rd., Columbus 2, Ohio.

WYBLE, Jerome B. (*A* 1947) Mgr., Industrial Burner Div., Griffith-Consumers, 1413 New York Ave. N.W., Washington 5, and • 1443 Lawrence St. N.E., Washington 17, D. C.

WYKOFF, Walter R. (*J* 1946) Research Engr., Battelle Memorial Institute, 505 King Ave., Columbus 1, and • 912 West 11th Ave., Columbus 12, Ohio.

WYLD, Reginald G. (*M* 1937) Engr., • Samson United Corp., 1700 University Ave., Rochester, and 33 Monroe St., Honeoye Falls, N. Y.

WYLIE, Wilson J. (*M* 1945) Mgr., Power Dept., • Toronto Hydro Electric System, 14 Carlton St., Toronto, and 459 Briar Hill Ave., Toronto 12, Ont., Canada.

WYNN, Carl E. (*A* 1946) Sales Promotion, Crane Co., and • 3563 Coleman Ave., Memphis 12, Tenn.

Y

YAGER, John J. (*M* 1921) Pres., Goergen-Mackwirth Co., Inc., 817 Sycamore St., Buffalo, and • 425 Woodbridge Ave., Buffalo 14, N. Y.

YAGLOU, C. P.* (*M* 1923) Prof., Indus. Hygiene, • Harvard School of Public Health, 55 Shattuck St., Boston, and 10 Vernon Rd., Waverley 79, Mass.

YANCEY, Foster V. (*M* 1946) Mgr., • Atlanta Gas Light Co., 109 Church St., and 405 Seminole Dr., Marietta, Ga.

YANCEY, Richard H., III (*A* 1946) Sales Engr., Advanced Refrigeration, Inc., 350 Peachtree St., and • 3181 Mathieson Dr., Atlanta, Ga.

YARBOROUGH, T. R. (*M* 1946) Pres., Y-B Refrigeration & Air Conditioning Co., Inc., 36 N. Fort Harrison Ave., Clearwater, Fla.

YARBROUGH, William B. (*A* 1947) Mech. Engr., • Sherlock, Smith & Adams, Inc., 301 Washington Ave., and 423 S. McDonough St., Montgomery, Ala.

YARDLEY, Jack E. (*J* 1948; *S* 1947) Mech. Engr., • E. I. Du Pont de Nemours, and 92 Gilmer Ct., Orange, Texas.

YATES, Ernest F. (*A* 1946) Mech. Engr., • Reg. F. Taylor, Cons. Engr., 416 National Standard Bldg., Houston 2, and 8418 Bonner Dr., Houston 12, Texas.

YATES, Joseph E. (*M* 1939) Safety Supvsr., • Pacific Power & Light Co., 309 Public Service Bldg., Portland 4, and 1820 Northeast 57th Ave., Portland, Ore.

YATES, Robert A. (*A* 1945) Mgr., • Yates & Co., 231 Tenth St., and 431-16th St., Brandon, Man., Canada.

YATES, Walter (*Life Member*; *M* 1902) Governing Dir., • Matthews & Yates, Ltd., Cyclone Works, Swinton and the Dell, 4 Egerton Park, Worsley, Lancs., England.

YEAGER, George F. (*M* 1944) Capt., T. C., Ward 33C, Valley Forge General Hospital, Phoenixville, and • 1221 Fourth Ave., Altoona, Pa.

YEAZEL, George D. (*A* 1946) Sales Mgr., • Wholesale Equipment Corp., 1338 McGee St., and 3921 Linwood Blvd., Kansas City, Mo.

YEAZEL, Harold F. (*A* 1945) Asst. Sales Mgr., Lennox Furnace Co., Inc., 400 N. Midler Ave., Syracuse 1, and • 1411 Oak St., Syracuse 8, N. Y.

YELLEN, Charles F. (*A* 1945) Htg., Vent., Maint. Engr., Pratt & Whitney Aircraft Corp., Div. of United Aircraft, 400 S. Main St., East Hartford 8, and • 61 Imlay St., Hartford 5, Conn.

YEOMANS, Paul H. (*M* 1944) Cons. Engr., 56 Cedarbrook Rd., Ardmore, Pa.

YERKES, William L. (*M* 1941) Branch Mgr., • Carrier Corp., 1500 S. Santa Fe Ave., Los Angeles 21, and 1617 N. Ontario Ave., Burbank, Calif.

YOE, Charles (*A* 1948) Engr., Shelley Electric Co., 123 S. Main, and • 1832 McKnight Dr., Wichita, Kans.

YORK, John E. (*M* 1948) Bldg. Service Engr., Stone & Webster Engineering Corp., 49 Federal St., Boston, and • 34 Oakcrest Rd., South Weymouth, Mass.

YOST, Claude (*M* 1944) Mech. Engr., • Zumwalt & Vinther, 1807 Mercantile Bldg., Dallas 1, and 5502 Goodwin Ave., Dallas 6, Texas.

YOUNG, Bert C. (*A* 1946) Secy.-Treas., • Young and Sons, Piping and Heating, 1113 Rice St., Bellwood, Ill.

YOUNG, Chester C. (*M* 1943) Utilization Engr., • Lone Star Gas Co., Dallas Div. of Distribution, 301 S. Harwood St., Dallas 1, and 4336 Stanhope St., Dallas 5, Texas.

YOUNG, Dick H. (*A* 1946) Partner and Mgr., • Young Heating Co., 400 W. Park Ave., and 235 Maryland, Waterloo, Ia.

YOUNG, Emil O. (*A* 1935) Owner, • Young Regulator Co., 5209 Euclid Ave., Cleveland 3, and 3628 Cummings Rd., Cleveland Heights, Ohio.

YOUNG, Frank R. (*J* 1946) Sales Engr., Coastal Equipment Co., 2015-19 Congress, Houston 2, and • 7607 Mossrose St., Houston 12, Texas.

YOUNG, George Harrison (*J* 1944) Chief Engr., V. E. Sprouse Co., and • 2225 California St., Columbus, Ind.

YOUNG, Glenn R. (*S* 1947) Student, • Texas A. & M. College, Box 1142, College Station, and 1400 Delaware Dr., Port Arthur, Texas.

YOUNG, Harold J. (*M* 1937) Sales Engr., Young Radiator Co., Occidental Hotel Bldg., and • 1364 Lakeshore Dr., Muskegon, Mich.

YOUNG, James W. (*J* 1947; *S* 1946) Estimator, Vice-Pres., ● Young and Sons, 1113 S. Rice St., Bellwood, Ill.

YOUNG, J. T., Jr. (*A* 1936) Mgr., ● Crane Co., P. O. Box 1410, Salt Lake City 11, and 15 S. Third St., No. 8, Salt Lake City 2, Utah.

YOUNG, Paul W. (*A* 1947) Htg. Engr., ● C. A. Crosta, Inc., 1830 Market St., Denver 2, and 1104 Lincoln St., Denver 3, Colo.

YOUNG, Robert H., Jr. (*A* 1947) Htg. Engr., ● A. P. Engelhart Co., 2730 N. Saginaw St., and 2730½ N. Saginaw St., Flint, Mich.

YOUNGBLOOD, Clete W. (*A* 1944) Owner, ● Youngblood Plumbing & Heating Supply Co., 1700 Broadway, and 707 North 23rd St., Paducah, Ky.

YOUNGER, John R. (*A* 1947; *J* 1941) Student, 317 S. Chauncey, West Lafayette, and ● 410 W. Washington, Monticello, Ind.

YOUNGER, Robert D. (*S* 1948) Indiana Weathermakers, 625 North East St., Indianapolis 2, and ● 410 W. Washington, Monticello, Ind.

YOUNGMAN, Edward C. (*A* 1946) Mech Engr., ● Mead and Hunt, Cons. Engrs., 550 State St., Madison 3, and 1214 Edgehill Dr., Shorewood Hills, Madison 5, Wis.

YULA, Ralph W. (*A* 1944) Cons. Chem. Engrs., ● Singmaster & Breyer, 420 Lexington Ave., New York 17, and 20-11 147th St., Whitestone, N. Y.

Z

ZACK, H. J. (*M* 1928) Prop., The Zack Co., 2311 Van Buren St., Chicago 12, Ill.

ZAHNER, Leo W., Sr. (*A* 1944) Owner, ● A. Zahner & Co., 3041-43 Wyandotte, Kansas City 8, and 4434 Madison, Kansas City, Mo.

ZAKI, Hussein M. (*A* 1945; *J* 1941; *S* 1940) Chief Engr., Refrigeration Dept., ● The Tractor & Engineering Co., P. O. B. 366, and 5 Ismail Anwar St., Dokki, Cairo, Egypt.

ZANONE, Henry A. (*A* 1943) Htg. and Vent. Engr., Anderson Plumbing & Engineering Co., 1901-1913 W. Main St., Louisville, and ● Rt. 1, Box 441, Shively, Ky.

ZAVORSKI, Leonard (*M* 1944) Vice-Pres. in charge of Prod., Tuttle & Bailey, Inc., and ● 6 Lake Ct., New Britain, Conn.

ZEIGLER, Donald D. (*J* 1944; *S* 1942) Lt., Propeller Laboratory, Wright Field, Dayton, Ohio.

ZELLAK, Joseph (*A* 1944) Vice-Pres., Sauer Co., Inc., 868 N. Washington Ave., Box 4657, Fort Hayes Station, and ● 1928 Baldridge Rd., Columbus, Ohio.

ZENAN, John G. (*M* 1948) Designing Engr. (Supvsr.), Paramount Pictures, Inc., 5451 Marathon, Los Angeles, and ● 11102 Archwood Pl., North Hollywood, Calif.

ZIBOLD, Carl E. (*M* 1929) Mech. Engr., Htg. and Vent., War Dept., Service Command Engrs., 270 Broadway, New York, and ● 13 Chadwick Rd., White Plains, N. Y.

ZIEBER, W. E. (*M* 1935) Dir. of Research, ● York Corp., and 22 S. Keesey St., York, Pa.

ZIEL, Herbert E.* (*M* 1941) Mech. Engr., ● Albert Kahn Assocs., Archts. & Engrs., Inc., 345 New Center Bldg., and 694 Glynn Ct., Detroit 2, Mich.

ZIEMBA, Walter P. (*A* 1945) Draftsman, ● N. B. Hubbard, 220 Bagley, Detroit 26, and 19732 Kenosha, Detroit 24, Mich.

ZIESSE, Karl L. (*A* 1931) Partner, Phoenix Sprinkler & Heating Co., 115 Campau Ave., N.W., Grand Rapids, Mich.

ZIEVE, Edward R. (*J* 1948; *S* 1946) Asst. to Air Cond. Mgr., Clarage Fan Co., Portage St., and ● 1019 W. Kalamazoo Ave., Kalamazoo, Mich.

ZIMMERMAN, Richard F. (*A* 1948) Mgr. and Owner, ● R. F. Zimmerman & Co., Box 1721, 1121 Spring St., and 152 Albany St., Shreveport, La.

ZINGHEIM, William C. (*M* 1943) Owner, ● William C. Zingheim Co., 450 E. Ohio St., and 8541 Drexel Ave., Chicago, Ill.

ZINK, David D. (*M* 1931) Chief Mech. Engr., George Dahl, Archts. & Engrs., 1920½ Main St., Dallas 1, and ● 3622 Mockingbird Lane, Dallas 5, Texas.

ZINTEL, George V. (*A* 1941) Sales Engr., Himelblau Byfield & Co., 36 Throop St., Chicago, and ● 1428 Summerdale, Chicago 40, Ill.

ZUBER, Otto C. (*A* 1938) Chief Engr., ● Amana Society, Refrig. Div., Amana, and South Amana, Ia.

ZUMBEHL, Lambert E. (*A* 1945) Partner, ● Manufacturers' Sales Co., 2025 Main, Kansas City 8, and 5329 Woodland, Kansas City 4, Mo.

ZUMWALT, Ross (*A* 1941; *J* 1938) Partner, ● Zumwalt & Vinther, 1807 Mercantile Bank Bldg., and 9435 Waterview Rd., Dallas, Texas.

ZWALLY, August L. (*A* 1948) Office Mgr., Standard Brass & Mfg. Co., 901 Hope St., and ● 908 Elmwood Ave., Shreveport, La.

ZWERLING, Seymour J. (*J* 1944) Chief Engr., Triangle Sheet Metal Works, Inc., 115 New Hyde Park Rd., New Hyde Park, L. I., and ● 430 Ocean Pkwy., Apt. 3N, Brooklyn 18, N. Y.

ZYNDA, John R. (*A* 1948; *J* 1942) Mech. Engr., Industrial Builder and Designers, The Austin Co., 2842 W. Grand Blvd., Detroit 2, and ● 8876 Burt Rd., Detroit 28, Mich.

SUMMARY OF MEMBERSHIP

Charter Member	1
Honorary Members	2
Presidential Members	24
Life Members	112
Members	2727
Associate Members	2653
Junior Members	396
Student Members	148
Total	6063

UNITED STATES AND POSSESSIONS

Alabama	15
Arizona	15
Arkansas	12
California	330
Colorado	77
Connecticut	119
Delaware	13
District of Columbia	113
Florida	42
Georgia	120
Idaho	4
Illinois	414
Indiana	180
Iowa	66
Kansas	33
Kentucky	24
Louisiana	73
Maine	9
Maryland	70
Massachusetts	155
Michigan	348
Minnesota	215
Mississippi	5
Missouri	246
Montana	6
Nebraska	43
Nevada	9
New Hampshire	4
New Jersey	171
New Mexico	10
New York	623
North Carolina	88
North Dakota	1
Ohio	409
Oklahoma	33
Oregon	96
Pennsylvania	379
Rhode Island	15
South Carolina	20
South Dakota	3
Tennessee	76
Texas	366
Utah	42
Vermont	5
Virginia	84
Washington	87
West Virginia	16
Wisconsin	133
Wyoming	6
Hawaii	5
Puerto Rico	1
	5429
DOMINION OF CANADA	384

FOREIGN COUNTRIES

Argentina	9
Australia	12
Belgium	3
Bermuda	1
Brazil	7
Canal Zone	1
Central America	1
Chile	2
China	9
Cuba	3
Denmark	3
Dominican Republic	1
Egypt	12
England	87
France	10
Holland	2
India	10
Iran	2
Ireland	2
Italy	3
Mexico	9
Netherlands West Indies	2
Newfoundland	2
New Zealand	8
North Africa	1
Norway	2
Nova Scotia	1
Philippine Islands	1
Portugal	1
South Africa	19
South Wales	2
Spain	1
Sweden	11
Switzerland	5
Turkey	3
Uruguay	1
Venezuela	1
	250
TOTAL MEMBERSHIP	6063

LIST OF MEMBERS

(Geographically Arranged)

UNITED STATES *and* POSSESSIONS

ALABAMA

Athens—
Lecureux, E.

Birmingham—
Boehm, R. C.
Gause, H. C.
Gilliland, L. L.
Miller, E. B.
Myer, H.
Walden, H. K.

Dothan—
Manuel, J. B.

Montgomery—
Dowdy, R. B.
Drum, L. J., Jr.
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Aiken, H. H.
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Mason, G. C.

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Tanner, D.
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Shepard, L. W.

Hamden—
Bartlett, G. M.
Burkle, J. L.
Larkin, J. A.

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Bemis, P. D.
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Hummel, D. M.
Johnson, W. A.
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Lawless, A. J.
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North, S. L.
O'Callaghan, L. J.
O'Shea, J. J.
Petty, A. V.
Piske, R. A., Jr.
Player, F. A.
Reil, H. W.
Richards, G. H.
Riggs, O. C.
Rittelmeyer, J. M.
Roberts, S. N.
Rumbold, A. H.
Seat, J. H.
Seckinger, B. J., Jr.
Seepe, P. E.
Sheahan, J. A.
Shumate, J. C.
Smith, A. J.
Sockwell, C., Jr.
Sockwell, T. R.
Stephenson, K. A.
Stoner, W. C.
Streater, W. A.
Strother, W. E.
Sudderth, L., Jr.
Templin, C. L.
Tucker, T. T.
Underwood, J. L.
Van Nouhuys, H. C.
Wagner, L. D.
West, J. H.
West, W. P.
Wilson, M. J.
Wise, M. W.
Yancey, R. H., III

Augusta—
Amphlett, A. L. M.
Arndt, H. W.
Holland, G. R.

Avondale Estates—
Ware, J. H., Jr.

Brunswick—
Gilmore, J. L.

College Park—
Croley, J. G.

Columbus—
Rambo, C.
Wages, R. W.

Decatur—
Beach, R. L.
Eberhart, J. F.
Goode, A. E.

Dunwoody—
Sockwell, C., Sr.

East Point—
Anderson, E. A.

Fort Valley—
Otts, J. G.

Macon—
McKay, A. W.

Marietta—
Small, R. A.
Stotz, R. B.
Yancey, F. V.

Pelham—
Curry, W. H.

Rossville—
Achey, H. N.
Achey, H. S.
Callaway, J. H.

Savannah—
Eisenberg, M. F.

Toccoa—
Donovan, R. F.

IDAHO

Boise—
Berkeley, C. D.
Lessinger, E. F.

Pocatello—
Fereday, M.

Twin Falls—
Detweiler, J. R.

ILLINOIS

Aurora—
Dreyer, M. C.
Jungels, J. W.
Stevens, W. B.

Batavia—
Derby, M. R.

Beardstown—
Beatty, J. W.

Bellwood—
Young, B. C.
Young, J. W.

Berwyn—
Lobstein, M. C.

Bloomington—
Magirl, W. J.
Nesmith, O. E.
Palmer, N. A.
Soper, H. A.
Whitmer, R. P.

Blue Island—
Fay, A. C.

Carbondale—
Owen, C. E.
Owen, C. E., Jr.

Carterville—
Colp, J. L.
Owen, F. W.

Champaign—
Markland, C. E.
Mazer, J. L.
Roose, R. W.

Chicago—
Abramson, R. J.
Adams, W. J.
Aeberly, J. J.
Allen, A. B.
Ammerman, A. S., Jr.
Anderson, C. O.
Anderson, G. A.
Anderson, H. E.
Anoff, S. M.
Avery, E. G.
Bain, L. F.
Bamond, M. J.
Banach, C. J.
Baumann, A. W.
Becker, C. S.
Beery, C. E.
Birner, I. L.
Bishop, M. W.
Bevington, C. H.
Bladen, A. M.
Blaker, A. H.
Bleier, F. P.
Bodinus, W. S.
Boles, H. S.
Borrquist, G. W.
Boston, E. B.
Boyle, J. R.
Brackett, W. H.
Braun, L. T.
Breyer, F.
Brigham, C. M.
Brooke, I. E.
Broom, B. A.
Brown, A. P.
Brown, E. B., Jr.
Buckley, M. L.
Bueter, N. E.
Burgess, R. H.
Burnam, C. M., Jr.
Byerley, F. A., III
Casey, B. L.
Chapin, H. G.
Christmann, W. F.
Christophersen, A. E.
Clifford, L. F.
Clo, H. E.
Close, J. W.
Coffey, G. B.
Connell, L. L.
Connors, E. C.
Conway, F. J.
Coogan, J. T.
Couch, H. J.
Coulter, T. H.
Cranage, T.
Crone, C. E.
Crose, O. P.
Cross, R. C.
Cummiskey, J. F.
Dannehy, J. J.
Dasing, E.
Dauber, O. W.
De Land, C. W.
Elmzen, H. R.
Emmert, L. D.
Emmett, J., Jr.
Endo, H.
Engonopulos, B. G.
Epstein, L.
Ericsson, E. B.
Fakter, M.
Fischer, W. F.
Foran, L. E.
Frank, J. M.
Frazee, F. B.
Freyder, G. G.
Gellert, L. W.
Getschow, R. M.
Gillespie, H. M.
Goelz, A. H.
Goodman, W.
Gothard, W. W.
Gotschall, H. C.
Gragg, H. G.
Graves, C. C.
Gray, S. A.
Gregornik, N. A.
Griffin, C. J.
Gritschke, E. R.
Grubbs, J. K.
Gupta, N. L.
Gustafson, C. A.
Haas, S. L.
Haines, J. J.
Hand, W. L.
Hanley, T. F., Jr.
Hansen, J. S.
Hart, H. M.
Hashagen, J. B.
Hattis, B. S.
Hattis, R. E.
Hayes, J. J.
Heitman, J. G.
Helland, A. E.
Hellmers, C. C., Jr.
Hieronymus, R. E.
Hill, E. V.
Himelblau, H.
Hinckley, H. B.
Hochschulz, A.
Hofmann, E. A.
Hoskins, W. G.
Howatt, J.
Hubbard, G. W.
Hustoel, A. M.
Ingersoll, R. S.
Johnson, B. A.
Johnson, C. W.
Jung, H. G.
Kaiser, F.
Keating, A. J.
Keeney, F. P.
Keeton, R. W.
Kehm, H. S.
Kelley, W. P.
Kenney, D. F.
Kerr, A. W.
Kimbrough, C. W.
Kincaid, W. V.
King, A. C.
King, J. S.
Knox, W.
Kolber, I. A.
Kreisman, H.
Krogman, W. L.
Kucera, H. T.
Kuechenberg, W. A.
Kuglin, C. R.
Lagodzinski, H. J.
Lang, L. P.
Langford, D. R.
Lappin, F. S.
La Roi, G. H., II
Lauterbach, H., Jr.
Lebowitz, M. F.
Lenone, J. M.
Lewis, S. R.
Lichten, E. B.
Lippitt, A. W.
Litwack, H. E.
Lodge, R. H.
Lund, J. F.
Malone, D. G.
Malvin, R. C.
Mandell, L. D., Jr.
Manny, J. H.

Martin, A. B.
Martin, W. J.
Matchett, J. C.
Mathis, E.
Mathis, J. W.
Mattingly, M. F.
Mautner, E. W.
May, A. O.
May, M. F.
McCauley, J. H.
McClellan, J. E.
McDonnell, E. N.
McRae, M. W.
Mehaffey, R. V.
Merens, S. H.
Mertz, W. A.
Miller, F. A.
Miller, O., Jr.
Miller, R. T.
Milliken, J. H.
Moore, R. S.
Morey, A. A.
Mueller, H. C.
Muessig, J. W.
Mullholland, K. L.
Nelson, A. N.
Nelson, R. O.
Nesteruk, W. M.
Newport, C. F.
Offen, B.
Olsen, C. F.
Ostermeier, E. J.
Patten, J. E.
Paul, L. O.
Peterson, W. E.
Philippi, J. J.
Pickett, C. A.
Pierce, J. D.
Pogue, R. B.
Pope, S. A.
Potvin, L. J.
Powers, F. W.
Prentice, O. J.
Price, C. E.
Raider, G. K.
Raymond, F. I.
Rea, R. F.
Reger, H. P.
Reichelt, E.
Rex, H. E.
Rietz, E. W.
Roche, J. M.
Rottmayer, S. I.
Runge, N. P.
Sachs, S.
Sander, A. J.
Schaefer, A.
Scharres, J. W.
Scheidecker, D. B.
Schulein, L. E.
Scott, J. C.
Senk, E. P.
Shields, R. W.
Shultz, E.
Snyman, G. C.
Solstad, L. L.
Spencer, R. M.
Spielmann, G. P.
Stahl, W. A.
Stermer, C. J.
Stevens, H. C.
Stevenson, M. J.
Stout, A. G.
Streb, L. H.
Sundeen, E. E.
Swanson, N. W.
Swart, H. G.
Thomsen, N. B.
Tiller, L.
Tobin, J. F.
Townsend, J. M.
Trickler, E. E.
Trumbo, S. M.
Turner, G. G.
Tuttle, A. A.
Van Epps, H. H.
Van Weelden, M. J.
Vreuls, C. M.
Walker, K. A.
Walsh, T. A.
Walters, W. T.
Ward, O. G.
Waterfall, W.
Weil, M.
Weiss, A. J.
Wendt, E. H.
Wesby, V. L.
Wheeler, H. E.
White, E. B.
Whitehead, E. R.
Widdowfield, A. S.
Williams, E. B.
Wilson, W. H.
Wirth, E. D.
Wittenmeier, F. G.
Wolfe, C. E., Sr.
Zack, H. J.
Zingheim, W. C.
Zintel, G. V.

Decatur—
Keller, D. L.

Deerfield—
Lige, W. W.

Des Plaines—
Allshouse, I. P.
Lockhart, H. A.

Dixon—
Riopelle, W. J.

Downers Grove—
Ostermeier, D. E.
Peterson, J. E.

East St. Louis—
Bemarkt, G. H.
Williams, K. O.

Elgin—
Anderson, C. C.
Gavelek, W. A.
Grossman, F. A.
Johnson, R. A.

Elmhurst—
Gaylord, F. H.

Evanston—
Crump, A. L.
Fraser, G. M.
Jefferson, C. H.
Jennings, B. H.
Kearney, J. S.
Oosten, L. S.
Pfister, V. A.
Schroeder, W. R.
Walters, A. L.

Franklin Park—
Leuthesser, F. W., Jr.

Glencoe—
Mittendorff, E. M.

Glen Ellyn—
Sherman, V. L.

Glenview—
Nightingale, G. F.

Harvey—
Wright, L. T., Jr.

Highland Park—
Arenberg, M. K.

Homewood—
Wilkinson, F. J.

Hubbard Woods—
Alschuler, J. H.

Jackson—
Ludlow, H. M.

Kewanee—
Bronson, C. E.
Dickson, R. B.
Hartman, J. M.
Palmer, E. M.
Russell, W. B.

La Grange—
Eaton, B. K.
Emerson, E. K.
Estep, L. G.
Kavanagh, P. E.

La Grange Park—
Maylard, J. B.

Lansing—
Clarke, J. H.

Maywood—
Stamps, H. F.

Mendota—
Roland, J.
Sormane, W.

Midlothian—
Fairbairn, J. K.

Moline—
Beling, E. H.
Holuba, H. J.
Nelson, A. W.
Nelson, R. H.

Monmouth—
O'Daniel, J. A.

Morton Grove—
Dell, J. A.
Gossett, E. J.
Moore, R. E.
O'Connell, P. M.
Patterson, R. A.
Pullum, C. E.

Mount Prospect—
Nessell, C. W.
Schuetz, C. C.
Schwerman, C. H.

Mt. Vernon—
Benoist, L. L.
Benoist, R. E.

Northbrook—
Prebensen, H. J.

North Chicago—
Marschall, P. J.

Oak Lawn—
Towner, C. E.

Oak Park—
Borzello, N.
Deyo, C. D., Jr.
Doody, F. A.
Fitzgerald, M. J.
Glover, R. P.
Johns, H. B.
Keller, A. B.
May, E. M.
Meiller, D. V.
Smith, L. J.
Strong, A. P., Jr.
Tracy, W. E.
Uhlhorn, W. J.

Ottawa—
Bazzoni, J. P.

Park Ridge—
Berzelius, C. E.
DuBois, L. J.
Floreth, J. J.
Heckel, E. P.
Heckel, E. P., Jr.
Mench, J. G.
Sutcliffe, A. G.

Pecatonica—
Washington, L. W.

Peoria—
Abendroth, H. F.
Hauer, F. W.
Hull, E. O.
Meyer, F. L.

River Forest—
Hudson, R. B.
Richmond, K. C.
Wempe, R. H.

Rockford—
Braatz, C. J.
Browne, S. D.
Debes, C. N.
Kennedy, W. W.
Lathers, V. M.
Lester, E. A.
McGavock, E. A.
Stewart, D. J.

Rock Island—
Kimble, C. W.

Springfield—
Long, E. J.
Sharp, J. E.

Urbana—
Bareither, H. D.
Buckley, N. A.
Carroll, J. R., Jr.
Fahnestock, M. K.
Fellows, J. R.
Harris, W. S.
Helfinstine, R. J.
Konzo, S.
Kratz, A. P.
Severns, W. H.
Stenn, S.
Willard, A. C.

Vandalia—
Connors, F. E.

Warrenville—
Aronson, H. H.

Waukegan—
Huhn, W. E.

Wheaton—
Sommerfield, S. S.

Wilmette—
Narowetz, L. L., Jr.
Thompson, F. W.

Winnetka—
Brunn, C. G.
Killian, V. J.

Wyoming—
Bedard, E. L.

INDIANA

Anderson—
Dean, C. H.

Carmel—
Wallace, R. R.

Columbus—
Young, G. H.

East Chicago—
Evanson, M.

Elkhart—
Meyer, R. P.

Evansville—
Berry, N. E.
Boyer, C. T.
Knighton, J. K.
Koenig, A. C.
Pierce, H. C.
Wiegand, H. M.
Wright, J. F.

Fort Wayne—
Case, D. V., Jr.
Hattersley, E. H.
Pressler, J. D.
Reed, V. E., Jr.

Roth, J. L.
Sinish, W. R.
Winner, R. J.

Gary—
Kirtland, E. M.

Greencastle—
Perry, M. A.

Greenfield—
McQueen, B.

Hagerstown—
Hagen, R. T.

Hammond—
Callis, D. K.

Huntingburg—
Collins, J.

Huntington—
Redrup, W. D.
Smith, G. W.

Indianapolis—
Alexander, H. V.
Allen, A. G.
Allen, J. L.
Ammerman, C. R.
Arzet, F. A.
Babcock, D.
Barton, F. C.
Bearden, J. D.
Bevington, W. C.
Blackman, R. C.
Blackwell, J. S.
Boone, F. S.
Bradfield, J. L.
Bragg, R. E.
Buschmann, A. W.
Carlson, C. J.
Clark, L. W.
Clarke, J. L.
Clemens, J. E.
Cockley, J. E.
Colby, J. R.
Cotton, I. W.
Davis, T. R.
Dickson, D. R.
Dillon, D. A.
Donie, R. A.
Drum, R. I.
Dwyer, W. H.
Dwyer, W. H., Jr.
Elliott, J. H.
Ely, J. W.
Fenstermaker, S., Jr.
Fenstermaker, S. E.
Fenstermaker, W. R.
Fischer, F. C.
Fox, W. L.
Freije, W. F.
Garber, W. E., Jr.
Goebel, H. A.
Gombert, F. S.
Goohs, W. E.
Grear, W. W.
Griswell, H. D.
Hagedon, C. H.
Hague, W. S.
Hardin, J. T.
Hayes, G. J.
Hayes, J. G.
Heidenreich, G.
Helwig, E. C.
Hoffmann, W. A.
Hosmer, G. H.
Hoyt, R. A.
Jackson, G. O.
Jackson, J. W.
Jackson, R. O.
Janitz, R. H.
Jehle, F.
Johnson, H. F., Jr.
Jordan, P. R.
Joslin, G. C.
Kelm, E. C.
Lee, C. M.
Lindeman, C. F.
Locke, C. F. A.
Malm, E. L.
McDaniels, J. A.
McGeary, P. W.
Morris, B.
Morrison, F.
Mulrey, M. D.
Newton, A. E.
Niesse, J. H.
Novak, G. J.
Nyland, J. A.
Paetz, G. A.
Payton, J. F.
Perham, S. H.
Pfau, A. C.
Pherigo, F. S.
Post, G. A.
Pruitt, C. H.
Roche, A. O., Jr.
Rotz, J. M.
Ryan, K. W.
Sanbern, E. N.
Schwitzer, L., Jr.
Shuttleworth, R.
Simmons, G. P.
Simmons, N. L.
Simmons, N. M.
Skinner, N. D.
Stevens, H. R.
Stickle, F. A.
Supple, G. B.
Vogel, G. W.
Waldon, O. D.
Warren, C. N.
Weiland, C. C.
Wesner, E. L.
Whittington, W. P.
Will, C. A.
Williams, G.
Williams, G. M.
Wolf, R. L.

Lafayette—
Beery, V. L.
Boester, C. F.
Henze, A. L.
Montague, F. H.
Montgomery, T. F.
Morse, F. B.
Walker, K.

La Porte—
Bard, W. S.
Dring, R. W.
Shrock, J. H.
Tenkonohy, R. J.

Lebanon—
Coryell, G. L.

Logansport—
Baker, T. A.

Marion—
Liniger, R.

Michigan City—
Stockwell, W. R.
Westphal, E. R.
Westphal, N. E.

Milford—
Scott, A. C.

Monrovia—
Voorhees, G. A.

Monticello—
Younger, R. D.

Muncie—
Davis, W. M.
Price, C. F.
Shreeve, L. D.

Noblesville—
Jennings, J. H.

North Judson—
Cunningham, J. S.

Oaktown—
Bolin, H. W.

Peru—
Thrush, H. A.

South Bend—
Davis, W. L.

Terre Haute—
Belden, A. G., Jr.
Stuart, R. A.

Vincennes—
O'Donnell, L. D.

West Lafayette—
Anik, B.
Baker, M.
Barnard, W. B.
Bridgers, F. H.
Deverall, C. R.
Hambley, C. J.
Jacks, P. E.
James, R. G.
Kercheval, W. L.
Knox, A. E.
Menke, A. C.
Merker, W. T.
Miller, W. T.
Priest, C. R.
Timmis, W. W.
Touloukian, Y. S.
Vanderford, J. R.
Warner, C. F.

IOWA

Ackley—
Nelson, G. O.

Amana—
Zuber, O. C.

Ames—
Gould, M. E.
Sandfort, J. F.
Schroeder, D. E.
Thom, H. C. S.

Bettendorf—
Stock, C. S.

Cedar Rapids—
Engskow, J. C.
Holbrook, J. A.
Messenger, A. R.
Nyquist, J. D.
Schultz, C. W.

Cherokee—
Miller, M. S.

Council Bluffs—
Edelman, H. W.
Magarrell, K. R.

Davenport—
Brooke, J. O.

Des Moines—
Anderson, E. R.
Bartels, E. M.
Borg, E. H.
Campbell, B.
Dawson, R. E.
Dolge, E. A.
Duitch, P. R.
Frankle, H. R.
Gebuhr, J. V.
Helstrom, C. W.
Johnson, T. R.
Kline, F. L.
Landes, B. E.
La Rue, P.
Lindholm, W. D.
McCarthy, F. W.
McGuiness, C. H.
Murphy, D. C.
North, C. P.
Olson, E. O.
Osborn, F. W.
Schnell, R. H.
Schuler, W. B.
Schwirtz, B. A.
Stuart, W. W.
Summerville, E. A.
Tappen, M. M.
Triggs, F. E.
Tritle, H. J.
Wells, D. E.
Wheeler, C. A.

Iowa City—
Croft, H. O.

Marshalltown—
Booth, R. W.
Stover, R. S.

Ottumwa—
Brady, G. A.

Plymouth—
Friedline, J. M.

Sioux City—
Farkas, F. S.
Hagan, W. V.
Hartnett, D. E.
Nelson, F. L.

Washington—
Norton, L. I.

Waterloo—
Burch, W. E.
Evans, S. M.
Hedeen, L. E.
Herbert, R. M.
Smith, S. T.
Todd, M. L.
Winterbottom, J. W.
Winterbottom, R. F.
Young, D. H.

KANSAS

Atchison—
Case, D. V.

Fort Leavenworth—
Marston, A. D.

Great Bend—
Morrison, W. L.

Hutchinson—
Stevens, H. L.

Junction City—
Froelich, H. A.

Kansas City—
Arthur, J. M., Jr.
Betz, H. D.
Degler, H. E.
Edge, A. J.
Henry, R. W.
Mart, L. T.
Massaglia, P. E. C.
McMichael, C. L.
Radotinsky, J. W.

Lawrence—
Robb, J. E.

Leavenworth—
Roser, E., III

Manhattan—
Gould, J. L.

Overland Park—
Brown, N. L.
Newbanks, N. N.
Roark, I. L., Jr.

Salina—
Gage, B. B.
Ryan, W. F.

Sunflower—
Lytle, W. T.
Mathey, N. J.

Topeka—
Dees, L. L.
Graves, C. S.
Loebsack, V. H.

Wichita—
Bauer, R. F.
Jenner, J. W.
Kice, J. W.
Olds, D.
Turner, W. M.
Yoe, C.

KENTUCKY

Covington—
Kummer, C. J.
Thompson, E. B.

Ft. Knox—
Ruemmele, A. M.

Frankfort—
Roush, B. B.

Lexington—
Cropper, R. O.
Tenney, D.

Louisville—
Groot, H. W.
Hellstrom, J.
Hubbuch, N. J., Jr.
Jones, H. S.
Kane, J. M.
Mattimore, J. D.
May, J. W.
Murphy, H. C.
Nutting, A.
Pound, H. W.
Reed, J. C.
Ronald, E. R.
Weekes, R. W.

Owensboro—
Bottorf, J. D.

Paducah—
Slattery, P. H.
Youngblood, C. W.

Shively—
Zanone, H. A.

Somerset—
Smith, V. D.

LOUISIANA

Bossier City—
Daniel, D. C.

Houghton—
Cheatwood, W. H.

Lake Charles—
Heinisch, J. E.

Monroe—
Phillips, M. E.

New Orleans—
Adair, J. S.
Bankston, C. V.
Bean, T. H., Jr.
Bryner, J. J.
Burke, J. S.
Burns, F. G.
Busenlener, L. V.
Calongne, H. J., Jr.
Clay, W. L.
Cooke, W.
Crary, J. O.
Cressy, L. V.
Daussat, W. J.
Dudley, W. H., Jr.
Eckhardt, E., Jr.
Elizardi, R.
Feitel, J. V.
Fischer, F. P.
Flettrich, H. L.
Friedler, J. J., Jr.
Gamble, C. B.
Goode, R. K.
Graham, F. D.
Grant, W. H., Jr.
Green, T. Z.
Guest, R. B.
Gutknecht, F.
Helwick, N. J.
Hero, G. A., Jr.
Holzer, R. J., Jr.
Jenny, T. J.
Jordy, J. J.
Karchmer, J. H.
Kelly, H. J.
Kerr, G. C.
Lane, C. W.
Livaudais, M.
Maxwell, L. R.
May, G. E.
Moses, W. B., Jr.
Moses, W. G.
Moynan, J. S.
Nelson, L. K.
Offner, T.
Oster, W. P.
Poujade, J. V.
Prats, S. N.
Reed, C. E.
Ricks, P. G., II
Rothrock, R. K.
Salaun, H. L.
Salzer, A., Jr.
Smith, E. A.
Stokes, T. A.
Thoman, E. O.
Waldo, H. J.
Weatherby, E. P., Jr.
Weil, L. S.

Shreveport—
Beaty, S. W.
Dykes, O. J., Jr.
Fitzgerald, W. E.
Kearby, E. J.
Menefee, J. I.
Otto, A. H.
Parsons, L. D., Jr.
Rottmann, P. O.
Stravolemos, E.
Zimmerman, R. F.
Zwally, A. L.

West Monroe—
Atkins, O. H.

MAINE

Auburn—
Fowles, H. H.

Bangor—
Prince, R. F.

Portland—
Fels, A. B.
Haynes, C. V.
Leland, W. B.
Lunt, W. F.
Marsh, G. R.
Merrill, C. J.

Sanford—
Stilphen, N. E.

MARYLAND

Annapolis—
Minick, A. L.

Anne Arundel County—
Johnston, R. M.

Baltimore—
Chinn, G. I.
Collier, W. I.
Crabbin, W. W.
Crosby, E. L.
Dehler, F. C.
Dressell, R. E.
Dukehart, M. M.
Earp, S.
Flanigan, W. P.
Fuller, C. W.
Gerhardt, E. D.
Glaser, H. D.
Haines, F. H.
Harris, H. M.
Hauf, J. C., Jr.
Kent, E. R.
Leilich, R. L.
Levitt, L. L.
Mac Gann, L. S.
Malone, J. F.
Mathaney, E. H.
Mayer, W. J.
McCrea, L. W.
Morris, E. J.
Nest, R. E.
Peters, B. G.
Posey, J.
Priester, G. B.
Roche, G. J.
Seiter, J. E.
Smoot, T. H.
Snyder, E. J.
Stokes, A. D.
Taze, E. H.
Vance L. G.
Vincent, P. J.

Bethesda—
Goodwin, E. W.
Gregg, S. L.
Markert, J. W.

Cambridge—
Daniel, C. E.

Chevy Chase—
Beitzell, A. E.
Beline, M. B.
Frankel, G. S.
Humphrey, L. G., Jr.
Robeson, B. P.

College Park—
Carleton, H. G.

Cumberland—
Griffith, C. A.

Edgewater Beach—
Merle, A.

Elkton—
McCloskey, J. H.

Glen Burnie—
Rodgers, J. S.

Hyattsville—
Mitchell, A. E.

Kensington—
McKim, P. H.
Spurney, F. E.

Landover—
Norrington, W. L.

Laurel—
Alexander, J. W.

Rainier—
Barber, R. C.

Rockville—
Brunett, A. L.

Silver Spring—
Eagleton, S. P.
King, W. O.
Martin, W. A.
McArdle, F. E.
Shuman, L.
Stack, A. E.

Stoneleigh—
Peters, C. J.

Takoma Park—
Flagg, L. F.
Godbold, B. P.
Morton, H. S.
Russell, B. A.

MASSACHUSETTS

Acton—
Gates, J. N.

Andover—
Wilson, A. M.

Arlington—
Brenton, R. S.
Kenney, D. J.

Arlington Heights—
Tarr, H. M.

Ashland—
Jones, F.

Auburndale—
Ahearn, W. J.

Belmont—
Fitch, W. R.
Shipp, W. H.

Boston—
Archer, D. M.
Bell, W. C.
Bernard, E. L.
Bonner, J.
Brigham, F. H.
Brinton, J. W.
Buchanan, W. P.
Campia, O. J.
Cashin, W. K.
Colby, J. H.
Cole, H. S.
Donohoe, J. B.
Dover, D. E.
Dow, C. H.
Drinker, P.
Dusossoit, E. A.
Farnum, W. S.
Field, E.
Geissenhainer, L. R.
Hare, A. L.
Hart, T. S.
Hoagland, E. J.
Jennings, W. G.
Kelley, J. J.
Kimball, C. W.
Licandro, J. P.
McCoy, T. F.
Means, J. M.
Merrill, F. A.
Miller, D. C.
Pettingell, J. M.
Ritter, I. S.
Shaer, I. E.
Swaney, C. R.
Tierney, L. J. J.
Tuttle, J. F.
Von Rehberg, H. L.
Waterman, J. H.
William, F. C.
Yaglou, C. P.

Brookline—
Flint, C. T.

Cambridge—
Blair, D. W.
Dawson, F. C.
Gerrish, G. B.
Hesselschwerdt, A. L., Jr.
Holt, J.
Peterson, C. M. F.
Saurwein, G. K.
Shedroff, D. I.
Spence, R. A.
Wilkes, G. B.

Canton—
Carlson, E. E.

Charlestown—
Mann, L. B.

Chestnut Hill—
McDonald, J. J.

Dorchester—
Ehrenzeller, A.
Goodrich, C. F.
Hosterman, C. O.
Kingsbury, N. E.
Landau, M.
Sullivan, R. P.

Dover—
Lincoln, R. L.

East Boxford—
Shaw, B. E.

Fall River—
Walmsley, A. E.

Fitchburg—
Dolan, W. H.
Illig, E. E.
Illig, W. R.
Karlson, A. F.
McKittrick, P. A.

Granville Center—
Cross, R. E.

Harwich Port—
Maxwell, G. W.

Holyoke—
MacDonald, G. D.

Hyde Park—
Austin, W. H.
Bartlett, A. C.
Blair, H. A.
Ellis, F. R.
Holmes, R. E.
Huggins, L. G.
Jones, F. C., Jr.
Minkler, W. A.
Tillotson, J. J.
Van De Weghe, R. C.

Lancaster—
Taggart, R. C.

Lawrence—
Bride, W. T.

Lenox—
Woodger, H. W.

Leominster—
Kern, R. T.
Torrens, G. B.

Lynn—
Farrow, H. L.

Marblehead—
Sprague, G. W.
Williams, W. A.

Mattapan—
Brown, M.

Medford—
Brissette, L. A.
Warner, C. A.

Melrose—
Franklin, R. S.
Richards, L. V.

Milton—
Collins, D. M.
Sheffield, R. A.
Turnbull, F. J.

Nantucket—
Edgarton, L. S.

Natick—
Meredith, J. W.

Needham—
Goodwin, W. C.
Webb, J. S.

New Bedford—
Belanger, W.

Newton—
Levine, L. J.
Martin, H. L.

Newton Centre—
Curry, R. F.
Shaw, N. J. H.

Newtonville—
Emerson, R. R.
Moore, H. C.

Northampton—
Burrows, A. J.

North Quincy—
Parker, H. E.

Pittsfield—
Nicholls, J. M.

Revere—
Brayman, A. I.
Cail, M. L.
Foulds, P. A. L.

Rockland—
Allison, W. F.

Roslindale—
Larson, C. W.

Salem—
Masterson, W. R.

Somerville—
Whitten, H. E.

South Boston—
Dane, I. S.

South Weymouth—
York, J. E.

Springfield—
Lovenberg, A. M.
McClean, F. C.
Murphy, W. W.

Stoneham—
Fava, A. A.

Waban—
McMullen, E. W.
Sack, H. S.

Ware—
Scott, D. C.

Watertown—
White, P. H.
Wiegner, H. B.

Wellesley Hills—
Barnes, W. E.
Groves, S. A.

Westfield—
Smith, S. K.

Westford—
Duncan, L. P.

West Newton—
Burbo, W. G.
Hodgkinson, W. S.
Wahlin, B. J.

West Roxbury—
Krapohl, W. H.
McPherson, W. A.

Winchester—
Carrier, E. G.
Doherty, J. J.

Wollaston—
Blair, E. L.

Worcester—
Bachmann, W. L.
Callan, J. J., Jr.
Kolb, R. P.
Walsh, J. W.
Wechsberg, O.

MICHIGAN

Albion—
Gable, H. R.

Allen Park—
McIntosh. R. M.

Alto—
Wieland, J. J.

Ann Arbor—
Arar, R. M.
Briskin, B.
Calhoon, F. N.
Clark, J. W.
Epple, A. B.
Kammeraad, K. J.
Kessler, C. F.
Kerai, M. R.
Lee, C. C.
Lesley, P. F., Jr.
Linsky, B.
Marin, A.
Nyman, R. A.
O'Bannon, L. S.
Schrock, R. E.
Wigglesworth, G. L., Jr.

Battle Creek—
Burtis, H. D.
Christenson, H.
Dyer, W. S.
Murray, F. L.
Smith, R. B.

Bay City—
Henry, E. C.
McCoy, F. F.

Birmingham—
Chester, T.
Hadjisky, J. N.
Hyde, E. F.
Schultz, S. F.

Blissfield—
Grew, R. E.

Bloomfield Hills—
Steggall, H. B.

Charlotte—
Oberlin, J. A.

Clarkston—
Watson, W. W.

Comstock Park—
Appelt, J. E.

Dearborn—
Kramer, J. J.
Lemmen, R. N.
Wallace, J. B.

Detroit—
Adam, R. W.
Anderson, E. J.
Anderson, G. W.
Andrew, G. J.
Baker, C. H.
Band, J. P.
Barnum, W. E., Jr.
Barth, H. E.
Baumgardner, C. M.
Bay, C. H.
Beattie, J.
Beecraft, G. A.
Berryman, R. H.
Bichler, J. S.
Biggers, R. H.
Bigham, B. H.
Bishop, F. R.
Blackmore, F. H.
Blair, H. C.
Boales, W. G.
Bolle, F. G., Jr.
Borak, E.
Bottum, E. W.
Brodie, A. H.
Brown, W. A.
Bruce, M.
Burch, L. A.
Busse, H.
Butler, R. P.
Caton, R. R., Jr.
Caughman, R. B.
Cauhorn, A. V.
Champlin, R. C.
Chapman, D. B.
Chappell, H. D.
Clar, R., Jr.
Clark, E. H.
Collins, L. F.
Connell, R. F.
Conover, E. W.
Coon, T. E.
Crawford, F. A.
Cummins, G. H.
Dauch, E. O.
Davis, G. L., Jr.
Deppmann, A. C.
Deppmann, R. L.
Dixon, W.
Dolan, H. P.
Donohoe, C. F.
Dubry, E. E.
Duke, R. Q.
Dull, W. M.
Dunbar, D. H.
Durkee, M. C.
Elliott, N. B.
Emrick, A. A.
Esslinger, L. A.
Ewald, J. H.
Falk, D. S.
Farrell, E. J.
Farrington, W. R.
Feinberg, E.
Ferris, D. M.
Fisher, A. E.
Gallmeier, S. H.
Glanz, E. F.
Goss, M. H.
Grady, E. J.
Griswold, A. S.
Gross, M. H.
Harrigan, E. M.
Hogan, E. L.
Hosman, P. S.
Hubbard, N. B.
Hubbell, N. S.
Hughson, H. H.
Jaffke, W. W.
Johnson, F. W.
Kasameyer, A. L.
Kaufman, H. J.
Kellogg, W. T.
Kilner, J. S.
Kincaide, M. C.
King, D. J.
Kirkpatrick, A. H.
Knibb, A. E.
Kolasa, M. J.
Kuhlman, C. E.
Lee, L. A.
Lees, J.
Lewis, D. H.
Linsenmeyer, F. J.
Livermore, J. N.
Ludwig, A. D.
Luty, D. J.
Mabley, T. H.
Major, L. F.
Mally, C. F.
Martel, C. L.
Marzolf, F. X.

Mason, L. T.
Maurer, L.
Maynard, J. E.
McCarl, H. E.
McCormick, G. W., Jr.
McCrea, J. B.
McGeorge, R. H.
McIntire, J. F.
McLean, D.
McNamara, G. Q.
Mericle, C. D.
Milward, R. K.
Moretti, G.
Morse, C. T.
Morse, L. S., Jr.
Muth, A. J.
Oberschulte, R. H.
O'Gorman, J. S., Jr.
Old, W. H.
Olivieri, J. B.
Ollesheimer, L. T.
Osberger, T. L.
Osgood, H. P.
Paetz, H. E.
Park, J. A.
Parrott, L. G.
Partlan, R. L.
Paterson, R. O.
Pavey, C. A.
Pearson, F. L.
Peterson, D. J.
Petronis, A.
Pfeiffer, G. R.
Pierce, C.
Porte, C. E.
Purcell, F. C.
Randall, R. D.
Randall, W. C.
Reader, J. T.
Robinson, G. W.
Robson, J. W.
Rowe, W. A.
Rubin, L.
Runnings, H. M.
Sanford, S.
Sanger, E.
Saulson, S.
Sawyer, H. C.
Schaarschmidt, K. F.
Scherger, F. J.
Schimpke, B. J.
Selving, H. T.
Shaw, G. W. D.
Sheley, E. D.
Shepperd, P. D.
Shiller, B. P.
Signor, C. W.
Singleton, A. B.
Smith, E. T.
Smith, W. O.
Snyder, J. W.
Spitzley, J. H.
Spitzley, R. L.
Spurgeon, J. H.
Starrett, F. W.
Stites, R., Jr.
Strand, C. A.
Taylor, H. J.
Terry, J.
Toonder, C. L.
Tracy, J. W.
Trambauer, C. W.
Tuttle, G. H.
Tykle, F. G.
Uicker, J. J.
Wagoner, K. J.
Waid, G. H.
Walters, T. A.
Whelan, W. J.
Whittaker, G. S.
Whybrew, G. H.
Wigle, K. G.
Williams, F. H.
Wilson, K. L.
Winans, G. D.
Witheridge, W. N.
Woodson, J. W.
Ziel, H. E.
Ziemba, W. P.
Zynda, J. R.

Dowagiac—
Harden, J. C.
Polad, T. H.
Woodhouse, G. D.

Duluth—
Sher, A. I.

East Lansing—
Anderson, J. T.
Hussain, T. A.
Miller, L. G.
Pesterfield, C. H.

Elberta—
Edwards, W. W.

Excelsior—
Woolman, H. D.

Ferndale—
Lindsley, F. A.
McCaul, L. K.

Flint—
Hendriksen, L.
Young, R. H., Jr.

Gladstone—
Carlsen, H. J.

Grand Rapids—
Alexander, J. L.
Boot, A.
Bradfield, W. W.
Bratt, H. D.
Calcaterra, L. A.
Clarke, W. L.
Dean, V. C.
Evert, M. C.
Goodwin, F. T.
Goote, M.
Jasper, H. C.
Lett, M. A.
Mangrum, R. W.
Marshall, O. D.
McMaster, S. G.
Pulte, J. W.
Schilken, D. R.
Shedd, R. W.
Stafford, T. D.
Swart, R. H.
Van Spriell, L.
Walter, B. J.
Warren, F. C.
Wilson, H. F.
Ziesse, K. L.

Grosse Pointe—
Feely, F. J.
McConachie, L. L.
Patterson, F. H.
Thomas, J. E.

Highland Park—
Green, E. J.
Horner, F. S.
Sanders, G. O.

Hillsdale—
Oxenrider, M.

Holland—
Cooper, B. G.
DeRoo, W. C.
Harbin, F., Jr.
Schultze, D. P.
Weyenberg, H.
Winchester, P. D.

Houghton—
Fricke, R. A.
Wittig, F. E.

Huntington Woods—
Green, D. P.
Keyser, H. M.

Iron River—
Boyd, L. E.

Ishpeming—
Hoff, O. I.

Jackson—
Harrower, W. C.
Kelly, O. A.
Link, C. H.
Minor, J. E.
Page, V. C.
Tilford, L. A.

Kalamazoo—
Bradfield, W. W., Jr.
Brundage, F. W.
Deming, R. E.
Downs, S. H.
Limbacher, H. R.
Mahoney, C. L.
McConner, C. R
Metzger, H. J.
Rupert, J. D.
Saunders, C. V.
Schlicksing, W. G.
Temple, W. J.
Wasson, R. A.
Wilson, R. W.
Wolters, H. W.
Zieve, E. R.

Lakeside—
Royce, R. F.

Lansing—
Aikin, A. A.
Burr, L. R.
Caplan, K. J.
Crisman, L. J.
Distel, R. E.
Faggion, A. J.
Fox, E. C.
Hill, V. H.
Lankton, F. E.
McCauley, D. G.
Miller, J. W.
Parsons, R. A.
Robinson, K. E.
Rupp, C. J.
Thompson, W. G.
Vanderlip, P. J.
Vandervoort, R. B.

Lawrence—
Morton, P. S.

Marlette—
Hurlburt, R. G.

Milford—
Woodbridge, W. L.

Muskegon—
Gibson, H. E.
Hughes, M. W.
Wibalda, R. K.
Young, H. J.

Pleasant Ridge—
Witmer, H. S.

Plymouth—
Wilson, C. H.

Rochester—
Akers, G. W.

Saginaw—
Low, C. J.
Rittenhouse, O. R.
Root, E. B.
Witheridge, D. E.
Witheridge, J. M.

Spring Lake—
Wilson, J. D.

Wayland—
Snook, A. H.

Willow Run—
Stark, R. C.

Ypsilanti—
Jorgensen, E. W.

MINNESOTA

Albany—
Kittleson, H. B.

Anoka—
Linden, M.

Bayport—
Swanson, E. C.

Chisholm—
Vasenius, A. W.

Cloquet—
Anway, H. W.
Schlenk, H., Jr.

Duluth—
Foster, C.

Edina—
Gerrish, D. C.
Meyer, K. A.

Excelsior—
Rowley, F. B.

Hibbing—
Bispala, J. T.

Hopkins—
Quigley, M. E.

Marshall—
Bisbee, B. A.

Minneapolis—
Algren, A. B.
Anderson, G. E.
Anderson, R. O.
Atkinson, R. P.
Baker, J. T.
Balch, R. M., Jr.
Bell, E. F.
Bensen, C. L.
Bjerken, M. H.
Bloom, R. L.
Borry, J. V.
Bowler, R. W.
Bredeson, C. R.
Bren, L. W.
Brown, G. M.
Buck, W. B.
Burns, E. J.
Burritt, C. G.
Burton, W. A.
Butler, R. C.
Campbell, R. L.
Carley, T. S.
Carlson, C. O.
Carlson, R. M.
Chalmers, C. H.
Cilaciyan, A.
Collier, J. R.
Craig, J. A.
Cronstrom, K. A.
Crosby, H. S.
Dahl, L. J.
Dahlstrom, G. A.
Davidson, J. C.
Dinham, R. E.
Eastin, M. R.
Erickson, E. T.
Evans, R. W.
Feilzer, J. H.
Fergestad, M. L.
Ferrara, A. L.
Finnell, E. C.
Forfar, D. M.
Fox, F. J.
Frey, G. W.
Furber, S. L.
Gausewitz, W. H.
Gendein, S.
Gerrish, H. E.
Gerrish, J. K.
Gianos, T. C.

Gorgen, R. E.
Gray, J. D., Jr.
Griefnow, O. W.
Gross, L. C.
Gruenberg, S. B.
Haines, J. E.
Haley, R. T.
Hanson, L. C.
Hanson, L. P.
Harris, H. R.
Harris, R. C.
Heikkinen, H. K.
Helstrom, H. G.
Herman, N. B.
Honey, R. L.
Hovda, A. F.
Huch, A. J.
Huckins, E. R.
Iserman, M. H.
Jahn, W. E.
Jamieson, J. R., Jr.
Jenkins, H. C.
Johnson, H. K.
Johnson, R. W.
Jordan, R. C.
Juhl, E. P.
Kayser, P. G.
Kendrick, G. M.
Kliever, W. H.
Knoblauch, H. K.
Knowles, E. L.
Krause, L. J.
Lamson, F. S.
Lange, F. F.
Larson, C. P.
Larson, C. W.
Lawrence, C. T.
Lee, M. N.
Lee, R. H.
Legler, F. W.
Leighton, A. H.
Lilja, O. L.
Locke, J. S.
Lund, C. E.
Martenis, W. W.
Matthies, L. A.
Mattson, R. K.
McDonald, T.
McLouth, B. F.
Milligan, D. G.
Mills, H. C.
Mooney, B. P.
Morrow, E. J.
Nelson, R. A.
Nelson, V. E.
Nichols, H. R.
Nicols, J. A.
Olson, E. O.
Olson, W. A.
Orr, G. M.
Oslund, D. L.
Parkans, L. M.
Pearson, V. E.
Petersen, C. P.
Porter, H. M.
Quade, H., Jr.
Reiher, H. C.
Reisberg, L. K.
Resch, R. J.
Ries, A. S., Jr.
Roberts, H. P.
Robinson, P. D.
Rosenstein, D. L.
Rudberg, J. A.
Sanders, C. M., Jr.
Schad, C. A.
Schernbeck, F. H.
Schultz, A. W.
Sedgwick, D. E.
Seelert, E. H.
Sierk, H. G.
Smith, S., Jr.
Snyder, E. F., Jr.
Spanton, M. D.
Sperry, H. A.
Squier, R. T.
Stafford, J. F.
Stewart, R. M.
Stiller, F. W.
Svoboda, G. J.
Swanson, A. E.
Taylor, D. G.
Uhl, E. J.
Uhl, W. F.
Walters, R. R.
Weber, W. A.
Whitnah, S.
Wiik, A.
Wiik, E. M.
Williams, H. B.
Wilson, D. P.
Wiser, C. E.

Mound—
Larson, H. B. R.

Olivia—
Pease, L. W.

Owatonna—
Anderson, G. A. M.
Haines, R. W.

Robbinsdale—
Hyde, L. L.
Ruth, R. J.

Rochester—
Adams, N. D.
Swenberg, W. A.

St. Louis Park—
Harris, W. L.

St. Paul—
Anderson, D. B.
Backstrom, R. E.
Barnett, R. E.
Bauer, A. E.
Bean, G. S.
Bergman, A. E.
Blazek, L. J., Jr.
Bostrom, H. R.
Colman, R. C.
Custer, J. B.
Estes, E. C.
Gausman, C. E.
Hamm, J. G.
Healy, D. L., Jr.
Hickey, D. W.
Hultgren, J. T. B.
Johnson, E. A.
MacKenzie, J. M.
McClung, K. R.
McNamara, W.
Miller, K. W.
Oberg, H. C.
Otto, R. W.
Paine, H. A.
Persson, N. B.
Peterson, J. R.
Ruff, D. W. C.
Rugg, H. H.
Ruud, R. E.
Sandberg, J. A.
Sanford, A. L.
Schampel, H. B.
Schneeberg, F. H.
Shimazaki, T. T.
Shorba, M.
Sturm, W.
Sweeney, R. H.
Webber, E. C.
Winterer, F. C.
Wunderlich, M. S.

St. Peter—
Forderbrugen, K. J.

MISSISSIPPI

Clarksdale—
Kremser, R. C., Jr.

Columbus—
Norris, C. G.

Lumberton—
Stevenson, D. B., Jr.

Meridian—
Mann, I. W., Jr.

Vicksburg—
Stepan, T. E.

MISSOURI

Brentwood—
Bishop, A. C.

Clayton—
Isaacson, I., Jr.
Kaenter, R. J.
Russell, W. A.
Smith, R. C.
Van Alsburg, J. H.
Weber, E. F.

Eureka—
Kingsland, G. D.

Ferguson—
Barsha, N. B.
Otten, W. A.
Szombathy, A. R.
Szombathy, L. R.

Glencoe—
Disney, M. A.

Glendale—
Saenger, L. W.

Hannibal—
Wilson, G. H.

Jefferson City—
Wagner, W. J. O.
Woodman, L. E.

Joplin—
Gaines, E. F.
Jones, J. T.
Rainey, H. D.
Satterlee, H. A.

Kansas City—
Adamson, L. C.
Allen, D. M.
Allen, R. C., Jr.
Atwater, H. A.
Ball, W.
Barnes, A. R.
Barnes, J. G., Jr.
Brackmann, W. H.
Bruce, L. E.
Caleb, D.
Campbell, E. K.
Campbell, K.
Campbell, R. P.
Cantwell, A. B.
Cassell, W. L.
Cheasley, T. C.
Clegg, C.
Conroy, W. T.
Cook, B. F.
Cover, E. B.
Dahms, A. A.
Davis, C. A. L.
Dean, F. J., Jr.
Dodds, F. F.
Downes, N. W.
Dukelow, J. S.
Durbin, S. A.
Dyer, W. K.
Ehlers, F. G.
Faust, H. G., Jr.
Fehlig, J. B.
Fehlig, J. B., Jr.
Flarsheim, C. A.
Forslund, O. A.
Gay, C. E., Sr.
Gillham, W. E.
Gould, H. E.
Haas, E., Jr.
Harbordt, O. E.
Harryman, M. M.
Harvey, E. W.
Heaven, L. P.
Heckert, W. P.
Holton, W. J.
How, R. F.
Howarth, W. E.
Izard, L. W.
Jacobson, A. D.
Jacobson, E. L.
Jones, C. D.
Jones, T. S.
Ladewig, F. K.
Leffel, P. C.
Lewis, G. V.
Lewis, H. H.
Lewis, J. G.
Lochman, E. W.
Mason, R. B.
McCann, S. C.
Millis, L. W.
Mooney, W.
Mullen, C. H.
Nottberg, G.
Nottberg, H., Jr.
Nottberg, H., Sr.
O'Daniel, P.
O'Dower, H. J.
Painter, D. H.
Patterson, H. V.
Pellmounter, T.
Pellmounter, T. V.
Perry, C. E.
Perton, F. S.
Ralston, E. E.
Redmond, G. J., Jr.
Reichow, W. A.
Rivard, M. M.
Ryan, J. B.
Sanders, W. L.
Schaad, F. N.
Scherrer, J. R., Jr.
Schreiber, W. F.
Schumacher, C. W.
Scurlock, U. M.
Sheppard, F. A.
Smith, E. L.
Smith, H. C.
Stevens, K. M.
Stoffer, G. H.
Stoner, D. W.
Telgemeier, A. H.
Thomas, R. L.
Traynor, J. H.
Upham, R. W.
Waldsmith, E. C.
Ward, A. R.
Weiss, C. A.
Werner, C. V.
White, W. E.
Wiedeman, W.
Wiedenmann, W. A.
Wilder, W.
Wright, H. H.
Yeazel, G. D.
Zahner, L. W., Sr.
Zumbehl, L. E.

Kirkwood—
Ahlff, A. A.
Grossmann, H. A.
Hartwein, C. E.
Kipp, H. J.
Langenberg, E. B.
Schwind, L. M.
Thompson, W. D.

Lee's Summit—
Garrison, C. H.

Lemay—
Meeka, J., Jr.

Normandy—
Bemis, W. A.
Kothe, R. B.
Uhlemeyer, W. M.

Overland—
Grossenbacher, H. E.

Richmond Heights—
Harder, E. P.
McQuitty, R. M.
Siegel, D. E.

St. Joseph—
Harton, A. J.

St. Louis—
Barry, J., Jr.
Becker, G. E.
Blackmore, J. J.
Bradley, E. P.
Burnap, C. H.
Carlock, M. F.
Carlson, E. E.
Casey, J. J.
Clucas, E. T.
Coad, J. D.
Combs, C. F.
Compton, B. C.
Cooper, J. W.
Cordes, E. W.
Corrigan, J. A.
Corrigan, T. J.
Dabbs, J. T.
Davis, C. R.
DeNeille, J. L.
Dorffi, A. A.
Dube, J. E.
Dulle, W. L.
Fagin, D. J.
Falvey, J. D.
Ferris, A. F.
Gay, C. E., Jr.
Gettinger, E. W.
Gilmore, L. A.
Goellner, J. A.
Gross, L.
Halt, H. R.
Hamig, L. L.
Heiman, S. J.
Helle, F. J.
Herkenhoff, D. A.
Hester, T. J.
Hoppin, C. A., Sr.
Hostetter, J. C.
Hyde, D. F.
Ince, F. E.
Kaber, W. C.
Kane, M. E.
Kelley, D. F.
Kelly, W. C.
Klein, W. A.
Knipe, W. E.
Kremer, R. H.
Kuntz, E. C.
Lauten, F. C.
Lebman, F. M.
Lewin, B. J.
Loseman, J. L.
Lynch, J. T.
Malone, J. S.
May, C. O.
McClure, C. J. R.
McMahon, L. A.
McMahon, T. W.
Metcalf, R. H.
Moon, L. W.
Naylor, J. F., Jr.
Niemoeller, A. R.
Norris, W. P.
Oonk, W. J.
Ownby, R. W.
Pattiz, G. B.
Pellegrini, L. C.
Phillips, R. C., Jr.
Pieksen, G. W.
Ploesser, H. M.
Quick, L. P.
Rebmann, C. P.
Reeves, R. O.
Rodenheiser, G. B.
Rosebrough, J. S.
Rosebrough, R. M.
Schulte, R. A.
Sharp, H. C.
Simons, B. C.
Simpson, W. B.
Smith, O. L.
Smith, R. J.
Sodemann, W. C. B.
Stammer, E. L.
Steckhan, L.
Strauch, P. C.
Swallow, J. H.
Toensfeldt, R.
Vollmar, T. M.
Watkins, J. C.
Weidle, B. E.
Werley, W. C.
Wilson, H. F.

Springfield—
James, R. E.
Owen, W. H.

University City—
Evans, B. L.
Hall, R. E.
Langenberg, G. A.

Webster Groves—
Axthelm, F. G.
Carter, D. G.
Carter, J. H.
Myers, G. W. F.

MONTANA

Billings—
Cohagen, C. G.
Prussing, R. L.

Butte—
Sullivan, T. J.
Talley, D.

Dillon—
Boyer, C. L.

Great Falls—
Ginn, T. M.

NEBRASKA

David City—
Reardon, J. F.

Hastings—
Bernstrom, C. B.
Lainson, H.
Nutting, R. E.
Swingle, W. T.

Lincoln—
Green, E. W.
Lehman, M. G.

Omaha—
Bierl, J. G.
Blanchard, N. M.
Brown, E. A.
Carter, C. A.
Colburn, G. W.
Dempsey, E. P.
Duffy, W. R.
Failor, C. A.
Frankle, M. S.
Goll, W. A.
Goth, C. A.
Grimm, L. E.
Howard, W. B.
Jensen, A. O.
Kleinkauf, H. Y.
Manchester, F. P., Jr.
Martin, K. E.
Mason, R. E.
Mathis, J.
McCulley, D. E.
Merwin, G. E.
Olson, M. J.
Peterson, B. G.
Pospisil, P. J.
Prawl, F. E.
Reifschneider, J.
Ruchte, C. O.
Saxon, R. B.
Simmonds, V.
Sleister, P. E.
Smith, O. J.
Stark, J. E.
White, W. R.

Plattsmouth—
Bauer, J.

Schuyler—
Matousek, A. G.

Scottsbluff—
Witschy, R. J.

NEVADA

Henderson—
Allen, G. W.
Watkins, W. O.

Las Vegas—
Annabel, C. H.
Inman, C. M.

Reno—
Mast, C. M.
Salter, T. J., Jr.
Stevens, H. R.
Stevens, J. E.
Szymanski, S. R.

NEW HAMPSHIRE

Durham—
Seeley, L. E.

Elkins—
Baker, R. H.

Hanover—
Tash, T.

Manchester—
Morin, R. P.

NEW JERSEY

Arlington—
Cochrane, W.

Asbury Park—
Strevell, R. P.

Atlantic City—
Strouse, B. H.

Atlantic Highlands—
Danowitz, C. J.

Barber—
Stevens, F. D.

Bayonne—
Devlin, J. J.

Belleville—
Thornton, T. L.

Bernardsville—
Patrick, H. M.

Bloomfield—
Berry, R. U.
Brown, C. W.
Faust, F. H.
Hicks, B. A.
Johnson, W. E.
McLenegan, D. W.
Newell, R. W.
Turner, J. P., Jr.

Bogota—
Griess, P. G.

Caldwell—
Harrigan, E. R.
Schmidt, H.

Camden—
Albert, W. J.
Battan, S. W.
Brown, W. M.
Holt, D. R.
Hynes, L. P.
Kappel, G. W. A.
Kern, C. J.
Morgan, D. E.
Plum, L. H.
Teuber, H. N.
Webster, E. K.
Webster, W., Jr.

Cliffside Park—
Butler, P. D.

Collingswood—
Mohrfeld, H. H.

Cranford—
Baksa, S.
Beach, A. F., Jr.

Dumont—
Burges, J. H. M.
Campbell, R. E.
Hoertel, H. E.

East Orange—
Fairchild, H. P.
Fritsche, C.
Reilly, J. H.
Rubel, H. L.
Schroth, A. H.
Swain, W. A.
Turno, W. G. W.

Edgewater—
Nitzberg, S. H.

Elizabeth—
Beebe, F. E. W.
Bermel, A. H.
Loeser, C. M.
Lyman, S. E.
Rudio, H. M.
Wheller, H. S.

Englewood—
Christesen, M. C.
Thomas, B. F., Jr.
Whitacre, V. L.

Essex Fells—
Soule, L. C.
Swaney, F. J.

Fanwood—
Kyte, R. L.

Fort Monmouth—
Diamond, D. D.

Freehold—
Buck, D. T.

Glen Ridge—
Thompson, R. E.

Hackensack—
Hudik, F.

Haddonfield—
Love, J. E.
Slater, W. H.

Hawthorne—
Smyth, G. E.

Hillside—
Tichenor, L. R., Jr.

Hoboken—
Taylor, T. S.
Van Woert, A. B.

Ho-Ho-Kus—
Best, E. T.

Irvington—
Feldermann, W.
Reinke, A. G.
Siggins, G. S.

Jersey City—
Callahan, P. J.
Horwitz, S.
Walterthum, J. J.

Kearny—
Shaffer, C. E.

Little Falls—
Lundt, E. C.

Livingston—
Peary, H. W.

Lyndhurst—
Ehrlich, M. W.

Manville—
Parkinson, J. S.

Maplewood—
Moraweck, A. H., Jr.

Margate—
Beirn, J. B.

Merchantville—
Binder, C. G.

Millburn—
Shepard, E. C.
Stengel, F. J.

Montclair—
Abbott, F. S.
Jacobus, D. S.
Kaveny, J. G.

Moorestown—
Makin, H. T., Jr.

Mountain Lakes—
Pinter, J. L.

Newark—
Anderson, W. T., Jr.
Bull, H. A.
Dickinson, N. S.
Driggs, A. A., Jr.
Haitmanek, L. M.
Jones, H. L.
Kruse, W. C., Jr.
Kuttler, J. B.
Leinroth, J. P.
Lenaz, R. A.
Norman, G. C.
Parker, D. F.
Ray, L. B.
Werner, P. H.

New Brunswick—
Wolin, M. W.

New Milford—
Scharmer, G. A.

North Bergen—
Vitali, O. J.

Nutley—
Morris, C. R.

Oradell—
Wendel, F. E.

Orange—
Crawford, J. H., Jr.

Passaic—
Blazer, B. V.

Paterson—
McBride, J. A.
McBride, J. N.
Montesano, F. P.

Plainfield—
Hedlund, R. A.
Pond, W. H.
Proctor, C. W.
Reis, R.
Wagner, H. C., Jr.

Pompton Plains—
Ward, J. A.

Rahway—
Hoecker, G. F., Jr.
Snavely, E. R.

Raritan—
Rodee, E. J.

Red Bank—
Fidelius, W. R.
Miner, H. H.

Ridgewood—
Martin, G. W.
Miller, A. T.
Newton, D. A.
Terhune, R. D.
Walton, C. W., Jr.

River Edge—
Stewart, C. W.

Roselle Park—
Ambrose, E. R.
Tiernan, J.

Short Hills—
Lair, P. H.
Lester, W. L. G.

Somerville—
Patrick, G. P.

Sparta—
Brex, I. E.

Summit—
Des Reis, J. F.
Morehouse, H. P.
Oaks, O. O.

Teaneck—
Heebner, W. M.
Phillips, L. R.
Tucker, J. R.

Tenafly—
Garner, R. V.
Jessup, F. J., Jr.

Trenton—
Moran, E. V., Jr.
Nussbaum, O. J.

Union City—
Matheka, C. R.
Taverna, F. F.

Upper Montclair—
Broome, J. H.
Burton, C. C.
Donnelly, J. F., Sr.
Koster, H. H.

Verona—
Anderson, E. L.

Vineland—
Houck, R. C.

West Collingswood—
Mizener, R. S.

West Englewood—
Hutcheon, C. R.

Westfield—
Bacon, W. H., Jr.
Croney, P. A.
Cross, W. D.
Frambach, F. S.
Oppenheimer, P. H.

Westmont—
Robinson, E. R.

West New York—
Stinard, R. L.

West Orange—
Adlam, T. N.
Ferguson, R. R.
Levine, S. J.
Raymer, W. F.

Westwood—
Wedebrock, A. L.

Woodbridge—
Simkin, M.

Woodbury—
Dickson, G. P.

NEW MEXICO

Albuquerque—
Frankenfeld, H. V.
James, J. K.
Jones, W. L.
Munn, H. F.
Pride, H. K.

Eunice—
Brown, J. W.

Los Alamos—
Hill, J. H.
Musser, S. A.
Via, C. W.

Santa Fe—
Ross, E. F.

NEW YORK

Albany—
Bond, H. A.
Horowitz, H.
Murray, T. F.
Taylor, R. B.
Teeling, G. A.
Westover, W.

Auburn—
Patrick, A. L.

Big Flats—
Davis, B. C.

Binghamton—
Schmidt, A. F.

Bronx—
Carson, J. H.
Colombo, J. D.
Falk, J.
Queenin, M. A.
Sheridan, T. J.
Wildermuth, R. O.

Bronxville—
Bishop, C. R.
Dornheim, G. A.
Nee, R. M.

Brooklyn—
Altemueller, G. F.
Angell, L. D.
Arnold, J. S.
Bailey, F. T.
Bassevitch, A.
Bilgrei, E.
Birkett, H. S.
Boemi, H.
Dailey, J. F.
Dwyer, T. F.
Eells, H. B.
Feldman, N. R.
Ficarra, F. X.
Freeman, A. W.
Goldberg, M.
Hartmann, C. W., Jr.
Hartmann, H.
Janet, H. L.
Kimmel, A. J.
Kleinhomer, W. G.
Kresh, S.
Leventhal, B.
Levine, C.
Quist, O. F., Jr.
Reh, H. C.
Steele, H. S.
Stein, W.
Thornburg, H. A.
Tracy, W. E.
Tusch, W.
Wachs, L. J.
Whealton, D. J.
Whelan, L.
Williams, H. E.
Wurts, H. H.
Zwerling, S. J.

Buffalo—
Adema, G. E.
Beman, M. C.
Booth, C. A.
Brown, E. P.
Cherry, L. A.
Cheyney, C. C.
Collins, J. A.
Conaty, B. M.
Cox, E. H.
Criqui, A. E.
Davis, J.
De Jarlais, G. M.
Farnham, R.
Fuchs, J.
Harding, L. A.
Heath, W. R.
Hedley, P. S.
Holt, W. H.
Householder, H. L.
Jackson, M. S.
Kaupp, C. W.
Killeen, T. F.
Kirschhofer, F. J.
Landers, J. J.
Lenihan, W. O.
Love, C. H.
Madison, R. D.
Mahoney, D. J.
Moesel, F. A.
Olds, S. T.
Pendleton, M. E.
Pleuthner, R. L.
Quackenbush, J. M.
Quackenbush, S. M.
Reif, A. F.
Reif, C. A.
Roebuck, W., Jr.
Scott, C. E.
Seelbach, H., Jr.
Seelbach, W. R.
Seyfang, W. G.
Smith, R. K.
Sommers, W. J.
Spencer, W. E.
Stell, W. H., Jr.
Strouse, S. W.
Thompson, Q. P.
Trefts, J. C., Jr.
Voisinet, W. E.
Walker, E. R.
Warnecke, R. I.
Weber, F. J.
Wendt, E. F.
Weston, C. E.
Yager, J. J.

Canajoharie—
Martin, W. T.

Cooperstown—
McGown, F. H., Jr.

Croton-on-Hudson
Wallen, G. R.

DeWitt—
Chur, R. R.
Keane, G. F.
Mooney, M. E.
Perry, H. E.

Dobbs Ferry—
Bertolett, C.
Hewett, J. B.
Lee, B. H.
Mulholland, D. J.

Eden—
Ensign, W. A.

Fairport—
Peck, H. E.

Fayetteville—
Chur, C. H., Jr.
Grant, W. A.
Traynor, H. S.

Glens Falls—
Kalbfleisch, T. F., Jr.

Groton—
Sahab, M. S.

Hamburg—
Morgan, R. W.
Schafer, H. C.

Hartsdale—
Giannini, A.

Hastings-on-Hudson
Reynolds, T. W.

Herkimer—
Nagle, C. J.

Irvington—
Bastedo, A. E.
Hastings, A.
King, T. E.

Ithaca—
Dropkin, D.
Elwood, W. H.
Mackey, C. O.
Sawdon, W. M.
Williams, J. W.

Jamestown—
McCoy, P. W.
Sanford, H. L.

Kenmore—
Bryce, J. H.
Candee, B. C.
Criqui, A. A.
Mould, H. W., Jr.

Lake Hill—
Freitag, F. G.

Lake Placid—
Bovard, C. A.

Lancaster—
Meidenbauer, P. E., Jr.

LeRoy—
Pohle, K. F.

Lockport—
Saunders, L. P.

Long Island—
Ahlrichs, H. (New Hyde Park)
Alt, H. L. (St. Albans)
Apt, S. R. (Bayside)
Bachmann, A. J. (Westbury)
Baker, H. A. (Whitestone)
Bappler, C. T. (Elmhurst)
Bearg, M. J. (Hollis)
Bennis, R. R. (Elmhurst)
Bernhard, G. (Hewlett)
Bloom, L. (Freeport)
Bulyk, J. (Flushing)
Burkhardt, C. H. (Flushing)
Bush, R. J. (Whitestone)
Carroll, D. E. (Bayside)
Conway, R. W. (Rockville Centre)
Crone, T. E. (Jamaica)
Demuth, H. (Williston Park)
Eastwood, H. F. (Merrick)
Eriksen, W. R. (Flushing)
Foxhall, W. B. (Jackson Heights)
Friedlieb, M. J. (Far Rockaway)
Gilman, F. W. (Long Island City)
Ginsberg, M. R. (Jamaica)
Gornston, M. H. (Forest Hills)
Graber, E. (Douglaston)
Heymsfield, H. R. (Jamaica Estates)
Hiers, C. R. (Great Neck)
Hilmer, G. O. (Springfield Gardens)
Hutchins, P. C. (Bayside)
Jalonack, I. G. (Roslyn Heights)
Junger, H. G. (Queens Village)
Kaplan, M. J. (Hempstead)
Kerbel, J. (Hollis)
Kern, J. F., Jr. (Massapequa)
Langberg, M. (Lynbrook)
Luzzi, T. E. (Bellerose)
MacKay, H. J. (Woodhaven)
MacWatt, D. A. (Plandome)
Magnusson, N. (Jamaica)
Marc, H. M. (Garden City)
Marino, F. A. (Corona)
Martens, E. D. (Hempstead)
Marty, E. O. (Plandome)
Matzen, H. B. (Rockville Centre)
Miller, F. T. J. (Far Rockaway)
Miller, N. R. (Hollis)
Olsen, G. E. (Arverne)
Pabst, C. S. (Woodhaven)
Paulding, L. G. (Hempstead)
Peters, W. F., III (Merrick)
Quirk, C. H. (Hempstead)
Rainson, S. J. (Great Neck)
Raynis, T. (Manhasset)
Rose, J. C. (Queens Village)
Ross, S. S. (Woodside)
Rudd, D. J. (Babylon)
Schechter, J. E. (Woodmere)
Schundler, H. O., Jr. (Long Island City)
Schwartz, M. (Inwood)
Shelldrop, T. F. (Hempstead)
Silvera, A. (Jackson Heights)
Spiegel, D. (Woodmere)
Spoerr, F. F. (Hempstead)
Sterne, C. M. (Long Island City)
Thomson, T. N. (Huntington)
Tucker, F. N. (Freeport)
Verity, E. W. (Great Neck)
Wallace, G. J. (East Elmhurst)
Warren, O. A. (Great Neck)
Whittaker, W. K. (St. Albans)
Wolpert, N. N. (Glen Cove)

Mamaroneck—
Gschwind, J. F.
Howes, P. B.
Howes, L. K.

Marietta—
Baker, D. L.

Mt. Vernon—
Brod, B. M.
Broderick, E. L.
Costello, P. F.
Herske, A. R.
Jander, Y.
Medcalf, L. C.
Sellman, N. T.

New Rochelle—
Abrams, A.
Farley, W. F.
Fitz, J. C.
Gross, V. L.
Rose, H. J.
Virrill, G. A.

New York—
Adams, E. E.
Adams, O. C.
Addams, H.
Addams, P. K.
Addington, H. B.
Albright, C. B.
Almert, H.
Ashley, E. E.
Auslander, G.
Baker, T.
Baldwin, C. W.
Balsam, C. P.
Barbieri, P. J.
Barfus, L.
Barton, K. L.
Baum, A. L.
Beaghen, G. W.
Bearman, A. A.
Becker, P. F.
Belford, L. B.
Bergan, J. R.
Berman, L. K.
Bianculli, V. A.
Bodinger, J. H.
Bond, H. H.
Bondy, W. S.
Booker, J. W.
Buckalter, R. I.
Brown, D.
Buensod, A. C.
Buffalano, A. C.
Cameron, J. A., Jr.
Campion, C. R.
Carbone, J. H.
Carpenter, R. H.
Chambers, S. A.
Chandler, R.
Chase, C. L.
Chase, R. E., Jr.
Christie, R. W.
Chu, Y.
Clay, W.
Cole, V.
Collette, J. R.
Colvin, O. D.
Cox, L. E.
Cucci, V. J.
Cummings, G. C.
Daly, J. D.
Darling, R. B.
Darts, J. A.
Dastur, M. N.
Davies, C.
Davis, C.
Demeter, J.
Denny, H. R.
Dodge, H. A.
Doherty, R. S.
Donnelly, R.
Doughty, C. J.
Dunne, R. V. D.
Dutcher, H. S.
Eadie, J. G.
Ebner, R. C.
Eliason, O. C.
Farbman, L. X.
Farrar, C. W.
Feder, N.
Feldman, A. M.
Ferretti, J. J.
Fetscher, J. J.
Fiedler, H. W.
Fitts, J. C.
Fleisher, W. L.
Fleisher, W. L., Jr.
Fletcher, S. W.
Flink, C. H.
Frederick, H. W.
Friedman, M.
Friend, W. F.
Fuller, C. A.
Fullington, G. A.
Gabbert, W. L.
Geiringer, P. L.
Giannini, M. C.
Godes, E.
Goldmann, P.
Gordon, P. B.
Grant, E. C.
Greenburg, L.
Greilsamer, P.
Gruitch, J. M.
Hanburger, F. W.
Handman, N. J.
Harvey, A. D.
Heibel, W. E.
Heller, J. A.
Henry, A. S., Jr.
Herkimer, H.
Herkimer, H.
High, J. M.
Hinrichsen, A. F.
Hiratsuka, S.
Hobbie, E. H.
Hoffman, C. S.
Holbrook, F. M.
Hollis, R. C.
Honerkamp, F.
Hosking, H. L.
Hotchkiss, C. H. B.
Huebner, W. O.
Huyett, M. Y.
Hyde, B. P.
Jacobi, B. A.
Janos, W. A.
Janssen, H. J.
Jarcho, M. D.
Johnson, H. S.
Johnson, S. O.
Kaczenski, C.
Kahn, C. R., Jr.
Kahn, W. C., Jr.
Kaplun, E. A.
Kayan, C. F.
Kelly, C. J.
Kemler, E. N.
Kimball, D. D.
Kingsbury, J. W.
Koehler, C. S.
Kopecky, J. J.
Kornblum, H. R.
Kreiner, J.

Kuhlmann, R.
Kunen, H. K.
Kurth, F. J.
Lavorgna, M. L.
Lawrence, F. D.
Lewis, H. F.
Lewis, V. I.
Lieblich, M.
Lucke, C. E.
Lyon, J. P.
Markush, E. U.
McClintock, W.
McFarlan, A. I.
McGuire, J. W.
McHugh, J. J.
McMullen, C. S.
Milener, E. D.
Miller, C. A.
Miller, H. A.
Miller, J.
Milnes, A.
Moesel, F. L.
Munier, L. L.
Munkelt, F. H.
Murphy, J. R.
Meyer, H. C., Jr.
Murray, F. A.
Murray, W. W., Jr.
Mytinger, K. L.
Nelligann, G.
Nelson, C. E.
Nevin, J. F.
Offner, A. J.
Olson, N. I.
Olvany, W. J.
Patorno, S. A. S.
Paul, D. W.
Peacock, H.
Phillips, L. S.
Pizer, M. M.
Pollak, R.
Porter, H. T.
Purinton, D. J.
Pryke, J. K. M.
Raisler, R. K.
Rather, M. F.
Reed, T. M., Jr.
Reid, H. P.
Reinhardsen, D.
Rice, J. A.
Ritchie, E. J.
Ritter, A.
Robertson, J. D. W.
Rosenberg, P.
Ross, J. O.
Roth, C. F.
Rothenbach, W. J.
Ryan, H. J.
Sale, F. B.
Samuels, S.
Saunders, M. K.
Sawhill, R. V.
Schauer, R. A.
Schoepflin, P. H.
Schulze, B. H.
Seelinger, H. N.
Self, V. F.
Shataloff, N. S.
Shea, F. X.
Sherbrooke, W. A.
Short, W. W.
Simpson, E. H.
Skidmore, J. G.
Smith, C. H.
Smith, M. S.
Snow, D.
Sobel, F.
Soule, J. P.
Spencer, S. A.
Steinmetz, C. W. A.
Sternberg, E.
Stevens, E. K.
Stevens, T. R.
Strahan, J. L.
Strock, C.
Sweeney, G. J.
Syska, A. G.
Tiltz, B. E.
VanNieukerken, J. M.
Vetlesen, G. U.
Vroome, A. E.
Walker, W. S.
Webster, C. C.
Wheeler, J., Jr.
Wheeler, W. H.
White, J. H.
Whitelaw, H. L.
Willner, I.
Wolff, R. A.
Wrightson, W. T.
Yula, R. W.

Niagara Falls—
Edwards, G. B.
Woolcock, E.

North Tarrytown—
Weiss, A. P.

North Tonawanda—
Schulmeister, W. A.

Oneida—
Springer, J. J.

Oswego—
Crawford, E. F.
Demarest, R. T.
Tucker, S.

Pelham—
Head, F. T.
Smith, S.

Perry—
Perez, W. M.

Pittsford—
Reddington, R. T.

Port Chester—
Pegg, E. H. R.

Rochester—
Cherne, R. E.
Cook, R. P.
Dickason, G. D.
Dollinger, L. L., Jr.
Grau, E. R.
Green, E. L.
Hakes, L. M.
Leonhard, L. W.
MacIntyre, H. B.
McWilliams, J. W.
Mosher, H. A.
Penafeather, J. C.
Perkins, S. H.
Schmitt, W. C.
Sheldon, N. E.
Stacy, S. C.
Teal, B. C.
Treadway, J. Q.
Wilder, E. L.
Willson, F. J.
Wyld, R. G.

Rome—
Lynch, W. L.
May, J. P.
Mills, D. L.
Wesley, W.

Scarsdale—
Armspach, O. W.
Cumming, R. W.
Engle, A.
Franck, P.
Kennedy, W. F.
Scott, G. M.

Schenectady—
Harrigan, J. E.
Harrington, E. D.
Hunziker, C. E.
Weiss, E. J.
Welch, L. A., Jr.

Skaneateles—
McCumber, B. R.
Stacey, A. E., Jr.

Snyder—
Bardo, F. J., Jr.
Mollenberg, H. J.

Staten Island—
Gregory, R. C.
Grieco, A. V.
Johnson, E. B.
O'Neill, J. E.
Peyrek, T. R.
Pfuhler, J. L.
Ruggles, R. F.
Vivarttas, E. A.
Volkhardt, A. N.
Waechter, H. P.

Syracuse—
Ashley, C. M.
Baker, R. A.
Boggs, H. V.
Carrier, W. H.
Childs, L. A.
Cunningham, T. M.
Day, V. S.
Driscoll, W. H.
Feldman, M. M.
French, D.
Fritzberg, L. H.
Gammill, O. E., Jr.
Gilboy, W. O.
Goodhue, B. C.
Hanson, L. C.
Heaphy, J. A.
Hellekson, O. H.
Hillen, W. G.
Hockensmith, F. E.
Ingels, M.
Jones, A. L.
Kallusch, H. A.
Kennedy, J. C.
Krayenhof, H. G.
Laube, H. L.
Lewis, L. L.
Lynn, J. F.
Lyon, D. M.
MacCrea, J. M.
Manier, R. L.
McGrath, W. L.
Meek, G. W.
Morris, J. E.
Murphy, E. T.
Neyhart, F. B.
Noble, M.
Ormsby, H. K., Jr.
Patterson, J. C.
Pope, E. F.
Robson, P. D.
Schmidt, J. F.
Schuler, W. R.
Seitz, R. C.
Shanklin, A. P.
Shawhan, S. F.
Sprague, K. T.
Spriggs, C. U.
Sterry, H. L.
Stevens, J. W.
Stewart, J. P.
Strong, H. G.
Walsh, G. W., Jr.
Weninger, M.
Woese, C. F.
Yeazel, H. F.

Tonawanda—
Karlsteen, G. H.

Troy—
Bekeshus, J. H.
Carofano, D. A.

Tuckahoe—
Goulding, W.
Leveridge, R. H.
McCann, F. D.
Williamson, C. C.

Utica—
Gilbert, I. W.
Laine, F.
La Row, L. E.
Randolph, H. F.
Riehl, W. L.
Tuite, J. M.

Valhalla—
Mehne, C. A.

Watertown—
Aikin, F. W.

Watervliet—
Light, J. C.
Schubert, A. G.

White Plains—
Belsky, G. A.
Callahan, T. H.
Zibold, C. E.

Williamsville—
Coburn, J. B. V.

Yonkers—
Burns, R.
Calnan, D. J.
Hanson, F. E.
Harmonay, W. L.
Harris, H. J.
Knecht, A. W.
Ormiston, J. B.
Rainger, W. F.
Schoen, D. D.
Stein, S. C.
Werker, H.
Whitt, S. A.

NORTH CAROLINA

Asheville—
Price, W. C.
Wilson, W. E.

Charlotte—
Bailey, J. L.
Barnes, H. S.
Berger, W. W.
Brandt, E. H., Jr.
Burt, R. L.
Clark, J. R.
Cousart, K.
Crockford, R. H.
de Witt, E. S.
Embree, E. G.
Fink, R. C.
Graham, W. A.
Hallenbeck, C. W.
Jones, E. C.
Kirkwood, T. A.
Long, O. B.
MacDonald, J.
Mason, R. E.
McGary, R. O.
McKenzie, H. E.
Petty, C. E.
Price, A. Z.
Reed, W. H., III
Schiwetz, D. P.
Selden, K. W., Jr.
Setzer, C. M., Jr.
Sisk, R. D. V.
Smith, W. P., Jr.
Trimble, C. R.
Warren, R. M., Jr.
Wooten, M. F., Jr.

Durham—
Brown, W. L., Jr.
Daddario, F. T.
Ervin, F. R.
Iskyan, H. S.
Nicholson, S. J.
Reed, F. J.
Skinner, A., Jr.
Wallace, W. M., II

Graham—
White, R. A.

Greensboro—
Adams, C. Z.
Du Chateau, M. F.
Graham, W. D.
Graham, W. D., Jr.
Guest, P. L., Jr.

Harding, E. R.
Hart, J. E.
Hartsfield, C. G.
Hoffman, H.
Hoffman, H. B.
Holliday, F. R., Jr.
Holliday, F. R., Sr.
Hunter, R. K.
Klages, F. E. P.
Nash, B. T.
Rottman, G. B.
Sullivan, W. H.
Sullivan, W. H., Jr.

High Point—
Gray, E. G.
Gray, H. E.
Gray, W. E.

Raleigh—
Bunn, J. W., Jr.
Burney, L. B.
Rice, R. B.
Rock, G. A.
Wilson, B.

Salem Station—
Page, A.

Spindale—
Barkley, K. L.

State College Station
Vaughan, L. L.

Winston-Salem—
Allcorn, L. H., Jr.
Allen, R. W.
Avera, W. W.
Bahnson, A. H., Jr.
Boxall, F.
Brown, M. D.
Byrum, E. G., Jr.
Cooper, W. H.
Cornwall, C. C.
Crosland, R. B., Jr.
Horton, L. E.
Karnes, T. C., Jr.
McCallum, C. E.
Saunders, M. G., Jr.
Steadman, C. C., Jr.
Stimson, D.

NORTH DAKOTA

Rolla—
Munro, W. J.

OHIO

Akron—
Murray, R. P.
Oswald, L. S.
Roma, G. N.

Ashland—
Rybolt, A. L.
Selig, E. T., Jr.

Barberton—
McLeish, W. S.

Bay Village—
Taliaferro, R. R.

Berea—
Dee, V. C.

Black Lick—
Aitken, T.

Campbell—
Sgambati, A. P.

Canton—
Eynon, W. E.

Chagrin Falls—
Parmelee, G. V.

Cincinnati—
Allan, J. E.
Beach, M. W.
Bechtol, J. J.
Beineke, R. C.
Bengle, C. V.
Bird, C.
Blum, R. J., Jr.
Buenger, A.
Carsey, E. A.
Clark, R. J.
Coombe, J.
Cooper, W. B.
Coyne, J. H.
De Bra, F. B.
Edwards, A. W.
Edwards, I. G.
Ehlers, W. D.
Elliott, C. L.
Fenker, C. M.
Fine, M. E.
Froehlich, B. F.
Gannon, R. R.
Gerdsen, A. H.
Goepper, F. S.
Hauer, B. T.
Helburn, I. B.
Hermann, H. N.
Hoffmann, H. C.
Hotze, V.
Houlis, L. D.
Houliston, G. B.
Hudepohl, L. F.
Huelsmann, A. G.
Jennings, H. K.
Jones, J. D.
Juer, F.
Juergens, W. A.
Junker, W. H.
Kahle, H.
Killian, W. J.
Kinney, A. M.
Kramig, R. E., Jr.
Kuempel, L. L.
Lewis, H. E.
Little, K. B.
Mathewson, M. E.
McNamee, E. W.
Moore, H. W.
Motz, O. W.
Murphy, G. R.
Mursinna, G. P.
Peck, R. E.
Pfriem, P. G.
Pillen, H. A.
Pistler, W. C.
Powers, L. G.
Quinlivan, L. P.
Reiley, T. D.
Richard, E. J.
Ruff, A. G.
Russell, H. E.
Schoonover, W. A.
Seibert, E. W.
Shuster, W. W.
Sigmund, R. W.
Silberstein, B. G.
Sproull, H. E.
Stevens, W. R.
Sutfin, G. V.
Taggart, R. F.
Ward, F. J.
Weaver, C. D., Jr.
Williams, E. C.
Wilson, F. W.
Wood, D. J.
Wright, K. A.

Cleveland—
Auerbach, L. F.
Avery, L. T.
Baggaley, W.
Baker, J. G.
Berger, J. L.
Bergman, H.
Berry, P. M.
Billington, D. B.
Black, J. M.
Boeddener, G.
Boehm, J. C., Jr.
Borkat, P.
Braun, C. R., Jr.
Bryan, W. L., Jr.
Burkes, L. C.
Byers, R. L.
Cary, E. B.
Cohen, P.
Conner, R. M.
Conrad, A. F., Jr.
Cummings, C. H.
Cummings, R. J.
Curtis, H. F.
Cutting, R. H.
Dahlstrom, J. A.
Dalton, R. T.
Davis, K. T.
Dickson, R. W., Jr.
Donelson, W. N.
Dunbar, L. W.
Eck, M. C.
Entenmann, W. O.
Erichsen, E.
Evans, W. W.
Evelett, C. F.
Fleck, W. R.
Fleming, P. B.
Frensdorf, S. F.
Friedman, A.
Galaba, A.
Gamble, B. L.
Gayman, P. D.
Geltz, R. W.
Givelber, S. H.
Gladieux, D. W.
Gottschalk, K. A.
Gottwald, C.
Gowan, G. J.
Gray, E. W.
Greiling, W. W.
Guilbery, S. R.
Hall, J. A.
Hall, N. H.
Hancock, F. A.
Hansen, C. E.
Harper, D. R.
Harvey, L. C.
Heisterkamp, H. W.
Huebscher, R. G.
Humphreys, C. M.
Jackett, L. H.
James, J. W.
Johnson, P. H.
Jones, J. P.
Kane, J. M.
Kaufman, A. M.
Kitchen, F. A.
Kochel, R. K.
Kohn, W. P.
Koper, C. H.
Koubek, J. V.
Lavelle, A. E.
Levy, M. I.
Locklin, D. W.
Lynch, C. B.
Mandt, R. D.
Manna, A. F.
Mannen, D. E.
Matthews, C. R.
Maurer, E. E.
McClanahan, L. C.
McKeeman, C. A.
Mehlek, J. F.
Miles, J. C.
Miller, W. P.
Minor, F. K.
Moore, W. R.
Morse, E. F.
Murphy, T. E.
Nachman, G. P.
Noel, C. E.
Platz, J. F.
Pogalies, L. H.
Repp, H. L.
Richmond, J.
Rowe, W. M.
Sagar, P. B.
Seigel, L. G.
Sharp, H. R.
Sherman, R. E.
Slawson, L. E.
Stamberger, R. F.
Stanek, E. W.
Stewart, C. W.
Stobbe, G. C.
Stolberg, C. P.
Tahsler, D. H.
Tasker, C.
Taze, D. L.
Teverbaugh, J. E.
Theiss, E. S.
Tuve, G. L.
Urban, R. A.
Vanderhoof, A. L.
Venning, J. R.
Weager, T. A., Jr.
Webb, E. C.
Weenink, C. A.
Wetzell, H. E.
Wheeler, C. W.
White, M. R.
Wise, R. A.
Wright, C. P.
Young, E. O.

Cleveland Heights—
Frisse, J. L.
Jack, R. A.
Kinkaid, J. R.
Leising, R. E.
McIntosh, C. B.
Rhoton, W. R.
Rogers, W. M.
Watterson, W. B.
Weiner, H. R.

Columbus—
Alionier, H. R.
Ashley, R. D.
Bell, T. H.
Bobst, E. F.
Bogen, A. D.
Breneman, R. B.
Brown, A. I.
Curl, R. S.
Darby, T. E.
Engdahl, R. B.
English, A. T.
Favret, L. E.
Fenner, W. M.
Gibbard, H. S.
Grimm, J. M.
Guy, J. A.
Hamer, F. S.
Hamlin, M. R.
Hays, H. C.
Hess, N. T.
Hofmeister, H. J.
Hutchison, I. B.
Jackson, R. B.
Jennings, R. B.
Johnson, P. B.
Keatts, R. M.
Lamberson, L. D., Jr.
Leiby, R. S.
Liebert, R. C.
Lilly, F. J.
Little, V. R.
Long, E. L.
Lorimer, C. F.
Mathers, W.
McGovern, A. F.
Myers, J. A.
Myler, W. M., Jr.
Norland, C. O.
Norman, E. A., Jr.
Oelgoetz, J. F.
Piper, D. D.
Pirrung, R. W.
Pryor, A. S.
Ramsey, E. C.
Schott, F. C.
Schumacher, J. F.
Seabright, F. C.
Sherman, R. A.
Shifflette, D. F.
Slemmons, J. D.
Smith, R. H.
Speer, J.
Sweeney, A. R.
Swepston, M. M.
Trimble, J. I.
Vyff, P. C.
Walker, T. R.
Wilcox, L. J.
Williams, A. W.

Williams, J. K.
Wolfe, A. H.
Wolfe, C. H.
Wollerman, A. E.
Wood, G. K.
Wyatt, D. H.
Wykoff, W. R.
Zellak, J.

Cortland—
Swenehart, D. W.

Cuyahoga Falls—
Humphrey, D. E.
Ray, G. E.
Smithers, T.
Strong, S. S.

Dayton—
Anderson, S., Jr.
Baker, I. C.
Budde, W. R.
Doudican, C. T.
Farnbacher, J. M.
Gibbons, M. J.
Gibbons, M. J., Jr.
Gonzalez, R. A.
Jones, E. A.
Kunzog, T. W.
Leupold, G. L.
Lindsay, G. W.
Newton, A. B.
Weitzel, P. H.
Worsham, H.
Zeigler, D. D.

Defiance—
Barton, J.

East Cleveland—
Clark, R. L.
Nobis, H. M.
Pasiadis, F. H.
Pinney, T. M.
Steffner, E. F.
Stern, L. M.

Elyria—
Downe, E. R.
Grandstaff, C. L.
Johnson, J. B., Jr.
Ryden, E. H.
Von Kamp, N. H.

Euclid—
Geiger, R. L.
Gruendel, W. C.
Teller, W. R.
Wilhelm, J. E.

Geneva—
Sheldon, R. W.

Glendale—
Thomas, R. H.

Hamilton—
Daugherty, R. J.
Minda, W. F.
Thomas, L. G. L.

Hilliards—
Eibling, J. A.

Hudson—
Lamb, J. H.

Kent—
Saginor, S. V.

Lakewood—
Cheeseman, E. W.
Farr, A. H.
Hall, J. R.
Longcoy, G. B.
Schurman, J. A.

Lima—
Chadwick, G. F.
Hawisher, H. H.

Logan—
Kitchen, D. E.
Potts, A. P.

London—
Visintine, E. C.

Lorain—
Holden, R. G.
Jackson, W. F.
Ross, D. S.

Lynhurst—
Allen, C. G.

Mansfield—
Guest, J. F.

Maple Heights—
Boggs, D.

Middletown—
Byrd, T. I.

Newark—
Waggoner, J. H.

New Philadelphia—
Jenkins, C. P.
Rubin, S.

North Canton—
Acheson, L. K.

Northfield—
Glanzer, C. J.

Norwood—
Callan, W. D.

Oberlin—
Murphy, T. O.
Ries, L. S.
Sable, E. J.

Olmsted Falls—
Brennan, C. T.

Osborn—
Layton, J. W.

Painesville—
Hobbs, J. C.

Parma—
Kluger, E. C.

Piqua—
Herrman, D. D.
Lange, R. T.

Rocky River—
Kreider, F. B.
Reed, G. G.
Watchler, W. J.
Weldy, L. O.

Shaker Heights—
Crawford, J. N.

Solon—
Wilson, R. A.

South Euclid—
Baker, H. E.
Linn, G. B.
Silk, W. H.

South Park—
Barney, W. E.

Springfield—
Aitken, M. L.
Harman, R. H.
McGovern, T. R.

Spring Valley—
Wood, C. F.

Struthers—
Runge, E. A.

Toledo—
Edgington, F. A.
Hoffman, C. F.
Hunsaker, R. E.
Levinson, D. S.
Lumm, A. H., Jr.
McKitrick, W. D.
Moorehead, R. C.
Richardson, F. C., Jr.
Vincent, H. B.
Watkins, G. B.
Weaver, E. A.

University Heights—
La Salvia, J. J.
Orabella, M. J.

Urbana—
Hegele, R. H.

Warren—
Manning, C. E.

Warrensville Heights
Dickens, L. A.

Washington C. H.—
Thrailkill, H. K.

Washingtonville—
Cochran, L. D.

Waverly—
Armbruster, F. T. W.

Wickliffe—
Nottage, H. B.

Willoughby—
Dravage, T. D.

Wilmington—
Farquhar, H. F.
Marconett, V. G.
Sapp, C. L.

Youngstown—
Hyman, C. A.
Montgomery, J. R.
Olson, A. A.
Tolerton, H. A.

Zanesville—
Burnham, H. T.

OKLAHOMA

Norman—
Dawson, E. F.

Oklahoma City—
Ash, N. B.
Carnahan, J. H.
Carroll, W. M.
Dolan, R. G.
Donceel, G. T.
Dugger, E. R.
Ellingson, E. T. P.
Frankfurt, W. W.
Gray, E. W.
Groth, D. R.
Hayes, C. R., Jr.
Loeffler, F. X.
Loeffler, F. X., Jr.
Morin, A. R.
Patten, J. R.
Randleman, K. B.
Sain, K. L.
Shafer, H. S.
Spaan, J. H., Jr.
Swan, R. E.
Trowbridge, C. Y.
Westbrook, C. H.

Seminole—
Crane, R. M.

Tulsa—
Holmes, A. D.
Jones, E.
Lee, W. R.
Loeffler, J. G.
McCune, L. J.
Meinholtz, H. W.
Munn, W. B.
Thomas, F. M.
Watt, J. N.

OREGON

Beaverton—
McKenzie, H. W.

Corvallis—
Coon, C. A.
Willey, E. C.

Eugene—
Cooper, C. H.

Gladstone—
Williams, L. G.

Medford—
Hoey, J. K.
Wilson, A. A.

Ontario—
Birdsall, H. W.

Portland—
Armstrong, C. E.
Atkinson, R. R.
Banks, J. B.
Beers, V. A.
Blankenship, D.
Bohren, A. H.
Bonebrake, J. H.
Brissenden, C. W.
Brocha, J. F.
Burtchaell, J. T.
Burton, W. R.
Byrne, J. J.
Campau, W. R.
Carroll, E. E.
Castrow, O. E.
Chewning, R. C.
Clark, A. C.
Day, L. C.
Day, S. S.
Dougherty, C. P.
Farnes, B. W.
Finlay, A. E.
Flocke, K. N.
Freeman, J. A.
Gaylord, A. K.
Gehrs, W.
Gish, W. A.
Hanson, K. H.
Hanthorn, W.
Harrington, L. J.
Heinkel, C. E.
Hoss, A. N.
Johnson, F. R.
Johnston, A. K.
Jones, L. R.
Judson, A. L.
Kelly, E. E.
Kendrick, A. E.
Kollas, W. J.
Kroeker, J. D.
Kugel, E. F.
Langdon, T. C.
Lankow, R. P.
Lokey, E. R.
Lord, R. H.
Lynch, J. R.
MacGregor, C. M.
Martig, R. W.
Matthews, O. W., III
Maxwell, W. D.
McClung, T. H.
McDermott, J. P.
Mead, H. K.
Morrison, W. B.
Murhard, E. A.
Murhard, K. R.
Neubauer, E. W.
Ninman, A. T.
Nolan, T. J.
Norte, W. R.
Ott, M. E.

Peterson, R. W.
Pfeifer, V. A.
Pindell, W. R.
Ponder, E. A.
Pysher, M. W.
Ramsey, W. P.
Rigby, E. D.
Risley, G. H.
Sandsted, P. F.
Siegert, E. P.
Simpson, W. A.
Smith, U. G.
Stover, W. H.
Taylor, T. E.
Thornburg, B. M.
Turner, E. S.
Ueberrhein, W. H.
Urban, F. F.
Vradenburg, W. C.
Walker, C. L.
Weiant, A. S.
Wheeler, B. J.
Widmer, W. J.
Yates, J. E.

Salem—
Van Wyngarden, J. E.

Sweet Home—
Swaski, K. J.

Tillamook—
Ingram, J. D.

PENNSYLVANIA

Abington—
Park, N. W.

Allentown—
Glance, A. C.
Goundie, J. K.
Hanemann, A. M.
Hendrix, W. T.
Hersh, F. C.
Hilder, F. L.
Korn, C. B.
Le Grand, I. F.

Altoona—
Yeager, G. F.

Ambler—
McElgin, J. W.
Schmidt, C. W.

Ardmore—
Quinn, J. J., Jr.
Yeomans, P. H.

Bala Cynwyd—
Albright, J. C.

Berwyn—
Wandless, F. W.

Bethlehem—
Brandt, A. D.
Montgomery, C. T., Sr.
O'Connell, W. H.
Whittier, F. W.

Bridgeville—
Sanders, V.

Canonsburg—
Rainey, N. W.

Cheltenham—
Garnett, W.
Hingston, G. N.

Conshohocken—
Wilder, F. B.

Creighton—
Cox, S. F.
Englehart, O. D.

Dallas—
Mulcey, P. A.

Dravosburg—
Marshall, A. W.

Drexel Hill—
Burke, J. J.
Clarkson, R. C., Jr.
Matz, G. N.

Easton—
Moulsdale, T. D.
Urmston, B. S.

Elizabethtown—
Dibble, S. E.

Erie—
Joyce, H. B.
Kennedy, D. P.
Mayne, W. L.
Meyers, C. F.
Sullivan, T. J., Jr.

Glenmore—
Gant, H. P.

Glennville—
Fisher, E. F.

Glenside—
Tucker, L. A.

Greenville—
Hunt, M.

Harrisburg—
Eicher, H. C.
Geiger, I. H.

Hatboro—
Eisenstein, M.
Steilen, L. J.

Havertown—
Burritt, E. E., Jr.
Call, J.
Conover, D. D.
Fyfe, J. H.
Jones, A.
King, H. K.
Kipe, J. M.

Hershey—
Snavely, A. B.

Hollidaysburg—
Tierney, L. F.

Indiana—
McCall, M.

Irwin—
Cost, G. W.

Jenkintown—
Tuckerman, G. E.

Johnstown—
Holmes, P. B.
Hunter, L. N.
Schlentner, K. O.
Von Rosenberg, P. C.

Kingston—
Macdonald, D. B.

Lancaster—
Brown, H. C., Jr.
Lloyd, E. C.
Weitzel, C. B.

Lansdowne—
Ackermann, R. H.
Cromie, R. W.
James, H. R.
Johnson, A. J.
Mather, H. H.
Seltzer, P. A.
Smith, G. F.

Lebanon—
Repino, P. A.

Macungie—
Singmaster, J. W.

McKeesport—
Dugan, T. M.
Stickrath, K. J.

McKees Rocks—
Landgraf, G. F.

Mechanicsburg—
Heath, G. A.

Merion—
Davidson, L. C.

Milbourne—
Sullivan, J. R.

Moylan—
Cornelius, G. E.

Narberth—
Sigel, R. J.
Wilmot, C. S.

New Castle—
Thayer, H. H.

New Hope—
Davidson, P. L.

New Kensington—
Edwards, J. D.

Norristown—
High, A. K.

Oxford—
Ware, J. H., III

Philadelphia—
Alexander, G. P.
Atkins, T. J.
Augusterfer, R. J.
Baldwin, R. T.
Barnard, M. E.
Barnes, J. C.
Barr, G. W.
Bartlett, C. E.
Bates, J. H.
Berger, C. D.
Bertrand, G. F.
Black, E. N., III
Blankin, M. F.
Bogaty, H. S.
Bornemann, W. A.
Buck, L.
Buzzard, F. H.
Caldwell, A. C.
Cavanagh, P. A.
Church, L. M.
Church, R. A.
Cody, H. C.
Corbman, A. L.
Coward, C. W.
Crew, F. D.
Culbert, W. P.
Curley, E. I.
Dafter, E. H.
D'Ambly, A. E.
Darby, F. N.
Dever, H. F.
Dietz, C. F.
Director, I.
Doerrfuss, H. W.
Dome, A. G.
Donovan, W. J.
Eastman, C. B.
Elliot, E.
Erickson, H. H.
Faltenbacher, H. J.
Farrington, S. E.
Goff, J. A.
Goldner, H. W.
Greenberg, B. F.
Gross, C. J.
Hedges, H. B.
Hucker, J. H.
Hunger, R. F.
Hutchison, J. E.
Ickeringill, J. C.
Jackson, J. S.
Jungels, A. J.
Keeling, F. V.
Kelble, F. R.
Kirkbride, J. O.
Koch, A. H.
Kriebel, A. E.
Kun, I. B.
Lambert, E. C.
Lee, R. J.
Leese, M. L.
Leopold, C. S.
Locke, R. A.
Lubking, C. J.
Ludwig, W. D.
Lyons, H. W.
Macfarlan, N. S.
Mack, L.
MacLean, R. M.
Macrow, L.
Malloy, W. W.
Marshall, J.
Martocello, J. A.
McCullough, H. G.
McIlvaine, J. H.
Mellon, J. T. J.
Meloney, E. J.
Millham, F. B.
Mirabile, J. J.
Moody, L. E.
Morgan, F. X.
Murdoch, J. P.
Mutimer, A. G.
Nesbitt, A. J.
Nusbaum, L.
Nusbaum, S. R.
Parent, H. M.
Peller, L.
Pfeiffer, F. F.
Plewes, S. E.
Powell, G. W., Jr.
Powers, E. C.
Prewitt, H. B.
Rettew, H. F.
Rink, C. N.
Roberts, E. F., Jr.
Roberts, H. L.
Robertson, A. M.
Rugart, K.
Sabin, E. R.
Schenck, W. P.
Scott, W. S.
Semel, E.
Sheffler, M.
Sheffler, M. A.
Smiles, R. H.
Smith, A. M.
Smith, C. W.
Smith, D. J.
Smith, D. K.
Speckman, C. H.
Stolker, E. A.
Tebo, F. A.
Terry, M. C.
Thompson, H. D.
Thompson, P. J.
Timmis, P.
Touton, R. D.
Traugott, M.
Wagner, E. K.
Weger, L.
Wegmann, A.
Weid, H. L.
Weintraub, J. A.
Wells, W. F.
Whitney, C. W.
Wiegmann, K. H.
Wildman, E. L.
Wilson, J. F.
Wiltberger, C. F.
Woolston, R. H.

Pittsburgh—
Allison, J. H.
Bailey, F. N.
Baker, W. H., Jr.
Bateman, W. H.
Beighel, H. A.
Benn, C. L.
Biber, H. A.
Bickell, G. C.

Biggs, R. A.
Bokman, T. P.
Borton, A. R.
Brauer, R.
Chapman, W. P.
Chipman, E. E.
Cohen, W. P.
Coleman, J. L., Jr.
Collins, J. F. S., Jr.
Comstock, G. M.
Cooperman, E.
Cullen, C. W.
Darrah, R. D.
Day, H. C.
Doherty, R. J.
Dorfan, M. I.
Edwards, P. A.
Evans, D. A.
Ferderber, M. B.
Fife, C. M.
Goerg, B.
Good, C. S.
Gottschall, W. C.
Grabman, H. B.
Hach, E. C.
Hawk, C. A., Jr.
Hebley, H. F.
Heckler, F. W.
Heilman, R. H.
Hemeon, W. C. L.
Hickey, D. E.
Hickox, M.
Horne, E. C.
Hupp, H. L.
Jones, L. K.
Kaufman, A. M.
Keist, W. E.
Kirkendall, H. J.
Knox, J. R.
Langan, J.
Little, R.
Loucks, D. W.
Lynn, F. E.
Maehling, L. S.
Maier, G. M.
McCann, J. L.
McIntosh, F. C.
Metzger, A. F.
Meyer, E. W.
Miller, R. A.
Moore, H. L.
Mowrey, C. F.
Nass, A. F.
Park, H. E.
Park, P. S., Jr.
Peacock, G. S.
Penney, G. W.
Pietsch, H. A.
Platts, E. M.
Proie, J.
Reed, V. A., Jr.
Reich, H. H.
Reilly, B. B.
Reynolds, J. C.
Riddle, K. L.
Rieseck, W. L.
Riesmeyer, E. H., Jr.
Riley, J. N.
Rockwell, T. F.
Rose, H. J.
Ryerson, H. E.
Schneider, C. H.
Schoedel, J. J.
Sheppard, W. K.
Shepstone, O.
Sherrer, J. W., Jr.
Simpson, G. L.
Simpson, W. D.
Small, B. R.
Smith, E. O.
Smyers, E. C.
Speller, F. N.
Stanger, R. B.
Stanger, W. F.
Stevenson, W. W.
Strachan, G. W.
Tennant, R. J. J.
Tower, E. S.
Troller, T. H.
Walker, L. S.
Waters, G. G.
Williams, O. L.

Pottstown—
Harberger, G. L.

Reading—
Corbit, C. A.
Keperling, H. R.
Luck, A. W.
Mabon, J. E.
Potteiger, C. A.
Reese, H. L.
Wilkins, E. S.

Ridley Park—
Mawby, P.

Scranton—
Gilboy, J. P., Jr.
Mahon, B. B.

Shillington—
Shelley, K. B.

Springfield—
Grossman, H. E.
Guzzardi, S. S.

State College—
Joy, F. A.
Lifton, D.
Queer, E. R.
Shepperd, W. B.
Wright, C. C.

Stroudsburg—
Kiefer, E. J.

Swarthmore—
Hobbs, W. S.
Robinson, A. S.

Upper Darby—
Frankhouser, E. V.

Villanova—
Morehouse, J. S.

Wallingford—
Arnold, R. S. L.

Washington—
Frazier, J. E.

Wayne—
Shea, M. B.

Waynesboro—
Alvarez, J.
Beam, L. H.
Kline, W. O.

Wilkes-Barre—
Johnson, R. C.

Williamsport—
Anderson, W. S., Jr.
Axeman, J. E.
McLain, R. D.
Pfeiffer, J. F.

Wyndmoor—
Stroh, S. M.

Wynnewood—
Rush, M. K.

Wyomissing—
Smith, O. F., Jr.

York—
Blum, R. D.
Brydia, E. M.
Crawford, D. H.
English, R. B.
Frank, G. D.
Hertzler, J. R.
Kartorie, V. T.
Kottcamp, H. E.
Mohn, H. L.
Neiman, C. H., Jr.
Nicoll, S. F.
Parsons, L. G.
Ruff, A. W.
Scott, J.
Stempel, E. H.
Tignor, W. L.
Walsh, E. R., Jr.
Wood, F. C.
Zieber, W. E.

RHODE ISLAND

Centredale—
Fenner, E. M.

North Providence—
Blanding, R. L.

Providence—
Coleman, J. B.
Corey, G. R., Sr.
Essley, H. A.
Gibbs, E. W.
Hartwell, J. C.
Houlihan, E. T.
Malin, B. S.
Mandell, L. C.
Pett, A. W.
Potter, C. D.
Romer, W. H.
Schoerner, R. T.
Welshman, H., Jr.

SOUTH CAROLINA

Anderson—
Dean, F. F.

Bennettsville—
Powers, R. W.

Charleston—
Bailey, F. A., Jr.
Garvin, J. L.

Columbia—
Blackstone, A. L., Jr.
Crouse, M. E.
Hartin, W. R., Jr.
Herty, F. B.
Kerr, W. E.
McDowell, H. L.

Ft. Jackson—
Sloane, D. J.

Greenville—
Freeman, L. E.
Morgan, G. R.
Ramseur, V. D., Jr.
Rouse, R. K.
Shepard, J. deB.
Stipp, R. A.
Waldrep, J. E.

Lancaster—
Lasley, J. B.

Rock Hill—
Thomas, G. G.

SOUTH DAKOTA

Rapid City—
Laws, C. W.

Sioux Falls—
Monick, F. R.
Smith, C. F., Jr.

TENNESSEE

Bristol—
Torok, E.

Chattanooga—
Campbell, G. S.
Corlew, J. B.
Shull, D. E.

Johnson City—
Kegarise, R. R.
Lautz, F. A.
Muse, M. H.
Sanders, W. R.

Kingsport—
Herbert, J. S.

Knoxville—
Cross, F. G.
Goans, J. W.
Hajek, W. J.
Lawrence, L. F., Jr.
Matthews, J. E.
Oakley, L. W.
Roy, E. W.

Memphis—
Bevil, A. T.
Buckingham, R. B.
Burr, G. C.
Cooper, J. A.
Ellis, M. H., Jr.
Fischer, C. S.
Flinn, G. S.
Flinn, J. D.
Glaspie, D. L.
Hamlin, J. B.
Henson, W. L.
Hilton, J., II
Holmes, O. A., Jr.
Hoshall, R. H.
Hughes, C.
Hughes, R.
Humphrey, T. O. S., Jr.
Johnson, R. W.
Johnson, W. R.
Jung, F. P.
Koch, J. J.
Lammons, J. B.
Lancaster, H. W., Jr.
Lee, B. J.
Lenz, A. W.
McIntosh, J. W.
McKee, T. M., Jr.
Mitchell, J. S.
Nolan, J. J.
O'Brien, T. J.
Overman, R. E., Jr.
Phillips, R. W.
Powell, L. D.
Richmond, G. B.
Schulz, W. F.
Scott, E. E.
Shelby, A. W.
Simpson, H. A.
Slater, W. F.
Thorpe, W. E.
Wellford, W. L., Jr.
Wilson, H. H.
Woodson, E. G.
Wynn, C. E.

Milan—
McClintock, W. C.

Nashville—
Armistead, W. C.
Armistead, W. C., Jr.
Brown, F.
Fly, E. P.
Gallagher, J. M., Jr.
Horn, E. C.
Shelby, L. W.
Swats, W. F.
Whittemore, W. M., Jr.
Wilson, V. H.

Oak Ridge—
Parker, G. S.
Turner, J. F.

Raleigh—
Danielson, W. A.
Ledbetter, N. C.

Union City—
Merryman, C. P.

TEXAS

Amarillo—
Burnett, E. S.
Towne, C. O.

Austin—
Henry, A.
Schuett, D. F.
Wilke, I. W.

Bay City—
Schulz, B. J.
Tooke, T. B.

Beaumont—
Broussard, D. E.
Humble, J. D.
Shell, J. D.
Talbot, J. M.

Brownsville—
Price, P. M.

Bryan—
Field, E., Jr.

Camp Hood—
Deuth, G. Q.

Camp Howze—
Clow, S. A.

Christoval—
Simpson, R. H.

College Station—
Badgett, W. H.
Bettencourt, H. J., Jr.
Breland, B., Jr.
Callins, J. G.
Clark, J. R.
Crawley, J. B.
Goodloe, J. C., Jr.
Hopper, J. S.
Jahn, R., Jr.
Jensen, A. F.
Kerr, J. W.
Kirkley, C. R.
Lentz, T. H.
Long, W. E.
Martyn, H. J., Jr.
Michels, E. C.
Morris, W. K.
Mullinix, R. M.
Murphree, S. E., Jr.
Palmer, J. C.
Phillips, H. W., Jr.
Phillips, R. F.
Ray, S. E.
Rohrabacher, W. E.
Smith, E. G.
Smith, L. W.
Spears, J. M., Jr.
Thompson, L. W., Jr.
Tippett, G. R.
Tuffly, H. J.
Vaughan, J. E., Jr.
Walker, M. T.
Walthall, T. J.
Werlla, B. C.
Wilson, J. H.
Young, G. R.

Colorado City—
Brown, L., Jr.

Corpus Christi—
Clemins, R. J.
Locher, D. E.

Dallas—
Allen, R. F.
Allison, R. E.
Angus, F. M.
Anspacher, T. H.
Aronoff, M. S.
Ashcraft, J. P.
Avera, A. F.
Barbeck, C. A.
Barbeck, W. R.
Baron, A. E.
Bell, D. G.
Benson, M. A.
Bishop, J. A.
Blum, H., Jr.
Bock, I. I.
Brandt, S. S.
Brown, M. L.
Brown, M. W.
Carter, A. B.
Catlett, W. A.
Chase, J. C.
Clark, H. G., Jr.
Cline, C. C.
Cohn, H.
Cox, R. G.
Cox, V. G.
Dillard, J. P.
Dowdell, J. R.
Edmondson, J. V.
Ellsberry, S. A., Jr.
Farmer, J. E.
Farrow, E. E.
Foss, B. S., Jr.
Frost, W. E.
Gardner, C. R.
Gardner, M. K.
Gessell, E. T.
Gilbert, L. S.
Gilmore, C. F.
Gray, F. L., Jr.
Hanson, R. W.
Harrington, P. W.
Hatzenbuehler, E. J.
Henegar, B. V.
Herndon, D. C.
Jackson, M. W.
Kaun, W. F.
Kearns, W. J.
Keck, E. T., Jr.
Keeney, W. S.
Kneese, V. C.
Knight, R. C.
Kuhn, W. H.
Lacy, J. W.
Lagow, A. C.
Lambert, E. G.
Landauer, L. L.
Levy, B. W.
Linskie, G. A.
Lowe, J. B.
Luedecke, W. H.
Lyford, R. G.
Maley, D. P., Jr.
Martyn, H. J.
Matthews, R. R.
McLeod, C. H.
Meffert, G. H.
Mercer, B. G.
Mixon, R. A.
Moler, W. H.
Murray, M. J.
Nation, O.
Newby, I. P.
O'Connor, J., Jr.
Pettit, E. N., Jr.
Pfeiffer, D. C.
Pines, S.
Poythress, J. D.
Rapp, E. A.
Ray, J. A.
Roberts, H. H.
Rodgers, F. A.
Sampson, W. D.
Schick, K. W.
Shafer, M. L.
Snyder, L. R.
Stern, E. J.
Stone, A. A.
Tate, H. L.
Templeton, H. J.
Tye, J. L.
Ullrich, A. B., Jr.
Vinther, P. N.
Wessler, G. H., Jr.
Wilson, J. E.
Yost, C.
Young, C. C.
Zink, D. D.
Zumwalt, R.

Delhart—
Welch, T. I.

Denton—
Jackson, R. E.

Dickinson—
Hall, M. S.

El Paso—
Carns, V. J.
Jackson, G. H.

Fort Worth—
Barmann, P. V.
Bauman, C. S.
Beals, D. E.
Edwards, C. E.
Grimmer, R. A.
Gunn, F.
Harris, A. M.
Hobson, W. C., Jr.
Hoyler, T. H.
Jones, H. L.
MacEachin, G. C.
Marsalis, M. E.
McLaren, F. S.
Miles, O. K.
Parker, T. S.
Werner, R. E.
Witte, G. C., Jr.

Freeport—
Ketchum, E. R.

Galena Park—
Crowe, R. H.
Haney, A. A.

Galveston—
Cartwright, S. E.
Guill, A. W.
Kauffman, D. S.
Letsos, J. N., Jr.
Warren, C. W.

Harlingen—
Stracke, S. L.
Wolf, R. B.

Houston—
Allen, E. C.
Anderson, N. B.
Andrews, W. M.
Armstrong, R. E.
Asbury, E. M.
Atlas, S. F.
Ayres, R. O.
Barnes, A. F.
Barnes, W. L.
Beaird, B. J.
Beauchamp, J. H.
Bible, H. U.
Boehler, C. L.
Bovay, H. E., Jr.
Boyd, R. L.
Boyd, S. W.
Brandt, F. C.
Broadwell, H. W.
Bromberg, S.
Brown, D. A.
Brown, M. L., Jr.
Bugher, G. A.
Burns, T. V., Jr.
Burton, J. E.
Canterbury, H. M.
Chase, A. M., Jr.
Collins, G. J.
Cook, R. L.
Cooper, D. S.
Crocker, C. G.
Daniel, J. M.
Darby, J. W.
Davis, J. T.
De Vines, H. L.
Dickey, A. T.
Dillender, E. A.
Doeppenschmidt, L. C
Ellis, C. W.
Etie, W. R.
Ewell, W. A.
Ezell, P. B.
Fisher, B. P.
Fleming, C. L.
Floeter, E. C., Jr.
Gillis, H. W., Jr.
Goldman, R. J.
Goldman, S.
Grogin, G. K.
Hess, A. E.
Holland, J. W.
Holt, W. M.
Howard, F. B.
Howell, E. L.
Howell, L.
Ibison, J. L.
Jenkins, R. L.
Johnson, R. B.
Kleir, I. R.
Kribs, C. L., Jr.
Kriechbaum, R. R.
Ladewig, L. L.
Lashley, W. L., Jr.
Laughlin, W. C.
Lay, R. M.
Leatherwood, T. W.
Leonard, A. F.
Lewis, J. C.
Lichty, C. P.
Lippert, W. M.
MacFerrin, J. B.
Mannon, N. R.
Marshall, J. W.
Mayo, W. P., Jr.
McCullough, G. W.
McKinney, C. A.
McLane, E. H.
McMillan, H. D., Jr.
McRoberts, R. C.
Mills, D. M.
Milton, T.
Mitchell, A. J.
Molnari, B. A.
Montgomery, F. W.
Moody, W. D.
Morgan, R. L.
Morrow, J. D.
Nachlas, O. M.
Naman, I. A.
Natkin, A. J.
Owen, P. H., Jr.
Peiser, M. B.
Poole, J. A.
Presseur, H. W.
Quin, C. C.
Quinby, L. B.
Rasmussen, A. A.
Robinson, D. M.
Roll, P. E.
Rudloff, C. S.
Salinger, R. J.
Sandifer, R. S.
Shannon, B. L.
Sheere, A. D.
Shoals, C. A.
Sitton, E. R.
Skinner, F.
Smith, A. M.
Smith, D. S.
Stansbury, E. J., Jr.
Stephenson, J. H.
Taylor, R. F.
Thomas, A. D.
Thomas, E. R.
Timmerman, W. C.
Tucker, R. E.
Walsh, J. A.
Warner, I. J.
Way, N.
Way, W. J., II
Wheeler, J. A.
Will, H. C.
Williams, H. O.
Wilson, J. A.
Wittbold, R. H.
Woodruff, C. S.
Workman, A. E.
Yates, E. F.
Young, F. R.

Jacksonville—
Singleton, G. R., Jr.

Kilgore—
Hammett, L. D.

Longview—
Brown, R. C.
Schuster, P. H.

Lubbock—
Ainsworth, S. E.
Anthony, W. R.
Welch, B.

Mercedes—
Atteberry, C.

Nacogdoches—
Jones, O. D.

Nederland—
Tansil, J. T.

New Baden—
Bolton, O. J.

New Braunfels—
Giesecke, F. E.
Rompel, W. A.

Oklaunion—
King, T. D.

Orange—
Johnston, J. J.
Yardley, J. E.

Paris—
Johnson, S. C.

Pasadena—
Powitzky, C. E.

Port Arthur—
Sanford, E. H.
Voskamp, E. L.

San Antonio—
Bacon, E.
Barnes, R. W.
Benham, F. C., Jr.
Bernhardt, R. J.
Cotter, R. P.
Diver, M. L.
Essex, J. L.
James, R. P.
Kotzebue, R. W.
Mathis, L. N.
Monier, K. A. J.
Pawkett, L. S.
Rhine, G. R.
Rummel, A. J.
Ryden, R. S.
Schuchart, O. W.
Shafer, W. P., Jr.
Staley, M. E.
Wallis, W. E.

San Juan—
Martin, S. S.

Sherman—
Burns, R. O.
Collins, W. A., Jr.

Texas City—
Ammons, S. E.

Trinidad—
Eaton, R. L.

Tyler—
Griffith, J. B.
Layton, R. E., Jr.

Waco—
Brooks, J. A.
Horton, M. A.
Kay, H. M.
Shelfer, E. L.

Wichita Falls—
Luker, M., Jr.
McCall, M. W.

UTAH

Logan—
Wangsgaard, D.

Salt Lake City—
Ashton, J. L.
Baker, E. L.
Brown, R. C.
Campbell, G. C.
Chytraus, O. E.
Curtis, A. R.
Dyer, A. R.
East, R. H.
Fairclough, R. J.
Ferguson, C. E.
Foulger, S. W.
Gollaher, M. L.
Gritton, E. V.
Harrison, W. Z.
Hillard, H. F.
Holford, D. B.
Huber, P. O.
Irvine, L. K.
Jespersen, S. J.
Lee, R. H.
Lym, J. H.
Maycock, A. A.
Maycock, G. E.
McAllister, A. F.
Midgley, R. C.
Miller, H. D.
Murdock, C. E.
Pons, R. A.
Reynolds, C. M.
Richardson, E. L.
Richardson, H. G.
Richeda, A.
Robison, D. J.
Sayler, W. H.
Smith, E. D.
Soderborg, G. L., Sr.
Spencer, C. H.
Via, J. H.
Watts, E. J.
Wilde, D. R.
Young, J. T., Jr.

VERMONT

Bellows Falls—
Tyler, R. D.

Brattleboro—
Bearse, A. H., Jr.

Burlington—
Lanou, J. E.
Tuthill, A. F.

Woodstock—
Ambrose, A. H.

VIRGINIA

Alexandria—
Fogg, J. H.
Gault, G. W.
Goergens, A. G.
Hart, J. H.
Kluckhuhn, F. H.
Lively, G. P.
Millard, J. W.
Ross, M.
Singleton, W. H.
Underwood, G. T.
Weaver, J. V. O.

Arlington—
Cover, R. R.
DeSomma, A. E.
Ferrarini, J.
Gates, A. S., Jr.
Grimes, F. M.
Kajuk, A. E.
Luttrell, L. W.
Marshall, W. D.
Sontag, H.
Taylor, C. R.
Walz, G. R.
Whittlesey, C.

Danville—
Farley, W. S.

Falls Church—
Ley, R. B.
Phillips, W. L.
Stearns, E. J., Jr.

Front Royal—
Hartsook, G. S., Jr.
Nordine, L. F.

Lynchburg—
Doering, F. L.
Franklin, S. H., Jr.
Hinnant, R. H.

McLean—
Nye, L. B., Jr.

Newport News—
Phillips, D. E.

Norfolk—
Boyenton, J. F.
Braz, A.
Capps, E. L.
Cox, W. A., Jr.
Duval, E. D.
Gray, R. O.
Grigg, J. L.
Hartman, P. C., Jr.
Lambert, T. A.
Mansfield, E. C.
McGinnis, F. L.
Moore, V. A.
Morris, K. H.
Nowitzky, H. S.
Ray, J. A., Jr.
Reynolds, J. F.
Robinson, W. P.
Rodgerson, H. T.
Shanahan, J. J.
Simpson, J. A.
Stokley, J. M.
Tazewell, E. B.
Thomas, R. C.
Warner, J. B.
Webster, W. H., Jr.
White, J. E.
Williams, G. E.

Portsmouth—
Beisel, K. E.
Bensinger, M.
Gorsuch, W. J.
Hayes, W. C.
Hayes, W. G.

Richmond—
Carle, W. E.
Graham, R. L.
Hankins, R. P.
Hinnant, C. H., Jr.
Johnston, J. A.
Martin, T. I., Jr.
Peebles, J. K., Jr.
Roach, E. R.
Taylor, M. I.
West, C. H., Jr.
Williams, E. H.

Roanoke—
Andrews, W. G.
Bailey, A. E.
Brown, R. L.
Dodge, R. V., Jr.
Grim, F.

Sandston—
Anderson, R. V.

Windsor—
Bailey, C. F.

WASHINGTON

Bremerton—
Bysom, L. L.
Clark, D. L.
Dominy, C. B.
Farrar, J. L.
Sines, C. F.

Longview—
Cairncross, G. F.
Pauley, R. D.

Mt. Vernon—
Helin, W. E.

Pasco—
Matheson, E. E.

Richland—
Arndt, M. H.
Musser, J. M.
Osterhage, C. S.

Seattle—
Allen, R. H.
Beggs, W. E.
Bouillon, L.
Brobeck, R. A.
Caskey, T. C.
Close, P. D.
Constant, E. S.
Corr, F. J.
Cox, W. W.
Culver, F. C.
Eastwood, E. O.
Emanuels, M.
Faulkner, J. H.
Finn, C. W.
Geiser, R. A.
Goodman, C. L.
Granston, R. O.
Griffin, D. C.
Griffith, H. T.
Hauan, M. J.
Johnson, W. L.
Kane, A. T.
Keefer, D. M.
Kirkwood, R. R.
Langdon, E. H.
Le Riche, R. E.
Liniger, R. H.
Lux, A. C.
Mallis, W.
May, C. W.
McKinstry, M. W.
McLennan, M. C.
Mead, D. O.
Morse, R. D.
Musgrave, M. N.
Nickerson, A. E.
Norby, K. H.
Norton, E. H.
Notkin, J. B.
Orebaugh, H. T.
Pangborn, C. A.
Peterson, S. D.
Pride, W. B.
Priebe, O. W.
Riley, E. F.
Rosen, E. J.
Rudolph, R. R.
Sparks, J. D.
Spofforth, W.
Stern, R. M.
Sutch, H. C.
Towne, R. M.
Tupper, E. B.
Twist, C. F.
Wallis, W. M.
Watt, R. D.
Weber, E. L.
Wesley, R. O.

Spokane—
Bowers, O. E.
Bunnell, E. W.
Connell, E. C.
Jennings, H. S.
Kelly, J. C.
Meagher, T. F.

Tacoma—
Chase, R. E., Sr.
Dapper, M. J.
Foote, E. E.
Smith, J. V.
Warren, H. F.

Vashon Island—
Jensen, J. E.

Wenatchee—
Segle, T. L.

Yakima—
Hargis, A. H.
Leichnitz, R. W.
Peterson, H. H.
Saar, L. F.

WEST VIRGINIA

Charleston—
Rosenblatt, A. M.
Shanklin, J. A.

Fairmont—
Tonry, R. C.
Wright, C. E.

Huntington—
Davis, C. W.
Johnson, L. O.
Schurman, J. H.
Sharp, J. R.

Largent—
Donnelly, J. A.

Martinsburg—
Caskey, L. H., Jr.

Parkersburg—
Bartels, C. J.

St. Albans—
Arvidson, E. R.
Dickinson, R. P., Jr.

South Charleston—
Pugh, D. C.

White Sulphur Springs—
McKie, T. G.
Tidman, R. P.

WISCONSIN

Appleton—
Barlow, F. J.
Jenkins, F. H.

Clintonville—
Quall, C. O.

Eau Claire—
Grosvold, F. E.
Hestekin, W. E.
Wood, F. J.

Elm Grove—
Winkler, R. A.

Hales Corners—
Deubel, J. A.

Kenosha—
Lee, J. A.

Kohler—
Hvoslef, F. W.

La Crosse—
Anderegg, R. H.
Becraft, E. R.
Labus, O. A.
Lubinsky, R. G.
Lucey, R. E.
Ringquist, C. L.
Trane, R. N.

Lancaster—
Hoffman, C. J.

Madison—
Akerman, J. R.
Dean, C. L.
Feirn, W. H.
Hall, G.
Hunzicker, D. L.
Kliefoth, M. H.
Larson, G. L.
Nelson, D. W.
Nystrom, P. E.
Okray, R. A.
Reuschlein, C. J.
Seymour, J. E.
White, J. C.
Youngman, E. C.

Marshfield—
Himsel, S. R.

Milwaukee—
Adams, R. B.
Alfery, H. F.
Allan, W.
Alyea, H. W.
Amundson, C. H.
Boden, W. F.
Bowers, A. F.
Cook, H. D.
Crew, M. W.
Cross, L. E.
Cutler, J. A.
Davis, D. W., Jr.
Ellis, H. W.
Frentzel, H. C.
Gerstenberger, E. J.
Gifford, E. W.
Goldsmith, F. W.
Griewisch, A. H.
Hamacher, W. F.
Hanley, F. V.
Haus, I. J.
Hearne, R. D.
Herrick, M. M.
Hessler, L. W.
Hoffmann, A.
Hoffmann, P. R.
Holland, W. T.
Hughey, T. M.
Illingworth, J. E.
Jackson, C. H.
Jacobs, R. H.
Jung, J. S.
King, R. L.
Kluge, B. M.
Knab, E. A.
Koch, R. G.
Krenz, A. S.
Leitgabel, K. A.
Lewis, C. E.
Lingen, R. A.
Lofte, J. A.
Marshall, W.
Marvin, P. R.
Miller, L. B.
Moe, P. A.
Morrison, A. McK.
Mueller, H. P.
Noll, W. F.
Nunlist, F. J., Jr.
Ouweneel, W. A.
Parri, I. W.
Podolske, A. R.
Reinke, L. F.
Ress, O. J.
Rodwell, R. D.
Rossiter, I. J.
Schaar, M.
Schreiber, H. W.
Spence, M. R.
Stevens, W. H.
Swisher, S. G., Jr.
Szekely, E.
Tutsch, R. J.
Valiquet, H. H.
Vernon, J. R.
Volk, G. H.
Volk, J. H.
Weimer, F. G.
Werwath, K. O.
Wesley, E. D.
Williams, D. D.
Wolfe, J. S.

Neenah—
Angermeyer, A. H.
Eiss, R. M.
Keyes, M. W.
Pasek, L. E.

Oshkosh—
Hoger, B. E.

Racine—
Brinen, H. F.
Desmond, O.
Dixon, A. G.
Dunn, A. N.
Jena, F. T.
Johnson, R. L.
Menden, P. J.
Oravetz, J. A.
Rheault, W. E.
Spieth, B.

Sheboygan—
Kleikamp, H.
Kuck, T. A.

South Milwaukee—
Hoar, R. S.

Superior—
Jarvis, G. E.

Thiensville—
Randolph, C. H.
Trostel, O. A.

Waukesha—
Hill, N. E.

Wausau—
Soronen, R. C.

Wauwatosa—
Eicholtz, M. V.
Peters, H. H.
Wendt, W. R., Jr.

Whitewater—
Colby, J. W.
Fullerton, L. I.

WYOMING

Cheyenne—
Brickham, N. H.
Cook, W. L.

Evanston—
Cazin, G.

Laramie—
Johnson, H. H.
Lindahl, E. J.

Sheridan—
Shaver, C. W., Jr.

HAWAII

Honolulu—
Adams, E. F.
Conger, H. L.

Lanikai—
Holman, E. L.

Pearl Harbor—
Trenhaile, D. T.

Wahiawa—
Wong, K. F.

PUERTO RICO

San Juan—
Saleva, G.

DOMINION OF CANADA

Ajax, Ont.—
Wardell, A.

Brandon, Man.—
Yates, R. A.

Calgary, Alta.—
Deeves, E. W.
Jenkins, S. D.
Sedgwick, S. W.

Chatham, Ont.—
Hill, H. G.

Chippawa, Ont.—
Mole, H. W.

Cooksville, Ont.—
Long, D. A.

Edmonton, Alta.—
Ball, F. T.
Barry, W. W.
Lees, W. D.
Panar, D.

Freeman, Ont.—
Goodram, W. E.

Galt, Ont.—
Caldwell, W. C.
Dowler, E. A.
Sheldon, W. D., Jr.
Thompson, F.

Gananoque, Ont.—
Gurney, E. R.

Halifax, Nova Scotia—
Hagen, G. M.
Meagher, A. T.

Hamilton, Ont.—
Dickenson, M. E.
Fitzsimons, R. H.
Pollitt, S. H.

Hampstead, Que.—
Montgomery, E. G.
Wright, J.

Islington, Ont.—
Smith, W. H.

Kitchener, Ont.—
Farago, W. J.
Peacock, W. H.
Pollock, C. A.
Schnurr, W. J.

Lambton P. O., Ont.
Kennedy, A. M.

Leaside, Ont.—
Barrett, C. M.
Evans, W. H.
Miller, W. W.
Norton, J. A.
Simpkins, A. C.

London, Ont.—
Allen, W. T.
Wood, A. W.

Midland, Ont.—
Kitchen, W. H. J.

Montreal, Que.—
Andrews, W. R.
Anglin, T. G.
Baker, J.
Ballantyne, G. L.
Baxter, W. E.
Becker, S. J.
Blatherwick, H. E.
Booth, C. A.
Champagne, A.
Chenevert, J. G.
Cockman, T. E.
Colford, J.
Colle, S. S.
Darling, A. B.
Dufault, F. H.
Dupuis, J. E. R.
Dykes, J. B.
Ferguson, W. N.
Fitzsimons, J. P.
Flanagan, J. B.

Forrester, N. J.
Friedman, F. J.
Gingras, G. C. J.
Gittleson, H.
Grossman, R.
Hamlet, F. A.
Hole, W. G.
Hood, L. A.
Hooper, F. W.
Horsburgh, A. E.
Horsburgh, B. J.
Hughes, J. W.
Hughes, W. U.
Hutchison, A.
Ilovitch, E. L.
Jockel, H. C.
Keith, J. P.
Kennedy, L. K.
Ker, R. J.
Lajoie, J. R.
Leggett, R. J.
Lewin, J.
Libby, R. S.
Lindsay, D. L.
Linton, J. P.
Lowe, S. C.
Lynes, G. K.
MacDermot, S. G.
MacQueen, D.
Madden, A. B.
Martin, R.
McDonald, I.
Monahan, M. B.
Montgomery, E. L.
Morrison, M. M.
Nathanson, M.
Nickle, A. J.
Noyes, R. R.
O'Connell, T. D.
Orr, W. J.
Osborne, G. H.
Parizeault, J. A. R.
Peart, A. M.
Perras, G. E.
Phillips, C. R.
Phipps, F. G.
Pineau, M. E.
Plamondon, S. R.
Ross, J. D.
St. Laurent, G.
Salter, S. W.
Shaw, J. A.
Sheppard, F. A.
Simpson, C. E.
Singer, G. G.
Smith, G. E.
Smith, R. W.
Standring, R. A.
Storey, J. H.
Terrance, E. H.
Timmins, W. W.
Tolhurst, G. C.
Toupin, V.
Trodd, E.
Twizell, E. W.
Walford, L. C. A.
Watkinson, G. H.
Wells, E. E.
Wiggs, G. L.
Wilkinson, A.
Williams, W. E.
Wilson, J.
Worthington, T. H.

Mt. Royal, Que.—
Clapperton, R.
Moore, A. G.

Oakville, Ont.—
Savage, S. W.
Stott, F. W.

Ottawa, Ont.—
Allen, A. W.
Colclough, O. T.
Dumont, V.
Gray, G. A.
Kent, A. D.
McGrail, T. E.
Pennock, W. B.
Schoenherr, E. J.
Stotesbury, B.

Pointe Claire, Que.—
Garneau, L.

Port Dalhousie—
Kingdon, F. W.

Preston, Ont.—
Everest, R. H.

Quebec, Que.—
Mulroney, G. J.
Paquet, J. M.
Truchon, L. P.

Regina, Sask.—
Daniels, D. D.

Sackville, N. B.—
Baxter, A. G.
Etter, N. W. P.
Hand, F. R.
Johns, C. F.

St. Catharines, Ont.
Gilbert, T.
Peterkin, S. M.

St. Hilaire, Que.—
Forest, L.

St. John, N. B.—
Thomas, F. A.

St. Laurent, Que.—
Lamontagne, A. F.
Watts, A. E.

Ste. Therese De Blainville, Que.—
Winters, H. G.

Sherbrooke, Que.—
Archambault, J. A.
Codere, J. M.
Savoie, J. L. R.

Sorel, Que.—
Chauvin, J. P.

Thorold, Ont.—
Calnan, E. J.

Timmins, Ont.—
Degilio, L.

Toronto, Ont.—
Abbott, T. J.
Adams, R. R.
Alexander, S. W.
Allsop, R. P.
Angus, D. L.
Angus, H. H.
Anthes, L. L.
Arrowsmith, J. O.
Bailey, M. C.
Baird, A. D. G.
Baker, L. P.
Ballach, A. B.
Barker, M. S.
Baxter, H. A.
Beavers, G. R.
Bellman, J. V.
Belyea, R. E.
Bevan, J. H.
Blackhall, W. R.
Blake, A. H.
Bowman, M. K.
Brittain, A., Jr.
Butler, D. H.
Butler, P. M.
Carter, A. W.
Casperd, H. W. H.
Chambers, F. W.
Christie, J. A.
Church, H. J.
Clapperton, T. C.
Clark, A. E.
Clark, A. M.
Clark, A. M.
Clifton, J. A.
Cochrane, R. L.
Cole, G. E.
Collins, J. W.
Connor, W. A.
Crump, S.
Darling, J. W.
Davis, E. J.
Delany, W. F.
Dickey, A. J.
Dion, A. M.
Dixon, M. F.
Dunn, R.
Eaton, W. G. M.
Edwards, A. F.
Ellis, F. E.
Elms, W. P.
Elsie, R. L.
English, G. A.
Ewens, F. G.
Ferris, A. L.
Fisher, S. L. V.
Fleming, J. G.
Foley, J. J.
Fox, E.
Fox, J. H.
Gordon, C. W.
Graham, W. F.
Gretton, J. D.
Gurney, E. H.
Hatch, G.
Henion, H. D.
Hewett, R. E.
Hills, A. H.
Hooper, F. C.
Hopkins, R.
Hopper, G. H.
Hughes, L. K.
Isserstedt, S. G.
Jenkinson, V. J.
Jenney, H. B.
Jennings, S. A.
Jones, A. T.
Kelly, F. C.
Kerr, R.
Kingsland, N. W.
Kinsinger, R. E.
Labadie, W.
Larter, E. A.
Lawlor, J. J.
Ledgett, F. D.
Leitch, A. S.
Leitch, K. D.
Lock, R. H.
Loftus, R. G.
Lynde, C. J., Jr.
Lyons, E. C.
MacDonald, D. J.
MacGregor, D. K.
Madely, F. J.
Mansell, G. R.
Marriner, J. M. S.
Martin, R. J. W.
Mathison, R. S.
Maxwell, R. S.
McGruer, A. E.
McKernan, G. S.
McLaren, T. H.
Monteith, E. M.
Moore, H. S.
Morgan, A. S.
Murray, H. G. S.
Napier, C. E.
Nearingburg, A.
Neilans, J. L.
O'Marra, W. W.
O'Neill, J. W.
O'Neill, J. F.
Orr, J. D.
Paul, D. I.
Petrinec, J. R.
Philip, W.
Playfair, G. A.
Powers, R. E.
Price, D. O.
Pritchard, H. T.
Ramsey, R.
Reed, A. G.
Ritchie, A. G.
Robinson, J. H.
Ross, J. H.
Roth, H. R.
Roy, R.
Russell, J. R.
Sale, G. N.
Seymour, C. D.
Shears, M. W.
Simpson, H.
Smith, N. A.
Spall, E. G.
Steeves, D. R.
Stencel, R. A.
Stott, D. A.
Strain, A. J.
Tait, A.
Taylor, A. R.
Taylor, F. W.
Thomas, M. F.
Thompson, J.
Todd, M. M.
Torry, C.
Treleaven, H. M.
Trickey, G.
Turnbull, E. R.
Usher, W. J., Jr.
Waldon, C. D.
Ward, D.
Watson, M. B.
West, L. C.
White, A. A.
White, J. A.
Williams, C. R.
Wolfe, J. S.
Woollard, M. S.
Wormley, R. F.
Wylie, W. J.

Trois-Rivieres, Que.
Germain, O.

Val Morin, Que.—
Davidson, J. W.

Vancouver, B. C.—
Bishop, A. H.
Clemens, J. D.
Godfrey, G. A.
Hale, F. J.
Johnston, R. E.
Leek, C. W.
Leek, W.
Minaker, M. E.
Ross, K. A.
Turland, C. H.

Victoria, B. C.—
Sheret, A.

West Kildonan, Man.
McKay, W. H.

Westmount, Que.—
Cambridge, W. A.
Lefebvre, E. J.
Watson, C. E. W.

Windsor, Ont.—
Hare, W. A.
Johnson, C. W.
Kearn, J.

Winnipeg, Man.—
Anderson, E.
Argue, E. J.
Atkinson, W. J.
Bell, J. A.
Bertram, J. F.
Charles, P. L.
Chester, F. L.
Dahlgren, G. E.
Davis, G. C.
Davis, J. C.
Finch, L.
Glass, R.
Glass, W.
Hatch, O. J.
Hepburn, E. M.
Kent, R. L.
Lambert, E.
Lush, C. N.
McCallum, A. W.
Michie, D. F.
Miller, E. R.
Moore, R. E.
Moss, A. W.
Narvey, S.
Piercy, A. K.

Price, E. H.
Randall, G. E.
Saunders, D. G.
Steele, J. B.
Stephenson, J. R.
Swain, D. S.
Swan, D.
Weir, F. F.
Worton, W.

Woodbridge, Ont.—
Powlesland, J. W.

Woodstock, Ont.—
Karges, A.

ARGENTINA

Buenos Aires—
Guibert, R.
Gundersen, R.
Jalles, A. R.
Lang, G. T.
Lix-Klett, L.
MacLean, I. R. S.
Tarak, H. H.

Santa Paula—
Costa, C. A.

Vicente Lopez—
del Campo, E

AUSTRALIA

Melbourne—
Atherton, A. E.
Bell, S. R.
Ross, R.
Scott, P. R.

Sydney—
Davey, G. I.
Dye, O. E.
Moloney, R. R.
Robinson, J. A.
Roseby, T. A.
Smith, G. E.

Thornbury—
Williams, F. K.

Waterloo—
Henderson, A. S.

BELGIUM

Auderghem-Brussels
Wanson, L. J.

Brussels—
Herman, M.
Lebrun, P.

BERMUDA

Somerset Bridge—
McCormack, D.

BRAZIL

Rio de Janeiro—
Botelho, N. J.
DeSales, M., Jr.
Doremus, L. A.
Rabe, A. E.
Somers, W. S.

Sao Paulo—
Bowles, J. R.
Hall, R. S.

CANAL ZONE

Quarry Heights—
Kinzer, O. A.

CENTRAL AMERICA

Nicaragua—
Cardenal A., L. G.

CHILE

Santiago—
Aranda, A.
Bloj, C.

CHINA

Hongkong—
Carter, D.

Shanghai—
Hutchinson, F. A.
Kwan, I. K.
Loh, N. S.
Loo, P. Y.
Melnikoff, C. G.
Muckle, J. M.
Waung, T. F.
Wong, W. S. B.

CUBA

Havana—
Amezaga, M. F.
Cadenas, M. A., Jr.
Colmenares, G. V.

DENMARK

Copenhagen—
Jespersen, S. F.
Reck, W. E.
Varming, J.

DOMINICAN REPUBLIC

Ciudad Trujillo—
Freites, A. A.

EGYPT

Cairo—
Brakha, M. V.
Eid, A. K.
El Attar, A. A.
Elsarky, A.
Ezz-El-Din, K.
Gad, A.
Girgis, S.
Habashi, F.
Kasparian, E.
Saleh, M.
Tahry, M. E.
Zaki, H. M.

ENGLAND

Ashton-Under-Lyne-
Sutton, G.

Banstead—
Saunders, S. G.

Birmingham—
Colton, F. R.
Cupitt, R.
Greenland, S. F.
James, W. B.
Otter, R. E.
Shilston, R. A.
White, F. R. L.

Bristol—
Whitaker, K. L.
Woffenden, H.

Bury—
Baker, H. E.

Bushey—
Greatorex, J. E.

Cheltenham—
Smith, B.

Dartford—
Pasteur, H. W.

Egham—
Happerfield, G. J.

Evesham—
Bawden, L. A.

Gerrards Cross—
Russell, J. N.

Greenford—
Fraser, J. J.
MacLachlan, V. D.

Harpenden—
Smith, D. V. H.

Harrow—
Case, W. G.
Jones, S. J.
Pearce, E. A.
Smith, W. E.

Heston—
Eamer, M. B.

Leeds—
Frean, F. C.
Richardson, R. D.

Leicester—
Gouldbourne, T. H.
Smith, E. H.
Snow, E. E.

London—
Benham, C. S. K.
Binns, A. J. H.
Bird, G. L. H.
Butt, R. E. W.
Daniel, W. E.
Gardner, R. A.
Grocott, J. F. L.
Haden, G. N.
Heard, J. A. E.
Heathcote, H. J.
Herring, E.
Horne, L. N.
Jackson, G. R.
Kennett, V. A.
Kindler, S.
Meyer, J. J.
Morrison, C. B.
Myers, A. F.
Nobbs, W. W.
Pinkerton, J. B.
Russell, E. N.
Smith, A. J.
Stevens, S. A.
Swain, W. L.
Thompson, I. J.
Troup, J. D.
Watts, L. C.
Whyte, F. J.

Luton—
Thacker, J. E.

Malden—
Chatfield, A. K. J.

Manchester—
Chadwick, J. B.
Merritt, C. J.
Poughee, B. R. E.
Sealy, S. I.
Ward, C. V.

Mottram in Longdendale—
Addie, G. R.

North Holmwood—
Murray, G. F. J.

North Wembley—
Eldred, H.

Nottingham—
Phillips, E. G.

Reading—
Hole, K. W.

Reigate—
Mann, W. N.

Rotherham—
Wilson, T. B.

Ruislip Manor—
Hadley, L. G.

St. Albans—
Davies, A. T.
Kell, J. R.

Sevenoaks—
Jarrett, R. F.

Sidcup—
Taylor, E. L.

Solihull—
How, C. P.

Stanmore—
Harvey, J. W.

Stockport—
Longworth, A. L.
Wild, H.

Wallington—
Harding, W.

Watford—
Purdue, F.

West Ewell—
Henton, L. W. J.

West Wickham—
Lipscombe, H. W. J.

Worsley—
Yates, W.

FRANCE

Asnieres (Seine)—
Touzard, P. M. A.

Paris—
Cartier, M. E.
Delalande, A.
Desplanches, A.
Jouanno, E. P.
Modiano, R.
Parodi, H.
Tunzini, B.

Sucy en Brie—
Beaurrienne, A.

Vanves (Seine)—
Ghillardi, F.

HOLLAND

Haarlem—
Hamaker, H. J.

Noordwijk aan Zee—
De Wilde, M. P.

INDIA

Bombay—
Char, R. D.
Duplant, J. L.
Henenfeld, H.
Neuman, S. I.

Calcutta—
Bechir, N. V.
Ghose, K. N.
Ghosh, B. B.
Mallik, J. R. B.
Sarkar, S. R.

Madras—
Manivelu, M.

IRAN

Abadan—
Baghi, A. R. M.

Teheran—
Badhni, J.

IRELAND

Belfast—
Campbell, S.

Dublin—
Leonard, L. C. G.

ITALY

Milano—
Gini, A.
Marzorati, G.
Santagostino, M.

MEXICO

Churubusco—
Huber, E.

Mexico—
Gilfrin, G. F.
Hammeken, L. P.
Ramoneda, E.
Rodriguez, M. F.
Tejeda, S. M. M.
Valdez, A.
Veraza, U. C.
Westendarp, F. G.

NETHERLAND WEST INDIES

Aruba—
Groom, J. W., Jr.

Curacao—
Correa, B. A.

NEWFOUNDLAND

St. Johns—
Bishop, F. W.
Ryan, F. J.

NEW ZEALAND

Auckland—
Cooke, W. L.
Taylor, H. J.

Christchurch—
Rastrick, R. J.
Rind, K.
Taylor, E. M.
Vale, H. A. L.

Dunedin—
Davies, G. W.

Wellington—
Vamos, G.

NORTH AFRICA

Algiers—
Macherel, F.

NORWAY

Oslo—
Alfsen, N.
Tjersland, A.

NOVA SCOTIA

Halifax—
MacDonald, E. L., Jr.

PHILIPPINE ISLANDS

Manila—
Hausman, L. M.

PORTUGAL

Lisbon—
Potier, O. N.

SOUTH AFRICA

Cape Town—
Bowie, R.
Daitsh, A.
Ross, B. W.

Claremont Cape Point—
Flagg, W. J.

Durban—
Blase, T. F.
Christierson, C. A.

Johannesburg—
Adams, T. K.
Allen, M. H. P.
Caldwell, R. J. S.
Goodman, J.
Gordon, H. H. W.
Kemsley, J. A.
Posthuma, J. A. L.
Sibert, A.
Swartzberg, J.
Thompson, A. E.
Windsor, W. G.

Kroonstad—
Grobler, P. S.

Salt River—
Ehlers, J.

SOUTH WALES

Glamorgan—
Arnold, C. J.
Brooke, B. B.

SPAIN

Madrid—
Alfageme, B.

SWEDEN

Appelviken—
Theorell, A. T.

Gustavsberg—
Wollrik, H. V.

Nockeby—
Eriksson, H. A.
Gille, H. B.

Stockholm—
Aminoff, E.
Capron, R. G.
Eklund, K. G.
Ostrom, E. W.
Rosell, A. F.
Rydberg, J. A.
Wrene, T.

SWITZERLAND

Baisthal-So—
Koenig, M. E. R.

Basel—
Bauer, J.

Geneva—
Goerg, R. A.

Zurich—
De Bruyn, L. F.
Hausler, W.

TURKEY

Istanbul—
Karakash, T. J.
Uran, N. F.
Veglery, A. G.

URUQUAY

Montevideo—
Varela, J. A.

VENEZUELA

Caracas—
Blas, R. J.